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# <sup>1</sup> Microstructural Behaviors of Matrices Based on Polylactic Acid and <sup>2</sup> Polyhydroxyalkanoates

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10 ABSTRACT: Individual films of polyhydroxyalkanoates (PHA) and polylactic acid (PLA) and their blends were developed by

11 solvent casting. PHA was obtained from activated sludges from a wastewater-treatment system at a laboratory scale. This work

12 focused on analyzing the microstructural properties and thermal behaviors of individual films of PHA and PLA as well as those

of their blends. The behaviors of the biodegradation processes of the individual films and blends were examined from a

14 microstructural point of view. ATR-FTIR spectra indicated the existence of weak molecular interactions between the polymers.

15 The formulation of blend films improved the crystallinity of PLA; additionally, it induced the polymer-recrystallization

16 phenomenon, because crystallized PHA acted as a PLA-nucleating agent. This phenomenon explains the improvements in the 17 films' water-vapor-barrier properties. The blends exposed to a biodegradation process showed an intermediate behavior between

PLA and PHA, leading to a consistent basis for designing systems tailored to a particular purpose.

19 KEYWORDS: biopolymers, polymer blends, infrared spectroscopy, crystallinity, modulated DSC, morphology

### 20 INTRODUCTION

<sup>21</sup> Polyhydroxylalkanoate (PHA) is a family of biopolyesters <sup>22</sup> synthesized by microorganisms from various carbon sources; <sup>23</sup> they are accumulated intracellularly under nutrient stress and <sup>24</sup> act as carbon and energy reserves.<sup>1</sup> PHAs can be produced by <sup>25</sup> both pure and mixed microbial cultures. Mixed cultures have <sup>26</sup> the advantage that they do not need sterile conditions and are <sup>27</sup> better able to adapt to complex substrates, such as industrial <sup>28</sup> wastes, than pure cultures.<sup>2</sup> For this, wastes from the dairy <sup>29</sup> industry, the sugar industry, forestry, and biodiesel production <sup>30</sup> can be utilized.<sup>3</sup> Cheese whey is a surplus material from the <sup>31</sup> dairy industry that is mainly discharged to both soils and water <sup>32</sup> bodies, causing serious environmental problems. PHA <sup>33</sup> production from cheese whey could revalorize this dairy <sup>34</sup> subproduct and, at the same time, solve the waste-disposal <sup>35</sup> problems.

A relevant characteristic of PHA is its versatility, because there are more than a hundred different monomers, including hydroxyvalerate and butyrate among others. The properties of yethe synthesized polymer are modified depending on the position of its functional groups and degrees of polymerization. This chemistry allows PHAs to be tailored to provide similar properties to traditional thermoplastics, such as polyethylene (PP), while maintaining biodegradtability.<sup>4</sup>

Polylactic acid (PLA), a thermoplastic aliphatic polyester de derived from lactic acid (2-hydroxy propionic acid), can be produced by condensation and polymerization directly from its basic building block, lactic acid, which is derived from the fermentation of sugars from carbohydrates sources, such as corn starch; cassava root, chips, and starch; and sugar cane.<sup>5</sup> 50 Polylactic acid is produced at the largest industrial scale of all 51 biodegradable polymers, and it is considered the most 52 promising candidate for replacing conventional plastics.<sup>6</sup> It is 53 being used in biomedical applications, for bottle production, 54 for filament production in 3D printing, and for compostable- 55 food-packaging production. It is also being evaluated as a 56 material for tissue engineering. Mass production has reduced 57 the cost of PLA production, making it an economically viable 58 choice for the fabrication of containers, plastic bags, and fibers. 59 Commercial-scale plants today produce hundreds of thousands 60 of tons of PLA per year.<sup>7</sup>

By controlling the molecular architecture, suppliers are able 62 to tailor the polymer to specific applications. Consequently, 63 new and improved grades of bioplastic resins are constantly 64 being introduced to the market. NatureWorks LLC focuses on 65 a multistep procedure involving the condensation reaction of 66 aqueous lactic acid for the production of a low-molecular- 67 weight PLA prepolymer. It is converted into a blend of lactide 68 stereoisomers in order to produce a large spectrum of PLA 69 grades.<sup>8</sup> The films based on PLA have excellent optics and 70 good machinability, barrier, and mechanical properties.<sup>5</sup> 71

PLA and PHA polymers are polyesters and are used in 72 consumer products by a wide industrial sector as a result of 73 their biocompatibility and sustainability.<sup>9</sup> They have thermal 74

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75 behaviors comparable to those of some conventional polymers,
 76 and this has generated much interest in exploring their physical
 77 and structural properties to identify potential applications.<sup>10</sup>

The combination of the two polymers allows the design of 79 new materials with tailorable properties differing meaningfully 80 from those of each component by adjusting the advantages of 81 each polymer in order to obtain materials for different 82 applications. In this sense, the formulation of blend systems 83 is easier and faster than copolymerization methods.<sup>11</sup> There 84 are many studies focused on PLA modification, such as the 85 addition of modifiers and copolymerization.<sup>12</sup> The addition of 86 a highly ordered stereochemical structure, such as that of PHA, 87 could improve the film properties of PLA.<sup>13,14</sup> In this sense, 88 blending PLA with another biobased and biodegradable 89 material, PHA, in order to obtain tailor-made materials 90 constitutes a promising alternative.

This work focused on analyzing the microstructural properties and thermal behaviors of PHA and PLA individual films as well as those of their blends. Furthermore, the biodegradation processes of the individual films and PLA/PHA blends were examined from a microstructural point of view.

### 96 MATERIALS AND METHODS

97 Polylactic acid (PLA), grade 4043D in pellet form (98% L-lactide with 98 a D-isomer content of approximately 2%) and designed for the 99 production of films, was purchased from Natureworks under the 100 trademark Ingeo. As is well-known, the production of PLA involves 101 the conversion of starch in dextrose via a hydrolysis process and 102 fermentation by microorganisms to synthesize the chain of the 103 polylactide polymer.

Polyhydroxylalkanoate (PHA) was obtained from activated sludges from a wastewater-treatment system at the laboratory scale (CIDCA). A two-stage biological system was proposed to produce PHA by aerobic mixed culture from hydrolyzed cheese whey. The first step involved the selection of PHA-accumulating organisms using an aerobic sequencing batch reactor (SBR) operated under a feast– famine regime. Then, there was the stage of PHA accumulation in an arobic batch reactor that was inoculated with biomass taken from SBR enriched with PHA-accumulating bacteria.

113 **Extraction and Quantification of PHA.** Extraction and 114 characterization of PHA from the batch-reactor biomass were 115 performed following the method proposed by Venkateswar Reddy 116 et al.<sup>15</sup> A hydroxybutyrate—hydroxyvalerate (HB—HV) copolymer 117 with a purity of 96% and a molar relation 95:5 HB—HV was obtained. 118 **Film Preparation.** The films were prepared by dissolving PHA 119 and PLA in chloroform at 1 and 2% (w/v), respectively, under stirring 120 for 3 h. PLA/PHA mixtures were prepared in the following 121 proportions: 20/80, 40/60, 60/40, and 80/20 (w/w). They were 122 stirred for 30 min at 60 °C.

Filmogenic solutions of PLA, PHA, and their blends were cast into 124 glass Petri dishes (9 cm diameter) that were left under a fume hood. 125 Later, the samples were dried in a vacuum oven at 60  $^{\circ}$ C to ensure 126 solvent removal from the matrices. When the solutions were cast, 127 constant mass-molding-area ratios were maintained in order to 128 ensure uniform thicknesses in the different samples, because the 129 control solutions (PLA and PHA) had different concentrations.

Film thickness was measured by means of a coating-thickness gauge
(Check Line DCN-900) for nonconductive materials on nonferrous
ubstrates. For each specimen, at least 14 measurements at different
positions were taken.

134 **Water-Vapor Permeability.** Water-vapor-permeability (WVP) 135 tests were carried out according to the technique described by Rivero 136 et al.<sup>16</sup> based on a modified version of ASTM<sup>17</sup> method E96. A 137 permeation cell maintained at 20 °C was used for the assays. Eight 138 measurements were performed once steady-state conditions were 139 reached. All measurements were performed at least four times for each 140 specimen. **Thermal Analysis by MDSC.** Thermal analysis of the samples 141 was conducted by the modulated-differential-scanning-calorimetry 142 (MDSC) technique. Q100 (TA Instruments) controlled by a TA 143 5000 module (TA Instruments) and equipped with a cryogenic-144 quench-cooling accessory was used under a  $N_2$  atmosphere. This 145 technique allowed us to measure the calorific capacity of the sample 146 and simultaneously differentiate between the reversible (dependent 147 on the calorific capacity) and irreversible events (dependent on the 148 time and temperature) that the sample experienced. Likewise, it 149 allowed the resolution of complex transitions. 150

A standard heating ramp of 10 °C min<sup>-1</sup> with a modulation- 151 temperature amplitude of 0.5 °C and a modulation period of 60 s was 152 used. The first scan (heating) was performed in order to delete the 153 thermal story from -50 °C up to 200 °C. Once the first scan was 154 completed, the sample was cooled to -80 °C, and then a second 155 heating scan was recorded. Informed results were the averages of two 156 replicates to ensure reproducibility of the results. 157

The results were analyzed by using the Universal Analysis V1.7F 158 software (TA Instruments). Different parameters were determined 159 from the obtained thermograms: melting temperature  $(T_m)$ , enthalpy 160 corresponding to the area of the endothermic peak  $(\Delta H_m)$ , 161 crystallization temperature during the cooling stage  $(T_c)$ , crystal-162 lization enthalpy  $(\Delta H_c)$ , and glass-transition temperature  $(T_g)$  163 determined from the reversible signal.

**ATR-FTIR Spectroscopy.** The interactions between the system 165 components were analyzed using the ATR-FTIR technique. Spectra of 166 the samples were registered by using the Thermo Scientific Nicolet 167 iS10 FT-IR Spectrometer in the wavenumber region of 4000–400 168 cm<sup>-1</sup>, performing 64 scans at a 4 cm<sup>-1</sup> resolution. Specimens were 169 placed onto the diamond ATR crystal (Smart iTX accessory), and the 170 software Omnic 8 (Thermo Scientific) was used for the data-analysis 171 process. To ensure the reproducibility of the results, the tests were 172 performed in triplicate.

**X-ray Diffraction.** X-ray diffractograms of individual PVA and 174 PLA films and their blends were evaluated by using an X'Pert Pro P 175 Analytical Model PW 3040/60 (Almelo) operated at room temper- 176 ature. The Cu K $\alpha$  radiation (1.542 Å) was generated at 30 mA and 40 177 kV. Scattered radiation was detected in an angular range of 3–60° 178 (2 $\theta$ ) at a step size of 0.02°. The crystallinity degree (CD) was 179 calculated following the procedure described in previous works.<sup>18,19</sup> 180

**Structural Studies by SEM.** The microstructures of the matrices 181 were examined by using an FEI model Quanta 200 scanning electron 182 microscope. Individual films and blend matrices were immersed in 183 liquid nitrogen and fractured cryogenically. Samples were mounted 184 onto metal stubs by using double-sided tape and observed at low 185 pressure and an acceleration voltage of 12.5 kV, without any metal or 186 carbon coating. 187

**Biodegradation Test.** A series of plastic pots  $(400 \text{ cm}^3)$  were 188 used as soil containers, and the microflora present was used as a 189 degrading medium. Square specimens of  $3 \times 3$  cm with a thickness of 190 approximately 25  $\mu$ m on average were put into a plastic mesh to allow 191 the access of moisture and microorganisms and the retrieval of 192 degraded specimens. In order to guarantee aerobic degradation, the 193 film samples were buried. The samples were conditioned at a relative 194 humidity of 50% and a temperature of 20 °C. Containers were 195 sprayed regularly with a defined and constant amount of water. 196 Similar conditions were employed by Rivero et al.<sup>20</sup> At specific time 197 intervals, specimens were recovered from the soil and cleaned with a 198 brush to avoid any possible damage of the structure.

In accordance with the described methodology in ASTM D5988- 200 03,<sup>21</sup> a ratio of 1 g of compost per 25 g of soil was used. Studies of the 201 morphology of the degraded films were performed by means of SEM, 202 MDSC, and ATR-FTIR analysis. 203

**Statistical Analysis.** For statistical analysis, version 10.0 of Systat- 204 software (Systat, Inc.) was used. Analysis of variance (ANOVA), 205 linear regressions, and Fisher's least-significant-difference test for 206 mean comparison were performed. The significance level used was 207 0.05. 208

#### 209 RESULTS AND DISCUSSION

f1

Thermal Analysis. The thermograms obtained by means of MDSC from PLA, PHA, and their blends can be observed in Figure 1, where the stages of heating and cooling are shown. The temperatures of the thermal transitions and the enthalpy values (J g<sup>-1</sup>) of the characteristic events during the heating



**Figure 1.** MDSC curves of individual (PLA and PHA) and blend films with different proportions of PLA/PHA showing (a) heating stage, (b) cooling stage, and (c) reversing heat flow (W  $g^{-1}$ ), evidencing the glass-transition temperatures ( $T_g$ ) of each component.

and cooling stages obtained from MDSC curves are 215 t1 summarized in Table 1. 216 t1

As it is possible to see in Figure 1a, the thermal analysis 217 allowed us to observe a peak for each individual film, 218 attributable to the melting of the crystalline domains 219 corresponding to PLA and PHA at 147.7 and 172.7 °C, with 220 the associated enthalpies of 20.1 and 86.6 J  $g^{-1}$ , respectively. 221 The intensity of the melting peak is related to the number of 222 crystals or crystalline populations (crystalline fraction) that 223 exist in the material when the melting occurs. Using MDSC, 224 Thellen et al.<sup>4</sup> reported that crystal melting is produced at 225 higher temperatures in samples of PHA containing lower 226 percentages of valerate, because as the valerate content 227 increases, the onset of crystal melting occurs at lower 228 temperatures. In the present study, the PHA thermograms 229 evidenced the presence of a peak with a shoulder, which could 230 represent the melting of crystal lamellae, as was reported by 231 Thellen et al.<sup>4</sup> for extruded PHA. 2.32

On the other hand, PHA films exhibited a  $T_g$  at -4.7 °C, 233 whereas PLA showed a marked transition at 58.1 °C (Figure 234 1c). Glass-transition temperatures ranging from 2.7 to -4.4 °C 235 for a PHA matrix obtained by casting were reported by da Silva 236 et al.<sup>22</sup> 237

The thermograms of all the mixtures exhibited PLA-  $^{238}$  recrystallization peaks at 107 °C; this transition was more  $^{239}$  evident with higher PLA proportions in the mixture (Figure  $^{240}$  1a). These results indicate that the incorporation of PHA  $^{241}$  contributes to the process of recrystallization of PLA in all the  $^{242}$  blend formulations. This effect was more marked in the  $^{80/20}$   $^{243}$  blend, a behavior that could be explained by bearing in mind  $^{244}$  that a low proportion of crystalline domains of PHA dispersed  $^{245}$  in a continuous matrix of PLA induced the phenomenon of  $^{246}$  nucleation of this latter polymer. The presence of double  $^{247}$  melting temperatures in the PLA/PHA blends corresponds to  $^{248}$  the melting of both the "as formed" and recrystallized  $^{249}$  polymer.  $^{10}$ 

According to Abdelwahab et al.<sup>10</sup> and Ikehara et al.,<sup>23</sup> 251 recrystallization strongly depends on the melting-temperature 252 differences among the components of the mixture. When the 253  $T_{\rm m}$  difference is very large, the component with the higher 254 melting temperature crystallizes first, and its spherulites 255 contribute to fill all the volume. 256

The 20/80 blend exhibited a peak at 171.9  $^{\circ}$ C because of the 257 melting of the PHA crystalline fraction and a shoulder at 148.4 258  $^{\circ}$ C corresponding to the melting of PLA. The 80/20, 60/40, 259 and 40/60 blends exhibited two endothermic transitions; the 260 enthalpy associated with the first event diminished with the 261 incorporation of a higher proportion of PHA to the blend, 262 whereas the enthalpy of the endothermic peak, characteristic of 263 the PHA-crystalline phase, became more prominent (Figure 1a 264 and Table 1). These findings were in accordance with a higher 265 crystalline degree.

From the obtained DSC curves, two  $T_g$  values were observed 267 irrespective of the blend composition. These results suggest 268 that the analyzed PLA/PHA blends are immiscible in the 269 amorphous state (Figure 1c). 270

According to Lipatov and Alekseeva,<sup>24</sup> the appearance of 271 two transitions associated with the glass-transition temper- 272 atures supports the existence of a partially miscible system (i.e., 273 materials with a heterogeneous biphasic structure). 274

During the cooling step, PHA exhibited a peak of 275 crystallization at 58.7 °C with an associated enthalpy of 48.4 276 J  $g^{-1}$ , whereas the thermogram of PLA did not show this 277

	-	
	heating stage	cooling stage
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Table 1. Thermal Analysis of Single and Blend Matrices with Different Proportions of PLA/PHA<sup>a</sup>

	0 0				0 0	
	characteristic events of PHA		characteristic events of PLA		characteristic events of PHA	
PLA/PHA	$T_{\rm m}$ (°C)	$\Delta H_{\rm m} ({\rm J g}^{-1})$	$T_{\rm m}$ (°C)	$\Delta H_{\rm m} ({\rm J g}^{-1})$	$T_{\rm c}$ (°C)	$\Delta H_{\rm c} ({\rm J g}^{-1})$
100/0	_	_	147.7(1.0) a	20.1(1.3) c	_	—
80/20	170.4(1.2) a	1.5(0.07) a	150.3(1.9) a	20.0(0.7) c	_	—
60/40	169.9(0.6) a	9.1(0.1) b	149.8(0.6) a	13.4(0.5) b	_	—
40/60	170.3(0.4) a	18.8(0.7) c	149.5(0.9) a	5.8(0.1) a	65.6(0.5) b	18.8(0.1) a
20/80	171.9(0.8) a	61.7(1.2) d	—	—	65.9(3.8) b	31.4(1.9) b
0/100	172.7(0.1) a	86.6(0.1) e	—	—	58.8(0.5) a	48.4(0.4) c
Different letters i	in the same column i	ndicate significant diff	erences $(p < 0.05)$ and	mong samples.		

278 transition (Figure 1b and Table 1). Taking these results into 279 account, it is possible to infer that the crystallinity of PHA is 280 greater than that of PLA.

The thermal analysis of the PLA/PHA mixtures showed that 281 282 the peak of crystallization attributable to PHA was observed 283 only in the 20/80 and 40/60 mixtures, with a minor associated enthalpy regarding a single PHA matrix (Figure 1b). On the 284 other hand, the thermograms of the individual PLA film and 285 the 60/40 and 80/20 mixtures did not exhibit this thermal 2.86 transition (Figure 1b). Nevertheless, an event was observed at 2.87 57.7 °C attributable to the glass-transition temperature of the 2.88 289 PLA-enriched phase. Similar results were informed by Arrieta et al.,<sup>12</sup> Furukawa et al.,<sup>25</sup> and Zhang and Thomas,<sup>11</sup> indicating 290 that these results are a signal of the fact that the PHA in the 291 292 mixtures does not crystallize during the cooling stage when it is 293 the minor proportion.

Microstructural Analysis. *FTIR Analysis*. From the ATR-FTIR spectra, the functional characteristic groups of PLA and PHA were identified (Figure 2a,b). They are consistent with the literature.<sup>5,26,27</sup>

 $f_2$ 

In the PLA spectrum, the band located at 1746 cm<sup>-1</sup> is a 2.98 strong peak that corresponds to the stretching of the carbonyls' 2.99 amorphous phase.<sup>5</sup> The bands located at 1180 and 1080 cm<sup>-1</sup> 300 belong to the asymmetric and symmetric stretching vibrations 301 of C-O-C. As is known, PLA is a hydrophobic polymer 302 because of the presence of -CH side groups. The peaks at 303 about 2997 and 2946 cm<sup>-1</sup> correspond to the asymmetric and 304 symmetric stretching vibrations of the -CH groups in the side 305 chains, respectively (data not shown). 306

<sup>307</sup> On the other hand, in the PHA spectrum, the peak at 1719 <sup>308</sup> cm<sup>-1</sup> is attributable to the stretching of the crystalline carbonyl <sup>309</sup> group, and the stretching of the carbonyl group of the <sup>310</sup> amorphous phase is virtually imperceptible. The 40/60 and <sup>311</sup> 20/80 samples exhibited peaks at 1748 and 1755 cm<sup>-1</sup> (Figure <sup>312</sup> 2b), which were assigned to the amorphous and crystalline <sup>313</sup> bands of PLA, respectively.<sup>24</sup>

Furthermore, Figure 2a,b depicts the ATR-FTIR spectra of the PLA/PHA blend matrices. The spectra of the 80/20 and of 60/40 compositions followed a similar pattern to that of the pristine PLA, whereas the 40/60 and 20/80 mixtures were is identified mainly with the PHA spectrum. All of them unfolded both bands corresponding to the stretching of carbonyls located at 1746 and 1719 cm<sup>-1</sup> due to PLA and PHA phase, respectively (Figure 2a,b).

In the cases of the 80/20, 60/40, and 40/60 blends, the bands in the C-O-C and C-C stretching and CH deformation mode region (1300-1000 cm<sup>-1</sup>) are visualized at about the same wavenumbers as those of pure PHA (Figure 226 2a,b).



Figure 2. ATR-FTIR spectra of individual (PLA and PHA) and blend matrices with different proportions of PLA/PHA.

It is noteworthy that the intensities of these bands were 327 interdependent and mutually dependent, one being increased 328 at the expense of the other, meaning that the ratio of intensities 329 of these two bands changed in agreement with the ratio of the 330 individual components. These results allowed us to infer the 331 immiscibility of these components and that there were no 332 strong molecular interactions between the polymers. 333

*X-ray Diffraction.* The typical diffraction patterns of <sup>334</sup> individual PHA and PLA and those of the composite films <sup>335</sup> are depicted in Figure 3. The X-ray diffractogram of the PLA <sup>336</sup> f<sup>35</sup> films exhibited a pattern corresponding to an amorphous <sup>337</sup> material with a peak located at  $2\theta = 17^{\circ}$ , which was associated <sup>338</sup> with the reflection of the crystals of the polymer; <sup>13,28</sup> the <sup>339</sup>

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Figure 3. X-ray diffractograms of individual (PLA and PHA) and blend films with different proportions of PLA/PHA. Table inset shows the crystallinity degrees (%) of the samples.

340 estimated crystallinity degree was 14.3% (table insert in Figure 341 3). In contrast, PHA is a highly ordered polymer, and it is 342 known to crystallize in an orthorhombic cell.<sup>10</sup>

343 X-ray-diffraction analysis was used to determine the 344 crystalline structures and crystallinity degrees of the blends. 345 The PHA spectrum showed diffraction peaks at  $2\theta = 13.8$  and 346  $17^{\circ}$ , corresponding to the (020) and (110) planes, 347 respectively.<sup>11</sup> Additionally, reflections at  $2\theta = 20.3$ , 22.4, 25.4, and 30.8° were detected, which were characteristics of <sup>348</sup> the PHA polymer, its CD being 18.3%.<sup>14</sup> 349

The inclusion of PHA in the blends increased the  $_{350}$  crystallinity of the materials. The highest crystallinity degrees  $_{351}$  of the 60/40 and 40/60 blends were confirmed by means of X-  $_{352}$  rays (table insert in Figure 3). The diffractograms showed  $_{353}$  peaks of higher intensity in relation to individual matrices.  $_{354}$ 

This behavior allows us to infer that PHA induces the 355 recrystallization of PLA due to its capacity to act as an agent of 356 nucleation. According to Furukawa et al.<sup>24</sup> and Zhang and 357 Thomas,<sup>11</sup> it generates better packing density of the polymeric 358 segments and promotes better adhesion and interaction at the 359 interface level. However, the microstructure, porosity, and 360 permeability of the matrix seem to depend on the PLA/PHA 361 proportions, as presented below. 362

SEM Observations. From the macroscopic point of view, 363 the blend of the two polymers appeared to be well mixed in the 364 matrices with no apparent phase separation, although FTIR 365 showed the immiscibility of both components. The average 366 thickness of the films was 25  $\mu$ m, which was corroborated by 367 microscopic analysis. As it can be seen in Figure 4, all matrices 368 f4 presented homogeneous appearances irrespective of the PLA/ 369 PHA ratio. 370

The films showed important differences when analyzed in 371 the cross-sections of single or blend matrices. PLA-only films 372 showed a homogeneous appearance, without pores and with 373 good structural integrity. Addition of the PHA polymer led to 374 films whose cross-section was rough, giving a structure with a 375 fibrous appearance (Figure 4). 376

The cross-sections and surfaces of the 20/80 and 40/60 377 mixtures revealed the presence of an orderly structure, 378 attributable to the growth and crystallization of the spherulites 379



Figure 4. Cross-section SEM micrographs of individual (PLA and PHA) and blend films with different proportions of PLA/PHA.

<sup>380</sup> of PHA, proving to be a network formed by codomains <sup>381</sup> corresponding to the different polymers with a granular, <sup>382</sup> interspersed appearance and a repetitive pattern. It is <sup>383</sup> important to remark that the highest proportion of PHA in <sup>384</sup> the blends (PLA/PHA = 20/80) evidenced a porous <sup>385</sup> microstructure as a result of the structural arrangement <sup>386</sup> between the polymers. According to Abdelwahab et al.,<sup>10</sup> the <sup>387</sup> interface interactions between the PHA and PLA phases could <sup>388</sup> influence the nucleation phenomenon as supported by the <sup>389</sup> XRD results.

These micrographs reinforced the results of immiscibility obtained by other techniques. As the PLA proportion increased, the morphology of the matrices became more homogeneous and less rough, until the 80/20 mixture presented an appearance where the PLA-enriched phase formed a continuous domain in which the PHA-enriched phase was dispersed and homogeneously distributed, as can be presented an appearance 4.

398 *Water-Vapor Permeability*. Table 2 shows the WVP values 399 of the individual films and PLA/PHA blends. The formulation

Table 2. Water-Vapor-Barrier Properties of the Individual(PLA and PHA) and Blend Films with DifferentProportions of PLA/PHA<sup>a</sup>

PLA/PHA	WVP (× $10^{11}$ g s <sup>-1</sup> m <sup>-1</sup> Pa <sup>-1</sup> )
100/0	1.73(0.25) b
80/20	0.62(0.06) a
60/40	0.68(0.07) a
40/60	0.72(0.05) a
20/80	2.22(0.38) b
0/100	2.24(0.30) b
Different letters indicate	significant differences ( $p < 0.05$ ) among

samples.

400 of the blend matrices improved the barrier properties of the 401 materials, obtaining a reduction of 40% in the WVP values for 402 the 40/60, 60/40, and 80/20 blends compared with the values 403 of the individual films (Table 2). Meanwhile, the 20/80 blend 404 did not show significant differences (p > 0.05).

405 According to Arrieta et al.,<sup>12</sup> the crystallization of PLA 406 reduces the water-vapor permeability because the crystals 407 decrease the volume of the amorphous phase, generating a 408 path of greater tortuosity and reducing mass matter transfer.

409 The improvement of the barrier properties is related to the 410 higher crystallinity of the PLA/PHA blend matrices, as 411 observed by the X-ray diffraction technique and the MDSC 412 thermal analysis.

413 *Soil-Biodegradation Studies.* The influence of the micro-414 structure developed during the formulation of the blends on 415 the biodegradation process was examined. A morphological 416 study by SEM during soil-biodegradation experiments was 417 complementary to visual examination as it helped to confirm 418 the existence of structural modifications in the films, allowing a 419 detailed evaluation of the degradation process.

420 The results showed that the degradation behavior of the 421 biobased polymers followed different patterns regarding the 422 morphological characteristic of each matrix. As can be seen in 423 Figure 5a, the biodegradation occurred in both the PHA and 424 PLA phases.

The biodegradation assay revealed that the PHA films exhibited remarkable biodegradation after 30 days, whereas the blend matrices (PLA/PHA) showed changes around 50 days, which indicated a delay in the process of biodegradation 428 (Figure 5a). According to Weng et al.,<sup>27</sup> a PHA polymer could 429 be biodegraded at a high rate under composting as well as soil- 430 environment conditions; in contrast, although PLA was 431 biodegradable under composting conditions, its degradation 432 rate in soil was slow. 433

SEM micrographs show the fractured surface of the PLA/ 434 PHA matrices after a biodegradation process of 50 days 435 (Figure 5a). It can be seen that the biodegradation was 436 intensified with higher proportions of PHA in the blend 437 system. As the proportion of PHA increased, particularly from 438 40/60 to 20/80, the matrices showed greater interstices or 439 cavities (Figure 4), which could facilitate the biodegradation 440 process. Zhang and Thomas<sup>11</sup> explained that the inclusion of 441 PHA improved the degradation degree of PLA at room 442 temperature. The authors reported that PHA and PLA exhibit 443 different degradation patterns. PHA is mainly degraded by the 444 attack of various enzymes at the surface. According to Weng et 445 al.<sup>27</sup> the degradation of PHA can be attributed to erosion 446 catalyzed by bacteria from the surface to the interior. 447

In contrast, PLA degradation is produced throughout the 448 whole sample, starting with a nonenzymatic hydrolysis that 449 leads to a reduction in the molecular weight.<sup>11</sup> Then, low- 450 molecular-weight PLA diffuses out of the bulk polymer and can 451 be metabolized by microorganisms, producing water, carbon 452 dioxide, and humus.<sup>29</sup> 453

On the other hand, the thermograms of the 20/80, 40/60 454 and 60/40 blend matrices exposed to the biodegradation 455 process for 50 days showed a decrease of the transition 456 enthalpy, corresponding to the melting of the PHA crystalline 457 fraction being more marked in the blends with the greatest 458 proportion of PHA (Figure 5b). In this sense, Dharmalingam<sup>30</sup> 459 found that the changes of melting enthalpy ( $\Delta H_m$ ) for a 460 composite material based on PLA/PHA blends represent 461 depolymerization. Consequently, this phenomenon could 462 indicate a higher sensitivity to the degradation process in the 463 presence of higher proportions of PHA, independent of the 464 rearrangement formed between both polymers. 465

The chemical-structure changes of the matrices exposed to 466 the biodegradation process were investigated by ATR-FTIR 467 (Figure 5c). 468

ATR-FTIR spectra corroborated the changes caused in the 469 structure of the polymers. After 50 days of exposure to the 470 biodegradation process, ATR-FTIR spectra of the PHA and 471 blend films showed that the bands lost definition. 472

For all the samples assayed, the peaks in the 4000-3000 473 cm<sup>-1</sup> region became broadened after the biodegradation 474 process (data not shown). According to Weng et al.,<sup>27</sup> this 475 fact was attributable to the formation of hydroxyl and 476 carboxylic groups. This was also confirmed by the shift of 477 the absorption peak of the C=O stretching vibration after 478 biodegradation. 479

Ludueña et al.<sup>31</sup> pointed out that chemical and enzymatic 480 hydrolysis are the main mechanisms of chain rupture during 481 the degradation process. Then, biodegradation process 482 depends on water availability, which produces hydrolysis, and 483 microbial attack of the matrix. Water diffusion in the soil leads 484 to a hydrolytic degradation of the material modifying the 485 surface, resulting in a porous structure with evident signs of 486 degradation. A similar explanation was proposed by Rocca- 487 Smith et al.<sup>32</sup> 488

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Figure 5. Monitoring of the behaviors of samples after they were submitted to biodegradation processes (buried for 50 days) through (a) SEM micrographs of the PLA/PHA blend matrices with enlarged sections showing the degradation (magnification is indicated in the micrographs), (b) MDSC analysis, and (b) FTIR-ATR studies.

The biodegradability of the blends was more marked in films formulated with increasing proportions of PHA; similar results were reported by Zhang and Thomas.<sup>11</sup>

Conclusions. Thermal and microstructural studies revealed 492 493 that blends of PLA/PHA-based systems were partially miscible. The formulation of blend matrices improved the crystallinity of 494 495 PLA; additionally, it induced the polymer-recrystallization 496 process, because crystallized PHA acted as a PLA-nucleating agent. This phenomenon explains the improvements in water-497 vapor-barrier film properties. Moreover, the blends exposed to 498 499 a biodegradation process showed an intermediate behavior 500 between those of PLA and PHA, leading to a consistent basis 501 for designing systems tailored to a particular purpose or use. This work, therefore, contributes to the knowledge of 502 503 microstructures, allowing one to develop and test materials

# 504 with specific technological applications.

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