Tri-band Minkowski Island Patch Antenna with Complementary Split Ring Resonator at the Ground Plane

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Abstract—The Minkoski Island patch with antenna complementary split ring resonator at the ground plane are proposed in this work. At the first stage, the normal square patch antennas mainly designed. Then, the Minkowski patch antenna was designed using 1st iteration technique and 2nd iteration technique. The Minkowski fractal shape slot was embedded in the center of the patch to form a Minkowski Island patch antenna. The next step is to apply the partial ground technique and embed the split ring resonator at the ground plane. This antenna was operating in tri-band frequency that is at 2.400 GHz, 3.500 GHz and 5.200 GHz with a return loss of - 11.868 dB, - 13.554 dB and - 18.112 dB respectively. The gain measured of this antenna is 1.286 dB, 1.410 dB and 3.945 dB.

Keywords—Minkowski Island, split ring resonator, patch antenna, return loss, gain

I. INTRODUCTION

The demands of the multiband antenna that operate in many frequency ranges are highly in the telecommunication sector. Several new techniques combine to enhance the performance of the antenna and to miniaturize the patch antenna size. This is to cater the high demand of high end user nowadays, especially on the Wireless Local Area Network (WLAN) and Worldwide Interoperability for Microwave Access (WiMAX) application [1].

The microstrip patch antenna is the best selection for the researcher because it is a low cost material, lightweight and also easy to fabricate. Many researchers had improved the parameter result with to give better performance and efficiency of the patch antenna design. The parameters that can be considered to improve are return loss, gain, directivity and bandwidth [2-11]. This improvement work can use many types of various shapes of antennas, the additional special structure into the patch antenna or attach of RF component or integrated circuit into the patch antenna.

Fractals geometry shape can be composed of multiple copies of the similarity structure with different size and scale. Minkowski shape is one of the fractal geometry that can be applied in designing the dual band, tri-band or quad-band patch antenna [12-13]. The other example fractal shapes are

Sierpinski [14], Hilbert [15] and also Koch [16]. The Minkowski curve can be characterized by the iteration factor [17], shown in Figure 1. Zero iteration is represented by the normal patch without any scraped out of copper [18]. First iteration show that four rectangular or square shape of copper had been cut from the patch. Second iteration show another eight rectangular had been cut from the patch.

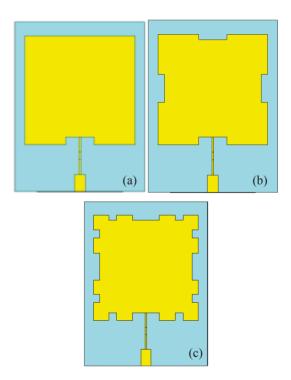


Figure 1. Schematic diagram of Minkowski Island patch antenna with split ring resonator at the ground plane, (a) plan view, (b) ground plane view

Minkowski Island is the improvement technique of the Minkowski fractal of embedding the Minkowski slot in the center of the antenna patch. There is also Minkowski Island that applied in the frequency selective surface [19], fractal monopole antenna [20], reflectarray antenna design [21] and microstrip patch antenna [22].

Split ring resonator (SRR) is an example of a left handed material (LHM) structure beside photonic band gap (PBG), electronic band gap (EBG) and artificial magnetic conductor (AMC). Double negative (DNG) metamaterial is posses negative values of dielectric permittivity and magnetic permeability. The basic structure of split ring resonators is edge couple split ring resonator (EC-SRR). The other researcher had been introduced many types of split ring resonator such as double H-shaped SRR (DH-RR) [23], quadruple P-spiral SRR (QPS-SRR) [24] and others. Different types of SRR structure also can be found in these technical papers [25-30].

This multiband Minkowski Island patch antenna with complementary SRR had been operating in three different bands of frequency that is 2.400 GHz and 5.200 GHz for WLAN while the 3.500 GHz for WiMAX application. The techniques used in these works are Minkowski Island fractal on the patch, partial ground and complementary split ring resonator of the ground plane.

II. ANTENNA DESIGN

The proposed antenna is designed on a FR-4 substrate with dielectric constant of 4.3 and a thickness of 1.6 mm. The thickness of the copper is 0.035 mm. Figure 2 shows the schematic diagram of the Minkowski Island patch antenna with complementary SRR at the ground plane.

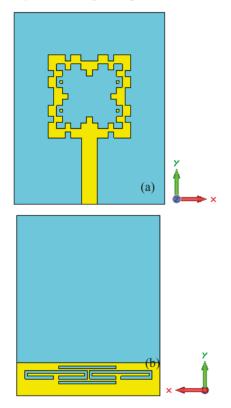


Figure 2. Schematic diagram of Minkowski Island patch antenna with split ring resonator at the ground plane, (a) plan view, (b) ground plane view

This Minkowski Island patch antenna consists four main elements – patch, feed line, partial ground and complementary split ring resonator. The Minkowski patch part dimension is 16.48 mm width x 16.48 mm length, located at the top of the substrate. The feed line is located at the bottom of the patch antenna part with 13.15 mm in length. This patch antenna has the feeding structure of a 50 ohm microstrip line. The feed line is located between the rectangular parasitic patches element the at bottom part of the patch antenna. Table I shows the dimension of the modified Minkowski patch antenna.

TABLE I.	DIMENSION OF THE MINKOWSKI ISLAND PATCH ANTENNA
	WITH SRR AT THE GROUND PLANE

Part	Symbol	Dimension (mm)
Substrate width	Ws	30.00
Substrate length	L_s	38.00
Patch width	W _p	16.48
Patch length	L _p	16.48
Feed width	W_f	3.06
Feed length	L_f	13.15
Ground width	Wg	30.00
Ground length	Lg	7.00

The complementary structure of split ring resonator had been attached at the ground plane of the FR-4substrate. It consists a combination of two main parts – straight line part and rectangular shaped split ring part. The location of this complimentary SRR is at the bottom of the partial ground plane. Figure 3 shows the complementary spiral split ring resonator structure on the ground plane. Table II shows the dimension of the complementary SRR structure. The width of this SRR structure is 13.00 mm width x 0.60 mm length. The gap of the split ring resonator structure is 0.50 mm. The straight line dimension is 12.00 mm width x 0.60 mm length.



Figure 3. Schematic diagram of complementary split ring resonator on the ground plane

Part	Symbol	Dimension (mm)
SRR width	Ws	13.00
SRR length	L_s	0.60
Straight line width	W_L	12.00
Straight line length	L_L	0.60
Gap between two SRR	W_p	0.50

Figure 4 shows the stage of development of Minkowski Island patch antenna with different complementary split ring resonator. Design A is normal partial ground, located at the bottom of the FR-4 substrate. The dimension of this ground plane is 30.00 mm width x 7 mm length x 0.035 mm thick. In Design B, a pair of complementary SRR had been added into the partial ground while Design C consist of complementary SRR with two straight lines at the bottom at top of complementary SRR.

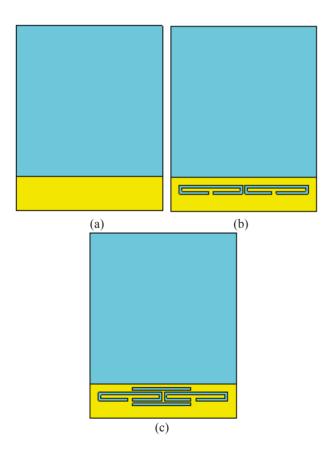


Figure 4. Minkowski Island patch antenna with different design on ground plane, (a) Design A - normal partial ground, (b) Design B - partial ground with complementary SRR, (c) Design C - partial ground with extended complementary SRR

III. RESULT

The parameters that are considered in this work are resonant frequency, return loss, bandwidth, gain and directivity of the antenna. Figure 4 and Table III represent the return loss from 1.000 GHz to 7.000 GHz frequency range of Minkowski Island patch antenna with complementary SRR structure (Design A, Design B and Design C).

The return loss of different three stages of Minkowski Island patch antenna with complementary SRR had been shown in Figure 5. The resonant frequency of Design *A* is at 2.400 GHz with – 14.380 dB of return loss and at 4.900 GHz with - 28.684 dB. The – 10.00 dB bandwidth of this design is 0.396 GHz at the frequency between 2.177 GHz and 2.573 GHz. The other bandwidth is 0.415 GHz at the frequency between 4.676 GHz and 5.091 GHz.

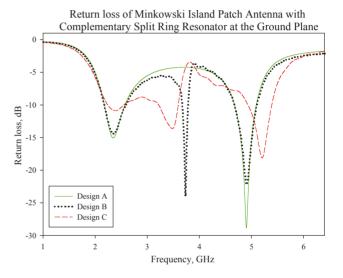


Figure 5. Minkowski Island patch antenna with complementary SRR on the ground (Design *A*, *B* and *C*)

The three resonant frequencies of Design *B* are 2.352 GHz, 3.728 GHz and 4.904 GHz with a respective return loss of - 14.418 dB, -23.863 dB, and – 22.234 dB. By the addition of the SRR, it creates a new resonant frequency at 3.728 GHz compared to the normal partial ground that have only two resonant frequencies.

The optimization of the wanted resonant frequencies had been done in Design C. The three resonant frequencies exist in this design are at 2.400 GHz, 3.500 GHz and 5.200 GHz with -10.868 dB, -13.554 dB and -19.259 dB.

From the simulation, it shows that the second and the third resonant frequency (2.400 GHz and 5.200 GHz) had been optimized by resize (reduce or increase) the Minkowski patch antenna. The Minkowski Island shaped has the potential to reduce the size of the patch. The resonant frequency point of the middle resonant frequency (3.500 GHz) can be controlled by reducing the size of the SRR and also the number of the

SRR in the ground plane of the antenna.

TABLE III. RESONANT FREQUENCY, RETURN LOSS, AND BANDWIDTH OF DIFFERENT DESIGN OF MINKOWSKI ISLAND PATCH ANTENNA WITH SRR AT THE GROUND PLANE

Design	Resonant frequency, <i>f_r</i> (GHz)	Return loss (dB)	Bandwidth (GHz), <i>f</i> ₁ - <i>f</i> ₂ (GHz)
Design A	2.400	- 14.380	0.396, 2.177 - 2.573
	4.900	- 28.684	0.415, 4.676 – 5.091
Design B	2.352	- 14.418	0.417, 2.170 – 2.587
	3.728	- 23.863	0.113, 3.669 - 3.782
	4.904	- 22.234	0.432, 4.669 – 5.101
Design C	2.400	- 10.868	0.309, 2.241 – 2.550
	3.500	- 13.554	0.376, 3.218 – 3.594
	5.200	- 18.112	0.458, 4.931 – 5.389

Figure 6 shown the 3D radiation pattern of Design C at resonant frequency, fr of 2.400 GHz. Figure 7 represents the 2D radiation pattern of the Minkowski Island patch antenna with complementary SRR (Design C). Figure 8 shows the surface current for Minkowski Island patch antenna with complementary SRR (Design A, Design B and Design C) at 2.400 GHz, 3.500 GHz and also at 5.2 GHz of frequency point.

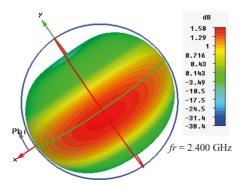


Figure 6. Minkowski Island patch antenna with complementary SRR on the ground (Design A, B and C)

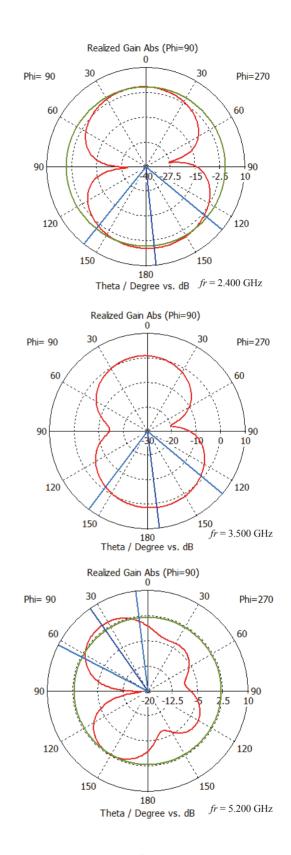


Figure 7. 2D radiation pattern at 90^{0} for Design C (a) 2.4 GHz, (b) 3.5 GHz, (c) 5.2 GHz

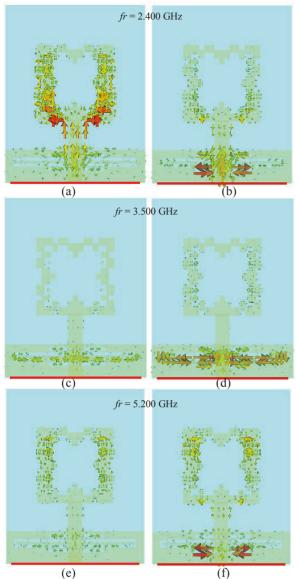


Figure 8. Surface current at various frequencies and degree for Design *C*, (a) 2.400 GHz at 90⁰, (b) 2.400 GHz at 180⁰, (c) 3.500 GHz at 90⁰, (d) 3.500 GHz at 180⁰, (e) 5.200 GHz at 90⁰, (d) 5.200 GHz at 180⁰

From the surface current schematic analysis, it shows that the Minkowski patch antenna are effected the at 2.400 GHz and also at 5.200 GHz of resonant frequency. The changes of the feedline also had been effect on these two frequencies. The split ring resonator structure and the partial ground technique are effected the 3.500 GHz of frequency.

Table IV shows the gain of the Minkowski Island patch antenna with SRR at the ground plane. It shows that the Design *A* had been achieved 1.575 dB at 2.400 GHz and 3.441 dB at 4.900 GHz. The addition of the split ring resonator in Design *B* had been created three bands of frequency with two positive gain result (1.551 dB at 2.352 GHz and 3.419 dB at 4.904 GHz) and a negative gain result at 3.720 GHz with -

0.782 dB. This problem had been cater while the optimization works in Design *C*. In this optimization design it shows that the 3.720 GHz of frequency had been shifted to the 3.500 GHz with positive gain of 1.410 dB. This antenna also achieved 1.286 dB at 2.400 GHz and 3.419 dB at 5.200 GHz.

TABLE IV.	GAIN PERFORMANCE OF THE MINKOWSKI ISLAND PATC	
	ANTENNA WITH SRR AT THE GROUND PLANE	

Design	Resonant frequency, f _r (GHz)	Gain (dB)
Design A	2.400	1.575
	4.900	3.441
Design B	2.352	1.551
	3.720	-0.782
	4.904	3.419
Design C	2.400	1.286
	3.500	1.410
	5.200	3.419

The proposed antenna design can be potentially integrated with RF transmitter and RF receiver [31-32] to form a complete WLAN front-end system.

IV. CONCLUSION

From the simulation, it shows that the Minkowski Island patch antenna with complementary SRR in Design B and Design C had been successfully produced a multiband of resonant frequency. Design C had been improved the gain compared with Design B. The combination of the partial ground technique, split ring resonator technique and Minkowski Island technique had been making this antenna gain improved, miniaturized the patch size and develop the triband of frequency. Thus, the proposed antenna can be a suitable design for the tri-band operation for WLAN and WiMAX application.

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