

Experimental evaluation of postdetection diversity reception of narrow-band digital FM signals in Rayleigh fading

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# Experimental Evaluation of Postdetection Diversity Reception of Narrow-Band Digital FM Signals in Rayleigh Fading

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Abstract-Postdetection diversity is attractive for narrow-band digital FM signal reception because a cophasing function that may be difficult to realize in a fast Rayleigh fading environment, is not required. The combining scheme evaluated in this paper weighs each frequency detector (FD) output in proportion to the vth power of the received signal envelope of that branch. Maximum diversity improvement can be obtained when v = 2 (this combiner is referred to as postdetection maximal ratio combiner (MRC) in this paper). This paper presents experimental results of postdetection diversity reception in the Gaussian minimum shift keying (GMSK) signal transmission system. Diversity combining and FDdecision algorithms (decision feedback equalizer (DFE) and maximum likelihood sequence estimator (MLSE)) are performed by software on a computer using the data of the sampled FD output and received signal envelope obtained from a laboratory transmission system. It will be shown that the MRC can attain about a 1-dB larger diversity gain than the selection combiner (SC) when two-branch diversity is used. The degradations of two-branch diversity improvement caused by the differences between FD sensitivities and between received signal envelope detector gains are evaluated.

#### I. INTRODUCTION

'N DIGITAL mobile radio, a narrow-band digital FM mod-Lulation or continuous phase modulation (CPM) [1] is a promising modulation scheme because of its narrow-band power spectrum and constant envelope property (Gaussian minimum shift keying (GMSK) [2] and generalized tamed FM (GTFM) [3] are special cases of narrow-band digital FM). Although both coherent and noncoherent (differential and frequency) detection can be applied to the reception of narrow-band digital FM signals, frequency detection is of much greater interest because of its resistance to carrier frequency drift and also because carrier recovery is not required. However, the bit error rate (BER) performance with frequency detector (FD) reception is severely degraded by the increased intersymbol interference (ISI) due to premodulation filtering used in a narrow-band digital FM systems. Several improved decision schemes using decision feedback equalizer (DFE) [4], [5] and maximum likelihood sequence estimator (MLSE) [3], [6] have been investigated.

It is well known that signal transmissions for land mobile radio suffer from multipath Rayleigh fading, which severely degrades the BER performance. Diversity reception [7] is a powerful technique to reduce the impact of fading. Predetec-

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tion diversity that coherently combines the received signals before demodulation may be difficult to implement because of fast phase variations in the received fading signal. Another reason for the preference of postdetection diversity is that if a predetection selection combiner (SC) is used, switching between two fading signals may cause an abrupt phase change that will produce bit errors. Postdetection diversity combines the detector outputs which are in phase; therefore, it requires no cophasing function, and can be applied to narrow-band digital FM systems. Recently, Adachi et al. [5], [8] predicted theoretically that when each FD output is weighted before combination in proportion to the square of the received signal envelope, the two branch postdetection diversity gain is only about 0.9 dB inferior to the predetection maximal-ratio combiner (MRC) and that about a 1.5-dB larger diversity gain than SC is possible.

This paper presents a follow-up study to [5] and [8] and emphasizes the experimental evaluation of postdetection diversity reception of narrow-band digital FM signals. Section II describes a postdetection diversity combining scheme that weights the detector outputs in proportion to the  $\nu$ th power of each received signal envelope and combines them before the decision operation. In Section III, the postdetection combining is applied to a GMSK transmission system and the average BER performance obtained by computer simulation using data on sampled FD outputs (eyes) and received signal envelopes are presented. MLSE and DFE are considered as decision schemes. How the value of  $\nu$  affects the average BER is first investigated. Next, the BER performance of MRC ( $\nu = 2$ ) is compared with that of SC.

Both the DFE and MLSE algorithms are based on the sum of the FD outputs of each branch weighted by the received signal envelope. Therefore, degradations of diversity improvement caused by differences between FD sensitivities and between received signal envelope detector gains are also evaluated for two-branch diversity reception.

#### II. POSTDETECTION DIVERSITY COMBINING

Fig. 1 shows a block diagram of narrow-band binary digital FM signal reception with postdetection diversity combining. A transmitted signal with carrier angular frequency  $\omega_c$  can be represented as  $s(t) = \text{Re} [A \exp j \{\omega_c + \phi(t)\}]$ , where  $\phi(t)$  is the modulating phase given by

$$\phi(t) = \pi h \sum_{n=-\infty}^{\infty} a_n \int_{-\infty}^{t} g(t - nT) dt$$
 (1)

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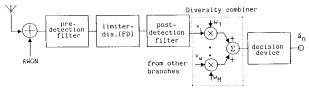


Fig. 1. Block diagram of narrow-band binary digital FM signal reception with postdetection diversity combining.

with  $a_n = \pm 1$  being the nonreturn-to-zero (NRZ) data, *h* the modulation index, and *T* the bit duration. g(t) is the frequency pulse response. In the case of GMSK, h = 0.5 and

$$g(t) = \frac{1}{2T} \left[ \operatorname{erf} \left( \beta \left( \frac{t}{T} + 0.5 \right) \right) - \operatorname{erf} \left( \beta \left( \frac{t}{T} - 0.5 \right) \right) \right]$$
(2)

where  $\operatorname{erf}(x)$  is the error function,  $\beta = \pi B_b T \sqrt{2/\ln 2}$  and  $B_b$  is the premodulation filter 3-dB bandwidth. We assume a multiplicative fading and a predetection filter that is wide enough to prevent severe received signal distortion. The FD (a limiter-discriminator followed by a postdetection filter is assumed) delivers the instantaneous angular frequency deviation of the received signal plus additive white Gaussian noise (AWGN). The FD output of the *m*th branch can be represented as

$$v_m(t) = \pi h \sum_{n=-\infty}^{\infty} a_n G(t - nT) + \text{noise term}$$
(3)

where G(t) is the response of the transmission channel including both predetection and postdetection filters to g(t). When an *l*-bit integrate-and-dump (I&D) postdetection filtering is used, G(t) becomes

$$G(t) = \int_{-|T/2}^{+|T/2} g(t-\tau) d\tau.$$
 (4)

When the received signal fades, the FD output  $v_m(t)$  is corrupted by noise due to AWGN. Therefore, it seems that little can be gained by simply combining all FD outputs. It is necessary to weight each FD output before combining so that the contribution of a noisy branch to the combiner output can be reduced. Letting  $R_m(t)$  be the received signal envelope of the *m*th branch,

$$w_{m}(t) = \frac{R_{m}^{\nu}(t)}{\sum_{m=1}^{M} R_{m}^{\nu}(t)}$$
(5)

can be used as the weighting factor.  $w_m(t)$  has been normalized so that the combiner output has the same eye level as in the no diversity case. The combiner output, fed to a decision device employing MLSE or DFE, is therefore represented as

$$v(t) = \sum_{m=1}^{M} w_m(t) v_m(t).$$
 (6)

SC is a special case where the weighting factor is unity for the FD output associated with the largest signal envelope and zero for all other branches. Using the normalized weighting factor of (5), the combiner output has a form identical to (3) except for the noise term that is now the sum of weighted noises from each FD. Therefore, this implies that improved decision schemes such as DFE and MLSE, can also be applied to postdetection diversity reception without any modification. The DFE and MLSE decision algorithms will be briefly reviewed before presenting the experimental results in Section III.

## A. DFE Decision Algorithm

We assume that the *n*th data  $a_n$  is to be detected without loss of generality. The sampling time is assumed to be taken at  $t_n = (n + \alpha)T$ , where  $\alpha$  is the appropriate sampling time offset that produces the minimum BER and is  $-1/2 \le \alpha \le 0$ . The combiner output is given by

$$\nu_n = \nu(t_n) = a_n \pi h G_a + \pi h \sum_{k=-\infty, \neq 0}^{\infty} a_{n-k} G_{k+a}$$
  
+weighted sum of noises. (7)

The second term of (7) is ISI from the past and future bits. A *K*-bit DFE is considered. It cancels the ISI from the past bits  $a_{n-k}$  ( $k = 1, 2, \dots, K$ ) using the previous decision result  $\hat{a}_{n-k}$  and subtracting  $\eta_{n-k} = \hat{a}_{n-k}\pi h G_{k+\alpha}$  (where  $G_{k+\alpha} = G((k + \alpha)T)$ ) from the combiner output prior to the decision on  $a_n$ . If all  $\hat{a}_{n-k}$  are correct, then the perfect cancellation of the ISI from the past *K* bits is possible. The decision is based on the polarity of

$$v'_n = v_n - \pi h \sum_{k=1}^K \hat{a}_{n-k} G_{k+\alpha}, \qquad (8)$$

and  $\hat{a}_n = 1$  if  $v'_n \ge 0$  and -1 if  $v'_n < 0$ . The 2-bit DFE proposed by Hirono *et al.* [4] uses 2-bit I&D postdetection filtering with  $\alpha = -1/2$  (thus the integration period is from t = (n - 3/2)T to (n + 1/2)T).

## B. MLSE Decision Algorithm

When the combiner output is sampled at  $t_n = (n - 1/2)T$ , we obtain

$$\nu_n = (a_n + a_{n-1})\pi h G_{1/2} + \pi h \sum_{k=-\infty, \neq 0, 1}^{\infty} a_{n-k} G_{k-1/2}$$
  
+weighted sum of noises, (9)

which is a three-level eye that depends on the consecutive two bits,  $a_n$  and  $a_{n-1}$ . This correlative property is effectively used in Chung's MLSE decision algorithm [3], which is based on the assumption of white Gaussian noise and no ISI. However, click noise appears at the FD output and furthermore ISI exists in the case of GMSK. Although Chung's MLSE is not a real one in the strict sense, it significantly improves BER performance. The following three parameters U, V, and  $W_n$ are introduced [3]:

$$U = W_n + v_{n+1} - A$$
$$V = W_n + v_{n+1} + A$$
(10)

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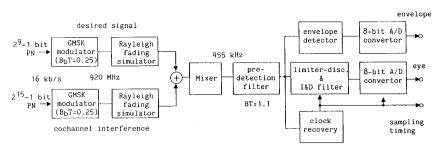


Fig. 2. Laboratory experiment block diagram (single branch).

where  $A = \pi h G_{1/2}$ . The decision rule is  $\hat{a}_n = 1$  if  $U \ge 0$  and -1 if V < 0. If neither  $U \ge 0$  or V < 0, a definite decision is not possible, and it is necessary to store both binary sequences in output shift registers until the condition where either  $U \ge 0$  or V < 0 occurs. Finally,  $W_{n+1}$  is updated using the present decision result:

$$W_{n+1} = \begin{cases} v_{n+1} - A, & \text{if } U \ge 0(\hat{a}_n = 1) \\ v_{n+1} + A, & \text{if } V < 0(\hat{a}_n = -1) \\ -W_n, & \text{if } U < 0 \text{ and } V \ge 0. \end{cases}$$
(11)

Adachi and Parsons [8] investigated theoretically how the values of  $\nu$  affect the BER and found that the BER can be minimized (or the diversity gain can be maximized) by choosing  $\nu = 2$ . This combiner was referred to as postdetection MRC [8]. The diversity gain of two-branch postdetection MRC approaches that of predetection MRC with a loss of about 0.9 dB in average signal energy per bit-to-noise power spectrum density ratio  $(E_b/N_0)$  when applied to MSK signal reception. This small difference in diversity gain between predetection and postdetection diversity can also be preserved for narrow-band digital FM signal reception [5]. The most attractive feature of postdetection diversity is that it requires no cophasing function to combine all FD outputs, thus its implementation is simpler. So far, postdetection SC has been extensively investigated for mobile radio use because of its simplicity [9]-[11]. However, comparison of postdetection MRC and SC predicted that [8] about a 1.5-dB larger diversity gain than SC can be obtained with M = 2 (two-branch diversity). This fact encourages us to apply postdetection MRC.

## **III.** EXPERIMENTS

We applied postdetection diversity using MRC and SC to a GMSK transmission system in multiplicative Rayleigh fading environments. In cellular mobile radio systems, the same radio channels are reused for spatially separated cells, in order to efficiently use the limited radio spectrum resources efficiently. The smaller the cell size becomes, the more the transmission performance is governed by cochannel interference. Hence the improvement in BER performance in the cochannel interference limited channel is as important as that in the AWGN channel. Therefore, both channels were considered in the experiments.

The DFE decision algorithm considered here was the 1-bit type [5]. The two output shift registers used for MLSE were 16 bits each.

# A. Experimental Procedure

The laboratory experiment block diagram for single branch case is shown in Fig. 2. A 16-kbit/s  $(2^9 - 1)$ -bit PN sequence was used as the transmitted data. A generated 920-MHz GMSK signal with h = 0.5 and  $B_bT = 0.25$  was fed into a fading simulator to produce a multiplicative Rayleigh fading signal with a maximum Doppler frequency of 40 Hz (this corresponds to a vehicle speed of about 47 km/h). The cochannel interference signal (GMSK with  $B_bT = 0.25$ ) was generated using a  $(2^{15} - 1)$ -bit PN sequence and fed to another Rayleigh fading simulator. The desired signal and cochannel interference signal were combined to form the input to the GMSK-FD receiver. The receiver had a predetection filter with a 3-dB bandwidth of 17 kHz (BT = 1.1) at an IF stage of 455 kHz and a limiter-discriminator followed by a 1-bit I&D postdetection filter.

Postdetection diversity combining with DFE and MLSE decision algorithms described in Section II was performed by software on the computer to allow a valid evaluation of BER performance. For this, the I&D filter output (eye) and the received signal envelope were converted into digital format using two 8-bit A/D convertors and sampled eye and envelope data were stored in memory. The maximum number of diversity branches considered in the experiment was four. Data for each diversity branch were collected using a single branch over a time interval of 32 periods of the  $(2^9 - 1)$ -bit PN sequence; the numbers of sampled eyes and associated envelopes were 16,352 each. The time interval between obtaining the data for each diversity branch was larger than 32 PN sequence periods and thus sufficiently large to make the fading of one branch independent of the others.

We used a sampling timing offset  $\alpha = -0.25$  for 1-bit DFE (found to be optimum through experiments). The A/D range for eye conversion was  $\pm 1.5 \pi$  rad and 50 dB for the received signal envelope.

## B. Results

First, the way in which the value of  $\nu$  affects the average BER was investigated for 1-bit DFE. The value of  $w_m$  were first calculated using the stored received signal envelope and then the sampled eyes were weighted to allow combination according to (6). The dependence of the average BER on the value of  $\nu$  for two-branch diversity (M = 2) is shown in Fig. 3 for various average  $E_b/N_0$ . It can be seen that, as  $\nu$  increases, the average BER decreases, but it almost remains

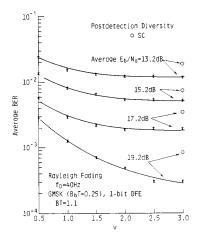


Fig. 3. Dependence of average BER on v for 1-bit DFE, M = 2.

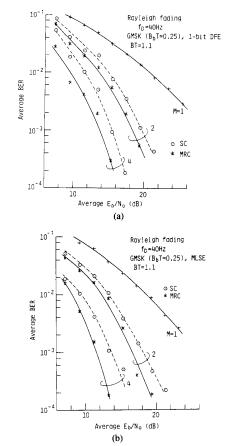


Fig. 4. Average BER performance as function of average  $E_b/N_0$ . (a) 1-bit DFE. (b) MLSE.

constant above  $\nu = 2$  (MRC). This is consistent with the analysis given in [8]. For comparison, the BER's achieved by postdetection SC are plotted in the figure for the same  $E_b/N_0$  values. As expected, MRC can achieve smaller average BERs than SC. In the subsequent experiments, both MRC and SC were used.

Fig. 4(a) and (b) show the average BER performance as a

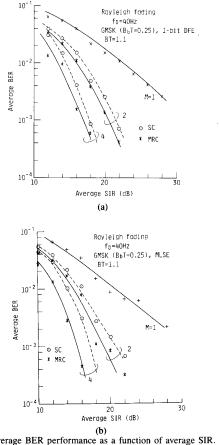


Fig. 5. Average BER performance as a function of average SIR. (a) 1-bit DFE. (b) MLSE.

function of average  $E_b/N_0$  for M = 1 (without diversity), 2 and 4 for 1-bit DFE and MLSE, respectively. It can be seen that when M = 2, MRC achieves a BER of  $10^{-2}$  with about 6-7 dB less average  $E_b/N_0$  than the no diversity case. This is about a 1-dB larger diversity gain than with SC. It was observed that as M increases, the difference between MRC and SC diversity gains tends to become larger. When M = 4, the diversity gain of MRC is about 10 dB at a BER of  $10^{-2}$ which is about 2 dB larger than with SC. The average BER performance as a function of average signal-to-interference ratio (SIR) is shown in Fig. 5. The diversity gain improvement of MRC over SC is observed as in AWGN channels.

Figs. 4 and 5 prove that postdetection MRC can be applied to narrow-band digital FM systems in order to yield larger diversity gains than is possible with SC. The only requirement is to weight all the FD outputs with the squared received signal envelope and combine them before input to the decision device.

Comparison of the performance achievable with the use of DFE and MLSE decision algorithms is interesting. Although Chung's MLSE is not a real one, it has been found to provide about 1 dB superior performance at a BER of  $10^{-2}$  in both AWGN and cochannel interference limited channels. The lower performance of DFE compared with MLSE is attributed to the fact that ISI from the future bits remains uncanceled.

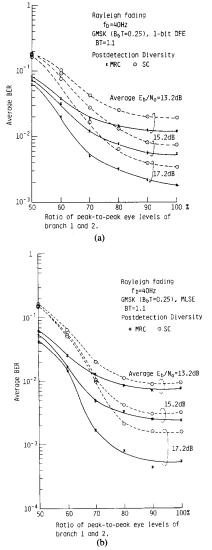


Fig. 6. Degradation due to difference between FD sensitivities. M = 2. (a) 1-bit DFE. (b) MLSE.

From the implementation point of view, however, the DFE decision algorithm is much simpler [5] than the MLSE decision algorithm and thus has a practical advantage over MLSE.

We have so far assumed identical FDs and identical received signal envelope detectors for all diversity branches. However, in practical receivers, there may be differences between demodulator sensitivities (or peak-to-peak eye levels without noise) and between envelope detector gains. Because both the DFE and MLSE decision algorithms are based on the sum of the weighted eye levels of each branch, those differences may degrade diversity improvements. Figs. 6 and 7 show the measured results for 1-bit DFE and MLSE when M = 2. It can be seen that MRC and SC experience similar degradation, however, MRC is still superior to SC. About 20-percent difference between FD sensitivities and about 2 dB difference between envelope detector gains are acceptable for both decision algorithms.

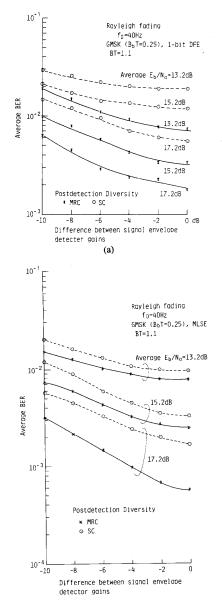


Fig. 7. Degradation due to difference between received signal envelope detector gains. M = 2. (a) 1-bit DFE. (b) MLSE.

#### IV. CONCLUSION

This paper has presented the experimental evaluation of postdetection diversity reception in narrow-band digital FM (GMSK) transmission system in multiplicative Rayleigh fading environments. As diversity combiners, both SC and MRC require the channel information of each diversity branch. The SC compares the values of the received signal envelopes and selects only the FD output of the branch having the maximum envelope. On the other hand, the MRC weights all FD outputs with the squared value of the envelope before combining them. Although the MRC algorithm adds some complexity to the combiner, diversity gains larger than those of the SC can be obtained because all FD outputs are effectively used. It has been experimentally shown that the MRC can attain about a 1-dB larger diversity gain than the SC when two-branch diversity is used. This improvement is in close agreement with the predicted value [5], [8].

In the experiment, postdetection diversity combining with improved decision algorithms was performed on a computer using the stored data of sampled eyes and received signal envelopes. This suggests the possibility that postdetection diversity combining and the decision algorithms (either DFE or MLSE) can be implemented in a single digital signal processor.

Postdetection diversity described in this paper is also applicable to other narrow-band modulation schemes such as GTFM and Nyquist pulse shaped PSK. Postdetection diversity analyzed for DPSK [7, ch. 6], and [12] is equivalent to the postdetection MRC of this paper.

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