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A new remote predictor of wave reflection based on runup asymmetry

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Abstract

Reflected waves account for a significant part of the nearshore energy budget and influence incoming waves, nearshore circulation and sediment transport. The use of swash parameters to estimate wave reflection is investigated at three different beaches ranging from highly reflective to dissipative. It is observed that it is essential to account for swash processes when estimating reflection, in particular at intermediate and reflective beaches with a steep beachface. Our results show that runup asymmetry in uprush/backwash can be used as a proxy for dissipation in the swash zone: larger asymmetry values indicating greater dissipation. In our dataset, a reflection predictor based on runup asymmetry has better skill in comparison to empirical predictors based on surf similarity, because runup is a process that integrates both surf and swash zone wave transformation. Runup asymmetry behaves as a swash similarity parameter and reflects an equilibrium between swash period, slope and dissipation.

Keywords: Nearshore; video imagery; runup asymmetry; swash dissipation; reflection

Highlights:

- Link between swash parameters and wave reflection investigated at three different beaches
- Asymmetry in uprush/backwash can be considered a proxy for swash dissipation
- Evidence of equilibrium between runup asymmetry, period and slope

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23

24 1. Introduction

25 Field and laboratory studies have demonstrated that incident wave energy is not entirely
26 dissipated when it reaches the shoreline. Part of the incident wave energy is reflected into deeper
27 water (Mansard & Funke, 1980; Miche, 1951; Tatavarti, Huntley, & Bowen, 1988). As a rule-of-thumb:
28 the steeper the beach, the more incident wave energy is reflected, and vice versa. At the steepest
29 beaches and in the case of long period waves, observations show that up to 60-80% of the incoming
30 wave energy is reflected (Battjes, 1974; Elgar et al., 1994). Reflected waves can strongly influence
31 and interact with incident waves; change individual wave shape (Abdelrahman and Thornton, 1987;
32 Rocha et al., 2017), intensify undertow (Martins et al., 2017), and generate standing or even resonant
33 waves (Almar et al., 2012; 2016). This effect on the hydrodynamics is thought to have a feedback on
34 submerged morphological bed forms (e.g. O'Hare and Davies, 1993; Hancock and Mei, 2008), and can
35 also modify offshore wave conditions. In deep water up to 15% of the total wave energy can be linked
36 to coastal reflection (Ardhuin and Roland, 2012) as reported in the Gulf of Guinea, West Africa (Laibi
37 et al., 2014), where beaches are generally steep and incident waves are long. Hence, it is crucial to
38 understand and accurately predict reflection at natural beaches.

39 Based on the laboratory study of Iribarren and Nogales (1949), Battjes (1974) demonstrated that
40 wave reflection is proportional to a "surf similarity" parameter ξ which quantifies surf zone
41 conditions:

42

$$43 \quad \xi = \frac{\tan(\alpha_f)}{\sqrt{H/L_0}} \quad (\text{Eq. 1})$$

44 where α_f is the foreshore slope, and H and L_0 are the wave height and deep-water wavelength
45 respectively. Dissipative conditions are generally associated with low values of ξ , typically less than
46 0.3 (Stockdon et al., 2006; Ruggiero et al., 2001; Ruessink et al., 1998, Raubenheimer and Guza, 1996;
47 Raubenheimer et al., 1995; Guza and Thornton, 1982), whereas intermediate and reflective
48 conditions are associated with larger values (Holland and Holman, 1999; Holland, 1995; Holman,
49 1986; Holman and Sallenger, 1985). The surf similarity equation provides satisfactory reflection
50 estimates for gentle slopes (low ξ) when dissipation is dominated by wave breaking, but
51 overestimates reflection for $\xi > 2.5$, when wave energy dissipation in the swash zone becomes more
52 significant (Ahrens, 1979; Seelig and Ahrens, 1981; Sutherland and O'Donoghue, 1998; Baldock, P.
53 Holmes, 1999). Furthermore, the surf similarity parameter is a seemingly weak proxy for reflection
54 in the case of complex bathymetries such as two-slope profiles (Mizuguchi, 1984; Elgar et al., 1994;
55 Davidson et al., 1996; Miles & Russell, 2004). Field and laboratory data (e.g. Dickson et al., 1995; Inch

56 et al., 2016) indicate that reflection is primarily proportional to the wave period and the effect of
57 wave height is negligible.

58 Muttray et al. (2006) indicate that reflection predictors based on ξ overestimate the effect of wave
59 breaking, and highlight the potential role of swash zone dynamics when predicting reflection. But,
60 while the description of reflection in terms of surf zone conditions has attracted a lot of attention,
61 literature describing wave energy reflection in terms of swash dynamics is rather limited. Guedes et
62 al (2011) observed no link between swash energy and ξ , implying that swash energy and wave
63 reflection are independent at the hourly scale. However, Martins et al. (2017) found a correlation
64 between peak swash potential energy and reflected wave energy at the time-scale of individual
65 waves on a steep, reflective, large-scale laboratory beach, suggesting that reflected waves energy can
66 be predicted based on detailed swash measurements.

67 Swash is far from a simple oscillation of the waterline. Whitham (1958) and Shen & Meyer (1963)
68 introduced a parabolic ballistic approach for run-up as a solution for a collapsing bore running over
69 a dry beach. Hughes et al. (1997), Guard & Baldock (2007) and Power et al. (2011) showed in the
70 field and with laboratory measurements that swash flow can be far from symmetric, with the
71 antagonistic effects of wave energy and gravity over beach slope. On the other hand, Guza & Bowen
72 (1976) depict the swash as the antinode of a standing wave for non-breaking waves, with a rather
73 symmetric runup shape. Observations show that runup asymmetry results predominantly from the
74 effect of bore dissipation during the uprush, which occurs mainly due to breaking and friction
75 (Hughes & Fowler, 1995; Puleo & Holland, 2001), and this includes the influence of sediment grain
76 size (Masselink & Hughes, 1998, Elfrink & Baldock, 2002) but also swash-swash interactions
77 (Baldock & Holmes, 1999; Hughes & Moseley, 2007); catch-up and absorption during the uprush, and
78 collision between uprush and the preceding backwash (Chen et al., 2016). Large values of runup
79 asymmetry are thought to indicate large dissipation and weak reflection. Because the measurement
80 of reflection and swash is a difficult task in the field, observations are scarce. Nonetheless, current
81 remote sensing techniques such as video imagery (Power et al., 2011; Almar et al., 2017) or LiDAR
82 (Blenkinsopp et al., 2010) are capable of obtaining suitable data.

83 This paper stresses the role played by swash in controlling reflection, which is ignored in most
84 common predictors based on surf zone conditions. A predictor for wave reflection based on swash
85 asymmetry is introduced and validated using datasets collected at three contrasting natural beaches
86 covering a range of conditions from dissipative to highly reflective. We investigate the advantage of
87 using swash dynamics for predicting reflection rather than the surf similarity parameter ξ , in

88 particular at complex beaches and hourly timescales. Finally, the role of asymmetry to indicate
89 “swash similarity” is discussed and some concluding remarks are provided.

90

91 2. Data and methods

92 Data were collected during three experiments undertaken in 2012-2013 at three different field
93 sites (Figure 1), ranging from dissipative to reflective beach slopes and low to high energetic wave
94 conditions. The corresponding hydro-morphological conditions during the three experiments are
95 shown in Figure 2.

96 A dissipative beach (upper beach slope $\alpha=0.05$) experiment was conducted at Mataquito, Chile,
97 from November 28th to December 14th, 2012 (Cienfuegos et al., 2014). Mataquito is a medium grain-
98 sized ($D_{50}=0.2$ mm), alongshore uniform, barred beach with a micro-tidal range and a wave climate
99 dominated by swell waves (annual mean derived from EraInterim -ECMWF, Dee et al., 2011- for the
100 1979-2012 period, $H_s \sim 2.4$ m, $T_p \sim 12$ s, SW). During the experiment, tidal amplitude ranged from
101 0.4 to 1 m. A large swell hit the coast on Dec. 2, ($H_s = 4$ m, $T_p = 18$ s, day 3 in Fig. 2, left panels), followed
102 by moderately energetic conditions starting on Dec. 5 ($H_s = 1-2$ m, $T_p = 10-15$ s).

103 An intermediate beach (upper beach slope $\alpha=0.12$) experiment was conducted at Nha Trang,
104 Vietnam, from December 3rd to 10th, 2013 (Lefebvre et al., 2014). Nha Trang is a uniform low-tide
105 terrace, medium grain-sized ($D_{50}=0.3$ mm) beach with a micro-tidal range and a low to moderate
106 energy wave climate (annual mean, $H_s < 1$ m, $T_p < 5$ s, E). During the experiment, tidal amplitude
107 decreased from 1.2 to 0.5 m. Wave height and period decreased continuously, from $H_s = 1$ m, $T_p = 9$ s
108 to $H_s = 0.5$ m and $T_p = 5$ s.

109 A reflective beach (upper beach slope $\alpha=0.15$) experiment was conducted at Grand Popo, Benin,
110 from February 17th to 28th, 2013. Grand Popo is a reflective, medium to coarse grain-sized ($D_{50}=0.6$
111 mm), alongshore uniform, low-tide terraced beach with a micro-tidal range and a wave climate
112 dominated by swell waves (annual mean, $H_s \sim 1.4$ m, $T_p \sim 9.4$ s, SW) (Almar et al., 2014a). During the
113 experiment, tidal amplitude increased from 0.5 m to 1.4 m. An energetic swell hit the coast on Feb.
114 23, ($H_s = 1.5$ m, $T_p = 18$ s), followed by moderate conditions.

115 At each site, the upper beach slope was extracted from daily topographic surveys undertaken at
116 low tide using differential GPS. Directional wave measurements were obtained in approximately 10
117 m water depth (red circles in Fig. 1) using an Acoustic Doppler Current Profiler (ADCP Workhorse
118 Sentinel 1200 KHz, 20-min wave bursts; see method in Jeans et al., 2002). Shore-based video swash
119 monitoring was undertaken at 2 Hz during daylight hours at the three experiment sites. Time series
120 of pixel intensity sampled along a cross-shore line (time stacks) (Holland & Holman, 1993) were

121 collected to measure wave runup, which was detected by applying a Radon Transform (RT) approach
 122 described in Almar et al. (2017). In this study, the ability of the RT to detect the instantaneous
 123 shoreline was assessed by comparison to concurrent LiDAR measurements and compared to the
 124 commonly used color contrast method (CC), which defines the waterline from RGB colorband
 125 contrast. Because the RT is based on motion detection it is more able than the CC approach for
 126 distinguishing between backwash and the groundwater seepage line, and is less sensitive to poor
 127 light conditions. Rectification of images from pixels into real-world coordinates was accomplished
 128 by direct linear transformation using DGPS ground control points (Holland et al., 1997) after a
 129 correction of the radial lens distortion (Heikkila & Silven, 1997). Although varying somewhat
 130 throughout the field of view, the pixel footprint was less than 0.1 m in the cross-shore direction over
 131 the region of interest (surf-swash zones). A single cross-shore transect was considered at the three
 132 sites, assuming alongshore-uniform processes, which will not be the case in the presence of
 133 longshore variability in the swash dynamics induced by irregular features such as crescentic sandbar
 134 (Nicolae Lerma et al., 2017) and beach cusps (Almar et al., 2018).

135 Swash energy flux F_{swash} was computed from 1-hr video time stacks (Power et al., 2011; Guedes et
 136 al., 2011; Senechal et al., 2011):

137

$$138 \quad F_{swash} = E_{swash} C_{gsw} \sim \frac{\rho g R_{sw}^2}{16} \quad (\text{Eq. 2})$$

139

140 Where ρ is water density (here 1025 kg/m³) and R is the horizontal runup computed from
 141 horizontal waterline timeseries S , $R_{sw} = 4(S \tan \alpha_{sw})$, using the RT (Radon Transform method, see
 142 Almar et al., 2017) and α_{sw} as the active swash slope, which is defined by Holland and Puleo (2001)
 143 as the dynamic slope within the swash zone which changes with tide. A constant shallow water group
 144 velocity is considered hereafter $C_{gsw} = \sqrt{gh} \sim 1 \text{ m/s}$, using an arbitrary depth of 0(10 cm) at swash
 145 inception, due to the lack of information. The directional wave spectra $E_d(\theta, f)$ were computed from
 146 an ADCP (Acoustic Doppler Current Profiler from RD Instrument), using the WavesMon software
 147 (see the manual) and the procedure described by Krogstad et al. (1988) and Strong et al.
 148 (2000). Incomig and reflected wave energy and direction were computed from co-localized pressure
 149 and current measurements from an ADCP (Acoustic Doppler Current Profiler, e.g. Sheremet et al.,
 150 2001). Though this technique is commonly used and offers good skill in retrieving swell band waves
 151 in intermediate to shallow depths (Herbers and Lentz, 2010), it can have some difficulty in capturing
 152 short wind waves due to the attenuation of the wave orbital motion with depth. Several methods
 153 exist to separate incoming and outgoing waves: the PUV temporal (e.g. Guza et al., 1974) and spectral

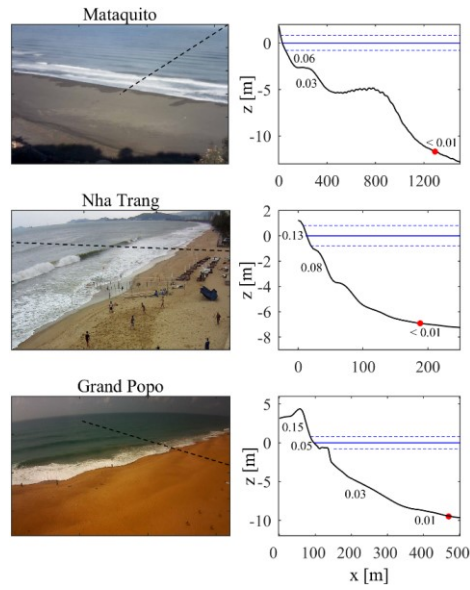
154 (Sheremet et al., 2002) methods, using pressure and velocity sensors, and array methods that only
 155 use cross-shore array of pressure sensors (or any free surface measurements), such as the recent
 156 method based on the Radon Transform developed by Almar et al., (2014b). Here, ~~incoming~~ incoming
 157 and outgoing wave heights were ~~defined-separated~~ using from $E_d(\theta, f)$ the ADCP spectra following
 158 the method described by Sheremet et al. (2002), integrating from the lower to upper cut-off
 159 frequency (range set to gravity-infragravity band 0.02 Hz-0.5 Hz), ~~based on the local shore-normal~~
 160 direction:

$$161 \quad H_{inc} = 4 \left(\int_{0.02 \text{ Hz}}^{0.5 \text{ Hz}} \int_{-90^\circ}^{90^\circ} E_d(\theta, f) d\theta df \right)^{1/2} \quad (\text{Eq. 3})$$

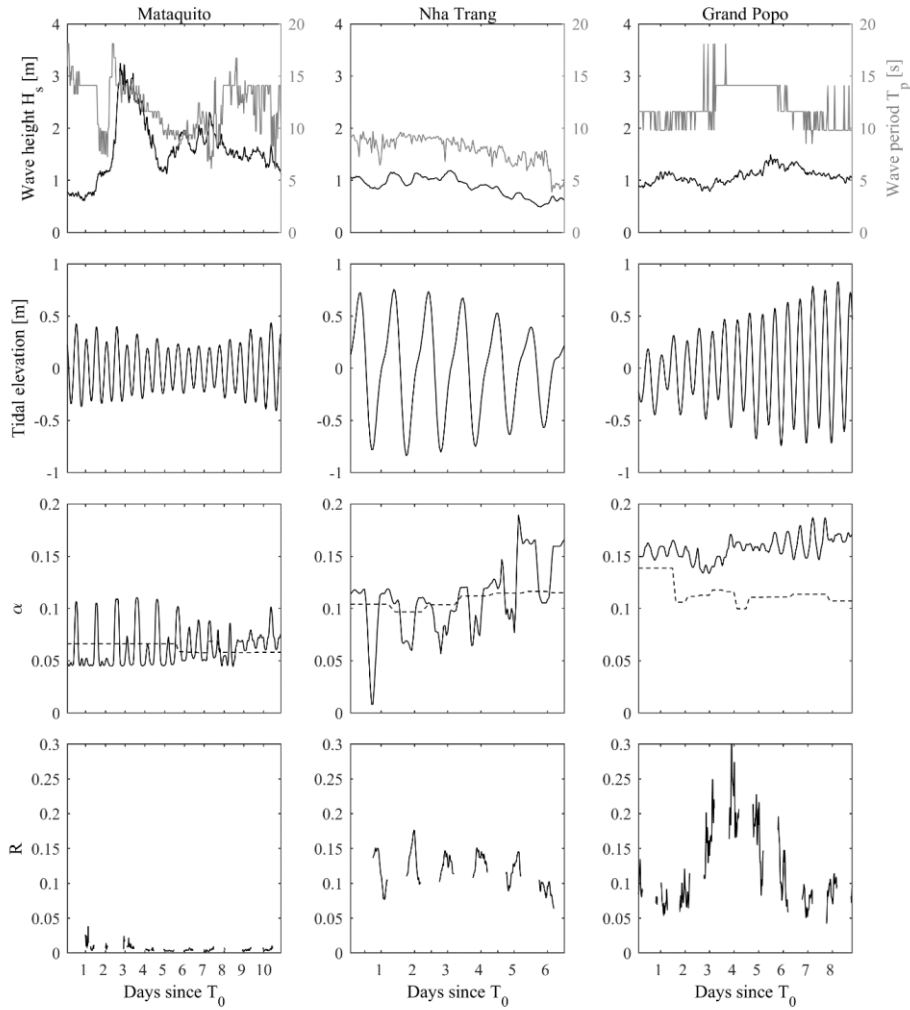
$$162 \quad H_{out} = 4 \left(\int_{0.02 \text{ Hz}}^{0.5 \text{ Hz}} \int_{270^\circ}^{90^\circ} E_d(\theta, f) d\theta df \right)^{1/2} \quad (\text{Eq. 4})$$

163 With $E_d(\theta, f)$ denoting the energy density and the term inside the parentheses representing the
 164 variance associated with the defined frequency band and the incidence angle from the shore-normal
 165 direction (see also Almar et al., 2014b). Peak period T_p is calculated as the inverse of the peak
 166 frequency in $E_d(\theta, f)$. Offshore incoming and reflected wave fluxes, F_{inc} and F_{ref} are computed as $F =$
 167 $ECg = \rho g H_s^2 T_p / 32\pi$ ($W.m^{-1}$) at the ADCP (depth~10m at the three sites), ~~Cg assuming being~~
 168 computed with linear theory using intermediate depth conditions~~deep water conditions for~~
 169 ~~convenience, even if long waves might be slightly shoaling at ADCP locations during energetic~~
 170 ~~conditions~~. Reflection is quantified as the ratio of reflected and incoming energy. At all sites, the ADCP
 171 was moored sufficiently far offshore to avoid reflection coefficient variability associated with the surf
 172 zone, as described by Baquerizo et al. (1997).

173



174
 175 Figure 1: Snapshots from video systems (left) and (right) bathymetry profiles, (top) Mataquito,
 176 (mid) Nha Trang, and (bottom) Grand Popo. In the left panels, dashed black lines indicate the cross-
 177 shore time stack locations. In the right panels, numbers are local beach slopes, the red circles, solid
 178 and dashed blue lines indicate the location of the ADCP, mean sea level, max and min spring tidal
 179 elevations, respectively.



180
 181 Figure 2: From left to right, Mataquito, Nha Trang and Grand Popo experiments. (Row 1) offshore
 182 significant wave height (H_s - black line) peak period (T_p - grey line), (Row 2) tide, (Row 3) shoreface
 183 slope α with (active swash slope, solid line) or without (dashed line) tidal modulation. (Row 4)
 184 reflection (R).

185

186 3. Results

187 3.1. Nearshore wave energy budget

188 It is hypothesized that it is essential to account for swash processes when estimating R and the
189 nearshore energy balance, in particular at reflective or complex beaches. This is investigated here
190 through the decomposition of the nearshore wave energy budget (e.g. Baquerizo et al., 1998; Carini
191 et al., 2015). The nearshore wave energy budget (e.g. Sheremet et al., 2001) may be expressed as:

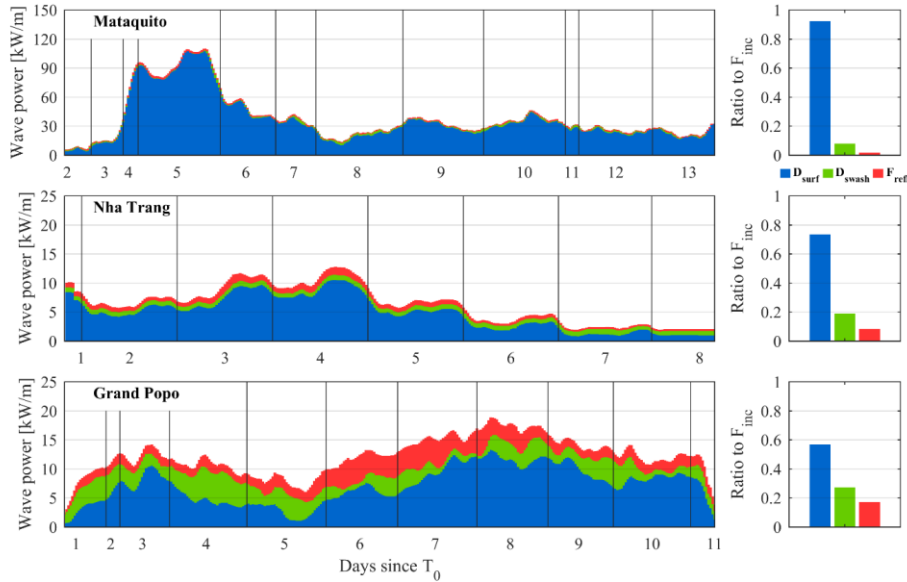
$$193 \quad F_{inc} - F_{ref} = D_{surf} + D_{swash} \quad (\text{Eq. 5})$$

194
195 With F_{inc} and F_{ref} the offshore incoming and reflected wave fluxes, D_{surf} and D_{swash} the wave
196 dissipation in the surf and swash zone respectively. We assume hereafter that reflection occurs only
197 in the swash zone, with the reflection from submerged bars considered to be negligible (for now) and
198 incident waves sufficiently shore-normal to be reflected back offshore and not get trapped (only
199 leaky modes). Swash energy flux F_{swash} computed in Eq. 2 can also be considered as:

$$201 \quad F_{swash} = D_{swash} + F_{ref} \quad (\text{Eq. 6})$$

202
203 Eq. 6 can only be satisfied under the assumption that reflected waves do not break when
204 propagating offshore and hence no energy is lost. Figure 3 shows the hourly evolution of D_{swash} , F_{ref}
205 and D_{surf} . F_{inc} and F_{ref} are measured at the ADCP (see Data and Methods Section) and D_{swash} is computed
206 from Eq. 6, D_{surf} is computed from the combination of Eq. 5 and 6. Figure 3 shows that the relative
207 contribution of D_{swash} increases with beach gradient. It is as small as 2 % at Mataquito, increases to
208 23 % at Nha Trang and up to 35 % at Grand Popo with the reflection coefficient R increasing in a
209 similar manner with values of 1%, 10% and 15 % respectively. As observed by Elgar et al. (1994) and
210 Miles and Russell (2001) R values are generally higher during high tide which is consistent with
211 higher reflection from a steeper beach face. At the two most reflective beaches, Grand Popo and Nha
212 Trang, the dissipation in the swash zone is important, due to the limited wave breaking over the
213 narrow terrace, in particular at high tide as also observed by Miles & Russell, (2004). Under such
214 conditions, swash plays a major role in governing the amount of reflected energy, as shown recently
215 by Martins et al., (2017). In contrast, dissipative beaches such as Mataquito are dominated by
216 breaking processes (Guedes et al., 2011), with minimal influence from the tide level.

217
218



219
 221 Figure 3: Left panels show a decomposition of the incoming wave power F_{inc} separated into surf
 222 zone dissipation D_{surf} (blue) from the combination of Eq. 5 and 6, swash zone dissipation D_{swash} (green)
 223 from Eq. 6, and reflected wave energy flux F_{ref} (red). The percentage contribution of each component
 224 to the total energy flux is shown in the right panels.

225
 226 *3.2. Wave reflection from runoff asymmetry*

227 Reflection measurements typically require the installation of instrumentation in intermediate
 228 water depths. The ability to estimate reflection based on swash characteristics would be beneficial
 229 and makes in-situ instrumentation redundant. We hypothesize here that D_{swash} is proportional to
 230 F_{swash} with $D_{swash} = K F_{swash}$ where K is an empirical coefficient that represents swash dissipation:

231
 232
$$K = (F_{swash} - F_{ref})/F_{swash} \quad (\text{Eq. 7})$$

233
 234 Laboratory measurements in the swash zone supported by numerical modelling such as in
 235 ~~Martins et al. (2017) estimate the bulk of energy reflected from the beach. A 0.5 coefficient of~~
 236 proportionality was found between reflected bulk and swash energy.

237

238 In accordance with the notion of surf similarity, a long wave on a mild slope would represent
239 comparable hydrodynamic conditions as a short wave and a steeper slope (Battjes, 1974). In other
240 words, a given swash slope appears steeper to longer waves than it does to shorter waves. As
241 observed for runup on rubble mound by several authors (e.g. Davidson et al., 1996), on a steeper
242 slope, more energy will be reflected (i.e. less energy will be dissipated). By contrast, a short wave on
243 a flat beach will dissipate its energy through bore breaking-induced turbulence and bottom friction
244 in the uprush which results in a thin layer of weak return flow during the backwash phase of the
245 swash cycle.

246 Figure 4 illustrates the contrasting swash shapes observed at the three sites. At Mataquito, the
247 runup time series presents a sawtooth shape; the already broken bore (Guard and Baldock, 2004) in
248 combination with a gentle swash slope leads to almost complete energy dissipation during the
249 uprush with a weak backwash. In contrast, at more reflective beaches, such as Nha Trang and even
250 more so at Grand Popo, large bores collapse at the shoreline and the steeper slope leads to strong
251 backwash which seemingly generates significant reflected wave energy (Martins et al., 2017). The
252 variability in uprush/backwash flows discussed above is characterized here through the front-to-lee
253 (temporal) asymmetry (see Elgar and Guza, 1985):

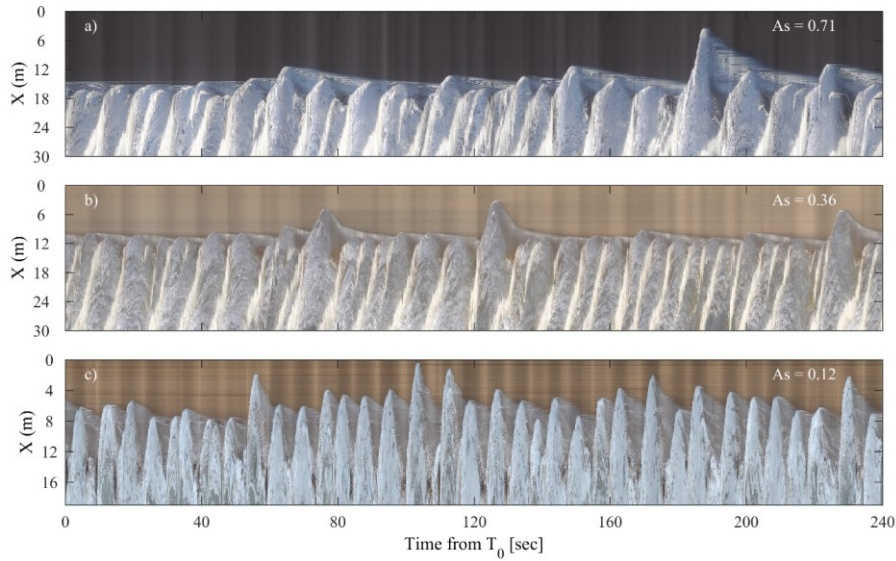
254

$$255 \quad A_s = \frac{\langle H^3(S-\bar{S}) \rangle}{\langle (S-\bar{S})^2 \rangle^{3/2}} \quad (\text{Eq. 8})$$

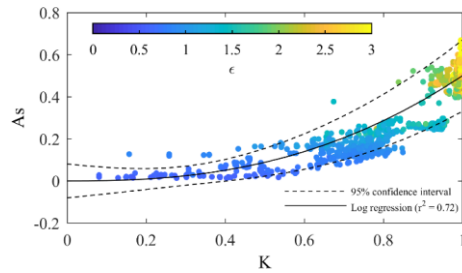
256

257 Where H denotes the Hilbert transform and S represents the horizontal swash excursion, $\langle \rangle$
258 indicates time averaging. Figure 4 shows an illustration of different swash conditions with the
259 corresponding runup asymmetry values ranging from pitched forward, dominated by uprush
260 ($A_s=0.71$) at Mataquito, to almost symmetrical ($A_s=0.12$) at Grand Popo.

261



262
 263 Figure 4: Illustration of video time stacks of the swash zone with asymmetry values at dissipative
 264 Mataquito (top), intermediate Nha Trang (mid) and reflective Grand Popo beaches (bottom).
 265



266
 267 Figure 5: Hourly runup asymmetry As (Eq. 8) (computed from the three datasets) as a
 268 function of the swash dissipation parameter K (Eq. 7). Colours represent the Miche swash similarity
 269 parameter ϵ ($\epsilon = S \frac{\omega^2}{g} \alpha_{sw}$, where S is the horizontal swash excursion, α_{sw} is the active swash slope, g
 270 is the acceleration due to gravity and ω is the angular wave frequency $2\pi/T$ with the swash period
 271 T). The solid line is a logarithmic regression and dashed lines show the 95% confidence intervals.
 272

273 In Figure 5, the aggregate of all of the data collected from the three sites is presented in terms of
 274 the swash reflection parameter, the corresponding swash similarity parameter (colour) and the

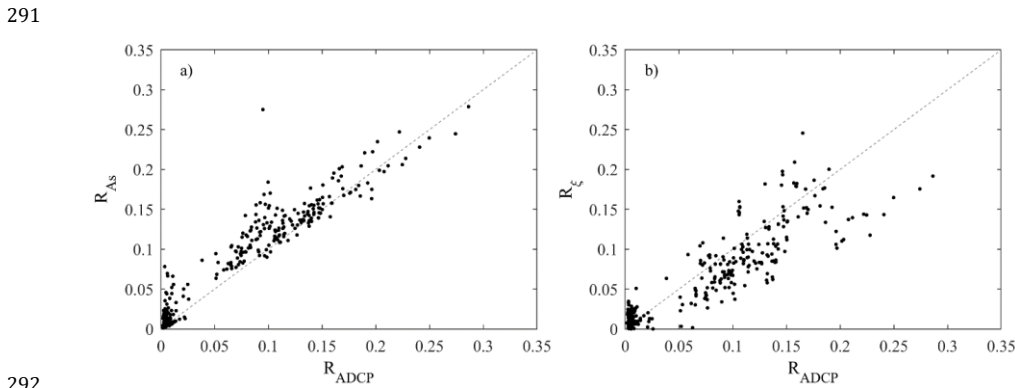
275 estimated asymmetry. It can be noted that there is a positive correlation between swash asymmetry
 276 and swash dissipation. A functional form can be obtained as:

$$277 \quad K = aAs^b \quad (\text{Eq. 9})$$

279
 280 Where logarithmic best fit regression gives $a=1.3$ and $b=0.4$ (significant at 95% level, Figure 5). It
 281 is now possible to estimate the reflection coefficient directly as a function of the remotely sensed
 282 swash asymmetry:

$$283 \quad R_{As} = \frac{F_{swash}(1-K)}{F_{inc}} \quad (\text{Eq. 10})$$

285
 286 Figure 6 indicates a strong relationship between hourly R_{As} and reflection observed offshore R_{adcp} ,
 287 with a coefficient of determination of 0.72 (significant at 95% level). Method skill worsens for low
 288 reflection values as the Mataquito data is clustered with no clear dependence on As (see Figure 5).
 289 However, this swash-based predictor offers a better result for these three datasets than conventional
 290 predictor based on surf conditions (following the surf similarity parameter $R_\xi = 0.1\xi^2$, with $R^2 = 0.38$).



292
 293 Figure 6: Predicted hourly reflection coefficients from a) runup asymmetry R_{As} and b)
 294 conventional predictor based on surf conditions using Battjes's formula $R_\xi = 0.1\xi^2$, as a function of
 295 observed reflection coefficient from ADCP R_{adcp} . Dashed lines show 1:1 agreement.

296

297 **4. Discussion**

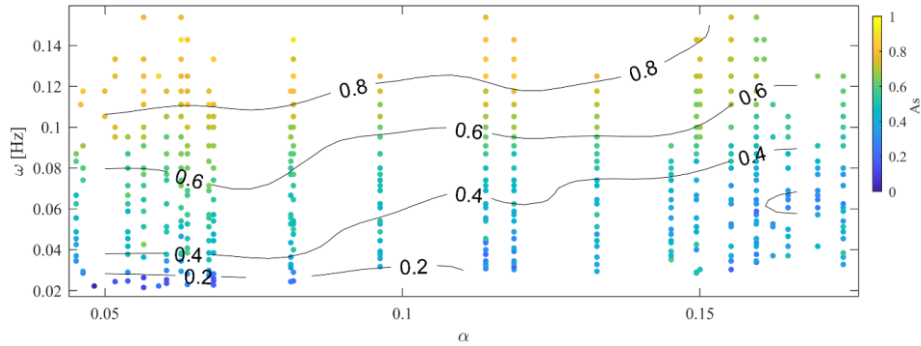
298 Runup asymmetry is an all-encompassing parameter that is the result of surf and swash zone
299 wave transformation, and their interaction with morphology. The strongest agreement between
300 asymmetry and wave reflection is found at the most reflective Grand Popo and Nha Trang beaches.
301 This relationship weakens at the dissipative Mataquito beach, where the dependence of reflection on
302 swash dynamics also weakens (see the surf scaling parameter, Guza and Inman, 1975). In such a case,
303 the reflection can be scaled more appropriately using deep-water parameters (Guza & Thornton,
304 1982; Diaz-Sanchez et al., 2013). The results show that a swash-based reflection proxy is less
305 accurate at dissipative beaches, where runup asymmetry may not be the key controlling factor, or
306 the noise in the reflection data is large compared to the signal itself. This is in line with the
307 observation of Guedes et al., (2011). While the newly developed runup asymmetry predictor is
308 clearly advantageous in comparison with other predictors at two-slope beaches (i.e. different swash
309 and surf slopes) it might be affected by the presence of a submerged sandbar such as observed at
310 Mataquito. Irregular morphological features, such as sandbars, can also introduce multiple reflecting
311 and energy dissipating features (Davies, 1982; Mei, 1985; Bailard et al., 1992; Elgar et al., 2003; Almar
312 et al., 2018) which inherently weakens the link between swash dynamics and offshore waves. Waves
313 transmitted over the bars may undergo partial reflection at the shoreline (Miche, 1951; Elgar et al.,
314 1994), followed by re-reflections from the bars, complicating the wave transformation (Yu and Mei,
315 2000). Noteworthy, the scatter observed in Figure 6 can be partly attributed to the noise in F_{ref} and
316 F_{inc} estimated at the ADCP. As described in Section 2 (Data and methods), the ADCP can have
317 difficulties to retrieve waves at the lower and upper cut-off frequencies, in particular in capturing
318 short wind waves (e.g. Nha Trang) in relatively deep water and longest waves (e.g. Mataquito).

319 Identifying the backwash leading edge is notoriously difficult from video imaging and much can
320 be left up to interpretation as the leading edge infiltrates into the bed (Vousdoukas, 2014). The RT
321 method (Almar et al., 2017) is based on motion (i.e. flow) detection rather than colour contrast used
322 in pioneering studies of Holland & Holman (1993) and Holland et al. (1995, 2001). Whereas no
323 substantial differences are expected in terms of swash statistics, the RT might be more suited when
324 studying swash shape, such as asymmetry, as it describes main flow behaviour rather than the
325 behaviour of a weak backwash flow. Most swash models, for example, the ballistic approach of Shen
326 et Meyer (1963) do not account for swash asymmetry and the influence of swash interactions
327 (Bergsma et al., 2018) on the characteristics of the shoreline motion. This is because these sources of
328 energy loss predominately occur seaward of the instantaneous shoreline through the interaction of
329 the incoming bore with the preceding backwash (Baldock and Holmes, 1999). Our data shows that

330 runup shape, which reflects the level of dissipation, can vary substantially; part of this observed
331 variability could be attributed to the dissipation resulting from these swash interactions (Baldock &
332 Holmes, 1999; Hughes & Mosseley, 2007; Brocchini and Baldock, 2008). While the long period swell
333 waves and steep beach at Grand Popo were observed to lead to minimal interactions, interactions
334 were common at Mataquito. The long-duration return flow of short waves over flat beaches has the
335 potential to enhance swash-swash interaction, dissipating energy and promoting an asymmetric
336 shape.

337 The normalized swash slope parameter (Battjes et al., 2004) suggests that swash dynamics is
338 primarily influenced by wave period and active swash slope, and thus potentially runup asymmetry
339 A_s . Following the approach in Martins et al., (2017), the range of A_s values for different swash slopes
340 and periods is investigated on an individual swash basis. In Figure 7, the distribution of A_s averaged
341 over the three experiments is presented as a function of swash slope α and swash frequency ω . A_s
342 decreases with α and increases with ω : for a given slope, shorter swashes tend to have higher
343 dissipation (strong A_s) while longer swashes reflect more energy (weak A_s). In a similar manner to
344 the estimation of reflection from the combination of A_s and runup excursion length, this suggests that
345 A_s and ω could be used to estimate swash slope remotely. Because swash hydrodynamics adapt more
346 rapidly than morphology to rapidly varying offshore conditions, there is the potential for high-
347 frequency A_s and subsequent reflection to provide a short-term predictor of beach slope evolution,
348 though further analysis is required to confirm this.

349 This new reflection predictor based uniquely on swash dynamics offers the potential to estimate
350 reflection using shore-based remote sensing systems such as video cameras. These tools enable
351 inexpensive and relatively simple long-term monitoring of swash motion (e.g. Guedes et al., 2011;
352 Almar et al, 2017) and hence reflection (via the new predictor), and this has significant advantages
353 over more conventional reflection measurement approaches which require costly in-situ marine
354 deployments and are typically limited to relatively short durations (e.g. Baquerizo et al., 1997). In the
355 current work, only a single cross-shore transect was analysed, however two-dimensional
356 information on reflection can be obtained by extracting swash motion and A_s at several alongshore
357 locations which may give new insight into the longshore variability of wave reflection and its effect
358 on surf zone dynamics (Nicolae Lerma et al., 2017; Almar et al., 2018).



359
 360 Figure 7: Distribution of runup asymmetry A_s as a function of swash frequency ω (inverse of
 361 individual swash duration) and active swash slope α . Dashed black contour lines represent iso-
 362 asymmetry levels.

363

364 5. Conclusions

365 A new predictor for wave reflection using video-derived runup asymmetry is proposed and
 366 applied to dissipative, intermediate and reflective beaches. A decomposition of the incoming wave
 367 energy fluxes into surf and swash zone dissipation and reflected waves showed that it is essential to
 368 account for swash-zone processes when estimating reflection, in particular at intermediate and
 369 reflective beaches. Our results show that runup asymmetry in uprush/backwash is correlated with
 370 swash dissipation: strong values of runup asymmetry indicate large swash-based energy dissipation.
 371 For our dataset, the new predictor based on remotely-sensed swash characteristics offers improved
 372 results ($R^2=0.72$) with better skill in comparison to conventional predictors based on surf similarity
 373 ($R^2=0.38$). This is because runup is the result of surf and swash zone wave transformation, and their
 374 interaction with the local morphology. In addition, it is shown that runup asymmetry reflects an
 375 equilibrium between swash period, slope and dissipation.

376

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386

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