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# A high step up Application of Stand-Alone Photovoltaic and Battery Power Systems

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**Abstract**

A three-port dc–dc converter integrating photovoltaic (PV) and battery power for high step-up applications is proposed in this paper. The topology includes five power switches, two coupled inductors, and two active-clamp circuits. The coupled inductors are used to achieve high step-up voltage gain and to reduce the voltage stress of input side switches. Two sets of active-clamp circuits are used to recycle the energy stored in the leakage inductors and to improve the system efficiency. The operation mode does not need to be changed when a transition between charging and discharging occurs. Moreover, tracking maximum power point of the PV source and regulating the output voltage can be operated simultaneously during charging/discharging transitions. As long as the sun irradiation level is not too low, the maximum power point tracking (MPPT) algorithm will be disabled only when the battery charging voltage is too high. Therefore, the control scheme of the proposed converter provides maximum utilization of PV power most of the time. As a result, the proposed converter has merits of high boosting level, reduced number of devices, and simple control strategy.

## I. Introduction

Integrated multiport converters for interfacing severalpower sources and storage devices are widely used in recentyears. Instead of using individual power electronic convertersfor each of the energy sources, multiport converters have the advantagesincluding less components, lower cost, more compactsize, and better dynamic performance. In many cases, at leastone energy storage device should be incorporated. For example,in the electric vehicle application, the regenerative energyoccurs during acceleration or startup. Therefore, it is very importantfor the port connected to the energy storage to allowbidirectional power flow.

Various kinds of topologies have been proposed due to the advantages of multiport converters. The combination strategies for the multiport converter include sharing switches, capacitors, inductors, or magnetic cores [1]. One could select a proper topology by considering many aspects such as cost, reliability, and flexibility depending on the applications. An application of hybrid energy supply using renewable energy sources and storage devices is shown in Fig. 1. The dc microgrid enabled by the solid-state transformer (SST) in the Future Renewable Electric Energy Delivery and Management System (FREEDM System) integrates various distributed renewable energy resources (DRERs) and distributed energy storage devices (DESDs) [2]. For instance, if solar power is selected as the renewable energy source and battery as the storage device, the battery can either supply the load with the solar energy at the same time or store the excess power from the solar panels for backup use. Therefore, the bidirectional power path must be provided for the battery port. The dc–dc converters interfacing the DRERs or DESDs are expected to have relative high voltage conversion ratios since the dc bus of the FREEDM system is 380 V. It is studied that for the dc–dc converters connected to the solar panels, voltage gain extension cells such as coupled inductors, transformers, and switched capacitors are often employed to achieve high voltage conversion ratios [3]. By utilizing the voltage gain extension cells, the extreme duty cycles that exist in typical boost converters can be avoided and the voltage stress on switches can be reduced. Thus, power switches with lower voltage rating and lower turn-on resistance can be chosen forthe converters to reduce conduction losses.

A converter using coupled inductors is relatively better than isolation transformers since the coupled inductors have simpler winding structure and lower conduction loss [4]. However, the leakage inductors of the coupled inductors will consume significant energy for a large winding ratio. In such case, the voltage stress and the loss of the switches will both be increased. A boost converter with

coupled inductor and active-clamp circuit is proposed in [4]. This boost converter can yield a high step-up voltage gain, reduce the voltage stress on switches, and recycle the energy in the leakage inductor.

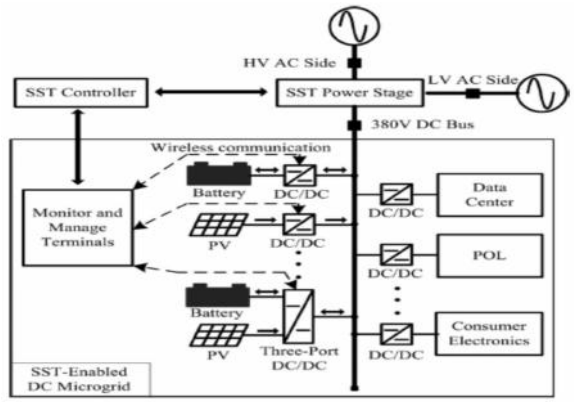



Fig. 1. Part of the FREEDM system diagram showing an SST-enabled DCmicro grid.

Many multiport converter topologies have been presented inthe literature and can be roughly divided into two categories.One is nonisolated type [5]–[13]: the nonisolated convertersare usually derived from the typical buck, boost, or buck–boosttopologies and are more compact in size. The other is isolatedtype [14]–[24]: the isolated converters using bridge topologiesand multiwinding transformers to match wide input voltageranges.

**Principle Of Operation**

This section introduces the topology of proposed nonisolated three-port dc–dc converter, as illustrated in Fig. 2. The converter is composed of two main switches $S1$ and $S2$ for the battery and PV port. Synchronous switch $S3$ is driven complementarily to $S1$ such that bidirectional power flow for the battery port can be achieved. Two coupled inductors with winding ratios $n1$ and $n2$ are used as voltage gain extension cells. Two sets of activeclamp circuits formed by $S4$, $Lk1$, $Cc1$ and $S5$, $Lk2$, $Cc2$ are used to recycle the leakage energy. $Lk1$ and $Lk2$ are both composed of a small leakage inductor from the coupled inductor and an external leakage inductor. Two independent control variables, duty cycles $d1$ and $d2$, allow the control over two ports of the converter, while the third port is for the power balance. The fixed-frequency driving signals of the auxiliary switches $S3$ and $S4$ are complementary to primary switch $S1$. Again, $S3$ provides a bidirectional path for the battery port. Similarly, $S5$ is driven in a complementary manner to $S2$. An 180◦ phase shift is applied between the driving signals of $S1$ and $S2$. There are four operation periods based on the available solar power. First, the sun is in the eclipse stage and the solar irradiation is either unavailable or very low. This operation period is defined as period 1, and the battery will serve as the main power source. As the sun starts to shine and the initial solar irradiation is enough for supplying part of the load demand, the operation period is changed to period 2. The load is supplied by both solar and battery power in this period. For period 3, the increasing isolation makes the solar power larger than the load demand. The battery will preserve extra solar power for backup use. During period 4, the charging voltage of the battery reaches the preset level and should be limited to prevent overcharging. According to the solar irradiation and the load demand, the proposed three-port converter can be operated under two modes. In the battery balance mode (mode 1), maximum power point tracking (MPPT) is always operated for the PV port to draw maximum power from the solar panels. The battery port will maintain the power balance by storing the unconsumed solar power during light-load condition or providing the power deficit during heavy-load condition.

**Simulation Results**

In Fig. 2, the sun radiation is in period 1. For the first 40 s, there is very little sunlight, so the MPPT is performed. However, once the level is too low or not available, MPPT is then disabled and the battery will become the only power source to supply the load. In Fig. 3(a) and (b), the sun irradiation is in period 2. The solar port is operated under MPPT and the battery port is discharged to supply part of the load. As the irradiation increases, the PV port will generate more power than the battery port. The increasing sun irradiation reaches period 3 in Fig. 4. The power generated from the PV port is now larger than the load demand, so the battery port should be charged to store additional power. Although the batteries are charged, the charging voltage is not high enough to trigger the BVC loop. Thus, the solar panels stillwork under MPPT. As shown in Fig. 14, the maximum charging voltage for the batteries is reached in period 4.

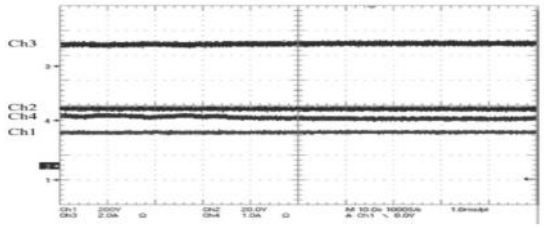
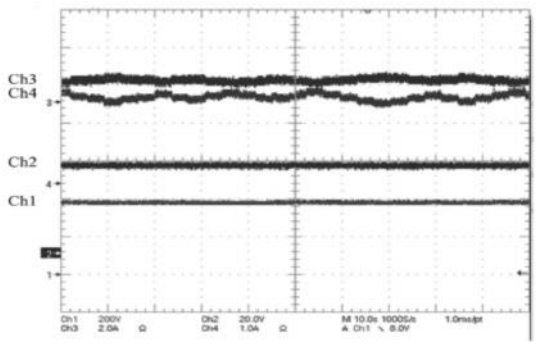
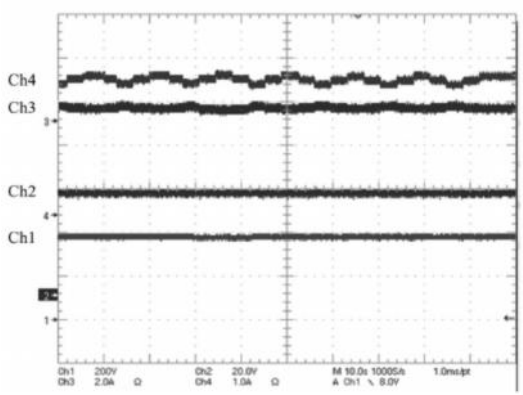



Fig. 2. Measured waveforms of mode operation in period 1 ($R$ = 3030 Ω,Ch1:$Vo$, Ch2: $Vb$, Ch3: $Ib$, Ch4: $I$pv ).




(a)




(b)

Fig. 3.Measured waveforms of mode operation in period 2. (a) Lower solar irradiation level. (b) Higher solar irradiation level (*R* = 1204 Ω, Ch1:*Vo*, Ch2: *Vb*, Ch3: *Ib*, Ch4: *I*pv ).

The BVC loop is then active to regulate the charging voltage and the MPPT is disabled.

At the beginning of Fig. 15, the load demand is set as 120 W (*R* = 1204 Ω), the solar port is generating its maximum power and the deficit is provided by the battery port. At the time $t \approx 32$ s, load demand is decreased to 72 W (R = 2000 Ω), which is lower than the power generated from the solar panels. The maximum solar power is still drawn from the panel after the load change and the batteries are charged by the additional solar power. It is observed that the current ripple of the battery is larger at the boundary of charging and discharging operations. When $t \approx 58$ s, the load is switched back to 120W, so the batteries are discharged again. It can be observed that the solar port works under MPPT as long as the battery voltage is not too high. The transitions of the battery between charging and discharging are smooth and the operation mode does not need to be changed.

It should be noted that even during the load change, MPPT is achieved and the output voltage is well regulated. This is one of the important features of three-port converters since MPPT and load regulation could not be maintained simultaneously for typical two-port converters [22].

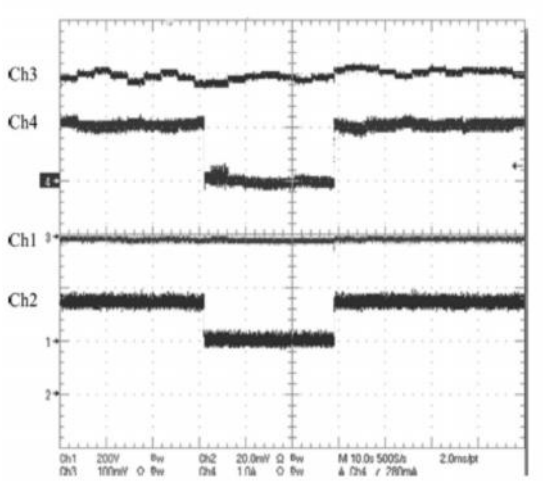



Fig. 4. Measured waveforms of load step response under SVC (Ch1:*Vo*,Ch2: *Io* , Ch3: *I*pv, Ch4: *Ib*).

Fig. 5(a) shows mode transition from SVC (mode 1: MPPT, *R* = 900 Ω) to BVC (mode 2: Battery voltage regulation, *R* = 3600 Ω) when the maximum charging voltage is reached. The PV port is operated under MPPT at the beginning to generate maximum solar power and the battery is discharged to share part of the load demand. It is noted that in mode 1, sometimes the solar power is slightly larger than the load demand; therefore, the batteries are temporally charged. The battery voltage in this case is clearly higher than discharging situation. However, the charging voltage during this short period is not high enough, so the converter is still operated in mode 1. When a load change (from 80% to 20%) happened at $t \approx 50$ s, the battery is suddenly charged with a large current and the battery voltage is then increased dramatically. When the charging voltage is higher than the maximum setting, the operation mode is switched to mode 2 immediately to regulate the battery voltage and prevent overcharging.

It can be seen that in mode 2, the solar panel is no longer operated around the maximum power point but the right side of it. Fig. 5(b) shows the transition from mode 2 to mode 1 when the load is suddenly increased. The SVC will take over the control on the PV port since the maximum setting of the battery voltage could not be met. Similarly, sometimes the batteries could be slightly charged according to the intensity of solar irradiation. Again, no matter what mode is operated for the PV port, the output voltage will be always regulated at 380 V.

**Conclusion And Future Work**

A high step-up three-port DC–DC converter for stand-alonepower systems is proposed to integrate solar and battery power.In the proposed topology, two coupled inductors are employedas voltage gain extension cells for high voltage output applications.

Discussion fromcontrol viewpoints including moving the effect of RHP-zerosto particular output, limitations on sensitivity of the system,tradeoffs in the feedback controller design, and implementationof an improved decoupling method should be presented in our future work.

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