



## A New Modular Multilevel Inverter Topology of Reduced Components

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**Abstract**— Harmonic content of the yield voltage waveform diminishes as the quantity of yield voltage level increments. The primary focal points are lower Total Harmonic Distortion (THD), less weight on the power switches and higher proficiency. Be that as it may, increment in the gadget number because of expanded voltage levels makes the control strategy complex and subsequently costly. This venture displays a nine level inverter with lessened DC sources which is equipped for acquiring all added substance and subtractive mixes of information DC levels. This topology requires less power changes contrasted with regular multilevel inverter and less entryway drives. The proposed topology is exhibited through a nine-level inverter with a proper balance plot and definite reproduction has been done in MATLAB/Simulink. A correlation is made between proposed topology and the customary multilevel topology on the premise of gadget include, number of levels the yield voltage and THD.

**Index Terms**— Classical topologies, multilevel inverter (MLI), pulsewidth modulation (PWM), reduced component count, total harmonic distortion (THD).

### I. INTRODUCTION

Over the most recent couple of decades, multilevel voltage-source inverters have risen as a practical answer for high-control dc-to-air conditioning change applications [2]. A multilevel inverter (MLI) is a linkage structure of different info dc levels (gotten from dc sources as well as capacitors) and power semiconductor gadgets to blend a staircase waveform. Voltage stresses experienced by the power switches are lower when contrasted with the general working voltage level [3]. Also, the multilevel waveform has a superior consonant profile when contrasted with a two-level waveform acquired from regular inverters. Different focal points of MLIs are decreased dv/dt weight on the heap and plausibility of blame tolerant operation [4]. Specialists are additionally investigating roads to utilize MLIs for low-control applications [5]. The nature of the multilevel waveform is upgraded by expanding the quantity of levels. Nonetheless, it incidentally prompts countless semiconductor gadgets and going with door driver circuits. This expands framework unpredictability and cost and has a

tendency to diminish the framework unwavering quality and proficiency. For a high-determination waveform, in this manner, useful contemplations require decrease in the quantity of switches and entryway driver circuits [6]. The topologies which have been broadly examined and are industrially accessible for multilevel voltage yield are impartial point clasped (NPC), fell H-connect (CHB), and flying capacitor (FC) converters [2], [4], [5]–[7]. Be that as it may, there is a critical increment in the quantity of energy switches, the quantity of switches leading all the while, and the general cost of the framework with the expansion in the quantity of yield levels. Specialists, hence, keep on focusing on decreasing the segment check in multilevel topologies through different methodologies. These methodologies can be characterized into three classifications: topological changes [9]–[12], utilization of deviated sources [14]–[16], and mix of topological changes and unbalanced source setups [17]–[19]. In this venture, another topology is proposed in which interchange dc sources are connected in inverse polarities by means of energy switches. This approach altogether reduces the quantity of energy switches required when contrasted with the traditional topologies. In addition, for symmetric information dc sources, the proposed topology demonstrates closeness with the CHB topology in two ways: 1) It needs different detached info dc voltages; and 2) input dc voltage levels can be joined into every single added substance esteem. In this manner, the topology can be utilized as an utility interface for sustainable power source frameworks where a substantial number of disengaged dc sources are accessible [3], [8], [10]. It can likewise be utilized as a part of medium-voltage drive applications where a stage moving transformer with different auxiliary windings is for the most part utilized (chiefly for the diminishment of line current bending), in this way giving separated dc sources [7]. The proposed topology may likewise be suitable for battery-controlled applications, (for example, electric vehicles and submarine drive).

### II. PROPOSED MULTILEVEL TOPOLOGY

In this segment, the structure of the proposed topology is presented, and its working standard is clarified with

the help of a solitary stage five-level inverter. Expressions for yield voltage, source streams, voltage stresses, and so forth., are moreover introduced.

### A. Summed up Structure

The summed up single-stage structure of the proposed topology is appeared in Fig. 1. It has  $n$  number of secluded info dc sources. The linkage structure is with the end goal that the higher potential terminal of the former source is associated with the lower potential terminal of the succeeding source and the other way around through power switches. Input sources are assigned as  $E_j$  (where  $j = 1$  to  $n$ ). Source current from each source is assigned as  $i_j(t)$ .

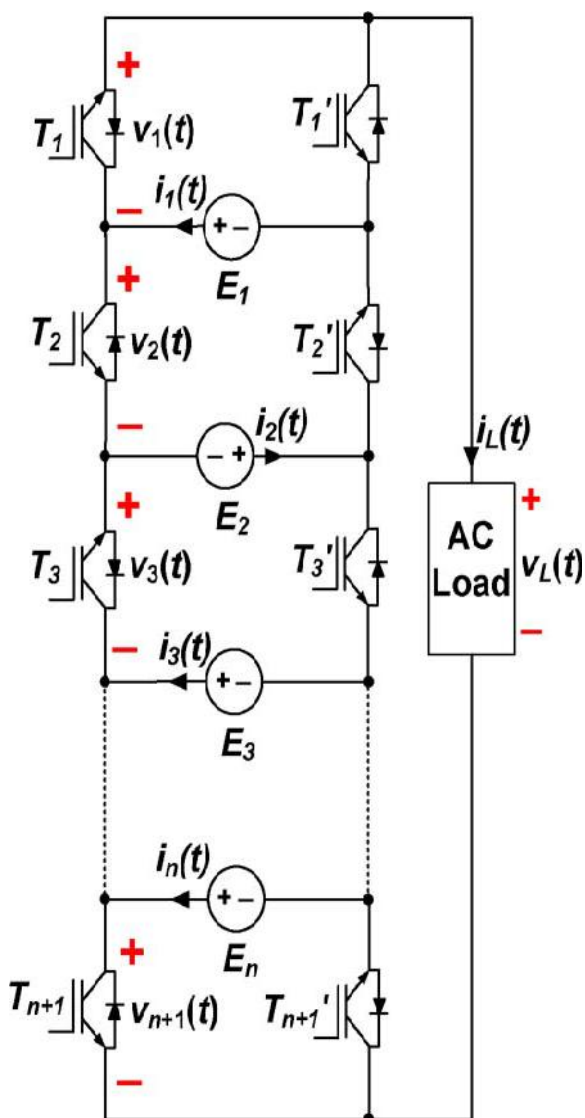


Fig. 1. Generalized single-phase structure of the proposed topology.

Control switches can be actualized utilizing a transistor gadget [e.g., MOSFET and protected entryway bipolar transistor (IGBT)] with an antiparallel diode. In Fig. 1, control switches are

represented with IGBTs with antiparallel diodes, and integral sets are assigned as  $(T_j, T_{j'})$  (where  $j = 1$  to  $n + 1$ ). Different nodal voltages are shown as  $v_j(t)$  (where  $j = 1$  to  $n + 1$ ). Stack voltage and load current are assigned as  $v_L(t)$  and  $i_L(t)$ , separately.

### B. Working Principle

The working standard of the proposed topology is portrayed with the assistance of a solitary stage inverter with two information dc sources  $E_1$  and  $E_2$ , as appeared in Fig. 2. It has three sets of dynamic switches  $(T_j, T_{j'})$  ( $j = 1, 2, 3$ ). Since the components of these sets are reciprocal, there are eight legitimate working modes. These modes are appeared in Fig. 3 and are abridged in Table I alongside nodal voltages and source streams. With the utilization of the working modes appeared in Fig. 3, the heap is provided with five levels, viz.,  $+2V_{dc}$ ,  $+V_{dc}$ , and zero for  $E_1 = E_2 = V_{dc}$ . With such a symmetric source setup, modes 3 and 4 wind up plainly repetitive for yield level  $+V_{dc}$ , while modes 6 and 7 end up noticeably excess for yield level  $-V_{dc}$ . It is imperative to note here that, for all positive voltage levels and one "zero" level (modes 1, 3, 4, and 5), switch  $T_{2'}$  dependably directs, while for all negative voltage levels and another "zero" level (modes 2, 6, 7, and 8), switch  $T_2$  dependably leads. In this way, it is conceivable to work these two switches at the essential recurrence to get five yield levels. To do as such, modes 1, 3 (or 4), and 5 should be utilized for the union of positive levels (counting a "zero" level), and modes 2, 6 (or 7), and 8 should be utilized for the combination of negative voltage levels (counting a "zero" level).

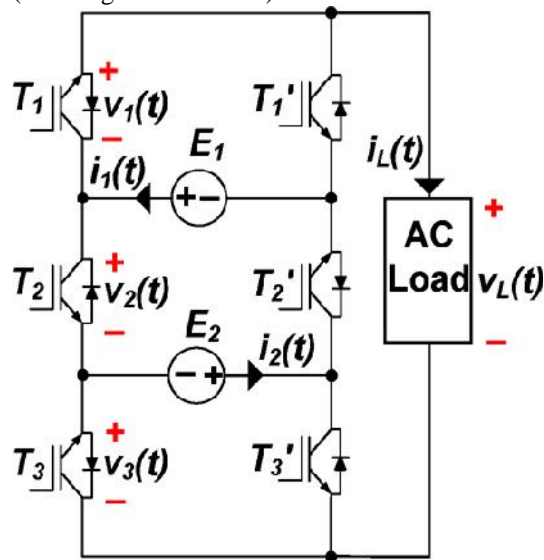


Fig. 2. Single-phase inverter based on the proposed topology with two input sources.

It is likewise vital to specify here that dc source voltages have been thought to be equivalent in this work. By and by, they may contrast (e.g., because of various conditions of charge of batteries or because of shading of a few cells if the sources are originating from a photovoltaic (PV) framework). To represent

this variety, both equipment based arrangements (e.g., utilizing separate dc–dc converters [8]) and control-calculation based arrangements (e.g., battery adjusting technique [19]) can be executed.

In the proposed topology has eight changes and to get any coveted voltage level, three changes should be ON. There are four sets of complimentary switches. Subsequently, three changes (to stay ON) can be browsed four conceivable outcomes in  $4C3 (= 4)$  ways and each switch has two potential outcomes (either ON or OFF). In this manner, add up to number of states feasible for the topology is  $2^4 = 16$ . In this single stage arrangement, the AC load is sustained by nine levels  $(E1 + E2), (E1), (E1 - E2), (E2), (0), (-E2), (E2 - E1), (-E1)$  and  $-(E1 + E2)$ . It is additionally imperative to specify that any unbalance in information DC source extents would not bring about a multilevel waveform with equivalent voltage steps. All the conceivable states, voltage levels and switch positions are outlined in Table, where excess states are assigned as  $(1, 1''), (2, 2''), (5, 5'', 5'''), (5'''), (6, 6'')$  and  $(7, 7'')$ . Excess can be utilized for ideal exchanging of energy semiconductor switches.

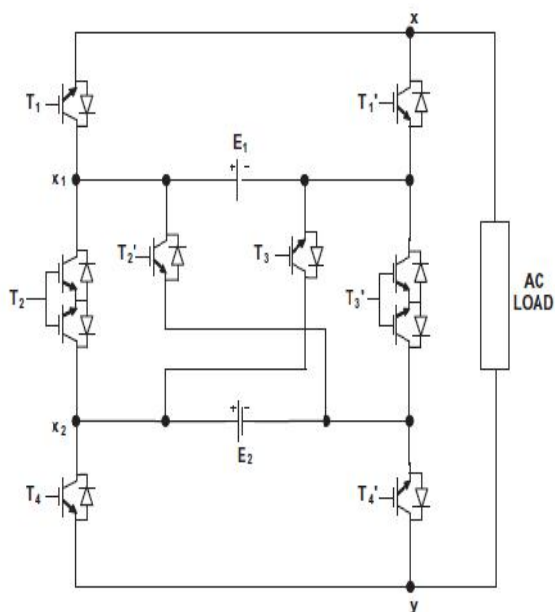


Fig. 3. Single-phase inverter based on the proposed topology with two input sources and eight switch network.

### III. Control switch arrangements:

The proposed inverter can be acknowledged with self commutating power switches like MOSFET's and IGBT's. It is additionally essential to note that the switches at positions  $T_2$  and  $T_3'$  are fundamentally required to be „fully directional switches“ generally their undesirable exchanging will occur. In this manner, at both positions  $T_2$  and  $T_3'$ , completely directional switches having the capacity of blocking voltages in both bearings are to be utilized. A typical

producer mix is having low ON state drop however requires just a single door driver circuit. This switch arrangement has been decided for switches  $T_2$  and  $T_3'$  of the proposed multilevel structure with two DC sources as appeared in Fig3.

### IV. Exchanging SCHEME

High-exchanging recurrence balance strategies like multicarrier PWM and space vector regulation methods have been utilized for MLI adjustment control [22], [23]. On the

other hand, dynamic symphonious end, particular consonant

end, and central recurrence technique are considered as low-exchanging recurrence strategies [24]–[26]. The proposed topology can be regulated with any of these strategies with reasonable adjustment. In the present work, the multicarrier PWM plan is utilized. In a multicarrier PWM plot, bearer signs are contrasted and the reference flag, and the beats acquired are utilized for exchanging of gadgets comparing to individual voltage levels. In the proposed topology, one switch may contribute for blend of more than one level at yield terminals. In addition, as specified in Section II-B, appropriate use of six modes (viz., modes 1, 2, 3, 5, 6, and 8) will prompt central exchanging of  $T_2$  and  $T_3'$

2 which bear voltage worry of  $2V_{dc}$  each when contrasted with the rest of the switches which bear voltage worry of  $V_{dc}$  each. In this manner, in this area, a control plan is portrayed where these modes are used to get a five-level yield. The treatment can, notwithstanding, be stretched out for larger amount inverters.

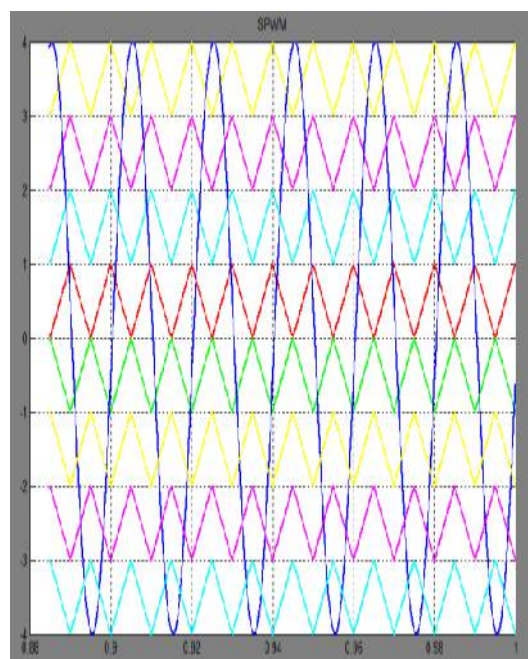


Fig. 4. (a) Reference and carrier waveforms for the proposed scheme for a Nine-level output.

IV.SIMULINK MODELLING

The component requirements of various topologies for a three-phase configuration are given in [1] in terms of the number of voltage levels ( $N$ ) in phase voltage. It can be inferred from the table that the number of components in the proposed structure is lower than those in other topologies, particularly for higher number of voltage levels. For example, implementing a nine-level inverter will entail component counts of 272, 188, and 108 for the NPC, FC, and CHB topologies, respectively, but only 72 in the proposed topology. It can also be observed from [1] that the proposed topology requires significantly lesser number of power switches than the classical topologies.

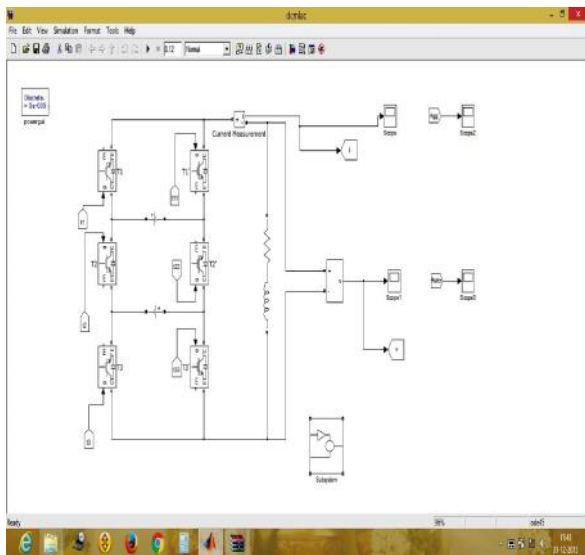


Fig5a:5-level inverter simulink diagram

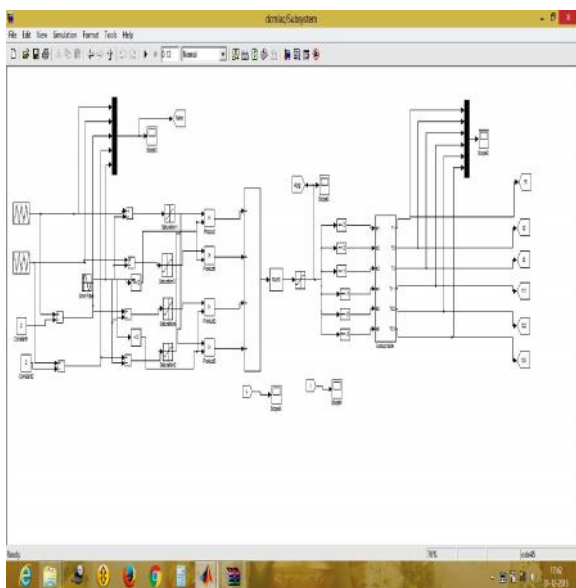


Fig5b:Control block diagram

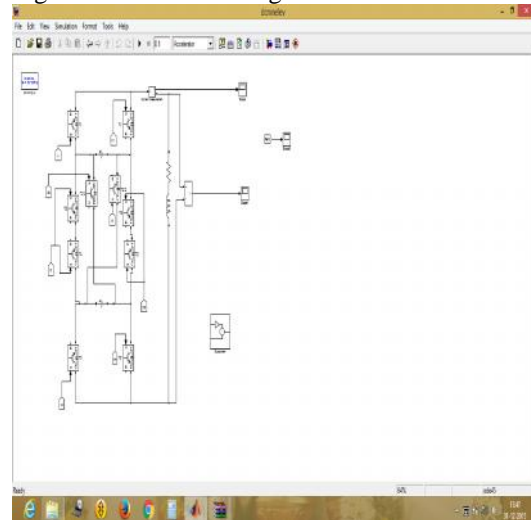


Fig6a:9-level inverter simulink diagram

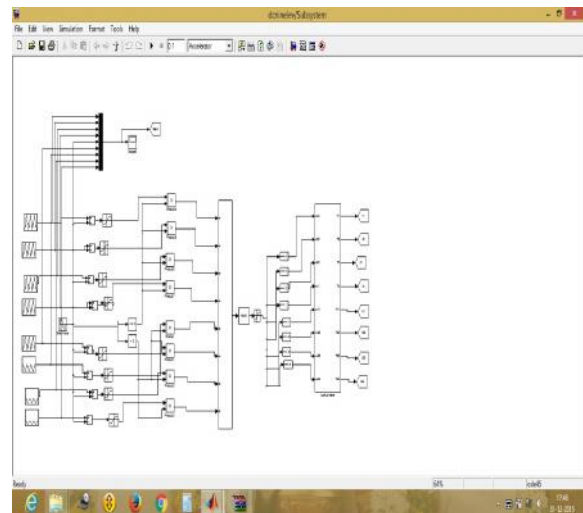
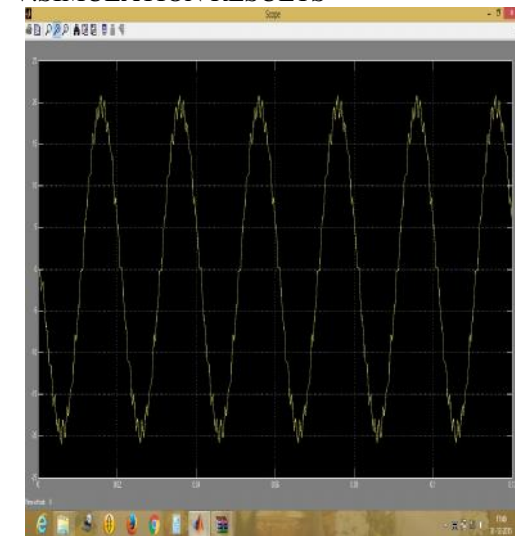
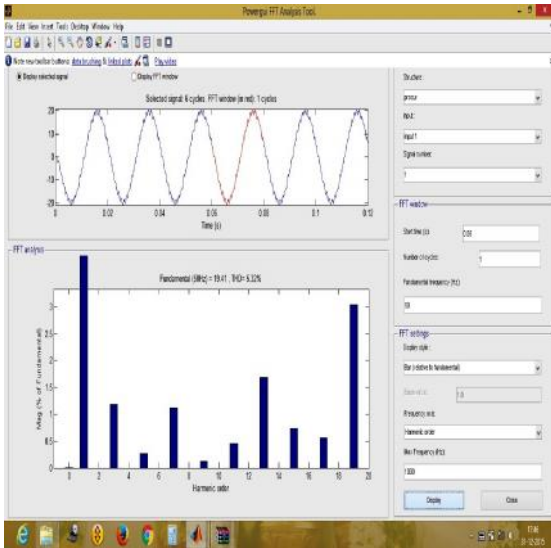


Fig6b:Control block diagram for 9-level inverter

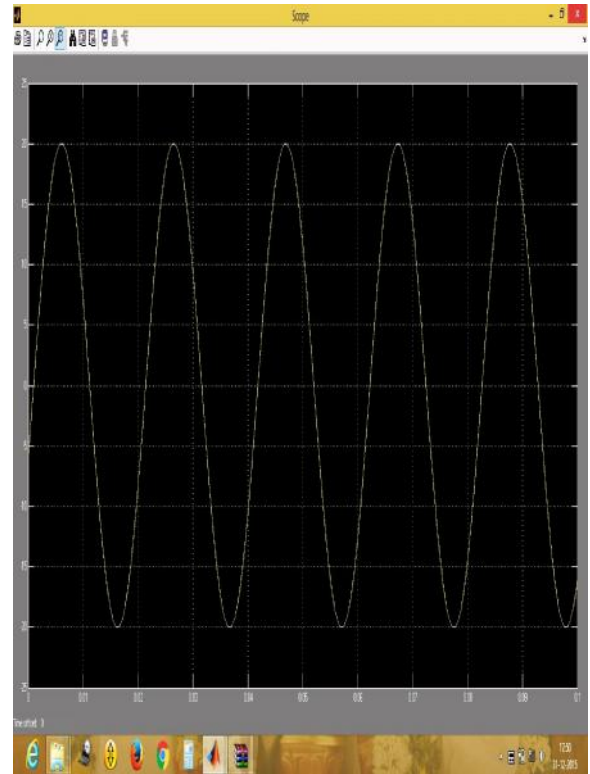
V.SIMULATION RESULTS



Simulation results.7 (a) Load current waveform



7(b) Harmonic spectrum of the load current



Simulation results.9 (a) Load current waveform

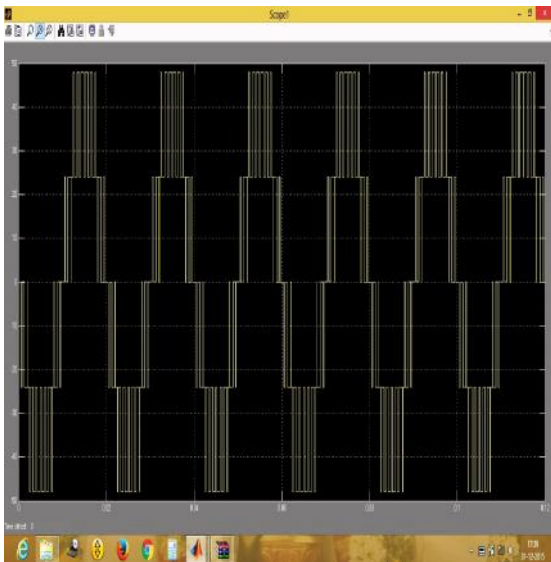
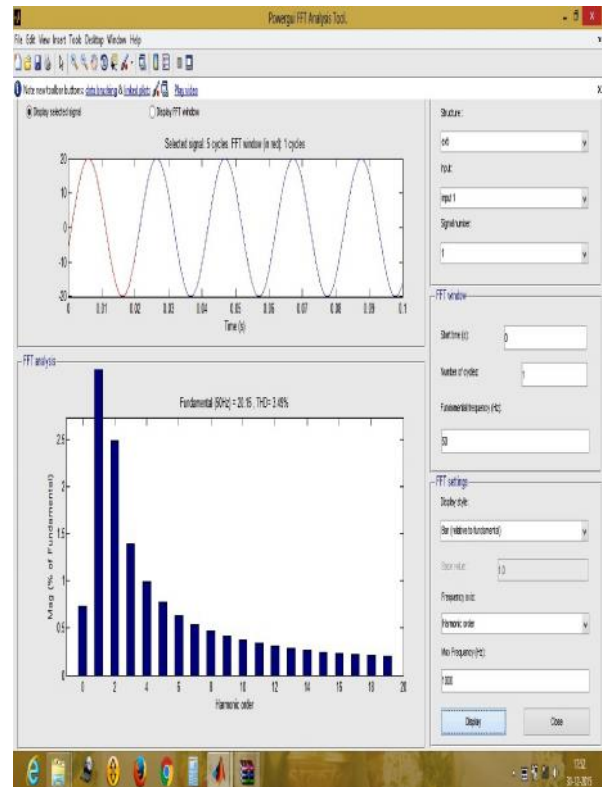
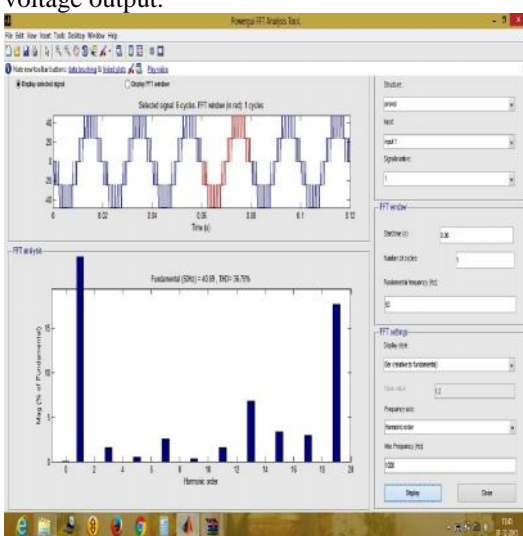


Fig. 8. Simulation results. (a) Five-level voltage output.



9(b) Harmonic spectrum of the load current



8(b) Harmonic spectrum of the load voltage

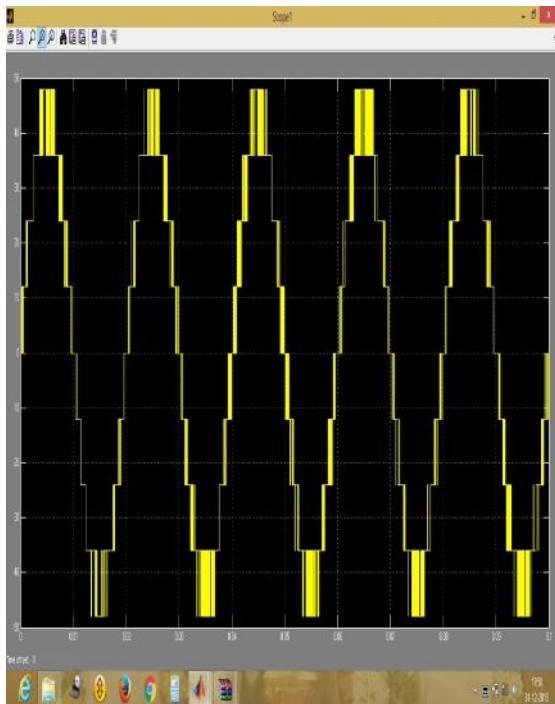
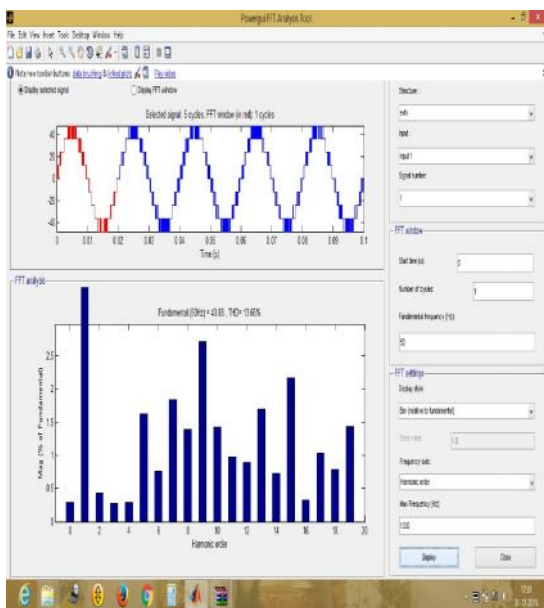


Fig. 10. Simulation results. (a) Nine-level voltage output.



10(b) Harmonic spectrum of the load voltage

## VI. CONCLUSION

As MLIs are gaining interest, efforts are being directed toward reducing the device count for increased number of output levels. A novel topology for MLIs has been proposed in this project to reduce the device count. The working principle of the proposed topology has been explained, and mathematical formulations corresponding to output voltage, source currents, voltage stresses on switches, and power losses have

been developed. Simulation studies performed on a five-level inverter based on the proposed structure have been simulated and a nine level inverter also proposed. By the simulation observation the total harmonic distortion was reduced in nine level when compared to the five level inverter output. Comparison of the proposed topology with conventional topologies reveals that the proposed topology significantly reduces the number of power switches and associated gate driver circuits. Analytical comparisons on the basis of losses and switch cost indicate that the proposed topology is highly competitive. The proposed topology can be effectively employed for applications where isolated dc sources are available. The advantage of the reduction in the device count, however, imposes two limitations: 1) requirement of isolated dc sources as is the case with the CHB topology and 2) curtailed modularity and fault-tolerant capabilities as compared to the CHB topology.

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