

Ultra-stiff large-area carpets of carbon nanotubes

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Abstract

Herewith, we report the influence of post-synthesis heat treatment (≤ 2350 °C and plasma temperatures) on the crystal structure, defect density, purity, alignment and dispersibility of free-standing large-area (several cm²) carpets of ultra-long (several mm) vertically aligned multi-wall carbon nanotubes (VA-MWCNTs). VA-MWCNTs were produced in large quantities (20-30 g/batch) using a semi-scaled-up aerosol-assisted chemical vapour deposition (AACVD) setup. Electron and X-ray diffraction showed that the heat treatment at 2350 °C under inert atmosphere purifies, removes residual catalyst particles, and partially aligns adjacent single crystals (crystallites) in polycrystalline MWCNTs. The purification and improvement in the crystallites alignment within the MWCNTs resulted in reduced dispersibility of the VA-MWCNTs in liquid media. High-resolution microscopy revealed that the crystallinity is improved in scales of few tens of nanometres while the point defects remain largely unaffected. The heat treatment also had a marked benefit on the mechanical

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properties of the carpets. For the first time, we report compression moduli as high as 120 MPa for VA-MWCNT carpets, *i.e.* an order of magnitude higher than previously reported figures. The application of higher temperatures (arc-discharge plasma, ≥ 4000 °C) resulted in the formation of a novel graphite-matrix composite reinforced with CVD and arc-discharge-like carbon nanotubes.

1. Introduction

Due to their unique anisotropic properties, vertically aligned carpets of multi-wall carbon nanotubes (VA-MWCNTs) are being investigated for a variety of applications such as composites¹⁻⁴, membranes and filters⁵⁻⁸, thermal interface materials⁹⁻¹¹, electronic devices¹² and supercapacitors¹³⁻¹⁶. In most of these applications, high structural uniformity, low crystallographic imperfections, high purity and alignment of MWCNTs are sought after in order to achieve improved reinforcement, high electrical and thermal conductivity, *etc.* Despite intense research on optimising chemical vapour deposition (CVD) techniques, due to its relatively low cost, versatility, scalability, and efficiency, for the production of high-quality VA-MWCNT carpets, the mechanical properties of individual CVD nanotubes¹⁷ are still inferior to the relatively defect-free arc-discharge MWCNTs. For instance, the Young's modulus of arc-discharge MWCNTs was reported to be around 1 TPa¹⁸⁻²⁰, compared to the broad range Young's moduli measured for CVD MWCNTs (10-100 GPa²¹ and 50-350 GPa^{18,22}). For applications such as MWCNT-reinforced composites, a number of reinforcement mechanisms are proposed including matrix toughening^{23,24} through bridging and deflecting crack propagation and nanotube pull-out mechanism on the fracture surface²⁵. Since the potency of such reinforcements strongly depends upon the catalyst content, purity, and defect density of the reinforcing CNTs²⁶, maximising the crystallinity and purity of CVD MWCNTs are of prime importance. The quality of MWCNTs could be substantially improved by optimising the CVD conditions²⁷⁻³⁰ or post-synthesis heat treatments³¹⁻³⁶.

Previous reports^{33–35,37} suggest that at temperatures beyond 2000 °C, CVD MWCNTs are purified, residual catalyst particles are removed, and the samples exhibit more intense characteristic (002) X-ray diffraction (XRD) and Raman G and 2D peaks. However, since high-temperature (≥ 2000 °C) processing of MWCNTs supported on common CVD substrates such as alumina, silicon and quartz could melt the substrate, the MWCNT powder is often collected off the CVD substrates and placed into annealing crucible. This transfer disturbs the original on-substrate alignment of MWCNTs which means that even if the annealing treatments improve any aspect of the MWCNTs, exploitation of the asymmetric nature of the VA-MWCNTs in a target application is not an option anymore. In contrast, VA-MWCNT carpets are often rigid enough and easily removable from the CVD substrates, if the thickness of the carpet is at least in the millimetre range^{30,38–42}. VA-MWCNT carpets of such thickness can be easily handled, treated, and still retain their original alignment. Considering the recent advancements in cost-effective synthesis of large-area (90 cm²³⁰ or up to *c.a.* 700 cm²^{43,44}) carpets of ultra-long MWCNTs, evaluation of the effectiveness of post-synthesis heat treatment on the bulk properties of these relatively new macroscopic morphologies of MWCNTs seems essential. The work by Fujisawa *et al.*³² highlights the effect of annealing on a bulk property of MWCNTs, *e.g.*, their volume resistivity and their work is complementary to the aforementioned classic reports on the effect of annealing on *structural* properties (crystallinity, purity, *etc.*). Moreover, although prolonging the deposition time yields thicker carpets, the purity and crystallinity of individual tubes are reported to decrease during the course of CVD^{29,30}. Hence, the post-synthesis treatments on large-area carpets of ultra-long MWCNTs, which are generally of lower quality compared to short powder-like MWCNTs produced by means of CVD, appears even more crucial to study.

In this work, we investigated the effect of heat treatment (2350 °C in argon atmosphere) on the properties of free-standing large-area (few cm²) carpets of ultra-long (few mm) VA-

MWCNT such as self-integrity (the ability to remain intact), alignment, crystallinity, defect density, oxidation resistance, purity, dispersibility and bulk mechanical properties. In addition, we also exposed VA-MWCNT carpets directly to very high temperatures and helium-carbon plasma in order to study their behaviour under extreme arc-discharge temperatures.

2. Experimental

VA-MWCNT carpets were produced using a semi-scaled-up³⁰ aerosol-assisted chemical vapour deposition (AACVD) setup reported previously^{27–30,45}. Subsequently, the VA-MWCNT carpets (thickness: 2–3 mm³⁰) were peeled off from a 10 cm by 9 cm silicon substrate for further post-synthesis treatment and characterisation (figure 1).

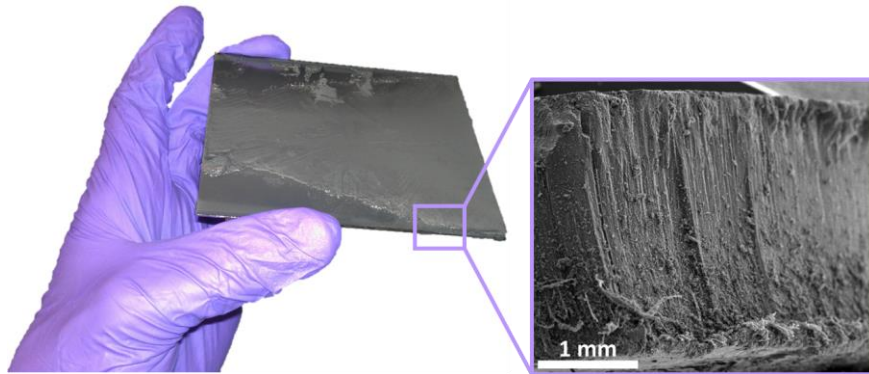


Figure 1. Free-standing VA-MWCNT carpet.

The heat treatment was carried out using a hot press (FCT Systeme GmbH) under constant 30.0 mbar 10% helium / 90% argon atmosphere without applied pressure. The samples were heated at 20 °C/min up to 2350°C, and kept for 3 hours before cooling down. The compression moduli of samples were measured using a cantilever based nanoindenter (Piuma Nanoindenter by Optics11), with a spherical indentation tip of 72 µm. The nanoindenter uses fibre-based optical interferometry to measure the indentation force and displacement at nanometre level. Indentation depth was 5 µm for ‘shallow’ indentation and 15 µm for ‘deep’ indentation, with a maximum indentation velocity of 6.7 µm/s. Compression moduli of

samples was estimated from the load-indentation curves using the Oliver and Pharr method⁴⁶, where the slope was estimated between 65% and 85% of maximum load. The plasma treatment was performed in an arc discharge reactor. The starting vacuum was 3×10^{-4} Torr and the chamber was subsequently filled with helium to a pressure of 50 mbar ensuring minimum presence of oxygen. Graphite rods supplied by Poco Graphite were used as the anode. The carpets were then wedged in a slit in the anode as shown in figure SI1 (supplementary information), so that some MWCNTs are in contact with the anode, and some are suspended. The arc took place between the carpets and a robust graphite electrode. The conditions of the annealing were 200 A DC current and 20 s of arc discharge, repeated 3 times.

Scanning electron microscopy (SEM), high-resolution transmission electron microscopy (HRTEM), selected area electron diffraction (SAED), Raman, thermogravimetric analyser (TGA), XRD and X-ray photoelectron spectroscopy (XPS) were used to study the structural properties of MWCNT samples (for details see the supplementary information).

3. Results and discussions

3.1. Heat treatment of large-area carpets of ultra-long MWCNTs

Figure 2 depicts the microstructure of the carpets before (**a-c**) and after (**d-f**) the heat treatment. Comparing the micrographs **a** and **d** in figure 2 reveals that at scales of around 100 μm , the alignment of MWCNTs in the heat-treated carpets is improved. This can be ascertained from the majority of individual MWCNTs remaining straight and parallel to the direction of growth over few-tens-of-microns lengths. In contrast, the local arrangement of MWCNTs in sub-micron scales was not hugely altered as shown in micrographs **e** and **f** (to be compared with **b** and **c** respectively).

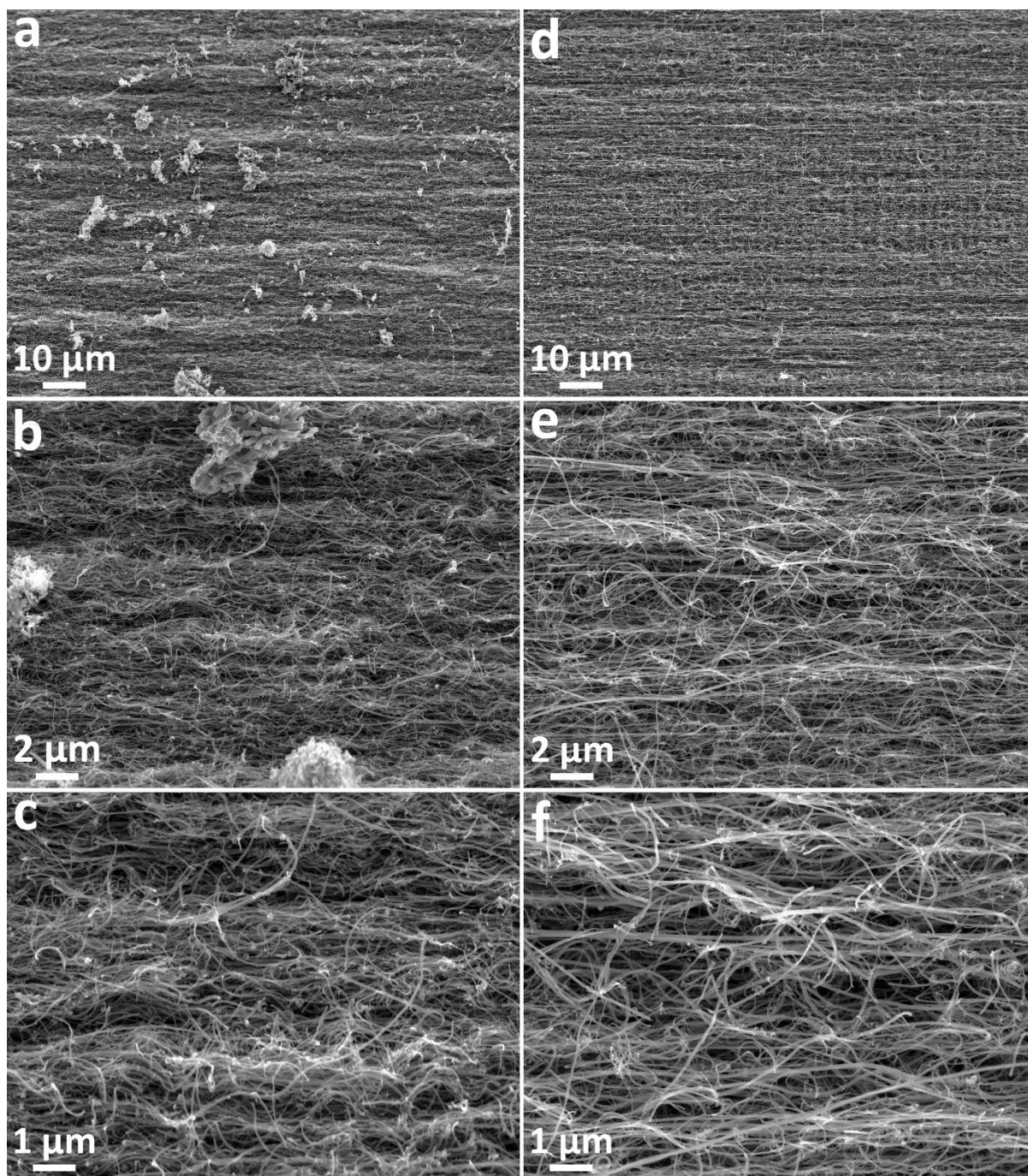


Figure 2. Scanning electron micrographs of the middle section of pristine (a, b and c) and heat-treated (d, e and f) carpets of VA-MWCNTs.

It is noteworthy that the MWCNT bundles within both the pristine and heat-treated carpets were generally more compact and aligned at the roots compared to the tips (see figure SI2). Therefore, the middle section of the carpets was used in SEM study. Comparing the TEM micrographs **a** and **d** in figure 3 shows that at scales of around 100 nm, the internal structure

of individual tubes in the heat-treated carpets exhibit less morphological distortions (bending, wall rupture, non-tubular graphitic particles, *etc.*), suggesting an overall enhancement of crystallinity. However, at scales of a few nanometres (compare micrographs **b** and **e** in figure 3), the arrangement of atoms in the lattice appeared unchanged. This implies that although the MWCNT crystallites have been partially annealed and aligned, full re-crystallisation of this type of CVD-grown MWCNTs is probably not achievable at these temperatures (2350 °C).

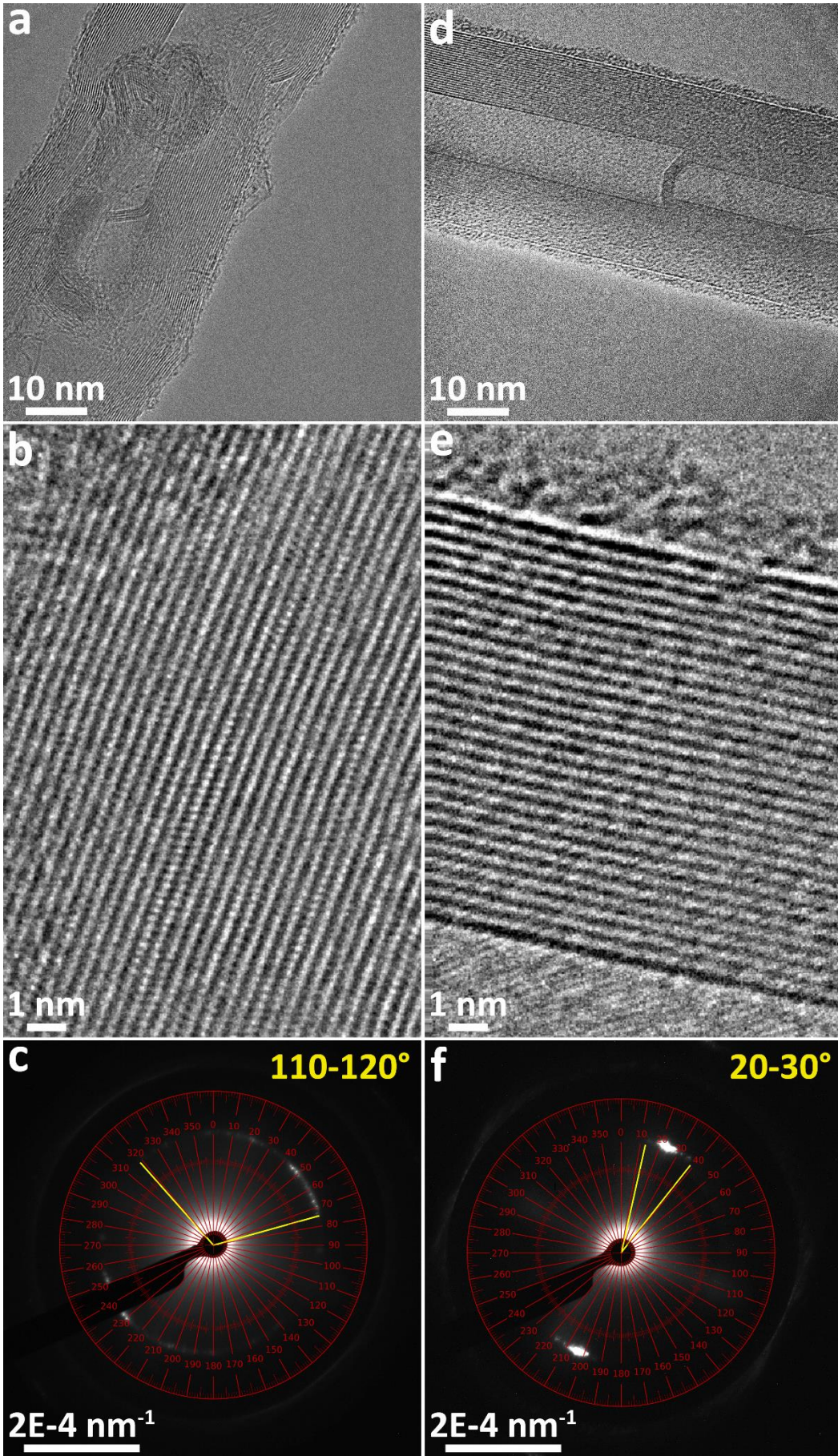


Figure 3. Transmission electron micrographs of pristine (a and b) and heat-treated (d and e) individual MWCNTs. Representative diffraction patterns of individual pristine (c) and heat-treated (f) MWCNTs.

This observation is in good agreement with the extensive studies of Franklin^{47,48} who argued that graphitisation and growth of crystallites in graphitic materials are strongly dependant on the relative initial orientations of neighbouring crystallites, and further graphitisation predominantly occurs by rearrangement of graphitic layers rather than movement of individual atoms. Here, we can similarly reason that despite the partial alignment and enlargement of MWCNT crystallites, the severe misalignment of crystallites which originated from the uncontrolled phenomena involved during the CVD requires a much higher energy/annealing temperatures to overcome. The original size of crystallites in CNTs during the synthesis could not be controlled neither, as their formation mechanism is fundamentally different from other sp^2 allotropes of carbon. For instance, unlike the case of CVD graphene, in which the size or morphology of crystallites (grains) can be controlled by the number of nucleation sites^{49–52}, crystallographic orientation of the underlying catalyst⁵³ and time^{52,54,55}, the crystallites in MWCNTs are likely to originate from the dynamics of the catalyst particles, as shown in a number of *in situ* microscopy studies^{56–60}. As the catalyst particles deform and/or change directions (in the case of tip-growth mechanism), new crystallites are born which are not necessarily in line with the preceding one(s). In order to avoid this, one might propose that new catalyst particles which are immobilised and do not exhibit constant deformation at temperatures below 1000 °C, yet showing good catalytic activities for CVD of MWCNTs should be engineered in future.

Our microscopy observations are supported by a set of systemic comparisons of electron (local) and X-ray (bulk) diffraction patterns obtained from pristine and heat-treated carpets which are presented later in this section. The spacing between the atomic planes in the walls

of the pristine and heat-treated MWCNTs remained unchanged, certifying that the stacking of the graphitic layers is stress-free and fully relaxed even in pristine conditions.

Comparison of SAED patterns of isolated individual pristine and heat-treated MWCNTs conclusively revealed that the heat treatment reduces the polycrystallinity of the MWCNTs. Random misorientations between different crystallites in MWCNTs results in arc-shaped (002) reflections in SAED patterns. Hence, measurements of the spot arc angle in the SAED patterns of untreated and heat-treated MWCNTs will provide an indication of the improvement of the crystalline quality after heat treatment. Examples are shown in Figure 3c and 3f and SI3. After removing the contribution of possible local tilts of the MWCNTs in the selected area for diffraction to the overall arc angle, it was concluded that there is a 60% improvement on average of the crystalline quality after the heat treatment, even though the standard deviation is large. As discussed earlier, the alignment of individual domains in the structure of MWCNTs which exhibit monocrystallinity is believed to be more energetically favoured than recrystallisation, and hence, is more probable. This local characterisation was supported by comparing the XRD patterns of bulk pristine and heat-treated carpets (figure 4). Both samples exhibited a sharp distinguishable (002) peak at around 26° , indicative of graphitic structure. The doubled intensity and 20% decrease in the full width at half maximum (FWHM) of the (002) peak confirmed improved crystallinity and increase in the size of crystallites in the heat-treated sample. The (100) and (004) peaks were also more pronounced in heat-treated samples while the elimination of the peaks associated to the residual catalyst particles (carbides and oxides^{33,34}, marked with asterisks) suggested purification of samples. Our SEM study (figure 2) and TGA results (figure 5a and 5b). Confirmed the purification.

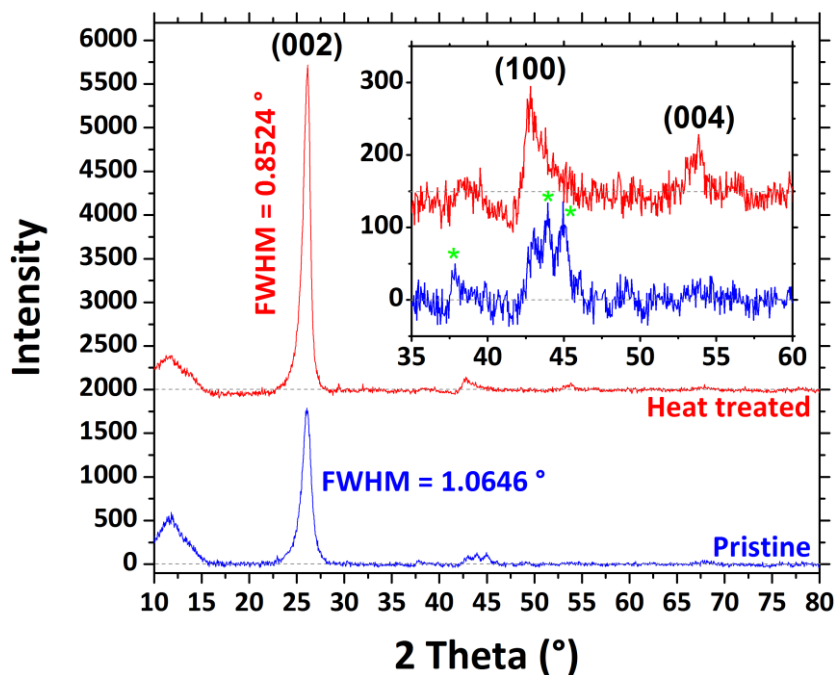


Figure 4. X-ray diffraction patterns of pristine and heat-treated carpets of VA-MWCNTs.

The heat treatment substantially improved the resistance of MWCNTs to oxidation in synthetic air. The temperatures of 20%, 50%, and 70% mass loss were all increased by *ca.* 200 °C, while the maximum rate of mass loss was halved from -1.37 to -0.68 wt.%/°C. The improvement of oxidation resistance is believed to be mainly due to the decreased concentration of residual iron-containing catalyst particles [29,30] (concentration of iron before heat treatment: 2.0 wt.%; after heat treatment: 0.3 wt.%). The increased oxidation resistance of carpets probably has little to do with the defect density because, contrary to a similar study³⁷, our Raman results showed insignificant change in the D-band/G-band and 2D-band/G-band ratios (figure 5c and 5d and SI4). We observed 20% decrease in the D-band/G-band ratio in the Raman spectra taken from the bottom of the carpets. Since the heat treatment effectively removes the catalyst particles and the carpets were synthesised in a bottom-growth fashion, this decrease is probably associated with the removal of the catalyst particles. The Raman D-band/G-band ratio of the core of the carpets were fairly position-dependant, but in average increased by around 0.2 after the treatment. The Raman 2D-

band/G-band ratios for pristine and treated samples did not change substantially except for the core of the carpets, in which the 2D-band/G-band ratio decreased by around 0.14. The origin of this decrease in the average Raman 2D-band/G-band and increase of the average D-band/G-band after the heat treatment is not fully understood yet, but given the relatively large uncertainty of the data and high sensitivity to the positions from which the spectra were taken, strong trends were not evident. Therefore, the annealing appears to be more effective in partial alignment of the crystallites of MWCNTs rather than healing the atomic-level defects. Due to the presence of relatively long and consequently heavily entangled MWCNTs in the carpets, dispersion of the samples could not be achieved and the carpets remained intact even after an hour of sonication using ultrasonic horn. Therefore, we were unable to drop-cast the samples and acquire average Raman spectra, representing the whole samples.

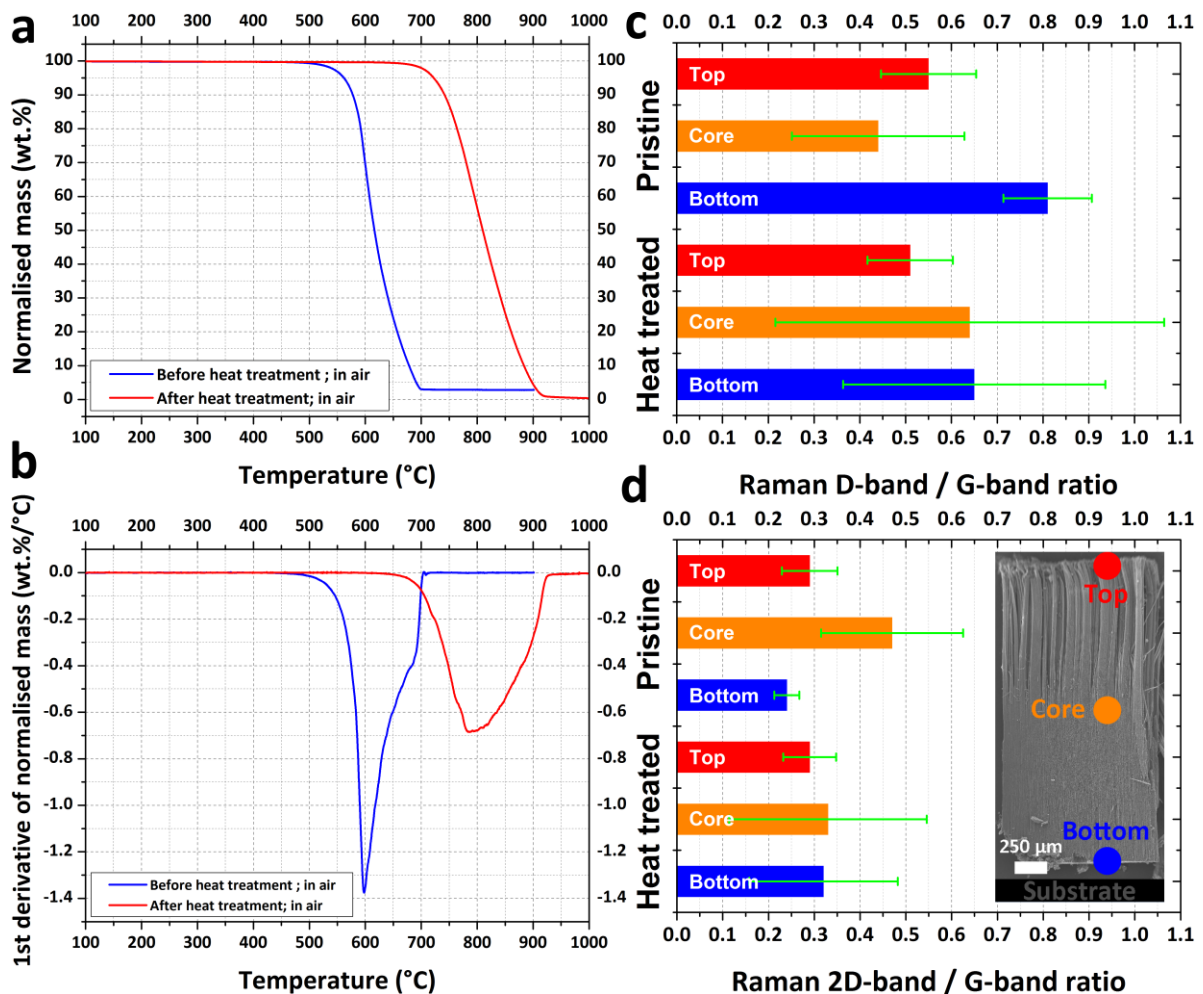


Figure 5. Oxidation resistance (a); oxidation rate (b); Raman D-band/G-band ratio (c) and Raman 2D-band/G-band ratio (d) of pristine and heat-treated carpets of VA-MWCNTs.

Measurement of the compression modulus of carpets using nanoindentation revealed that the heat-treated carpets, on average, show higher compression elasticity. Although the results were fairly independent of the indentation depth, the bottom and top of the carpets exhibited completely different compression moduli. The moduli measured from the top of both pristine and heat-treated carpets were comparable to values in literature^{38,61,62} (figure 6). However, the moduli measured from the bottom of the carpets were almost an order of magnitude higher than previously reported. This increase is not due to the presence of the catalyst particles at the bottom of the carpets nor is related to the defect density of individual MWCNTs, because the catalyst-free heat-treated samples showed even higher moduli (up to 120 MPa) and according to Raman (figure 5c) MWCNTs are more defective at the bottom. Therefore, this increase is probably due to the fact that at the bottom of the carpets the arrangement of MWCNTs is denser, smoother, and hence, the resistance to indentation is higher. Since our measurements were carried out on free-standing carpets, we were able to measure the moduli on both sides of the carpet, compared to previous works which were performed on supported carpets. To the best of our knowledge, the compression moduli of the bottom of these carpets are the highest values reported so far for VA-MWCNTs. Considering the anisotropic nature of CNTs, It is noteworthy to mention that the geometry of the indentation tip, force, displacement speed, *etc.* could potentially have a significant impact on the reported moduli. Therefore, the current study preliminarily provides an indicative comparison of improved compression moduli over the values previously reported in literature. In this regard, a metrology study formulating a *conversion table* for translation of the compression moduli of VA-MWCNT carpets obtained from different indentation setups

seems to be a necessary investigation for more accurate comparison of the moduli across the literature.

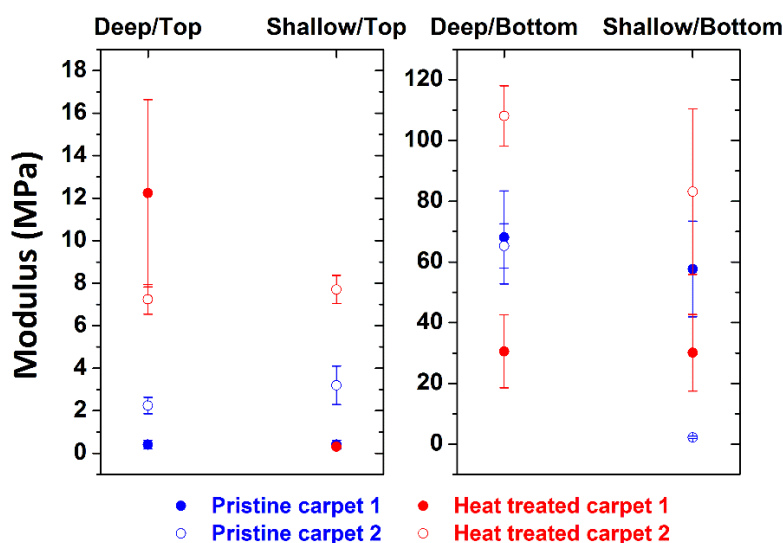


Figure 6. Compression moduli measured by nanoindentation on the bottom and top of the pristine and heat-treated carpets of VA-MWCNTs. ‘Shallow’ indentation: 5 μm ; ‘Deep’ indentation: 15 μm (for representative original load-indentation graphs see figure SI5 in supplementary information).

3.2. Plasma treatment of large-area carpets of ultra-long MWCNTs

Development of graphite-element furnaces to anneal MWCNTs at temperatures beyond 3000 $^{\circ}\text{C}$ is demanding^{63,64}. Alternatively, other sources of energy such as arc-discharge and laser could be considered to locally heat the carpets at temperatures as high as 10’000-20’000 K^{65,66}.

In our case, arc-discharge was used for localised heating of VA-MWCNT carpets. Arc-discharge did not significantly alter the morphology of the portion of VA-MWCNT carpets wedged in the graphite anode, possibly because the carpets were not directly exposed to the arc, or because there is a significant temperature gradient even at short distances from the arc. On the other hand, the suspended carpets yielded a rather interesting composite consisting of

graphite, CVD MWCNTs and arc-discharge-like CNTs⁶⁷. The preliminary results are presented in the supplementary information.

4. Conclusions

Post-synthesis processing of free-standing large-area carpets of ultra-long MWCNTs was shown to favourably alter their microstructure and properties. Heat treatment of VA-MWCNT carpets up to 2350 °C improved the overall sample purity and resulted in partial alignment of neighbouring crystallites only. It does, however, appear that full annealing of the material at nano and sub-nano scales, *e.g.* removal of point defects, is challenging. Nanoindentation on the VA-MWCNT carpets indicated a noticeable improvement in mechanical properties after heat treatment. However, it also showed that compression moduli of the bottom and top of the carpets (up to 100 MPa) varied significantly. This difference is not linked to the presence of catalyst particles or the defect density of individual tubes but it is due to the change in separation of the VA-MWCNTs at the root compared to the top surface. Exposure to arc-discharge plasma was found to largely transform the VA-MWCNTs into a novel carbon-carbon composite material which is of scientific interest in its own right, but beyond the scope of this present study. The development of processing procedures at higher thermal energies – than typical high-temperature furnaces provide – but less violent than plasma temperatures – to avoid evaporation and contamination – is essential to further improve the crystallinity and stiffness of the VA-MWCNT carpets and to exploit these in end-user applications.

Acknowledgements

The funding bodies who supported this work are European Commission's Seventh Framework Programme CONTACT and BioBone Marie Curie Initial Training Networks; Royal Society; European Research Council Starting Grant (ERC-2009-StG 240500 DEDIGROWTH); European Research Council Proof of Concept (ERC-2012-PoC309786

DEVICE & CONDUCT); the UK Government for Engineering and Physical Sciences Research Council (EPSRC) for the fellowship programme ‘Manufacturing the future: endohedral fullerenes, small molecules, big challenges’ (EP/K030108/1), Pathways to Impact grants and Impact Acceleration Accounts.

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