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# Extraction of strategically important elements from brines: Constraints and opportunities

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#### Abstract

Strategically important elements are those that are vital to advanced manufacturing, low carbon technologies and other growing industries. Ongoing depletion and supply risks to these elements are a critical concern, and thus, recovery of these elements from low-grade ores and brines has generated significant interest worldwide. Among the strategically important elements, this paper focuses on rare earth elements (REEs), the platinum-group metals and lithium due to their wide application in the advanced industrial economics. We critically review the current methods such as precipitation, ion exchange and solvent extraction for extracting these elements from low-grade ores and brines and provide insight into the technical challenges to the practical realisation of metal extraction from these low-grade sources. The challenges include the low concentration of the target elements in brines and inadequate selectivity of the existing methods. This review also critically analyzes the potential applicability of an integrated clean water production and metal extraction process based on conventional pressure-driven membrane and emerging membrane technologies (e.g., membrane distillation). Such a process can first enrich the strategically important elements in solution for their subsequent recovery along with clean water production.

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## **Research Highlight**

- ✤ Recovery of strategically important elements from brines is reviewed.
- ✤ Challenges associated with separation processes for metal extraction are discussed
- Membrane distillation is effective to recover strategically important elements
- ✤ Critical challenge associated with membrane processes is fouling.

# Extraction of strategically important elements from brines: constraints and opportunities

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#### Abstract

Strategically important elements are those that are vital to advanced manufacturing, low carbon technologies and other growing industries. Ongoing depletion and supply risks to these elements are a critical concern, and thus, recovery of these elements from low-grade ores and brines has generated significant interest worldwide. Among the strategically important elements, this paper focuses on rare earth elements (REEs), the platinum-group metals and lithium due to their wide application in the advanced industrial economics. We critically review the current methods such as precipitation, ion exchange and solvent extraction for extracting these elements from low-grade ores and brines and provide insight into the technical challenges to the practical realisation of metal extraction from these low-grade sources. The challenges include the low concentration of the target elements in brines and inadequate selectivity of the existing methods. This review also critically analyzes the potential applicability of an integrated clean water production and metal extraction process based on conventional pressure-driven membrane and emerging membrane technologies (e.g., membrane distillation). Such a process can first enrich the strategically important elements in solution for their subsequent recovery along with clean water production.

**Keywords**: Strategically important elements, challenges, low-grade ores and brines, emerging membrane process.

#### 1. Introduction

Recent technological advances are mostly based on innovative applications of a range of rare metals and metalloids into intelligent and high-tech devices. Examples include rare earth metals (e.g., cerium, lanthanum, neodymium, dysprosium, praseodymium, scandium, erbium, europium, terbium and yttrium), precious metals (e.g., rhodium, palladium, and platinum), radioactive metals (e.g. uranium and radium) and alkaline metals (e.g., magnesium, potassium, and lithium). These elements are indispensable in the electronic and electrical industries (Alonso et al., 2012), making them some of the most valuable non-renewable resources for our modern society. For example, the production of a smartphone requires a range of rare earth metals including neodymium, gadolinium and samarium along with others metals, such as lithium, indium, palladium, tantalum, silver, gold, copper, gallium, germanium, beryllium, and zirconium (Tanskanen, 2013). However, increasing depletion of some of these elements has been revealed as a major risk to viable economic development.

To date, most metals are produced from hard-rock mining. During the last two decades, advances in water purification (e.g., desalination) and resource recovery have led to the concept of seawater and brine being perceived as important untapped sources of precious and rare earth elements (Bardi, 2010; Gibert et al., 2010; Lee et al., 2013; Saito et al., 2006). It is also notable that these elements can cause severe environmental pollution due to their toxicity. Thus, the challenge to conserve these rare metals and metalloids and to protect the environment has strategically spurred the need to extract and recover them from complex solutions.

The main technologies used for producing metals from low-grade ores and brines are based on precipitation, ion exchange and hydrometallurgical processes. The ion exchange process is a selective process which requires a specific resin to recover valuable metals selectively. Hydrometallurgical treatments are based on the use of leaching agents in aqueous solutions such as strong acids and bases. These are often applied together with other complexing agents such as oxalic acid, cyanide, halide, acetic acid and thiosulfate (Beolchini et al., 2010). Given the techno-economic analysis, the technological challenges of the mentioned processes and the low levels of elements concentration have received attention. Hence, a cost-effective, low energy consuming and greener-recycling process needs to be developed to handle the challenges associated with next-generation metal demand and to conserve natural resources. Membrane-based technologies may provide a viable solution for efficient recovery of rare earth elements from brine as these processes can easily enrich the elements effectively.

This article critically discusses the opportunities and challenges of strategically important element recovery from low-grade ore and brine solution using conventional and emerging technologies. In terms of the strategically important elements, this paper focuses on the extraction of rare earth elements (REEs), the platinum-group metals and lithium due to their wide application in the advanced industrial economics. We conclude this article by providing an outlook of the opportunities for the separation of strategically important elements using integrated conventional and emerging membrane-based technologies. Wherever available, information on pilot or full-scale facilities in addition to lab-scale studies has been systematically presented. Information on the technology readiness level and economic feasibility is a notable gap in the literature.

#### 2. Strategically important elements

A range of chemical elements is strategically important to modern life. Indeed, they are essential in many everyday products ranging from mobile phones to automobiles. The emerging renewable energy market also utilises many of these elements (Figure 1). Among them, three of the most notable groups are rare earth elements (REEs), the platinum-group metals, and lithium. Although the application of these elements is often not well known to the general public unfamiliar with the industrial processes, the current rate of consumption of many of these strategically important elements is not sustainable.

REEs are probably the strategically important elements of the most critical concern, given their applications in emerging technologies including fuel cells and wind turbines (Figure 1) but uncertain future supplies. Over 500 kg of REEs including neodymium, molybdenum, and dysprosium (Figure 1) are required to make the permanent magnets in a single 3.5 MW wind turbine (Constantinides, 2016). Since the growth in wind power markets is expected to continue, the demand for neodymium magnets (NdFeB) in wind turbines in 2020 is expected to be increased to approximately 13.2 kilotons, which is about 1.7 times higher compared to the NdFeB amount required in 2015 (Pavel et al., 2017). If magnet composition remains invariable, about 3.2 kilotons of neodymium, 0.8 kilotons of praseodymium and 0.93 kilotons of dysprosium would be requested by the global wind power sector in 2020. This is equivalent to 15%, 13% and 66% of the total production of neodymium, praseodymium and dysprosium, respectively in 2014 (Pavel et al., 2017). A NdFeB magnet now incorporates 29-32% neodymium/praseodymium, which might decrease to 25% by 2020 and even further to 20% by 2030 (Lacal-Arántegui, 2015). Instead of using magnets with 3-6% dysprosium, newer generator models can use permanent magnets with only about 1% dysprosium. Pathak et al. (2015) claim to have developed a new way to replace dysprosium fully and neodymium partly (by about 20%) in the NdFeB magnet using cobalt and cerium (much cheaper and more available REE). The cerium and cobalt co-doped alloy shows excellent high-temperature magnetic properties. Terbium can replace dysprosium in a NdFeB magnet, but it is not considered a convenient substitute today. If terbium becomes cheaper than dysprosium, e.g. due to decreasing terbium demand in lighting (Pavel et al., 2016), it could be used as a substitute for some quantities of dysprosium in magnet applications.

Currently the world reserves of REEs in major countries such as China, Brazil, Vietnam, Russia and India stand at about 130 million tonnes (USGS, 2019). It is noted that the REEs reserve is not uniformly distributed globally. Most of the confirmed REE reserve is in China, which produces 85% of the global REEs output (Roskill, 2015). The current annual global production of REEs is about 120 kilotons (Izatt et al., 2016), yet the demand for REEs is expected to grow further as the renewable and electronic industries continue to expand. The annual growth rate of global REE demand is estimated to be about 5% (USGS, 2016). A similar prediction was made by Dutta et al. (2016) who noted that global REE demand is slated to grow at an annual rate of 5% by 2020. Graede (2015) indicated that there would be scarcity and supply risk for europium, dysprosium and erbium in addition to several other metals in the near future. This estimation is based on their scores in three areas, namely supply risk, environmental implications, and vulnerability to supply restrictions. Hence, the global availability of REEs appears to be at substantial risk for several reasons. These include the introduction of production quotas, export quotas and export taxes, enforced environmental legislation, and granting no new rare earth mining licenses (USGS, 2019). As a result, there has been increased interest and investigation into non-traditional REE resources, extraction, separation and purification processes.

The demand for platinum-group elements is likely to increase due to increasing demand for vehicles globally in the forthcoming decades. In 2016, the automobile industry continued to be the major consumer of platinum-group elements which accounted for approximately 84% of global rhodium consumption, 67% of palladium consumption and 46% of platinum consumption (CPM Group, 2017). Loferski (2011) noted that each year, the automobile industry alone uses 113 tons of platinum and other platinum-group metals as catalysts for air pollution control. Jollie (2017) predicts compound annual growth rates (CAGRs) of total platinum and palladium demand of 1.0 and 1.1%, respectively. An economic model by Zhang et al. (2016) shows a growth in the demand for platinum and palladium of approximately 5% and 45%, respectively over the next 15 years. This growth in demand for the platinum-group metals is driven largely by the increasing automobile sales, particularly in emerging markets such as China and India. The platinum-group metals are also essential for catalytic conversion in fuel cells. Thus, an even more significant increase in the demand for these metals is expected if fuel cell automobiles can be mass-produced in the future (Wittstock et al., 2016).

The current recoverable reserve of platinum-group metals of about 100 kilotons is geographically unevenly distributed. South Africa has about 80% of the global reserve of platinum-group metals and the remaining is in Russia (8%) and Zimbabwe (7%) (IDC, 2013). Notably, most of the world's supply of platinum-group elements comes from South Africa and Russia, which account for 56% and 24%, respectively, of the global production (USGS, 2019). The total worldwide supply in 2013 was 187.9 tons for platinum, 206.7 tons for palladium, and 22.1 tons for rhodium (Johnson, 2014). In comparison, the supply of platinum-group elements in 2000 was 153 tons for platinum, 224 tons for palladium and 20.9 tons for rhodium (Johnson, 2001). This reflects the growing worldwide use of platinum-group

elements. By contrast, Thormann et al. (2017) reported that the global platinum and palladium production decreased by 25% and 8%, respectively from 2010 to 2014. The decline observed throughout this period was mainly due to a consequence of the strikes in South Africa. According to Thormann et al. (2017), future estimates of demand, production and recycling, based on CAGRs of 0.4, 1.7 and 3.3% for primary production, recycling and demand of platinum, respectively, indicate a supply gap in the near future. The competition to obtain these elements has also led to geopolitical tension and instability.

Lithium is another notable strategically important element that is essential for rechargeable batteries (Figure 1). Due to the recent boom in the renewable energy industry and electric vehicles, lithium consumption for batteries has increased significantly in recent years. Lithium demand is expected to grow faster than supply in the coming decade. Martin et al. (2017) estimate an annual increase in lithium demand of 9% over the next 3 years.



**Figure 1:** Examples of strategically important element demand (kg/MW) in the renewable energy industry (Moss et al., 2011; Moss et al., 2013; Teske et al., 2016).

The supply security of strategically important elements to support our modern society depends not only on their geological deposits but also the availability of separation technologies for their extraction. The latter is particularly important in the context of the future circular economy when these elements are sourced from consumer products at the end of their lifetime rather than geological deposits. As a major exporter of many minerals, Australia is a notable example of the interplay between the availability of geological deposits and separation technologies. Australia provides 8% of the global REEs production (Skirrow et al., 2013) despite having a rather modest reserve of these elements. Australia is currently the world largest lithium producer with 34% of the global production (Table 1). Yet, in terms of geological availability of lithium, Australia is only ranked fourth in the world after China, Argentina, and Chile (USGS, 2016). It is noteworthy that Australia has many salt lakes and saline groundwater deposits that contain a range of strategically important elements (Timms, 2005).

In the current hydrometallurgical industry, processes for the separation/ extraction of strategically important elements are precipitation, ion exchange and solvent extraction. A major challenge of these processes is separation selectivity (Izatt et al., 2016). Hence, a pragmatic approach is important to recover these strategically important elements from low-grade sources including salt lake brines.

**Table 1**: The production, resources and reserve status of some prospective elements in Australia and their application for different purposes

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2	

# (Hoenderdaal et al., 2013; Skirrow et al., 2013; USGS, 2016)

3

Metals	Production		Resource		Reserve		Applications		
	Mass	<b>Global share</b>	Mass	<b>Global share</b>	Mass	<b>Global share</b>			
	(kt)	(%)	( <b>kt</b> )	(%)	(kt)	(%)			
Cerium	7.6	8	1481	3	NA	2.8	Catalytic converters in cars, hybrid vehicles, television		
							faceplates, silicon microprocessors.		
Lanthanum	4.6	8	742	3	NA	2.8	Cracking catalysts in petroleum refining, camera lenses,		
							battery electrodes, hydrogen storage, x-ray films.		
Dysprosium	0.115	4.8	NA	NA	8	0.64	Motors or generators, wind turbines, and electrical		
							vehicles, hard disk devices, transducers.		
Yttrium	NA	NA	100	18.5	NA	NA	Microwave generators, televisions and computer		
							screens, ceramics, superconductors.		
Platinum	0.22	0.11	2.35	1.2	NA	NA	Catalytic converters, electronic application, fuel cells		
Palladium	0.22	0.11	2.35	1.1	NA	NA			
Lithium	11.7	34	1006	8	1500	10.7	Electric batteries, cordless devices, ceramics, glass.		

4 NA: Not available

# 6 3. Key challenges associated with separation processes for strategically important 7 elements recovery

8 Low concentration and co-occurrence with other elements of much higher concentration, 9 processing cost and environmental impacts are major challenges to the cost-effective 10 recovery of strategically important elements from low-grade ores and brines. The significance 11 of these challenges depends on the source of brine. The high amount of water and energy 12 consumed in producing these elements also makes the separation process inefficient.

13

14 Strategically important elements often occur at low concentrations in low-grade ores and brines, and, thus, are difficult to recover in the presence of much higher concentrations of 15 other minerals which can interfere with the separation and enrichment process. Hu et al. 16 17 (2018) noted that the selective extraction of scandium was limited by the presence of other REEs, aluminium and iron. Similarly Barros et al. (2019) reported that the recovery of REE 18 was affected by the competition of other base metals present in the brine solution. Callura et 19 20 al. (2018) noted that the presence of competing ions (calcium, magnesium, zinc, iron and aluminium) could inhibit the complete recovery of REEs. The undesired elements such as 21 22 phosphate, iron, aluminium, nickel, chromium, manganese, zirconium, uranium and copper were first separated to reduce the impurities during REEs recovery in a week acidic medium 23 24 using oxalic acid (El-Awady, 2013). Safarzadeh et al. (2018) noted that nickel, copper and 25 cobalt need to be removed to achieve 99.9% purity of platinum group elements. SepraMet is a metal refinery located in Houston, Texas, which features the use of molecular recognition 26 technology-hydrometallurgical processes in the selective recovery of platinum group elements 27 28 from low-grade ores (Izatt et al., 2015). They noted that the unwanted or deleterious elements such as arsenic, iron and antimony need to be separated effectively for the target platinum group 29 30 elements recovery.

The level of lithium (0.06-1.21 g/L) in brine can be significantly low compared to magnesium 32 ion (3.4-113.7 g/L) (Table 2). The extraction efficiency of lithium depends on the 33 34 magnesium to lithium mass ratio (Table 2). A low magnesium to lithium (Mg/Li) ratio in brine means that it is easier, and therefore more economical to extract lithium. Zhao et al. 35 (2013) noted that when the Mg/Li ratio is below 6, lithium can be effectively separated by 36 37 chemical precipitation method. However, the Mg/Li ratio of most brines is higher than 6 (Table 2). Therefore, the use of an appropriate treatment process (e.g., nanofiltration) for 38 39 avoiding their interference with the crystallisation of lithium carbonate is essential to remove magnesium ion. 40

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42 Purity is an important parameter that is directly related to how strategically important 43 elements can be used and their commercial value. For example, over 99.9% purity of lithium 44 carbonate is required for the production of lithium-ion batteries (Virolainen et al., 2016). On 45 the other hand, lithium carbonate with purity below 99.6% can only be used for ceramic 46 production (Virolainen et al., 2016).

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Similar physiochemical properties of some strategically important elements can affect the separation of the target element. Most REEs occur together in mineral deposits and therefore separation of them from each other is quite difficult due to similar ionic radius and chemical properties (Cardoso et al., 2019). For example, related to the aforementioned example of separation of lithium from magnesium, magnesium too precipitates with lime as magnesium carbonate, which prevents the formation of lithium carbonate (Kogel, 2006).

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5	6
5	7

 Table 2: Composition of lithium in salt lake brine around the world

Source	Status			Concentration (g/L)					Impurities	References
		$Li^+$	$Mg^{2+}$	$Na^+$	$Ca^{2+}$	$\mathbf{K}^+$	В	<b>SO</b> 4 <sup>2-</sup>	-	
Atacama Salar Brine, Chile	Full-scale	3.02	17.6	61.9	0.41	28.2	1.72	37.9	Na <sup>+</sup> , K <sup>+</sup> , M $^{2^+}$	Ogawa et al. (2014)
Uyuni Salar Brine Bolivia		0.84	16.7	105.4	3.33	15.7	0.7	21.3	$Na^+, K^+, B$	An et al. (2012)
East Taijinar, China	Pilot-scale	0.14	5.64	117.03	0.43	3.79	-	-	Na <sup>+</sup> , K <sup>+</sup> ,	Sun et al. (2015)
West Taijinar, China		0.26	15.36	102.4	0.19	8.44	-	-	Na <sup>+</sup> , K <sup>+</sup> ,	Sun et al. (2015)
Chott Djerid Salt Lake, Tunisia		0.06	3.4	80	1.6	5.6	-	6.7	Na <sup>+</sup> , Ca <sup>2+</sup> , Mg <sup>2+</sup>	Somrani et al. (2013)
Longmucuo, China		1.21	89.5	-	-	-	-	-	-	Song et al. (2017)
North Arm Salt Lake, USA	Lab-scale	0.04	9.38	100.8	0.35	5.5	0.03	19.7	$Na^+$	Bush et al. (2016)
Salt lake brine, China		0.35	113.7	-	-	-	-	-	$Mg^{2+}$	Xiang et al. (2016)
Salt lake brine		0.15	8.88	2.69	-	-	-	-	-	Ji et al. (2017)
Geothermal brine		0.01	-	0.11	-	0.16	0.03	-	<b>K</b> <sup>+</sup>	Mroczek et al. (2015)
Synthetic brine		0.15	63.8	0.414	0.02	0.20		-	$Mg^{2+}$	Nie et al. (2017b)

The cost of the recovery process is an important consideration for the industry. The process 59 can be very expensive when multiple steps are required for the separation of these elements. 60 61 For example, lithium-losses are typically more than 10% in the multiple separation steps 62 (Virolainen et al., 2016). Solvent loss during multiple solvent extraction steps can make an extraction process further uneconomical. For example, using solvent extraction for the 63 separation of niobium and tantalum, evaporation loss of the solvent (i.e., hydrofluoric acid) 64 65 alone was 6-7% (Wang et al., 2010). Multiple separation steps also produce large amounts of secondary chemical waste resulting in high costs associated with their disposal. 66

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Separation processes used for the recovery of strategically important elements often raise 68 environmental concerns. For example, the use of large volume of organic solvents for the 69 70 recovery of these elements has an adverse environmental impact. This is because organic 71 solvents are toxic, corrosive, inherently volatile and flammable (Nishihama et al., 2003). Their volatility and solubility contributes to air, land and water pollution. Yang et al. (2013) 72 73 noted that mining and production processes in China have resulted in the creation of large polluted areas, which are now attracting international attention. Every ton of rare earth metal 74 75 produced generates approximately 8.5 kilograms of fluorine, 13 kilograms of dust, about 75 cubic meters of acidic wastewater and approximately 1 ton of radioactive waste residue 76 77 (Hurst, 2010). Tharumarajah and Koltun (2011) conducted life cycle assessment (LCA) on 78 Bayan Obo deposit in China to determine the equivalent greenhouse gas (GHG) emissions for production for rare earth oxides (REOs). Their analysis shows that the production of 79 samarium, europium and gadolinium oxides emits approximately 55 kg of CO<sub>2</sub> equivalent 80 81 per kg of oxide produced, which is significantly higher than for iron (0.02 kg of CO<sub>2</sub> equivalent) and copper (0.63 kg of CO<sub>2</sub> equivalent (Norgate and Haque, 2010). In a follow 82 83 up study, Koltun and Tharumarajah (2014) found that GHG emissions for light REOs

(lanthanum-, cerium-, praseodymium-oxide) were 32.29 kg CO<sub>2</sub> equivalent per kg of REO,
medium REOs (neodymium-, promethium-, samarium-oxide) were 30.29 kg CO<sub>2</sub> equivalent
per kg of REO and heavy REOs (gadolinium-, yttrium- lutetium and scandium-oxide)
were 34.49 kg CO<sub>2</sub> equivalent per kg of REO.

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#### 89 4. Current separation processes for strategically important elements recovery

90 Various separation processes have been used to extract strategically important elements from low-grade ores and brines. Traditional technology to extract these elements relies on subtle 91 92 differences in their thermodynamic behaviors in the aqueous phase through a series of precipitation and crystallization steps (Bernardis et al., 2005). The process to recover lithium 93 from the Uyuni Salar brine in Bolivia is shown in Figure 2 as an example. The Salar is a salt 94 95 surface crust overlying brine saturated sediment. Following the removal of calcium, 96 magnesium and boron, the concentrated brine can then be purified to remove other residual impurities such as sodium, sulphate and chlorine (An et al., 2012). The lithium concentrate is 97 98 then subjected to carbonation for the precipitation of lithium carbonate with high purity (99.6%). 99

100 Platinum-group metals and REEs are mainly recovered from the ore concentrate through acid leaching. Target elements from the leach solution are then separated by ion exchange or 101 102 solvent extraction processes. For example, the ion exchange process has been used for the 103 separation of platinum-group metals from the low-grade waste stream at Impala Refineries in Springs, South Africa (Figure 3). The concentrate contains about 65% platinum-group metals 104 (Crundwell, 2011). In this full-scale refinery plant, ion exchange, distillation and hydrolysis 105 106 have been used to separate the individual platinum-group metals from the leach solution. Another industrial process for the recovery of strategically important elements is solvent 107 extraction. In the Alwaye Plant in India, the separation of individual REEs from rare earth 108

- nitrate solution is achieved by a solvent extraction process using tri-n-butyl phosphate (TBP)
  (Figure 4). In this process, the feed solution containing rare earth nitrate is produced during
  the chemical treatment of monazite ore.
- 112



114 Figure 2: Flowsheet for the recovery of lithium as carbonate from Uyuni Salar brine, Bolivia

115 (An et al., 2012)



#### 125 **4.1. Precipitation**

Precipitation is commonly used to separate strategically important elements from brines. For 126 example, precipitation of lithium in the form of lithium carbonate from a concentrated lithium 127 solution has been reported previously (Nishihama et al., 2011). However, the high amount of 128 lime consumption for the precipitation of co-occurring magnesium and loss of lithium by co-129 precipitation are major challenges for the application of precipitation process for lithium 130 131 recovery (Chen et al., 2017). Lithium recovery in the form of lithium aluminate from Dead Sea brine and end brine (after potash production) has been reported by several researchers 132 133 (Epstein et al., 1981; Pelly, 1978). Pelly (1978) achieved 90% extraction efficiency of lithium aluminate from both Dead Sea brine and end brine. However, they found that higher 134 temperature has an adverse effect on the extraction efficiency, and the best yield was 135 136 achieved at room temperature (Pelly, 1978). Another study by Epstein et al. (1981) focused on lithium extraction from the Dead Sea brine by precipitation as lithium aluminate followed 137 by liquid-liquid extraction to separate the lithium from aluminium. Notably, evaporation-138 precipitation process has been used as the industry standard commercial process for lithium 139 production from brines (Kotsupalo et al., 2013; Li, X. et al., 2015; Paranthaman et al., 2017; 140 Yang et al., 2018; Yi et al., 2018). The process has shown excellent performance for lithium-141 precipitation and Li/Mg separation (Liu et al., 2018). However, this process is mainly suitable 142 to apply in areas with arid climate to have significant evaporation of the brine. Notably, brine 143 144 lakes occur at high altitudes and in areas with low rainfall, which makes an evaporationprecipitation process an effective approach for lithium extraction. As an alternative attempt, 145 using concentrated sulfuric acid, leached solution containing lithium was obtained from 146 147 roasted Zimbabwean petalite ore concentrate, and then, lithium carbonate was precipitated by adding sodium carbonate (Sitando and Crouse, 2012). However, treatment of petalite by the 148

leaching method requires highly concentrated acid (Sitando and Crouse, 2012), which raisessafety and environmental concerns.

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REEs can also be separated using acidic and alkaline precipitation processes. For example, 152 after extraction of uranium in a pilot plant, the effluent containing sulphate solution was 153 subjected to complete precipitation for recovering REEs at pH 9.3 using ammonium 154 155 hydroxide (Khawassek et al., 2015). REEs can be also separated in a weak acidic medium via precipitation using oxalic acid. The oxalate precipitate is free from undesired elements such 156 157 as phosphate, iron, aluminium, nickel, chromium, manganese, zirconium, uranium and copper (El-Awady, 2013). However, precipitation with oxalic acid is an expensive process. 158 Recovering this acid along with strategically important elements would result in substantial 159 160 savings for the process (Krishnamurthy and Gupta, 2004).

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Platinum-group metals can also be separated using precipitation process. Platinum is 162 precipitated as ammonium hexachloroplatinate with ammonium chloride from the leached 163 solution that is produced from an ore concentrate (Phetla et al., 2010). Palladium could be 164 precipitated using ascorbic acid. Palladium was reported to be precipitated selectively with an 165 increase in the ascorbic acid concentration, while the other elements such as ruthenium, 166 rhodium and iron were hardly precipitated (Lee et al., 2000). The precipitation behaviour of 167 168 the platinum-group metals from liquid waste in a sequential denitration process with formic acid was shown by Kondo and Kubota (1992). The precipitation of ruthenium and rhodium 169 increased linearly with the increase in pH of the denitrated solution. Above 98% of ruthenium 170 171 and rhodium could be recovered via precipitation at pH>7. However, the precipitation of base metals along with platinum-group metals is a major challenge in this process. 172

#### **4.2. Ion exchange**

Ion exchange is an efficient and commercially mature technology for the recovery of 175 strategically important elements from low-grade sources. Some advantages of ion exchange 176 process include simple design, applicability to dilute feeds, ability to achieve a high 177 concentration factor and no loss of separation media to the environment. The shortcoming to 178 ion exchange is that the method does not work well with concentrated feeds: the kinetics is 179 180 usually slow, and depending on the separation agent used, selectivity can be limited. Generally, the economics of ion exchange is driven mostly by the cost of resin regeneration 181 182 chemicals, which increases proportionally with the increase in concentration of dissolved salts in the brine samples. For example, ion exchange is more cost-effective when used to 183 treat brine water with ≤1500 mg/L dissolved salts (Kentish and Stevens, 2001). It is also 184 185 noted that at lower TDS, ion exchange is extremely attractive for its low capital and operational costs and high recovery (90-95%) rates (Aral et al., 2009). Ion exchange offers 186 high separation efficiency of Li from brines, but the application of this method is limited in 187 the large scale owing to the low loading capacity of resins (Al-Obaidani et al., 2008; Zhang et 188 al., 2010). 189

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Previous studies report that ion exchange could effectively recover platinum-group metals 191 (Blokhin et al., 2009; Katsutoshi et al., 2008; Peng et al., 2009). In the metal industry, 192 193 Smopex®, SuperLig® and Amberlite IRA-93 materials are widely known as effective ion exchange resins for the recovery of platinum-group metals (Hubicki et al., 2008; Yahorava 194 and Kotze, 2014). However, high cost and slow adsorption kinetics are the major limitations 195 196 of these resins. Ion exchange has been used to recover platinum group elements from brine solution. Sun et al. (2012) investigated the performance of AG1-x8 resin to separate platinum 197 and Rhodium from mixed chloride solution. They found that AG1-x8 could effectively 198

separate platinum and rhodium. Nikoloski et al. (2015) used three ion exchange resins of 199 different functional groups for the simultaneous recovery of platinum and palladium present 200 in chloride solution. The tested resins included a resin with a quaternary ammonium 201 202 functional group (Lewatit MonoPlus MP 600), a resin with a polyamine functional group (Purolite S985) and a resin with a thiouronium functional group (XUS 43600.00). They found 203 that, among the investigated resins, XUS 43600.00 was the best resin to recover platinum and 204 205 palladium chloride complexes. The recovery of platinum-group elements using Lewatit MP 600 WS and Purolite S985 anion exchangers were extensively studied by several researchers 206 207 (Kononova et al., 2010; Kononova et al., 2011; Mel'nikov et al., 2012). These anion exchangers showed high sorption and kinetic properties for platinum-group elements 208 recovery from synthetic brine. XUS 43600.00 with thiouronium functional group showed 209 210 high selectivity for platinum group elements recovery (Nikoloski et al., 2015), but no data is 211 readily available about the use of thiouronium functionalised resin in the simultaneous recovery of platinum, palladium and rhodium from brine solutions. 212

213

Lithium can also be recovered by ion exchange from brines. Hui (2000) reported that the 214 H<sub>2</sub>TiO<sub>3</sub> ion exchange resin could recover lithium from a brine of natural gas wells. The 215 H<sub>2</sub>TiO<sub>3</sub> ion exchanger has high selectivity for lithium with an exchange capacity of 25.34 mg 216 Lithium/g. In another study by Chitrakar et al. (2014), H<sub>2</sub>TiO<sub>3</sub> ion exchanger achieved 217 218 similar lithium adsorption capacity during the treatment of salt lake brine. Nishihama et al. (2011) have noted a selective recovery of lithium from seawater brine using two successive 219 processes of ion exchange. Firstly, they used k-MnO<sub>2</sub> adsorbent to concentrate lithium 220 221 followed by the purification of lithium from concentrated solution by a combination of acidic cation exchange resin to remove divalent metal ions and b-diketone/TOPO-impregnated resin 222 to remove sodium and potassium. Finally, the recovery of lithium as precipitates of lithium 223

carbonate was achieved using a saturated solution of ammonium carbonate. By this process, 224 the lithium yield was 56% and purity was 99.9% (Nishihama et al., 2011). The recovery of 225 226 lithium from seawater using IX type manganese oxide adsorbent has also been reported in 227 Korea (Liu et al., 2015). They noted that manganese oxide ion sieves could be considered as the most promising process for industrial application. Park et al. (2015) demonstrated that 228 HMnO could be effectively used for recovery of lithium from seawater with good selectivity. 229 Zandevakili et al. (2014) found more than 90% lithium recovery from Urmia Lake by MnO2 230 ion-sieve. Bukowsky et al. (1991) have studied 3 different ion exchange resin (MC50, TP207, 231 232 Y80-N) for recovery of lithium from synthetic brine containing higher contents of CaCl<sub>2</sub> and MgCl<sub>2</sub>. They found that resin Y80-N at room temperature and the resin TP207 at 50 °C can 233 be feasible to recover lithium chloride. Fukuda (2019) tested thirty IX resins in lithium 234 235 chloride solution. They found that out of the thirty, sulfonate, iminodiacetate and 236 aminomethylphosphonate resins could achieve lithium extraction capacity with the value of 16.3-32.9 mg-Li/g. However, none of the resins could adsorb lithium from a real brine 237 solution effectively as a much higher concentration of sodium, potassium, calcium and 238 magnesium ions are present (sometimes 100 times as high as lithium concentration), and 239 these ions have a higher affinity to cation exchange resins (Fukuda, 2019). Thus, sodium and 240 potassium can be partially recovered via evaporation as chloride salts, and magnesium and 241 calcium can be precipitated as carbonates by soda ash before the lithium concentration gets 242 243 high enough to be co-precipitated as a carbonate. Despite the unfavourable conditions for ion exchange resins with interfering ions, Dow Chemical (USA) introduced aluminium-loaded 244 resins which is claimed to extract lithium selectively from brine, although this approach 245 246 remains to be practically implemented (Fukuda, 2019).

Separation of REEs into their individual components as part of the Manhattan Project during 248 World War II was a notable achievement of the ion exchange process (Izatt et al., 2014). 249 Subsequent development of chelating resins was a significant advancement in the application 250 251 of the ion exchange process for the recovery of metals. Chelating ion exchange resins adsorb metals through a combination of ionic and co-ordinating interactions rather than the simple 252 electrostatic interactions in conventional ion exchange processes (Harland, 1994). Chelating 253 ion exchange resins are regularly used in commercial systems to separate metal ions 254 selectively. For example, neodymium is extracted from brine using the commercially 255 256 available D113-III chelating resin (Xiong et al., 2011). Although this process is common for metal recovery in general, the efficacy of the process is yet to be demonstrated for some 257 strategically important elements at industrial scale. Low concentration of the target elements 258 259 in the solution in the presence of high concentrations of other interfering elements leads to 260 slow recovery and high process cost.

261

#### 262 4.3. Solvent extraction

The solvent extraction process has been used at commercial scale for the recovery of 263 strategically important elements. This process is economically viable when the concentration 264 of the target element is high (Kentish and Stevens, 2001). When the components of a mixture 265 have similar physico-chemical properties the separation becomes difficult. In this process, 266 267 separation and purification of REEs are made from the acidic/alkaline leaching solution containing impurities such as calcium, iron, aluminium and lead (Jha et al., 2016). Hence, the 268 impurities affect the quality of the products formed and can be removed using precipitation 269 270 process. Di-(2-ethylhexyl)phosphoric acid (D2EHPA) is widely used as a solvent extraction agent to recover REEs on an industrial scale (Jha et al., 2016). Studies found that D2EHPA 271 could effectively separate high-grade europium, samarium gadolinium and scandium from 272

other metals in a mixed nitrate-chloride leachate (Makanyire et al., 2016; Rabie, 2007). 273 Another study by Perez et al. (2019) shows that highest extraction rates were obtained using 274 275 undiluted D2EHPA, especially for light REEs lanthanum (77.1%) and cerium (94.9%), while 276 D2EHPA diluted in xylene provided the highest selectivity for terbium (heavy REE). Using a three-stage cross-current extraction, terbium was first recovered from the diluted 277 methanesulfonic acid leachate with 100% selectivity and 97.5% recovery using 70% v/v 278 279 D2EHPA in xylene (Perez et al., 2019). Afterwards, the remaining lanthanum and cerium from the diluted raffinate were recovered using three stages of extraction with undiluted 280 281 D2EHPA with an efficiency of 98.8% for lanthanum and 100% for cerium (Perez et al., 2019). Studies have shown that neutral trialkyl phosphine oxides and tetraoctyl diglycol 282 amide have the capability of extracting cerium and europium elements effectively (Larsson et 283 284 al., 2012; Shimojo et al., 2008). Singh et al. (2008) reported that 2-ethylhexyl phosphoric acid-2-ethylhexyl ester (EHEHPA) could recover dysprosium with 98% purity from 285 concentrated HCl leaching solution. However, this separation required several stages due to 286 287 the low separation factor (i.e., presence of competing ions). Wang et al. (2011) studied the performance of solvent extraction using a mixture of sec-octylphenoxy acetic acid and 288 Cyanex272 for extraction of yttrium from other rare earth metals and reported high selectivity 289 of yttrium. However, the presence of iron, manganese, and aluminium are the common 290 impurities during extraction of these elements that affect the quality of products (Makanyire 291 292 et al., 2016). Hence, this has led to the use of other processes such as selective precipitation to remove the metals competing for adsorption with the target metals. In this process, several 293 elements are produced as a co-product/by-product. For example, REEs are recovered as a by-294 295 product of uranium extraction at Denison Mines, Elliot Lake in Canada (Krishnamurthy and 296 Gupta, 2004).

The solvent extraction process is also employed to recover platinum-group elements from 298 low-grade sources. Perez et al. (2019) investigated the separation of platinum and palladium 299 from chloride solution by solvent extraction using Alamine 300 as an extractant. They found 300 301 that platinum could be selectively extracted as the major component along with minor amounts of palladium using a saturated solution of sodium chloride at pH 1.5. This process 302 could achieve a 99.9% purity of platinum. Perez et al. (2019) also found a high palladium 303 304 recovery (99.8%) using a two-stage countercurrent extraction process with 0.5% LIX 84I (2hydroxy-5-nonylacetophenone oxime). In their process, scrubbing using diluted HCl was 305 306 done to remove the co-extracted base metal and resulted in platinum of 99.7% purity. The separation and recovery of palladium and platinum from chloride leach liquor was also 307 investigated by Reddy et al. (2010). 308

309

310 Previous studies report that solvent extraction with β-diketones and n-butanol can be used to extract lithium from brines. For example, Gabra and Torma (1978) established a lab-scale 311 lithium chloride extraction process with n-butanol using synthetic solutions including 312 different quantities of lithium, sodium chloride, potassium, and calcium chloride. They found 313 that this process could recover lithium chloride with 99.6% purity (Gabra and Torma, 1978). 314 Shi et al. (2016) reported separation of lithium and magnesium from Salt Lake brine by 315 liquid-liquid extraction with tributyl phosphate. They found that under the optimum 316 317 conditions, the extraction efficiency of lithium was 80.64% and 99.42% by a single-stage and a three-stage countercurrent extraction, respectively. Recently, Pure Energy Minerals Inc has 318 reported the results of preliminary pilot-scale tests by Tenova Advanced Technology and 319 LiSXTM technology on the Clayton Valley Project, which showed great potential for large-320 scale application of lithium extraction from brines using novel organic reagents including 321 ketone, β-diketone, ionic liquids, and crown ethers (Energy, 2019). This process extracted 322

lithium and separated sodium and potassium after calcium and magnesium removal. 323 However, these processes are still a long way from an industrial application due to technical 324 and economic limitations. Shi et al. (2013) investigated a pilot-scale experiment for the 325 recovery of lithium using TBP in N, N-di(2-ethylhexyl)acetamide/kerosene, and they 326 observed the extraction efficiency of lithium to reach 96%. This demonstrates that TBP is an 327 effective extractant for lithium recovery from salt lake brines. However, as mentioned in 328 329 Section 3, the high magnesium/lithium ratio in brine found in salt lakes is a challenge for large-scale lithium extraction. 330

331

The application of membrane in solvent extraction for the separation of strategically 332 important elements has been investigated in the past (Kim et al., 2015; Xing et al., 2016). In 333 334 this process, a membrane barrier, permeable to cations and impermeable to organic solvent, is located at the interface between the organic solvent and brine, thereby selectively extracting 335 the strategically important elements. A membrane-assisted solvent extraction process for the 336 recovery of REEs from nitric acid solutions was demonstrated by Kim et al. (2015). The 337 system exhibited high selectivity for REE extraction without co-extraction of other elements. 338 Xing et al. (2016) recently tested solvent stable hydrophilic nanoporous poly (ethylene-co-339 vinyl alcohol) membranes for lithium recovery. They observed a stable lithium extraction 340 process for approximately 45 days, indicating the potential of this process for large-scale 341 342 applications.

343

The conventional technologies have limitations in selectivity and efficiency in recovering metals from low-grade sources. It is also noteworthy that often these processes consume a huge amount of water during extracting metals. MacLean et al. (2009) estimated that mining and processing of metals utilise 0.03% of total world water. Given the scarcity of strategically

important elements and clean water, a process that can concentrate metal salts for their
extraction and produce clean water for reuse during the extraction process is highly
warranted. In this context, the integration of a membrane process with conventional
separation techniques could be a suitable approach (Marchetti et al., 2014; Székely et al.,
2012). Membrane technology can provide better metal separation compared to conventional
techniques (Chun-Te Lin and Livingston, 2007; Geens et al., 2007; Vandezande et al., 2008)
and also facilitate clean water production.

355

#### **5.** Membrane processes for the recovery of strategically important elements

Pressure-driven membrane processes such as nanofiltration (NF) and reverse osmosis (RO) 357 have been used for the separation of lithium from brine. Lithium was separated from diluted 358 359 brine in the form of lithium chloride by using NF membranes (Wen et al., 2006). Separation 360 of lithium from salt lake brines by the NF90 and a low-pressure RO membrane (LPRO) was investigated by Somrani et al. (2013). The NF90 membrane was found to be more efficient 361 for lithium separation compared to LPRO. This is probably due to its high hydraulic 362 permeability and separation efficiency of monovalent ions (e.g., lithium). In another study, 363 effective retention (97%) of divalent cations, namely Mg and Ca, was achieved by NF 364 membranes, while a moderate retention (70%) was observed for monovalent cations (Na and 365 Li) (Zhang et al., 2017), thus facilitating separation of lithium from the mixture. Separation 366 367 of lithium and magnesium from brine using NF membranes has also been reported by (Sun et al., 2015) and (Pramanik et al., 2019). They found that magnesium and lithium separation 368 was highly dependent on the pH, operating pressure, and Mg/Li ratio. The competitive 369 370 coefficient was susceptible to the Mg/Li ratio, when the Mg/Li ratio was less than 20 (Sun et al., 2015). An NF membrane with polyamide functional layer and positive charge was 371 fabricated for Li and Mg separation (Li, et al., 2015a,b). The results showed that the rejection 372

difference between magnesium chloride and lithium chloride reached 47.5% and the Mg/Li
ratio decreased from 20 to 7.7. Li et al. (2017) synthesized a composite NF membrane with
positively charged skin layer followed by modification with EDTA, which showed stable
separation behaviour of lithium ions.

377

REEs such as cerium and neodymium can also be separated using NF membranes (Murthy 378 and Choudhary, 2012). Rejection of neodymium ions from synthetic wastewater, as a 379 function of applied pressure, feed concentration and pH was investigated using a NF 380 381 membrane (Murthy and Choudhary, 2011). The rejection of neodymium ions increased with the increase in applied pressure and decreased with the increase in feed concentration. 382 Rejection of neodymium using NF membrane was influenced by solution pH (Murthy and 383 384 Choudhary, 2011). This was likely due to the charged nature of the membrane which changed with the variation in pH (Murthy and Choudhary, 2011). 385

386

Despite the potential of pressure-driven high retention membrane processes in the separation 387 of strategically important elements, these processes have some limitations. These processes 388 are energy-intensive and prone to severe membrane fouling, resulting in impaired membrane 389 performance and shortened membrane lifetime. Hence, combination of emerging 390 technologies such as membrane distillation (MD) and conventional processes such as 391 392 electrodialysis (ED) can be potentially used to recover strategically important elements from brines. These processes can achieve a high concentration factor for strategically important 393 elements by pre-concentrating brines. This is due to the mass transfer properties of the 394 395 membranes. In addition, compared to RO/NF, these processes are expected to have lower energy consumption and lower fouling propensity due to low applied hydraulic pressure 396 397 (Mazlan et al., 2016; McGovern, 2014).

The application of MD process could concentrate strategically important elements to 399 facilitate their recovery and it can also produce clean water (Table 3). MD has the capability 400 to concentrate salts up to the supersaturated state to allow crystallization (Ali et al., 2015). 401 Studies reported that there is ample opportunity for the recovery of lithium from seawater 402 brines using the MD-crystallization technique (Greenlee et al., 2009; Quist-Jensen, C. et al., 403 404 2016; Quist-Jensen, C.A. et al., 2016). Hollins (2013) evaluated the prospects for recovering minerals from desalination brines and focused on the extraction of Li from desalination 405 406 brines as a benchmark. They noted that 23000 tonnes of Li could be recovered from brines by 2030 compared to the current global production of 37000 tonnes. 407

408

409 ED can efficiently achieve lithium recovery from brines. This process was demonstrated to recover lithium in the form of lithium bromide from a sodium-contaminated lithium bromide 410 solution (Parsa et al., 2015) and lithium hydroxide from an aqueous solution (Bunani et al., 411 2017). After pre-concentrating and precipitating brine with sodium carbonate, 98% lithium 412 carbonate could be obtained from simulated lake brines using ED with a bipolar membrane 413 process (Jiang et al., 2014). The ED system can also be equipped with monovalent selective 414 ion exchange membrane for the recovery of lithium from salt lake brines (Ji et al., 2017). In 415 this way, the Mg/Li ratio of simulated brine was reduced from 60 to 7, which provided a 416 417 suitable Mg/Li condition for the extraction of lithium from the Li-enriched solution. However, the concentration of co-existing ions such as sodium, potassium and sulphate, 418 differs considerably in different types of brine, which may influence the applicability of ED 419 420 for lithium recovery (Nie et al., 2017a). In addition, the durability of the membranes is a challenge during long-term lithium recovery in this process (Jiang et al., 2014). 421

423 Table 3: Examples of strategically important elements separation using membrane processes.424

Technology	Source	Concentrate	Separated	Water	References
NF	Salt lake	<u> </u>	L ithium	NA	Wen et al. (2006)
111	brine		Lithium		Somrani et al. $(2000)$
	Unite		Lithium		Sum et al. $(2015)$
	Synthetic	NΛ	Lithium	NΛ	2013 Then at al. (2013)
	Synthetic	INA	Corium		Murthy and
	wastewater		Noodymium		Choudhary (2012)
			Neodymium		Murthy and
			Neouyinnunn		Choudhamy (2011)
					Choudhary (2011)
RO	Salt lake	NA	Lithium	NA	Somrani et al. (2013)
	brine				
MD	Seawater	500	NA	80	Duong et al. (2015)
	Brine				-
	Synthetic	NA	Lithium	NA	Quist-Jensen et al.
	brine				(2016b)
	Salt lake	NA	Lithium	NA	Zhou (2017)
	brine				
ED	Salt lake	NA	Lithium	NA	Liu et al. (2015)
	brine				Jiang et al. (2014)
					Ji et al. (2017)
	Geothermal	NA	Lithium	NA	Mroczek et al.
	brine				(2015)
	Synthetic	NA	Lithium	NA	Nie et al. (2017b)
	brine				Bunani et al. (2017)
					Parsa et al. (2015)
425 NA= I	Data not availab	ole			· · · · ·

A potential integrated process for the recovery of strategically important elements along with 435 clean water production is shown in Figure 5. In this process, membranes can be used to 436 concentrate the strategically important elements as well as produce clean water. Post-437 438 treatment with solvent extraction, ion exchange or precipitation process can be used to retrieve the target element selectively. For example, lithium could be effectively recovered 439 from brines using integrated NF and MD processes. In a previous study, NF could only retain 440 441 26% of the lithium and 88% of magnesium from the seawater (Drioli et al., 2016). Thus, MD can be used to treat the NF permeate, and to concentrate lithium for recovery. NF could also 442 443 be combined with the ED process by replacing the cation exchange membrane (Ge et al., 2016). The MD process can be also integrated with renewable energy sources. Low- grade or 444 waste heat can be used to operate MD process. However, economic analysis is essential for 445 the feasibility of the MD process since a considerable amount of energy is required to 446 evaporate water to separate water from non-volatile contaminants (Kiss and Kattan Readi, 447 448 2018). Recently, Deshmukh et al. (2018) examined some critical factors that affect the energy efficiency of MD processes and also noted how future membrane design and process 449 development could considerably boost MD efficiency. They found that the size of the system 450 451 along with porosity and thickness of the membrane could significantly influence the performance of the process. The cost of the MD system operation may vary from 0.26 to 130 452  $/m^3$  based on the optimum flow conditions and MD configurations (Deshmukh et al. (2018). 453 It was reported that by applying waste heat, the production cost of a 30,000  $m^3/d$  MD 454 desalination plant could be reduced from 2.2 to 0.66 \$/m<sup>3</sup> (Kesieme et al., 2013). However, 455 456 currently limited number of studies is available on the investigation of such an integrated process for the recovery of these elements along with clean water production. 457

The aforementioned membrane processes can concentrate strategically important elements in 459 the solution to enable their crystallisation. However, to date these lithium recovery processes 460 have been mainly tested at lab-scale. Therefore, the recovery of strategically important 461 elements along with clean water production from brines using these processes needs to be 462 further investigated. Particularly, the challenges associated with an integrated process, as 463 depicted in Figure 5, need to be addressed for the recovery of these elements and production 464 of clean water. Studies exploring application of MD on a large scale with a long-term 465 operational period reported several challenges of MD process (Van der Bruggen et al., 2008). 466 467 These include membrane fouling, scaling, and pore wetting which may restrict its commercial application. When applied to brine treatment, inorganic fouling in the form of scaling is the 468 predominant form of fouling on the membrane surface (Van der Bruggen et al., 2008). 469 470 Therefore, it is necessary to fabricate novel membranes with characteristics of low resistance 471 to mass transfer, low thermal conductivity, high thermal stability and chemical resistance to improve MD performance by minimising fouling and wetting phenomena, while enhancing 472 473 retention of target metal. In addition, there is a clear need to evaluate product purity, process efficiency and life cycle costs. 474





477 Figure 5. A roadmap of an integrated membrane and metal separation process for
478 strategically important elements and clean water recovery

#### 480 **6.** Perspective

The commercial viability of extracting metals is not only dependent on mineral 481 concentration, technology implemented, recovery rates, commodity pricing and final product 482 purity, but also market fluctuations for the minerals extracted (Shahmansouri et al., 2015; 483 Teat, 2012). Wei (1982) followed by Brown (2016) showed the potential of mining minerals 484 and metals from geothermal brines as a function of mineral concentration, value, demand, 485 import dependency, strategic consideration, existing sources of supply, technology readiness 486 level of recovery process, and resource uncertainty. They concluded that the recovery of 487 488 REEs and platinum group elements (except lithium) from brine is still in its infancy stage. Both Stull (2016) and Addleman et al. (2016) show that although some of these strategic 489 elements have a low supply risk, the recovery of REEs from geothermal brines is not 490 491 economically feasible with the current market prices of fresh products. It is particularly

difficult for the lower grade sources. However, a study by Grosjean et al. (2012) reported that 492 the lithium production costs from mining of spodumene is estimated to be 6-8 \$/kg, which is 493 not competitive with respect to the recovery cost from salt lake brines (2-3 \$/kg). The 494 495 economic feasibility of mining from brine solution further improves when simultaneous water, energy and mineral extractions are considered as proposed in European funded project 496 MEDINA and Global MVP project (Drioli et al., 2016; Drioli et al., 2011). Overall, there 497 498 might be a trade-off between energy cost and production of strategically important elements along with clean water production at high water recoveries. However, a comprehensive 499 500 techno-economic analysis between the operating cost of the technologies and price for the production of strategically important elements needs to be carried out. 501

502

#### 503 6. Conclusions

504 Water and minerals such as metals are critical resources, and these resources are the building blocks of a sustainable society and the global economy. With population-increase and 505 506 industrialization, the demand for these resources has increased. In this context, it is important to recover strategically important elements and clean water from low-grade sources such as 507 brines as discussed in this article. This may open up an exciting gateway to reduce the overall 508 cost and environmental burden of the ore-mining processes. The recovery of strategically 509 important elements from brines compared to that from ores is still in the early stages of 510 511 development. These elements often occur at low concentrations in brines, and, thus, are difficult to recover in presence of much higher concentrations of other minerals which can 512 interfere with the separation and enrichment process. The main technologies used for 513 514 producing metals from brines are based on precipitation, ion exchange and solvent extraction. A major challenge of these processes is separation selectivity. An integrated membrane-based 515 516 process may be suitable for efficiently enriching strategically important elements for their

51/	subsequent recovery, and, thus, may have a substantial role in shaping the future of this
518	industry. This may be an attractive pathway to bridge the gap between demand and supply of
519	the strategically important elements.
520	
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524	
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**Figure 1:** Examples of strategically important element demand (kg/MW) in the renewable energy industry (Moss et al., 2011; Moss et al., 2013; Teske et al., 2016).



Figure 2: Flowsheet for the recovery of lithium as carbonate from Uyuni Salar brine, Bolivia

(An et al., 2012)



Figure 3: Platinum-group metals and other precious metal recovery using ion exchange

process at Springs, South Africa (Crundwell, 2011).





Rare Earths Ltd, India (Krishnamurthy & Gupta, 2004).



Figure 5. A roadmap of an integrated membrane and metal separation process for strategically important elements and clean water recovery

Metals	Production		Resource		Reserve		Applications	
	Mass	Global share	Mass	Global share	Mass	Global share		
	(kt)	(%)	( <b>k</b> t)	(%)	( <b>k</b> t)	(%)		
Cerium	7.6	8	1481	3	NA	2.8	Catalytic converters in cars, hybrid vehicles, television	
							faceplates, silicon microprocessors.	
Lanthanum	4.6	8	742	3	NA	2.8 Cracking catalysts in petroleum refining, camera		
							battery electrodes, hydrogen storage, x-ray films.	
Dysprosium	0.115	4.8	NA	NA	8	0.64	Motors or generators, wind turbines, and electrical	
							vehicles, hard disk devices, transducers.	
Yttrium	NA	NA	100	18.5	NA	NA	Microwave generators, televisions and computer	
							screens, ceramics, superconductors.	
Platinum	0.22	0.11	2.35	1.2	NA	NA	Catalytic converters, electronic application, fuel cells	
Palladium	0.22	0.11	2.35	1.1	NA	NA		
Lithium	11.7	34	1006	8	1500	10.7	Electric batteries, cordless devices, ceramics, glass.	

**Table 1**: The production, resources and reserve status of some prospective elements in Australia and their application for different purposes(Hoenderdaal et al., 2013; Skirrow et al., 2013; USGS, 2016)

NA: Not available

Source	Status			(	Concentration	n (g/L)			Impurities	References
		$Li^+$	$Mg^{2+}$	$Na^+$	$Ca^{2+}$	$\mathbf{K}^{+}$	В	$SO_4^{2-}$		
Atacama Salar Brine, Chile	Full-scale	3.02	17.6	61.9	0.41	28.2	1.72	37.9	$Na^{+}, K^{+}, Mg^{2+}$	Ogawa et al. (2014)
Uyuni Salar Brine, Boliyia		0.84	16.7	105.4	3.33	15.7	0.7	21.3	Na <sup>+</sup> , K <sup>+</sup> , B	An et al. (2012)
East Taijinar,	Pilot-scale	0.14	5.64	117.03	0.43	3.79	-	-	Na <sup>+</sup> , K <sup>+</sup> ,	Sun et al. (2015)
West Taijinar,		0.26	15.36	102.4	0.19	8.44	-	-	Na <sup>+</sup> , K <sup>+</sup> ,	Sun et al. (2015)
Chott Djerid Salt Lake, Tunisia		0.06	3.4	80	1.6	5.6	-	6.7	Na <sup>+</sup> , Ca <sup>2+</sup> , Mg <sup>2+</sup>	Somrani et al. (2013)
Longmucuo, China		1.21	89.5	-	-	-	-	-	-	Song et al. (2017)
North Arm Salt	Lab-scale	0.04	9.38	100.8	0.35	5.5	0.03	19.7	$Na^+$	Bush et al. (2016)
Salt lake brine,		0.35	113.7	-	-	-	-	-	$Mg^{2+}$	Xiang et al. (2016)
Salt lake brine		0.15	8.88	2.69	-	-	-	-	-	Ji et al. (2017)
Geothermal brine		0.01	-	0.11	-	0.16	0.03	-	$\mathbf{K}^{+}$	Mroczek et al. (2015)
Synthetic brine		0.15	63.8	0.414	0.02	0.20		-	$Mg^{2+}$	Nie et al. (2017b)

### **Table 2:** Composition of lithium in salt lake brine around the world

Technology	Source	Concentrate	Separated	Water	References
		(%)	elements	recovery (%)	
NF	Salt lake	NA	Lithium	NA	Wen et al. (2006)
	brine		Lithium		Somrani et al. (2013)
			Lithium		Sun et al. (2015)
	Synthetic	NA	Lithium	NA	Zhang et al. (2017)
	wastewater		Cerium,		Murthy and
			Neodymium		Choudhary (2012)
			Neodymium		Murthy and
					Choudhary (2011)
RO	Salt lake	NA	Lithium	NA	Somrani et al. (2013)
	brine				
MD	Seawater	500	NA	80	Duong et al. (2015)
	Brine				
	Synthetic	NA	Lithium	NA	Quist-Jensen et al.
	brine				(2016b)
	Salt lake	NA	Lithium	NA	Zhou (2017)
	brine				
ED	Salt lake	NA	Lithium	NA	Liu et al. (2015)
	brine				Jiang et al. (2014)
					Ji et al. (2017)
	Geothermal	NA	Lithium	NA	Mroczek et al.
	brine				(2015)
	Synthetic	NA	Lithium	NA	Nie et al. (2017b)
	brine				Bunani et al. (2017)
					Parsa et al. (2015)

**Table 3:** Examples of strategically important elements separation using membrane processes.

NA= Data not available