# Phase modulator based on Silicon-on-Insulator (SOI) rib waveguide

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Abstract — This paper presents the study of electrical characteristic of phase modulator in the carrier injection mode. The phase modulator device has been integrated in the silicon-oninsulator (SOI) rib waveguide by using the p-i-n diode structure. The electrical device performance is predicted by using the 2-D semiconductor package SILVACO (CAD) software under DC operation. In summary, the phase modulator device required 0.035mA drive current to get  $\pi$  phase shift at wavelength 1.55 $\mu$ m meanwhile 0.066mA drive current is required for the 1.3 $\mu$ m wavelength.

*Index Terms*—Phase modulator, Silicon-on-Insulator, carrier injection, refractive index change.

#### I. INTRODUCTION

ONE of the new challenges in the optoelectronic field is the silicon photonics. Silicon photonics have been intensively studied by many research groups with the intention of linking it between the field of optical communication and the silicon integrated circuits. The performance of the integrated circuit (IC) will be improved by the integrating of the optics and the electronics on the same chip; in which it would benefit the telecommunications application for the development of the low cost solutions for the high-speed optoelectronic devices and systems. There are many benefits of the silicon as a photonic medium [1][3]. Especially, it is transparent in the range of optical telecommunications wavelengths (1.3 and 1.55μm) and because of it high index refraction. Due to its uniqueness characteristic, silicon is very

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suitable for the fabrication material of the high-index-contrast sub-micrometer structures [1]. Furthermore, the matured silicon integrated circuit process technology in bipolar and complementary metal-oxide semiconductor provides the breakthrough of the implementation of the dense silicon-based integrated optics and electronics on-chip. Optoelectronic devices such as the modulator and the switch is very much dependable on the plasma dispersion effect and the thermal effects in the silicon. From the previous research, it is proven that the most successful silicon optical modulators are based on the free carrier density. By inducing more free carrier in the guidance region, it will control the optical refractive index xccv bchanges [3,4]. This can be achieve by the doping of the p+ or n+ region nearer the waveguide. Soref and Bennet [7] quantified the changes they had identified from the research for the refractive index and in the absorption coefficents. The following equations are widely used in order to evaluate changes due to injection or depletion of carriers in silicon and hence are utilized in this report:

At 
$$\lambda_0$$
 = 1.55  $\mu$ m:   
  $\Delta n = \Delta n_{e^-+} \Delta n_h = -[8.8 \ x \ 10^{-22} \ \Delta N_e + 8.5 \ x \ 10^{-18} \ (\Delta N_h)^{0.8}]$  ...(1)

At 
$$\lambda_0$$
 = 1.3  $\mu$ m:   
  $\Delta n = \Delta n_{e +} \Delta n_h = -[6.2 \text{ x } 10^{-22} \text{ } \Delta N_e + 6.0 \text{ x } 10^{-18}$   $(\Delta N_h)^{0.8}]$ 

where:

 $\Delta n_e$   $\;$  change in refractive index resulting from change in free electron carrier concentrations.

 $\Delta n_h$  change in refractive index resulting from change in free hole concentrations.

The active cross section of the phase modulator device has been used in this work is shown in Figure 1. By observing the doping concentrations variations at the waveguide centre (x=4 $\mu$ m, y=8 $\mu$ m), it enable us to work out for the refractive index change for a specific forward bias voltage and therefore the resulting phase shift of the device, in which the relationship can be summarized as:

$$\Delta \theta = 2\pi \Delta n L/\lambda \qquad \dots (3)$$

where L is the length of the modulator. In this work, the length of the modulator is assumed as  $500\mu m$ .

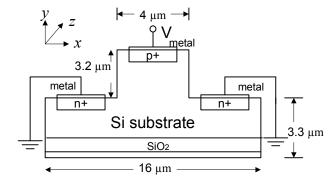


Figure 1: Cross section of the p-i-n phase modulator.

## II. PHASE MODULATOR DESIGN

Recently, several device configurations such as the p-i-n diode structure [6] and, MOS capacitor [10] have been proposed. We studied the micrometer scale silicon modulator based on the p-i-n diode structure to be operated at  $1.55\mu m$  and  $1.3\mu m$  optical wavelength.

The  $P^+$  type region is implanted with  $5x10^{18}$  cm<sup>-3</sup> Boron concentrations while the  $N^+$  type region is the phosphorus implanted region with a concentration of  $5x10^{18}$  cm<sup>-3</sup>. The structures have the background doping concentrations of  $1x10^{14}$ . The depth of the implanted region is about  $1.8~\mu m$  for  $N^+$  region and  $1.6~\mu m$  for  $P^+$  region. The rib height and width of the structure is chosen in order to have a single mode behaviour. The rib structure is designed to have  $3.2~\mu m$  in height and  $4~\mu m$  in width. With the chosen doping concentrations for the structure, the distance of the doped regions to the rib sidewalls turns to be  $1.4~\mu m$ .

The optical power of 1mW is applied to our design of phase modulator and the effect of the refractive index variations for  $1.55\mu m$  and  $1.3\mu m$  optical wavelength is investigated. The important parameters used in the simulations are shown in Table 1.

TABLE 1
SIMULATION PARAMETERS

Si refractive index	3.475
Si background carrier conc. (cm <sup>-3</sup> )	$1x10^{14}$
$\tau_{p (s)}$	2x10 <sup>-6</sup>
$ au_{\mathrm{n}}$ (s)	2x10 <sup>-6</sup>
Temperature (K)	300

# III. RESULTS AND DISCUSSION

In this work, the active region of the phase modulator have been tested under DC operation. The active device will be operated by applying an external electrical signal to the electrodes. The disturbed free carriers will cause distinct changes in the effective refractive index [11].

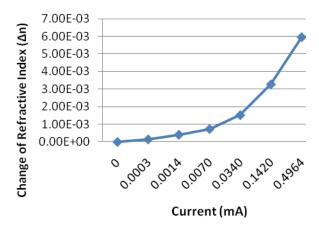


Figure 2. Change of refractive index at wavelength 1.55 µm.

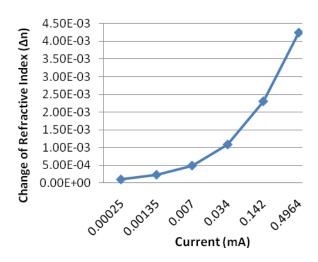


Figure 3. Change of refractive index at wavelength 1.3µm.

Figure 2 and 3 show the relationship between drive current and the refractive index change at 1.55  $\mu m$  and 1.3  $\mu m$  wavelength respectively. The refractive index change increase gradually when the drive current increase. The value of current to get  $\pi$  phase shift is obtained from the graph by referring the equation (3). The results indicate that the current (I $\pi$ ) are 0.035mA for 1.55  $\mu m$  wavelength and 0.066mA for 1.3  $\mu m$  wavelength. This result shows an improvement with respect to [4]. The smaller current value of  $\pi$  phase shift modulation at 1.55  $\mu m$  wavelength shows that the modulator can perform batter when operate at the particular wavelength compared to 1.3  $\mu m$  wavelength.

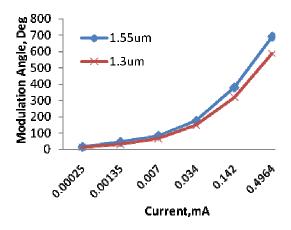


Figure 4. Modulation Angle against drive current

Figure 4 shows the modulation angle against drive current for the modulator at two different wavelengths. Once again, the length of the device is assumed as  $500 \mu m$ . We can see the different current is required to change the phase at a different angle. The change in modulation angle varies nonlinearly with applied current. Less drive current is required for a phase shift at a longer wavelength  $(1.55\mu m)$ .

### IV. CONCLUSION

The p-i-n diode structure has been chosen to simulate the characteristics of the modulator based on the refractive index change and the phase shift by using the effect of the current injection. Hopefully, this can be used as the guidance for the real experiment device. In conclusion, the phase modulator performance will depend on the value of the drive current ( $I\pi$ ) in which have been used to get the  $\pi$  phase shift. The smaller value of  $I\pi$  is required to have the better phase modulator.

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