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## Risk Analysis - An Economic Comparison of Oil and Coal Power Plants

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"RISK ANALYSIS-AN ECONOMIC COMPARISON OF OIL AND  
COAL POWER PLANTS"

BY

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B.S., University of South Florida, 1978

RESEARCH REPORT

Submitted in partial fulfillment of the requirements  
for the degree of Master of Science in Engineering  
in the Graduate Studies Program  
of the College of Engineering  
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1980

## ABSTRACT

The demand for electric energy increases every year. However, due to recent changes in the U. S. energy supplies, a growing gas shortage forced suppliers to curtail deliveries of natural gas for power generation. Many utilities anticipating supply problems switched to burning more costly light distillate oil. Unfortunately the Arab boycott of 1973 and the following price increases for oil forced again utilities to seek a cheaper source of fuel, namely coal, as a substitute for oil. Even though the U.S. has abundant supply in coal, the use of coal in power generation was limited in the past because of a higher capital cost associated with installing air pollution control devices. Therefore, current utilities primary concerns are "Does the lower fuel price of the coal power plant really outweigh its disadvantage of higher construction costs as compared to the oil-burning power plant?". Thus, the purpose of this paper is to evaluate the economic preference of the coal burning power plant compared to the oil-burning power plant in supplying base load power. An extensive analytical model accounting for the effects of escalating fuel prices was examined and a computer simulation model was developed to handle risk associated with various input parameters using the SLAM as a simulation language.

To my Father, Haaj Mohammad Reza, who has always inspired an interest in learning and a desire for academic achievements.

## ACKNOWLEDGEMENT

I would like to express my sincere thanks to Dr. Chan S. Park, my advisor, for his guidance and encouragement in the preparation of this report. I would also like to express my gratitude to Dr. Gary E. Whitehouse, the Chairman, whom I feel indebted to for his help and understanding.

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## CHAPTER 1

### INTRODUCTION

Fossil fuels are used to generate ninety percent of the electricity needed in the United States. In particular, coal has been a major contributor to U.S. energy needs for the past several decades. Its growth was limited by the abundance of cheap oil and gas in the past. However, the price increases following the Arab oil embargo of 1973 and the increase in demand for energy have again made coal a competing fuel for energy production. The use of coal faces many challenges because of its environmental impacts, but its ready availability makes it increasingly attractive.

#### Statement of the Problem

Coal is the most abundant domestic fossil resource with identified reserves sufficient to meet the nation's needs for an estimated 200 years. The combustion of coal produces airborne emissions of particulates, nitrogen and sulfur oxides. These emissions must be reduced to some acceptable levels specified by the environmental protection agency (EPA).

In many cases the flue gas desulfurization method is used to reduce the pollution. Scrubbers are installed to process the limestone which absorbs the sulfur oxides. The cost of pollution

control equipments and their installation constitutes a high portion of the total construction cost for a coal power plant. The cost of limestone consumed and also the cost of maintaining the pollution control equipments are high during the operational period.

The pollution resulting from burning oil is relatively minimal. For this reason the construction and operating and maintenance costs of an oil power plant are considerably lower than those of a coal power plant. However, the fuel cost for an oil power plant is much higher than of the coal power plant and it has been escalating during the last several years. Therefore, utilities primary concern is "What ranges for fuel cost of an oil power plant would make coal power plant the more economical alternative?".

#### Objective of the Report

The primary purpose of this research is to develop a methodology for evaluating economics of power generations under uncertainty. The objective will be accomplished in two steps.

- 1) Development of an analytical model - Of particular concern is the development of a comprehensive analytical model which incorporates various decision variables into a decision criterion which ultimately measures the desirability of power plant.
- 2) Simulation Model - Given the lack of available actual

data and the need to examine the performance of the models under a variety of conditions regarding investment settings, the logical alternative is to select a simulated environment in which the important parameters generating investment data could be controlled.

### Plan of Study

Chapter 2 provides a description of power plants selected for this study. Electricity generation by using fossil fuel is explained, and the environmental effects of burning fuels and method of pollution control are discussed.

In Chapter 3, a comprehensive mathematical model is presented for evaluation of power generation economics. All the cost elements during the construction and operational periods are identified and an algebraic relationship for calculating the total equivalent annual cost is derived.

Chapter 4 describes the risk analysis model for this study. The factors subject to uncertainty are identified and their probability distributions are discussed. SLAM, a FORTRAN based simulation language is selected to simulate the economic model of this study. The SLAM network model is presented and an explanation of this model is given. The program is developed based on the mathematical model presented in Chapter 3.

In Chapter 5 both the data used to develop probability distributions and the data estimated with certainty are explained.

The results of risk analysis are shown in Chapter 6. In this Chapter the expected cost of generating electricity by using coal is compared to the expected cost when using oil. The resulting probability distributions and also the probability distribution of the difference in cost between the two alternatives are shown. By using the distribution of the difference in cost of the two alternatives the probability that the coal power plant is more economical can be determined. The interrelationships and sensitivity of the alternatives to changes in input parameters are then analyzed.

Chapter 7 contains the summary and conclusions of the report along with recommendations for future research.

## CHAPTER 2

### DESCRIPTION OF POWER PLANTS

In this Chapter electricity generation by using Fossil Fuel is explained. Also the environmental effects of burning fuels and related regulations are discussed.

#### Power Generation Technique

The essential stages involved in a steam turbine electricity plant are outlined in Figure 1.

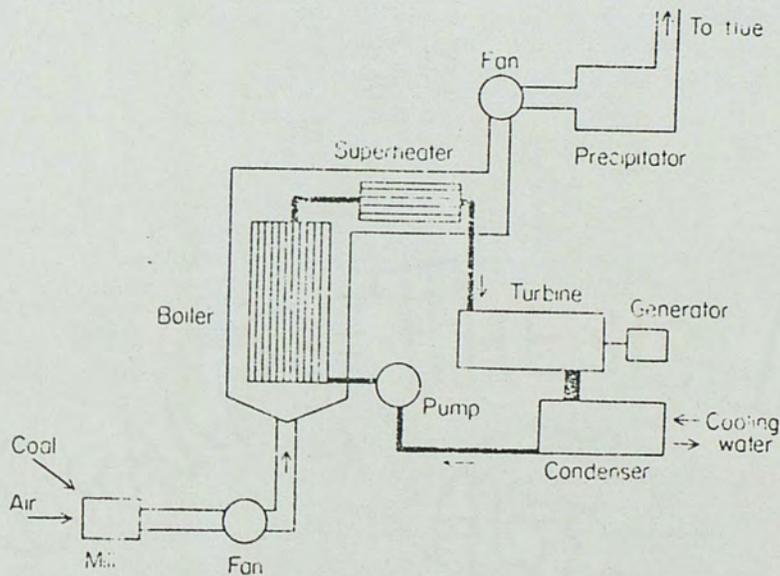


Figure 1. STEAM TURBINE ELECTRICITY GENERATOR  
Source: J. T. McMullan; R. Morgan; and R. B. Murray.  
"Electricity Generation and Transmission"  
Energy Resource and Supply (New York:  
Wiley-Interscience, 1976): 176.

The fuel, usually coal or oil is burnt in a type of burner. The heat released in combustion is extracted in the boiler, where it is used to raise steam at as high temperature as possible. The steam drives the turbine, and then passes to the condenser, is condensed to water and returned to the boiler. The turbine drives an alternator (AC Generator) whose output is transformed to a high voltage and transmitted to the consumer, where the voltage is reduced to a more appropriate value for the consumer's purposes.

The burning of fuels creates environmental air pollution problems. The pollution is mainly due to the emission of sulfur oxides and particulates from burning fossil fuel. The pollution resulted from burning oil can be kept below allowable limits by using oil with a lower sulfur content. But when coal is used the pollution is more damaging and needs to be controlled by some technological means. A typical 1000 MW coal power plant releases  $10^7$  tons of sulfur dioxide and nitrous oxide and  $10^5$  tons of ash to the atmosphere each year [1]. Based on the environmental regulations, the pollution from burning coal should be limited. The 1976 new source performance standards (NSPS) specifies the allowable pollution caused by burning coal as  $1.2 \text{ lb}/10^6 \text{ BTU SO}_x$ ,  $0.1 \text{ lb}/10^6 \text{ BTU}$  particulates and no standard for  $\text{NO}_x$ .

#### Pollution Control Technique

In this study it is assumed that flue gas desulfurization method is applied to control the coal plant pollution. For the

1000 MW plant size six desulfurization units are needed. Limestone is used and processed to absorb 80<sub>x</sub> produced by the burning of the coal. Figure 2 shows the process diagram for the coal power plant with flue gas desulfurization. The contact of flue gas with a water slurry of limestone causes the SO<sub>2</sub> to react and form insoluble CaSO<sub>3</sub>.

Part of the recirculating slurry is purged to remove the sulfur compounds from the process. The flue gas is saturated, and flyash is removed in a venturi system. Then the flue gas passes through the scrubber, where SO<sub>2</sub> is absorbed into a recirculating slurry of limestone and reaction by-products. The clean gas is reheated before passing up the stack. The slurry circulates from the bottom of the scrubber to a holding tank, where the reaction of the dissolved sulfite with calcium ions occurs. Also at the reaction tank, fresh limestone slurry is added. The main flow of circulating slurry is returned to the top of the scrubber; the purge is thickened; the overflow water is returned to the circulating slurry; and the under flow is pumped to the disposal pond.

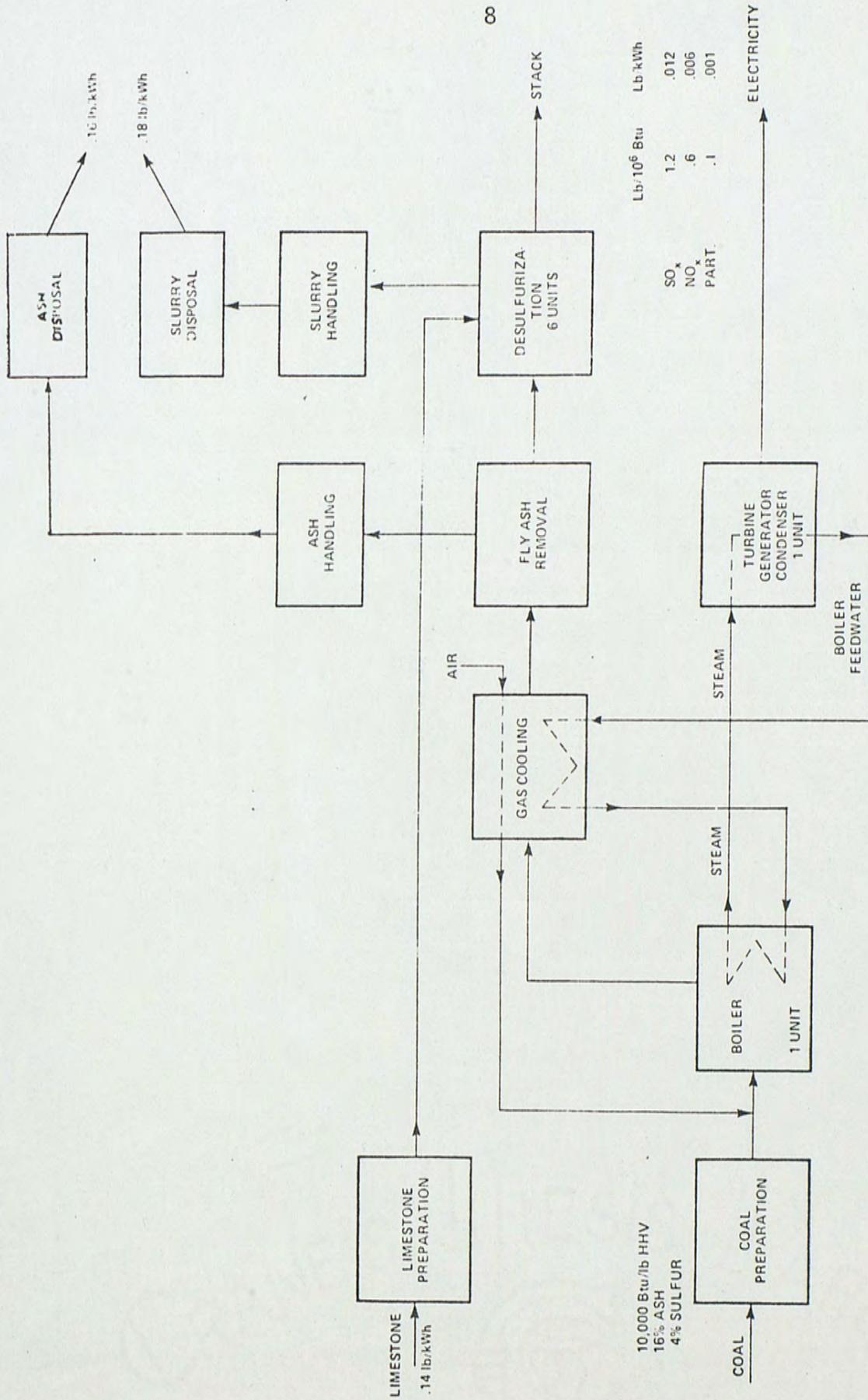


Figure 2. PROCESS DIAGRAM OF 1976 DESIGN COAL-FIRED PLANT WITH FLUE GAS DESULFURIZATION  
 Source: W. E. Balson, S. M. Barrager. "Case Study One: Comparison of Two Fossil Fuel Baseload Generation Technologies." Uncertainty Methods in Comparing Power Plants. California: EPRI, April 1979. 2-5.

## CHAPTER 3

### ECONOMICAL MODELING

In this Chapter a comprehensive mathematical model is presented for evaluation of power generation economics. In this model all the cost elements are identified and the total equivalent annual cost is calculated.

#### Structure of the Model

As shown in Figure 3, there are two phases in determining the total equivalent annual cost for each alternative. In Phase I the capital costs occurring during the construction period are calculated and in Phase II capital costs, depreciation charges and generation costs occurring throughout the entire plant service life are computed. The costs to be incurred during the construction period include debt finance cost, equity finance cost, insurance cost and Advalorem taxes. The costs related to the operational period are classified into three categories, i.e., capital costs, production costs and depreciation costs. Capital costs include debt finance cost, equity finance cost, insurance cost and Advalorem taxes. Production costs include fuel costs as well as operating and maintenance costs. Depreciation costs include depreciation costs and salvage value. Investment tax credit is received at the end of the construction period. All the tax deductible expenses are added to find the tax savings and then the after-tax cash flow is calculated. Finally the equivalent annual cost of the total

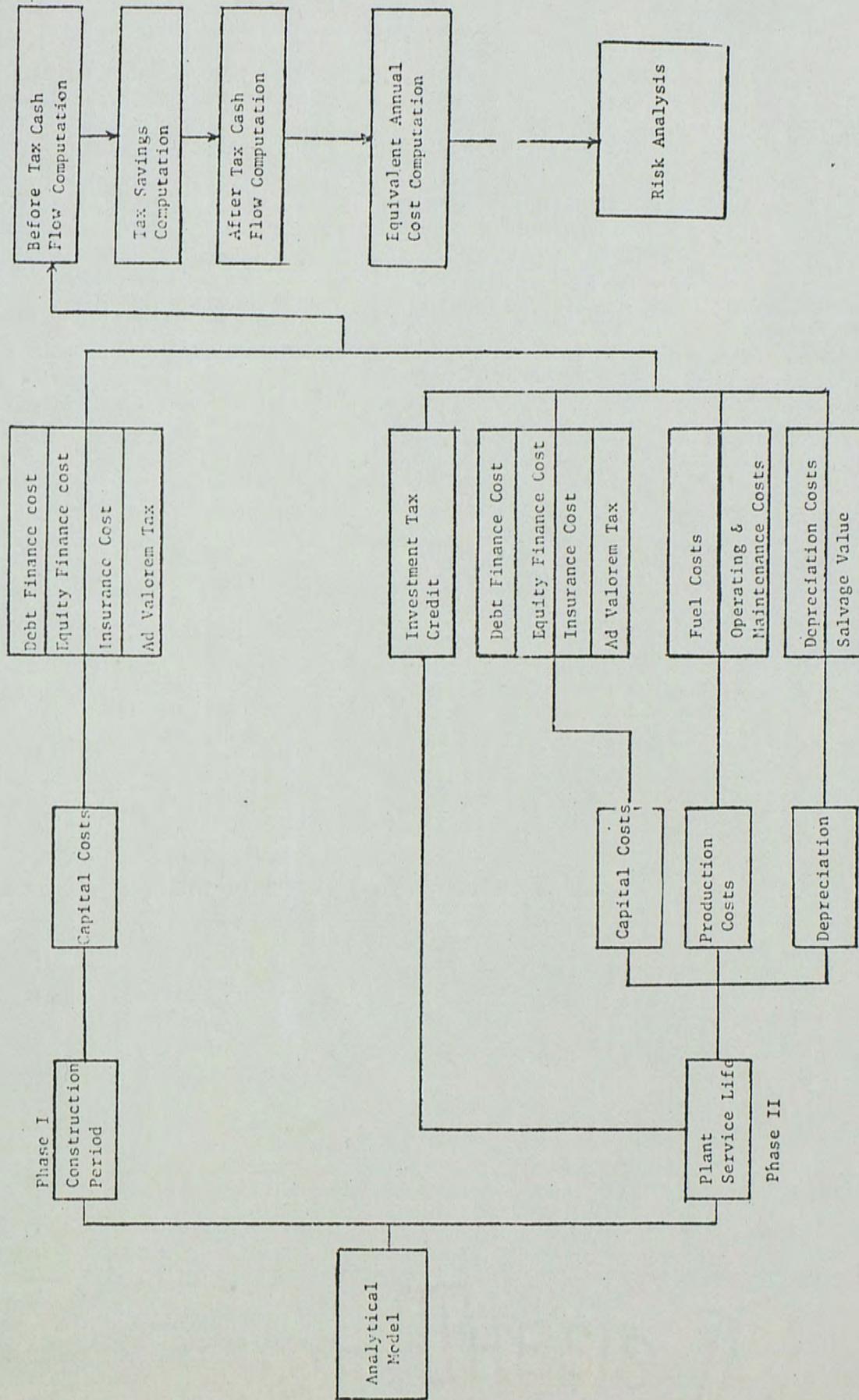


Figure 3. SYSTEMATIC MODEL BUILDING PROCESS

costs during the construction and operational period is determined.

All the costs are assumed to incur at the end of the year except the insurance cost which is paid at the beginning of each year.

### Model Description

#### Phase I Model

How the investment project is to be financed affects the investment decision. In this study, a mixed financing policy is assumed and the real cost of financing the investment is incorporated into the mathematical model. Common stocks are sold to provide new equity if there is no sufficient retained earning to finance the project and the remaining funds are financed by selling bonds. During the operational period, equal annual payments are made for the equity part of the funds. Each payment includes return on investment and principal repayment.

The principal for the issued bonds are paid at the end of operational period. A yearly interest is paid for these bonds during both the construction and operational periods. Thus, the only financial costs incurred during the construction period are the interest paid for the issued bonds and return on investment for the equity portion of the funds.

Followings are the detail cash flow formulations included in the Phase I model:

i) Debt Interest

$$DI_n = \left( \sum_{j=1}^n C_j \right) d i_d \quad (3-1)$$

$$n=1,2,\dots,N$$

where

$DI_n$ : Debt interest to be paid at the end of year n during the construction period.

N: The total number of years of construction.

$C_n$ : Plant construction cost in year n.

d: Debt ratio in financing mix.

$i_d$ : Debt interest rate.

ii) Equity Return

$$ER_n = \left( \sum_{j=1}^n C_j \right) (1-d) i_e \quad (3-2)$$

$$n = 1,2,\dots,N$$

where

$ER_n$ : Equity return to be made at the end of year n during the construction period.

$i_e$ : Equity return rate per year.

iii) Ad Valorem tax

The property tax is Ad valorem tax and it is based on the assumed value of property throughout the life of the project.

$$ADV_n = \left( \sum_{j=1}^n C_j \right) t_a \quad (3-3)$$

$$n = 1, 2, \dots, N$$

where

$ADV_n$  : Ad valorem tax to be paid at the end of year  $n$  during the construction period.

$t_a$  : Ad valorem tax rate.

iv) Insurance Cost

$$INS_n = \left( \sum_{j=1}^n C_j \right) \theta \quad (3-4)$$

$$n = 1, 2, \dots, N$$

where

$INS_n$  : Insurance cost in year  $n$ .

$\theta$  : Insurance rate per year (% of the total capital cost.)

v) Before-tax Cash Flow

The before tax cash flow during the construction period can be determined by adding i) through iv)

$$BTC_n = DI_n + ER_n + ADV_n + INS_n \quad (3-5)$$

vi) Adjustment for Tax Purpose

Interest paid on indebtedness is deductible as a business expense. This means that a project which is financed with borrowed capital has its taxable income reduced by the amount of interest involved. Since the equity repayments and insurance payments are non-tax deductible expenses, the adjustment figure for tax

purpose will be

$$TD_n = BTC_n - ER_n - INS_n \quad (3-6)$$

vii) Tax Savings

$$\begin{aligned} TS_n &= TD_n \cdot t \\ &= (DI_n + ADV_n) \cdot t \end{aligned} \quad (3-7)$$

where

$TS_n$  : Tax saving in year n during the construction.

t: Federal and State combined tax rate for income.

viii) After-tax Cash Flow

$$\begin{aligned} ATC_n &= BTC_n - TS_n \\ &= DI_n + ER_n + ADV_n + INS_n - (DI_n + ADV_n) \cdot t \\ &= (1-t) DI_n + ER_n + (1-t) ADV_n + INS_n \end{aligned} \quad (3-8)$$

where

$ATC_n$  : After-tax cash flows in year n during the construction.

ix) Equivalent Construction Cost

From equation 3-9, the total future worth of the Phase I model at the time the plant begins commercial operation can be computed as

$$FW(i)_I = \sum_{n=1}^N (ATC_n) (1+i)^{N-n} \quad (3-9)$$

where

$F_W(i)_I$ : Future worth of the project for Phase I.

i: Discount rate (or cost of capital).

### Phase II Model

The Phase II model consists of the total generation cost, and the capital recovery cost associated with the initial plant investment through the entire plant service life to calculate the future fuel cost as well as the operating and maintenance costs, it is necessary to determine the corresponding escalation rates. Following are the detail cash flow formulations involved in the Phase II model.

#### i) Fuel Cost

The fuel cost is a function of plant size, thermal conversion efficiency, and plant utilization factor. The fuel cost in each year would be calculated by the following:

$$F_n = (C)(H)(U_n)(8760/10^6) f_0 (1+q)^{n-1} \quad (3-10)$$

where

$F_n$ : Annual fuel cost in year n (\$).

C: Plant size in KW.

H: Heat rate at operating conditions in BTU/KWH.

$U_n$ : Plant utilization factor in year n.

$f_0$ : Fuel cost at the starting year (\$/10<sup>6</sup> BTU)

q: Average annual fuel escalation rate.

ii) Operating and Maintenance Cost (O&M)

Operating and maintenance costs consist of the fixed and variable portions. The fixed O&M cost can be expressed as function of the plant size, while the variable O&M cost is a function of the plant size, plant utilization factor, and efficiency of the plant.

The O&M cost can be written as:

$$(O\&M)_n = Of'_n + OU_n \quad \text{and} \quad (3-11)$$

Fixed Cost

$$Of'_n = (C) Of_0 (1+\Lambda)^{n-1} \quad (3-11-1)$$

where

$Of'_n$ : Fixed O&M cost in year n (\$).

$Of_0$ : Fixed O&M cost at the starting year (\$  
\$/KW)

$\Lambda$ : Average annual escalation rate of fixed O&M cost.

Variable Cost

$$OU_n = (C) (H) (U_n) (8760/10^6) OV_0 (1+\theta)^{n-1} \quad (3-11-2)$$

where

$OV_n$ : Variable O&M cost in year n (\$)  
(\$/10<sup>6</sup> BTU)

$OV_0$ : Variable O&M cost at the starting year

$\theta$ : Average annual escalation rate of variable O&M cost.

iii) Depreciation Cost

In computing depreciation deductions, a useful life and salvage value for the asset must be established. It is possible that the service life allowed for tax purpose may differ from the actual physical life of the asset as employed by the firm. Yearly depreciation deductions can be calculated by the following methods:

## a. Straight line depreciation method.

$$SLD = \frac{K - s}{n_d} \quad (3-12)$$

where

SLD: Straight line depreciation.

K: The total construction cost.

$n_d$ : The depreciable life.

s: Salvage value.

## b. Declining balance method

$$DB_n = R(1-R)^{n-1} \quad (3-13)$$

where

$DB_n$ : Declining balance depreciation.

R: Depreciation factor.

## c. Sum of years digit method

$$SYD_n = (K-S) \left( \frac{nd-n+1}{n(n+1)/2} \right) \quad (3-14)$$

where

$SYD_n$ : Sum of  $\left( \frac{nd-n+1}{n(n+1)/2} \right)$  years digit depreciation.

iv) Debt Finance Repayment

During the operational period the only payments for the debt portion of the funds are equal annual payments as the interest for the issued bonds and the principal of the debt portion is paid back at the end of the operational period.

$$\begin{aligned} DI_n &= Kd \cdot i_d & , \text{ If } n=1,2,\dots,T-1 \\ & Kd+Kd \cdot i_d & , \text{ If } n=T \end{aligned} \quad (3-15)$$

where

T: Plant service life in years.

$DI_n$ : Debt finance payment to be made in year n during plant service life.

v) Equity Finance Payment

The payments for the equity are paid by equal annual payments. A portion of this payment is for interest and can be calculated as:

$$ER_n = Kd(A/P, i_e, T)$$

where

$ER_n$ : Equity finance repayment to be made in year n during the plant service life.

$$\text{and } EIP = ( Kd i_e - ER_n ) (1+i_e)^T + ER_n [ 2 ] \quad (3-16)$$

where

EIP: The interest portion of the equity finance payment.

The debt portion of the funds also could be paid back by equal annual payment. In this case the interest portion of the payments should be calculated by using equation 3-16 and be considered as an expense for tax purposes.

vi) Ad Valorem Tax

$$ADV_n = (K - \sum_{j=1}^n D_j) t_a \quad (3-17)$$

where

$ADV_n$  : Ad valorem tax to be paid in year n during the plant service period

$D_n$  : Depreciation deducted for year n.

vii) Insurance Cost

$$INS_n = (K) \theta \quad (3-18)$$

where

$INS_n$  : Insurance cost to be paid in year n during the plant service life.

viii) Salvage Cost (Value)

If  $S_T$  is defined as the salvage value at the end of service life, then the end of year salvage as a function of n is given by:

$$S_n = \begin{cases} 0 & \text{If, } n \neq T \\ sK & \text{If, } n = T \end{cases} \quad (3-19)$$

where

s: Salvage rate.

ix) Before Tax Cash Flow

The total cash flow before tax at the end of nth year will be calculated by:

$$BTC_n = F_n + Of_n + OU_n + DI_n + ER_n + ADV_n + INS_n - S_n \quad (3-20)$$

x) Adjustments for Tax Purposes

Fuel cost, O&M cost, ad valorem tax, the interest paid for debt and the depreciation are tax deductible. For calculation of the tax deductible amount the following expression can be used.

$$TD_n = \begin{cases} BTC_n - TD_n - ER_n - INS_n & \text{If } n=1,2,\dots,T-1 \\ BTC_n + D_n - ER_n - INS_n + S_n - Kd & \text{If } n=T \end{cases} \quad (3-21)$$

where

$TD_n$  : Tax deductions in year n

xi) Tax Savings

$$TS_n = TD_n \cdot t$$

where

$TS_n$  : Tax savings in year n (3-22)

xii) Investment Tax Credit

$$ITC_n = \begin{cases} mK & \text{If } n=1 \\ 0 & \text{Otherwise} \end{cases} \quad (3-23)$$

where

$ITC_n$  : Investment tax credit in year n.

m: Investment tax credit rate.

xiii) After-tax Cash Flow

$$ATC_n = BTC_n - TS_n - ITC_n \quad (3-24)$$

where

$ATC_n$  : After-tax cash flow in year n.

xiv) Present Worth Equivalent

The total present worth of the Phase II model can be computed by using equation 3-25. This is the present worth at the time the plant begins its commercial operation.

$$PW(i)_{II} = \sum_{t=1}^T (ATC_n)(1+i)^{-n} \quad (3-25)$$

Annual Equivalent Cost Model

The cost of the two phase are combined together in order to find the annual equivalent cost.

$$AE(T,N,i) = \{FW(i)_I + PW(i)_{II}\} (A/P, T, i)$$

where  $AE(T,N,i)$ : The annual equivalent cost of the project.

The mathematical model developed in this Chapter includes all the cost elements which constitute the total cost of an investment. In order to incorporate explicitly the effect of inflation in the analysis, it

becomes necessary to use a combined discount rate in computing the annual equivalent cost. The combined discount rate is simply found by the following relation:

$$(1 + i) = (1 + k) (1 + i')$$

where  $i$  = combined discount rate

$k$  = the average inflation rate

$i'$  = the rate representing the earning power of money with no inflation

Based on this model, the risk analysis model is developed in the next Chapter.

## CHAPTER 4

### RISK ANALYSIS MODEL

Risk analysis consists of estimating the probability distribution of each factor affecting an investment decision, and then simulating the possible combinations of the values for each factor to determine the range of possible outcomes and the probability associated with each possible outcome [ 3 ].

In order to accomplish risk analysis, all the factors subject to uncertainty were well identified and probability distributions for all these factors were developed. Based on the analytical model described in Chapter 3, a computer program was developed in order to find the equivalent annual costs by incorporating the probabilistic information through Monte Carlo sampling techniques.

#### Identification of Stochastic Parameters

It is important to determine what the critical factors are which affect the economic choice between the two alternatives. In this study the important factors were identified through intuitive observation and sensitivity analysis. These factors are:

- Construction Cost.
- Fuel Cost.
- Operation and Maintenance Cost (Fixed and Variable).
- Fuel Escalation Rate.
- O&M Escalation Rate.

### Developing Probability Distributions

The probability distribution for all factors listed above need to be estimated. These distributions describe the likelihood of occurrence for the parameters. Three estimates, i.e., "optimistic", "pessimistic" and "most likely", for each factor are estimated by referring to various sources of information. It is assumed that these three estimates correspond to the "upper bound", "lower bound" and "mode", respectively, of the subjective probability distribution. The probability distribution is a beta distribution with a standard deviation equal to one-sixth ( $1/6$ ) of the spread between the lower and upper bounds. Beta type distributions provide flexibility and consistency in assessing probabilities in the risk analysis [4].

### Simulation

Once the probability distributions for all the important factors subject to risk are found, the equivalent annual cost that will result from a random combination of these factors needs to be determined. In Figure 4 the simulation process used in this study is illustrated. Monte Carlo methods are used to select values from probability distributions describing the likelihood of occurrence for the parameters having uncertainty. These selected values comprise a set of data utilized to compute the total equivalent annual cost for those parameters. This process is repeated with different sets of data being selected and an equivalent annual cost being computed for each set. By using these cost figures, a

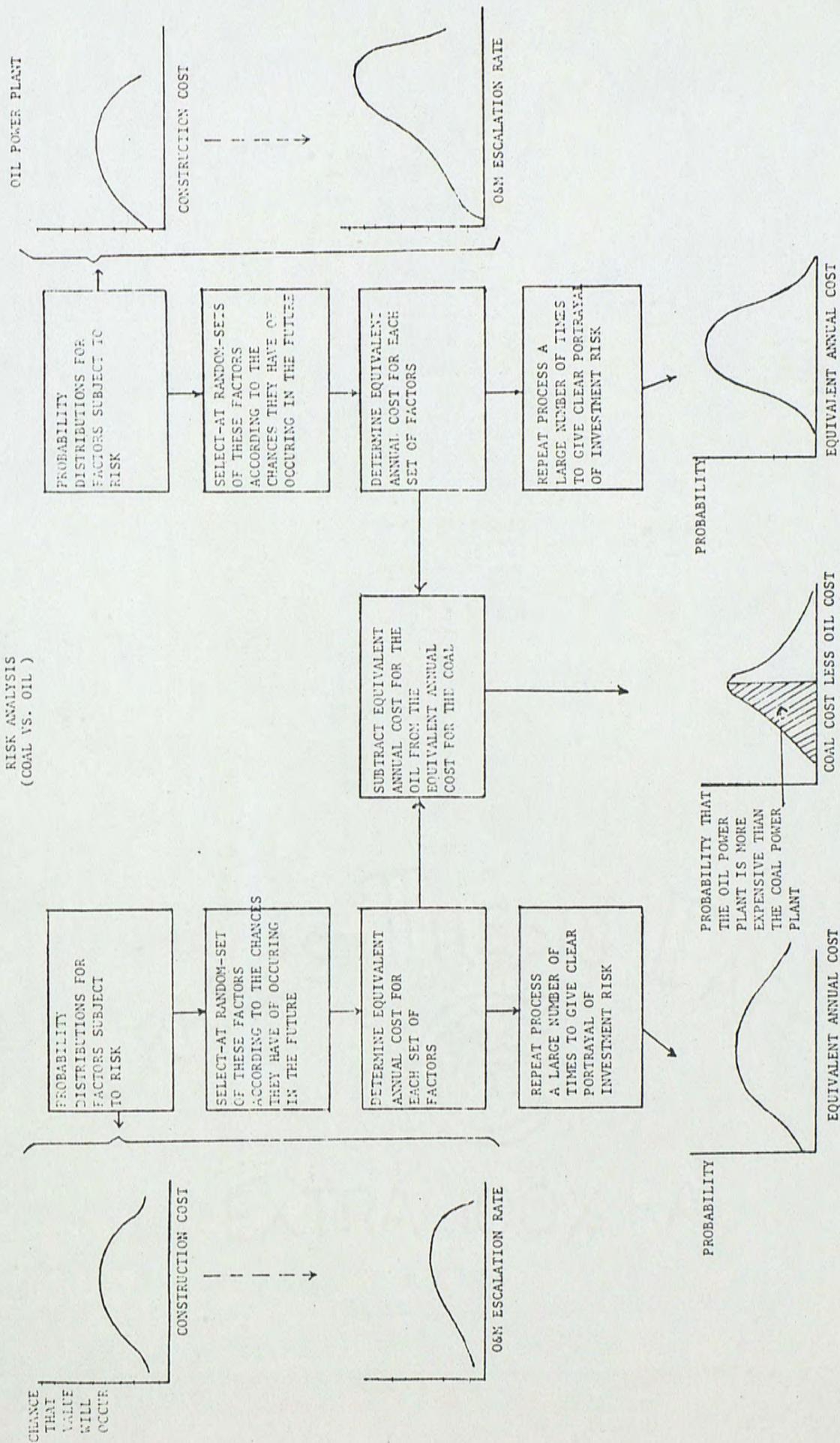


Figure 4. RISK ANALYSIS SIMULATION CHART

frequency distribution describing the likelihood that a particular equivalent annual cost might occur is generated. Then a probability distribution of the differences between the alternatives I (coal) and II (oil) is developed. From this probability distribution, the probability that alternative I will be less costly than alternative II can be determined.

#### Selected Simulation Language

For this study SLAM is used as the simulation language. Due to the flexibility inherent in SLAM, the complexities involved with programming models like the one used in this study are substantially reduced.

SLAM (Simulation Language for Alternative Modeling) is a FORTRAN based language which allows systems to be viewed from a process, event and state variable standpoint and all these can be combined in a unified systems modeling framework. In modeling this study's system, the process orientation of SLAM is most important and also unique. The process orientation of SLAM employs a network structure comprised of special symbols called nodes and branches in a manner similar to Q-GERT. These symbols model elements in a process such as queues, servers, and decision points. The modeling task consists of combining these symbols into a network model which pictorially represents the system of interest. Thus, a network is a pictorial representation of a process. The

entities in the system (such as people and items) flow through the network model. The pictorial representation of the system is transcribed by the modeler into a equivalent statement model for input to the SLAM processor. The use of SLAM as a simulation language facilitates the development of the necessary computer code to test and validate the risk analysis.

#### SLAM Modeling

A condensed network model for this is presented in Figure 5 and the statement listing is shown in Appendix 1. The explanation of the model will be given in terms of the statement listing. The model can be divided into four major segments. The first segment represents the initialization for all the data related to alternatives I (coal) and II (oil) and consists of statements 9 through 93. Statements 9 through 14 are initializations for values subject to uncertainty related to alternative I where three estimates, i.e., "optimistic", "most likely", and "pessimistic", are assigned to global variables.

The second segment shows the Monte Carlo sampling process for equivalent annual cost for alternative I and consists of statements 95 through 557. In this segment the costs during the construction and operational period are calculated and combined to give the result for the

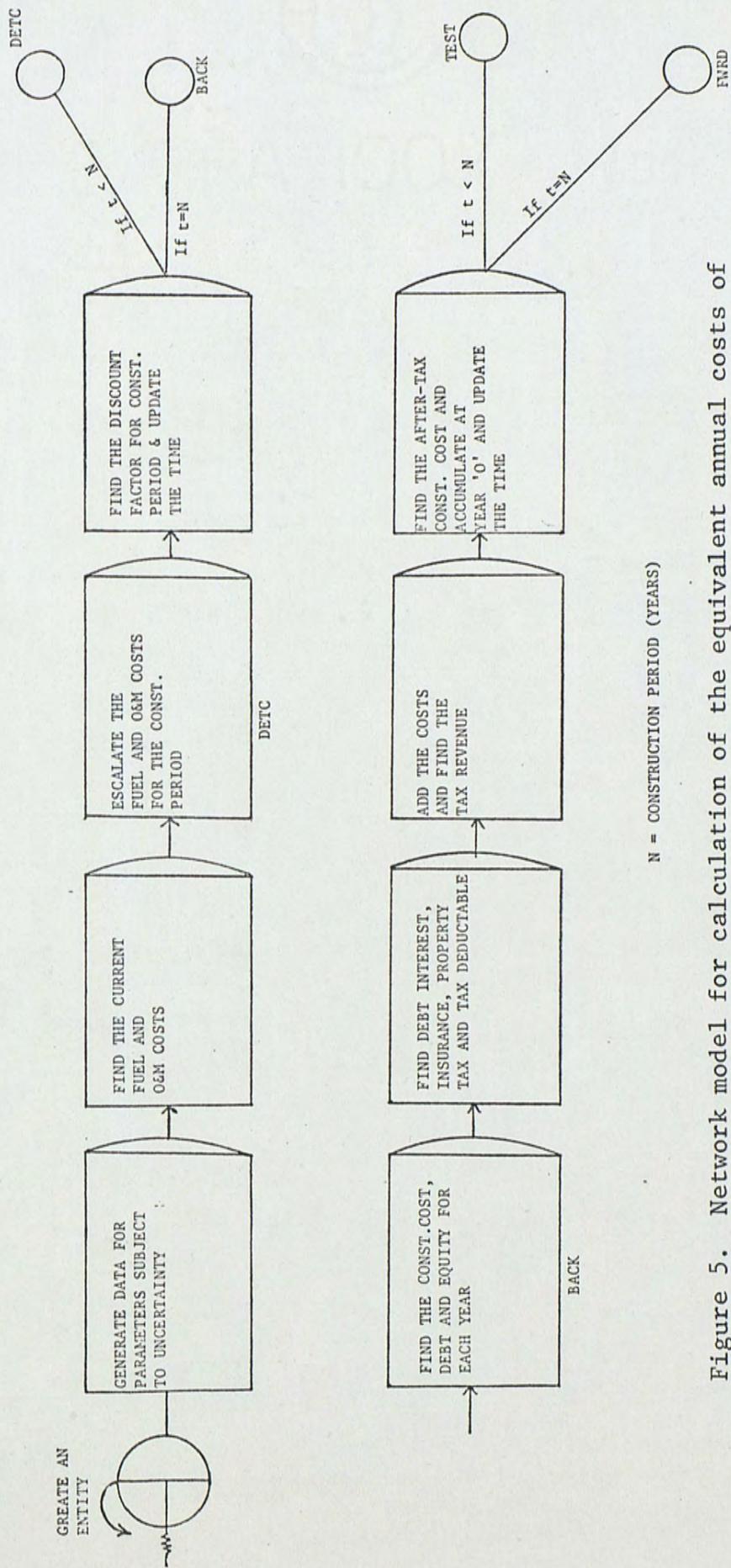


Figure 5. Network model for calculation of the equivalent annual costs of the two alternatives and their difference

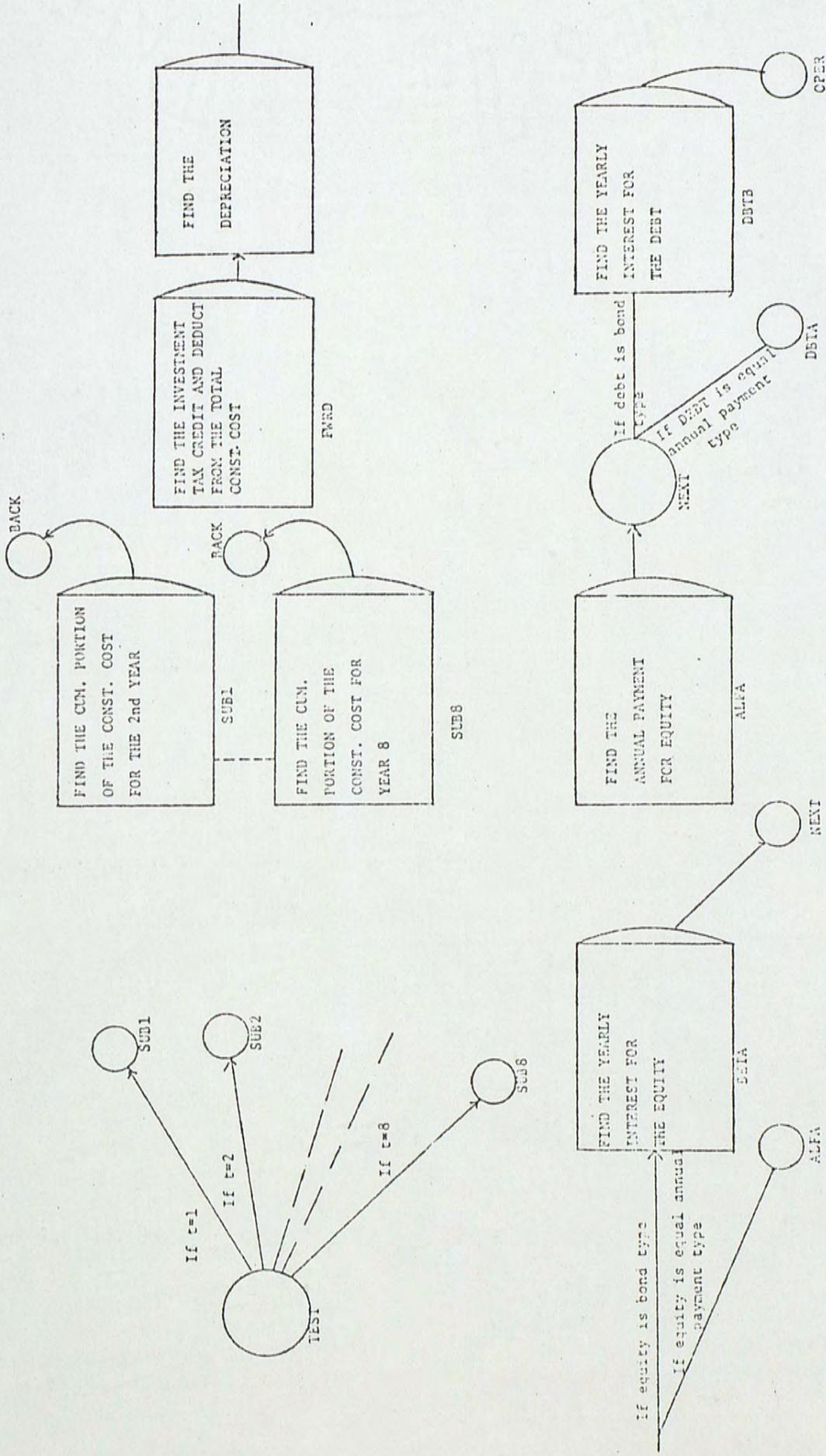
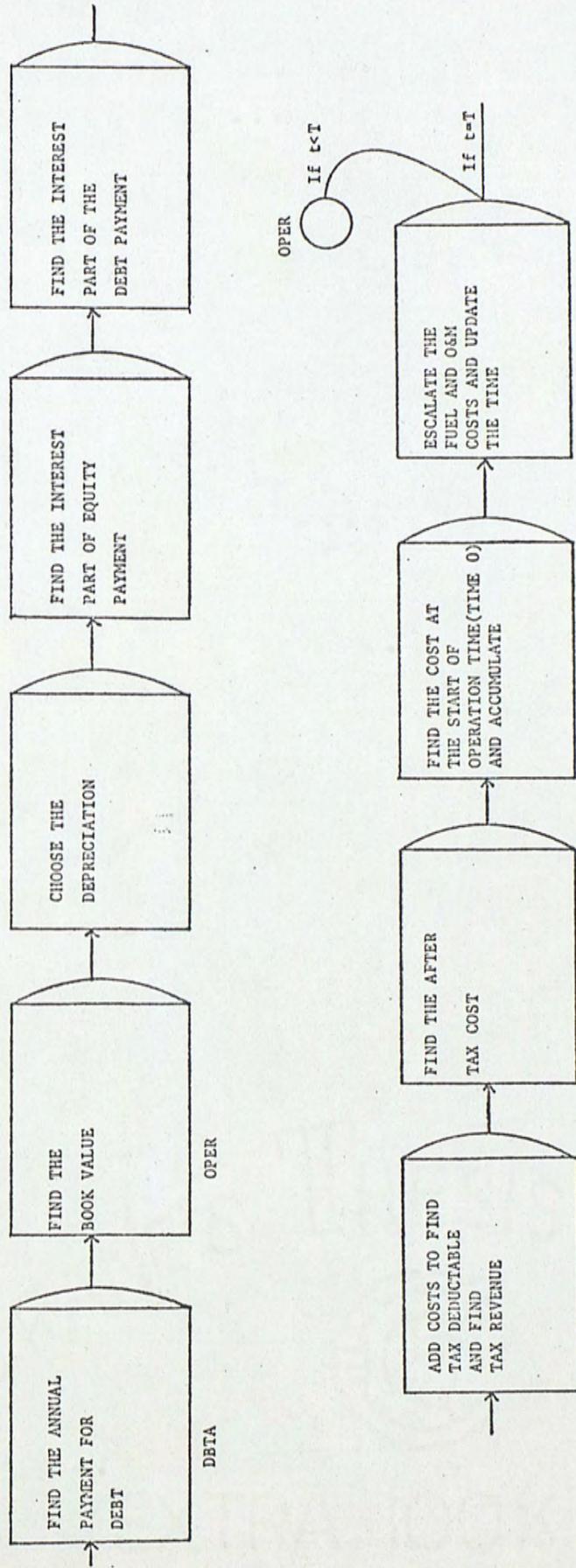


Figure 5. (Continued)



T = OPERATION PERIOD (YEARS)

Figure 5. (Continued)

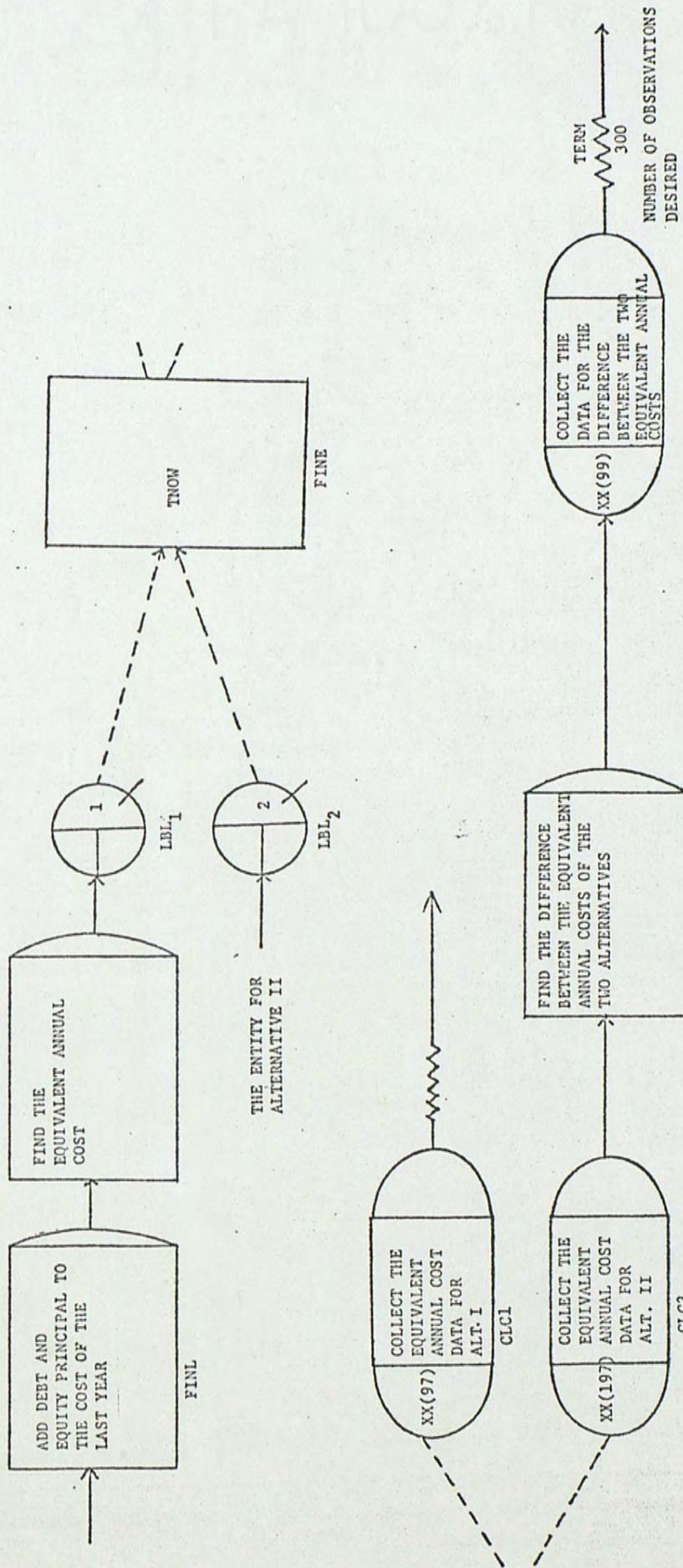


Figure 5. (Continued)

total cost for alternative I. This segment starts with the "network" statement which is the first statement of the network.

In the first part of this segment, the data subject to uncertainty are generated by the program. The following formulae show the relationship used for developing the distributions.

$$M = \frac{A\beta + B\alpha}{\alpha + \beta} \quad (4-1)$$

$$E = A + \frac{(B-A)(\alpha+1)}{\alpha+\beta+2} = \frac{1}{6} (A+B+4M) \quad (4-2)$$

where M: The most likely value of the parameter.

A: The optimistic value of the parameter.

B: The pessimistic value of the parameter.

E: The expected value of the parameter.

$\alpha$  &  $\beta$  : Parameters used to generate the beta distribution by solving equations (4-1) and (4-2).

The values of  $\alpha$  and  $\beta$  were found to be

$$\alpha = \frac{4(A-M)(A+B-2M)}{A^2 - B^2 - 2M(A-B)}, \quad \beta = \left(\frac{M-B}{A-M}\right) \alpha$$

These values were used in the SLAM statement, beta ( $\alpha, \beta, 2$ ) where 2 is the random number stream.

The value generated by the computer is the  $\frac{\alpha+1}{\alpha+\beta+2}$  portion of the equation (4-2), which is the mean of beta distribution and its value is between 0 and 1. Thus, the

value of random variable would be:

$$E=A+(B-A) \cdot \text{Beta}(\alpha, \beta, 2) \quad (4-3)$$

The fuel cost is calculated by using equation (3-10). Also the O&M costs are found by applying expressions (3-11-1) and (3-11-2). These costs are for the year when the construction begins and are escalated throughout the construction period. In the mathematical modeling explained in Chapter 3 different escalation rates were assumed for the fixed and variable portions of the O&M cost. However, based on the gathered data a single escalation rate can be applied to both portions of the O&M cost and in this study this rate is determined by ATRIB (85).

The present worth of the construction cost is calculated by statements 228 through 339.

The costs to be incurred during the construction period are equity return, debt interest, insurance cost, and Ad Valorem tax are tax deductible items and the tax savings for each year are calculated by equation (3-22). The present worth of the construction cost is calculated by multiplying the total construction cost of each year by a compound-amount factor to find the equivalent cost at the beginning of the operational period (time 0).

Calculation of the costs during the operational period starts from statement 348. The investment tax credit is received at the beginning of the operational period and this is shown in statement 349.

This program is designed to calculate three types of depreciation. Straight line (ATTRIB(31)), sum of the years digits (ATTRIB(58)) and declining balance (ATTRIB(53)) depreciation are calculated. Global variable XX(32) is related to straight line depreciation, and XX(33) and XX(34) correspond to declining line balance and sum of the years digits, respectively. According to the depreciation policy adopted one (1) is assigned to the respective global variable and zero (0) is assigned to the other two global variables. Statements 451 through 453 are for selection of the desired depreciation policy.

As discussed in Chapter 3, the equity and debt portion of the investment could be financed by equal annual payment policy or by issuing bonds. This program is designed with the flexibility of handling all possible cases of financing the investment. The global variables XX(48) and XX(51) correspond to equity and debt portion of the investment, respectively. According to the financing policy, these global variables are initialized at the beginning of the program. If the equal annual

payment policy is adopted one (1) and if bonds are issued (zero) 0 is assigned to the corresponding global variables. The interest paid for the debt portion of the investment is regarded as an expense and is a tax deductible expense. If the debt portion is financed by the equal annual payment policy, the interest portion of the payment should be calculated according to expression 3-16. This is accomplished in the program by statements 464 through 470.

In Chapter 3 the costs incurring during the operational period are discussed in detail. The fuel cost, O&M cost, Ad Valorem taxes and the interest paid for the debt are tax deductible expenses. These are all added to the depreciation to get the total tax deductible expenses and then tax savings for each year are determined (statements 477 through 484). The total after-tax cash flow during the operational period is multiplied by a discount factor to calculate the present worth at the time when the operation starts statement 502) Then all the values for the operation years are accumulated to find the total present worth of the investment.

The fuel and O&M costs are escalated by using the escalation rates which are generated at the earlier part of the program (statements 571 and 512). Thus, a

single escalation rate is assumed for the whole period of plant operation.

The principal for the total construction cost is paid back at the end of operational period if the funds are financed by issuing bonds. Finally, the equivalent annual cost is found by multiplying the capital recovery factor by  $A_{trib}(50)$  which is the present worth for the total cost during the construction and operational periods.

The third segment of the program represents the Monte Carlo sampling process for the equivalent annual cost of alternative II which is to be compared with alternative I. This is identical to the above procedure and consists of statements 566 through 807.

The last segment of the program represents a collection of equivalent annual cost statistics for each alternative and comparison of the two alternatives. The statements 808 through 818 represent this operation. The specific explanations are as follows:

By representing one particular sequence of Monte Carlo sampling of cash flow realizations as an entity, these entities are generated by the "CREATE" node (statement 96) and are routed to the assign nodes. The entities with the equivalent annual cost statistics wait in file 1 at the LAB1 QUEUE node to be compared with an

entity generated for alternative II. The identical simulation process is done for alternative II and the global variable XX(97) which carries the value of equivalent annual cost for alternative I can be interpreted as the counter part of XX(197) for alternative II. The entities with the equivalent annual cost statistics wait in file 2 at the LAB2 QUEUE node to be compared with those of alternative I.

In order to compare the two investment alternatives a MATCH node holds entities in files 1 and 2 at queue nodes LAB1 and LAB2 until there is an entity in each QUEUE node that has an ATTRIBUTE 90 value that is the same. Attribute 90 represents the mark time of both entities of alternatives I and II at their creation. This implies that the equivalent annual costs sampled from each alternative be compared in terms of their respective common sampling time period. Once a match occurs, the entity associated with alternative I is routed to the COLCT node LAB2 while the entity associated with alternative II is routed to the node CLC<sub>2</sub> where statistics are collected on the equivalent annual cost. Following the node CLC<sub>2</sub>, both entities arrive at the assign node (statement 817) where the difference equivalent annual costs is computed by  $XX(99)=XX(97)-XX(197)$ . At the completion of computation of the

difference in equivalent annual cost, the entity arrives at the COLT node where statistics are collected on the difference in annual equivalent costs. The 'TERM' statement then destroys the entity. The above process will repeat until the total number of entities to be processed on a simulation run reaches the number listed with TERM statement. The ENDNET statement denotes an end to the network description.

## CHAPTER 5

### INPUT DATA DESCRIPTION

In the previous Chapter the factors subject to risk were identified as construction cost, fuel cost, O&M cost and the escalation rate for the fuel and O&M costs. When Monte Carlo simulation is used, finding subjective probability distributions from which stochastic parameters are to be generated is a very important task. In this Chapter the data used to develop such probability distributions will be explained. Also the validity and source of the input data will be discussed.

#### Selection of Starting Base and Load Capacity

The year 1985 was selected as starting time for commercial operation of the plant so this would allow 5 years for construction of the coal power plant. Since most of the gathered cost estimates for construction, operating and maintenance is based on a plant size of 1000 megawatt (MW) capacity, this capacity was chosen for comparison purposes.

#### Plant Construction Cost

The construction cost data (\$/KW) used in this study is based on the assumption that the plant size is 1000 MW. However, for other plant capacities the costs vary substantially. Figure 6 shows the sensitivity of unit capital cost (\$/KW) to plant size.

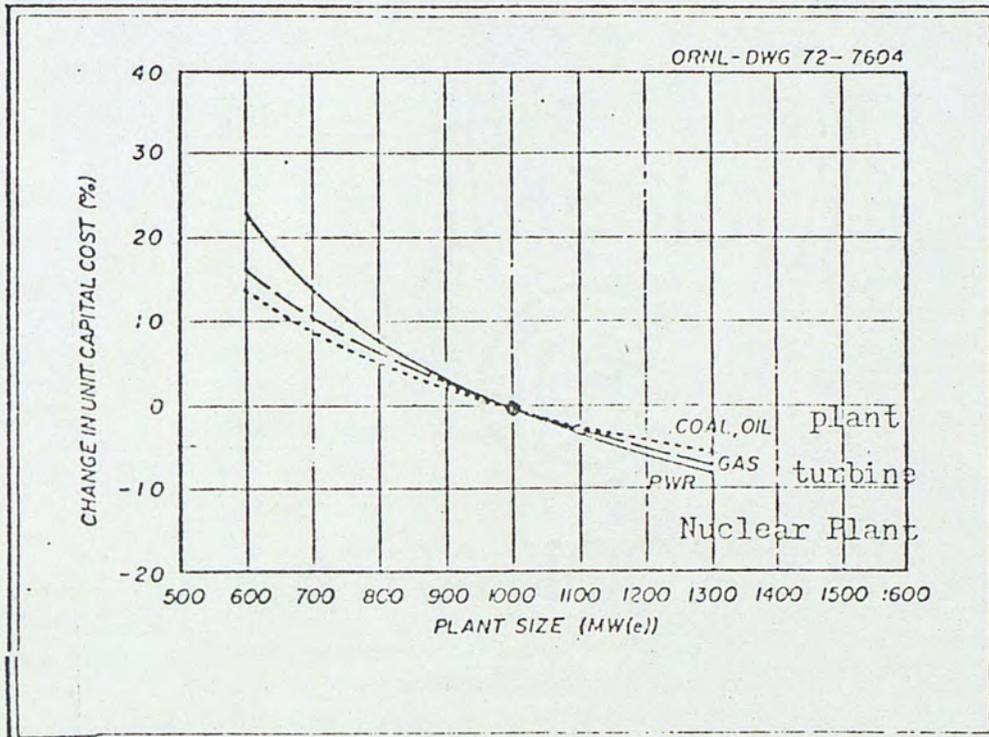


Figure 6. THE SENSITIVITY OF UNIT CAPITAL COST TO PLANT SIZE  
Source: Power Engineering, January 1973

As shown in this Figure a higher unit capital cost would be incurred for a smaller plant. For coal and oil power plants the unit capital cost for a 600 MW plant is 20% more than the unit capital cost for a 1300 MW power plant.

i) Coal Power Plant

For controlling the pollution, limestone scrubbers are used. Depending on the quality of coal use, the cost of pollution control varies as required to meet EPA standards. In some cases it consists of 25-30% of the total capital cost [ 5 ]. The plants in this study were assumed to be constructed in Southeast part of the country where "EASTERN"

coal with 4% sulfur content and 16% ash is used. Table 1 shows the range of construction costs involved for the 1000 MW coal power plant.

Table 1. COAL POWER PLANT CONSTRUCTION COST ESTIMATES

	<u>Low</u>	<u>Most Likely</u>	<u>High</u>
a. Process plant investment (\$/KW)	401	424	445
b. General facilities (\$/KW)	80	85	89
c. Project contingencies (\$/KW)	77	81	85
d. Pollution control facilities (\$/KW)	80	98	131
	—	—	—
TOTAL	638	688	750

Source: Balson, W. E. et al. 2-7.

The above estimates were made based on meeting the 1975 New Source Performance Standard (NSPS) for sulfur dioxide emission (1.2 lbs SO<sub>2</sub>/10<sup>6</sup> BTU).

#### ii) Oil Power Plant

The cost of construction of an oil power plant is generally lower than a coal power plant due mainly to the cost of pollution control equipments which are substantially lower for the oil power plant.

#### Plant Construction Time and Financing

Construction lead time and the rate of construction are important factors for planning and financing the project. In order to

avoid having extra interest costs only the amount needed for each year of construction is financed. A more detailed description of the financing policy was shown in Section 3.2.1.

The construction lead time and cumulative yearly construction for the coal power plant are listed in Table 2.

As it is shown in this table the construction cost for the beginning years of the construction period are less than of the later years.

Table 2. CONSTRUCTION PLANNING FOR COAL POWER PLANT

Construction Period: 5 years	
1st year cumulative constructed portion	10%
2nd year cumulative construction portion	25%
3rd year cumulative construction portion	45%
4th year cumulative construction portion	70%
5th year cumulative construction portion	100%

i) Oil Power Plant

The construction lead time for the oil power plant is generally shorter than of the coal power plant. In Table 3 the construction lead time and cumulative yearly construction for the oil power plant are shown.

Table 3. CONSTRUCTION PLANNING FOR OIL POWER PLANT

Construction period: 4 years	
1st year cumulative construction portion	15%
2nd year cumulative construction portion	35%
3rd year cumulative construction portion	65%
4th year cumulative construction portion	100%

#### Projection of Fuel Cost

Fuel cost is a very important factor in this study and affects the total cost of the project significantly. However, this portion of the cost is subject to general uncertainty and is a major factor when studying the oil power plant since the fuel cost constitutes a major portion of the total cost for the oil power plant. Because the period of operation for power plants in the study is 30 years and the average escalation rates for fuel costs used in this study are assumed to be less than the current escalation rates.

#### Operation and Maintenance Costs

The pollution control expenses were considered as O&M costs. For coal power plant, the flue gas desulfurization method is used to control the pollution where limestone is used in the process as explained in Chapter 3. The O&M costs consist of the fixed and variable portions. The cost of maintaining scrubbers and other pollution control equipments are included in the fixed portion of O&M cost and the cost of limestone is regarded as a variable O&M

cost. Similar to the escalation rate of the fuel cost, the average O&M escalation rate used in this study is assumed to be less than the current escalation rates.

#### Plant Efficiency (Heat Rate)

The heat rate is a function of scale and technological parameters reflected in the plant specifications and design. The plant heat rate affects the fuel cost and the variable portion of the O&M cost. The oil power plant has a higher efficiency than the coal power plant. This is reflected as a lower value for the heat rate corresponding to the oil power plant. The values of heat rate used in this study were based on the average annual values.

#### Data Input for Assessment of Probabilities

As described in Chapter 4, the variables associated with uncertainty in this study were: Construction cost, fuel and O&M costs, and their respective escalation rates.

Beta distribution was chosen as the most appropriate to attain flexibility and consistency in assigning probabilities.

The three estimates used in developing BETA distributions for the parameters are listed in Table 4.

#### Other Input Data

The data listed in Table 5 are estimated with certainty and their values do not change in the program.

Table 4. ESTIMATES-BETA DISTRIBUTION PARAMETERS

Probabilistic Variables	Coal Power Plant			Oil Power Plant		
	Opti- mistic Value	Most likely Value	Pessi- mistic Value	Opti- mistic Value	Most likely Value	Pessi- mistic Value
Construction Cost (\$/KW)	640	690	750	490	530	580
Fuel Cost (\$/10 <sup>6</sup> BTU) 1980	1.2	1.6	1.9	2.5	3.0	3.7
Fixed O&M Cost (\$/KW) 1980	9.8	10.3	10.9	1.5	1.85	2.25
Viriabile O&M Cost (\$/KW.HR) 1980	.0017	.0025	.0030	.0024	.003	.0035
Fuel Escalation Rate (%/Year)	4	5	7	6	8	12
O&M Escalation Rate (%/Year)	12	15	17	5	7.5	9.5

Source: The Technical Assessment Group of EPRI Planning Staff. Technical Assessment Guide, PS-866-SR, (Palo Alto, California: Electric Power Research Institute, 1978).  
Balson, W. E. et al.  
Y. S. Dept. of Energy. Short Term Energy Outlook., October, 1979.

TABLE 5. INPUT DATA ESTIMATED WITH CERTAINTY

Input	Data Used	
	Coal Power Plant	Oil Power Plant
1. Plant Size (MW)	1000	1000
2. Heat Rate (BTU/KW)	10000	9500
3. Plant Capacity Factor (% over 30 years)	70	70
4. Economic Plant Life (years)	30	30
5. Depreciation (years)	20	20
6. Construction Lead Time (years)	5	4
7. Discount Rate (%)	12	12
8. Effective Combined State and Federal Income Tax Rate	0.5	0.5
9. Debt Ratio	0.5	0.5
10. Equity Ratio	0.5	0.5
11. AD Valorem Tax Rate	0.005	0.005
12. Insurance Rate	0.001	0.001
13. Investment Tax Credit Rate	0.05	0.05
14. Debt Payment Rate (Bond Interest Rate)	0.10	0.10
15. Equity Return Rate	0.15	0.15
16. Plant Salvage Value (% of Initial Invest- ment)	-0.005	-0.005

## CHAPTER 6

### ECONOMIC ANALYSIS

In this Chapter the expected cost of generating electricity by using coal is compared to the expected cost when using oil. The distributions resulting from risk analysis are compared for the two alternatives. Then, the interrelationships and sensitivity of these alternatives to changes in the input parameters are analyzed.

#### Simulation Experimental Design

It is important to have a sufficiently large number of Monte Carlo trials to reduce sampling variation to a level which is tolerable in view of the accuracy needed and economically justified. In Table 6 the results of simulations with different numbers of observations are listed.

Table 6. Simulation results with various numbers of observations

No. of Observations	Alternative	Mean (\$)	STD.DEV (\$)	Prob. [EAC(Oil) > EAC(Coal)]
100	Coal	$312 \times 10^6$	$32 \times 10^6$	54%
	Oil	$317 \times 10^6$	$41 \times 10^6$	
200	Coal	$317 \times 10^6$	$32 \times 10^6$	60%
	Oil	$319 \times 10^6$	$40 \times 10^6$	
300	Coal	$306 \times 10^6$	$31.5 \times 10^6$	60.3%
	Oil	$320 \times 10^6$	$42.6 \times 10^6$	
500	Coal	$303 \times 10^6$	$31 \times 10^6$	59.5%
	Oil	$316 \times 10^6$	$41 \times 10^6$	

As it is expected the values of outcomes dampen or stabilize as the number of trials is increased. The number of trails at which the results become stable appears to be 300.

#### Simulation Results

The results of each simulation run include the probability distribution for the cost of each alternative and also the probability distribution of the cost difference between generating electricity by coal and by oil. Developing the distribution of the cost differences between these two alternatives allows us to quantify the probability that the first alternative (coal) will be less costly than the second alternative (oil). In Table 6 with 300 observations the expected cost of alternative I is  $\$306 \times 10^6$  which is less than  $\$320 \times 10^6$  of the expected cost of alternative II. Also the standard deviation of alternative I is less than that of alternative II indicating that the risk associated with alternative I is less than the risk involved with alternative II. The probability that alternative I will be less costly than alternative II is 60.3%. In Figure 7 graphs for the distributions of the costs for the two alternatives and their difference are shown.

#### Applying Current Escalation Rates

As explained in Chapter 5, the rates of escalation of the fuel cost for the alternatives have very significant effect on the results of the study. The escalation rates which are listed in Table 4 are assumed to be average value over a 30 year period, despite of the fact that these values are lower than the current

\*\*STATISTICS FOR VARIABLES BASED ON OBSERVATION\*\*

FILE NUMBER	ASSOCIATED MODE TYPE	MEAN VALUE	STANDARD DEVIATION	COEFF. OF VARIATION	MINIMUM VALUE	MAXIMUM VALUE	NUMBER OF OBSERVATIONS
1	AVN.EQ.COST1	0.3057E+09	0.3155E+08	0.1032E+00	0.2334E+09	0.3825E+09	300
2	AVN.EQ.COST2	0.3200E+09	0.4262E+08	0.1332E+00	0.2283E+09	0.4390E+09	300
3	DIFFERENCE	-0.1421E+08	0.5178E+08	-0.3645E+01	-0.1705E+09	0.1106E+09	300

\*\*FILE STATISTICS\*\*

FILE NUMBER	AVERAGE LENGTH	STANDARD DEVIATION	MAXIMUM LENGTH	CURRENT LENGTH
1	0.0	0.0	1	0
2	0.0	0.0	1	0
3	2.0000	0.0	4	2

\*\*HISTOGRAM NUMBER 1\*\*

AVN.EQ.COST1

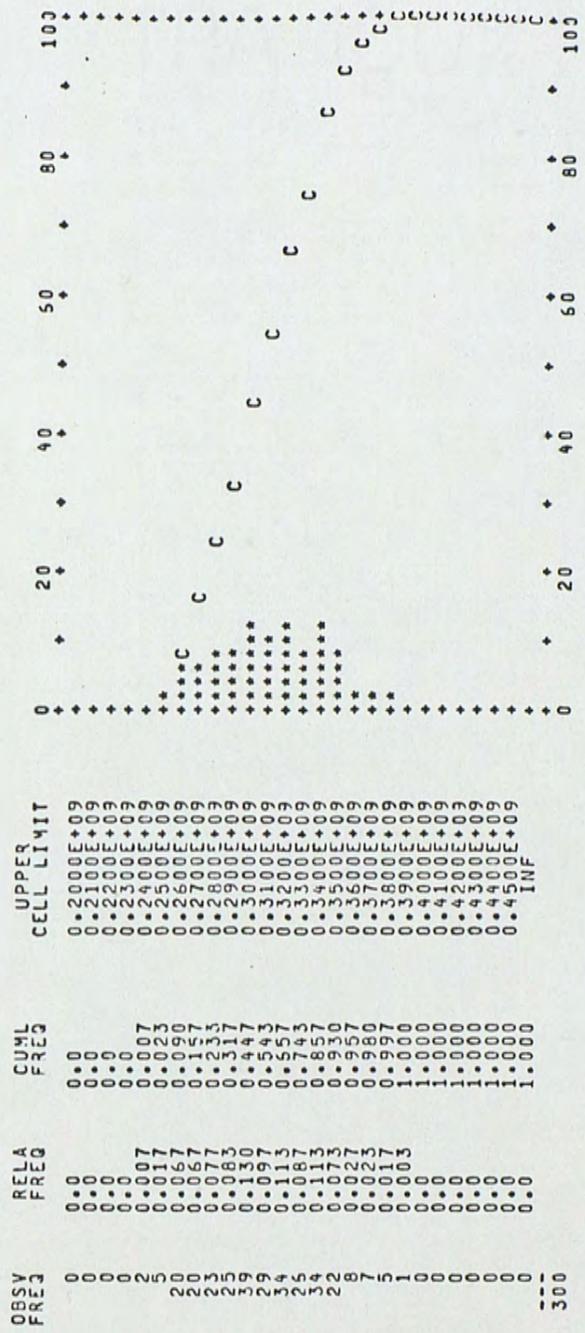


Figure 7. THE DISTRIBUTION OF ANNUAL EQUIVALENT COST OF THE TWO ALTERNATIVES AND THEIR DIFFERENCE

\*\*HISTOGRAM NUMBER 2\*\*

ANV.EQ.COST2

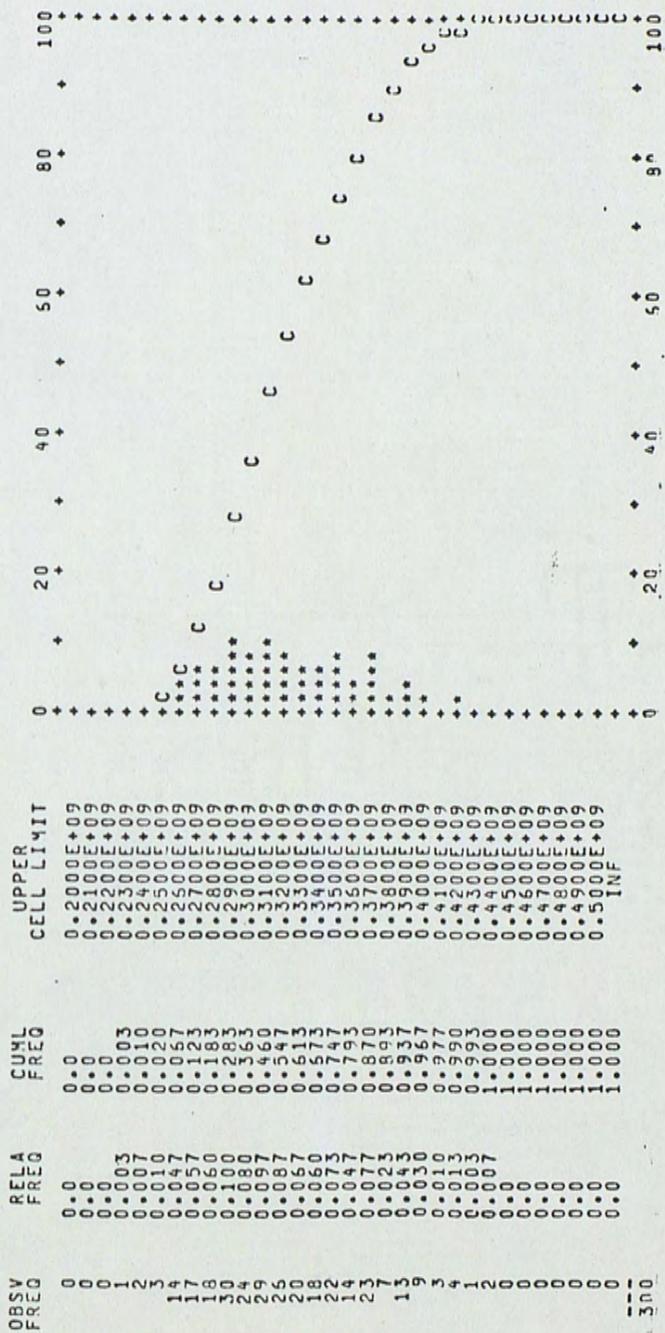


Figure 7. (Continued)

\*\*HISTOGRAM NUMBER 3\*\*

DIFFERENCE

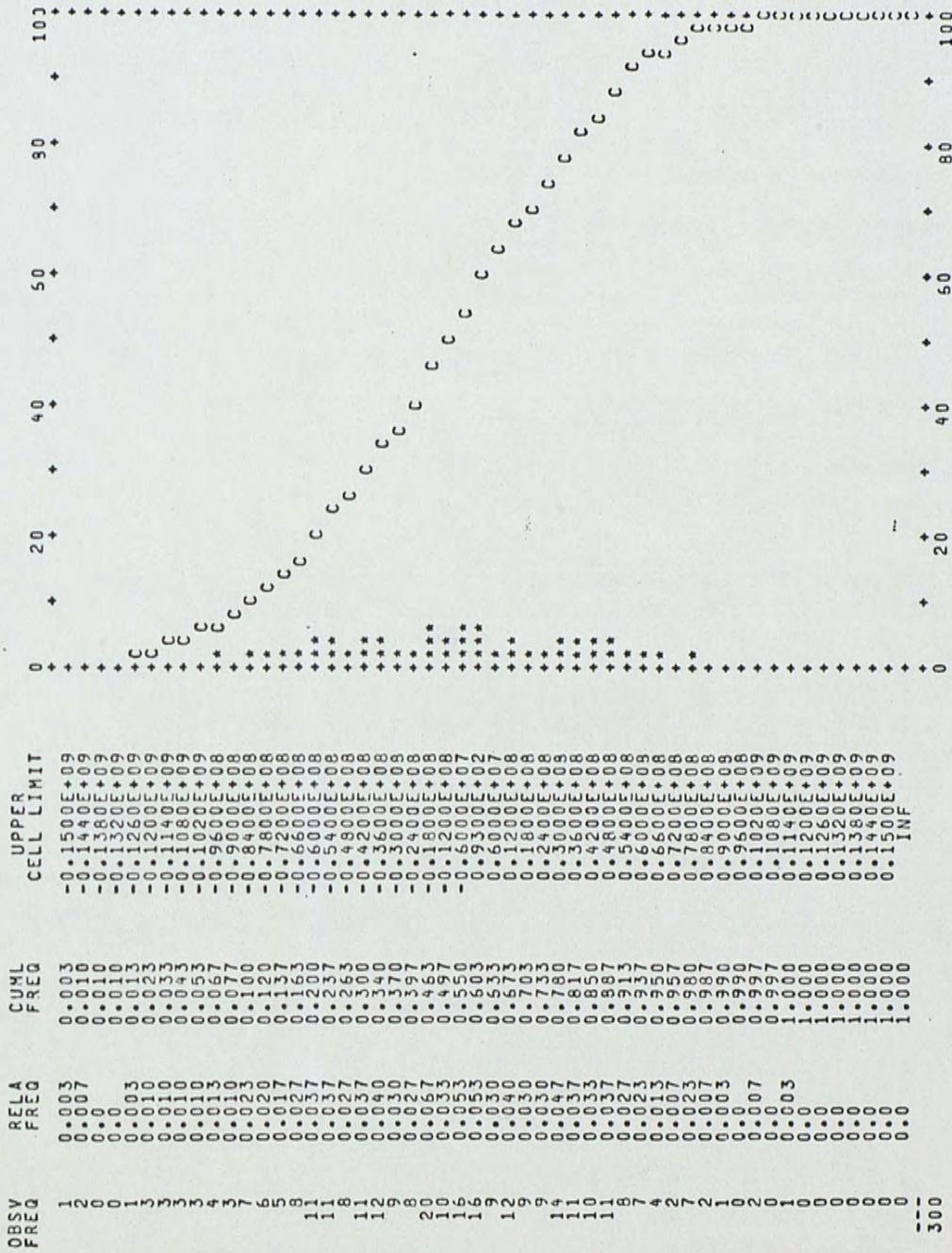


Figure 7. (Continued)

escalation rates. Some estimations of the current escalation rates are listed in Table 7. These values were used in a simulation and the results are summarized in Table 8.

Table 7. ESTIMATED CURRENT ESCALATION RATES FOR THE FUEL COST

Probabilistic Variables	Coal Power Plant			Oil	Power Plant	
	Optimistic value	Most likely Value	Pessimistic value	Optimistic value	Most likely value	Pessimistic value
Fuel Escalation Rate (%/year)	7	10	12	8	12	15

As shown in Table 8 a higher escalation rate for the fuel cost increases the cost of alternative II (Oil) very significantly and this increase is substantially higher than the cost increase of alternative I (Coal). The probability that alternative II will be more costly than alternative I increases to 87%. Another important observation is the change in value of the standard deviation of alternative II which is the result of assuming a wide range for the escalation rate of the fuel cost. The distribution for the cost is spread such that the risk involved with this alternative is in general much greater than of the previous case.

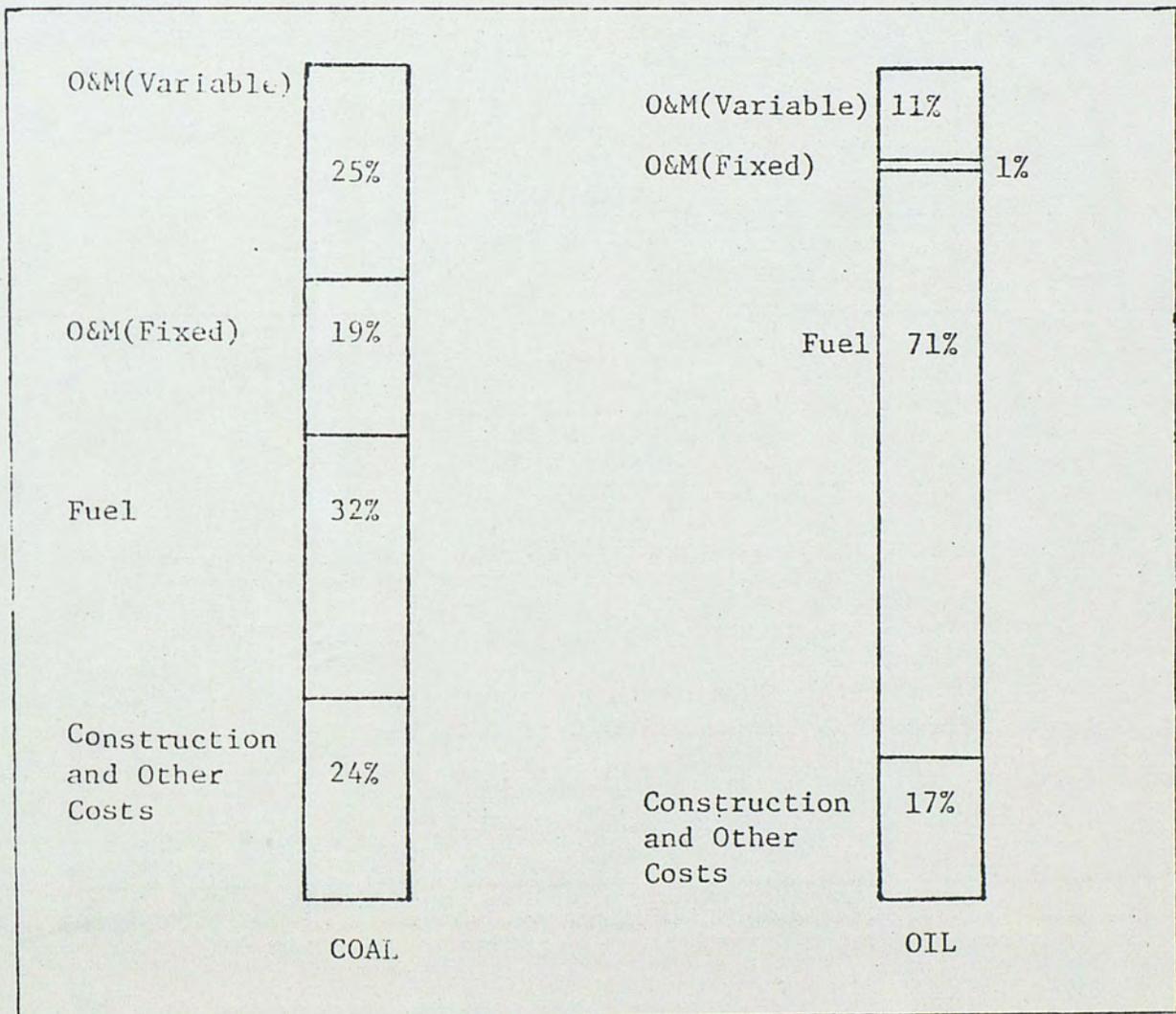
#### Evaluation of Cost Elements

It is of interest to examine the percent contribution of each cost element to the total annual equivalent cost for the results shown in Figure 7.

Table 8. SIMULATION RESULTS USING  
CURRENT ESCALATION RATES

Alternative	Mean	STD.DEV.	Prob. P[EAC(Oil) > EAC (Coal)]
I(Coal)	$413 \times 10^6$	$49 \times 10^6$	87%
II(Oil)	$560 \times 10^6$	$128 \times 10^6$	

Table 9. COST ELEMENTS FOR THE TWO  
ALTERNATIVES



According to the results shown in Table 9, seventy one percent of the total cost of the oil power plant is used for fuel whereas only 32% of the coal power plant is for fuel.

The cost of pollution control is included in the variable portion of the O&M cost which constitutes 25% of the total cost of the coal power plant. A major portion of these costs are for supplying and processing the limestone which is used for controlling the pollution. For the oil power plant 11% of the total cost is for the variable O&M costs. The fixed O&M costs constitute 19% of the total cost of the coal power plant and only 1% of the cost of the oil power plant. For the coal power plant the cost of maintaining the scrubbers and other pollution control devices is included in the fixed portion of the O&M costs. The remaining costs are mainly the construction cost as well as insurance costs, debt interest, and taxes. These costs constitute 24% of the total cost of the coal power plant and 17% of the total cost of the oil power plant.

#### The Effect of System Load Factor

Since operating and fuel costs are linear functions of system load factor, the system capacity factor is an important operating characteristic for a power plant. The results of simulations for some selected values of load factor are summarized in Figure 8. As it is shown in this Figure for values of the load factor of 55% or less the oil power plant would become the less costly alternative.

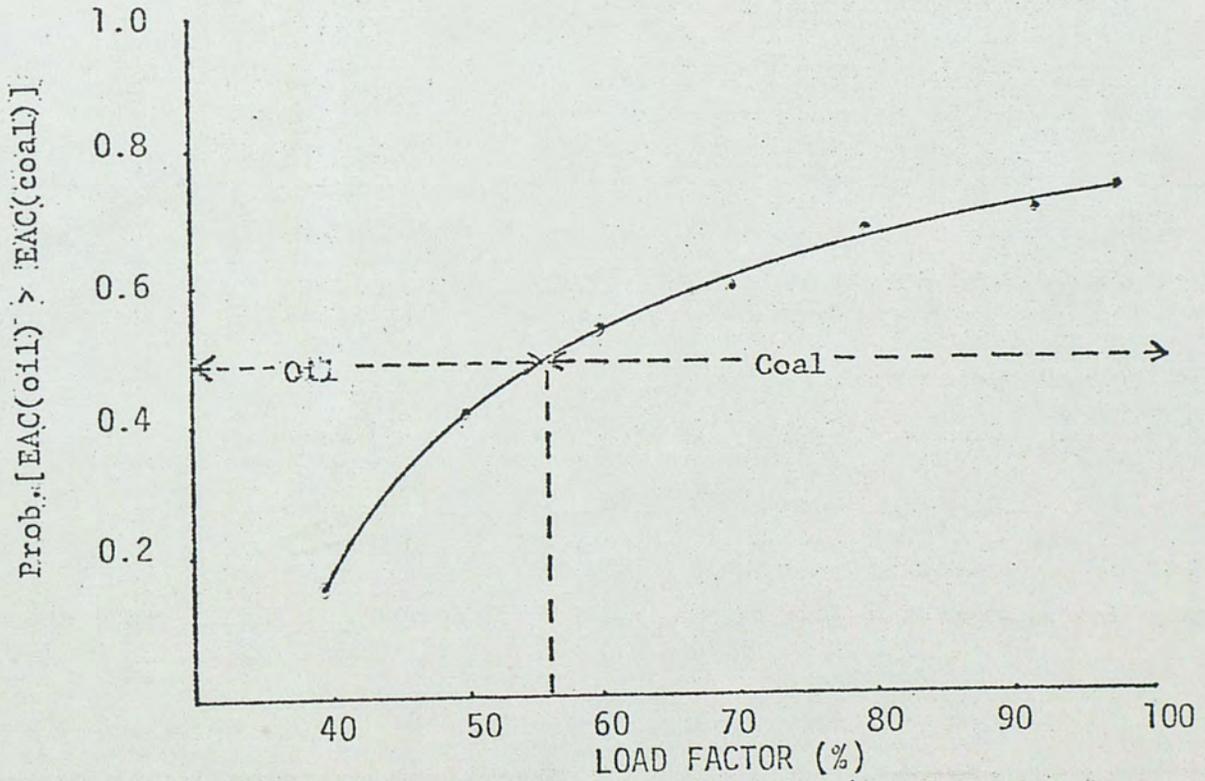
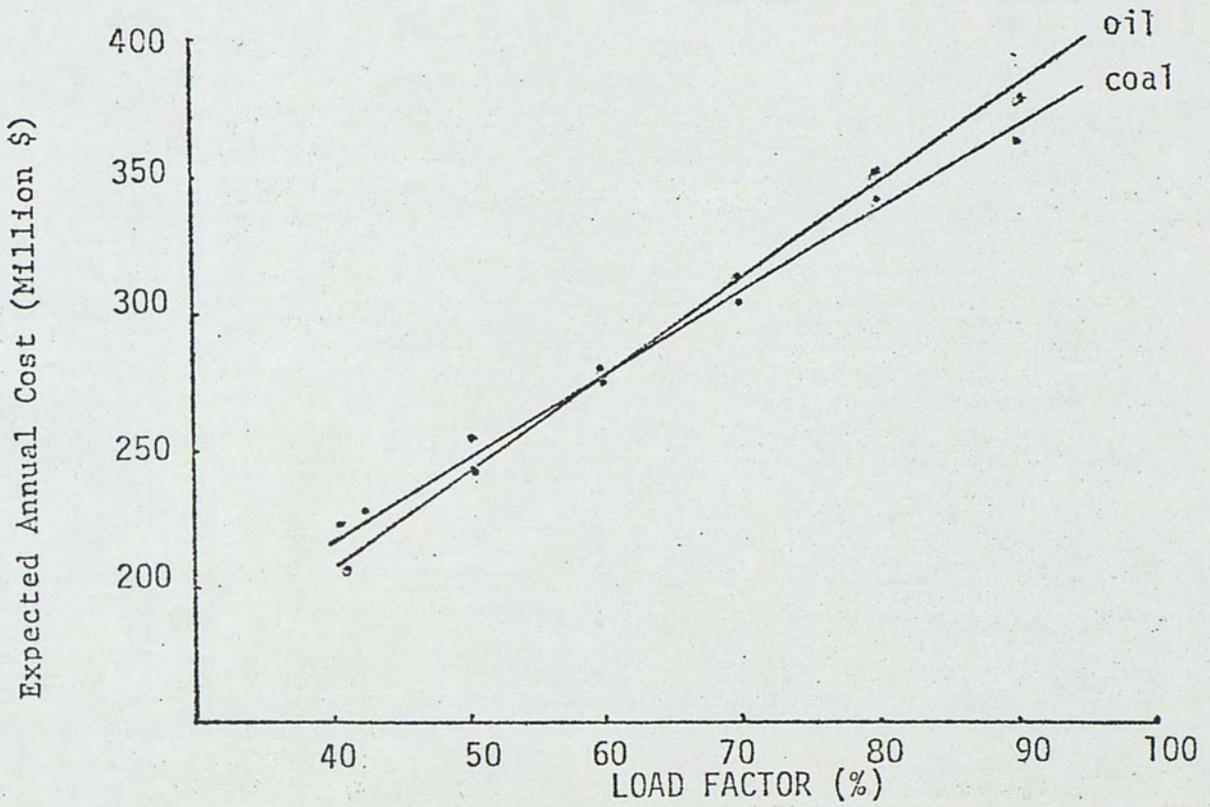


Figure 8. THE EFFECT OF LOAD FACTOR ON THE TOTAL COST AND ECONOMIC ATTRACTIVENESS

### The effect of Discount Rate

As described in Chapter 3 the present worth of the net after-tax cash flow for each year is calculated and the equivalent annual cost for each alternative is found as a function of the discount rate. Thus, the selection of an appropriate discount rate in evaluation of capital investment is important.

Figure 9 shows the sensitivity of the equivalent annual cost of the two alternatives to the discount rate. As shown in this Figure, higher discount rates result in lower equivalent annual costs for both alternatives under study. For discount rates higher than 7%, alternative I (Coal) would be less costly than alternative II (Oil).

### The Effective of Construction Cost

To examine the sensitivity of the total cost of alternatives to the construction cost, the original values for construction costs were inflated by increments of 5%. The results of the respective simulations are shown in Figure 10. Based on these results the total equivalent annual cost of coal power plant is more sensitive to construction cost than of the oil power plant and an increase of 28% or more in the construction costs would make the coal power plant a more costly alternative.

### The Effect of Fuel Cost

As discussed in Chapter 4 the cost of fuel is a critical factor in economical analysis of power plants. The importance of this

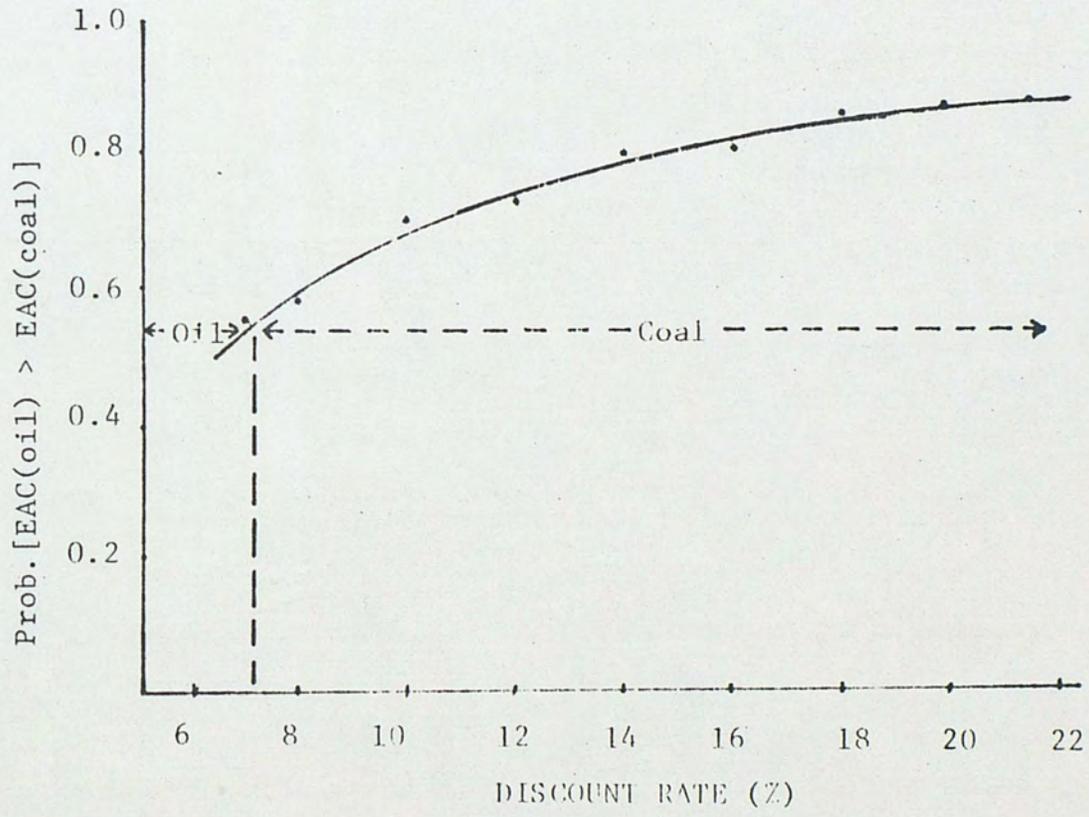
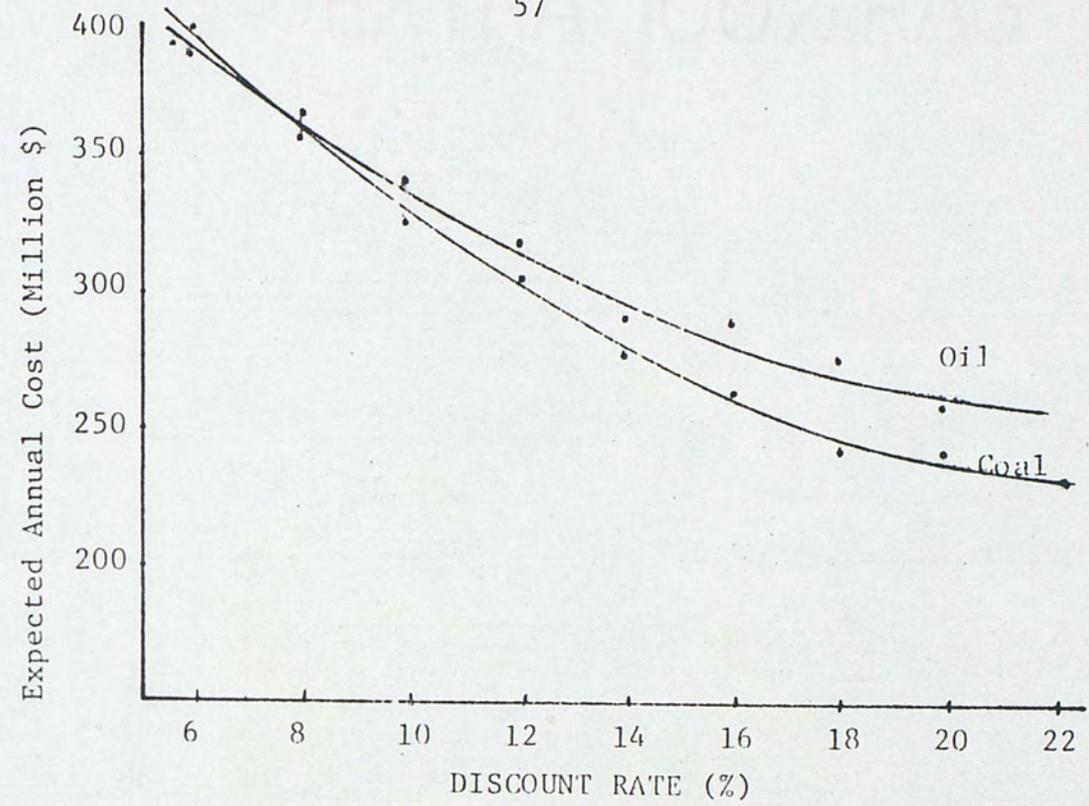


Figure 9. THE EFFECT OF DISCOUNT RATE ON THE TOTAL COST AND ECONOMIC ATTRACTIVENESS

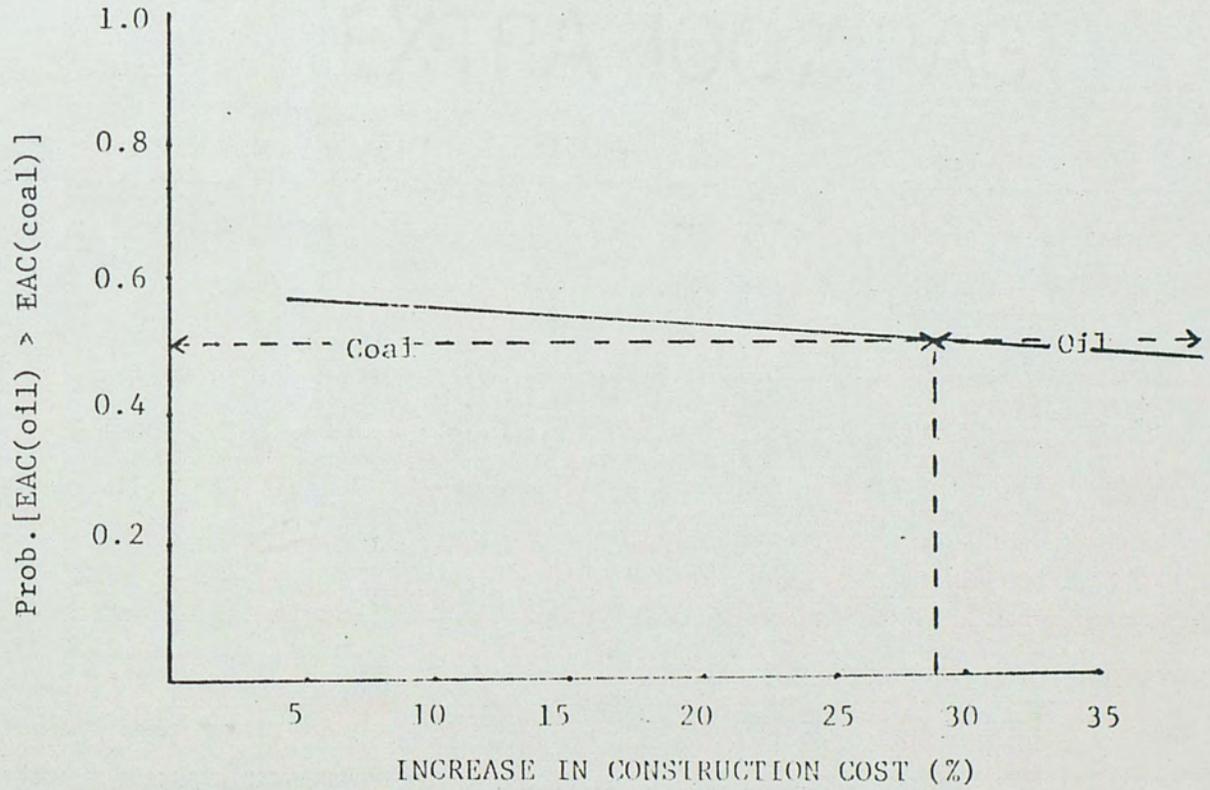
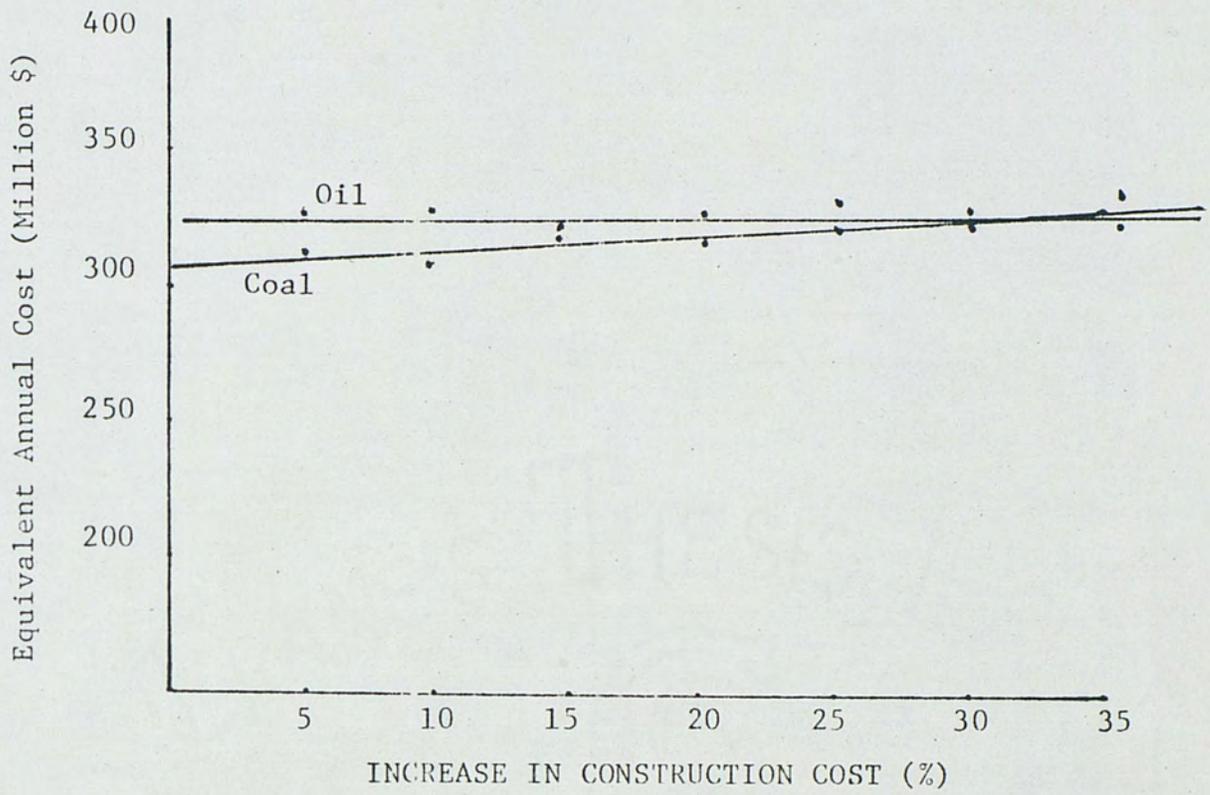


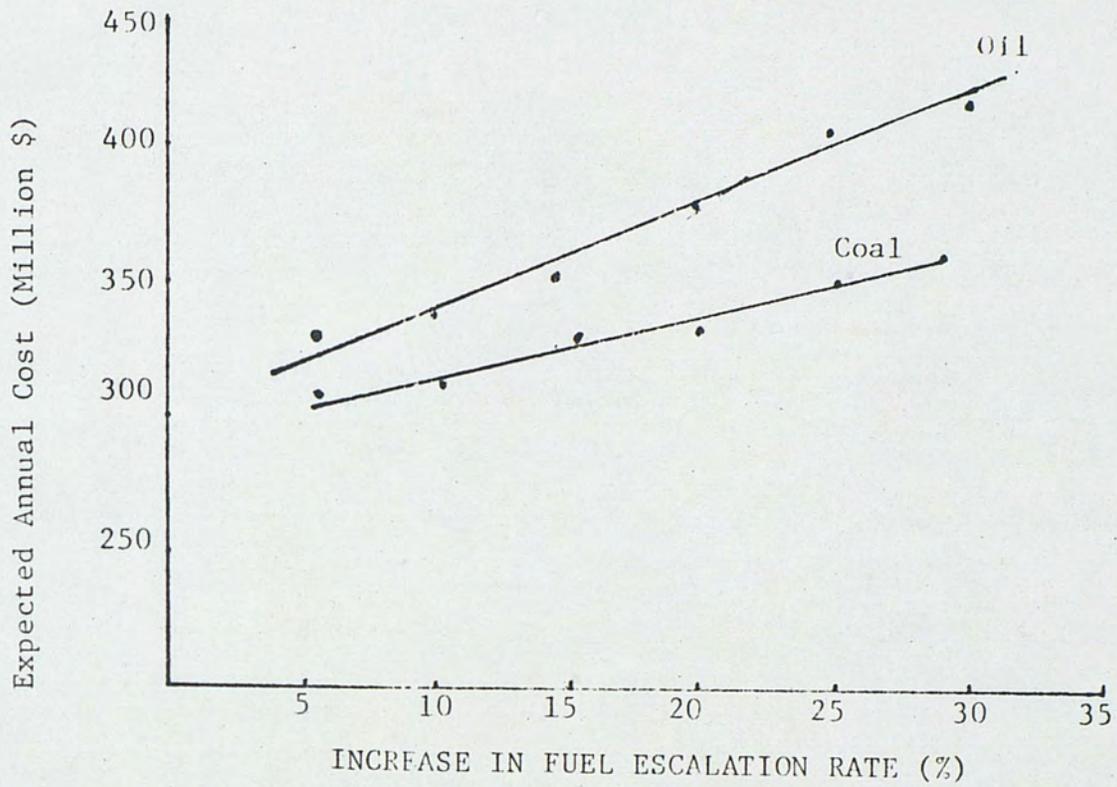
Figure 10. THE EFFECT OF CONSTRUCTION COST ON THE TOTAL COST AND ECONOMIC ATTRACTIVENESS

factor is greater for the oil power plant since the fuel cost constitutes a major portion of the total cost of this alternative.

In this study the values for the average escalation rate of fuel cost are 5.16% for coal and 7.4% for oil. These values were inflated by increments of 5% to examine the sensitivity of the total cost of the alternatives to the fuel cost. In Figure 11 the values of the total cost are plotted vs. the inflated values of fuel escalation rate. In this Figure the high sensitivity of the total cost of the oil power plant to the fuel cost is shown.

#### The Effect of O&M Cost

To examine the sensitivity of the total cost of both alternatives to the O&M cost, simulation runs were made by assuming a set of values for the O&M escalation rates. The simulation results are presented in Figure 12. According to the results shown in this Figure, the total cost of the coal power plant is substantially more sensitive to the O&M cost than the oil power plant. For O&M escalation rates 3% higher than the rates assumed in this study the coal power plant would be the more costly alternative.



Esc. Rate(Coal)	5.16	5.4	5.7	5.9	6.2	6.4	6.7	7
Esc. Rate(Oil)	7.4	7.8	8.1	8.5	8.9	9.2	9.6	10

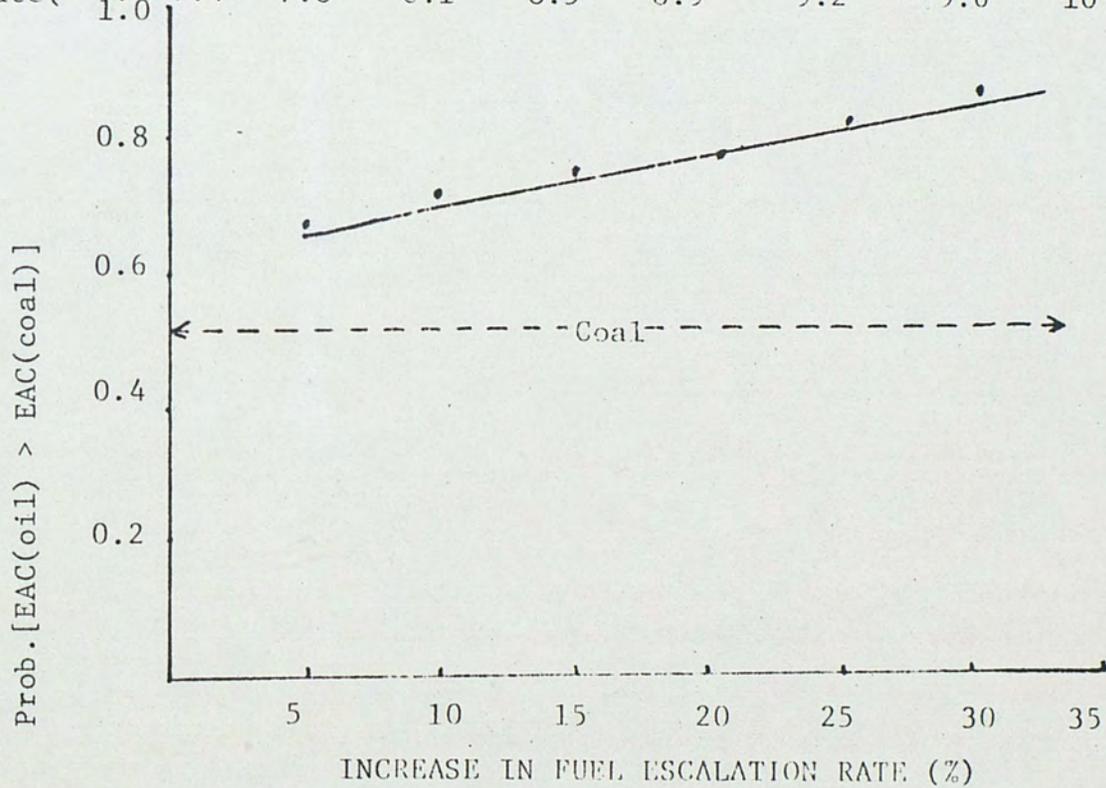
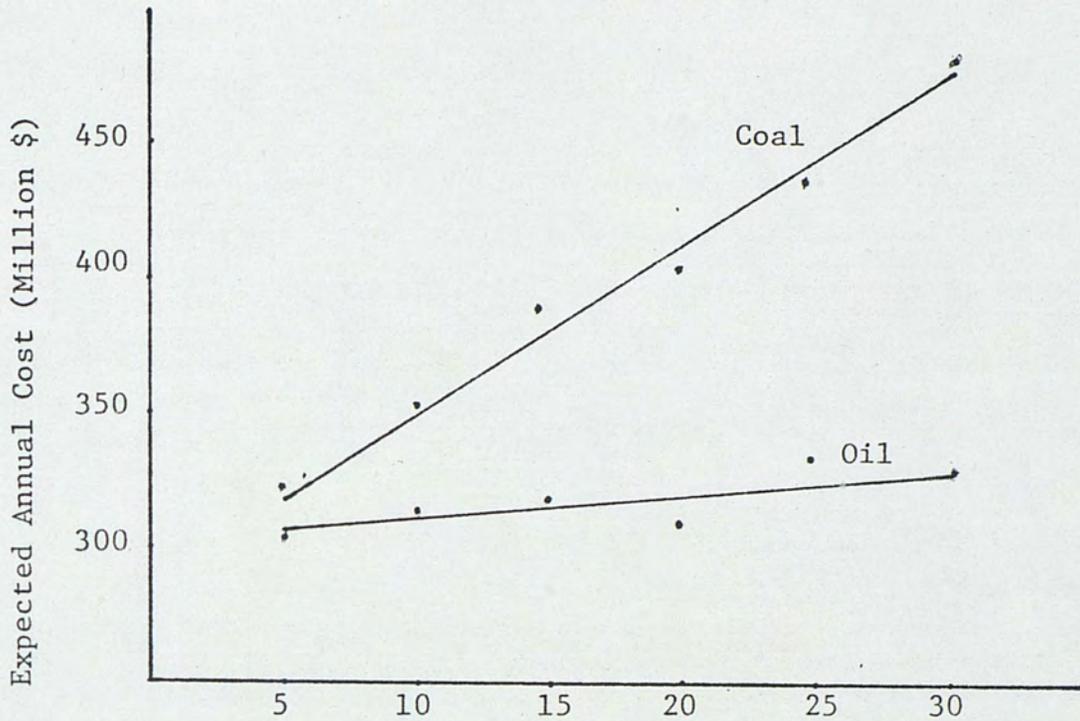


Figure 11. THE EFFECT OF FUEL COST ON THE TOTAL COST AND ECONOMICAL ATTRACTIVENESS



		INCREASE IN ESCALATION RATE OF O&M COST (%)						
Esc. Rate (Coal)		14.8	15.5	16.3	17	17.8	18.5	19.2
Esc. Rate (Oil)		8.3	8.7	9.1	9.5	10	10.4	10.8
	1.0							

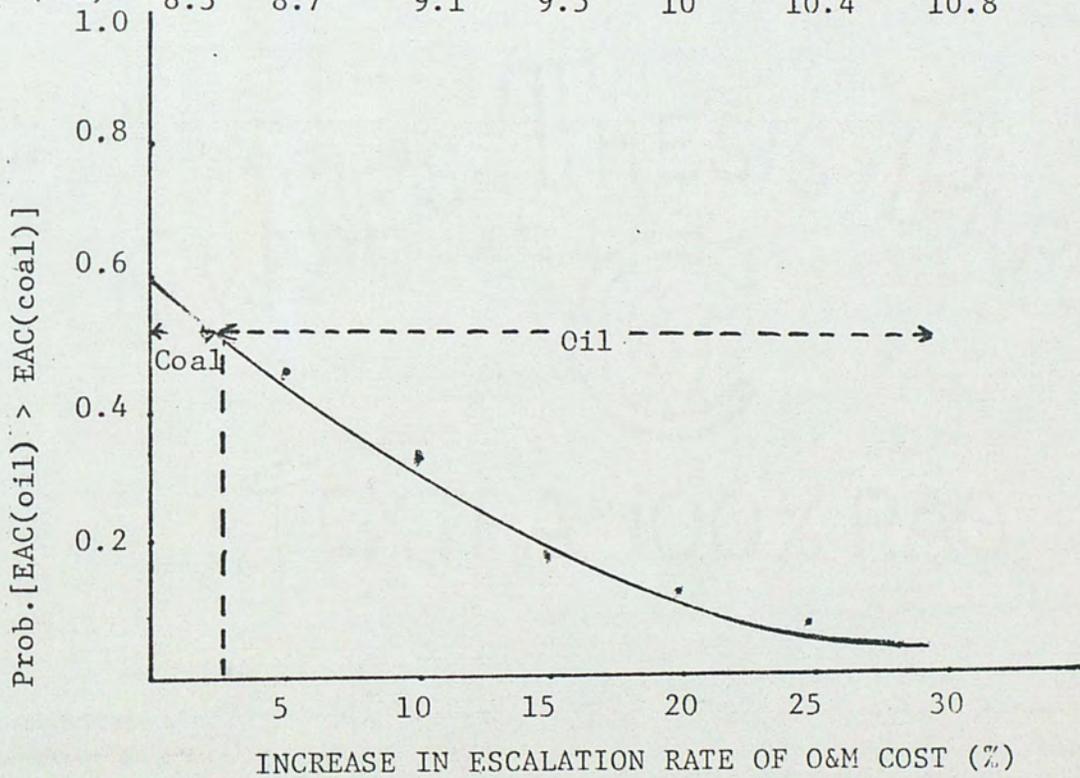


Figure 12. THE EFFECT OF O&M COST ON THE TOTAL COST AND ECONOMIC ATTRACTIVENESS

## CHAPTER 7

### SUMMARY, CONCLUSIONS AND RECOMMENDATIONS

#### Summary and Conclusions

This report describes the application of risk analysis approach to the problem of assessing the cost of two competing technologies for electric power production. Oil and coal power plants were compared assuming equal plant size, operating life and a similar financing policy. It has been shown that the comparison of two technologies is complicated by various factors. The difficulty stems from the fact that these technologies differ along many dimensions; capital cost, fuel cost, operating and maintenance cost, and environmental effects. Furthermore, the combustion of coal produces airborne emissions of particulates, nitrogen and sulfur oxides. These emissions should be reduced to some acceptable levels specified by Environmental Protection Agency (EPA).

A comprehensive mathematical model for evaluation of power plants was developed. The cost elements were identified and the total equivalent annual cost was derived in order to accomplish risk analysis, all the factors subject to uncertainty were identified and corresponding probability distributions for all

these factors were defined. A computer program was developed to find the equivalent annual costs by incorporating the probabilistic information through Monte Carlo sampling techniques. SLAM was the computer language used in this study and the inherent flexibility of this language reduced the complexity involved in programming the economical model of this study.

By referring to various sources of information, the necessary data was collected for this study. For factors subject to uncertainty three estimates i.e., "optimistic", "most likely", and "pessimistic" were made. These estimates were used to develop the probability distributions for the respective parameters.

The expected cost of generating electricity by using coal was compared to the expected cost when oil is used. The distributions resulting from risk analysis were compared for the two alternatives and the interrelationships and sensitivity of these alternatives to changes in the input parameters were analyzed.

According to the results achieved with 300 observations in a simulation run the expected equivalent annual cost of the oil power plant was higher than of the coal power plant. The same observation was made with the standard deviations of costs of the two alternatives. This indicates that the risk involved with the oil power plant is higher than the associated risk with the coal power plant. The probability that the coal power plant would be less costly than the oil power plant was 60%.

By applying fuel escalation rates closer to the current rates a significant increase was observed in the values of the expected equivalent annual costs and the respective standard deviations. In this case the probability that the coal power plant would be less costly than the oil power plant increased to 87%.

Seventy one per cent of the total cost of the oil power plant was found to be due to the fuel costs, whereas, for the coal power plant only 32% of the total cost was observed to be for the fuel cost. However, the construction and O&M costs of the coal power plant were found to constitute a higher percentage of the total cost of this alternative than the respective cost elements for the oil power plant.

By assuming higher values for the load factor the economic attractiveness of the coal power plant was further enhanced. For all values of load factor less than 55% the oil power plant appeared to be the less costly alternative.

For an increase in the value of discount rate the expected value of equivalent annual cost was decreased. Discount rates lower than 7% would make the oil power plant the less costly alternative.

The coal power plant was found to be more sensitive to an increase in the construction cost. For any increase in construction costs greater than 28% over the initially estimated value the coal power plant would become the more costly alternative.

For the coal power plant the O&M cost was found to have significant effect on the total equivalent annual cost. For O&M escalation rates 3% higher than the rates assumed in this study the coal power plant would be the more costly option to undertake.

#### Recommendation for Future Research

The selection of SLAM as the simulation language simplified the programming effort to a minimum. A significant advantage of the program developed for this study is its flexibility and capability of handling various conditions when studying power generation economics. Development of an interactive version of SLAM could put the package at the reach of a wider range of users. The role of the user would be reduced to selecting options offered by the program and entering the data pertaining to his specific case, without mastering SLAM simulation language.

Another feature of the possible extension of the study is to develop a comprehensive program to evaluate a variety of power plants such as nuclear, solar, and synthetic fuel.

APPENDIX I

SLAM SIMULATION PROGRAM LISTINGS

JES2 JOB LOG -- SYSTEM IPO1 -- NODE CFR

22.57.57 JOB 2940 \$HASP373 SLAM STARTED - INIT 3 - CLASS 5 - SYS IPO1  
23.09.12 JOB 2940 \$HASP395 SLAM ENDED

----- JES2 JOB STATISTICS -----

10 JUL 80 JOB EXECUTION DATE

830 CARDS READ

1,228 SYSOUT PRINT RECORDS

0 SYSOUT PUNCH RECORDS

0 SYSOUT PLOT RECORDS

11.24 MINUTES EXECUTION TIME

1	//SLAM JOB (XF1924,01,300),MEDI	JOB 2940
2	***PASSWRD \$CGF1770 \$PASSWRD(S) SUCCESSFULLY SCANNED	
3	// EXEC IRFAX,PROG=SLAM500	
4	*** DATE LAST MODIFIED - 09/26/79 BY J. W. RADFORD	
5	XXIRF4X EXEC PGM=IRLINK,DISP=SHR	000500000
6	XXSTEPL13 DD DSN=FTU,SS,IRLINK,DISP=SHR	001000000
7	XXFT05F001 DD SYSOUT=	001500000
8	//FT07F001 DD SYSOUT=	002000000
9	//SYSLINK DD EXEC PGM=IRLOG,PARM=*,PROG*,COND=EVEN	003000000
10	XXSTEP2 DD DSN=FTU,SS,IRLINK,DISP=SHR	003500000
11	XXSYSPRINT DD DSN=FTU,SS,IRLINK,DISP=SHR	004000000
12	XXLOGFILE DD DSN=FTU,OU=,P1003,LOGFILE,DISP=SHR	004500000
13	*** PROJ 1003 FTU SYSTEMS PROGRAMMING	005000000
	//	005500000
		006000000

STMT NO.	MESSAGE	4MIN 02.64SEC SRB	0MIN 13.27SEC VIRT	380K SYS	216K.
4	IEF653I SUBSTITUTION JCL - PGM=SLAM500				
5	IEF653I SUBSTITUTION JCL - PGM=SLAM500,COND=EVEN				
6	ALLO FOR SLAM IRF4X				
7	151 ALLOCATED TO STEPL13				
8	151 ALLOCATED TO SYS00030				
9	151 ALLOCATED TO FT05F001				
10	151 ALLOCATED TO FT06F001				
11	SLAM IRF4X - STEP WAS EXECUTED - COND CODE 0000				
12	FTU,SS,IRLINK,STEP WAS EXECUTED - COND CODE 0000				
13	SYSLINK DD EXEC PGM=IRLINK,STEP WAS EXECUTED - COND CODE 0000				
14	VOLSER VOLUME=FTUPK2.				
15	VOLSER VOLUME=FTUPK2.				
16	VOLSER VOLUME=FTUPK2.				
17	JES2 JOB02940.010101				
18	JES2 JOB02940.00102				
19	SYSLINK DD EXEC PGM=IRLINK,STEP WAS EXECUTED - COND CODE 0000				
20	VOL SER VOLUME=SYSWK1.				
21	STEP /IRF4X / STOP 80192.2257				
22	STEP /IRF4X / STOP 80192.2309				
23	ALLO FOR SLAM_STEP2				

JOB PERFORMANCE ANALYSIS AND CHARGES FOR USE OF C.F.R.D.C. SYSID-IP VS/2 RELEASE-03.8 MODEL-165

JOBNAME - SLAM ACCOUNT NO. - XF1954 DATE - 10 JUL 80 JOB CLASS - 5 36.3 CAPACITY  
22:57:58 STARTED 23:09:12 ENDED 00:11:14 ELAPSED 00:11:09 NET TIME CAS-ACTRT REL 3.6M

BASIC CHARGES- CPU TIME 242.95 SECONDS AT .07500 \$/SEC = 18.22  
VOLUNTARY WAIT - 425.70 SECONDS AT .00000 \$/SEC =  
VIRT CORE - 92.213 KCPU SEC AT .00037 \$/KCS = 34.12  
PAGE-INS 193 AT .00000 \$EACH = .00  
PAGE-OUTS 128 AT .00000 \$EACH = .00  
BASIC SUB- TOTAL = 52.34\*

DEVICE CHARGES-DEVICE CLASS NUM ---MOUNTING---CHARGE ---EXCP---CHARGE ---OCCUP---CHARGE  
DASD 00 .00 .00 3.35 .00 = 3.35  
TAPE 00 .00 .00 .00 .00 = .00  
U/R .00 .00 .00 .00 .00 = .00  
OTHER .00 .00 .00 .00 .00 = .00  
DEVICE SUB- TOTAL = 3.35\*

PRIORITY AND SHIFT TOTAL = .00 JOB TOTAL = 55.69 JOB CHARGE = \$55.69\*

\*\*\*\*\*  
SLAM  
VERSION 1.0  
RELEASE 1.0  
\*\*\*\*\*

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EXPRESS WRITTEN PERMISSION OF PRITSKER AND ASSOCIATES, INC.

PRITSKER AND ASSOCIATES, INC.

P.O. BOX 2413  
WEST LAFAYETTE, INDIANA 47906

GEN,MEDI,EXERCISE,01/22/90,1;  
LIMITS,2,90,200;

\*\*\*\*\*  
INITIALIZATION FOR ALTERNATIVE I  
\*\*\*\*\*

\*\*\*\*\*VARIABLES SUBJECT TO UNCERTAINTY \*\*\*\*\*  
INTLC,XX(74)=640,XX(73)=690,XX(83)=750,; CONSTRUCTION COST (\$/KW)  
INTLC,XX(18)=1.2,XX(19)=1.6,XX(20)=1.9,; FUEL COST  
INTLC,XX(80)=9.8,XX(86)=10.3,XX(88)=10.9,; O&M COST(FIXED)  
INTLC,XX(28)=0.0017,XX(29)=0.0025,XX(30)=0.003,; O&M COST(VARBL.)  
INTLC,XX(37)=0.12,XX(39)=0.15,XX(24)=0.17,; O&M ESC.RATE  
INTLC,XX(93)=0.04,XX(94)=0.05,XX(95)=0.07,; FUEL ESCALATION RATE  
\*\*\*\*\*  
\*\*\*\*\*VARIABLES ESTIMATED WITH CERTAINTY \*\*\*\*\*

INTLC,XX(26)=30 ; OP.LIFE  
INTLC,XX(66)=20 ; DEP.LIFE  
INTLC,XX(27)=0.05 ; INV.TAX CREDIT RATE  
INTLC,XX(2)=0.5 ; TAX RATE  
INTLC,XX(16)=5 ; ; CONSTRUCTION PERIOD  
INTLC,XX(5)=0.005 ; PROP.TAX  
INTLC,XX(6)=0.001 ; INS.RATE  
INTLC,XX(32)=1,XX(33)=0,XX(34)=0; STRAIGHT LINE DEPRECIATION  
INTLC,XX(77)=-0.005 ; SALVAGE VALUE(% OF INIT.INVST.)  
INTLC,XX(78)=10000 ; HEAT RATE  
INTLC,XX(82)=0.7 ; CAPACITY FACTOR  
INTLC,XX(90)=1000000,XX(300)=0,; PLANT SIZE(KW)  
INTLC,XX(51)=0; DEBT:BOND TYPE  
INTLC,XX(48)=1; EQUITY:EQUAL ANNUAL PAYMENT TYPE  
INTLC,XX(1)=1.12 ; 1+ INTEREST RATE  
INTLC,XX(3)=0.15;EQUITY INTEREST RATE  
INTLC,XX(4)=0.10;DEBT INTEREST RATE  
INTLC,XX(11)=0.5 ; DEBT PORTION OF THE INVESTMENT  
INTLC,XX(12)=0.1 ; ; PORTION TO BE CONSTRUCTED BY THE END OF YEAR 1  
INTLC,XX(13)=0.25 ; ; PORTION TO BE CONSTRUCTED BY THE END OF YEAR 2  
INTLC,XX(14)=0.45 ; ; PORTION TO BE CONSTRUCTED BY THE END OF YEAR 3  
INTLC,XX(15)=0.7 ; ; PORTION TO BE CONSTRUCTED BY THE END OF YEAR 4  
INTLC,XX(58)=1 ; ; PORTION TO BE CONSTRUCTED BY THE END OF YEAR 5  
INTLC, ; XX(59)=0,XX(60)=0,XX(61)=0,XX(62)=0; REMAINING YEARLY PORTIONS OF  
THE PROJECT CONSTRUCTION  
INTLC,XX(35)=0.1 ; DECLINING BALANCE DEPRECIATION FACTOR  
INTLC,XX(7)=0 ,XX(8)=0 ,XX(36)=1 ; INITIALIZATIONS

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INITIALIZATION FOR ALTERNATIVE II

CONSTRUCTION COST(\$/KW)  
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O&M COST(FIXED)  
O&M COST (VARIABLE)  
ESC. RATE (O&M)

CONSTANTS USED FOR ADJUSTING ESCALATION RATES

NETWORK  
CREATE,1  
ASSIGN,TRIB(90)=TNOW;

THIS PART GENERATES DATA BY BETA DISTRIBUTION

CONSTRUCTION COST  
FUEL COST  
O&M COST

CONSTANTS USED FOR ADJUSTING ESCALATION RATES

NETWORK  
CREATE,1  
ASSIGN,TRIB(90)=TNOW;







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344 ***** THIS PART OF THE PROGRAM CALCULATES THE TOTAL COST
345 ***** DURING THE OPERATION PERIOD *****
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***** THIS PART OF THE PROGRAM CALCULATES THE TOTAL COST
***** DURING THE OPERATION PERIOD *****
*****
***** AT(27) IS THE INVESTMENT TAX CREDIT BIAS DEDUCTED FROM TOTAL COST
*****
***** FIND THE DEPRECIATION *****
ASSIGN, ATRIB(27)=XX(27)*XX(21),
ATRIB(16)=ATRIB(16)-ATRIB(27),
ATRIB(26)=ATRIB(6),
ATRIB(34)=XX(21),

*****
***** AT(27) IS THE INVESTMENT TAX CREDIT BIAS DEDUCTED FROM TOTAL COST
*****
***** FIND THE DEPRECIATION *****
ASSIGN, ATRIB(30)=XX(21)-XX(25),
ATRIB(76)=ATRIB(30),
XX(76)=XX(65),
ATRIB(31)=ATRIB(30)/XX(66),
ATRIB(51)=XX(35),
ATRIB(52)=XX(36)-ATRIB(51),
ASSIGN, ATRIB(55)=XX(35),
ATRIB(54)=XX(66)+XX(36),
ATRIB(55)=ATRIB(54)*XX(66),
ATRIB(55)=ATRIB(55)/2,

*****
***** AT(30) IS (P-L) FOR SLO@AT(55) IS (N+1)/2 FOR SYD DEPRECIATION
*****
***** CHECK FOR TYPE OF EQUITY *****
ACT, XX(48).EQ.0, BETA;
ACT, XX(48).EQ.1, ALFA;

*****
***** WHEN EQUITY IS BOND TYPE FIND YRLY INTRST *****
ASSIGN, ATRIB(64)=ATRIB(6)*XX(3),
ATRIB(63)=ATRIB(6);
ACT, **NEXT;

*****
***** AT(64) IS THE YEARLY INTEREST FOR THE EQUITY *****
***** WHEN EQUITY IS EQUAL ANNUAL PYMNT TYPE *****
***** FIND THE ANNUAL PAYMENT *****
ASSIGN, XX(40)=XX(3)+1,
XX(41)=XX(3),
ASSIGN, ATRIB(61)=ATRIB(61)+1,
XX(41)=XX(41)*XX(40),
ACT, ATRIB(61).LT.XX(26), EQIT;
ACT, ATRIB(61).GE.XX(26), EQCT;
ASSIGN, XX(42)=XX(41)-1,
XX(43)=XX(41)*XX(3),
XX(44)=XX(43)/XX(42),
ATRIB(35)=ATRIB(6)*XX(44),
ASSIGN, XX(45)=ATRIB(6)*XX(3),
XX(45)=XX(45)-ATRIB(35),
ATRIB(62)=XX(40)/XX(40);

*****
***** AT(36) IS ANNUAL PAYMENT (A=INTRST+PRINCP.)@XX(46) IS (P-I-A) *****
***** CHECK FOR TYPE OF DEBT *****
GOOV, 2;
ACT, XX(51).EQ.0, DBT3;
ACT, XX(51).EQ.1, DBTA;

*****
***** WHEN DEBT IS BOND TYPE FIND YRLY INTRST *****
ASSIGN, ATRIB(66)=ATRIB(5)*XX(4),
ATRIB(67)=ATRIB(5);
ACT, **OPER;

*****
***** AT(66) IS THE YEARLY INTEREST FOR THE DEBT *****
***** WHEN DEBT IS EQUAL ANNUAL PAYMENT TYPE *****
***** FIND THE ANNUAL PAYMENT *****
ASSIGN, XX(49)=XX(4)+1,

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417 ATRIB(7)=0;
418 XX(50)=XX(4)+1;
419 ASSIGN, ATRIB(65)=AT(56)/XX(50);
420 ACT, ATRIB(65).LT, XX(26), REDO;
421 ACT, ATRIB(65).GE, XX(26), CALC;
422 ASSIGN, XX(52)=XX(50)-1;
423 XX(53)=XX(50)+XX(4);
424 XX(54)=XX(53)/XX(52);
425 ATRIB(68)=AT(56)/XX(54);
426 XX(55)=AT(56)/XX(54);
427 XX(56)=XX(55)+XX(4);
428 ATRIB(69)=XX(49)/XX(49);
429
430
431 AT(68) IS ANNUAL PAYMNT FOR DEBT INCLUCES INTRST AND XX(56)=P-I-A
432
433 *****
434 ASSIGN, ATRIB(56)=XX(55)-AT(56);
435 ATRIB(57)=AT(56)/XX(55);
436 ATRIB(58)=AT(56)/XX(55);
437
438 AT(58) IS SYD DEPRETIATION
439
440 ASSIGN, ATRIB(31)=AT(58)/XX(76);
441 ATRIB(76)=AT(58)-AT(31);
442 XX(76)=XX(75)-1;
443 ACT, XX(76).LE, 0, CRCT;
444 ACT, XX(76).GT, 0, OKEY;
445 ASSIGN, XX(76)=1;
446
447 AT(31) IS THE SLD @AT(76) IS THE BOOK VALUE
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***** THIS PART OF THE PROGRAM IS FOR THE ALTERNATIVE II *****
CREATE,1;
ASSIGN,ATRIB(90)=TN0;

***** THIS PART GENERATES DATA BY BETA DISTRIBUTION *****
***** CONSTRUCTION COST *****
ASSIGN,ATRIB(1)=XX(174)-XX(173),ATRIB(2)=XX(174)+XX(183),
ASSIGN,ATRIB(3)=XX(173)*2;
ASSIGN,ATRIB(4)=ATRIB(2)-ATRIB(3),ATRIB(4)=ATRIB(4)+ATRIB(1),
ASSIGN,ATRIB(5)=XX(174)*XX(174)+ATRIB(6)=XX(183)*XX(183),
ASSIGN,ATRIB(6)=ATRIB(5)-ATRIB(7)=XX(174)-XX(183);
ASSIGN,ATRIB(8)=ATRIB(4)/ATRIB(7);
ASSIGN,ATRIB(9)=XX(173)-XX(183);
ASSIGN,XX(92)=ATRIB(9)/ATRIB(10)=ATRIB(8)+ATRIB(9);
XX(92)=ATRIB(9),XX(87)=ATRIB(10);
XX(92)=XX(92)+XX(87),XX(87)=2;
ASSIGN,XX(81)=XX(183)-XX(174),XX(81)=XX(81)+XX(89);
XX(121)=XX(81)+XX(174),ATRIB(73)=XX(121)+XX(190);
ASSIGN,ATRIB(73)=ATRIB(73)+XX(373);

***** FUEL COST *****
ASSIGN,ATRIB(1)=XX(118)-XX(119),ATRIB(2)=XX(118)+XX(120),
ATRIB(3)=XX(119)*2;
ASSIGN,ATRIB(4)=ATRIB(2)-ATRIB(3),ATRIB(4)=ATRIB(4)+ATRIB(1),
ATRIB(5)=ATRIB(4)+4;
ASSIGN,ATRIB(6)=ATRIB(5)+XX(118)*XX(118),ATRIB(6)=XX(120)+XX(120);
ASSIGN,ATRIB(7)=ATRIB(6)+XX(118)-XX(120);
ASSIGN,ATRIB(8)=ATRIB(7)+ATRIB(3),ATRIB(8)=ATRIB(6)-ATRIB(7);
ASSIGN,ATRIB(9)=XX(119)-XX(120);
ASSIGN,ATRIB(10)=ATRIB(9)+ATRIB(8)+ATRIB(9);
XX(92)=ATRIB(10),XX(87)=ATRIB(10);
XX(92)=XX(92)+XX(87),XX(87)=2;
ASSIGN,XX(81)=XX(120)-XX(118),XX(81)=XX(81)+XX(89);
ATRIB(79)=XX(81)+XX(118);
ASSIGN,ATRIB(79)=ATRIB(79)+XX(379);

***** O3M COST (FIXED) *****
ASSIGN,ATRIB(1)=XX(180)-XX(186),ATRIB(2)=XX(180)+XX(188),
ATRIB(3)=XX(186)*2;
ASSIGN,ATRIB(4)=ATRIB(2)-ATRIB(3),ATRIB(4)=ATRIB(4)+ATRIB(1),
ATRIB(5)=XX(180)+XX(190)*XX(190),ATRIB(5)=XX(188)+XX(188);
ASSIGN,ATRIB(6)=ATRIB(5)-ATRIB(7)=XX(180)-XX(188);
ASSIGN,ATRIB(8)=ATRIB(4)/ATRIB(7);
ASSIGN,ATRIB(9)=XX(186)-XX(188);
ASSIGN,XX(92)=ATRIB(9)/ATRIB(10)=ATRIB(8)+ATRIB(9);
XX(92)=ATRIB(9),XX(87)=ATRIB(10);
XX(92)=XX(92)+XX(87),XX(87)=2;
ASSIGN,XX(81)=XX(180)-XX(186),XX(81)=XX(81)+XX(89);
ATRIB(81)=XX(81)+XX(180);

***** O3M COST (VARBL) *****
ASSIGN,ATRIB(81)=ATRIB(81)+XX(381);
ASSIGN,ATRIB(81)=XX(128)-XX(129),O3M COST (VARBL);
ASSIGN,ATRIB(81)=XX(129)*2;
ASSIGN,ATRIB(82)=ATRIB(2)-ATRIB(3),ATRIB(82)=ATRIB(4)+ATRIB(1),
ASSIGN,ATRIB(83)=XX(128)+XX(130);
ASSIGN,ATRIB(84)=ATRIB(4)+4;
ASSIGN,ATRIB(85)=XX(128)*XX(128)+ATRIB(6)=XX(130)+XX(130);
ASSIGN,ATRIB(86)=ATRIB(85)-ATRIB(87)=XX(128)-XX(130);
ASSIGN,ATRIB(87)=ATRIB(86)+ATRIB(3),ATRIB(87)=ATRIB(6)-ATRIB(7);
ASSIGN,ATRIB(88)=ATRIB(87)+ATRIB(7)+XX(130);
ASSIGN,XX(92)=ATRIB(88)/ATRIB(89)=XX(130)+ATRIB(9);
XX(92)=ATRIB(88),XX(87)=ATRIB(89);
XX(92)=XX(92)+XX(87),XX(87)=2;
ASSIGN,XX(81)=XX(130)-XX(128),XX(81)=XX(81)+XX(89);
ATRIB(82)=XX(81)+XX(128);
ASSIGN,ATRIB(82)=ATRIB(82)+XX(382);

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77089 03M ESC RATE
77090 1) = XX(137) * ATRIB(2) = XX(157) * XX(124),
77091 2) = XX(139) * ATRIB(3) * ATRIB(4) = ATRIB(1),
77092 3) = XX(137) * ATRIB(6) = XX(124) * XX(124),
77093 4) = XX(137) * ATRIB(7) = XX(137) * XX(124),
77094 5) = XX(137) * ATRIB(7) * ATRIB(7) = ATRIB(6) - ATRIB(7),
77095 6) = XX(139) * XX(124),
77096 7) = ATRIB(10) = ATRIB(8) * ATRIB(9);
77097 8) = XX(137) * XX(87) * 2);
77098 9) = XX(124) * XX(81) * XX(89),
77099 10) = XX(137) * ATRIB(85) = ATRIB(85) * XX(385) ;
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711 SUC1 ASSIGN,TRIB(20)=XX(113);
712 SUC2 ACT,TRIB(20)=XX(114);
713 SUC3 ACT,TRIB(20)=XX(115);
714 SUC4 ACT,TRIB(20)=XX(115);
715 SUC5 ACT,TRIB(20)=XX(158);
716 SUC6 ACT,TRIB(20)=XX(159);
717 SUC7 ACT,TRIB(20)=XX(160);
718 SUC8 ACT,TRIB(20)=XX(161);
719 FWR2 ACT,TRIB(20)=XX(162);
720 FWR2 ACT,TRIB(27)=XX(127),XX(121),TRIB(16)=TRIB(16)-TRIB(27),
721 FWR2 ACT,TRIB(34)=TRIB(34)=XX(121);
722 FWR2 ASSIGN,TRIB(30)=XX(125),TRIB(76)=TRIB(30),XX(176)=XX(166),
723 FWR2 ACT,TRIB(51)=XX(135),TRIB(52)=XX(136)-TRIB(51);
724 FWR2 ASSIGN,TRIB(54)=XX(136),XX(136),
725 FWR2 ACT,XX(148),EQ0,BE12;
726 FWR2 ACT,XX(148),EQ1,ALF2;
727 FWR2 ASSIGN,TRIB(64)=TRIB(6),XX(103),TRIB(63)=TRIB(6);
728 FWR2 ACT,XX(140),XX(140);
729 FWR2 ASSIGN,XX(140)=XX(103)+1,XX(141)=XX(103)+1;
730 FWR2 ASSIGN,TRIB(61)=TRIB(61)+1,XX(141)=XX(141)*XX(140);
731 FWR2 ACT,TRIB(61),LE,XX(126),EQC2;
732 FWR2 ACT,TRIB(61),GE,XX(126),EQC2;
733 FWR2 ASSIGN,XX(142)=XX(141)-1,XX(143)=XX(141)*XX(103);
734 FWR2 XX(144)=XX(143)/XX(142),TRIB(36)=TRIB(6)*XX(144);
735 FWR2 ASSIGN,XX(145)=TRIB(6),XX(103),XX(146)=XX(145)-TRIB(36),
736 FWR2 ACT,XX(140)/XX(140);
737 FWR2 ACT,XX(151),EQ0,DB12;
738 FWR2 ACT,XX(151),EQ1,DB13;
739 FWR2 ASSIGN,TRIB(66)=TRIB(5),XX(104),TRIB(67)=TRIB(5);
740 FWR2 ACT,OP,LE2;
741 FWR2 ASSIGN,XX(149)=XX(104)+1,TRIB(65)=0,XX(150)=XX(104)+1;
742 FWR2 RED2 ACT,TRIB(65),LE,XX(126),CAL2;
743 FWR2 RED2 ACT,TRIB(65),GE,XX(126),CAL2;
744 FWR2 CAL2 ASSIGN,XX(152)=XX(150),XX(153)=XX(150)*XX(104);
745 FWR2 CAL2 XX(154)=XX(153)/XX(152),TRIB(68)=TRIB(5)*XX(154);
746 FWR2 ASSIGN,XX(155)=TRIB(6),XX(104),XX(156)=XX(155)-TRIB(68),
747 FWR2 OPE2 ACT,TRIB(69)=XX(149),XX(149),TRIB(46);
748 FWR2 OPE2 ACT,TRIB(68)=XX(166)-TRIB(46);
749 FWR2 OPE2 ACT,TRIB(57)=TRIB(57)*TRIB(30);
750 FWR2 OPE2 ASSIGN,TRIB(31)=TRIB(76)/XX(176),TRIB(76)=TRIB(76)-TRIB(31),
751 FWR2 XX(176)=XX(176)-1;
752 FWR2 ACT,XX(176),LE,0,CRC2;
753 FWR2 ACT,XX(176),GT,0,OKE2;
754 FWR2 OPE2 ASSIGN,XX(176)=1,XX(133)=0;
755 FWR2 OPE2 ASSIGN,TRIB(53)=XX(121),XX(134)=0;
756 FWR2 OPE2 ACT,TRIB(58)=TRIB(18),XX(134),TRIB(53)=TRIB(53)*XX(133),
757 FWR2 OPE2 ACT,TRIB(37)=XX(146)*TRIB(62),TRIB(37)=TRIB(37)+TRIB(36),
758 FWR2 OPE2 XX(147)=TRIB(36)-TRIB(37);
759 FWR2 OPE2 XX(157)=TRIB(68)=XX(156)+TRIB(70);
760 FWR2 OPE2 ASSIGN,TRIB(34)=TRIB(34)-TRIB(31),
761 FWR2 OPE2 ASSIGN,TRIB(34)=TRIB(34)-TRIB(53),
762 FWR2 OPE2 ACT,TRIB(34)=TRIB(34)*XX(105);
763 FWR2 OPE2 ACT,TRIB(34)=TRIB(2)+TRIB(25),
764 FWR2 OPE2 ACT,TRIB(40)=TRIB(40)+TRIB(7),
765 FWR2 OPE2 ACT,TRIB(40)=TRIB(40)+TRIB(28),
766 FWR2 OPE2 ACT,TRIB(40)=TRIB(40)+TRIB(35),
767 FWR2 OPE2 ACT,TRIB(41)=TRIB(41)+TRIB(31),
768 FWR2 OPE2 ACT,TRIB(41)=TRIB(41)+TRIB(58),
769 FWR2 OPE2 ACT,TRIB(41)=TRIB(41)+TRIB(53),
770 FWR2 OPE2 ASSIGN,TRIB(40)=TRIB(40)+TRIB(10);
771 FWR2 OPE2 OPE2 ACT,TRIB(40)=TRIB(40)+TRIB(10);
772 FWR2 OPE2 OPE2 ACT,TRIB(40)=TRIB(40)+TRIB(10);
773 FWR2 OPE2 OPE2 ACT,TRIB(40)=TRIB(40)+TRIB(10);
774 FWR2 OPE2 OPE2 ACT,TRIB(40)=TRIB(40)+TRIB(10);
775 FWR2 OPE2 OPE2 ACT,TRIB(40)=TRIB(40)+TRIB(10);
776 FWR2 OPE2 OPE2 ACT,TRIB(40)=TRIB(40)+TRIB(10);
777 FWR2 OPE2 OPE2 ACT,TRIB(40)=TRIB(40)+TRIB(10);
778 FWR2 OPE2 OPE2 ACT,TRIB(40)=TRIB(40)+TRIB(10);
779 FWR2 OPE2 OPE2 ACT,TRIB(40)=TRIB(40)+TRIB(10);
780 FWR2 OPE2 OPE2 ACT,TRIB(40)=TRIB(40)+TRIB(10);
781 FWR2 OPE2 OPE2 ACT,TRIB(40)=TRIB(40)+TRIB(10);
782 FWR2 OPE2 OPE2 ACT,TRIB(40)=TRIB(40)+TRIB(10);
783 FWR2 OPE2 OPE2 ACT,TRIB(40)=TRIB(40)+TRIB(10);
784 FWR2 OPE2 OPE2 ACT,TRIB(40)=TRIB(40)+TRIB(10);

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785  ATRIB(40)=ATRIB(40)+ATRIB(56);
786  ATRIB(40)=ATRIB(40)+ATRIB(54);
787  ATRIB(40)=ATRIB(40)+XX(157); ATRIB(40)=ATRIB(40)-ATRIB(42);
788  ASSIGN,ATRIB(40)=ATRIB(40)/ATRIB(3); ATRIB(40)=ATRIB(40)+ATRIB(42);
789  ATRIB(62)=ATRIB(62)+XX(140); ATRIB(69)=ATRIB(69)+XX(149);
790  ATRIB(45)=ATRIB(45)+ATRIB(43);
791  ASSIGN,ATRIB(45)=ATRIB(24)+XX(109); ATRIB(25)=ATRIB(25)+XX(110);
792  ATRIB(26)=ATRIB(26)-ATRIB(36);
793  ATRIB(51)=ATRIB(51)+ATRIB(52); ATRIB(3)=ATRIB(3)+XX(101);
794  ASSIGN,ATRIB(46)=ATRIB(46)+1;
795  ACT,ATRIB(46)=LT,XX(126),OPF2;
796  ASSIGN,ATRIB(46)=GE,XX(126),F12;
797  ASSIGN,ATRIB(47)=ATRIB(3)/XX(101);
798  ATRIB(67)=ATRIB(67)+ATRIB(63);
799  ATRIB(69)=ATRIB(67)-XX(125); ATRIB(48)=ATRIB(47);
800  ATRIB(50)=ATRIB(49)+ATRIB(16);
801  ASSIGN,XX(167)=XX(101)-1,XX(169)=XX(101);
802  ASSIGN,ATRIB(71)=ATRIB(71)+1,XX(169)=XX(169)+XX(101);
803  ACT,ATRIB(71)=LT,XX(126),LAS2;
804  ACT,ATRIB(71)=GE,XX(126),EDA2;
805  ASSIGN,XX(170)=XX(167)+XX(169);
806  ATRIB(75)=XX(172); ATRIB(72)=ATRIB(50)+XX(172);
807  QUEUE(2)=FNAME;
808  MATCH,90,LBL1/CLC1,LBL2/CLC2;
809  ;
810  ;
811  ;
812  ;
813  ;
814  CLC1 COLCT,XX(97),ANN,EQ,COST1,25,0.20E+09,0.10E+08 ;
815  TERM;
816  CLC2 COLCT,XX(197),ANN,EQ,COST2,30,0.20E+09,0.10E+08;
817  ASSIGN,XX(99)=XX(97)-XX(197);
818  COLCT,XX(99),DIFFERENCE,50,-0.15E+09,0.5E+7;
819  ;
820  ;
821  TERM,300;
822  ENDNET;
823  ;

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S L A M E C H O R E P O R T
SIMULATION PROJECT EXERCISE          BY MEDI
DATE 1/22/1980                        RUN NUMBER 1 OF 1
SLAM VERSION JAN 79

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*****
COLLECTION OF DESIRED DATA
*****
NUMBER OF OBSERVATIONS DESIRED
*****
GENERAL OPTIONS
PRINT INPUT STATEMENTS (ILIST):      YES
PRINT ECHO REPORT (IECHO):           YES
EXECUTE SIMULATIONS (IXOT):         YES
PRINT INTERMEDIATE RESULTS HEADING (IPRH): YES
PRINT SUMMARY REPORT (ISMRY):       YES

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LIMITS ON FILES
MAXIMUM NUMBER OF USER FILES (MFILES): 2
MAXIMUM NUMBER OF USER ATTRIBUTES (MATR): 90
MAXIMUM NUMBER OF CONCURRENT ENTRIES (MNTRY): 200

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FILE SUMMARY
FILE NUMBER          INITIAL ENTRIES  RANKING CRITERION
1                    0                FIFO
2                    0                FIFO

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STATISTICS BASED ON OBSERVATIONS

COLLECT NUMBER	COLLECTION MODE	IDENTIFIER	HISTOGRAM SPECIFICATIONS
			NCEL HLOW HWID
1	NETWORK	ANN*EQ.COST1	25 0.200E+09 0.100E+08
2	NETWORK	ANN*EQ.COST2	30 0.200E+09 0.100E+08
3	NETWORK	DIFFERENCE	50 -0.150E+09 0.600E+07

RANDDM NUMBER STREAMS

STREAM NUMBER	SEED VALUE	REINITIALIZATION OF STREAM
1	1274321477	NO
2	2135124613	NO
3	1743251541	NO
4	1624217675	NO
5	2014632579	NO
6	2036774231	NO
7	1452313571	NO
8	1254240657	NO
9	1410143363	NO
10	2135621895	NO

INITIALIZATION OPTIONS

BEGINNING TIME OF SIMULATION (TTBEG): 0.0  
 ENDING TIME OF SIMULATION (TTFIN): 0.1000E+21  
 STATISTICAL ARRAYS CLEARED (JJCLR): YES  
 VARIABLES INITIALIZED (JJVAR): YES  
 FILES INITIALIZED (JJFIL): YES

NSET/OSSET STORAGE ALLOCATION

DIMENSION OF NSET/OSSET (NVSSET): 25000  
 WORDS ALLOCATED TO FILLING SYSTEM: 18800  
 WORDS ALLOCATED TO NETWORK: 6010  
 WORDS AVAILABLE FOR PLOTS/TABLES: 190

INPUT ERRORS DETECTED: 0

EXECUTION WILL BE ATTEMPTED

\*\*INTERMEDIATE RESULTS\*\*

S L A M S U M M A R Y R E P O R T

SIMULATION PROJECT EXERCISE BY MEDI  
 DATE 1/22/1980 RUN NUMBER 1 OF 1  
 CURRENT TIME 0.2990E+03  
 STATISTICAL ARRAYS CLEARED AT TIME 0.0

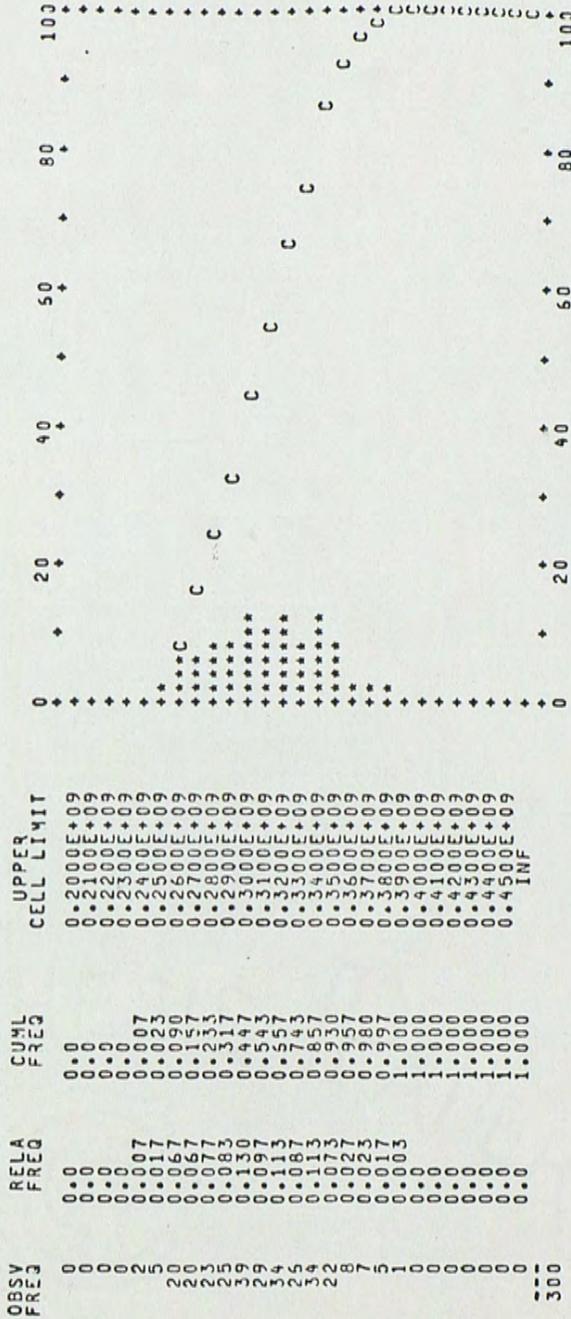
\*\*STATISTICS FOR VARIABLES BASED ON OBSERVATION\*\*

	MEAN VALUE	STANDARD DEVIATION	COEFF OF VARIATION	MINIMUM VALUE	MAXIMUM VALUE	NUMBER OF OBSERVATIONS
ANN.EQ.COST1	0.3057E+09	0.3155E+08	0.1032E+00	0.2334E+09	0.3825E+09	300
ANN.EQ.COST2	0.3200E+09	0.4262E+08	0.1332E+00	0.2283E+09	0.4309E+09	300
DIFFERENCE	-0.1421E+08	0.5178E+08	-0.3645E+01	-0.1705E+09	0.1106E+09	300

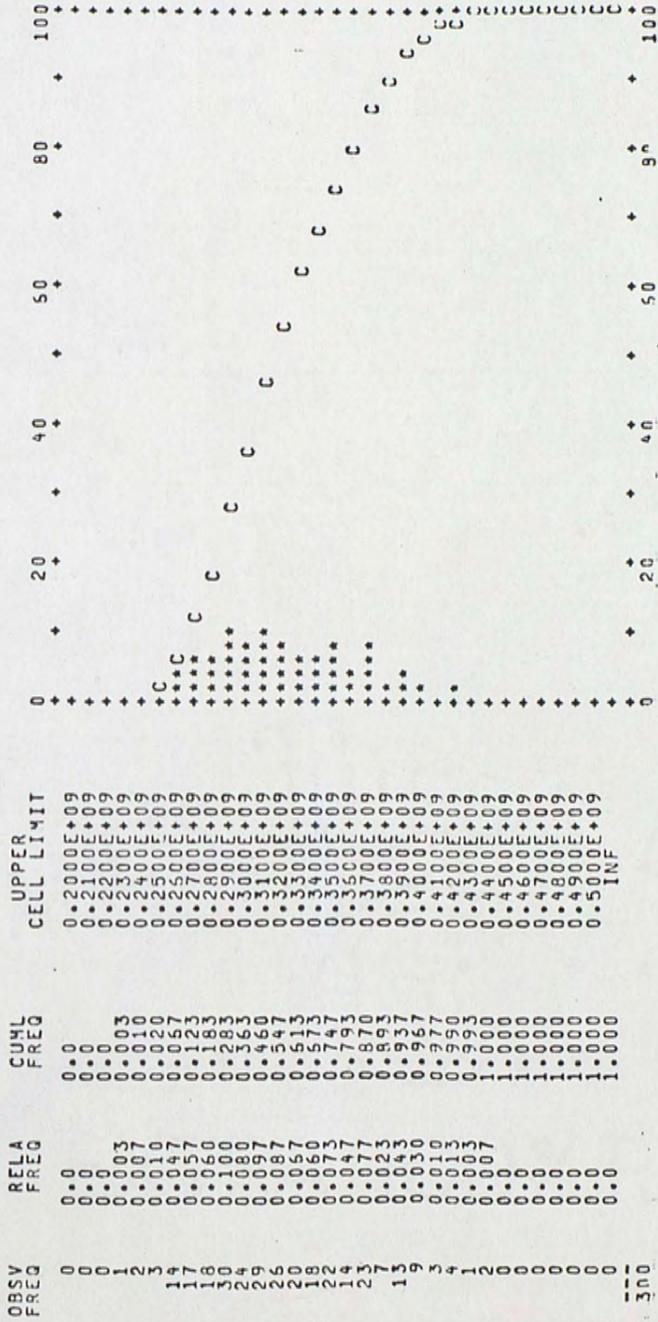
\*\*FILE STATISTICS\*\*

FILE NUMBER	ASSOCIATED NODE TYPE	AVERAGE LENGTH	STANDARD DEVIATION	MAXIMUM LENGTH	CURRENT LENGTH
1	QUEUE	0.0	0.0	1	0
2	QUEUE	0.0	0.0	1	0
3	QUEUE	2.0000	0.0	4	2

\*\*HISTOGRAM NUMBER 1\*\*  
ANN.EQ.COST1

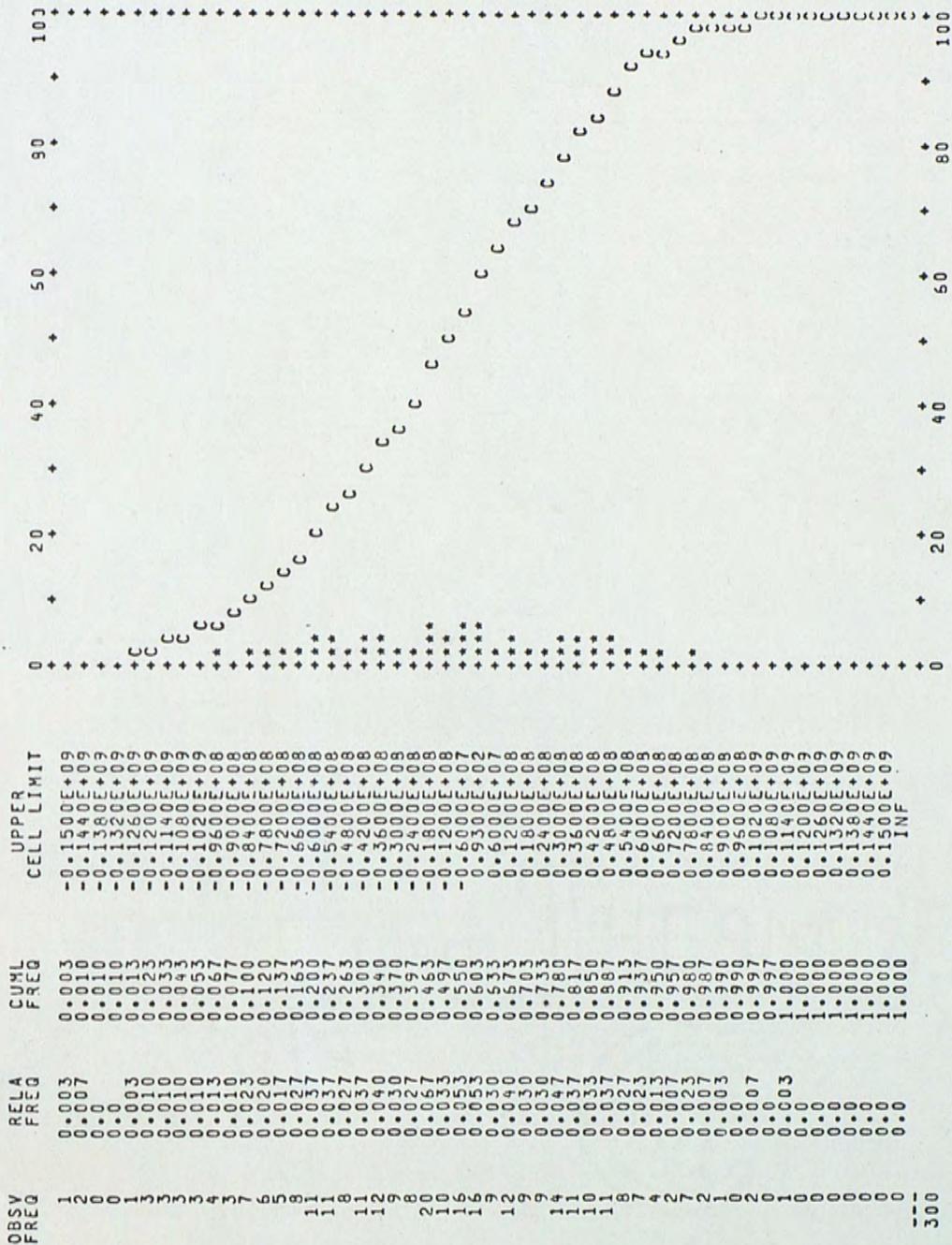


\*\*HISTOGRAM NUMBER 2\*\*  
ANN.EQ.COST2



\*\*HISTOGRAM NUMBER 3\*\*

DIFFERENCE



## REFERENCES

1. Crawley, Gerard M. "Advantages of Fission Reactors." Energy. New York: McMillian Publishing Co., Inc., 1975. 116.
2. Brooking, S. A., and Burgiss, A. R. "Present Worth of Interest Tax Credit." Engineering Economist 21 (Winter 1976): 111-118.
3. Canada, John R. Intermediate Economic Analysis for Management and Engineering. Englewood Cliffs , N. J.: Prentice-Hall, Inc., 1971. 283.
4. McBride, W., and McClell, C. "PERT and The Beta Distribution." IEEE Transaction on Engineering Management 4 EM. (December 1976): 166-69.
5. Budwaani, R. N. "Fossil Fired Power Plants - What it Takes to Get Them Built." Power Engineering, May 1978, pp. 36-42.