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Trend-Surface Analysis of the Trunk Lake Granitic Pluton, Maine

Bruce Ramsey

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TREND-SURFACE ANALYSIS
of the
TUNK LAKE GRANITIC PLUTON, MAINE

by
Bruce Ramsey

A Thesis
Submitted to the Faculty
of the
University of North Dakota
in partial fulfillment of the requirements
for the degree of
Bachelor of Science in Geology

Grand Forks, North Dakota

May 1972

This thesis submitted by Bruce Ramsey in partial fulfillment of the requirements for the degree of Bachelor of Science in Geology from the University of North Dakota is hereby approved by the Faculty Advisor under whom the work has been done.

Harold Kerner
(advisor)

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ABSTRACT

A trend-surface modal analysis of the Tunk Lake granitic pluton was performed using a program for the IBM 36/40 computer (Appendix 1) by Heiner and Geller (MIRL Report No. 9) and data from Karner (1968). The quartz, total mafics, oligoclase, perthite, and albite in perthite percentages were analysed.

All the trends show a southwest-northeast alignment, with the perthite, albite-in-perthite, and total mafic values increasing towards the margin of the pluton and quartz and oligoclase values decreasing outward to the margin. There is an area in the northwest part of the pluton which is an area of high values for total mafics, perthite, and albite-in-perthite, and an area of low values for quartz and oligoclase.

For the sixth-degree surfaces, the total mafics accounted for 49 percent of the total variation, quartz for 40 percent, oligoclase for 71 percent, perthite for 67 percent, and albite-in-perthite for 75 percent. The difference in the percentages points to two different types of trend. The quartz and total mafics trends are not as distinct as the oligoclase, perthite, and albite in perthite trends. This is a reflection of different processes involved in the formation of the pluton resulting in different trends. Water vapor pressure and cooling temperature govern the trends of oligoclase, perthite, and albite-in-perthite and magma differentiation and movement govern the trends of quartz and total mafics.

INTRODUCTION

This study was done in fulfillment of the senior thesis requirement for the University of North Dakota Bachelor of Science in Geology Degree. There are two objectives of this study, (1) to adapt and catalog for future use a trend-surface program that will run on the University's 360/40 computer, (2) to aid in interpretation of the geologic history of the Tunk Lake granitic pluton by an analysis of the variation of modal quartz, total mafics, perthite, albite in perthite, and oligoclase described by Karner (1968).

METHODS

The systematic change of some variate noted on a contour map is referred to as a trend. Trends of a certain variate are common characteristics of rocks exposed in outcrop belts or over a map area. Establishment of mineralogic, chemical, sedimentologic, or geophysical trends is important in interpreting geologic history and can have economic significance in that they can provide information in exploration for ore bodies, oil and gas accumulation and other natural resources.

The trend of some variate of a large number of data points can be assessed by drawing contour lines of equal value. The equal-value line represents the dependent variate, z , plotted on an x, y , grid which represents the independent, geographic variables. This method can be very subjective, especially if the census of data points is incomplete or if z shows much local variation or "noise".

Through use of a statistical method for determining the trend and plotting the contour lines one can extract the most information possible from the data while eliminating the subjective error encountered by drawing contour lines. Polynomial functions can be computed which give useful approximations of the trend. The method of computation involves the principle of "least squares" (Krumbein and Graybill 1965). Data points are located with respect to rectangular x, y, coordinates. Ordinates for the dependent variable z are constructed for each location. With respect to these ordinates, the three dimensional linear surface, $z = a + bx + cy$, is computed which minimizes the sum of squares of the residual values ($S = \sum_{i=1}^n (z_{i\text{observed}} - z_{i\text{calculated}})^2$). By computing equations of higher degrees a surface of better "fit" or a reduction in the sum of squares is obtained.

Digital computers must be used for computation of the higher degree equations. There are several programs which will perform the necessary computations and plot the contours and residual ($z_{i\text{observed}} - z_{i\text{calculated}}$). The program used in the Tunk Lake analysis was adapted from Good's (1964) program for the IBM 1620 by Heiner and Geller (MIRL Report No. 9) for the IBM 360/40. The only change made was the elimination of the Alpha Subroutine which performs logical IF operations. The University's compiler is capable of supporting logical IF statements, eliminating the necessity for the Alpha Subroutine.

This program will evaluate, for a maximum of five hundred data points, the first- through sixth-degree equations; list the x, y, and z values and their corresponding z calculated and res-

idual values; compute the error measurements; and plot the z calculated and residual values for each equation. The error measures consist of:

Total variation, $V = \sum_{i=1}^n (z_i - \bar{z})^2$ where i is the i th data point and $\bar{z} = \frac{1}{n} \sum z_i$, and n = number of data points.

Variation not explained by the surface, $S = \sum_{i=1}^n (z_{i\text{observed}} - z_{i\text{calculated}})^2$

Variation explained by the surface, $E = V - S$

The coefficient of determination, $T = \frac{E}{V}$

The coefficient of correlation, $L = T^{\frac{1}{2}}$

Standard deviation, $D = \left(\frac{S}{N}\right)^{\frac{1}{2}}$

The percentage of the total variation accounted for by a certain surface is equal to the coefficient of determination multiplied by one hundred.

Modal data for the Tunk Lake pluton rocks are taken from Karner (1968), who used one hundred and thirty-two irregularly spaced data points and contoured the quartz, total mafics, perthite, albite-in-perthite, and oligoclase percentages (Fig. 1). This trend-surface analysis uses the same modal variates. The first-through sixth-degree surfaces were calculated and contoured for each, their corresponding residuals were plotted and their error measures were computed.

RESULTS

The lower degree residual plots accentuate the anomalous areas, but their corresponding contour surfaces are poor. Since the higher degree surfaces account for a larger percentage of total variation and reduce the residual values, resulting in

a more "accurate" contoured surface, these areas don't show as distinctly or at all on the higher degree residual plots.

A point is reached in the calculation of higher degree equations where a large percentage of the total variation is already accounted for, and the calculation of higher degree equations results in a small increase in this percentage. But with the higher degree equations, the contour surfaces become more complex and harder to read and it is dubious whether or not the calculation of progressively higher degree surfaces, after a large percentage of total variation has been accounted for, is meaningful.

With the above in mind, the author included (1) the first-degree contour surface and residual plots and (2) the sixth-degree contour surface and residual plot or (3) the fourth-degree surface and residual plot and the sixth-degree surface, in hopes of showing the trend and anomalous areas clearly.

TOTAL MAFICS

The contoured first-degree surface reveals a total mafic trend oriented southwest-northeast and increasing in value towards the northwest (Fig. 2a). Its corresponding residual plot shows a strong positive area in the northwest and a less distinct positive area towards the east edge of the pluton (Fig. 2b). The second-through sixth-degree contour surfaces show an increasing complexity of the trend, with the sixth-degree surface (Fig. 2c), accounting for 49 percent of the total variation (Table 1). Each surface shows a northeast orientation of the trend with values increasing outward from the center of the pluton, and an area of high values in the northwest part of the pluton. The contour of

the sixth-degree surface closely resembles Karner's (1968) contour of the total mafics percentage (Fig. 1), and its residual plot shows no distinct areas of positive or negative values.

QUARTZ

The contoured first-degree surface for quartz shows the same southwest-northeast orientation of the trend as total mafics, and also increases in value towards the northwest (Fig. 3a). The first degree residual plot shows two general positive areas, one in the center and one towards the southern part of the pluton (Fig. 3b).

As with total mafics, the second- through sixth-degree surfaces show an increasing complexity of the trend, with the progressively higher degree surfaces accounting for a progressively larger percentage of the total variation. The sixth degree surface accounts for 40 percent of the total variation (Table 1). The trend is oriented northwest; the values decrease outward and there is an area of low values in the northwest corner of the pluton (Fig. 3c). The sixth-degree residual plot shows no areas of positive or negative values (Fig. 3d).

OLIGOCLASE

The first-degree linear surface is limited geometrically to an "average" which minimizes the sum of squares. Consequently, if there is a distinct trend, the residual plot of the first-degree surface will show distinct positive and negative areas. For oligoclase, the contoured first-degree surface is an "average" of the oligoclase values (Fig. 4c), and its residual plot shows marginal negative values and positive values in the center (Fig.

4b). The fourth-degree surface (Fig. 4c) shows the trend (oriented northeast with decreasing values towards the margins of the pluton and an area of low values in the northwest) more clearly than the sixth-degree surface (Fig. 4e). From Table 1, the coefficient of determination for the fourth-degree surface is .62 and for the sixth-degree surface is .71. Both account for a high percentage of the total variation, but the sixth-degree is more complex and bears a closer resemblance to Karner's (1968) contour map. The fourth-degree residual plot shows no distinct positive or negative areas. (Fig. 4d).

PERTHITE

The contoured first-degree surface of the perthite values is also an average of sorts (Fig. 5a), and its residual plot also shows distinct positive and negative areas (Fig. 5b). The positive area lies towards the outside of the pluton and the negative values lie in the center. The second- through sixth-degree surfaces show a northeast trend with values increasing toward the margin of the pluton, and an area of high values in the northwest part of the pluton. Again, the higher degree surfaces become increasingly complex. The fourth-degree surface (Fig. 5c) shows the trend most clearly and accounts for 62 percent of the variability. The sixth-degree surface accounts for 67 percent of the variability, is more complex than the fourth, but bears a closer resemblance to Karner's (1968) contour of the perthite values. (Fig. 5e). The fourth-degree residual plot shows no distinct areas of positive or negative values (Fig. 5d).

ALBITE-IN-PERTHITE

The albite-in-perthite contoured surfaces closely resemble those of the perthite. The first-degree contour surface (Fig. 6a), is an "average" of the albite-in-perthite values, and its residual plot show the same positive and negative areas as the perthite residual plot (Fig. 6b). The fourth-degree surface accounts for 70 percent of the total variation; the sixth-degree surface accounts for 75 percent. The second-through sixth-degree surfaces all show the northeast orientation of the trend, values increasing outward, and an area of high positive values in the northwest part of the pluton. Again, the fourth-degree contour surface (Fig. 6c) is clearer than the fifth or sixth, but the sixth more closely resembles Karner's (1968) map of albite-in-perthite. The higher degree residual plots show no distinct positive or negative areas. The fourth is included (Fig. 6d) for comparison with the first.

INTERPRETATION

All of the trends are orientated in a southwest-northeast direction and show an anomalous area in the northwest corner of the pluton. This is an area of high values for total mafics, perthite, and albite-in-perthite and of low values for quartz and oligoclase. The total mafics, perthite, and albite-in-perthite values increase from the center of the pluton outwards, and the quartz and oligoclase values decrease towards the margins.

All this agrees very well with Karner's study, and for further interpretation the author will refer you to his work. The most significant result of the study was the seemingly low coefficient

of determination for quartz and total mafics compared to those of oligoclase, perthite, and albite-in-perthite. This is a reflection of the different processes involved in the formation of the pluton. There were likely several processes occurring during the cooling of the pluton which could affect the mineralogic trends. Those which affect the oligoclase, perthite, and albite-in-perthite trends (cooling temperatures and water vapor pressure) produced more distinct trends than those which affect quartz and total mafics trends (magma differentiation and movement).

DISCUSSION

The trend-surface analysis of any variate with respect to geographical coordinates will yield quick and accurate results from a minimum of data points and establishment of the trend of the variate will yield "target" areas for closer study. Establishment of the trend of some variate — lithologic, sedimentary, chemical, mineralogic, geochemical or geophysical — is important in interpreting the geologic history of some rock body. They also have economic significance in providing information which will further aid in exploration for ore bodies, oil and gas accumulation, and other natural resources.

ACKNOWLEDGMENTS

The author would like to express his thanks to Dr. Karner for suggesting this study, for help and advice given throughout the study, and for the use of his data, and would like to thank Dr. Ting for help given in running the computer program.

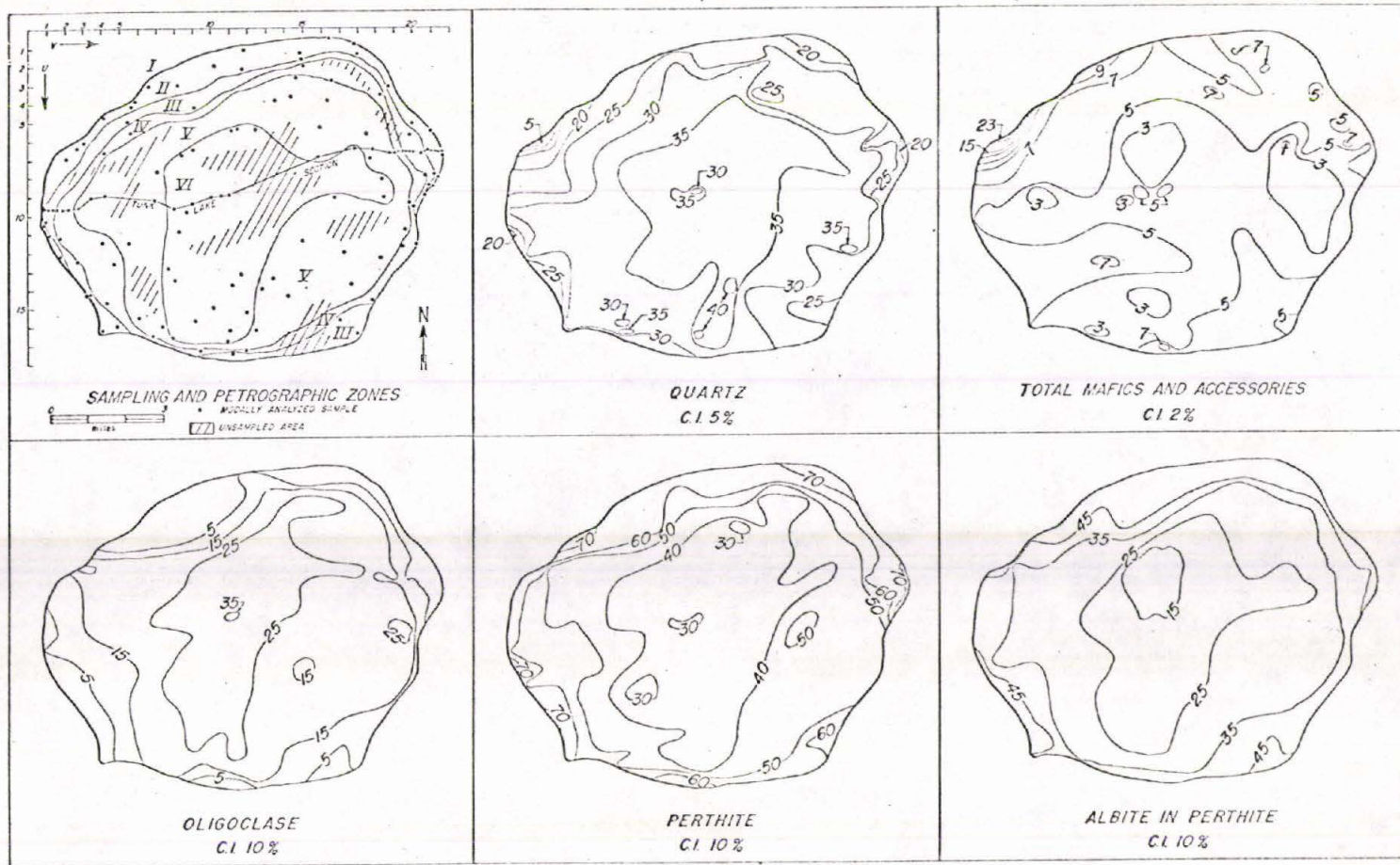


Figure 2. Modal variation in the Tunk Lake granite pluton. Mineral data are in volume percent (Karnier 1968).

Table 1. Error measures for the first through sixth-degree surfaces for total mafics, quartz, oligoclase, perthite, and albite in perthite.

<u>Total Mafics</u>						
Surface	1	2	3	4	5	6
D	2.53	2.44	2.35	2.26	2.12	1.95
T	.141	.200	.259	.314	.399	.490
L	.375	.445	.509	.560	.632	.700
<u>Quartz</u>						
Surface	1	2	3	4	5	6
D	6.09	5.65	5.61	5.49	5.34	5.01
T	.122	.243	.252	.285	.325	.404
L	.347	.493	.503	.534	.570	.636
<u>Oligoclase</u>						
Surface	1	2	3	4	5	6
D	9.98	7.31	6.99	6.21	6.04	5.43
T	.006	.466	.512	.615	.635	.705
L	.077	.683	.716	.784	.797	.840
<u>Perthite</u>						
Surface	1	2	3	4	5	6
D	12.14	8.57	8.29	7.62	7.46	7.03
T	.027	.515	.547	.619	.633	.674
L	.169	.718	.740	.786	.796	.821
<u>Albite in perthite</u>						
Surface	1	2	3	4	5	6
D	9.57	6.24	5.88	5.33	5.12	4.84
T	.028	.586	.633	.698	.721	.751
L	.169	.766	.800	.836	.849	.867

LAKE TREND-SURFACE ANALYSIS PROGRAMME

ADJUSTED FIRST-DEGREE SURFACE

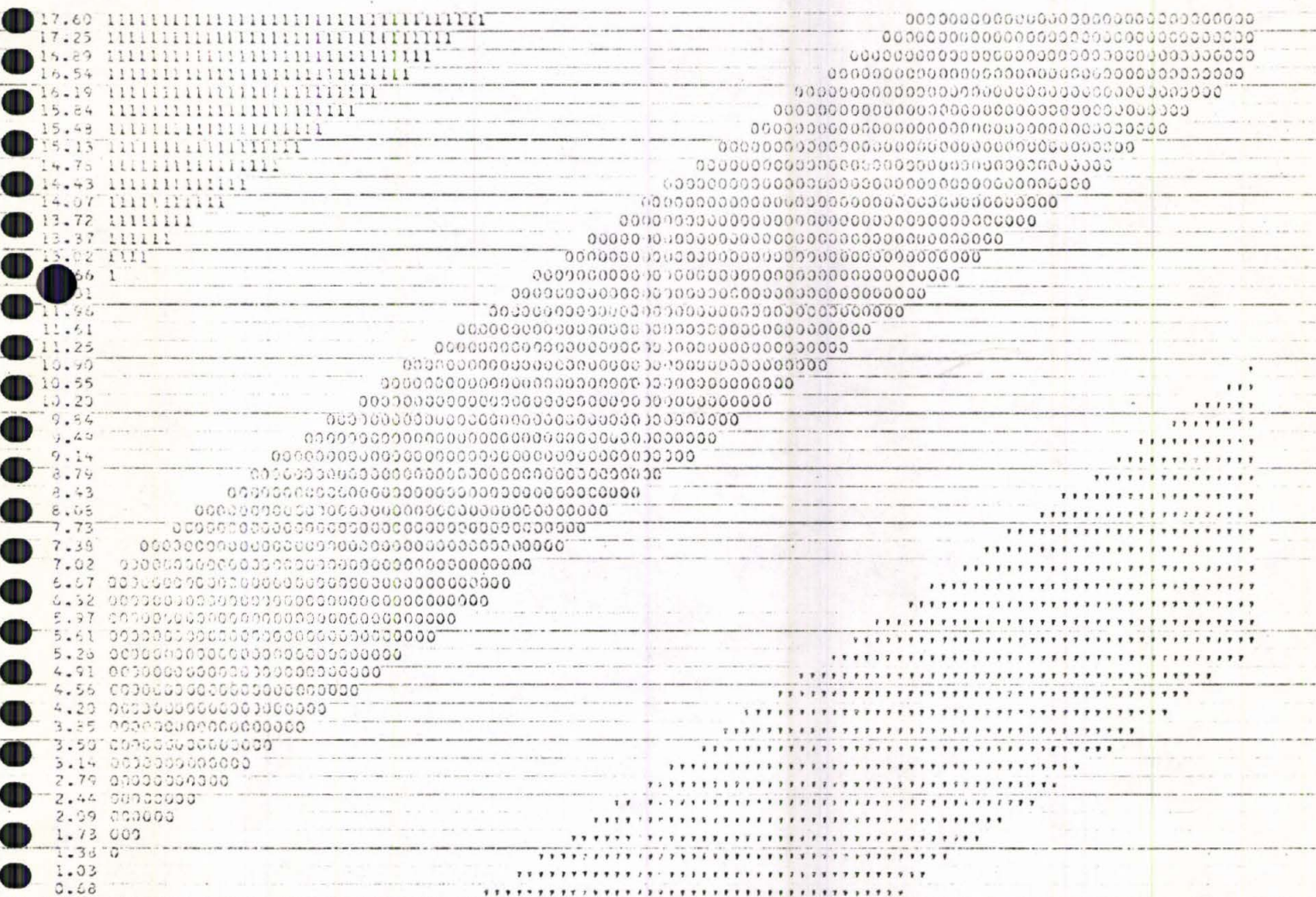
ROUTING LIMITS
MINIMUM X = 22.791988 MINIMUM Y = 0.800000
MAXIMUM X = 17.599991 MINIMUM Y = 0.700000

X-SCALE IS HORIZONTAL
SCALE VALUE = 0.60 * 0.2115 X (SCALE VALUE)

Y-SCALE IS VERTICAL

CONTOUR INTERVAL = 1.00
REFERENCE CONTOUR (.....) = 3.00

0123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789



0123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789

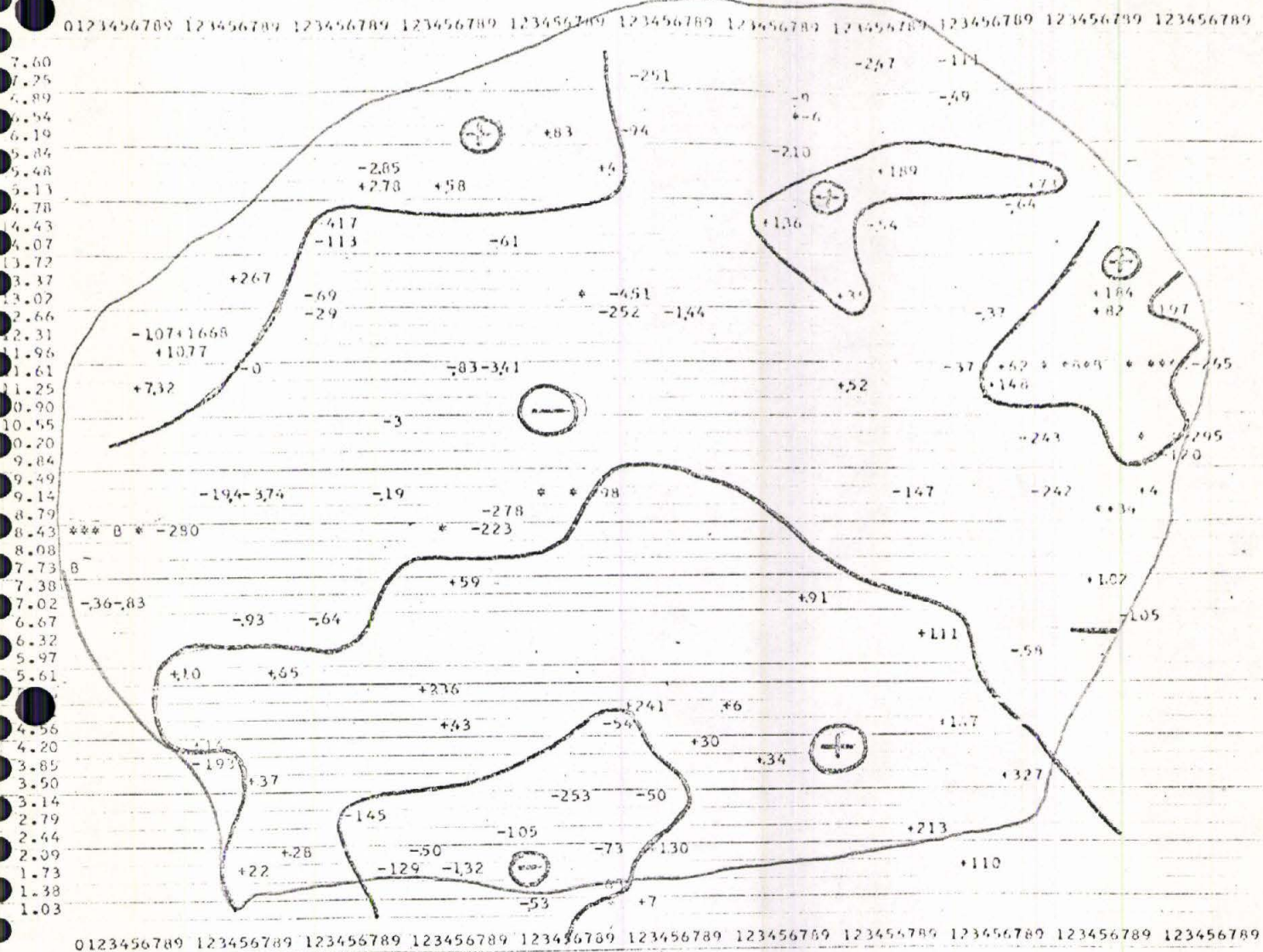
Figure 2a. Contour of first-degree surface for total mafics (see appendix, p. 54 for instructions on how to read the contours.)

MAX X = 22.000000 MINIMUM X = 0.000000
 MIN Y = 17.999991 MINIMUM Y = 0.000000

ALL VALUES HAVE BEEN MULTIPLIED BY A FACTOR OF 10 TO THE 2 POWER

ALL IS HORIZONTAL
 01 = 0.00 + 0.0115 X (SCALE VALUE)

ALL IS VERTICAL



PRINT VALUES

447	B -163
-218	* 53
19	-106
231	B -183
-105	21
155	
46	* 360
69	
331	
219	
242	
264	
75	
-180	
-110	
-200	
213	
96	
118	
-317	
-139	
-96	
-20	
17	

Figure 2b. Plot of first-degree residuals (see appendix, p. 55-56, for instructions on how to read residual plots.)

ANK LAKE TREND-SURFACE ANALYSIS PROGRAMME

CONToured SIXTH-DEGREE SURFACE

PLOTTING LIMITS

MAXIMUM X = 22.797988 MINIMUM X = 0.800000
 MAXIMUM Y = 17.593991 MINIMUM Y = 0.700000

X-SCALE IS HORIZONTAL

VALUE = 0.50 + 0.211 * X (SCALE VALUE)

Y-SCALE IS VERTICAL

CONTOUR INTERVAL = 1.00
 REFERENCE CONTOUR (.....) = 3.00

0123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789



0123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789

Figure 2c. Contour of sixth-degree surface for total mafics.

ORDER OF SIXTH DEGREE RESIDUALS

SCALING LIMITS

AVIUM X = 27.99999 MINIMUM X = 0.800000
 MAXIMUM Y = 17.999991 MINIMUM Y = 0.700000

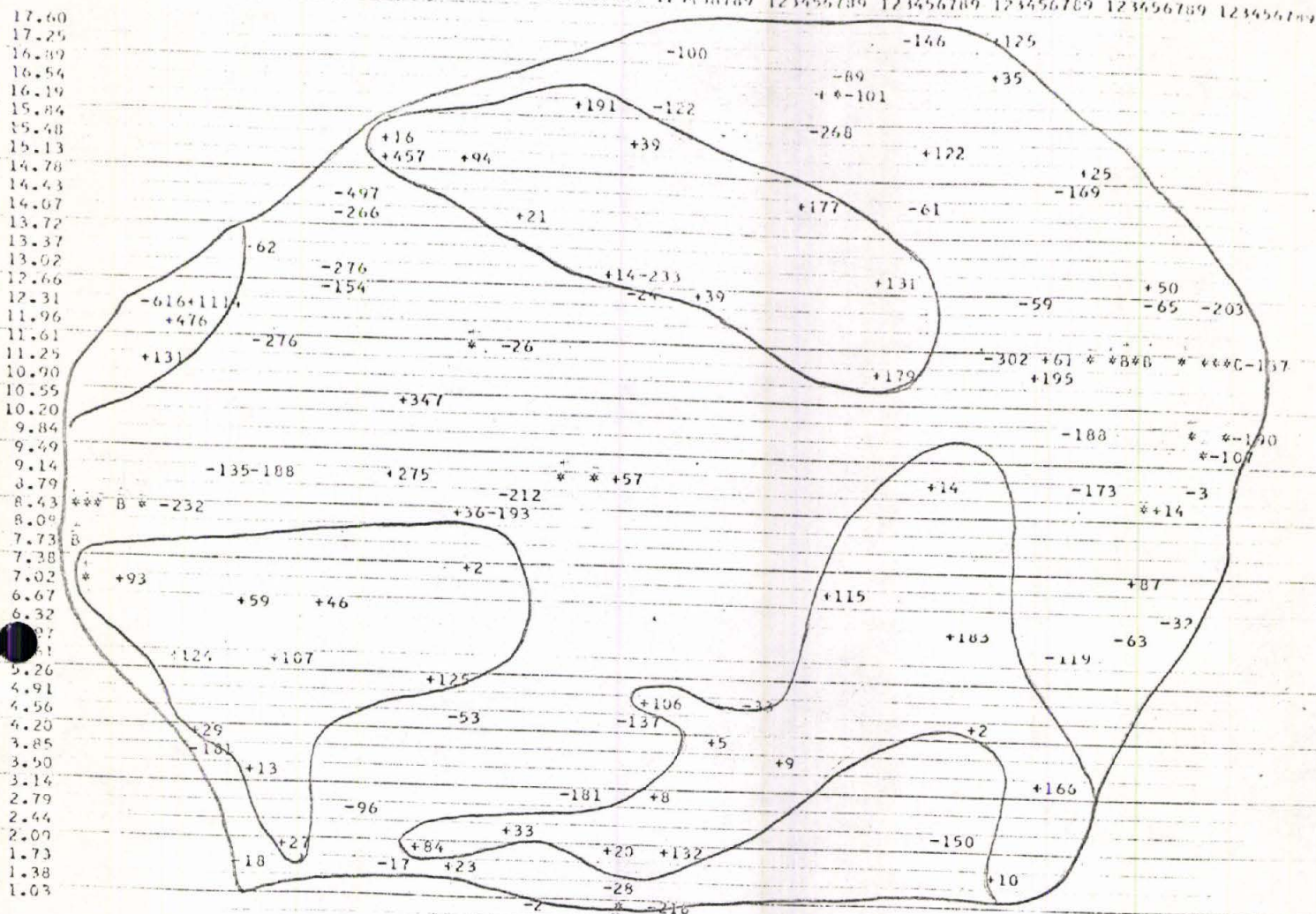
PLOTTED VALUES HAVE BEEN MULTIPLIED BY A FACTOR OF 10 TO THE 2 POWER

X-SCALE IS HORIZONTAL

OF = 0.80 + 0.2115 X (SCALE VALUE)

Y-SCALE IS VERTICAL

0123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789



0123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789

OVERPRINT VALUES

351	B -200
248	* -275
-43	47
140	B -23
-209	203
46	
-68	* 179
-93	
205	* 200
107	
184	
246	
82	
-82	
-17	
-102	

Figure 2d. Plot of sixth-degree residuals for total mafics.

TONG LAKE TREND SURFACE ANALYSIS PROGRAMME

CONTOURED FIRST-DEGREE SURFACE

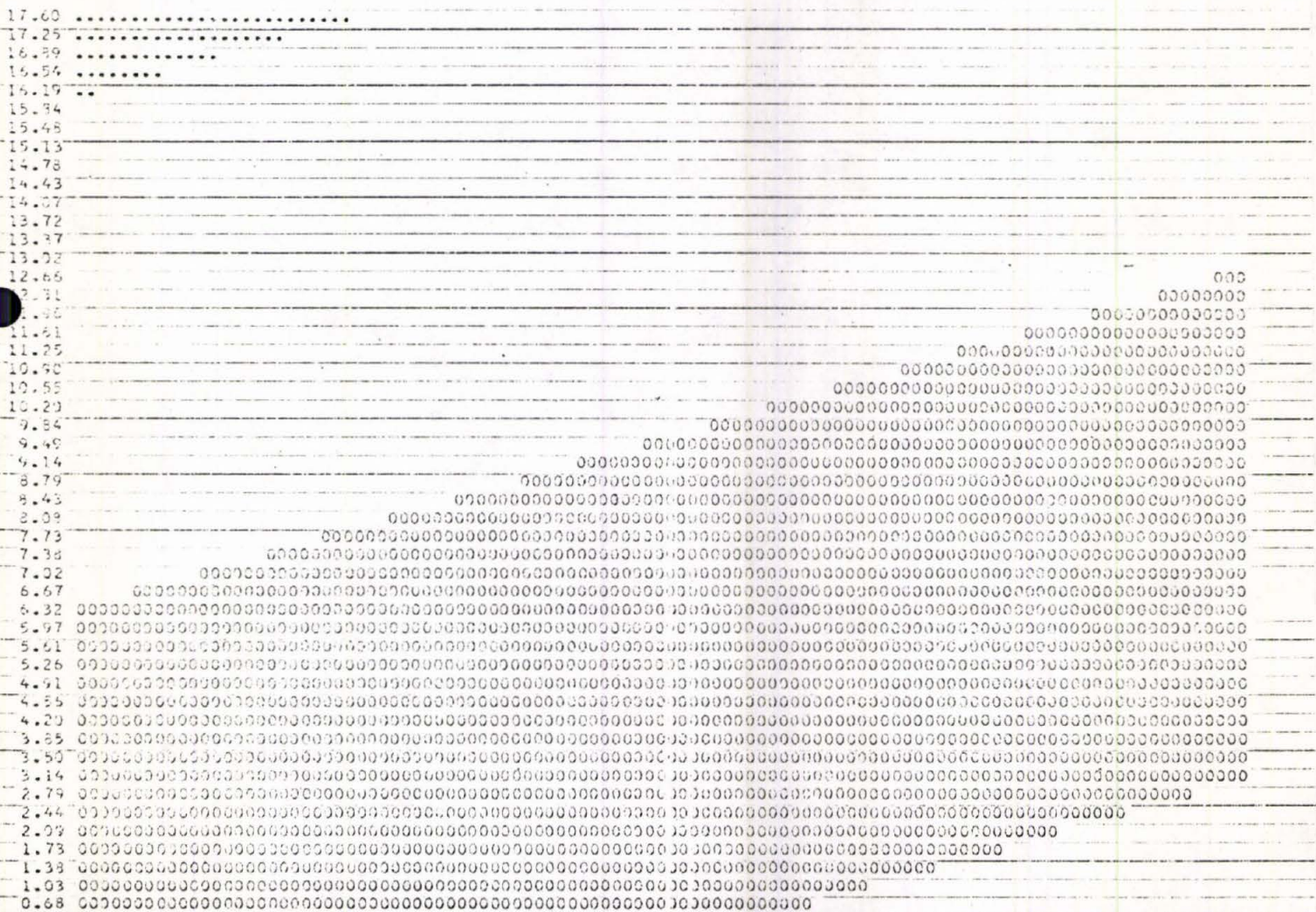
PLOTTING LIMITS
MAXIMUM X = 22.799988 MINIMUM X = 0.800000
MAXIMUM Y = 17.599991 MINIMUM Y = 0.700000

X-SCALE IS HORIZONTAL
X-VALUE = 0.80 + 0.2115 X (SCALE VALUE)

Y-SCALE IS VERTICAL

CONTOUR INTERVAL = 5.00
REFERENCE CONTOUR (.....) = 20.00

0123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789



0123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789

Figure 3a. Contour of first-degree surface for quartz.

OF FIRST-DEGREE RESIDUALS

PLACING 1 (M11)

MAXIMUM X = 22.79999 MINIMUM X = 0.000000
 MAXIMUM Y = 17.99999 MINIMUM Y = 0.000000

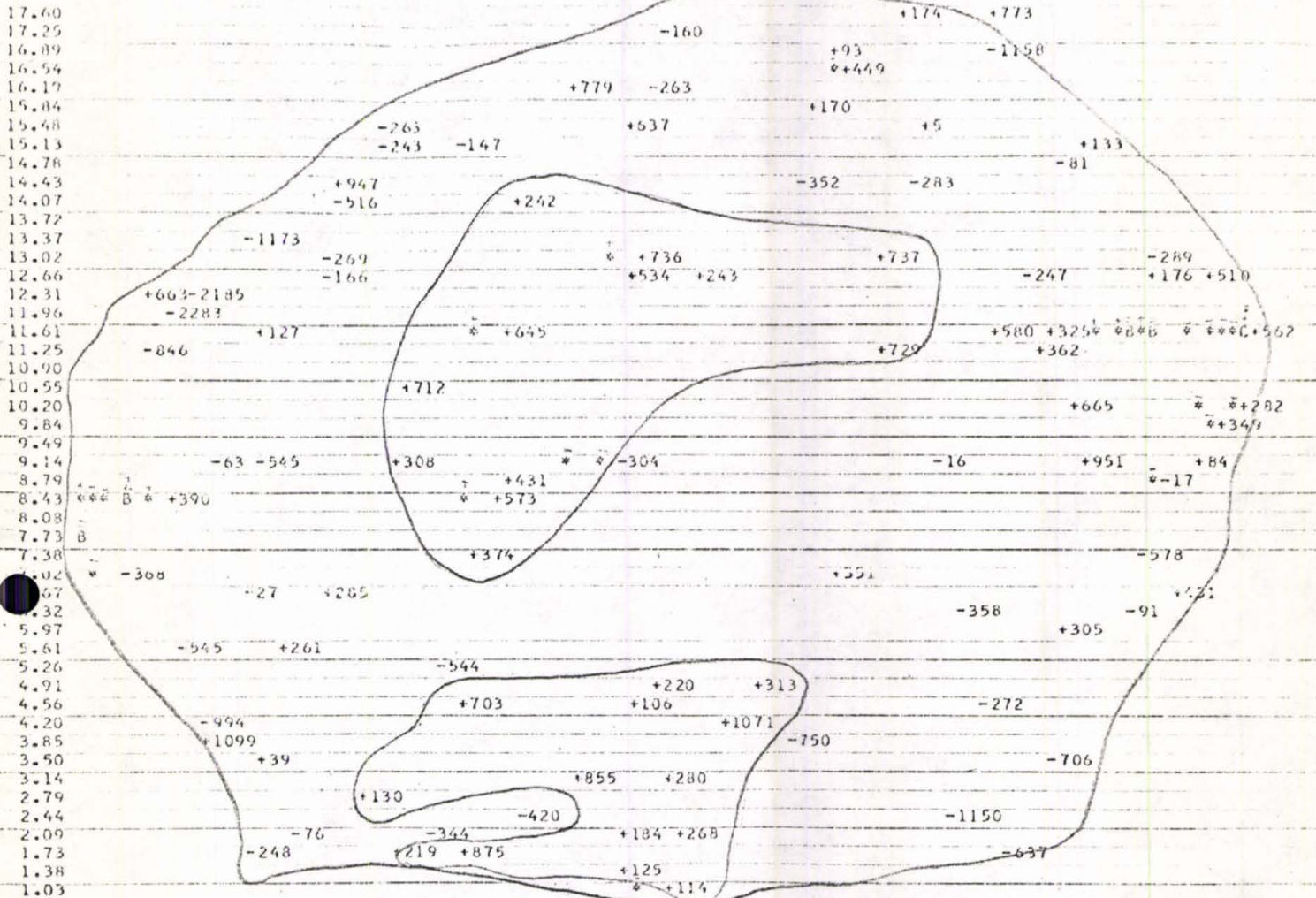
PRINTED VALUES HAVE BEEN MULTIPLIED BY A FACTOR OF 10 TO THE 2 POWER

X-AXIS IS HORIZONTAL

SCALE VALUE = 0.00 + 0.2115 X (SCALE VALUE)

SCALE IS VERTICAL

0123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789



0123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789

OVERPRINT VALUES

- * -547
- * -869
- * 645
- * 232
- * -105
- * -58
- B 184
- B 715
- B 105
- B 594
- * -707
- * 98
- * -948
- * 1086
- B 149
- B -763
- B -101
- B -516
- B -33
- B -169
- * -506
- * -1023
- * -439
- * -219
- B 50
- B 4
- B 174
- B -195
- B -193
- B -177
- B -974
- B -304
- B 307

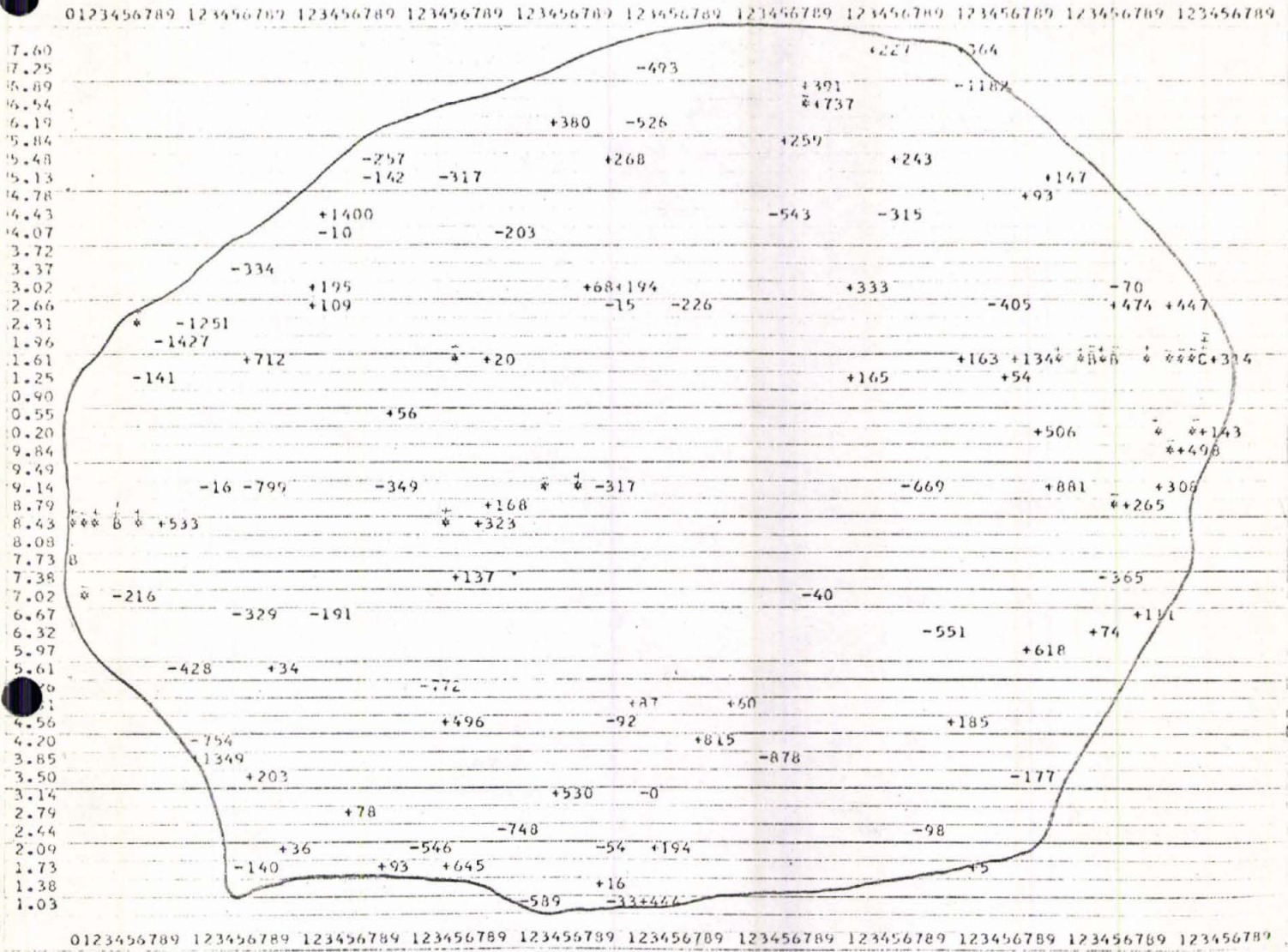
Figure 3b. Plot of first-degree residuals for quartz.

MAX X = 22.79999 MINIMUM X = 0.000000
 MAX Y = 17.59999 MINIMUM Y = 0.700000

ALL VALUES HAVE BEEN MULTIPLIED BY A FACTOR OF 10 TO THE 2 POWER

ALL IS HORIZONTAL
 TUE = 0.00 + 0.2115 X (SCALE VALUE)

ALL IS VERTICAL



RPRINT VALUES
 -260 B 986
 1057 * 871
 * 351
 * 639
 -210 B -235
 268 -104
 287
 -470
 -686 * -969
 435
 -436
 -158
 206
 -272
 -357
 -1082
 131
 1241
 -378
 -756
 -319
 241
 -584
 194
 -16

Figure 3d. Plot of sixth-degree surface for quartz.

TUNK LAKE TREND-SURFACE ANALYSIS PROGRAMME

CONTINUED FIRST-DEGREE SURFACE

PLOTTING LIMITS

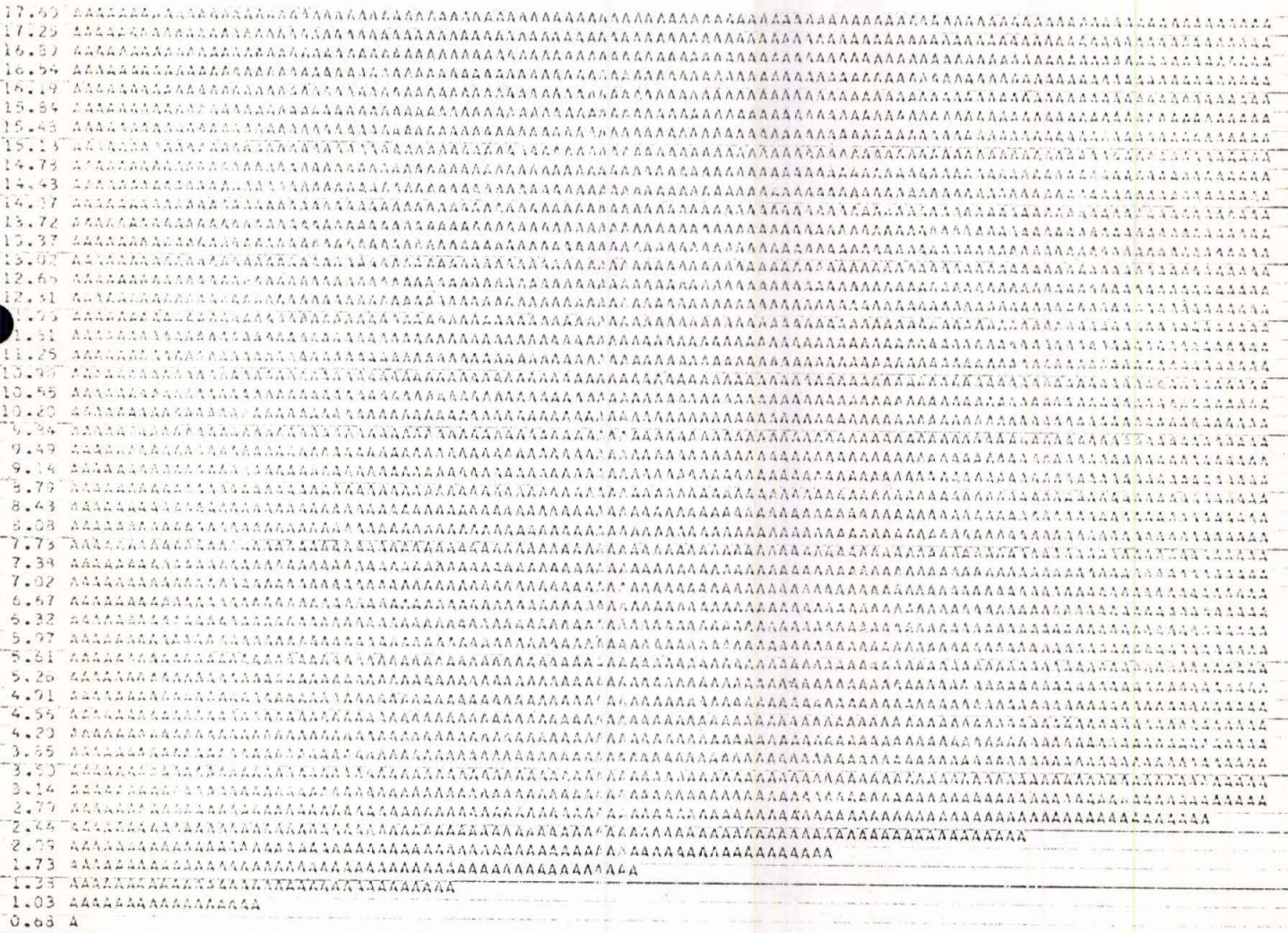
MAXIMUM X = 22.79998 MINIMUM X = 0.80000
MAXIMUM Y = 17.99999 MINIMUM Y = 0.70000

X-SCALE IS HORIZONTAL
X-VALUE = 0.80 + 0.2115 X (SCALE VALUE)

Y-SCALE IS VERTICAL

CONTOUR INTERVAL = 5.00
REFERENCE CONTOUR (.....) = 20.00

0123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789



0123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789

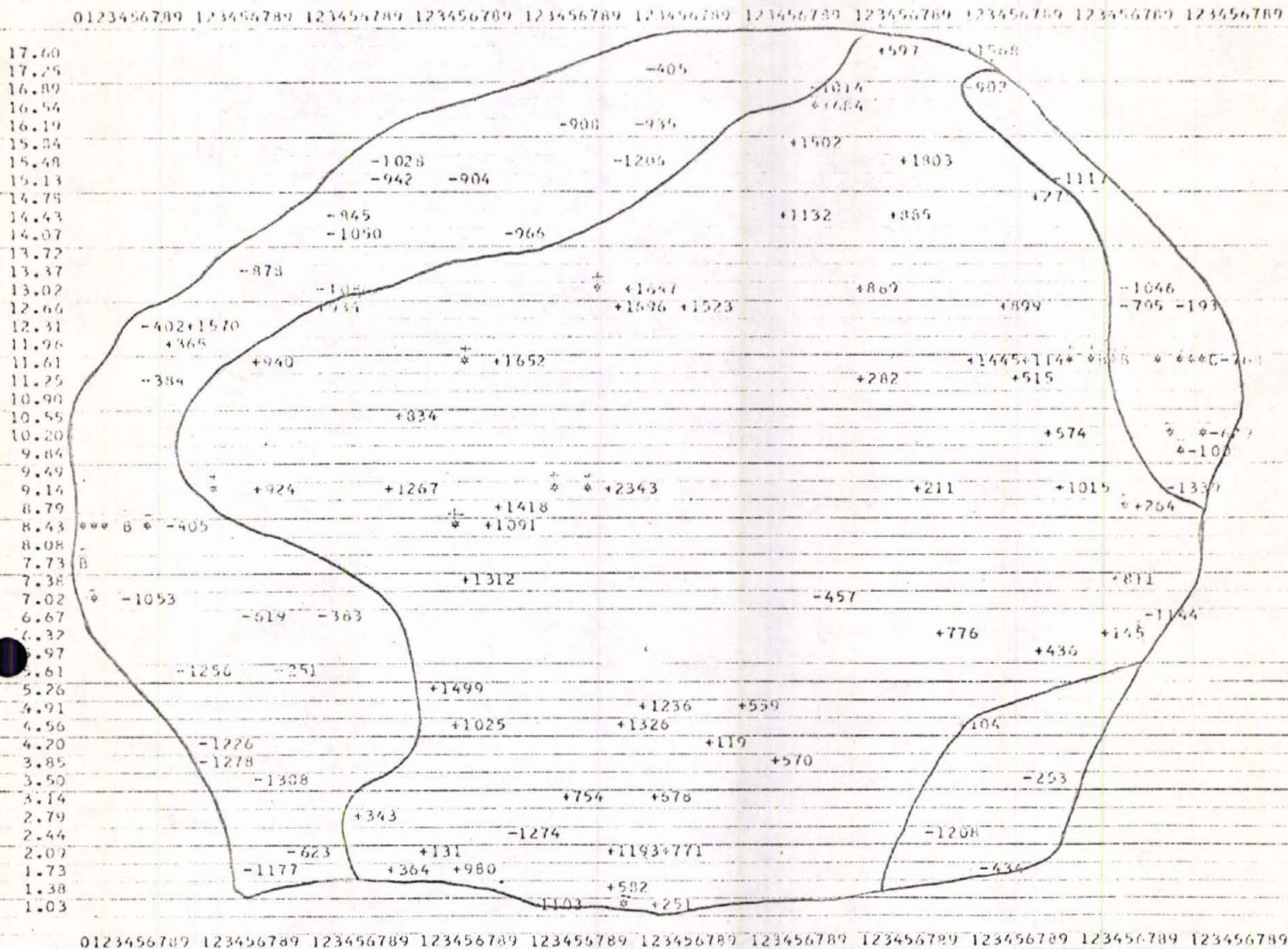
Figure 4a. Contour of first-degree surface for oligoclase.

TYPE OF FIRST DEGREE RESIDUALS
 MINIMUM X = 22.79998 MINIMUM Y = 0.00000
 MAXIMUM X = 17.89991 MAXIMUM Y = 0.70000

OTHER VALUES HAVE BEEN MULTIPLIED BY A FACTOR OF 10 TO THE 2. POWER

SCALE IS HORIZONTAL
 1 UNIT = 0.001 X 0.2115 X (SCALE VALUE)

SCALE IS VERTICAL



OVERPRINT VALUES

*	-851	* 1206
*	1518	* -1230
*		* -1252
*	1027	* -1273
*	326	B - 674
*	718	- 434
B	-152	* - 494
*	97	* 586
*	-872	
B	-112	B - 123
*	-1063	-1147
*	-895	
*	-1163	* -1256
*	-1053	
*	-1153	* -1328
*	-994	
*	1094	
*	016	
*	-457	
*	-1089	
*	-1107	
*	1095	
*	1903	
*	1444	
*	1206	

Figure 4b. Plot of first-degree residuals for oligoclase.

TUNK LAKE TACNO-SURFACE ANALYSIS PROGRAMME

CONToured FOURTH DEGREE SURFACE

PLOTTING LIMITS

MAXIMUM X = 22.794988 MINIMUM X = 0.800000
 MAXIMUM Y = 17.599791 MINIMUM Y = 0.700000

X-SCALE IS HORIZONTAL

X-VALUE = 0.80 + 0.2115 X (SCALE VALUE)

Y-SCALE IS VERTICAL

CONTOUR INTERVAL = 5.00
 REFERENCE CONTOUR (.....) = 20.00

0123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789



0123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789

Figure 4c. Contour of fourth-degree surface for oligoclase.

PLOT OF FOURTH-DEGREE SURFACES

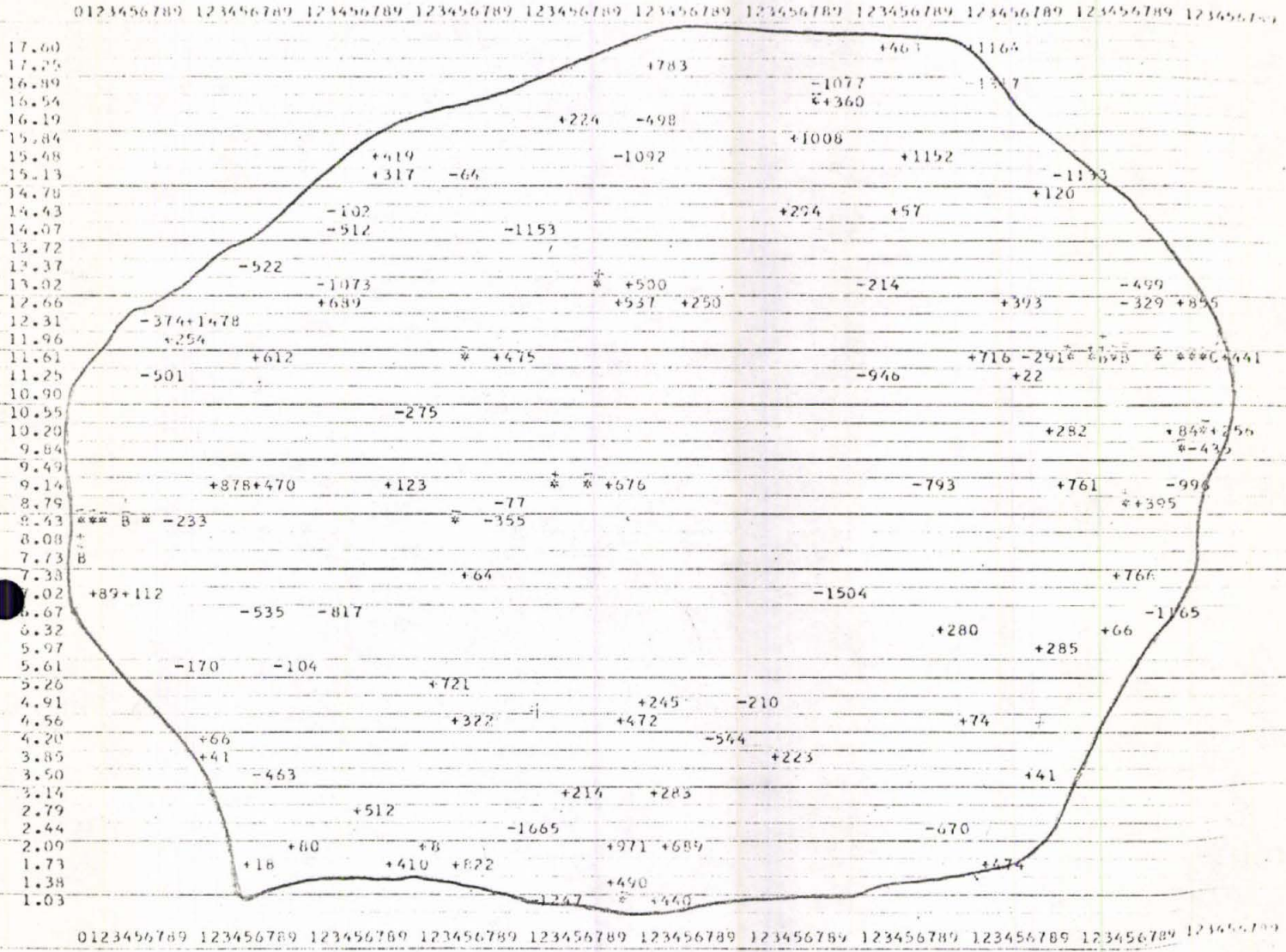
BOUNDING LIMITS

MAXIMUM X = 22.799988 MINIMUM X = 0.800000
 MAXIMUM Y = 17.899991 MINIMUM Y = 0.700000

ALL VALUES HAVE BEEN MULTIPLIED BY A FACTOR OF 10 TO THE 2 POWER

X-SCALE IS HORIZONTAL
 X-VALUE = 0.00 + 0.2115 X (SCALE VALUE)

Y-SCALE IS VERTICAL



OVERPRINT VALUES

-1067	*-203
444	*1295
-134	*-428
280	*-480
798	*-577
11	B-129
303	72
-473	*-138
-437	*-750
-639	
-258	B1063
-260	96
-57	
103	*-1245
106	
106	
317	
546	
287	

Figure 4d. Plot of fourth-degree surface for oligoclase.

TUNY LAKE TRENCH SURFACE ANALYSIS PROGRAMME

CONTOURED SIXTH-DEGREE SURFACE

PLOTTING LIMITS

MAXIMUM X = 22.791988 MINIMUM X = 0.800000
MAXIMUM Y = 17.599991 MINIMUM Y = 0.700000

X-SCALE IS HORIZONTAL

X-VALUE = 0.10 X 0.2115 X (SCALE VALUE)

Y-SCALE IS VERTICAL

CONTOUR INTERVAL = 5.00

REFERENCE CONTOUR (.....) = 20.00

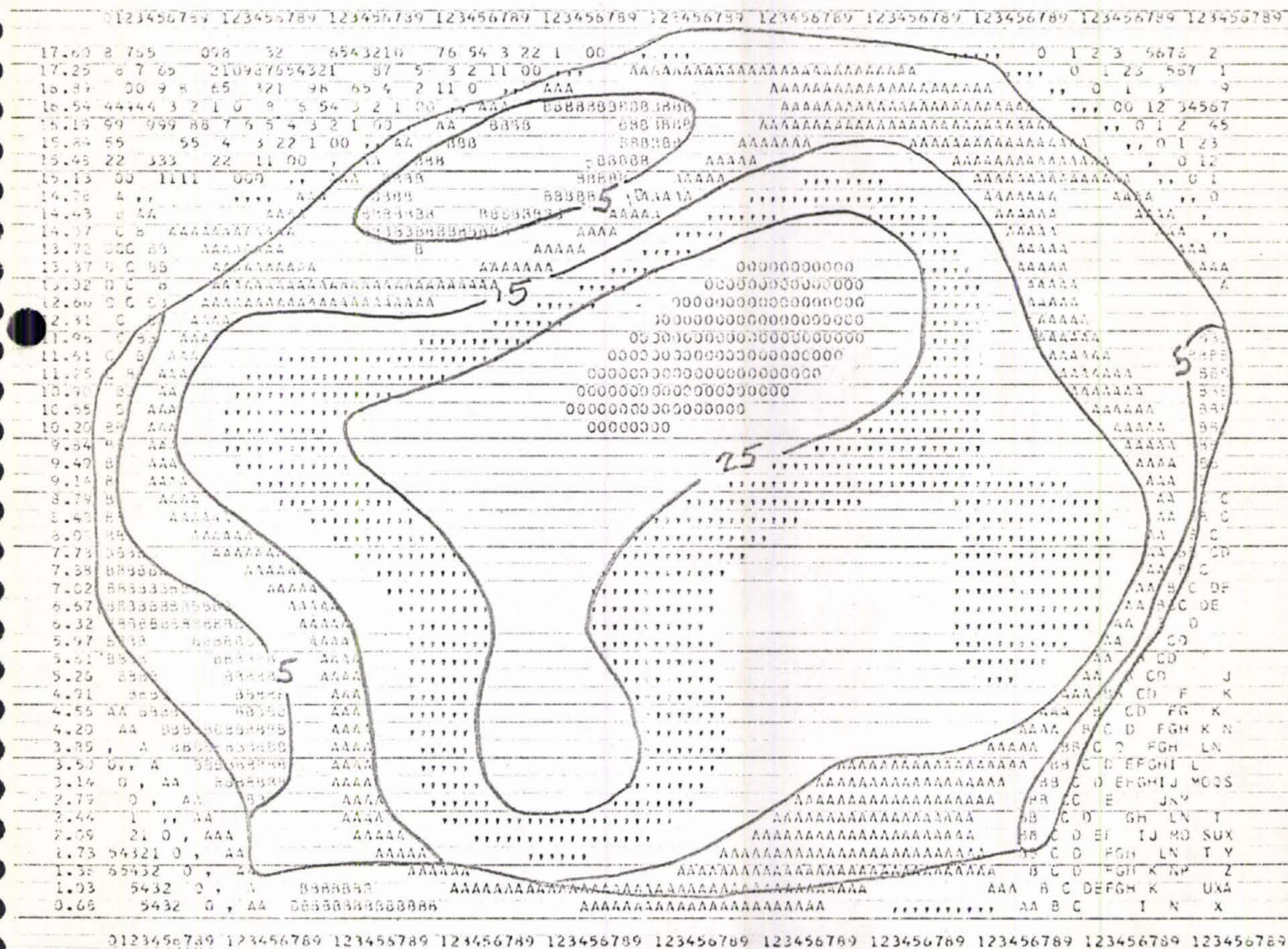


Figure 4e. Contour of sixth-degree surface for oligoclase.

FIGURE 1a. FIRST-DEGREE SURFACE ANALYSIS PROGRAM

CONTOUR OF FIRST-DEGREE SURFACE

DEFINING LIMITS

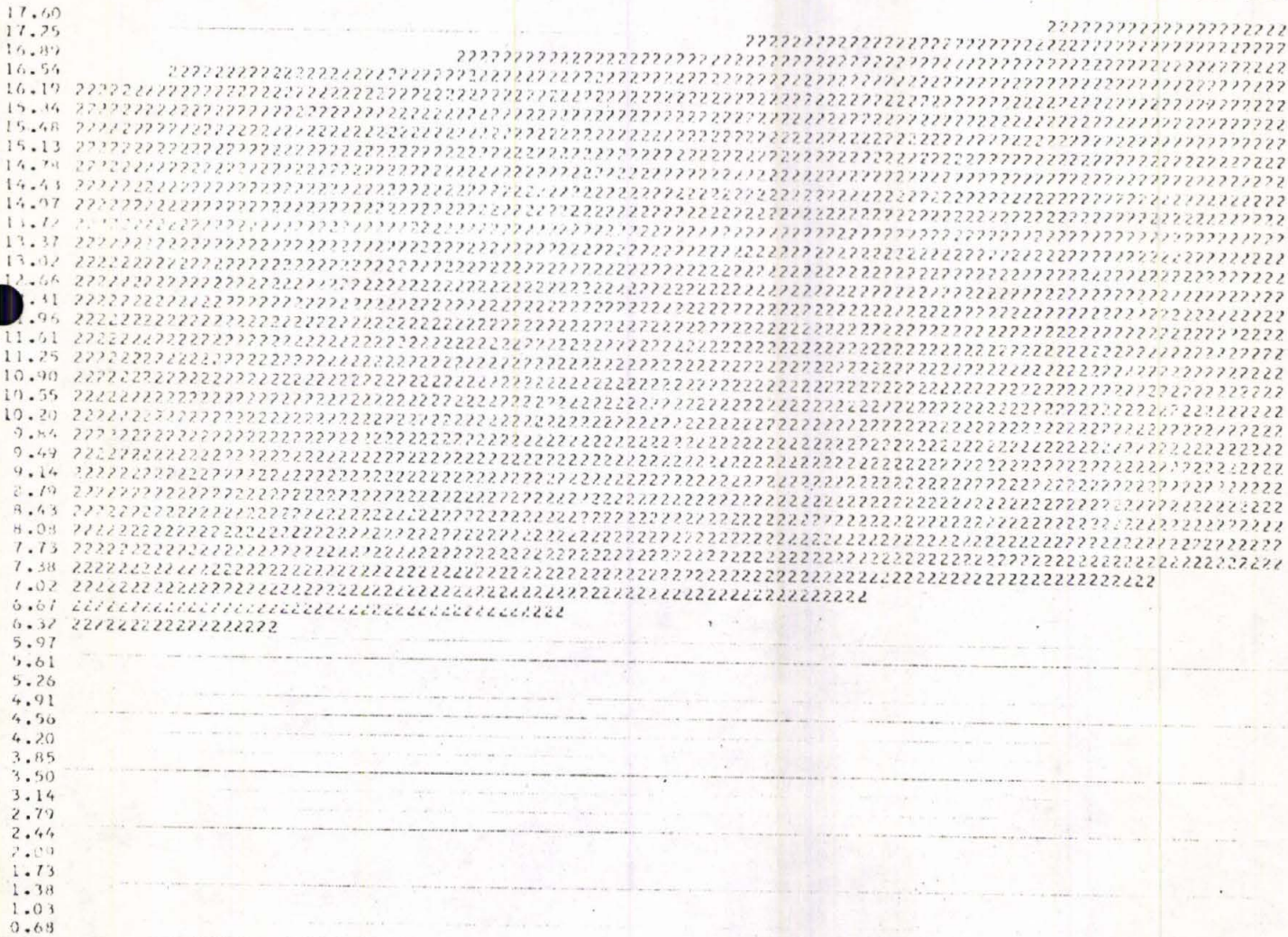
MAXIMUM X = 27.79998 MINIMUM X = 0.800000
MAXIMUM Y = 17.99999 MINIMUM Y = 0.700000

X-SCALE IS HORIZONTAL
X-VALUE = 0.80 + 0.2115 X (SCALE VALUE)

Y-SCALE IS VERTICAL

CONTOUR INTERVAL = 5.00
REFERENCE CONTOUR (.....) = 20.00

0123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789



0123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789

Figure 5a. Contour of first-degree surface for perthite.

MAXIMUM X = 22.700000 MINIMUM X = 0.000000
 MAXIMUM Y = 17.500000 MINIMUM Y = 0.000000

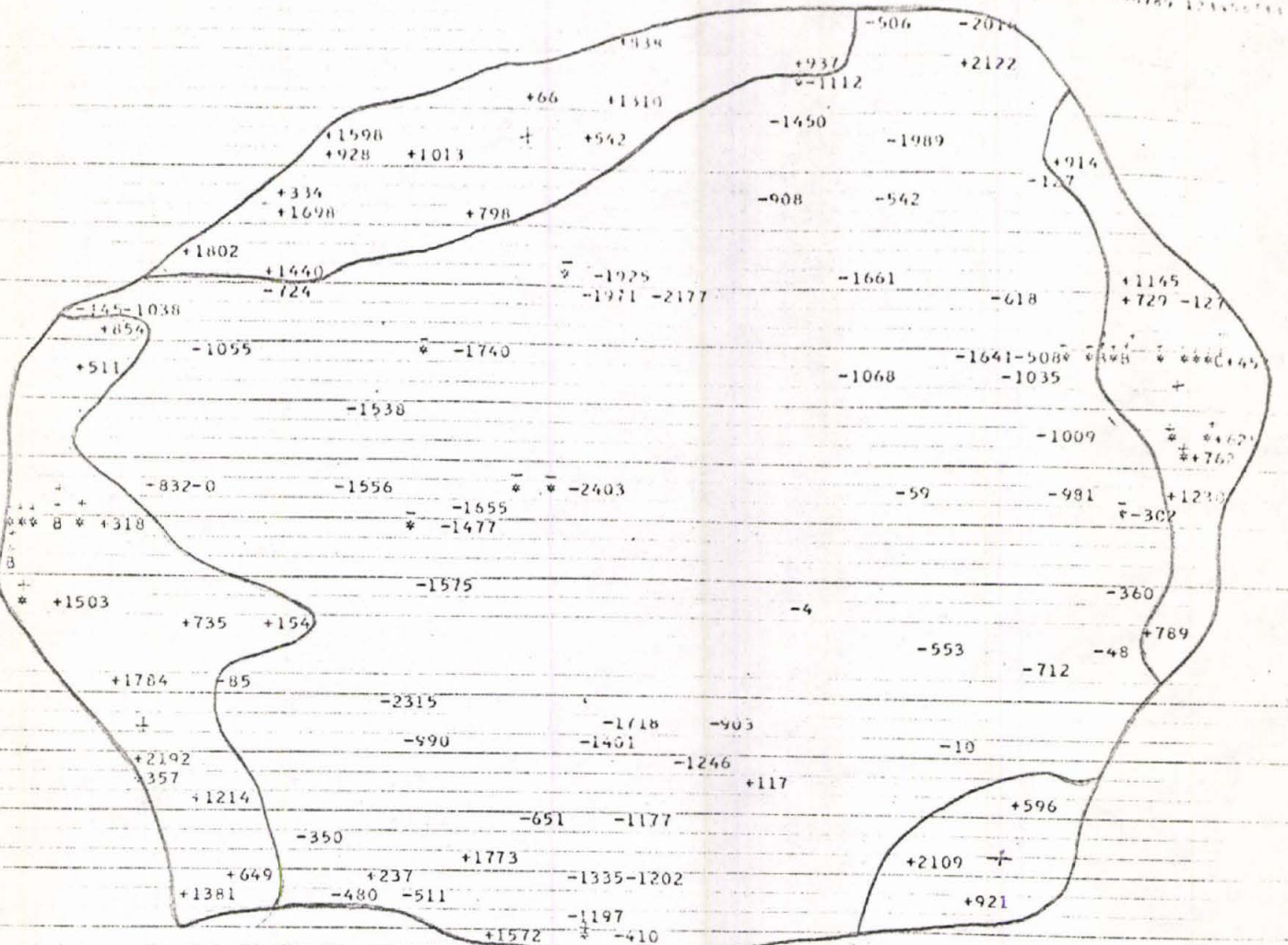
PLOTTED VALUES HAVE BEEN MULTIPLIED BY A FACTOR OF 10 TO THE POWER

X-SCALE IS HORIZONTAL
 X-VALUE = 0.80 + 0.2115 X (SCALE VALUE)

Y-SCALE IS VERTICAL

0123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789

17.60
 17.25
 16.89
 16.54
 16.19
 15.84
 15.48
 15.13
 14.78
 14.43
 14.07
 13.72
 13.37
 13.02
 12.66
 12.31
 11.96
 11.61
 11.25
 10.90
 10.55
 10.20
 9.84
 9.49
 9.14
 8.79
 8.43
 8.08
 7.73
 7.38
 7.02
 6.67
 6.32
 5.97
 5.61
 5.26
 4.91
 4.56
 4.20
 3.85
 3.50
 3.14
 2.79
 2.44
 2.09
 1.73
 1.38
 1.03



0123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789

OVERPRINT VALUES

* 1167	B 125
	85
* -1937	347
	-999
* -1957	
* -541	B 411
* -1064	1161
B 955	
* 686	* 2316
* 666	
B 1456	* 1152
* 1237	
* 834	
* 1425	
* 1266	
* 2716	
C 447	
* -232	
1387	
472	
684	
* 1267	
* -2311	
* -1204	
* -217	
* 1098	
* 1581	
* 1325	

Figure 5b. Plot of first-degree residual for perthite.

TINK LAKE TRENCH SURFACE ANALYSIS PROGRAMME

CONToured FOURTH DEGREE SURFACE

CUTTING LIMITS

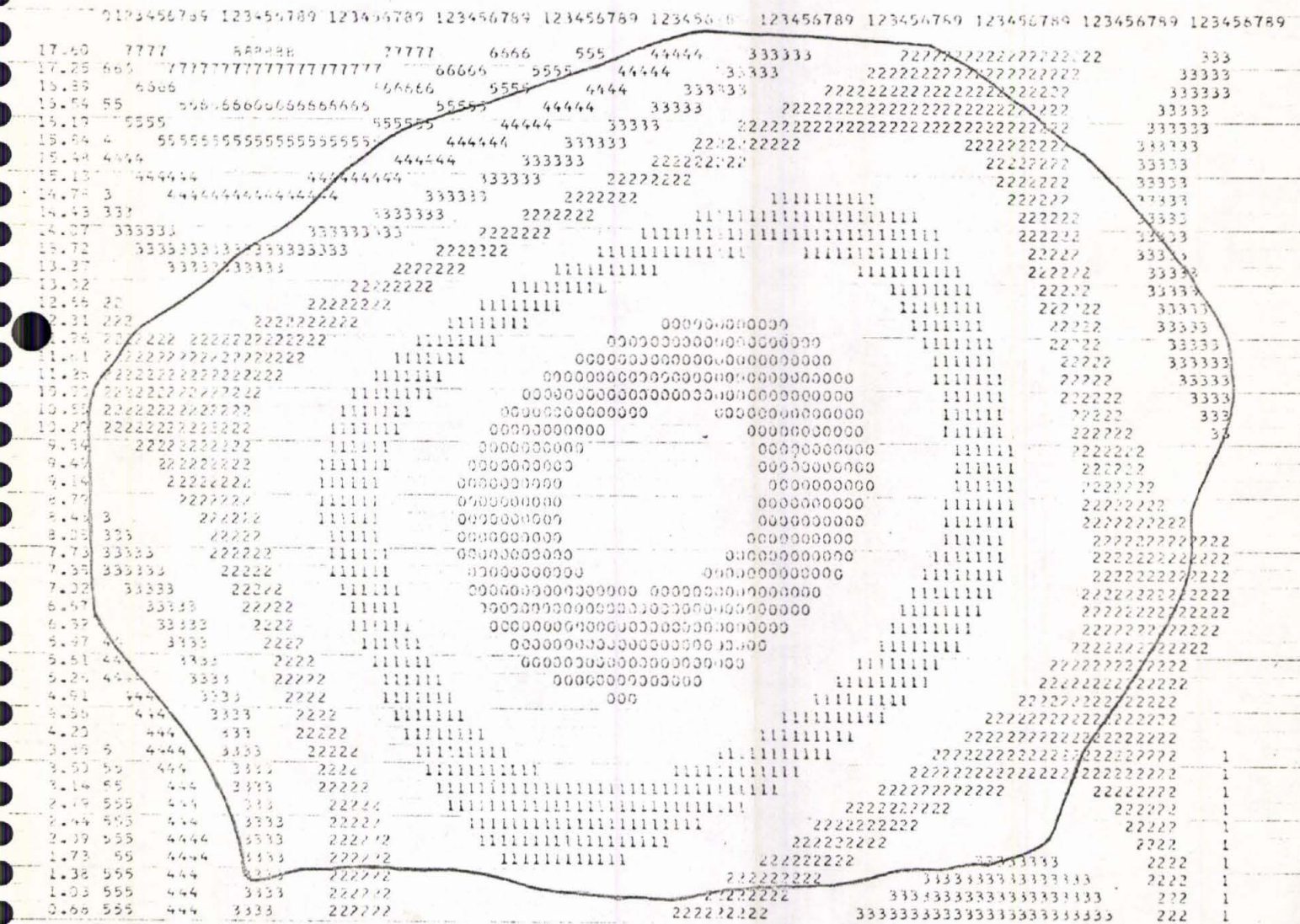
MINIMUM X = 22.79998 MINIMUM Y = 0.80000
 MAXIMUM X = 17.599991 MINIMUM Y = 0.700000

X-SCALE IS HORIZONTAL

(X-VALUE = 0.00 + 0.2115 X (SCALE VALUE))

Y-SCALE IS VERTICAL

CONTOUR INTERVAL = 5.00
 REFERENCE CONTOUR (.....) = 20.00



0123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789

Figure 5c. Contour of fourth-degree surface for perthite.

OF SIXTH-DEGREE RESIDUALS

LOG UNITS

MIN X = 22.799908 MINIMUM X = 0.000000
MIN Y = 17.599991 MINIMUM Y = 0.000000

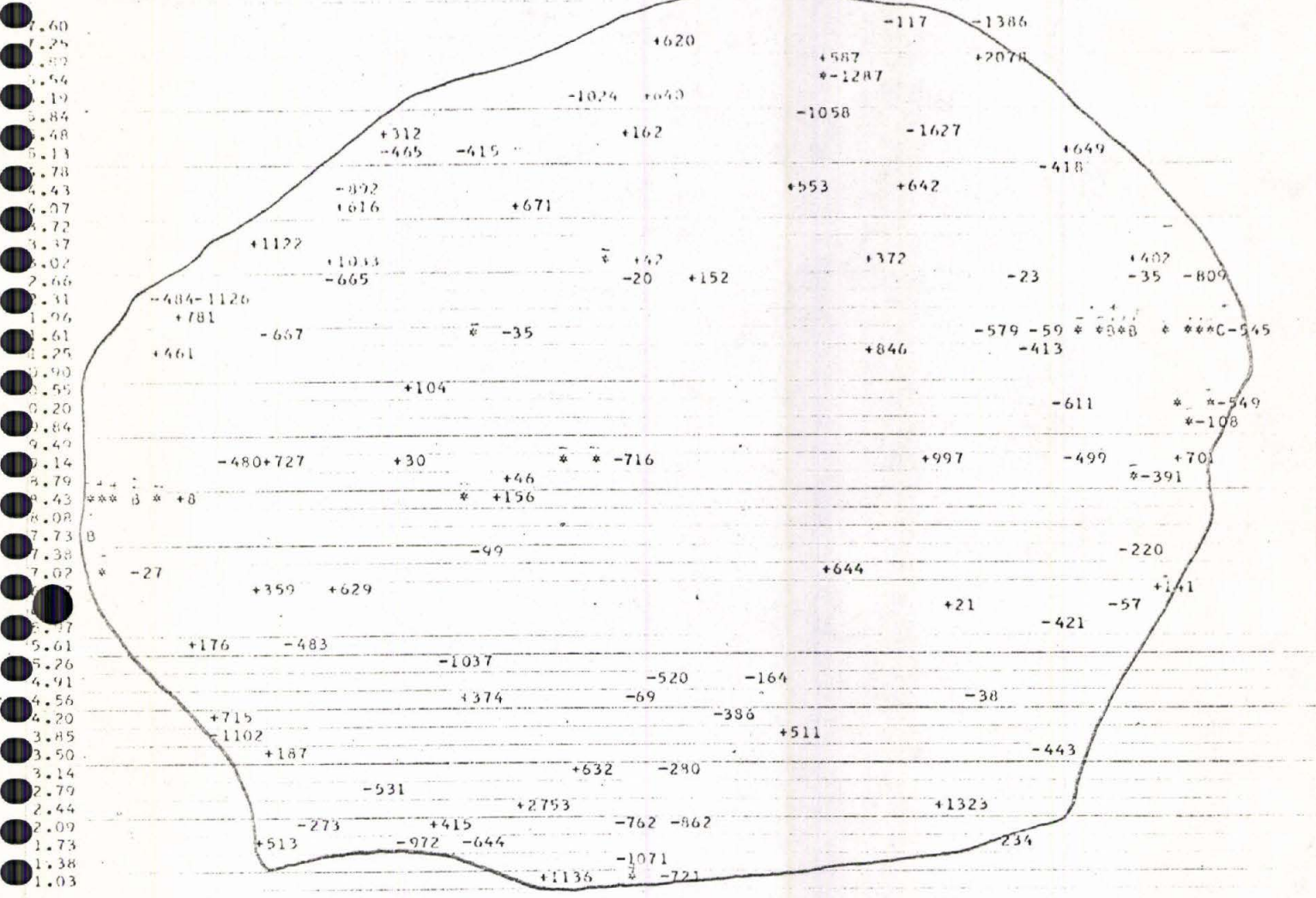
ED VALUES HAVE BEEN MULTIPLIED BY A FACTOR OF 10 TO THE 2 POWER

S HORIZONTAL

0.00 + 0.2115 X (SCALE VALUE)

ME IS VERTICAL

0123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789



0123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789

PRINT VALUES

890	*	198	*
		470	*
183	*	452	*
		-627	B
269	*	-630	
-654	*	-203	*
373	*	645	*
538	B	-764	B
215		-97	
142	*		
836	B	845	*
525			
-52	*	777	*
430	*		
264	*		
213	*		
553			
-335	*		
541	*		
1147	*		
-574	*		
-76	*		
207	*		

Figure 5d. Plot of fourth-degree residuals for perthite.

TUNG LAKE TRENDS-SURFACE ANALYSIS PR. GRAMME

CONTAINED SIXTH-DEGREE SURFACE

PLOTTING LIMITS

MAXIMUM X = 02.79999 MINIMUM X = 0.800000
MAXIMUM Y = 17.99991 MINIMUM Y = 0.700000

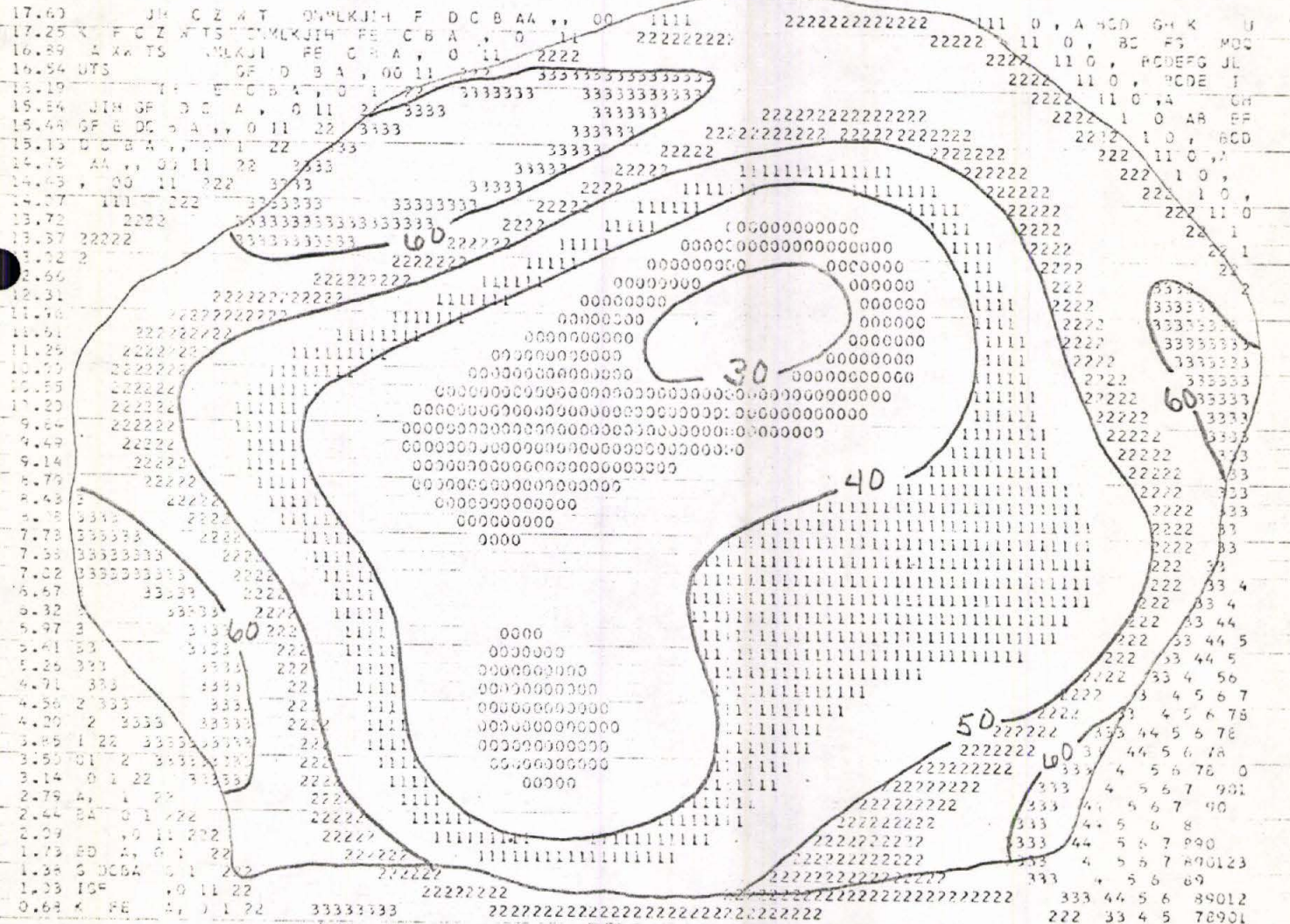
X-SCALE IS HORIZONTAL

A-VALUE = 0.80 + 0.2115 X (SCALE VALUE)

Y-SCALE IS VERTICAL

CONTOUR INTERVAL = 5.00
REFERENCE CONTOUR (.....) = 20.00

0123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789



0123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789

Figure 5e. Contour of sixth-degree surface for perthite.

TUNK LAKE TRENDS-SURFACE ANALYSIS PROGRAMME

CENTROURED FI-ST-DEGREE SURFACE

PLOTTING LIMITS

MAXIMUM X = 22.79988 MINIMUM X = 0.80000
MAXIMUM Y = 17.99991 MINIMUM Y = 0.70000

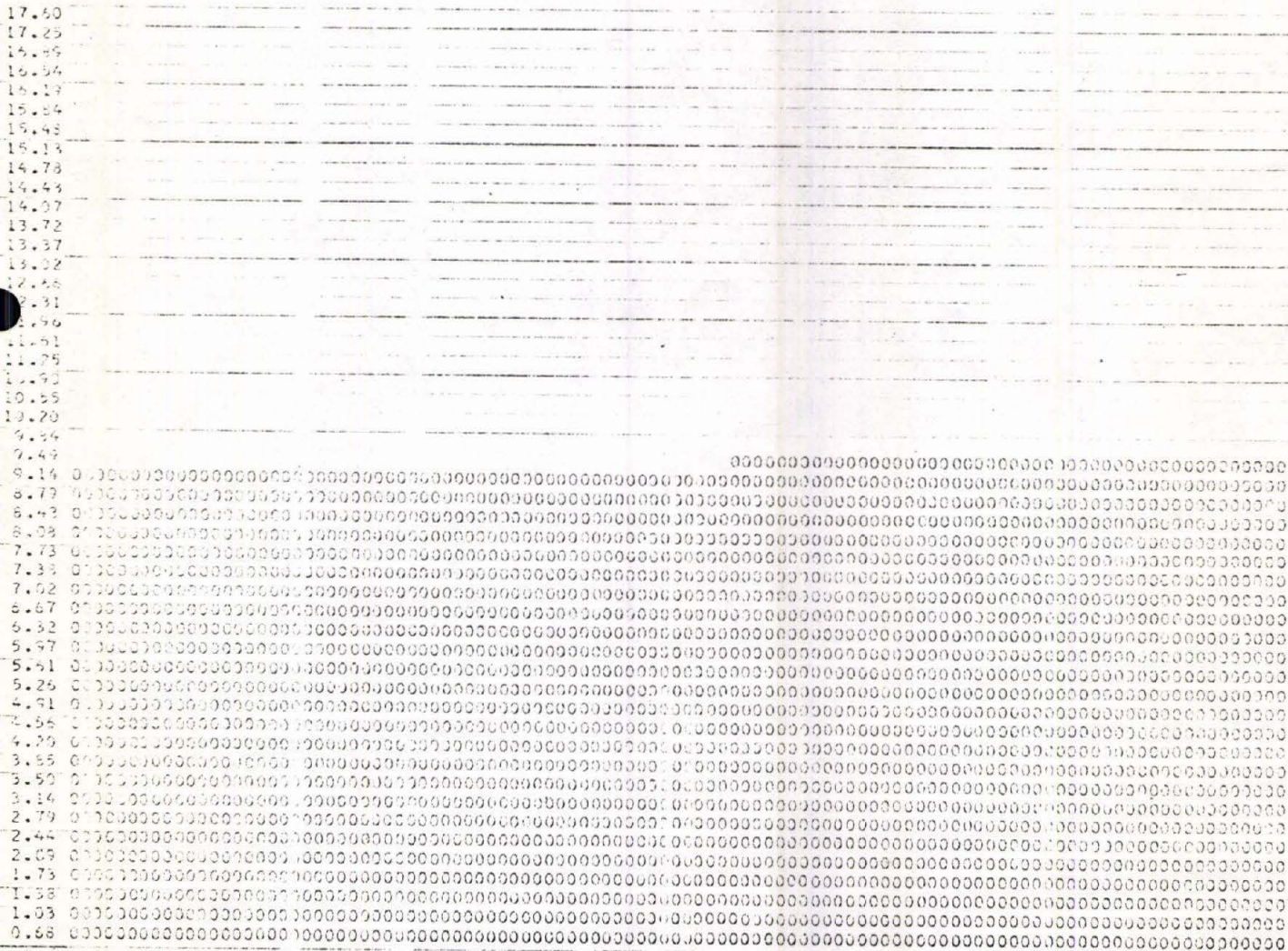
X-SCALE IS HORIZONTAL

X-VALUE = 0.80 + 0.2115 X (SCALE VALUE)

Y-SCALE IS VERTICAL

CENTOUR INT-VAL = 5.00
REFERENCE C-NTUR (.....) = 20.00

0123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789



0123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789

Figure 6a. Contour surface for the first-degree albite-in-perthite.

PLOT OF FIRST-DEGREE RESIDUALS

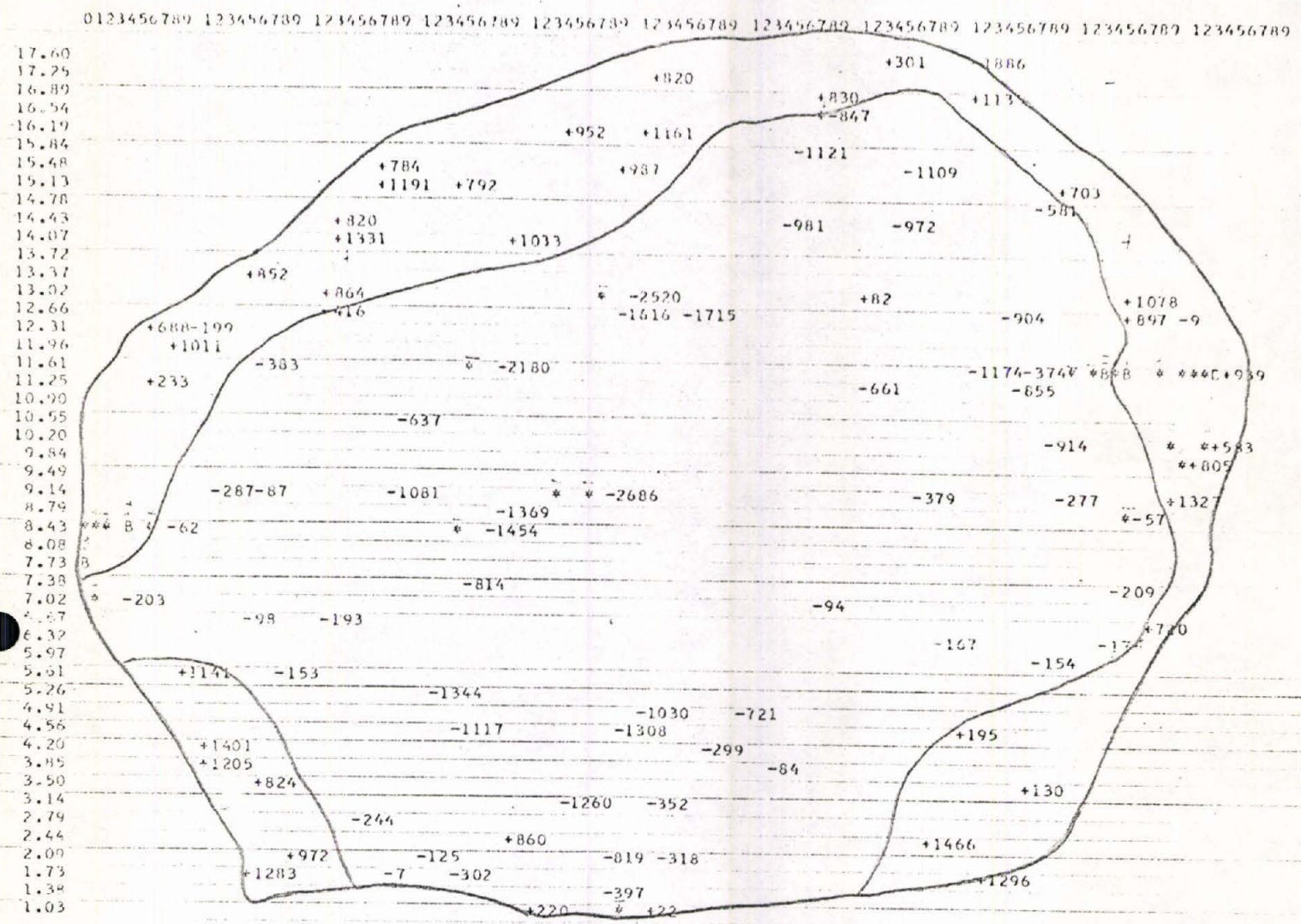
PLOTTING LIMITS

MAXIMUM X = 17.799988 MINIMUM X = 0.000000
 MAXIMUM Y = 17.599991 MINIMUM Y = 0.700000

PLotted VALUES HAVE BEEN MULTIPLIED BY A FACTOR OF 10 TO THE 2 POWER

SCALE IS HORIZONTAL
 AUM = 0.00 + 0.2115 X (SCALE VALUE)

Y-SCALE IS VERTICAL



0123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789

OVERPRINT VALUES

- * 744
- * 932
- * 836
- * -2220
- * 836
- B 36
- * -1070
- * 337
- * -62
- * 237
- * -465
- * 1462
- B -765
- B 658
- * -65
- * 1166
- * 744
- B 534
- * 1234
- * 1184
- * 938
- * 1025
- * 431
- * 531
- * 931
- * 531
- * 431
- * 784
- * 1084
- * 1002
- * -2084
- * -1684

Figure 6b. Plot of first-degree residuals, albite-in perthite.

TWIN LAKE TRENDS-SURFACE ANALYSIS PROGRAMME

CONTOURED SIXTH-DEGREE SURFACE

PLOTTING LIMITS

MAXIMUM X = 22.799988 MINIMUM X = 0.000000
 MAXIMUM Y = 17.599991 MINIMUM Y = 0.700000

X-SCALE IS HORIZONTAL

X-VALUE = 0.80 + 0.2115 X (SCALE VALUE)

Y-SCALE IS VERTICAL

CONTOUR INTERVAL = 5.00

REFERENCE CONTOUR (.....) = 20.00

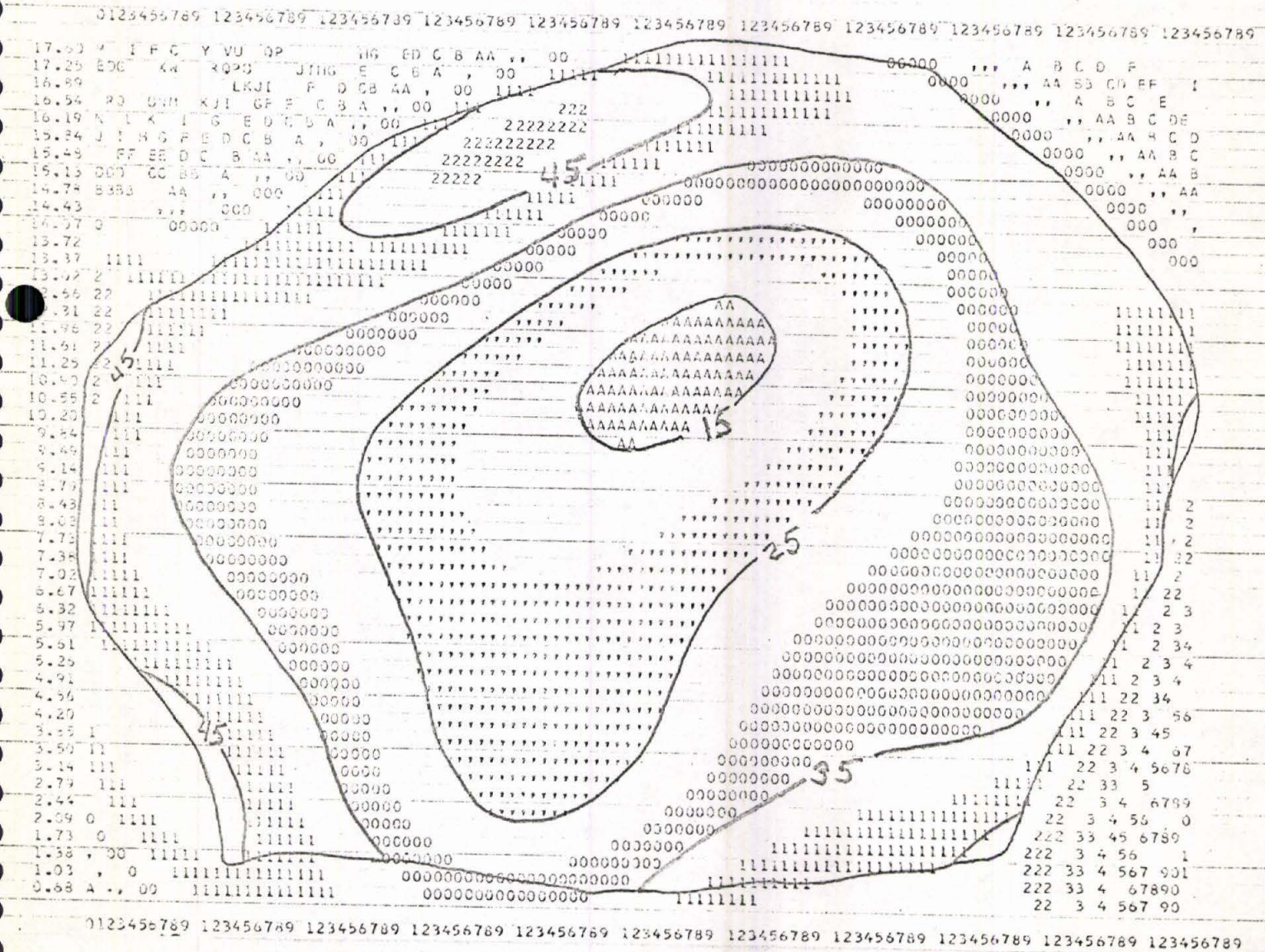


Figure 6e. Contour of sixth-degree surface for albite-in-perthite.

REFERENCES

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APPENDIX

Included in the appendix is a sample of the cataloging input and MIRL Report No. 9 (Heiner and Geller) which contains all the necessary information on how to punch control cards for the program and the program itself.

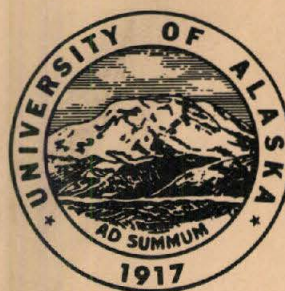
The program was cataloged in the following manner:

```
// JOB      (acc. & user no.)  (name)
  ASSGN SYSCLB,U.A.
  ASSNG SYSCLB,A'131'
// OPTION CATALOG
  PHASE TRENMAIN,ROOT
// EXEC FFORTRAN
  (source deck of main program, range)
/* INCLUDE
  (object deck of phase fetching subroutine, p. 49)
/*
  PHASE TRENLNKL,*
// EXEC FFORTRAN
  (source decks of link1, t2, contur, emslvr)
/*
  PHASE TRENLNK2,TRENLNKL
// EXEC FFORTRAN
  (source decks of link2, order3, plot3)
/*
// EXEC LNKEDT
/&
  ASSGN SYSCLB,UA
```

The rest of the input followed directly from Heiner and Geller, except for the changed IF statements using the ALPHA subroutine, which has been eliminated. The card deck as it was programmed and used has been entrusted to the care of Dr. Francis Ting, and any one interested in using it should contact him.

Before cataloging, a check should be made with the computer center, 4th floor Twamley Hall. The program will be erased after May 1, 1972.

M. I. R. L.
Report No 9



**FORTRAN IV TREND-SURFACE
PROGRAM for the IBM 360
MODEL 40 COMPUTER**

By Lawrence E. Heiner
Stephen P. Geller

Mineral Industry Research Laboratory
University of Alaska
College, Alaska 99710

ABSTRACT

A Fortran IV trend surface program with polynomial contouring and residual plotting has been adapted to the University of Alaska IBM 360 Model 40 Computer. The program will compute equations of polynomials of the first through sixth degree, measures of the goodness of fit of the surfaces, tabulate original data, x y coordinates and corresponding residuals for each surface; contour each polynomial, and plot original values and residuals for each surface computed.

943 38 23
10/1/81

ACKNOWLEDGEMENTS

The authors wish to acknowledge their debt to the members of the State Geological Survey of Kansas who wrote the original program and who helped in its conversion by giving helpful suggestions and advice through correspondence. The University of Kansas version is published as "Computer Contribution 3" by Daniel F. Merriam, editor, and Mont O'Leary, R. H. Lippert, and Owen T. Spitz.

Funds for computer time and programming assistance were obtained through a grant from the Computer Fund Committee of the University of Alaska.

Subroutine ALPHA was donated by Mr. Bruce Morton of the Geophysical Institute, University of Alaska.

The authors also wish to extend their appreciation to Mr. Edward Gauss who was instrumental in obtaining funds necessary for program conversion, and to Ernest Wolff, who was working with one of the authors on the application of the program to Alaskan mineral deposits.

INTRODUCTION

Purpose of Program

The program has been written to facilitate understanding of various types of geologic, geochemical, geophysical and other data through the use of trend surface analysis. The program is designed for use by exploration firms, other organizations and individuals interested in rapid analysis of field data. It will indicate "target" areas, thereby localizing the search area. Polynomial surfaces are fitted to data (geochemical, geophysical or geological) which are expressed in x, y, z form; x and y being the map coordinates of the data and z being the measured parameter. Successive orders of polynomial equations (e.g. $z = a + bx + cy + \dots$) are fitted to x y z data by the method of least squares. Contouring of these polynomials produce "trend" maps. Residuals (observed data minus computed values) are plotted at each data station to produce anomaly maps. Hence regional trends of data, with anomolous highs and lows eliminated, and anomolous areas (data "noise"), with the regional trend eliminated, may be contoured and mapped. This latter process sharpens anomolies.

The procedure is not new, but the advent of high speed electronic computers have spurred investigations of the use of trend surfaces to aid in mineral exploration and analysis of geologic data. Several investigators are noted in the bibliography.

History

The history of the program development may best be presented by quoting Merriam (1966).

"The original version of this program was published by John W. Harbaugh (1963) in BALGOL for the IBM 7090. In late 1963, Donald I. Good translated the program into FORTRAN II for the IBM 1620, but vast differences in language and hardware necessitated a complete rewriting. Good's

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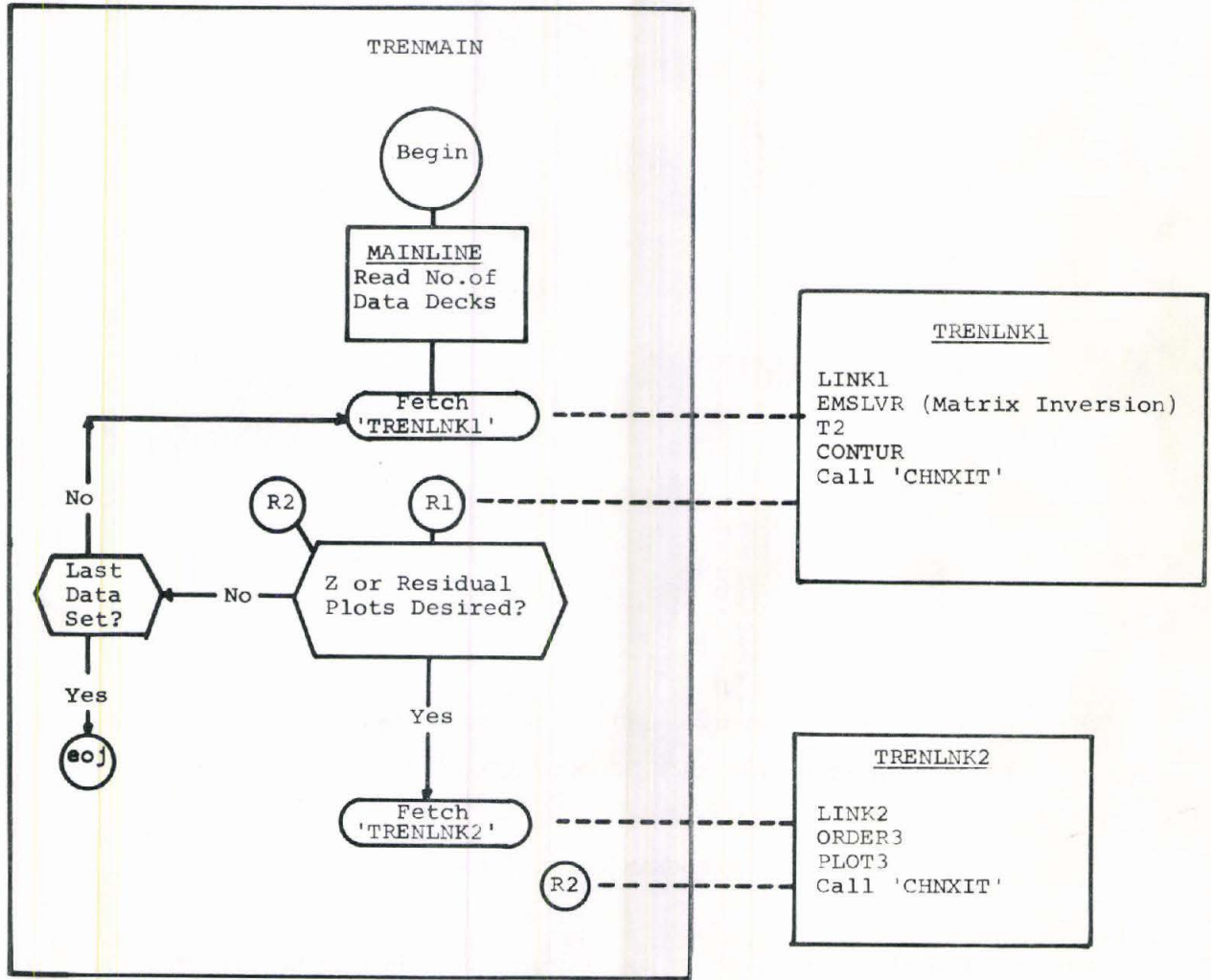
program was published in 1964 as Kansas Geological Survey Special Distribution Publication 14. Shortly after publication of this program, the University of Kansas replaced the 1620 with a larger IBM 7040. In September, 1964, Owen T. Spitz converted the program to FORTRAN IV, revising it to its present two-link chain program form for adaptation to the IBM 7040 with 16K."

Conversion to the IBM 360/40 at the University of Alaska was not too difficult. The University's FORTRAN IV compiler is the E-Level Subset version which does not support reading of FORMAT statements as data, and logical IF statements. An appropriate FORMAT statement, written into the program, solved the first problem; the second was solved by the use of an Assembler-Written FUNCTION, Subroutine 'ALPHA' which performs logical compares on two variables, returning a result of floating-point -1, zero, or +1 for .LT., .EQ., and .GT. respectively.

The Chaining was implemented by using the DOS operating system's program-fetch facilities, and breaking the program into three phases: A root phase containing the mainline and common subroutines, and two overlay phases which replace each other in core (see Figure 1). An assembler subroutine 'CHAIN' was written to effect the overlays. CHAIN accepts an argument of either fixed-point 1 or 2, calling for respectively TRENLNK1 or TRENLNK2 to be fetched. After the fetch, control is passed to the entry point of the called overlay phase. Return to the mainline is accomplished by calling 'CHNXIT', an alternate entry-point of 'CHAIN', which located the stored return address to the mainline and branches to it. This preserves the original logic of the 7040 program, which called a sub-routine 'CHAIN' in this manner.

Another modification was the reading in of a card to define A-Format representations of all the plot characters, which had been done before by setting variables equal to previously calculated numbers, at execution time.

FIGURE I



✓

PROGRAM STRUCTURE

Root Phase 'TRENMAIN'

Includes: The Mainline Program
 RANGE
 ALPHA
 CHAIN
 FORTRAN IOCS & Subroutines

Overlay Phase 'TRENLNK1'

Includes: LINK1
 T2
 CONTUR
 EMSLVR

Overlay Phase 'TRENLNK2'

Includes: LINK2
 ORDER3
 PLOT3

The program and DOS Supervisor fill about 50K bytes (12K words) of 360 storage. The University of Alaska's 360 has 65K bytes of storage available.

PROGRAM DESCRIPTION

Control through the program is exactly as described by Merriam (1966). "Flow of control through the chained program and various subroutines is briefly illustrated in Figure 1. The main steps within each chain link are listed below in order of occurrence:

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LINK 1

Plotting symbols are generated.
Data parameters are read into the program and checked.
x y z coordinates are read in.
Coefficient matrices are generated and solved.
Subroutine T2 is called.

Subroutine T2

Trend surface z values, residuals, error measures, and equations of surfaces are calculated and printed.
Link 1 control cards are read in and checked.
Map titles are printed.
Subroutine CONTUR is called.

Subroutine CONTUR

Trend surfaces are calculated and printed.
(At this point, control of the program returns to mainline.
Link 2 option is interrogated and Link 2 is called if so indicated by option.)

LINK 2

Link 2 control cards are read in and partially checked.
Map titles are printed.
Subroutine PLOT 3 is called.

Subroutine PLOT 3

Remainder of Link 2 control cards are checked.
z and residual values are ordered and plotted."

INPUT DATA PREPARATION

Much of the following input data specifications is again taken verbatim from Merriam (1966) as much of it was not altered during the conversion. All numbers on control cards are integers unless mention is made of a decimal point. Figure 2 shows diagrammatically that input to the program consists of an initial "N" card which specifies the number of data decks to be run. Each Data Deck is composed of:

1. Three lead control cards which contain information concerning the data cards to follow.
2. Data cards containing one x y z coordinate triplet per card.
3. Link 1 and 2 control cards which specify contouring and plotting.

Control and Data Cards

"N" Card: The first card immediately following the source, object deck of // EXEC TRENMAIN which specifies the number of data decks (1 to 99) which are to be processed. This number is punched in columns 1 and 2 of the "N" card and is right justified.

Lead Control Cards:

Card 1: Begin in column one and punch:

ABCDEFGHIJKLMN OPQRSTUVWXYZ.0123456789*+-

Card 2: This card is a 79 character title card used to identify the data being processed. It is repeated in each section of the output. Column one is blank and the title is placed in Columns 2-80.

Card 3: Column 1 Blank

Columns 2-4 contain the number of sets of x y z coordinates that are read in as data. This value may range from 1 to

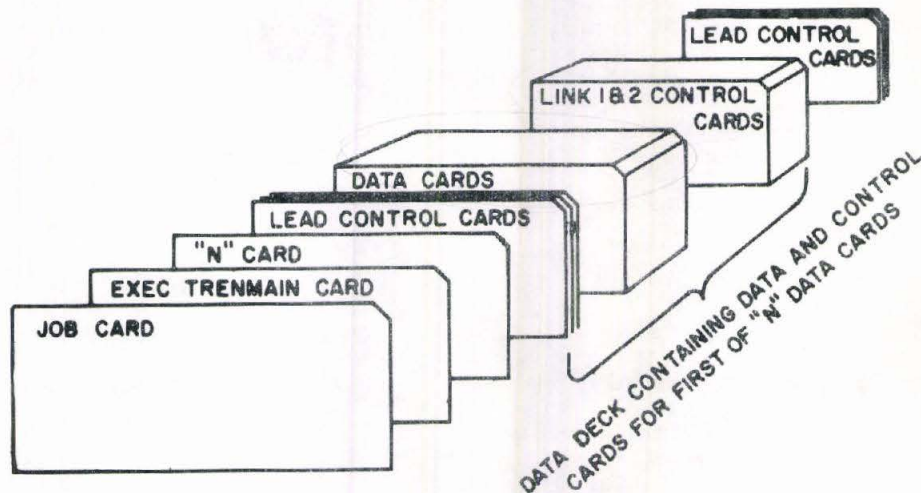


Figure 2.- Make-up of trend-surface program package

500 and must be right justified.

Column 5 Blank

Columns 6-11 contain the indicators for calculation of the first through sixth degree equations respectively. For each equation to be fitted to the data, a one (1) must be punched in the column assigned to that equation. Otherwise, that column must be punched zero or left blank.

Data Cards: The data cards contain the x y z coordinates of each control point (normally, one control point or coordinate triplet per card).

The x and y values define the location of cartesian coordinates of each control point, while the z value refers to the numerical value of the point itself. The x and y values may be scaled in inches and tenths of an inch, centimeters, or any convenient unit. To keep all x and y values positive, origin must be taken as the lower left-hand corner of the map.

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The number of points (cards) must agree with the number specified in columns 2-4 on card 3 of the lead control cards. The maximum number of points which may be handled by this program is 500. The minimum allowable number of points is determined by the highest order of trend surface to be computed. This minimum number may be computed by the formula

$$N = \frac{(P+1)(P+2)}{2}$$

where N is the minimum number of points allowable and P is the highest order of trend surface to be computed. Computation of a sixth-degree trend surface, for example, requires a minimum of 28 control points. Surfaces computed with a minimum number of control points are "trend" surfaces as the surface is not a best fit but an exact fit (i.e. the residuals are zero).

Location of the coordinate values on the data cards must be of the format: 1X,2F7.0,F8.0.

Link 1 and 2 control cards: The control cards described in this section specify printing of the contour maps (Link 1) and plotting of z values and residuals (Link 2). An option is provided whereby Link 2 is not called if residual or data plots are not desired.

Link 1

Card 1

Columns 1-5: Contain the total number of contour maps to be printed from this data deck. This value must be right justified.

Column 6: Blank

Column 7: Contains the option for Link 2. If plots of the z values and/or the residual values are desired,

✓

this column contains a 1 (one); otherwise, it must be a 0 (zero) or blank.

Card 2

This is the first of a set of M cards which contain the contouring parameters of each map to be contoured. (M is the number specified in columns 1-5 of card 1).

Column 1: Blank

Column 2: Contains the contour map indicator, MP, which designates the degree of the equation of the map to be contoured. If MP is 1, the first-degree is contoured; if 2, the second-degree surface is contoured, etc. This number cannot be larger than 6.

Column 3: Contains the orientation indicator, IOR. This variable controls the orientation of the printed map on the paper. If IOR is 1, the x axis is horizontal. If IOR is 2, the y axis is horizontal. If IOR is 3, the contoured map is oriented so that it occupies as much space as possible. For instance, if an interval of 10 units on the x axis and an interval of 5 units on the y axis is to be contoured, the map is oriented with the x axis vertical. If IOR is 4, the contoured map is oriented so that it occupies as little space as possible.

Column 4: Contains the plotting limit indicator, M3. If M3 is 1, the x-plotting interval is the interval between the maximum and minimum values of the X data array, and the y-plotting interval is the interval between the maximum and minimum values of the Y data array.

✓

If M3 is 0 (zero), the plotting limits are read in on a card that immediately follows this card (not this set of cards). These limits are on the card in the form:

Column 1: Blank

Columns 2-16: Contain the maximum x-plotting limit. If no decimal is punched it is assumed to be between columns 10 and 11.

Columns 17-31: Contain the minimum x-plotting limit. If no decimal point is punched, it is assumed to be between columns 25 and 26.

Columns 32-46: Contain the maximum y-plotting limit. If no decimal point is punched, it is assumed to be between columns 40 and 41.

Columns 47-61: Contain the minimum y-plotting limit. If no decimal point is punched, it is assumed to be between columns 55 and 56.

Column 5: Contains the card tabulator indicator, MT. If MT is 1, the output is to be listed at six lines per inch. If MT is 0 (zero) the output is to be listed at ten lines per inch.

√ Columns 6-9: Contain the program variable NCOL, which indicates the number of horizontal columns of output. The value of NCOL may range from 12-120 inclusive and must be right justified. The contour map occupies NCOL - 10 columns.

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Columns 10-19: Contain the program variable CON which is the contour interval of the contour map. This value must not be zero or negative. If no decimal point is punched, it is assumed to be between columns 17 and 18.

Columns 20-29: Contain the program variable REF which is the reference contour. This value regulates the placement of the reference symbol (.....) on the contour map. If no decimal point is punched, it is assumed to be between columns 27 and 28.

The remaining cards control the plotting of the original data and the residuals. If this output is not desired, column 7 of card 1 in the previous section must be zero or blank, and the following control cards are omitted.

Link 2

Card 1

Column 1-5 contain the total number of plots to be made. This value must be right justified.

Card 2

This is the first of a set of M cards that contain the plotting parameters for each set of values to be plotted. (M is the number specified on card 1).

Column 1: Blank

Column 2: Contains the residual plot indicator, MP. If MP is 0 (zero), the original data are plotted. If MP is 1, the first-degree residuals are plotted; if 2, the second-degree residuals are plotted, etc. This

indicator cannot be larger than 6.

Column 3: Contains the orientation indicator, IOR.
IOR has the same function here as described in Link 1,
card 2, column 3.

Column 4: Contains the plotting limit indicator, M3.
M3 has the same function here as described in Link 1,
card 2, column 4.

Column 5: Contains the card tabulator indicator, MT.
MT has the same function here as described in Link 1,
card 2, column 5.

Columns 6-9: Contain the value of the program variable
NCOL. NCOL has the same function here as described in
Link 1, card 2, columns 6-9 except that the value of
NCOL in Link 2 may range from 16-120 inclusive and the
plot occupies NCOL - 15 columns. (Note: for the con-
tour maps and the residual plots to have the same scale,
the value of NCOL for Link 2 should be four greater than
NCOL for a corresponding contour map in Link 1).

Comments

Each letter occupies approximately $\frac{1}{10}$ of an inch of space while each line
requires about $\frac{1}{6}$ of an inch. If output is listed at 6 lines per inch the verti-
cal scale is scaled to conform to actual dimensions. To calculate the number of
columns needed to produce "N" lines of map when the X coordinate is horizontal
substitute into the following:

$$\# \text{ Columns} = \frac{(1.666667)(\# \text{ Lines})(X_{\text{max}} - X_{\text{min}})}{y_{\text{max}} - y_{\text{min}}} + 11$$

For output at 10 lines per inch and X coordinate horizontal, # of columns may be

found by:

$$\# \text{ Columns} = \frac{(\# \text{ Lines})(X_{\text{max}} - X_{\text{min}})}{y_{\text{max}} - y_{\text{min}}} + 11$$

When the y axis is selected as the horizontal the above formulas apply if change in x and change in y are reversed. In this instance however the vertical increment is positive. This means that the vertical coordinates should increase in a negative direction from the lower left hand edge of the map area; otherwise the output does not properly represent data originally sealed as increasing positively in the x and y directions from this origin.

EXECUTION

The IBM 360 Model 40 requires that the FORTRAN program and data be punched with the Model 029 key punch. The program deck as received from the Kansas Geological Survey was punched with an 026 key punch. The University of Alaska computer center has written a "CONVERT" program which may be used each time the program is executed to correct differences between the two key punches. Therefore, changes in the original deck were made with the available key punch at the time of correction resulting in a mixed deck. Converted decks (029) can be produced by the computer center.

Compilation time for the entire program is approximately ten minutes. Object decks for each subroutine were therefore produced which eliminates this time each run. To execute the program at the University of Alaska under DOS, the following is needed:

1. Catalog on Core-Image Library

1 → // JOB CATALOG TREND PROGRAM
// OPTION CATAL
PHASE TRENMAIN, ROOT
2 → { INCLUDE
Object decks of
Mainline, RANGE, ALPHA, CHAIN

✓

```

/*
    PHASE TRENLNK1,*
    INCLUDE
    Object Decks of
    LINK1, T2, CONTUR, EMSLVR
    */
  
```

```

    PHASE TRENLNK2, TRENLNK1
    INCLUDE
    Object Decks of
    LINK2, ORDER3, PLOT3
    */
  
```

```

// EXEC LNKEDT
  
```

```

/&
  
```

2. Execute: (Scratch tapes on units 8, 9, 14)

```

1 // JOB TREND
2 // EXEC TRENMAIN
3 'N' Card
4 'Alphanumeric' Card
5 Lead Control Cards
6 Data
7 LINK1 and 2 Control Cards
  (Repeat 4,5,6,7 for more data)
8 /*
9 /&
  
```

The following is an example of input needed to execute the program. This data will produce all statistics mentioned, contour surfaces for first through fifth degree polynomials, a plot of original data and residual plots for each surface.

// JOB TREND 704 HEINER/WOLFF
// EXEC TRENMAIN

1
6 8 13 19 27
ABCDEFGHIJKLMN O PQRSTU VWXYZ.0123456789*+-
CLEARY HILL AREA A ZINC VALUES HEINER / WOLFF
53 111111

1.8	4.6	125
1.8	4.2	175
1.8	3.8	175
1.8	3.4	175
1.8	3.0	200
1.8	2.6	200
1.8	2.2	175
1.8	1.8	125
1.8	1.4	125
2.6	4.2	100
2.6	3.8	075
2.6	3.4	125
2.6	3.0	075
2.6	2.6	250
2.6	2.2	200
2.6	1.8	001
2.6	1.4	050
4.2	4.2	050
4.2	3.8	075
4.2	3.4	075
4.2	3.0	200
4.2	2.6	050
4.2	2.2	050
4.2	1.8	200
5.0	4.2	075
5.0	3.8	200
5.0	3.4	050
5.0	3.0	050
5.0	2.6	200
5.0	2.2	125
5.0	1.8	150
5.8	4.2	175
5.8	3.8	150
5.8	3.4	200
5.8	3.0	175
5.8	2.6	075
5.8	2.2	200
5.8	1.8	100
7.4	4.6	175
7.4	4.2	125
7.4	3.8	350
7.4	3.4	125
7.4	3.0	150
7.4	2.6	200
7.4	2.2	100
7.4	1.8	125
8.2	4.2	175
8.2	3.8	200
8.2	3.0	175
8.2	2.6	200
8.2	2.2	350
8.2	1.8	125
8.2	1.4	350

6 1
1101 91 25.0 175.0

1100 ↓
of analyzed

↓
Cuts

↓
Ref. Cont.

2101	91	9.0	0.0	5.0	0.0
		25.0	175.0		
3101	91	9.0	0.0	5.0	0.0
		25.0	175.0		
4101	91	9.0	0.0	5.0	0.0
		25.0	175.0		
5101	91	9.0	0.0	5.0	0.0
		25.0	175.0		
6101	91	9.0	0.0	5.0	0.0
		25.0	175.0		
		9.0	0.0	5.0	0.0
7					
0101	95				
		9.0	0.0	5.0	0.0
1101	95				
		9.0	0.0	5.0	0.0
2101	95				
		9.0	0.0	5.0	0.0
3101	95				
		9.0	0.0	5.0	0.0
4101	95				
		9.0	0.0	5.0	0.0
5101	95				
		9.0	0.0	5.0	0.0
6101	95				
		9.0	0.0	5.0	0.0

	COMMON NTAPE1,NTAPE2,NTAPE3,NTAPE4,NTAPE5,NTAPE6	
	DOUBLE PRECISION A(28,6)	MAIN 610
	COMMON A,DUMMY(1605),IPLOT	MAIN 620
	NTAPE1=8 10	
	NTAPE2=9 13	
	NTAPE3=14	
	NTAPE4 = 4	MAIN 580
	NTAPE5 = 5	MAIN 590
	NTAPE6=1	
	READ(1,102) J	
102	FORMAT(I2)	MAIN 650
	DO 5 KIK=1,J	MAIN 660
	CALL CHAIN (1)	MAIN 670
	IF(IPLOT) 5,5,4	MAIN 680
4	CALL CHAIN (2)	MAIN 690
5	CONTINUE	MAIN 700
	CALL EXIT	MAIN 710
	CALL RANGE(0,0,N,N)	MAIN 720
	END	MAIN 730
	 SUBROUTINE RANGE(LL,LU,N,NER)	RANG 010
C		RANG 020
C	RANGE DETERMINES WHETHER OR NOT N FALLS IN THE CLOSED	RANG 030
C	INTERVAL (LL,LU)	RANG 040
C		RANG 050
	NER = 0	RANG 060
	IF(LL - N) 5, 15, 10	RANG 070
5	IF (LU-N) 10, 15, 15	RANG 080
10	NER = 1	RANG 090
15	RETURN	RANG 100
	END	RANG 110
	 SUBROUTINE LINK1	
C	MODIFIED FOR ORDERS 4,5 AND 6 5/65 R.H. LIPPERT, M.T.O'LEARY	LINK 010
	COMMON NTAPE1,NTAPE2,NTAPE3,NTAPE4,NTAPE5,NTAPE6	
	DOUBLE PRECISION T(28,29),A(28,6),U(28)	
	COMMON A,X(500),Y(500),Z(500),JARBO(52),ID(40),MTD(6),N,	
1	SUMZ, FN, IP, DUMB(4)	LINK 050
	EQUIVALENCE (MTD(1), M5), (MTD(2), M6), (MTD(3), M7)	LINK 060
	EQUIVALENCE (MTD(4),M8), (MTD(5),M9), (T(1,1),A(1,1))	
C		LINK 080
C		LINK 090
C	-----	LINK 100
C	CREATE PLOTTING CHARACTERS	LINK 110

	READ(1,160) (JARBO(K),K=1,52)	
160	FORMAT(40A1,12A2)	
C		LINK 640
C	-----	LINK 650
C	READ IN DATA PARAMETERS	LINK 660
C	-----	LINK 670
	READ(1,20) (ID(I),I=1,40)	
20	FORMAT (1X, 39A2, A1)	LINK 690
	READ(1,95) N, (MTD(I),I=1,6)	
95	FORMAT (1X, I3, 1X, 6I1)	
C		LINK 710
C	-----	LINK 720
C	CHECK DATA PARAMETERS	LINK 730
C	-----	LINK 740
	NERR = 0	LINK 750
	CALL RANGE(1,500,N ,NKR)	LINK 760

	KAW=1	LINK 770
	IF(NKR) 600, 600, 700	LINK 780
C		LINK 790
	600 CALL RANGE(0,1,M5,NKR)	LINK 800
	KAW=2	LINK 810
	IF(NKR) 605, 605, 700	LINK 820
	605 CALL RANGE(0,1,M6,NKR)	LINK 830
	KAW=3	LINK 840
	IF(NKR) 610, 610, 700	LINK 850
C		LINK 860
	610 CALL RANGE(0,1,M7,NKR)	LINK 870
	KAW=4	LINK 880
	IF(NKR) 615, 615, 700	LINK 890
C		LINK 900
	615 CALL RANGE(0,1,M8,NKR)	LINK 910
	KAW=5	LINK 920
	IF(NKR)616,616,700	LINK 930
C		LINK 940
	616 CALL RANGE(0,1,M9,NKR)	LINK 950
	KAW=6	LINK 960
	IF(NKR)618,618,700	LINK 970
	618 CALL RANGE (0,1,MTD(6),NKR)	LINK 980
	KAW = 7	LINK 990
C		LINK1000
	620 IA = MTD(1) + MTD(2) + MTD(3)+MTD(4)+MTD(5) + MTD(6)	LINK1010
	KAW = 8	LINK1020
	IF (IA) 700, 700, 710	LINK1030
C		LINK1040
	700 WRITE(3,705) KAW	LINK1060
	705 FORMAT (1X, 13HPROGRAM ERROR I3)	LINK1070
	NERR = 1	LINK1080
	GO TO (600,605,610,615,616, 618,620,706),KAW	LINK1090
C		LINK1100
	710 IF(NERR) 100, 100, 706	
	706 WRITE(3,707)	
	707 FORMAT(13HINVALID DATA)	LINK1120
	CALL EXIT	LINK1130
C		LINK1140
	-----	LINK1150
C	READ IN XYZ-COORDINATES	LINK1160
C	-----	
	100 READ(1,105) (X(I),Y(I),Z(I),I=1,N)	
	105 FORMAT(1X,2F7.0,F8.0)	
C		LINK1210
	-----	LINK1220
C	CALCULATE COEFFICIENT MATRIX AND COLUMN VECTOR	LINK1230
C	-----	LINK1240
	I=7	LINK1250
	107 I = I - 1	LINK1260
	IF(MTD(I) - 1) 107, 108, 108	LINK1270
	108 L = I	LINK1280
C		LINK1290
	SELECT ORDER OF LARGEST COEFFICIENT MATRIX TO BE GENERATED	LINK1300
C		LINK1310
	GO TO (121, 122, 123,125,126, 127),L	LINK1320
	121 MM = 3	LINK1330
	GO TO 124	LINK1340
	122 MM = 6	LINK1350
	GO TO 124	LINK1360
	123 MM = 10	LINK1370
	GO TO 124	LINK1380
	125 MM=15	

GO TO 124	LINK1390
126 MM=21	LINK1400
GO TO 124	LINK1410
127 MM = 28	LINK1420
124 MM1 = MM + 1	LINK1430
C	LINK1440
STASH COORDINATE DATA ON TAPE	LINK1450
C	LINK1460
REWIND NTAPE2	LINK1470
DO 9998 I=1,N	LINK1480
9998 WRITE(NTAPE2) X(I), Y(I), Z(I)	LINK1490
REWIND NTAPE2	LINK1500
REWIND NTAPE3	LINK1510
C	LINK1520
ZERO COEFFICIENT MATRIX AND COLUMN VECTOR	LINK1530
C	LINK1540
DO 10 I = 1,MM,1	LINK1550
DO 10 J = 1,MM1,1	LINK1560
10 T(I,J) = 0.0	LINK1570
C	LINK1580
DO 185 I = 1,N,1	LINK1590
C	LINK1600
PICK UP X,Y,Z COORDINATES ONE AT A TIME	LINK1610
C	LINK1620
READ(NTAPE2) P,Q,R	LINK1630
U(1) = 1.	LINK1640
U(2) = P	LINK1650
U(3) = Q	LINK1660
C	LINK1670
IF (L - 2) 117, 115, 115	LINK1680
115 U(4) = P*P	LINK1690
U(5) = P*Q	LINK1700
U(6) = Q*Q	LINK1710
C	LINK1720
IF (L - 3) 117, 116, 116	LINK1730
116 U(7) = U(4) * P	LINK1740
U(8) = U(4) * Q	LINK1750
U(9) = P * U(6)	LINK1760
U(10) = U(6) * Q	LINK1770
C	LINK1780
IF(L-4)117,111,111	LINK1790
111 U(11)=U(7)*P	LINK1800
U(12)=U(7)*Q	LINK1810
U(13)=U(4)*U(6)	LINK1820
U(14)=U(2)*U(10)	LINK1830
U(15)=U(10)*Q	LINK1840
IF(L-5)117,112,112	LINK1850
112 U(16)=U(11)*P	LINK1860
U(17)=U(11)*Q	LINK1870
U(18)=U(12)*Q	LINK1880
U(19)=U(13)*Q	LINK1890
U(20)=U(14)*Q	LINK1900
U(21)=U(15)*Q	LINK1910
C	LINK1920
IF(L-6) 117,110,110	LINK1930
110 U(22) = U(16) * P	LINK1940
U(23) = U(16) * Q	LINK1950
U(24) = U(17) * Q	LINK1960
U(25) = U(18) * Q	LINK1970
U(26) = U(19) * Q	LINK1980

	U(27) = U(20) * Q	LINK1990
	U(28) = U(21) * Q	LINK2000
C		LINK2010
	117 DO 185 J = 1,MM,1	LINK2020
	T(J,MM1) = T(J,MM1) + U(J) * R	LINK2030
	DO 185 K=1,MM	LINK2040
	185 T(K,J)=T(K,J)+U(J)*U(K)	LINK2050
C		LINK2060
C		LINK2070
C		LINK2080
	SUMZ=T(1,MM1)	LINK2090
	FN=T(1,1)	LINK2100
C	-----	LINK2110
C	SOLVE MATRICES	LINK2120
C	-----	LINK2130
	IP = 0	LINK2140
	217 IF (IP - L) 218, 580, 580	LINK2150
	218 IP=IP+1	LINK2160
C		LINK2170
C		LINK2180
C		LINK2190
	GO TO (219,220,221,222,223, 224), IP	LINK2200
	219 M=3	LINK2210
	GO TO 234	LINK2220
	220 M=6	LINK2230
	GO TO 234	LINK2240
	221 M=10	LINK2250
	GO TO 234	LINK2260
	222 M=15	LINK2270
	GO TO 234	LINK2280
	223 M=21	LINK2290
	GO TO 234	LINK2300
	224 M = 28	LINK2310
	234 M1=M+1	LINK2320
C		LINK2330
C	SAVE COEFFICIENT MATRIX BEFORE ORDERING EMSLVR	LINK2340
C		LINK2350
	REWIND NTAPE1	LINK2360
	WRITE(NTAPE1) T	LINK2370
C		LINK2380
	DO 250 J = 1,M,1	LINK2390
	250 T(J,M1) = T(J,MM1)	LINK2400
	CALL EMSLVR(T,U,M,MAT)	LINK2410
C		LINK2420
C	REPLACE COEFFICIENT MATRIX IN CORE CONTINUE CALCULATIONS.	LINK2430
C		LINK2440
	REWIND NTAPE1	LINK2450
	READ(NTAPE1)T	LINK2460
C		LINK2470
	MTD(IP) = MTD(IP) + MAT	LINK2480
C		LINK2490
C	STASH CALCULATED COEFFICIENTS ON TAPE 3	LINK2500
C		LINK2510
	DO 260 J = 1,M,1	LINK2520
	260 WRITE(NTAPE3) U(J)	LINK2530
	GO TO 217	LINK2540
C	REPLACE X,Y,Z COORDINATES IN COMMON	LINK2550
C	*****	LINK2560
C	*****	LINK2570
	580 REWIND NTAPE2	LINK2580

	DU 9999 I=1,N	LINK2590
	9999 READ(NTAPE2)X(I),Y(I),Z(I)	LINK2600
C	CALL T2	LINK2610
<i>Return?</i>	CALL CHNXIT	LINK2620
	END	LINK2630
	SUBROUTINE EMSLVR (A,ACOE,N,NPQ)	LINK2640
C	WILL ORDER THE MATRIX BEFORE EACH ELIMINATION IF	EMSL 010
C	MORDER=+1	EMSL 020
C	N= ORDER OF MATRIX	EMSL 030
C	WILL SOLVE AN (N)X(N+1) MATRIX	EMSL 040
C	REQUIRES MATRICES OF THE FORM (A)X(COE)=(B)	EMSL 050
C	ACOE=VARIABLES TO BE SOLVED FOR	EMSL 060
C	A(I,J)= MATRIX ENTRIES	EMSL 070
C	COLUMN (I,N+1) OF THE A MATRIX CORRESPONDS TO	EMSL 080
C	COLUMN MATRIX B	EMSL 090
C	DIMENSIONED VARIABLES MUST BE AT LEAST OF ORDER N	EMSL 100
C	OR N+1 AS SHOWN BELOW	EMSL 110
C	DIMENSION A(N,N+1), IC(N), COE(N+1), ACOE(N)	EMSL 120
C	ANSWERS TO SINGULAR MATRICES ARE ZERO(0)	EMSL 130
C	DOUBLE PRECISION A(28,29),ACOE(28),COE(29),AB,AX,AY,SUM	EMSL 140
	DIMENSION IC(28)	EMSL 150
	NPQ=1	EMSL 160
	12 NM=N	EMSL 170
	NN=0	EMSL 180
	KK=0	EMSL 190
	MM=0	EMSL 200
	NP1=N+1	EMSL 210
	NM1=N-1	EMSL 220
	DO 3 J=1,N	EMSL 230
	3 A(J,NP1)=-A(J,NP1)	EMSL 240
C	INITIALIZE SUBSCRIPT COLUMN	EMSL 250
	799 DO 800 J=1,N	EMSL 260
	800 IC(J)=J	EMSL 270
	KKK=0	EMSL 280
C	-----	EMSL 290
C	MATRIX ORDERING ROUTINE	EMSL 300
C	-----	EMSL 310
	999 KKK=KKK+1	EMSL 320
	AB=DABS(A(KKK,KKK))	EMSL 330
	IBIG=KKK	EMSL 340
	JBIG=KKK	EMSL 350
	DO 901 I=KKK,N	EMSL 360
	DO 901 J=KKK,N	EMSL 370
	IF(AB-DABS(A(I,J)))900,901,901	EMSL 380
	900 AB=DABS(A(I,J))	EMSL 390
	IBIG=I	EMSL 400
	JBIG=J	EMSL 410
	901 CONTINUE	EMSL 420
	910 DO 920 I=1, NP1	EMSL 430
	AX=A(KKK,I)	EMSL 440
	A(KKK,I)=A(IBIG,I)	EMSL 450
	920 A(IBIG,I)=AX	EMSL 460
	DO 930 J=1,N	EMSL 470
	AY=A(J,KKK)	EMSL 480
	A(J,KKK)=A(J,JBIG)	EMSL 490
	930 A(J,JBIG)=AY	EMSL 500
	940 IDUM=IC(KKK)	EMSL 510
	IC(KKK)=IC(JBIG)	EMSL 520
	IC(JBIG)=IDUM	EMSL 530
		EMSL 540

	IF(NM1-KKK) 71,71,999	EMSL 550
C	-----	EMSL 560
	71 CONTINUE	EMSL 570
	75 NN=NN+1	EMSL 580
	NNN=NN+1	EMSL 590
	MM=MM+1	EMSL 600
C	-----	EMSL 610
C	CHECK FOR SINGULAR MATRIX	EMSL 620
C	-----	EMSL 630
	IF (A(NN,NN)) 77,1700,77	EMSL 640
C	-----	EMSL 650
C	MATRIX SOLUTION ROUTINE	EMSL 660
C	-----	EMSL 670
	77 DO 81 I=NN,N	EMSL 680
	IF(A(I,NN))79,81,79	EMSL 690
	79 DO 80 J=NNN,NP1	EMSL 700
	A(I,J)=A(I,J)/A(I,NN)	EMSL 710
	80 CONTINUE	EMSL 720
	81 CONTINUE	EMSL 730
	KK=KK+1	EMSL 740
	IF(KK-NM1)85,85,100	EMSL 750
	85 DO 95 I=NNN,N	EMSL 760
	IF(A(I,NN))89,95,89	EMSL 770
	89 DO 90 J=NNN,NP1	EMSL 780
	A(I,J)=A(I,J)-A(NN,J)	EMSL 790
	90 CONTINUE	EMSL 800
	95 CONTINUE	EMSL 810
	91 IF(KK-NM1+1)92,92,75	EMSL 820
	92 KKK=MM	EMSL 830
	GO TO 999	EMSL 840
C	-----	EMSL 850
C	BACK SOLVE UPPER TRIANGULAR MATRIX	EMSL 860
C	-----	EMSL 870
	100 COE(NP1)=1.0	EMSL 880
	DO 110 K=1,NM	EMSL 890
	SUM=0.0	EMSL 900
	J=NP1-K	EMSL 910
	L=J+1	EMSL 920
	DO 109 I=L,NP1	EMSL 930
	109 SUM=SUM-A(J,I)*COE(I)	EMSL 940
	110 COE(J)=SUM	EMSL 950
C	-----	EMSL 960
C	REORDER ANSWER MATRIX	EMSL 970
C	-----	EMSL 980
	DO 1005 I=1,NM	EMSL 990
	K1=IC(I)	EMSL1000
	ACOE(K1)=COE(I)	EMSL1010
	1005 CONTINUE	EMSL1020
	WRITE(3,2)	
	DO 1599 J=1,NM	EMSL1040
	1599 WRITE(3,1) ACOE(J),J,IC(J)	
	1600 RETURN	
	1 FORMAT(1H E15.6,2I8)	EMSL1060
	2 FORMAT(1H037H VARIABLE IDENT ORDERED COL	EMSL1070
	14HUMNS)	EMSL1080
	1700 WRITE(3,10)	EMSL1090
	10 FORMAT(1H0,16H SINGULAR MATRIX)	EMSL1110
	NPQ=-1	EMSL1120
	1601 DO 1900 I=1,N	EMSL1130
	1900 ACOE(I)=0.	EMSL1140
	RETURN	EMSL1150
	END	EMSL1160

	SUBROUTINE T2	T2	010
	COMMON NTAPE1,NTAPE2,NTAPE3,NTAPE4,NTAPE5,NTAPE6		
C	PROGRAM - TREND SURFACE LINK 2	T2	030
C	LANGUAGE - FORTRAN IV	T2	040
C	COMPUTER - IBM 7040 16 K CORE	T2	050
C	PROGRAMMER - DONALD I GOOD	T2	060
C	DATE COMPLETED - APRIL 1964	T2	070
C	REVISED SEPT 1964 OWEN T SPITZ	T2	080
C	MODIFIED FOR ORDERS 4,5 AND 6 5/65 R.H. LIPPERT, M.T.O'LEARY	T2	090
C	FOR DOCUMENTATION SEE KANSAS GEOLOGICAL SURVEY SPECIAL	T2	100
C	DISTRIBUTION PUBLICATION 14 FOR 1620 VERSION	T2	110
C		T2	120
C		T2	130
	DOUBLE PRECISION A(28,6)	T2	140
	COMMON A,X(500),Y(500),Z(500),JARBO(52),ID(40),MTD(6),N,SUMZ,	T2	150
	IFN,XMAX,XMIN,YMAX,YMIN,IPL0T	T2	160
	DIMENSION IREFU(11),IREFL(26),RL(500),RQ(500),RC(500),VAR(6),	T2	170
	ISQ(6),TVAR(6),SD(6),DET(6),COR(6),RQR(500),RQN(500),RSX(500)	T2	180
	EQUIVALENCE(JARBO(1),IREFL(1)),(JARBO(27),IREFU(1))	T2	190
	EQUIVALENCE(X(1),RL(1),RQR(1)),(Y(1),RQ(1),RQN(1)),(XMAX,IP)		
C		T2	210
	DO 9997 K=1,6	T2	220
	DO 9997 J=1,28	T2	230
9997	A(J,K)=0.0	T2	240
	M=1	T2	250
	REWIND NTAPE3	T2	260
	DO 9998 K=1,IP	T2	270
	M=M+K+1	T2	280
	DO 9998 J=1,M	T2	290
9998	READ(NTAPE3) A(J,K)	T2	300
	XMAX = X(1)	T2	310
	XMIN = X(1)	T2	320
	YMAX = Y(1)	T2	330
	YMIN = Y(1)	T2	340
C	-----	T2	350
C	WRITE DATA ARRAYS ON INTERMEDIATE TAPE 1	T2	360
C	-----	T2	370
	REWIND NTAPE1	T2	380
	WRITE(NTAPE1) Z	T2	390
C	-----	T2	400
C	DETERMINE MAXIMUM AND MINIMUM VALUES OF X AND Y ARRAYS	T2	410
C	-----	T2	420
	DO 870 I=2,N,1	T2	430
	IF(XMAX-X(I))835,840,840	T2	440
835	XMAX = X(I)	T2	450
840	IF (XMIN - X(I))850,850,845	T2	460
845	XMIN = X(I)	T2	470
850	IF (YMAX - Y(I))855,860,860	T2	480
855	YMAX = Y(I)	T2	490
860	IF (YMIN - Y(I))870,870,865	T2	500
865	YMIN = Y(I)	T2	510
870	CONTINUE	T2	520
C	-----	T2	530
C	CALCULATE AND PUNCH TREND SURFACE Z-VALUES, RESIDUALS, AND	T2	540
C	ERROR TERMS	T2	550
C	-----	T2	560
	DO 321 I=1,6,1	T2	570
321	SQ(I)=0.0	T2	580
	ZSQ=0.0	T2	590
C		T2	600

	WRITE(3,319)								
	317	FORMAT (1H1 39A2, A1)						T2	620
	316	WRITE(3,317) (ID(I),I=1,40)							
	319	FORMAT (1H0 11H X-COORD 12H Y-COORD 12H Z-VALUE						T2	640
	319112H	1ST-SURF 12H 1ST-RESID 12H 2ND-SURF						T2	650
	212H	2ND-RESID 12H 3RD-SURF 12H 3RD-RESID)						T2	660
C		DO 465 I = 1,N,1						T2	670
C								T2	680
C								T2	690
		AX = X(I)						T2	700
		AY = Y(I)						T2	710
		AZ=Z(I)						T2	720
C								T2	730
		IF(MTD(1)) 10,10,5						T2	740
	5	Z1=A(1,1)+A(2,1)*AX+A(3,1)*AY						T2	750
		GO TO 15						T2	760
	10	Z1 = 0.0						T2	770
C								T2	780
								T2	790
	15	IF(MTD(2)) 17,17,16						T2	800
	16	ZQ1 = AX * (A(2,2) + A(4,2) * AX + A(5,2) * AY)						T2	810
		ZQ2=AY * (A(3,2) + A(6,2) * AY)						T2	820
		Z2= A(1,2) + ZQ1 + ZQ2						T2	830
		GO TO 18						T2	840
	17	Z2 = 0.0						T2	850
C								T2	860
								T2	870
	18	IF (MTD(3)) 20,20,19						T2	880
	19	ZC1 = AX * (A(2,3) + AX * (A(4,3) + A(7,3) * AX))						T2	890
		ZC2=AY * (A(3,3) + AY * (A(6,3) + A(10,3) * AY))						T2	900
		ZC3 = AX * AY * (A(5,3) + A(8,3) * AX + A(9,3) * AY)						T2	910
		Z3= A(1,3)+ZC1 + ZC2 + ZC3						T2	920
		GO TO 21						T2	930
	20	Z3 = 0.0						T2	940
C								T2	950
								T2	960
	21	IF(MTD(1))334, 334, 330						T2	970
	330	RL(I)=AZ-Z1						T2	980
		GO TO 335						T2	990
	334	RL(I) = 0.0						T2	1000
	335	IF (MTD(2)) 349, 349, 345						T2	1010
	345	RQ(I)=AZ-Z2						T2	1020
		GO TO 350						T2	1030
	349	RQ(I) = 0.0						T2	1040
	350	IF (MTD(3)) 364, 364, 360						T2	1050
	360	RC(I)=AZ-Z3						T2	1060
		GO TO 371						T2	1070
	364	RC(I) = 0.0						T2	1080
C								T2	1090
								T2	1100
	371	SQ(1)=SQ(1)+RL(I)*RL(I)						T2	1110
		SQ(2)=SQ(2)+RQ(I)*RQ(I)						T2	1120
		SQ(3)=SQ(3)+RC(I)*RC(I)						T2	1130
		ZSQ=ZSQ+AZ*AZ						T2	1140
C								T2	1150
	465	WRITE(3,470) AX,AY,AZ,Z1,RL(I),Z2,RQ(I),Z3,RC(I)						T2	1160
	470	FORMAT(1X,F11.3,8F12.3)						T2	1170
C								T2	1180
C								T2	1190
C		WRITE RESIDUAL ARRAYS ON INTERMEDIATE TAPE 1						T2	1200
C								T2	1210
		WRITE(NTAPE1) RL						T2	1220
		WRITE(NTAPE1) RQ						T2	1230

	WRITE(NTAPE1) RC	T2	1210
C		T2	1220
	REWIND NTAPE2	T2	1230
	DO 9292 I=1,N	T2	1240
9292	READ(NTAPE2) X(I),Y(I),Z(I)	T2	1250
416	WRITE(3,317) (ID(I),I=1,40)		
	WRITE(3,419)		
419	FORMAT (1H0 11H X-COORD 12H Y-COORD 12H Z-VALUE	T2	1280
419112H	4TH-SURF 12H 4TH-RESID 12H 5TH-SURF 12H 5TH-RESID	T2	1290
	212H 6TH-SURF 12H 6TH-RESID)	T2	1300
C		T2	1310
	DO 471 I = 1, N, 1	T2	1320
C		T2	1330
	AX = X(I)	T2	1340
	AY = Y(I)	T2	1350
	AZ=Z(I)	T2	1360
C		T2	1370
	IF (MTD(4)) 200,200,199	T2	1380
199	ZQR1 = AX*(A(2,4) + AX * (A(4,4) + AY * (A(8,4) + AY * A(13,4))))	T2	1390
	ZQR2 = AY*(A(3,4)+AX*A(5,4)+AY*(A(6,4) + AX*A(9,4)))	T2	1400
	ZQR3 = AX*AX*AX*(A(7,4) + AX *A(11,4) + AY*A(12,4))	T2	1410
	ZQR4 = AY *AY*AY*(A(10,4) + AX * A(14,4) + AY * A(15,4))	T2	1420
	Z4 = A(1,4) + ZQR1 + ZQR2 + ZQR3 + ZQR4	T2	1430
	GO TO 201	T2	1440
200	Z4 = 0.0	T2	1450
C		T2	1460
201	IF(MTD(5)) 203,203,202	T2	1470
202	ZQN1 = AX * (A(2,5)+AX*A(4,5)+AY*(A(5,5) + AX*A(8,5)))	T2	1480
	ZQN2 = AY * (A(3,5) + AY * (A(6,5) + AX * A(9,5)))	T2	1490
	ZQN3 = AX*AX*AY*AY*(A(13,5)+AX*A(18,5)+AY*A(19,5))	T2	1500
	ZQN4 = AX*AX*AX*(A(7,5)+AY*A(12,5)+AX*(A(11,5)+AX*A(16,5)+AY*A(17,5))	T2	1510
	ZQN5=AY*AY*AY*(A(10,5)+AX*A(14,5)+AY*(A(15,5)+AX*A(20,5)+AY*A(21,5))	T2	1520
	Z5 = A(1,5) + ZQN1 + ZQN2 + ZQN3 + ZQN4 + ZQN5	T2	1530
	GO TO 382	T2	1540
203	Z5 = 0.0	T2	1550
382	IF(MTD(6)) 384,384,383	T2	1560
383	Z61 = AX * (A(2,6) + AY * (A(5,6) + AX * A(8,6)) + AX * (A(4,6) +	T2	1570
	1 AX * A(7,6)))	T2	1580
	Z62 = AY * (A(3,6) + AY * (A(6,6) + AX * (A(9,6) + AX * A(13,6)) +	T2	1590
	1 AY * A(10,6)))	T2	1600
	Z63 = AY*AX*AX*AX* (A(12,6) + AX * (A(17,6) + AY * A(24,6)) + AY	T2	1610
	1 * (A(18,6) + AY * A(25,6)))	T2	1620
	Z64 = AX*AY*AY*AY* (A(14,6) + AX * A(19,6))	T2	1630
	Z65 = AX*AX*AX*AX* (A(11,6) + AX * (A(16,6) + AY * A(23,6) + AX *	T2	1640
	1 A(22,6)))	T2	1650
	Z66 = AY*AY*AY*AY* (A(15,6) + AX * (A(20,6) + AX * A(26,6) + AY *	T2	1660
	1A(27,6)) + AY * (A(21,6) + AY * A(28,6)))	T2	1670
	Z6 = A(1,6)+ Z61 + Z62 + Z63 + Z64 + Z65 + Z66	T2	1680
	GO TO 365	T2	1690
384	Z6 = 0.0	T2	1700
C		T2	1710
		T2	1720
365	IF(MTD(4))367,367,366	T2	1730
366	RQR(I)=AZ-Z4	T2	1740
	GO TO 368	T2	1750
367	RQR(I)=0.	T2	1760
368	IF(MTD(5))370,370,369	T2	1770
369	RQN(I)=AZ-Z5	T2	1780
	GO TO 385	T2	1790
		T2	1800

370	RQN(I)=0.0	T2	1810
385	IF(MTD(6)) 387,387,386	T2	1820
386	RSX(I) = AZ - Z6	T2	1830
	GO TO 381	T2	1840
387	RSX(I) = 0.0	T2	1850
381	SQ(4)=SQ(4)+RQR(I)*RQR(I)	T2	1860
	SQ(5)=SQ(5)+RQN(I)*RQN(I)	T2	1870
	SQ(6) = SQ(6) + RSX(I) * RSX(I)	T2	1880
C		T2	1890
471	WRITE(3,472) AX,AY,AZ,Z4,RQR(I),Z5,RQN(I),Z6,RSX(I)		
472	FORMAT(1X,F11.3,8F12.3)	T2	1910
C		T2	1920
	WRITE(NTAPE1)RQR	T2	1930
	WRITE(NTAPE1)RQN	T2	1940
	WRITE(NTAPE1)RSX	T2	1950
C		T2	1960
C	-----	T2	1970
C	CALCULATE ERROR MEASURES	T2	1980
C	-----	T2	1990
	TVARI=ZSQ-(SUMZ*SUMZ)/FN	T2	2000
	SN=N-1	T2	2010
	RSN=1./SN	T2	2020
C		T2	2030
	DO 520 I=1,6,1	T2	2040
	IF(MTD(I))500,500,480	T2	2050
C		T2	2060
480	SD(I)=SQRT (RSN*SQ(I))	T2	2070
	VAR(I)=TVARI-SQ(I)	T2	2080
	TVAR(I)=TVARI	T2	2090
	DET(I)=VAR(I)/TVARI	T2	2100
	IF(DET(I))485,490,490	T2	2110
C		T2	2120
485	COR(I)=-SQRT (-DET(I))	T2	2130
	GO TO 520	T2	2140
490	COR(I)=SQRT (DET(I))	T2	2150
	GO TO 520	T2	2160
C		T2	2170
500	SD(I)=0.0	T2	2180
	VAR(I)=0.0	T2	2190
	TVAR(I)=0.0	T2	2200
	DET(I)=0.0	T2	2210
	COR(I)=0.0	T2	2220
C		T2	2230
520	CONTINUE	T2	2240
C	-----	T2	2250
C	PUNCH EQUATIONS OF SURFACES	T2	2260
C	-----	T2	2270
	WRITE(3,317) (ID(I),I=1,40)		
C		T2	2290
	IF(MTD(1))40,40,35	T2	2300
35	WRITE(3,585)		
585	FORMAT(1H0 39HCOEFFICIENTS OF FIRST-DEGREE EQUATION)	T2	2320
	WRITE(3,595) (A(I,1),I=1,3)		
595	FORMAT (4H0Z = F15.5, 2H + F14.5, 4H X + F13.5, 2H Y)	T2	2340
C		T2	2350
40	IF(MTD(2))50,50,45	T2	2360
45	WRITE(3,605)		
605	FORMAT(1H0 39HCOEFFICIENTS OF SECOND-DEGREE EQUATION)	T2	2380
	WRITE(3,615) (A(I,2),I=1,6)		
615	FORMAT (4H0Z = F15.5, 2H + F14.5, 4H X + F13.5, 4H Y + F13.5,	T2	2400

	1 5H X2 + , F13.5, 5H XY + F13.5, 3H Y2)	T2	2410
C	50 IF(MTD(3)) 56, 56,55	T2	2420
	55 WRITE(3,625)	T2	2430
	625 FORMAT(1H0 39HCOEFFICIENTS OF THIRD-DEGREE EQUATION)	T2	2450
	WRITE(3,635) (A(I,3),I=1,10)		
	635 FORMAT (4H0Z = F15.5, 2H + F14.5, 4H X + F13.5, 4H Y + F13.5,	T2	2470
	1 5H X2 + , F13.5, 5H XY + F13.5, 5H Y2 +/F13.5, 5H X3 + F13.5,	T2	2480
	2 6H X2Y + , F13.5, 6H XY2 + F13.5, 3H Y3)	T2	2490
C		T2	2500
	56 IF(MTD(4))58,58,57	T2	2510
	57 WRITE(3,626)		
	626 FORMAT(1H0 39HCOEFFICIENTS OF FOURTH-DEGREE EQUATION)	T2	2530
	WRITE(3,627) (A(I,4),I=1,15)		
	627 FORMAT (4H0Z = F15.5, 2H + F14.5, 4H X + F13.5, 4H Y + F13.5,	T2	2550
	1 5H X2 + , F13.5, 5H XY + F13.5, 5H Y2 +/F13.5, 5H X3 + F13.5,	T2	2560
	2 6H X2Y + , F13.5, 6H XY2 + F13.5, 5H Y3 + F13.5, 5H X4 + F13.5,	T2	2570
	3 6H X3Y + /F13.5, 7H X2Y2 + F13.5, 7H XY3 + F13.5,3H Y4)	T2	2580
C		T2	2590
	58 IF(MTD(5)) 60, 60, 59	T2	2600
	59 WRITE(3,628)		
	628 FORMAT(1H0 39HCOEFFICIENTS OF FIFTH-DEGREE EQUATION)	T2	2620
	WRITE(3,629) (A(I,5),I=1,21)		
	629 FORMAT (4H0Z = F15.5, 2H + F14.5, 4H X + F13.5, 4H Y + F13.5,	T2	2640
	1 5H X2 + , F13.5, 5H XY + F13.5, 5H Y2 +/F13.5, 5H X3 + F13.5,	T2	2650
	2 6H X2Y + , F13.5, 6H XY2 + F13.5, 5H Y3 + F13.5, 5H X4 + F13.5,	T2	2660
	3 6H X3Y + /F13.5, 7H X2Y2 + F13.5, 7H XY3 + F13.5,7H Y4 +	T2	2670
	4F13.5,5H X5 + F13.5, 6H X4Y + F13.5, 7H X3Y2 + / F13.5,	T2	2680
	5 7H X2Y3 + F13.5, 6H XY4 + F13.5, 3H Y5)	T2	2690
C		T2	2700
	60 IF(MTD(6)) 640,640,61	T2	2710
	61 WRITE(3,630)		
	630 FORMAT(1H0 39HCOEFFICIENTS OF SIXTH-DEGREE EQUATION)	T2	2730
	WRITE(3,631) (A(I,6),I=1,28)		
	631 FORMAT (4H0Z = F15.5, 2H + F14.5, 4H X + F13.5, 4H Y + F13.5,	T2	2750
	1 5H X2 + , F13.5, 5H XY + F13.5, 5H Y2 +/F13.5, 5H X3 + F13.5,	T2	2760
	2 6H X2Y + , F13.5, 6H XY2 + F13.5, 5H Y3 + F13.5, 5H X4 + F13.5,	T2	2770
	3 6H X3Y + /F13.5, 7H X2Y2 + F13.5, 7H XY3 + F13.5,7H Y4 +	T2	2780
	4F13.5,5H X5 + F13.5, 6H X4Y + F13.5, 7H X3Y2 + / F13.5,	T2	2790
	5 7H X2Y3 + F13.5, 6H XY4 + F13.5, 5H Y5 + F13.5, 5H X6 + F13.5,	T2	2800
	66H X5Y + F13.5, 7H X4Y2 + / F13.5,7HX3Y3 + F13.5, 7H X2Y4 +	T2	2810
	7F13.5,6H XY5 + F13.5, 5H Y6)	T2	2820
C		T2	2830
C	-----	T2	2840
C	PUNCH ERROR MEASURES	T2	2850
C	-----	T2	2860
	640 WRITE(3,644)		
	644 FORMAT(1H0,/1H0,/1H0,/1H0,/1H0)	T2	2880
	WRITE(3,645) (SD(I),I=1,6),(VAR(I),I=1,6),(SQ(I),I=1,6)		
	645 FORMAT (1H0 29X, 14HERROR MEASURES / 1H0 7HSURFACE 25X, 12HFIRST-DT2	2900	
	1EGREE 2X, 13HSECOND-DEGREE,3X,12HTHIRD-DEGREE, 2X,13HFOURTH-DEGREE	T2	2910
	23X,12HFIFTH-DEGREE,2X,12HSIXTH-DEGREE /	T2	2920
	3 1H0 18HSTANDARD DEVIATION 11X, 6F15.2 /	T2	2930
	4/ 1H0 19HVARIATION EXPLAINED / 1X, 10HBY SURFACE 19X, 6E15.8 / 1HOT2	T2	2940
	523HVARIATION NOT EXPLAINED / 1X,10HBY SURFACE 19X, 6E15.8)	T2	2950
C		T2	2960
	WRITE(3,655) (TVAR(I),I=1,6),(DET(I),I=1,6),(COR(I),I=1,6)		
	655 FORMAT (1H0 15HTOTAL VARIATION 14X, 6E15.8 / 1H0 14HCOEFFICIENT OF	T2	2980
	1/ 1X, 13HDETERMINATION 16X, 6F15.8 / 1H0 14HCOEFFICIENT OF / 1X,	T2	2990
	211HCORRELATION 18X, 6F15.8)	T2	3000

C	-----	T2	3010
C	O'LEARY,S LEFT THUMB IS ON BACKWARDS.	T2	3020
C	-----	T2	3030
C	-----	T2	3040
C	READ IN NUMBER OF CONTOUR MAPS AND RESIDUAL INDICATOR	T2	3050
C	-----	T2	3060
	IK=0	T2	3070
	116 READ(1,117) NUMB,IPL0T		
	117 FORMAT (I5, 1X, I1)	T2	3090
	CALL RANGE(0, 1, IPL0T, I)	T2	3100
	IF(I)118,118,741	T2	3110
	741 KAW = 11	T2	3120
	WRITE(3,710) KAW		
	GO TO 720	T2	3140
C	-----	T2	3150
C	READ CONTOUR PARAMETERS	T2	3160
C	-----	T2	3170
	118 IK=IK+1	T2	3180
	IF(NUMB-1K)300,119,119	T2	3190
	119 READ(1,125) MP,IOR,M3,MT,NCOL,CON,REF		
	125 FORMAT (1X, 4I1, I4, 2F10.2)	T2	3210
C	-----	T2	3220
C	CHECK PLOTTING PARAMETERS FOR VALIDITY	T2	3230
C	-----	T2	3240
	NERR=0	T2	3250
	CALL RANGE (1,6,MP,NKR)	T2	3260
	KAW=13	T2	3270
	IF(NKR)700,700,705	T2	3280
	700 CALL RANGE(0,1,M3,NKR)	T2	3290
	KAW=14	T2	3300
	IF(NKR)715,715,705	T2	3310
	705 WRITE(3,710) KAW		
	710 FORMAT(1X, 13HPROGRAM ERROR I3)	T2	3330
	NERR=1	T2	3340
	IF(KAW-8)700,720,720	T2	3350
C	-----	T2	3360
	715 IF(NERR)730,730,720	T2	3370
	720 WRITE(3,725)		
	725 FORMAT (13HINVALID DATA)	T2	3390
	CALL EXIT	T2	3400
C	-----	T2	3410
	730 IF(M3)30,126,30	T2	3420
	126 READ(1,127) XPMAX,XPMIN,YPMAX,YPMIN		
	127 FORMAT (1X, 4F15.6)	T2	3440
	GO TO 107	T2	3450
C	-----	T2	3460
	30 XPMAX = XMAX	T2	3470
	XPMIN = XMIN	T2	3480
	YPMAX = YMAX	T2	3490
	YPMIN = YMIN	T2	3500
C	-----	T2	3510
	107 IF(MTD(MP)) 118, 118, 108	T2	3520
C	-----	T2	3530
C	PUNCH MAP TITLES AND CALL SUBROUTINE CONTUR	T2	3540
C	-----	T2	3550
	108 WRITE(3,317) (ID(I),I=1,40)		
C	-----	T2	3570
	GO TO (245, 255, 266, 299, 301, 302), MP	T2	3580
C	-----	T2	3590
	245 WRITE(3,251)		

251	FORMAT (1H0 32HCONTOURED FIRST-DEGREE SURFACE)	T2	3610
	GO TO 275	T2	3620
255	WRITE(3,261)		
261	FORMAT (1H0 32HCONTOURED SECOND-DEGREE SURFACE)	T2	3640
	GO TO 275	T2	3650
266	WRITE(3,271)		
271	FORMAT (1H0 32HCONTOURED THIRD-DEGREE SURFACE)	T2	3670
	GO TO 275	T2	3680
299	WRITE(3,281)		
281	FORMAT (1H0 32HCONTOURED FOURTH DEGREE SURFACE)	T2	3700
	GO TO 275	T2	3710
301	WRITE(3,291)		
291	FORMAT (1H0 32HCONTOURED FIFTH-DEGREE SURFACE)	T2	3730
	GO TO 275	T2	3740
302	WRITE(3,303)		
303	FORMAT (1H0 31HCONTOURED SIXTH-DEGREE SURFACE)	T2	3760
C		T2	3770
275	CALL CONTUR (MP, IOR, MT, NCOL, CON, REF, XPMAX, XPMIN, YPMAX,	T2	3780
	1 YPMIN, IREFU, IREFL, JKR)	T2	3790
	GO TO 118	T2	3800
C		T2	3810
300	REWIND NTAPE2	T2	3820
	DD 9324 I=1,N	T2	3830
9324	READ(NTAPE2) X(I),Y(I),Z(I)	T2	3840
	RETURN	T2	3850
	END	T2	3860
	SUBROUTINE CONTUR (LM, M2, MT, NCOL, R1, R2, XPMAX, XPMIN, YPMAX,	CONT	010
	1 YPMIN, IREFU, IREFL, KERR)	CONT	020
	COMMON NTAPE1, NTAPE2, NTAPE3, NTAPE4, NTAPE5, NTAPE6		
C		CONT	040
C	PROGRAM - SUBROUTINE CONTUR	CONT	050
C	LANGUAGE - FORTRAN II	CONT	060
C	PROGRAMMER - DONALD I GOOD	CONT	070
C	DATE COMPLETED - APRIL 1964	CONT	080
C	MODIFIED FOR ORDERS 4,5 AND 6 5/65 R.H. LIPPERT, M.T.O'LEARY	CONT	090
C		CONT	100
C		CONT	110
C	DOUBLE PRECISION A(28,6)	CONT	120
	COMMON A, MAP(110), DUMMY(1496)	CONT	130
	DIMENSION IREFU(11), IREFL(26)	CONT	140
C	-----	CONT	150
C	CALCULATE X AND Y PLOTTING DIMENSIONS	CONT	160
C	-----	CONT	170
	DX = XPMAX - XPMIN	CONT	180
	DY = YPMAX - YPMIN	CONT	190
	NC = NCOL - 11	CONT	200
	FNC = NC	CONT	210
	NC = NC + 1	CONT	220
C	-----	CONT	230
C	CHECK ARGUMENTS	CONT	240
C	-----	CONT	250
	KERR=0	CONT	260
C		CONT	270
	CALL RANGE(1,6,LM,NKR)	CONT	280
	KEW=1	CONT	290
	IF(NKR)5,5,50	CONT	300
C		CONT	310
5	CALL RANGE(1,4,M2,NKR)	CONT	320
	KEW=2	CONT	330
	IF(NKR)10,10,50	CONT	340

C	10 CALL RANGE(0,1,MT,NKR)	CONT 350
	KEW=3	CONT 360
	IF(NKR)15,15,50	CONT 370
C	15 CALL RANGE(12,120,NCOL,NKR)	CONT 380
	KEW=4	CONT 390
	IF(NKR)20,20,50	CONT 400
C	20 IF(R1)25,25,30	CONT 410
	25 KEW=5	CONT 420
	GO TO 50	CONT 430
C	30 IF(DX)35,35,40	CONT 440
	35 KEW=6	CONT 450
	GO TO 50	CONT 460
C	40 IF(DY)45,45,125	CONT 470
	45 KEW=7	CONT 480
C	50 WRITE(3,55) KEW	CONT 490
	55 FORMAT (1X, 23HSUBROUTINE CONTUR ERROR I2, 49H, YOUR CONTROL CAR	CONT 500
	IDS ARE PROBABLY ALL ////ED UP.)	CONT 510
	KERR=1	CONT 520
	GO TO (5,10,15,20,30,40,574),KEW	CONT 530
C	125 IF(KERR)130,130,574	CONT 540
C	-----	CONT 560
C	PUNCH PLOTTING LIMITS	CONT 570
C	-----	CONT 580
C	130 WRITE(3,60) XPMAX,XPMIN,YPMAX,YPMIN	CONT 590
	60 FORMAT (1H0 15HPLOTTING LIMITS / 1X, 11HMAXIMUM X = F15.6, 5X,	CONT 600
	1 11HMINIMUM X = F15.6/ 1X, 11HMAXIMUM Y = F15.6, 5X,	CONT 610
	2 11HMINIMUM Y = F15.6)	CONT 620
C	-----	CONT 630
C	CHOOSE ORIENTATION	CONT 640
C	-----	CONT 660
C	GO TO (135, 165, 195, 196), M2	CONT 670
C	135 EXL = XPMIN	CONT 680
	EXR = XPMAX	CONT 690
	EXT = YPMAX	CONT 700
	EXB = YPMIN	CONT 710
	M6 = 0	CONT 720
	GO TO 200	CONT 730
C	165 EXL = YPMIN	CONT 740
	EXR = YPMAX	CONT 750
	EXT = XPMIN	CONT 760
	EXB = XPMAX	CONT 770
	M6 = 1	CONT 780
	GO TO 200	CONT 790
C	195 IF (DX - DY) 135, 135, 165	CONT 800
	196 IF (DX - DY) 165, 135, 135	CONT 810
C	-----	CONT 820
C	CALCULATE VERTICAL AND HORIZONTAL PLOTTING INCREMENTS	CONT 830
C	-----	CONT 840
C	200 HINC = (EXR - EXL) / FNC	CONT 850
C		CONT 860
		CONT 870
		CONT 880
		CONT 890
		CONT 900
		CONT 910
		CONT 920
		CONT 930
		CONT 940

	IF (MT) 201, 202, 201	CONT 950
	201 VINC = HINC * 1.6666667	CONT 960
	GO TO 214	CONT 970
	202 VINC = HINC	CONT 980
C		CONT 990
	214 IF (M6) 220, 215, 220	CONT1000
	215 VINC = - VINC	CONT1010
C	-----	CONT1020
C	PUNCH MAP PARAMETERS AND SCALES	CONT1030
C	-----	CONT1040
	220 IF (M6) 300, 280, 300	CONT1050
	280 WRITE(3,285) EXL,HINC	
	285 FORMAT (1H0 21HX-SCALE IS HORIZONTAL / 1X, 9HX-VALUE = F8.2,	CONT1070
	1 2H + F8.4, 16H X (SCALE VALUE))	CONT1080
	WRITE(3,295)	
	295 FORMAT (1H0 19HY-SCALE IS VERTICAL)	CONT1100
	GO TO 320	CONT1110
	300 WRITE(3,305) EXL,HINC	
	305 FORMAT (1H0 21HY-SCALE IS HORIZONTAL / 1X, 9HY-VALUE = F8.2,	CONT1130
	1 2H + F8.4, 16H X (SCALE VALUE))	CONT1140
	WRITE(3,315)	
	315 FORMAT (1H0 19HX-SCALE IS VERTICAL)	CONT1160
	320 WRITE(3,325) R1,R2	
	325 FORMAT (1H0 18HCONTOUR INTERVAL = F29.2/ 1X, 17HREFERENCE CONTOUR	CONT1180
	1 10H (.....) = F20.2)	CONT1190
C		CONT1200
	IF (NCOL - 80) 340, 340, 330	CONT1210
C		CONT1220
	330 WRITE(3,335)	
	335 FORMAT (1H0 9X, 10H0123456789 10H 123456789 10H 123456789	CONT1240
	3351 10H 123456789 10H 123456789 10H 123456789 2H 1	CONT1250
	2 8H23456789 10H 123456789 10H 123456789 10H 123456789	CONT1260
	3 10H 123456789 /)	CONT1270
	GO TO 344	CONT1280
C		CONT1290
	340 WRITE(3,341)	
	341 FORMAT (1H0 9X, 10H0123456789 10H 123456789 10H 123456789	CONT1310
	2 10H 123456789 10H 123456789 10H 123456789 10H 123456789 /)	CONT1320
C	-----	CONT1330
C	CHOOSE CHARACTERS FOR LINE BY LINE PLOTTING	CONT1340
C	-----	CONT1350
	344 VERT = EXT - VINC	CONT1360
C		CONT1370
C	INCREMENT VERTICAL INDEX BY ONE LINE	CONT1380
C		CONT1390
	345 VERT = VERT + VINC	CONT1400
C		CONT1410
C	ZERO PLOTTING ARRAY, MAP	CONT1420
C		CONT1430
	DO 347 I = 1,NC,1	CONT1440
	347 MAP(I)=IREFU(26)	CONT1450
C		CONT1460
	HOR = EXL - HINC	CONT1470
	I = 0	CONT1480
C		CONT1490
C	INCREMENT HORIZONTAL INDEX BY ONE	CONT1500
C		CONT1510
	352 I = I + 1	CONT1520
	HOR = HOR + HINC	CONT1530
C		CONT1540

C	DETERMINE X AND Y VALUES OF THE PLOTTING POSITION	CONT1550
C		CONT1560
	IF (M6) 380, 365, 380	CONT1570
365	AX = HOR	CONT1580
	AY = VERT	CONT1590
	GO TO 390	CONT1600
380	AX = VERT	CONT1610
	AY = HOR	CONT1620
C		CONT1630
C	SELECT PLOTTING FUNCTION AND CALCULATE VALUE OF SURFACE AT THE	CONT1640
C	PLOTTING POSITION	CONT1650
C		CONT1660
390	GO TO (395, 405, 415, 416, 417, 418),LM	CONT1670
C		CONT1680
395	C = A(1,1)+A(2,1)*AX+A(3,1)*AY	CONT1690
	GO TO 420	CONT1700
C		CONT1710
405	ZQ1 = AX * (A(2,2) + A(4,2) * AX + A(5,2) * AY)	CONT1720
	ZQ2=AY * (A(3,2) + A(6,2) * AY)	CONT1730
	C = A(1,2) + ZQ1 + ZQ2	CONT1740
	GO TO 420	CONT1750
C		CONT1760
415	ZC1 = AX * (A(2,3) + AX * (A(4,3) + A(7,3) * AX))	CONT1770
	ZC2=AY * (A(3,3) + AY * (A(6,3) + A(10,3) * AY))	CONT1780
	ZC3 = AX * AY * (A(5,3) + A(8,3) * AX + A(9,3) * AY)	CONT1790
	C = A(1,3)+ZC1 + ZC2 + ZC3	CONT1800
	GO TO 420	CONT1810
C		CONT1820
416	ZQR1 = AX*(A(2,4) + AX * (A(4,4) + AY * (A(8,4) + AY * A(13,4))))	CONT1830
	ZQR2 = AY*(A(3,4)+AX*A(5,4)+AY*(A(6,4) + AX*A(9,4)))	CONT1840
	ZQR3 = AX*AX*AX*(A(7,4) + AX *A(11,4) + AY*A(12,4))	CONT1850
	ZQR4 = AY *AY*AY*(A(10,4) + AX * A(14,4) + AY * A(15,4))	CONT1860
	C = A(1,4) + ZQR1 + ZQR2 + ZQR3 + ZQR4	CONT1870
	GO TO 420	CONT1880
C		CONT1890
417	ZQN1 = AX * (A(2,5)+AX*A(4,5)+AY*(A(5,5) + AX*A(8,5)))	CONT1900
	ZQN2 = AY * (A(3,5) + AY * (A(6,5) + AX * A(9,5)))	CONT1910
	ZQN3 = AX*AX*AY*AY*(A(13,5)+AX*A(18,5)+AY*A(19,5))	CONT1920
	ZQN4 = AX*AX*AX*(A(7,5)+AY*A(12,5)+AX*(A(11,5)+AX*A(16,5)+AY*A(17,	CONT1930
	15)))	CONT1940
	ZQN5=AY*AY*AY*(A(10,5)+AX*A(14,5)+AY*(A(15,5)+AX*A(20,5)+AY*A(21,5	CONT1950
	1)))	CONT1960
	C = A(1,5) + ZQN1 + ZQN2 + ZQN3 + ZQN4 + ZQN5	CONT1970
C		CONT1980
	GO TO 420	CONT1990
C		CONT2000
418	Z61 = AX * (A(2,6) + AY * (A(5,6) + AX * A(8,6)) + AX * (A(4,6) +	CONT2010
	1 AX * A(7,6)))	CONT2020
	Z62 = AY * (A(3,6) + AY * (A(6,6) + AX * (A(9,6) + AX * A(13,6))) +	CONT2030
	1 AY * A(10,6)))	CONT2040
	Z63 = AY*AX*AX*AX* (A(12,6) + AX * (A(17,6) + AY * A(24,6)) + AY	CONT2050
	1 * (A(18,6) + AY * A(25,6)))	CONT2060
	Z64 = AX*AY*AY*AY* (A(14,6) + AX * A(19,6))	CONT2070
	Z65 = AX*AX*AX*AX* (A(11,6) + AX * (A(16,6) + AY * A(23,6) + AX *	CONT2080
	1 A(22,6)))	CONT2090
	Z66 = AY*AY*AY*AY* (A(15,6) + AX * (A(20,6) + AX * A(26,6) + AY *	CONT2100
	1A(27,6)) + AY * (A(21,6) + AY * A(28,6)))	CONT2110
	C = A(1,6)+ Z61 + Z62 + Z63 + Z64 + Z65 + Z66	CONT2120
C		CONT2130
C	DETERMINE OF SURFACE VALUE LIES ABOVE OR BELOW REFERENCE CONTOUR	CONT2140
C	(DELZ IS + OR -)	CONT2150

C		CONT2160
	420 DELZ = C - R2	CONT2170
	IF (DELZ) 480, 421, 421	CONT2180
C		CONT2190
C	DETERMINE IF SURFACE VALUE LIES IN REFERENCE BAND	CONT2200
C		CONT2210
	421 IF (DELZ - R1) 425, 430, 430	CONT2220
	425 MAP(I) = IREFU(1)	CONT2230
	GO TO 535	CONT2240
C		CONT2250
C	SCALE DELZ SO THAT IT FALLS IN RANGE OF PLOTTING SYMBOLS(IREFU)	CONT2260
C		CONT2270
	430 DELZ = DELZ - R1	CONT2280
	431 IF (DELZ - 20. * R1) 445, 435, 435	CONT2290
	435 DELZ = DELZ - 20. * R1	CONT2300
	GO TO 431	CONT2310
C		CONT2320
C	CHOOSE PLOTTING SYMBOL	CONT2330
C		CONT2340
	445 NOD = DELZ / R1	CONT2350
	J = -1	CONT2360
	K = 1	CONT2370
	460 J = J + 2	CONT2380
	K = K + 1	CONT2390
	IF (NOD - J) 535, 475, 460	CONT2400
	475 MAP(I) = IREFU(K)	CONT2410
	GO TO 535	CONT2420
C		CONT2430
C	SCALE DELZ SO THAT IT FALLS IN RANGE OF PLOTTING SYMBOLS(IREFL)	CONT2440
C		CONT2450
	480 DELZ = - DELZ	CONT2460
	485 IF (DELZ - 52. * R1) 500, 490, 490	CONT2470
	490 DELZ = DELZ - 52. * R1	CONT2480
	GO TO 485	CONT2490
C		CONT2500
C	CHOOSE PLOTTING SYMBOL	CONT2510
C		CONT2520
	500 NOD = DELZ / R1	CONT2530
	J = -1	CONT2540
	K = 0	CONT2550
	515 J = J + 2	CONT2560
	K = K + 1	CONT2570
	IF (NOD - J) 535, 530, 515	CONT2580
	530 MAP(I) = IREFL(K)	CONT2590
C		CONT2600
C	DETERMINE IF LAST HORIZONTAL POSITION HAS BEEN PROCESSED	CONT2610
C		CONT2620
	535 IF (I - NC) 352, 540, 540	CONT2630
C		CONT2640
C	PUNCH PLOTTING ARRAY	CONT2650
C		CONT2660
	540 WRITE(3,545) VERT,(MAP(I),I=1,NC)	CONT2680
	545 FORMAT(1X,F8.2,1X,62A1,48A1)	CONT2690
C		CONT2700
C	DETERMINE IF LAST LINE HAS BEEN PROCESSED	CONT2710
C		CONT2720
	IF (M6) 565, 560, 565	CONT2730
	560 IF (VERT - EXB) 570, 570, 345	CONT2740
	565 IF (VERT - EXB) 345, 570, 570	

C		CONT2750
C	PUNCH FINAL SCALES	CONT2760
C		CONT2770
C	570 IF (NCOL - 80) 571, 571, 572	CONT2780
C		CONT2790
C	571 WRITE(3,341)	
	GO TO 574	CONT2810
C	572 WRITE(3,335)	
C		CONT2830
C	574 RETURN	CONT2840
	END	CONT2850
	SUBROUTINE LINK2	
C	PROGRAM - TREND SURFACE LINK 2	LINK 010
C	LANGUAGE - FORTRAN IV	LINK 020
C	COMPUTER - IBM 7040 16 K CORE	LINK 030
C	PROGRAMMER - DONALD I GOOD	LINK 040
C	DATE COMPLETED - APRIL 1964	LINK 050
C	REVISED SEPT 1964 OWEN T SPITZ	LINK 060
C	MODIFIED FOR ORDERS 4,5 AND 6 5/65 R.H. LIPPERT, M.T.O'LEARY	LINK 070
C	FOR DOCUMENTATION SEE KANSAS GEOLOGICAL SURVEY SPECIAL	LINK 080
C	DISTRIBUTION PUBLICATION 14 FOR 1620 VERSION	LINK 090
C		LINK 100
C		LINK 110
	COMMON NTAPE1,NTAPE2,NTAPE3,NTAPE4,NTAPE5,NTAPE6	
	DOUBLE PRECISION A(28,6)	LINK 130
	DIMENSION JREF(12)	LINK 140
	COMMON A,X(500),Y(500),R(500),JARBO(52),ID(40),MTD(6),N,SUMZ, FN,	LINK 150
	IXMAX,XMIN,YMAX,YMIN,IPLLOT	LINK 160
	EQUIVALENCE(JARBO(28),JREF(3))	LINK 170
C		LINK 180
C	CHECK LINK 2 INDICATOR	LINK 190
C		LINK 200
	REWIND NTAPE1	LINK 210
	IF (IPLLOT - 1) 4, 5, 4	LINK 220
	4 KAW = 12	LINK 230
	WRITE(3,120) KAW	
	GO TO 105	LINK 250
C		LINK 260
	5 KN = N + 1	LINK 270
	IP = 0	LINK 280
C		LINK 290
C	CALCULATE PLOTTING SYMBOLS FOR SUBROUTINE PLOT3	LINK 300
	NOP=37	LINK 310
	JARBO(1)=JARBO(26)	LINK 320
	JARBO(27)=JARBO(40)	LINK 330
	JARBO(26)=JARBO(39)	LINK 340
C		LINK 350
C	READ IN PLOTTING PARAMETERS	LINK 360
C	-----	LINK 370
	READ(1,10) NUMB	
	10 FORMAT (I5)	LINK 390
C		LINK 400
	15 IP = IP + 1	LINK 410
	IF (NUMB - IP) 105, 19, 19	LINK 420
	19 READ(1,20) MP,IOR,M3,MT,NCOL	
	20 FORMAT (1X, 4I1, I4)	LINK 440
C		LINK 450
C	CHECK PARAMETERS FOR VALIDITY	LINK 460
C	-----	LINK 470
	NERR=0	LINK 480

CALL RANGE(0,6,MP,NKR)	LINK 490
KAW=9	LINK 500
IF(NKR)110,110,115	LINK 510
110 CALL RANGE(0,1,M3,NKR)	LINK 520
KAW=10	LINK 530
IF(NKR)125,125,115	LINK 540
115 WRITE(3,120) KAW	
120 FORMAT (1X, 13HPROGRAM ERROR I3)	LINK 560
NERR=1	LINK 570
IF(KAW-10)110,125,125	LINK 580
125 IF(NERR)25,25,130	LINK 590
130 WRITE(3,135)	
135 FORMAT(13HINVALID DATA)	LINK 610
CALL EXIT	LINK 620
C	LINK 630
25 IF(M3)40,30,40	LINK 640
30 READ(1,35) XPMAX,XPMIN,YPMAX,YPMIN	
35 FORMAT (1X, 4F15.6)	LINK 660
IF(ALPHA(NOP,MP))150,165,50	IF(NOP.EQ.MP) go to 165
40 XPMAX=XMAX	go to 50
XPMIN=XMIN	go to 50 include
YPMAX=YMAX	
YPMIN=YMIN	
C	LINK 690
50 IF (MP) 51, 52, 51	LINK 700
51 IF(MTD(MP))15,15,52	LINK 710
52 DX = XMAX - XMIN	LINK 720
DY = YMAX - YMIN	LINK 730
C *****	LINK 740
C REPLACE X,Y,Z COORDINATES IN COMMON	LINK 750
C *****	LINK 760
REWIND NTAPE2	LINK 770
DO 740 I=1,N	LINK 780
740 READ (NTAPE2) X(I),Y(I),R(I)	LINK 790
C -----	LINK 800
C PLACE RESIDUAL ARRAY FROM TAPE 1 INTO R ARRAY	LINK 810
C -----	LINK 820
NRD=MP+1	LINK 830
REWIND NTAPE1	LINK 840
DO 9976 ISQU=1,NRD	LINK 850
9976 READ(NTAPE1) R	LINK 860
GO TO (140, 145, 150, 155), IOR	LINK 870
140 CALL ORDER3(Y,X,R ,1,N,1)	LINK 880
K = 0	LINK 890
GO TO 165	LINK 900
145 CALL ORDER3(X,Y,R ,1,N,0)	LINK 910
K = 2	LINK 920
GO TO 165	LINK 930
150 IF (DX - DY) 140, 140, 145	LINK 940
155 IF (DX - DY) 145, 140, 140	LINK 950
C -----	LINK 960
C PUNCH MAP TITLES AND CALL PLOTTING SUBROUTINE PLOT3	LINK 970
C -----	LINK 980
165 WRITE(3,55) (ID(I),I=1,40)	LINK 990
55 FORMAT (1H1 39A2, A1)	LINK1000
C	LINK1010
IF (MP) 59, 60, 59	LINK1020
59 GO TO (70, 80, 90, 301, 303,305),MP	LINK1030
C	LINK1050
	LINK1060
	LINK1070
	LINK1080
	LINK1090

60	WRITE(3,65)	
65	FORMAT (1H0 37HPLOT OF ORIGINAL DATA (Z-COORDINATES))	LINK1110
	GO TO 160	LINK1120
C		LINK1130
70	WRITE(3,75)	
75	FORMAT (1H0 32HPLOT OF FIRST-DEGREE RESIDUALS)	LINK1150
	GO TO 160	LINK1160
C		LINK1170
80	WRITE(3,85)	
85	FORMAT (1H0 32HPLOT OF SECOND-DEGREE RESIDUALS)	LINK1190
	GO TO 160	LINK1200
C		LINK1210
90	WRITE(3,95)	
95	FORMAT (1H0 32HPLOT OF THIRD-DEGREE RESIDUALS)	LINK1230
	GO TO 160	LINK1240
C		LINK1250
301	WRITE(3,302)	
302	FORMAT (1H0 32HPLOT OF FOURTH-DEGREE RESIDUALS)	LINK1270
	GO TO 160	LINK1280
C		LINK1290
303	WRITE(3,304)	
304	FORMAT (1H0 32HPLOT OF FIFTH-DEGREE RESIDUALS)	LINK1310
C		LINK1320
	GO TO 160	LINK1330
305	WRITE(3,306)	
306	FORMAT (1H0 32HPLOT OF SIXTH-DEGREE RESIDUALS)	LINK1350
160	CALL PLOT3(X,Y,R,N, IOR, XPMAX, XPMIN, YPMAX, YPMIN, NCOL, MT, K, J, JREF, MELINK1360	
	1R, JARBO)	LINK1370
	NOP=MP	LINK1380
	GO TO 15	LINK1390
C		LINK1400
105	CONTINUE	LINK1410
	CALL CHNXIT	LINK1420
	END	LINK1430
	SUBROUTINE ORDER3(A,B,C,NF,NL,KD)	ORDE 010
	COMMON NTAPE1,NTAPE2,NTAPE3,NTAPE4,NTAPE5,NTAPE6	
C	PROGRAM - SUBROUTINE ORDER3	ORDE 030
C	LANGUAGE - FORTRAN II	ORDE 040
C	NECESSARY SUBROUTINES - RANGE	ORDE 050
C	COMPUTER - IBM 1620 60K CORE	ORDE 060
C	PROGRAMMER - DONALD I GOOD	ORDE 070
C	DATE COMPLETED - APRIL 1964	ORDE 080
C	MODIFIED FOR ORDERS 4,5 AND 6 5/65 R.H. LIPPERT, M.T.O'LEARY	ORDE 090
C		ORDE 100
C		ORDE 110
	DIMENSION A(500), B(500), C(500)	ORDE 120
C		ORDE 130
C	CALCULATE ORDERING PARAMETERS	ORDE 140
C		ORDE 150
	ND=NL-NF	ORDE 160
15	NP = NF + 1	ORDE 170
	NE = NL + 1	ORDE 180
C	-----	ORDE 190
C	ORDER ARRAYS IN ASCENDING ORDER ON A	ORDE 200
C	-----	ORDE 210
	DO 90 K = 1,ND,1	ORDE 220
C		ORDE 230
30	NE = NE - 1	ORDE 240
	AMAX = A(NF)	ORDE 250
	J = NF	ORDE 260
	DO 50 I = NP,NE,1	ORDE 270

	IF(AMAX - A(I)) 40, 50, 50	ORDE 280
	40 AMAX = A(I)	ORDE 290
	J = I	ORDE 300
	50 CONTINUE	ORDE 310
C		ORDE 320
	BAMAX=B(J)	ORDE 330
	CAMAX = C(J)	ORDE 340
C		ORDE 350
	A(J)=A(NE)	ORDE 360
	B(J)=B(NE)	ORDE 370
	C(J)=C(NE)	ORDE 380
C		ORDE 390
	A(NE) = AMAX	ORDE 400
	B(NE) = BAMAX	ORDE 410
	C(NE) = CAMAX	ORDE 420
C		ORDE 430
	90 CONTINUE	ORDE 440
C		ORDE 450
C	INVERT ARRAYS IF DESCENDING ORDER IS DESIRED	ORDE 460
C		ORDE 470
	IF(KD) 110, 110, 100	ORDE 480
100	NS2 = (NL - NF + 1) / 2 + NF - 1	ORDE 490
	NT = NL + NF	ORDE 500
	DO 105 I = NF, NS2, 1	ORDE 510
	AMAX = A(I)	ORDE 520
	BAMAX = B(I)	ORDE 530
	CAMAX = C(I)	ORDE 540
	K = NT - I	ORDE 550
	A(I) = A(K)	ORDE 560
	B(I) = B(K)	ORDE 570
	C(I) = C(K)	ORDE 580
	A(K) = AMAX	ORDE 590
	B(K) = BAMAX	ORDE 600
105	C(K) = CAMAX	ORDE 610
110	RETURN	ORDE 620
	END	ORDE 630
C	PROGRAM - SUBROUTINE PLOT3	PLOT 010
C	LANGUAGE - FORTRAN IV	PLOT 020
C	NECESSARY SUBROUTINES - RANGE, ORDER3.	PLOT 030
C	COMPUTER - IBM 1620 60K CORE	PLOT 040
C	PROGRAMMER - DONALD I GOOD	PLOT 050
C	DATE COMPLETED - APRIL 1964	PLOT 060
C	REVISED SEPT 1964 OWEN T SPITZ	PLOT 070
C		PLOT 080
C		PLOT 090
	SUBROUTINE PLOT3(X,Y,Z,N, IOR, XMAX, XMIN, YMAX, YMIN, NCOL, MT, M1, M2, JREF	PLOT 100
	IF, NKR, JARBO)	PLOT 110
C		PLOT 120
	COMMON NTAPE1,NTAPE2,NTAPE3,NTAPE4,NTAPE5,NTAPE6	
	DIMENSION X(500),Y(500),Z(500), JREF(12),IER(150),ITAB(150),MAP(11	PLOT 140
	10),IZD(5),KTAB(150)	PLOT 150
	DIMENSION JARBO(52)	PLOT 160
C		PLOT 170
C	DETERMINE NUMBER OF CHARACTERS, NCC, IN PLOTTING ARRAY	PLOT 180
C		PLOT 190
	NZ=150	PLOT 200
	NCD=NCOL-10	PLOT 210
	NCC=NCD-5	PLOT 220
	FNC=NCC	PLOT 230
C		PLOT 240

C	CALCULATE PLOTTING DIMENSIONS	PLOT 250
C		PLOT 260
	DX=XMAX-XMIN	PLOT 270
	DY=YMAX-YMIN	PLOT 280
C	-----	PLOT 290
C	CHECK ARGUMENTS FOR VALIDITY	PLOT 300
C	-----	PLOT 310
	NKR=0	PLOT 320
	CALL RANGE(1,500,N,NAR)	PLOT 330
	KAR=1	PLOT 340
	IF(NAR)720,720,759	PLOT 350
C		PLOT 360
	720 CALL RANGE(1,4,IOR,NAR)	PLOT 370
	KAR=2	PLOT 380
	IF(NAR)725,725,759	PLOT 390
C		PLOT 400
	725 CALL RANGE(16,120,NCOL,NAR)	PLOT 410
	KAR=3	PLOT 420
	IF(NAR)730,730,759	PLOT 430
C		PLOT 440
	730 CALL RANGE(0,1,MT,NAR)	PLOT 450
	KAR=4	PLOT 460
	IF(NAR)735,735,759	PLOT 470
C		PLOT 480
	735 CALL RANGE(0,2,M1,NAR)	PLOT 490
	KAR=5	PLOT 500
	IF(NAR)740,740,759	PLOT 510
C		PLOT 520
	740 IF(DX)745,745,750	PLOT 530
	745 KAR=6	PLOT 540
	GO TO 759	PLOT 550
C		PLOT 560
	750 IF(DY)755,755,765	PLOT 570
	755 KAR=7	PLOT 580
	759 WRITE(3,760) KAR	
	760 FORMAT(1X, 22HSUBROUTINE PLOT3 ERROR I2)	PLOT 600
	NKR=1	PLOT 610
	GO TO (720,725,730,735,740,750,710),KAR	PLOT 620
	765 IF(NKR)5,5,710	PLOT 630
C	-----	PLOT 640
C	PUNCH PLOTTING LIMITS	PLOT 650
C	-----	PLOT 660
	5 WRITE(3,770) XMAX,XMIN,YMAX,YMIN	
	770 FORMAT (1H0 15HPLOTTING LIMITS / 1X, 11HMAXIMUM X = F15.6, 5X,	PLOT 680
	1 11HMINIMUM X = F15.6/ 1X, 11HMAXIMUM Y = F15.6, 5X,	PLOT 690
	2 11HMINIMUM Y = F15.6)	PLOT 700
C		PLOT 710
C	ZERO CARRIAGE CONTROL ARRAY FOR OVERPRINT VALUES	PLOT 720
C		PLOT 730
	DO 10 I=1,NZ,1	PLOT 740
	KTAB(I)=JARBO(52)	PLOT 750
	10 ITAB(I)=JARBO(52)	PLOT 760
C	-----	PLOT 770
C	SCALE PLOTTED VALUES TO 4-DIGIT MAXIMUM	PLOT 780
C	-----	PLOT 790
	AZMAX=ABS(Z(1))	PLOT 800
	DO 20 I=2,N,1	PLOT 810
	IF(AZMAX-ABS(Z(I))) 15,20,20	PLOT 820
	15 AZMAX=ABS(Z(I))	PLOT 830
	20 CONTINUE	PLOT 840

C	IF (AZMAX) 21, 66, 21	PLOT 850
	21 M=(ALOG(9999.0/AZMAX))/ALOG(10.0)	PLOT 860
	IF(M)30,66,40	PLOT 870
C		PLOT 880
	30 ND=-M	PLOT 890
	CON=0.1	PLOT 900
	GO TO 50	PLOT 910
C		PLOT 920
	40 ND=M	PLOT 930
	CON=10.0	PLOT 940
C		PLOT 950
	50 DO 60 I=1,ND,1	PLOT 960
	DO 60 J=1,N,1	PLOT 970
	60 Z(J)=Z(J)*CON	PLOT 980
C		PLOT 990
C	PUNCH SCALE FACTOR	PLOT1000
C		PLOT1010
C		PLOT1020
	61 WRITE(3,65) M	
	65 FORMAT (1H0 40HPLOTTED VALUES HAVE BEEN MULTIPLIED BY A 20H FACTOR	PLOT1040
	1 OF 10 TO THE 15, 6H POWER)	PLOT1050
C	-----	
C	SELECT MAP ORIENTATION, CALCULATE HORIZONTAL PLOTTING INCREMENTS.	PLOT1060
C	PUNCH PLOTTING PARAMETERS	PLOT1070
C	-----	
	66 GO TO (70,80,90,100),IOR	PLOT1080
C		PLOT1090
	70 EXT=YMAX	PLOT1100
	M3=0	PLOT1110
	HINC = DX / FNC	PLOT1120
	WRITE(3,75) XMIN,HINC	PLOT1130
	75 FORMAT (1H0 21HX-SCALE IS HORIZONTAL / 1X, 9HX-VALUE = F8.2, 2H +	PLOT1140
	1 F8.4, 16H X (SCALE VALUE) / 1H0 19HY-SCALE IS VERTICAL)	PLOT1160
	GO TO 110	PLOT1170
C		PLOT1180
	80 EXT=XMIN	PLOT1190
	M3=1	PLOT1200
	HINC = DY / FNC	PLOT1210
	WRITE(3,85) YMIN,HINC	PLOT1220
	85 FORMAT (1H0 21HY-SCALE IS HORIZONTAL / 1X, 9HY-VALUE = F8.2, 2H +	PLOT1240
	1 F8.4, 16H X (SCALE VALUE) / 1H0 19HX-SCALE IS VERTICAL)	PLOT1250
	GO TO 110	PLOT1260
C		PLOT1270
	90 IF(DX-DY)70,70,80	PLOT1280
	100 IF(DX-DY)80,70,70	PLOT1290
C		PLOT1300
C	PUNCH HORIZONTAL SCALE	PLOT1310
C		PLOT1320
	110 IF(NCOL-80)120,120,130	PLOT1330
C		PLOT1340
	120 WRITE(3,125)	
	125 FORMAT (1H0 9X, 10H0123456789 10H 123456789 10H 123456789 10H 1234	PLOT1360
	156789 10H 123456789 10H 123456789 10H 123456789 /)	PLOT1370
	GO TO 140	PLOT1380
C		PLOT1390
	130 WRITE(3,135)	
	135 FORMAT (1H0 9X, 10H0123456789 10H 123456789 10H 123456789 10H 1234	PLOT1410
	156789 10H 123456789 10H 123456789 2H 1 8H23456789 10H 12	PLOT1420
	23456789 10H 123456789 10H 123456789 10H 123456789 /)	PLOT1430
C		PLOT1440

C	CALCULATE VERTICAL PLOTTING INCREMENT	PLOT1450
C		PLOT1460
	140 IF(MT)160,150,160	PLOT1470
	150 VINC=HINC	PLOT1480
	GO TO 170	PLOT1490
	160 VINC=HINC*1.6666667	PLOT1500
C	-----	PLOT1510
C	PLOTTING ROUTINE	PLOT1520
C	-----	PLOT1530
C		PLOT1540
C	ORDER X, Y, AND Z ARRAYS ON ARRAY CORRESPONDING TO VERTICAL SCALE	PLOT1550
C		PLOT1560
	170 IF(M3)200,180,200	PLOT1570
C		PLOT1580
	180 VINC=-VINC	PLOT1590
	IF(M1-1)220,190,190	PLOT1600
	190 CALL ORDER3(Y,X,Z,1,N,1)	PLOT1610
	M2=0	PLOT1620
	GO TO 220	PLOT1630
C		PLOT1640
	200 IF(M1-1)210,210,220	PLOT1650
	210 CALL ORDER3(X,Y,Z,1,N,0)	PLOT1660
	M2=2	PLOT1670
C		PLOT1680
C	INITIALIZATION STEPS FOR PLOTTING	PLOT1690
C		PLOT1700
	220 PLIM=EXT	PLOT1710
	KER=0	PLOT1720
C		PLOT1730
C	DETERMINE INDEX OF FIRST DATA POINT THAT FALLS IN VERTICAL	PLOT1740
C	PLOTTING RANGE	PLOT1750
C		PLOT1760
	IF (M3) 805, 800, 805	PLOT1770
	800 IF (YMIN - Y(1)) 221, 221, 226	PLOT1780
	221 DO 222 I = 1,N,1	PLOT1790
	IF (YMAX - Y(I)) 222, 228, 228	PLOT1800
	222 CONTINUE	PLOT1810
	GO TO 226	PLOT1820
	805 IF (X(1) - XMAX) 223, 223, 226	PLOT1830
	223 DO 224 I = 1,N,1	PLOT1840
	IF (XMIN - X(I)) 228, 228, 224	PLOT1850
	224 CONTINUE	PLOT1860
	226 WRITE(3,227)	
	227 FORMAT (1X, 27HNO POINTS IN VERTICAL RANGE)	PLOT1880
	GO TO 650	PLOT1890
	228 NL = I - 1	PLOT1900
C		PLOT1910
C	CALCULATE UPPER (TOWARD TOP OF PAGE) BOUND OF VERTICAL PLOTTING	PLOT1920
C	INTERVAL	PLOT1930
C		PLOT1940
	225 VERT=PLIM	PLOT1950
C		PLOT1960
C	INCREMENT OVERPRINT INDEX. BLANK PLOTTING ARRAY	PLOT1970
C		PLOT1980
	KERF=KER+1	PLOT1990
	DO 230 I=1,NCD,1	PLOT2000
	230 MAP(I)=JARBO(52)	PLOT2010
C		PLOT2020
C	CALCULATE LOWER (TOWARD BOTTOM OF PAGE) BOUND OF VERTICAL PLOTTING	PLOT2030
C	INTERVAL	PLOT2040

C		PLOT2050
C	PLIM=VERT+VINC	PLOT2060
C		PLOT2070
C	DETERMINE INDEX OF NEXT DATA POINT, NF	PLOT2080
C		PLOT2090
C	NF=NL+1	PLOT2100
C	I=NL	PLOT2110
C		PLOT2120
C	SET UP VALUES FOR VERTICAL INTERVAL	PLOT2130
C		PLOT2140
C	IF(M3)270,240,270	PLOT2150
C		PLOT2160
C	COUNT NO. OF DATA POINTS IN VERTICAL PLOTTING INTERVAL	PLOT2170
C		PLOT2180
C	240 I=I+1	PLOT2190
C	IF (I - N) 245, 245, 250	PLOT2200
C	245 IF(Y(I)-PLIM)250,240,240	PLOT2210
C		PLOT2220
C	DETERMINE INDEX OF LAST DATA POINT IN VERTICAL PLOTTING INTERVAL,	PLOT2230
C	NL. ORDER DATA POINTS IN VERTICAL PLOTTING INTERVAL	PLOT2240
C		PLOT2250
C	250 NL=I-1	PLOT2260
C	IF(NL-NF)590,300,260	PLOT2270
C	260 CALL ORDER3(X,Y,Z,NF,NL,1)	PLOT2280
C	GO TO 300	PLOT2290
C		PLOT2300
C	COUNT NO. OF DATA POINTS IN VERTICAL PLOTTING INTERVAL	PLOT2310
C		PLOT2320
C	270 I=I+1	PLOT2330
C	IF (I - N) 275, 275, 280	PLOT2340
C	275 IF(X(I)-PLIM)270,270,280	PLOT2350
C		PLOT2360
C	DETERMINE INDEX OF LAST DATA POINT IN VERTICAL PLOTTING INTERVAL,	PLOT2370
C	NL. ORDER DATA POINTS IN VERTICAL PLOTTING INTERVAL	PLOT2380
C		PLOT2390
C	280 NL=I-1	PLOT2400
C	IF(NL-NF)590,300,290	PLOT2410
C	290 CALL ORDER3(Y,X,Z,NF,NL,1)	PLOT2420
C		PLOT2430
C	PLACE Z-VALUES FOR VERTICAL INTERVAL IN PLOTTING ARRAY FROM	PLOT2440
C	RIGHT TO LEFT	PLOT2450
C		PLOT2460
C	300 I = NF - 1	PLOT2470
C	305 I = I + 1	PLOT2480
C		PLOT2490
C	DETERMINE POSITION, IDX, IN PLOTTING ARRAY TO PLACE SIGN OF	PLOT2500
C	PLOTTED VALUE	PLOT2510
C		PLOT2520
C	IF(M3)320,310,320	PLOT2530
C	310 IDX=(X(I)-XMIN)/HINC + 1.0	PLOT2540
C	GO TO 330	PLOT2550
C	320 IDX=(Y(I)-YMIN)/HINC + 1.0	PLOT2560
C		PLOT2570
C		PLOT2580
C	DETERMINE IF PLOTTED VALUE LIES IN HORIZONTAL PLOTTING RANGE	PLOT2590
C		PLOT2600
C	330 IF(IDX) 580, 580, 334	PLOT2610
C	334 IF (IDX - NCC - 1) 335, 335, 580	PLOT2620
C		PLOT2630
C	DETERMINE IF THIS POSITION IN THE PLOTTING ARRAY IS ALREADY	PLOT2640
C	OCCUPIED	PLOT2650

C	335 IF(MAP(IDX)-JARBO(52)) 470,340,470	PLOT2660
C		PLOT2670
C	BREAK PLOTTED VALUE INTO 4 SEPARATE DIGITS AND CODE THESE DIGITS	PLOT2680
C	IN THE DOUBLE DIGIT CODE	PLOT2690
C		PLOT2700
C	340 LAZ=ABS(Z(I))	PLOT2710
	DVD=LAZ	PLOT2720
	DSR=10000.0	PLOT2730
	J=1	PLOT2740
C		PLOT2750
	350 J=J+1	PLOT2760
	DSR=DSR*0.1	PLOT2770
	K=DVD/DSR	PLOT2780
	IZD(J)=JREF(K+3)	PLOT2790
	FK=K	PLOT2800
	REM=DVD-FK*DSR	PLOT2810
	IF(J-4)360,370,370	PLOT2820
	360 DVD=REM	PLOT2830
	GO TO 350	PLOT2840
	370 K = REM	PLOT2850
	IZD(5) = JREF(K+3)	PLOT2860
C		PLOT2870
C	DETERMINE LEFT-MOST NON-ZERO DIGIT OF PLOTTED VALUE (EXCEPT ZERO)	PLOT2880
C		PLOT2890
	J=1	PLOT2900
	380 J=J+1	PLOT2910
	IF (J - 5) 385, 390, 390	PLOT2920
	385 IF(ALPHA(IZD(J),JARBO(28)))390,386,390 IF(IZD.NE.JARBO(28)) GO TO 390	PLOT2930
	386 IZD(J)=JARBO(52)	PLOT2950
	GO TO 380	PLOT2960
	390 K=J-1	PLOT2970
C		PLOT2980
C	PLACE SIGN OF PLOTTED VALUE	PLOT2990
C		PLOT3000
	IF(Z(I))400,410,410	PLOT3010
	400 IZD(K)=JREF(2)	PLOT3020
	GO TO 420	PLOT3030
	410 IZD(K)=JREF(1)	PLOT3040
C		PLOT3050
C	PLACE DIGITIZED VALUE IN PLOTTING ARRAY	PLOT3060
C		PLOT3070
	420 IMP=IDX-1	PLOT3080
	J = K - 1	PLOT3090
	430 J = J + 1	PLOT3100
	IF (J - 5) 435, 435, 580	PLOT3110
	435 IMP = IMP + 1	PLOT3120
	IF(MAP(IMP)-JARBO(52)) 450,440,450	PLOT3130
	440 MAP(IMP)=IZD(J)	PLOT3140
	GO TO 430	PLOT3150
C		PLOT3160
C	ERROR ROUTINE FOR OVERLAP PLOTTING	PLOT3170
C		PLOT3180
	450 MAP(IDX)=JARBO(38)	PLOT3190
	L=IDX+1	PLOT3200
	IMP = IMP - 1	PLOT3210
	J = IDX	PLOT3220
	455 J = J + 1	PLOT3230
	IF(J - IMP) 460, 460, 465	PLOT3240
	460 MAP(J)=JARBO(52)	PLOT3250
	GO TO 455	PLOT3260

C	465	KER=KER+1		PLOT3270
		IER(KER)=Z(I)		PLOT3280
		ITAB(KER)=JARBO(38)		PLOT3290
		GO TO 580		PLOT3300
C				PLOT3310
C		ERROR ROUTINES FOR MULTIPLE PLOTTING		PLOT3320
C				PLOT3330
C		CHECK FOR ASTERISK		PLOT3340
	470	IF(ALPHA(MAP(IDX),JARBO(38)))	471,510,471 IF(MAP(IDX).EQ.JARBO(38)) go to 510	PLOT3350
	471	DO 472 ICU=1,12		PLOT3370
		IF(ALPHA(MAP(IDX),JREF(ICU)))	472,473,472 IF(MAP(IDX).NE.JREF(ICU)) go to 472	
	473	IF(ICU-3)	490,530,530	PLOT3390
	472	CONTINUE		PLOT3400
		IF(ALPHA(MAP(IDX),JARBO(52)))	530,490,530 IF(MAP(IDX).NE.JARBO(52)) go to 530	
C				PLOT3420
C		*IF 2 VALUES ARE TO OCCUPY MAP(IDX)		PLOT3430
C				PLOT3440
	490	KER=KER+2		PLOT3450
		IER(KER-1)=Z(I-1)		PLOT3460
		IER(KER) = Z(I)		PLOT3470
		JAR=2		PLOT3480
		ITAB(KER)=JARBO(JAR)		PLOT3490
		JAM=2		PLOT3500
		MAP(IDX)=JARBO(JAM)		PLOT3510
		IMP=IDX		PLOT3520
	495	IMP=IMP+1		PLOT3530
		IF(ALPHA(MAP(IMP),JARBO(52)))	496,580,496 IF(MAP(IMP).EQ.JARBO(52)) go to 580	
	496	DO 499 IRE=3,12		
		IF(ALPHA(MAP(IMP),JREF(IRE)))	499,501,499 IF(MAP(IMP).EQ.JREF(IRE)) go to 501	
	499	CONTINUE		PLOT3570
		GO TO 580		PLOT3580
	501	MAP(IMP)=JARBO(52)		PLOT3590
		GO TO 495		PLOT3600
C				PLOT3610
C		IF MAP(IDX) IS OCCUPIED BY AN *		PLOT3620
C				PLOT3630
	510	KER=KER+1		PLOT3640
	520	IER(KER)=Z(I)		PLOT3650
		ITAB(KER-1)=JARBO(52)		PLOT3660
		JAR=2		PLOT3670
		ITAB(KER)=JARBO(JAR)		PLOT3680
		JAM=2		PLOT3690
		MAP(IDX)=JARBO(JAM)		PLOT3700
		GO TO 580		PLOT3710
C				PLOT3720
C		IF 3-9 VALUES ARE TO OCCUPY MAP(IDX)		PLOT3730
C				PLOT3740
	530	DO 531 ICU=2,9		PLOT3750
		IF(ALPHA(MAP(IDX),JARBO(ICU)))	531,532,531 IF(MAP(IDX).EQ.JARBO(ICU)) go to 532	
	531	CONTINUE		PLOT3770
		GO TO 550		PLOT3780
	532	JAR=ICU		PLOT3790
		JAM=ICU		PLOT3800
	540	JAM=JAM+1		PLOT3810
		MAP(IDX)=JARBO(JAM)		PLOT3820
		KER = KER + 1		PLOT3830
		JAR=JAR+1		PLOT3840

	ITAB(KER)=JARBO(JAR)	PLOT3850
	ITAB(KER-1)=JARBO(52)	PLOT3860
	IER(KER) = Z(I)	PLOT3870
	GO TO 580	PLOT3880
C		PLOT3890
C	IF MORE THAN 9 VALUES ARE TO OCCUPY MAP(IDX)	PLOT3900
C		PLOT3910
	550 MAP(IDX)=JARBO(1)	PLOT3920
	560 KER=KER+1	PLOT3930
	IER(KER)=Z(I)	PLOT3940
	ITAB(KER-1)=JARBO(52)	PLOT3950
	ITAB(KER)=JARBO(1)	PLOT3960
C		PLOT3970
C	DETERMINE IF FINAL VALUE FOR THIS VERTICAL PLOTTING INTERVAL	PLOT3980
C	IS PROCESSED	PLOT3990
C		PLOT4000
	580 IF(ALPHA(KER,NZ))581,581,920 <i>IF(KER.GT.NZ) go to 920</i>	
	581 IF(I-NL)305,590,590	
C		PLOT4030
C	PUNCH PLOTTING ARRAY	PLOT4040
C		PLOT4050
	590 WRITE(3,595) VERT,(MAP(I),I=1,NC0)	
	595 FORMAT(1X,F8.2,1X,62A1,48A1)	PLOT4070
C		PLOT4080
C	INVERT LIST OF OVERPRINT AND CARRIAGE CONTROL VALUES IN LAST	PLOT4090
C	VERTICAL PLOTTING INTERVAL	PLOT4100
C		PLOT4110
	IF (KER - KERF) 620, 601, 600	PLOT4120
601	KTAB(KER)=JARBO(28)	PLOT4130
	GO TO 620	PLOT4140
600	KTAB(KERF)=JARBO(28)	PLOT4150
	KF=(KER-KERF+1)/2+KERF-1	PLOT4160
	J=KER+KERF	PLOT4170
	DO 610 I=KERF,KF,1	PLOT4180
	IED=IER(I)	PLOT4190
	ITB=ITAB(I)	PLOT4200
	K=J-I	PLOT4210
	IER(I)=IER(K)	PLOT4220
	ITAB(I)=ITAB(K)	PLOT4230
	IER(K)=IED	PLOT4240
610	ITAB(K)=ITB	PLOT4250
C		PLOT4260
C	DETERMINE IF LAST VERTICAL PLOTTING INTERVAL IS PLOTTED	PLOT4270
C		PLOT4280
	620 IF(M3)640,630,640	PLOT4290
	630 IF(PLIM-YMIN)650,225,225	PLOT4300
	640 IF(PLIM-XMAX)225,225,650	PLOT4310
C		PLOT4320
C	PUNCH FINAL SCALE	PLOT4330
C		PLOT4340
	650 IF(NCOL-80)660,660,670	PLOT4350
	660 WRITE(3,125)	
	GO TO 680	
	670 WRITE(3,135)	PLOT4370
C		
C	PUNCH OVERPRINT VALUES	PLOT4390
C		PLOT4400
	680 IF(KER)710,710,690	PLOT4410
	690 WRITE(3,695)	PLOT4420
	695 FORMAT (1H0 16HOVERPRINT VALUES)	
	WRITE(3,700) (KTAB(I),ITAB(I),IER(I),I=1,KER)	PLOT4440

700 FORMAT(2A1, I6)
710 RETURN
920 WRITE(3,925)
925 FORMAT(1H0, 36HOVERPRINT VALUES HAVE EXCEEDED ARRAY,/
11H0, 29HPLOT OF THIS MAP DISCONTINUED)
RETURN
END

✓
PLOT4460
PLOT4470

PLOT4490
PLOT4500
PLOT4510
PLOT4520

col 1 col 10 col 16
↓

SUBROUTINE ALPHA

1 * FORTRAN FUNCTIONS TO COMPARE TWO FULL OR DOUBLE WORD ALPHABETIC
 2 * VARIABLES.
 3 * USAGE.. IF(ALPHA(A,B))1,2,3 FULL WORDS.
 4 * IF(DALPHA(A,B))1,2,3 DOUBLE WORDS.
 5 * THE IF STATEMENT WILL BRANCH TO 1 IF A IS ALPHABETICALLY BEFORE B
 6 * OR BRANCH TO 2 IF A IS THE SAME AS B, OR TO 3 IF A IS ALPHABETICALLY
 7 * AFTER B. ALPHABETIC SEQUENCE IS BLANK . (+ & \$ *) - / , [= ' ' =
 8 * A THRU Z AND 0 THRU 9. SEE S/360 MANUAL FOR OTHER CODES.

000000

000000

000000 9207 F01F

000004 47F0 F012

000008 4100 0008

00000C 1BF0

00000E 9203 F01F

000012 9023 D01C

000016 9823 1000

00001A 6800 F040

00001E D503 2000 3000 00000

000024 4720 F034

000028 4780 F032

00002C 2100

00002E 47F0 F034

000032 2800

000034 9823 D01C

000038 07FE

00003A 000000000000

000040 4110000000000000

000000

0001F

00012

00008

0001F

0001C

00000

00040

00000

00034

00032

00034

00034

0001C

0001C

0001C

9 COMALPHA START 0
 10 ENTRY DALPHA
 11 ENTRY ALPHA
 12 USING *,15
 13 DALPHA MVI COMPAR+1,X'07' SET FOR 8 BYTE COMPARE.
 14 B SAVE
 15 ALPHA LA 0,ALPHA-DALPHA DECREASE BASE REG
 16 SR 15,0 FOR 2ND ENTRY POINT.
 17 MVI COMPAR+1,X'03' SET FOR 4 BYTE COMPARE.
 18 SAVE STM 2,3,28(13) SAVE REG. 2 AND 3 IN CALLING PROG.
 19 LM 2,3,0(1) ADDR. OF A AND B TO REG. 2 AND 3.
 20 LD 0,ONE PUT 1. IN FP REG. 0.
 21 COMPAR CLC 0(4,2),0(3) COMPARE A WITH B.
 22 BH DONE QUIT IF A IS AFTER B.
 23 BE SAME
 24 LNDR 0,0 PUT -1. IN FP REG. 0 IF A BEFORE B.
 25 B DONE
 26 SAME SDR 0,0 PUT 0. IN FP REG. 0 IF A SAME AS B.
 27 DONE LM 2,3,28(13) RESTORE REG. 2 AND 3.
 28 BR 14 RETURN TO CALLING PROGRAM.
 29 ONE DC D'1.' FLOATING ONE.
 30 END DALPHA

PHASE FETCHING SUBROUTINE FOR TREND ANALYSIS PROG.

PAGE 1

DOS CL2-0 03/13/67

LOC	OBJECT CODE	ADDR1	ADDR2	STMT	SOURCE	STATEMENT
000000				2	CHAIN	START 0
				3		SAVE (14,12)
				4+*	360N-CL-453	SAVE CHANGE LEVEL 2-0
000000	90EC D00C		0000C	5+	STM	14,12,12+4*(14+2-(14+2)/16*16)(13)
000000				6	USING	CHAIN,15
000004	50D0 F078		00078	7	ST	13,R13
				8	LA	13,SAVE (TO AVOID OVERLAYING REGISTER STATUS INFORMATION STORED IN MAINLINE PROGRAM, FOR RETURN BY 'CHNXIT')
000008	41D0 F080		00080			
00000C	5821 0000		00000	9	L	2,0(1) GET ADDRESS OF OPERAND OF 'CHAIN'
000010	5822 0000		00000	10	L	2,0(2) GET OPERAND
000014	5920 F074		00074	11	C	2,CURRENT PHASE IS SAME AS NOW IN MEMORY
000018	4780 F060		00060	12	BE	BRANCH TO APPROPRIATE ENTRY POINT
00001C	5020 F074		00074	13	ST	2,CURRENT STORE CURRENT PHASE ID
000020	5920 F0D8		000D8	14	C	2,=F'2' IS LINK2 DESIRED
000024	4780 F03A		0003A	15	BE	FETCH2
				16	FETCH1	LOAD TRENLNK1
				17+*	360N-CL-453	LOAD CHANGE LEVEL 2-0
000028				18+FETCH1	DC	OH'0'
000028	4110 F0C8		000C8	19+	LA	1,=CL8'TRENLNK1'
00002C	1800			20+	SR	0,0
00002E	0A04			21+	SVC	4
000030	41D0 F080		00080	22	LA	13,SAVE TO ENSURE NO DESTRUCTION BY SAVE
000034	58F0 F0DC		000DC	23	L	15,=V(LINK1)
000038	07FF			24	BR	15
				25	FETCH2	LOAD TRENLNK2
				26+*	360N-CL-453	LOAD CHANGE LEVEL 2-0
				27+FETCH2	DC	OH'0'
00003A				28+	LA	1,=CL8'TRENLNK2'
00003A	4110 F0D0		000D0	28+	LA	1,=CL8'TRENLNK2'
00003E	1800			29+	SR	0,0
000040	0A04			30+	SVC	4
000042	41D0 F080		00080	31	LA	13,SAVE TO ENSURE NO DESTRUCTION BY SAVE
000046	58F0 F0E0		000E0	32	L	15,=V(LINK2)
00004A	07FF			33	BR	15
				35 *		RETURN TO MAINLINE
				36	CHNXIT	SAVE (14,12)
				37+*	360N-CL-453	SAVE CHANGE LEVEL 2-0
00004C	90EC D00C		0000C	38+CHNXIT	STM	14,12,12+4*(14+2-(14+2)/16*16)(13)
000050	4120 004C		0004C	39	LA	2,CHNXIT-CHAIN
000054	1BF2			40	SR	15,2
000056	58D0 F078		00078	41	L	13,R13
				42		RETURN (14,12)
				43+*	360N-CL-453	RETURN CHANGE LEVEL 2-0
00005A	98EC D00C		0000C	44+	LM	14,12,12+4*(14+2-(14+2)/16*16)(13)
00005E	07FE			45+	BR	14
				47	BRANCH	C 2,=F'2' IDENTIFY PHASE, GO TO ENTRYPOINT
000060	5920 F0D8		000D8	47	BRANCH	C 2,=F'2' IDENTIFY PHASE, GO TO ENTRYPOINT
000064	4780 F06E		0006E	48	BE	BRL2
000068	58E0 F0DC		000DC	49	L	14,=V(LINK1) PICK UP ENTRY POINT

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LOC	OBJECT CODE	ADDR1	ADDR2	STMT	SOURCE	STATEMENT
00006C	07FE			50	BR	14 BRANCH
00006E	58E0 F0E0		000E0	51	BRL2	L 14,=V(LINK2)
000072	07FE			52	BR	14
000074	00000000			53	CURRENT	DC F'0' LABEL OF CURRENTLY RETRIEVED PHASE OVERLAY
000078				54	R13	DS F
000080				55	SAVE	DS 9D
0000C8				56		LTORG
0000C8	E3D9C5D5D3D5D2F1			57		=CL8*TRENLNK1'
0000D0	E3D9C5D5D3D5D2F2			58		=CL8*TRENLNK2'
0000D8	00000002			59		=F*2'
0000DC	00000000			60		=V(LINK1)
0000E0	00000000			61		=V(LINK2)
				62	ENTRY	CHNXIT
				63	END	

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STORAGE MAP

03/13/67	PHASE	XFR-AD	LOCORE	HICORE	DSK-AD	ESD TYPE	LABEL	LOADED	REL-FR
COMMON						COM		002000	001E70
ROOT	TRENMAIN	003E70	003E70	005E2F	2D 3 1	CSECT	FORTMAIN	003E70	003E70
						CSECT	IJTACOM	004260	004260
						ENTRY	IJTSAVE	0047AC	
						CSECT	CHAIN	004130	004130
						ENTRY	CHNXIT	00417C	
						CSECT	IJTFXIT	005E18	005E18
						ENTRY	EXIT	005E1E	
						CSECT	RANGE	003FE8	003FE8
						CSECT	COMALPHA	004218	004218
						* ENTRY	DALPHA	004218	
						ENTRY	ALPHA	004220	
						CSECT	IJTACON	004AC0	004AC0
						* ENTRY	FCVFI	004AC0	
						* ENTRY	FCVFO	004AC4	
						* ENTRY	FCVEI	004AC8	
						* ENTRY	FCVEO	004ACC	
						* ENTRY	FCVII	004AD0	
						* ENTRY	FCVIO	004AD4	
						* ENTRY	FCVDI	004C68	
						* ENTRY	FCVDO	004E58	
						CSECT	IJTFIOS	005408	005408
						ENTRY	UNITABE	005C3E	
						ENTRY	DOIIOXE	005A3E	
						ENTRY	GETUNTE	0057B8	
						ENTRY	OPENUNE	005806	
						ENTRY	SETLGUE	0058FC	
						ENTRY	CCWNOIE	0058E0	
						ENTRY	DSKWTME	005ADC	
						* ENTRY	ASNBUE	005C7C	
						* ENTRY	FILTABE	005870	
						ENTRY	IJJCPD1N	005408	
TRENLNK1		005E30	005E30	00C1D7	2D 5 2	CSECT	LINK1	005E30	005E30
						CSECT	IJTARBE	00BE50	00BE50
						CSECT	IJTAAFR	00BD80	00BD80
						CSECT	EMSLVR	006B90	006B90
						CSECT	T2	007548	007548
						CSECT	IJTSSQT	00C130	00C130
						ENTRY	SQRT	00C136	

STORAGE MAP (Continued)

03/13/67	PHASE	XFR-AD	LOCORE	HICORE	DSK-AD	ESD TYPE	LABEL	LOADED	REL-FR
						CSECT	CONTUR	00AA38	00AA38
	TRENLNK2	005E30	005E30	0093D0	2E 3 1	CSECT	LINK2	005E30	005E30
						CSECT	IJTARBE	008FF0	008FF0
						CSECT	IJTAAFR	008F50	008F50
						CSECT	ORDER3	006770	006770
						CSECT	PLOT3	006AD0	006AD0
						CSECT	IJTSLOG	0092D0	0092D0
						ENTRY	ALOG	0092EE	
						* ENTRY	ALOG10	0092D8	

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SAMPLE PROGRAM OUTPUT

Program output is verbatim from Merriam (1966).

Output from the preceding sample data and control cards are listed below and on the following pages.

EXPLANATION OF OUTPUT

"Error measures for the various surfaces are computed from the following formulas:

The "TOTAL VARIATION," V , is given by

$$V = \sum_{i=1}^N (z_i - \bar{z})^2$$

where z_i is the i th z data coordinate,

$$\bar{z} = \frac{\sum_{i=1}^N z_i}{N}$$

V is calculated entirely from the input data and hence is the same for each surface.

The "VARIATION NOT EXPLAINED BY SURFACE," S , is given by

$$S = \sum_{i=1}^N (z_i \text{ observed} - z_i \text{ calculated})^2.$$

This value is obtained by squaring the appropriate order of residuals and summing.

The "VARIATION EXPLAINED BY SURFACE," E , is given by

$$E = V - S.$$

The "COEFFICIENT OF DETERMINATION," T , is given by

$$T = \frac{E}{V}.$$

The value E , and hence T , may be negative if S is sufficiently large. The "COEFFICIENT OF CORRELATION," L , is given by

$$L = T^{1/2}.$$

If T is negative, L also is output as a negative number (Spiegel, 1961, p. 252-253). The "STANDARD DEVIATION," D, is given by

$$D = \left(\frac{S}{N} \right)^{1/2}$$

where N is the number of sets of data coordinates. Each of these quantities is calculated for each surface. If the equation of a particular surface is not calculated, the corresponding error measures are printed as zeros.

The scale on the left edge of the contour map reads directly in terms of whichever scale is specified as vertical, but the horizontal scales do not read directly. On the horizontal scales, only the units digits of the scale values are shown; blanks in the scales represent increments of ten. For example, the left-most blank represents ten and the next blank to the right represents 20. After the reading is made on the horizontal scale, the reading must be substituted for "SCALE VALUE" in the formula for the horizontal scale. The value given by this substitution corresponds directly to the original units of the horizontal axis (x or y). Scales are positioned on contour maps so that any character on the map is in direct line with the scales both vertically and horizontally. Any given character is selected from a calculation of the value of the surface of the center of the small region in which the character is plotted.

Contours are read in the following manner. The reference contour runs along the "letter-edge" of the band of dots. From this reference contour each edge of each band of characters represents an increment of one contour interval -- the letter bands proceeding downward (A,B,C,.....) from the reference contour and the number bands upward (0,1,2,.....). Both letter and number bands feature "wrap-around" character selection. For example, if a surface reaches a greater value above the reference contour than can be contoured by using 10 different bands of digits, the next higher band of digits is a band of 0's, the next a band of 1's, the next a band of 2's, etc. The same is true of letter bands. The next band lower than Z is A, the next lower is B, etc. The character selection may "wrap around" any number of times, but the reference band is printed only once. A

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result of this "wrap-around" feature is that unless the reference band is printed on the contour map, the specific values represented by the other band are not uniquely determined by the character in the band.

Contour maps are printed in the order in which they are encountered in the input data for Link 1. If it is specified that a surface be contoured but the equation of that surface has not been determined, the contouring of that surface is bypassed.

The next section of output is the plotting of the original data and the first through sixth-degree residuals on the x y plane. Again, if a certain order of residual is specified to be plotted but the equation of the corresponding surface has not been determined, the plotting of these residuals is bypassed.

Each residual plot is also preceded by the program title, name of the plot, plotting limits, and orientation of the scales. The plots may contain one additional preliminary statement. The plotting routine is designed so that the number of digits in the largest plotted value is always four. If values to be plotted do not have this property, the entire set of values is multiplied successively either by 10 or 0.1 until this property is attained. If the plotted values are scaled, the scale factor is printed.

The scales for axes residual plots are interpreted somewhat differently from the scales of the contour maps. Conversion of the horizontal scale reading, however, is the same. The position of the plotted number is indicated by the sign of the number. A zero is preceded by a plus sign. In addition, the horizontal scale should be shifted half a space to the left, and the vertical scale half a line upward while the plotted values remain stationary. Thus the scales establish horizontal and vertical limits on the location of the sign of the number rather than defining a unique central position. These limits may be made as small as possible by enlarging the printing area. (It should be noted that by proper manual selection of plotting limits, the total width of the plots and contour maps may be made to occupy more than one page by specifying identical plots with adjacent plotting limits).

Several symbols other than numbers may occur on the plots. These are the "overprint characters;" their meaning is explained below.

- * An attempt was made to write a number, but before it was completed another number to the right was encountered.
- B Two numbers fall within the limits of the region of this position.
- C Three numbers fall within the limits of the region of this position.
- D Four numbers fall within the limits of the region of this position.
- .
- .
- .
- I Nine numbers fall within the limits of the region of this position.
- Z Ten or more numbers fall within the limits of the region of this position.

The "overprint characters" are printed on the plot, and the "OVERPRINT VALUES" that they represent are listed in a single column following the plot. Each time a new line containing overprint values is encountered on the plot, a double space is made in the column of overprint values. Overprint values for this line are then read from left to right across the plot. The table of "OVERPRINT VALUES" is limited to 150 numbers. If control points are clustered or an unfortunate choice of SCALE VALUES results in more than 150 overprint values, the plot is discontinued, overprint values are suppressed, and a message is printed on the incomplete plot.

ERROR MESSAGES

Twenty-eight error messages have been built into the program to indicate that invalid data or control cards have been encountered in the program. These data or control card errors and the messages generated by the errors are listed below:

Program errors

- 1 Number of sets of data points outside allowable range (1-500).
- 2 Indicator for calculation of first-degree equation outside allowable range (0-1).
- 3 Indicator for calculation of second-degree equation outside allowable range (0-1).
- 4 Indicator for calculation of third-degree equation outside allowable range (0-1).
- 5 Indicator for calculation of fourth-degree equation outside allowable range (0-1).
- 6 Indicator for calculation of fifth-degree equation outside allowable range (0-1).
- 7 Indicator for calculation of sixth-degree equation outside allowable range (0-1).
- 8 Indicators for calculation of first-, second-, third-, fourth-, fifth-, and sixth-degree equations are all zero.
- 9 Residual plot indicator outside allowable range (0-6).
- 10 Plotting limit indicator for residual map outside allowable range (0-1).
- 11 Indicator for use of Link 2 outside allowable range (0-1).
- 12 Use of Link 2 attempted without proper specification in Link 1.
- 13 Contour map indicator outside allowable range (1-6).
- 14 Plotting limit indicator for contour map outside allowable range (0-1).

Subroutine CONTUR Errors

- 1 Indicator for evaluation subroutines outside allowable range (1-6).
- 2 Indicator for orientation outside allowable range (1-4).

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- 3 Card tabulator indicator outside allowable range (0-1).
 - 4 Number of columns of output outside allowable range (12-120).
 - 5 Contour interval negative or zero.
 - 6 Maximum x-plotting limit less than or equal to minimum x-plotting limit.
 - 7 Maximum y-plotting limit less than or equal to minimum y-plotting limit.

Subroutine PLOT3 Errors

- 1 Number of points to be plotted outside allowable range (1-500).
- ② Orientation indicator outside allowable range (1-4).
- ③ Number of columns of output outside allowable range (16-120).
- 4 Card tabulator indicator outside allowable range (0-1).
- 5 Indicator for previous ordering of elements outside allowable range (0-2).
- 6 Maximum x-plotting limit less than or equal to minimum x-plotting limit.
- ⑦ Maximum y-plotting limit less than or equal to minimum y-plotting limit."

SAMPLE OUTPUT

Examples of the output follow. This includes:

1. Tabulated input data, 1st degree through 5th degree surface values with corresponding residuals.
2. Statistical calculations.
3. Contoured 1st, 2nd, 3rd, and 4th surfaces.
4. Plot of original data.
5. Plot of 1st degree residuals.

X-COORD	Y-COORD	Z-VALUE	1ST-SURF	1ST-RESID	2ND-SURF	2ND-RESID	3RD-SURF	3RD-RESID
CLEARY HILL AREA	A	ZINC VALUES	HEINER & WOLFF					
1.800	4.600	125.000	111.320	13.680	140.505	-15.505	99.568	25.432
1.800	4.200	175.000	112.811	62.189	151.337	23.663	148.172	26.828
1.800	3.800	175.000	114.302	60.698	158.583	16.417	179.236	-4.236
1.800	3.400	175.000	115.793	59.207	162.243	12.757	194.778	-19.778
1.800	3.000	200.000	117.284	82.716	162.318	37.682	196.818	3.182
1.800	2.600	200.000	118.775	81.225	158.807	41.193	187.373	12.627
1.800	2.200	175.000	120.265	54.735	151.710	23.290	168.462	6.538
1.800	1.800	125.000	121.756	3.244	141.027	-16.027	142.103	-17.103
1.800	1.400	125.000	123.247	1.753	126.758	-1.758	110.314	14.686
2.600	4.200	100.000	121.034	-21.034	125.787	-25.787	102.033	-2.033
2.600	3.800	75.000	122.525	-47.525	133.776	-58.776	128.709	-53.709
2.600	3.400	125.000	124.016	0.984	138.179	-13.179	141.986	-16.986
2.600	3.000	75.000	125.507	-50.507	138.996	-63.996	143.884	-68.884
2.600	2.600	250.000	126.998	123.002	136.228	113.772	136.421	113.579
2.600	2.200	200.000	128.489	71.511	129.873	70.127	121.615	78.385
2.600	1.800	1.000	129.980	-128.980	119.933	-118.933	101.485	-100.485
2.600	1.400	50.000	131.470	-81.470	106.408	-56.408	78.049	-28.049
4.200	4.200	50.000	137.480	-87.480	102.125	-52.125	85.226	-35.226
4.200	3.800	75.000	138.971	-63.971	111.600	-36.600	102.920	-27.920
4.200	3.400	75.000	140.462	-65.462	117.488	-42.488	111.463	-36.463
4.200	3.000	200.000	141.953	58.047	119.791	80.209	112.873	87.127
4.200	2.600	50.000	143.444	-93.444	118.508	-68.508	109.169	-59.169
4.200	2.200	50.000	144.935	-94.935	113.639	-63.639	102.369	-52.369
4.200	1.800	200.000	146.426	53.574	105.184	94.816	94.492	105.508
5.000	4.200	75.000	145.703	-70.703	104.014	-29.014	102.576	-27.576
5.000	3.800	200.000	147.194	52.806	114.230	85.770	115.677	84.323
5.000	3.400	50.000	148.685	-98.685	120.861	-70.861	121.751	-71.751
5.000	3.000	50.000	150.176	-100.176	123.907	-73.907	122.815	-72.815
5.000	2.600	200.000	151.667	48.333	123.366	76.634	120.888	79.112
5.000	2.200	125.000	153.158	-28.158	119.240	5.760	117.989	7.011
5.000	1.800	150.000	154.649	-4.649	111.528	38.472	116.135	33.865
5.800	4.200	175.000	153.926	21.074	115.047	59.953	129.108	45.892
5.800	3.800	150.000	155.417	-5.417	126.007	23.993	137.549	12.451
5.800	3.400	200.000	156.908	43.092	133.381	66.619	141.084	58.916
5.800	3.000	175.000	158.399	16.601	137.169	37.831	141.734	33.266
5.800	2.600	75.000	159.890	-84.890	137.371	-62.371	141.516	-66.516
5.800	2.200	200.000	161.381	38.619	133.988	66.012	142.449	57.551
5.800	1.800	100.000	162.872	-62.872	127.018	-27.018	146.552	-46.552
7.400	4.600	175.000	168.882	6.118	148.522	26.478	184.166	-9.166
7.400	4.200	125.000	170.373	-45.373	164.553	-39.553	185.756	-60.756
7.400	3.800	350.000	171.863	178.137	176.998	173.002	184.670	165.330
7.400	3.400	125.000	173.354	-48.354	185.857	-60.857	182.926	-57.926
7.400	3.000	150.000	174.845	-24.845	191.131	-41.131	182.542	-32.542
7.400	2.600	200.000	176.336	23.664	192.818	7.182	185.538	14.462
7.400	2.200	100.000	177.827	-77.827	190.920	-90.920	193.932	-93.932
7.400	1.800	125.000	179.318	-54.318	185.436	-60.436	209.741	-84.741
8.200	4.200	175.000	178.596	-3.596	203.025	-28.025	203.891	-28.891
8.200	3.800	200.000	180.087	19.913	216.212	-16.212	197.939	2.061
8.200	3.000	175.000	183.069	-8.069	231.830	-56.830	192.450	-17.450
8.200	2.600	200.000	184.559	15.441	234.261	-34.261	196.951	3.049
8.200	2.200	350.000	186.050	163.950	233.105	116.895	208.972	141.028
8.200	1.800	125.000	187.541	-62.541	228.364	-103.364	230.533	-105.533
8.200	1.400	350.000	189.032	160.968	220.037	129.963	263.652	86.348

CLEARY HILL AREA A ZINC VALUES HEINER & WOLFF

X-COORD	Y-COORD	Z-VALUE	4TH-SURF	4TH-RESID	5TH-SURF	5TH-RESID	6TH-SURF	6TH-RESID
1.800	4.600	125.000	143.128	-18.128	123.553	1.447	134.124	-9.124
1.800	4.200	175.000	158.146	16.854	183.402	-8.402	145.004	29.996
1.800	3.800	175.000	179.386	-4.386	161.477	13.523	205.830	-30.830
1.800	3.400	175.000	198.561	-23.561	162.956	12.044	172.137	2.863
1.800	3.000	200.000	208.816	-8.816	196.842	3.158	159.797	40.203
1.800	2.600	200.000	204.727	-4.727	223.162	-23.162	210.879	-10.879
1.800	2.200	175.000	182.300	-7.300	199.266	-24.266	224.385	-49.385
1.800	1.800	125.000	138.977	-13.977	126.601	-1.601	99.538	25.462
1.800	1.400	125.000	73.628	51.372	96.982	28.018	120.387	4.613
2.600	4.200	100.000	52.900	47.100	93.577	6.423	76.846	23.154
2.600	3.800	75.000	82.750	-7.750	103.926	-28.926	114.016	-39.016
2.600	3.400	125.000	109.835	15.165	113.868	11.132	111.886	13.114
2.600	3.000	75.000	129.311	-54.311	141.415	-66.415	131.252	-56.252
2.600	2.600	250.000	137.767	112.233	156.747	93.253	185.575	64.425
2.600	2.200	200.000	133.225	66.775	127.573	72.427	171.496	28.504
2.600	1.800	1.000	115.139	-114.139	66.337	-65.337	16.592	-15.592
2.600	1.400	50.000	84.393	-34.393	76.434	-26.434	66.806	-16.806
4.200	4.200	50.000	64.885	-14.885	42.708	7.292	53.475	-3.475
4.200	3.800	75.000	87.326	-12.326	76.700	-1.700	72.944	2.056
4.200	3.400	75.000	104.185	-29.185	90.135	-15.135	75.127	-0.127
4.200	3.000	200.000	114.654	85.346	113.262	86.738	92.139	107.861
4.200	2.600	50.000	119.351	-69.351	129.217	-79.217	139.588	-89.588
4.200	2.200	50.000	120.319	-70.319	119.925	-69.925	147.756	-97.756
4.200	1.800	200.000	121.040	78.960	113.169	86.831	117.041	82.959
5.000	4.200	75.000	112.883	-37.883	97.287	-22.287	97.448	-22.448
5.000	3.800	200.000	126.443	73.557	117.536	82.464	126.830	73.170
5.000	3.400	50.000	132.317	-82.317	116.932	-66.932	112.834	-62.834
5.000	3.000	50.000	131.705	-81.705	128.585	-78.585	101.811	-51.811
5.000	2.600	200.000	127.237	72.763	138.669	61.331	124.397	75.603
5.000	2.200	125.000	122.975	2.025	132.922	-7.922	131.405	-6.405
5.000	1.800	150.000	124.413	25.587	143.433	6.567	153.018	-3.018
5.800	4.200	175.000	157.201	17.799	174.904	0.096	157.006	17.994
5.800	3.800	150.000	163.197	-13.197	170.787	-20.787	204.444	-54.444
5.800	3.400	200.000	158.932	41.068	149.606	50.394	174.506	25.494
5.800	3.000	175.000	147.615	27.385	144.480	30.520	133.819	41.181
5.800	2.600	75.000	133.891	-58.891	142.825	-67.825	127.631	-52.631
5.800	2.200	200.000	123.836	76.164	131.846	68.154	119.768	80.232
5.800	1.800	100.000	124.963	-24.963	145.707	-45.707	155.549	-55.549
7.400	4.600	175.000	160.095	14.905	147.356	27.644	159.944	15.056
7.400	4.200	125.000	191.831	-66.831	245.207	-120.207	178.319	-53.319
7.400	3.800	350.000	200.934	149.066	216.313	133.687	241.256	108.744
7.400	3.400	125.000	193.214	-68.214	180.453	-55.453	203.131	-78.131
7.400	3.000	150.000	175.906	-25.906	165.094	-15.094	162.069	-12.069
7.400	2.600	200.000	157.693	42.307	152.766	47.234	161.569	38.431
7.400	2.200	100.000	148.667	-48.667	127.078	-27.078	139.998	-39.998
7.400	1.800	125.000	160.368	-35.368	119.684	5.316	99.084	25.916
8.200	4.200	175.000	182.357	-7.357	169.867	5.133	182.194	-7.194
8.200	3.800	200.000	209.274	-9.274	182.973	17.027	187.131	12.869
8.200	3.000	175.000	209.949	-34.949	216.742	-41.742	166.444	8.556
8.200	2.600	200.000	203.639	-3.639	235.559	-35.559	245.522	-45.522
8.200	2.200	350.000	208.580	141.420	226.301	123.699	272.791	77.209
8.200	1.800	125.000	238.316	-113.316	216.056	-91.056	176.303	-51.303
8.200	1.400	350.000	307.831	42.169	326.685	23.315	339.229	10.771

CLEARY HILL AREA A ZINC VALUES HEINER & WOLFF

COEFFICIENTS OF FIRST-DEGREE EQUATION

$$Z = 109.96370 + 10.27890 X + -3.72738 Y$$

COEFFICIENTS OF SECOND-DEGREE EQUATION

$$Z = 121.96134 + -53.62819 X + 75.70629 Y + 7.14523 X^2 + -2.32092 XY + -11.20548 Y^2$$

COEFFICIENTS OF THIRD-DEGREE EQUATION

$$Z = 82.33379 + -112.06672 X + 178.89207 Y + 35.86439 X^2 + -53.22859 XY + -3.51221 Y^2 + -1.95002 X^3 + 0.13318 X^2Y + 8.29452 XY^2 + -5.25635 Y^3$$

COEFFICIENTS OF FOURTH-DEGREE EQUATION

$$Z = -900.61790 + 317.38703 X + 1034.09568 Y + 22.64319 X^2 + -466.05490 XY + -164.62384 Y^2 + -11.06947 X^3 + 50.19601 X^2Y + 77.01661 XY^2 + -3.90582 Y^3 + 0.88320 X^4 + -2.90731 X^3Y + -1.14432 X^2Y^2 + -6.55479 XY^3 + 2.33041 Y^4$$

COEFFICIENTS OF FIFTH-DEGREE EQUATION

$$Z = 5437.45318 + -732.15825 X + -9879.71934 Y + 502.45234 X^2 + -408.21164 XY + 8026.86923 Y^2 + -55.30572 X^3 + -221.84234 X^2Y + 418.97938 XY^2 + -3114.51078 Y^3 + -1.07526 X^4 + 39.46240 X^3Y + -10.85890 X^2Y^2 + -66.61468 XY^3 + 561.76284 Y^4 + 0.25426 X^5 + -1.51074 X^4Y + -2.10805 X^3Y^2 + 4.53431 X^2Y^3 + 1.13095 XY^4 + -37.86737 Y^5$$

COEFFICIENTS OF SIXTH-DEGREE EQUATION

$$Z = 44689.00622 + -10002.24113 X + -88899.51056 Y + 5317.79619 X^2 + 2680.67309 XY + 80517.50244 Y^2 + -922.84966 X^3 + -3068.46493 X^2Y + 2164.78669 XY^2 + -39151.97022 Y^3 + 82.59878 X^4 + 427.51956 X^3Y + 537.82421 X^2Y^2 + -1102.22680 XY^3 + 10440.25751 Y^4 + -5.05674 X^5 + -15.88500 X^4Y + -89.04009 X^3Y^2 + 21.17667 X^2Y^3 + 146.57134 XY^4 + -1429.20669 Y^5 + 0.15649 X^6 + 0.21266 X^5Y + 1.54851 X^4Y^2 + 6.36699X^3Y^3 + -9.07100 X^2Y^4 + -3.45165 XY^5 + 78.18539 Y^6$$

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ERROR MEASURES

SURFACE	FIRST-DEGREE	SECOND-DEGREE	THIRD-DEGREE	FOURTH-DEGREE	FIFTH-DEGREE	SIXTH-DEGREE
STANDARD DEVIATION	71.55	65.06	62.41	58.52	54.96	49.21
VARIATION EXPLAINED BY SURFACE	0.28445188E 05	0.74562500E 05	0.92103563E 05	0.11655356E 06	0.13759969E 06	0.16872581E 06
VARIATION NOT EXPLAINED BY SURFACE	0.26621081E 06	0.22009350E 06	0.20255244E 06	0.17810244E 06	0.15705631E 06	0.12593019E 06
TOTAL VARIATION	0.29465600E 06	0.29465600E 06	0.29465600E 06	0.29465600E 06	0.29465600E 06	0.29465600E 06
COEFFICIENT OF DETERMINATION	0.09653693	0.25304931	0.31257993	0.39555806	0.46698415	0.57261962
COEFFICIENT OF CORRELATION	0.31070393	0.50304008	0.55908847	0.62893409	0.68336242	0.75671637

CLEARY HILL AREA A ZINC VALUES HEINER & WOLFF

CONTOURED FIRST-DEGREE SURFACE

PLOTTING LIMITS

MAXIMUM X = 9.000000 MINIMUM X = 0.0
MAXIMUM Y = 5.000000 MINIMUM Y = 0.0

X-SCALE IS HORIZONTAL

X-VALUE = 0.0 + 0.1125 X (SCALE VALUE)

Y-SCALE IS VERTICAL

CONTOUR INTERVAL = 25.00
REFERENCE CONTOUR (.....) = 175.00

0123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789

5.00 BBBB8888 AAAAAAAAAAAAAAAAAAAAAA
4.81 BBB8888 AAAAAAAAAAAAAAAAAAAAAA
4.62 BBB8888 AAAAAAAAAAAAAAAAAAAAAA
4.44 BBB8888 AAAAAAAAAAAAAAAAAAAAAA
4.25 BBB8888 AAAAAAAAAAAAAAAAAAAAAA
4.06 BBB8888 AAAAAAAAAAAAAAAAAAAAAA
3.87 BBB8888 AAAAAAAAAAAAAAAAAAAAAA
3.69 BBB8888 AAAAAAAAAAAAAAAAAAAAAA
3.50 BBB8888 AAAAAAAAAAAAAAAAAAAAAA
3.31 BBB8888 AAAAAAAAAAAAAAAAAAAAAA
3.12 BBB8888 AAAAAAAAAAAAAAAAAAAAAA
2.94 BBB8888 AAAAAAAAAAAAAAAAAAAAAA
2.75 BBB8888 AAAAAAAAAAAAAAAAAAAAAA
2.56 BBB8888 AAAAAAAAAAAAAAAAAAAAAA
2.37 BBB8888 AAAAAAAAAAAAAAAAAAAAAA
2.19 BBB8888 AAAAAAAAAAAAAAAAAAAAAA
2.00 BBB8888 AAAAAAAAAAAAAAAAAAAAAA
1.81 BBB8888 AAAAAAAAAAAAAAAAAAAAAA
1.62 BBB8888 AAAAAAAAAAAAAAAAAAAAAA
1.44 BBB8888 AAAAAAAAAAAAAAAAAAAAAA
1.25 BBB8888 AAAAAAAAAAAAAAAAAAAAAA
1.06 BBB8888 AAAAAAAAAAAAAAAAAAAAAA
0.87 BBB8888 AAAAAAAAAAAAAAAAAAAAAA
0.69 BBB8888 AAAAAAAAAAAAAAAAAAAAAA
0.50 BBB8888 AAAAAAAAAAAAAAAAAAAAAA
0.31 BBB8888 AAAAAAAAAAAAAAAAAAAAAA
0.12 BBB8888 AAAAAAAAAAAAAAAAAAAAAA
-0.06 BBB8888 AAAAAAAAAAAAAAAAAAAAAA

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CLEARY HILL AREA A ZINC VALUES HEINER & WOLFF

CONTOURED SECCND-DEGREE SURFACE

PLOTTING LIMITS

MAXIMUM X = 9.000000 MINIMUM X = 0.0
 MAXIMUM Y = 5.000000 MINIMUM Y = 0.0

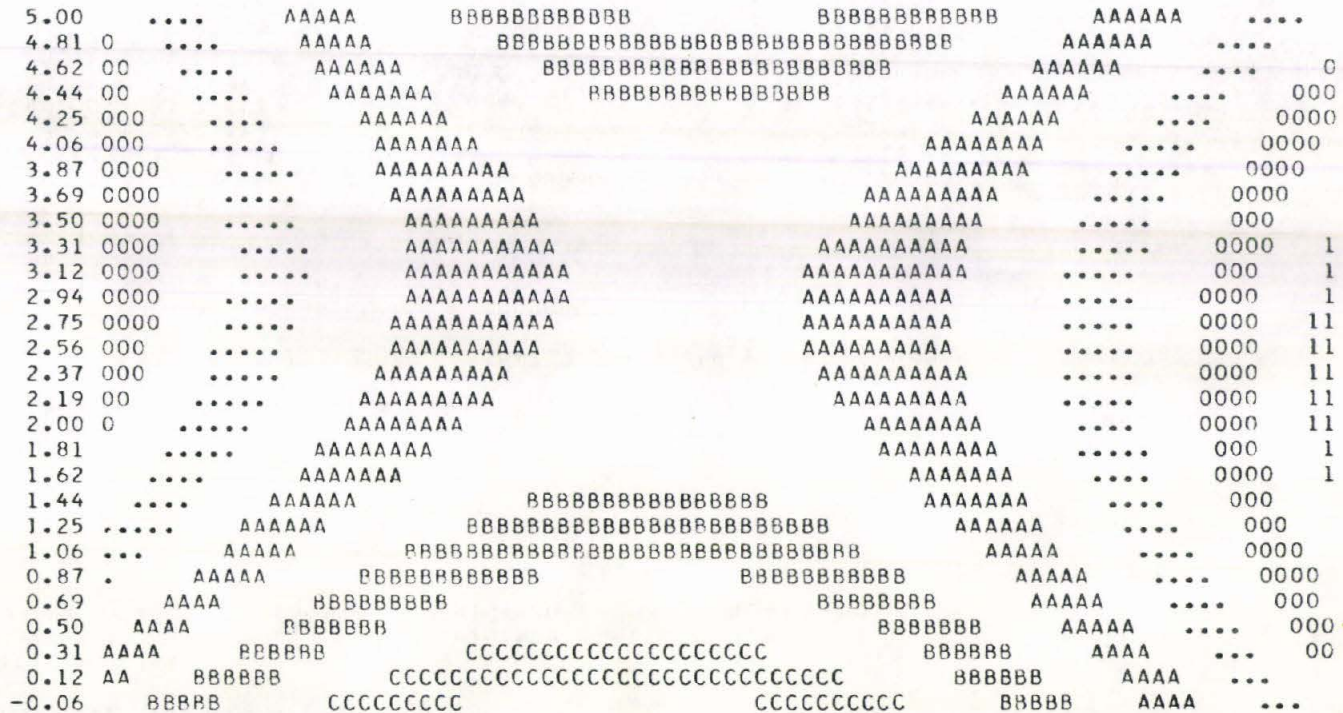
X-SCALE IS HORIZONTAL

X-VALUE = 0.0 + 0.1125 X (SCALE VALUE)

Y-SCALE IS VERTICAL

CONTOUR INTERVAL = 25.00
 REFERENCE CONTOUR (.....) = 175.00

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0123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789

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CLEARY HILL AREA A ZINC VALUES HEINER & WOLFF

CONTOURED THIRD-DEGREE SURFACE

PLOTTING LIMITS

MAXIMUM X = 9.000000 MINIMUM X = 0.0
 MAXIMUM Y = 5.000000 MINIMUM Y = 0.0

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X-SCALE IS HORIZONTAL

X-VALUE = 0.0 + 0.1125 X (SCALE VALUE)

Y-SCALE IS VERTICAL

CONTOUR INTERVAL = 25.00
 REFERENCE CONTOUR (.....) = 175.00

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```

5.00 0 .. AA BB CCCC DDDDDDDDD CCCC BBBB AAAA ..... 0000
4.81 1 0 . AA BB CCCCCC CCCCCCCC BBBB AAAA ..... 00
4.62 11 0 .. AA BBBB CCCCCCCC BBBB AAAA .....
4.44 22 1 0 .. AAA BBBB BBBB AAAA .....
4.25 3 2 11 00 .. AAA BBBB BBBB BBBB BBBB AAAA .....
4.06 33 2 1 00 .. AAA BBBB BBBB BBBB AAAA .....
3.87 33 2 1 00 .. AAAA BBBB AAAA .....
3.69 4 3 22 11 00 ... AAAA AAAA .....
3.50 4 33 2 11 00 .. AAAA AAAA .....
3.31 4 3 22 11 00 ... AAAA AAAA .....
3.12 4 3 22 11 00 ... AAAA AAAA .....
2.94 4 3 22 11 00 ... AAAA AAAA .....
2.75 4 33 2 11 00 .. AAAA AAAA .....
2.56 4 3 22 11 00 ... AAAA AAAA .....
2.37 33 2 1 00 ... AAAA AAAA .....
2.19 3 2 1 00 ... AAAA BBBB AAAA .....
2.00 3 22 1 00 .. AAAA BBBB BBBB AAAA .....
1.81 2 1 00 .. AAA BBBB BBBB BBBB AAAA .....
1.62 2 1 0 .. AAA BBBB BBBB BBBB BBBB AAAA .....
1.44 11 00 .. AAA BBBB BBBB BBBB AAAA .....
1.25 1 0 .. AAA BBBB BBBB AAAA .....
1.06 00 .. AAA BBBB BBBB AAAA .....
0.87 0 . AA BB CCCCCC BBBB AAA .....
0.69 . AA BB CCCCCCCCCCCCCC BBBB AAA .....
0.50 AA BB CCCCC CCCCC BBBB AAA ..
0.31 A BB CCCC CCCCC BBB AAA ...
0.12 BB CCCC DDDDDDD CCCC BB AAA ..
-0.06 CCC DDDDDDDDDDDDDDDD CCC BBB AA ...
    
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CLEARY HILL AREA A ZINC VALUES HEINER & WOLFF

CONTOURED FOURTH DEGREE SURFACE

PLOTTING LIMITS

MAXIMUM X = 9.000000 MINIMUM X = 0.0
 MAXIMUM Y = 5.000000 MINIMUM Y = 0.0

X-SCALE IS HORIZONTAL

X-VALUE = 0.0 + 0.1125 X (SCALE VALUE)

Y-SCALE IS VERTICAL

CONTOUR INTERVAL = 25.00
 REFERENCE CONTOUR (.....) = 175.00

0123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789

5.00	42 9 6543210	A B C	DDDDDDDDDD	CCCC	BBBB		BBBB	CC	DD	E							
4.81	753 0 76	0 A B CC	DDDDDD	CCC	BBB	AAAAAAAAAAAAAAAA	BBB	CC									
4.62	64 1 8	0. A BB CCC		CCCC	BBB	AAAAA	AAAAA	BBBB									
4.44	2 9 43	0 A B CCC		CCCCC	BBBB	AAAA	AAAAA									
4.25	53 0 65432	0 . A BB	CCCCCCCCCCC		BBB	AAAA										
4.06	310 76543	10 . AA BB	CCCCCCC		BBBB	AAAA										
3.87	4 1 76543	1 .. A BBB			BBBBB	AAAA										
3.69	2 9876543	1 0 . AA BBBB			BBBBBB	AAAAA		0000								
3.50	3 098 543	1 0 .. AA	BBBBBBBBBBBBBB			AAAAAA		0000								
3.31	10 43 1 0 . AA		BBBBBBBB			AAAAAAA		000								
3.12	2 876 3 1 00 ..	AAA				AAAAAAAAA		000 1								
2.94	10 654 32 1 00 ..	AAAA				AAAAAAAAAAAA		000 1								
2.75	9876 43 2 1 0 ..	AAAA				AAAAAAAAAAAAAAAA		00 11								
2.56	4 2 1 0 ..	AAAAA				AAAAAAAAAAAAAAAA		00 1								
2.37	8 54 32 11 0 ..	AAAAAA				AAAAAAAAAAAAAAAA		00 1								
2.19	76 43 2 1 0 ..	AAAAAA				AAAAAAAAAAAA		0 1 2								
2.00	54 32 11 0 ..	AAAAAA				AAAAAAA		0 1 2								
1.81	4 2 1 00 ..	AAAAA				AAAAAAAAAAAA		0 1 2 3								
1.62	2 1 0 ..	AAA				AAAAAAAAAAAAAAAA		00 1 2 3 4								
1.44	0 . AA	BBBBBBBBBBBBBBBB				AAAAAAAAAAAAAAAA		00 1 2 34 5								
1.25	A BB	CCCCCCCCCCC	BBBBB			AAAAAAA		000 11 22 34 5								
1.06	DDDD	DDDDDD	CCCC	BBBB		AAAAA		000 11 22 3 4 56 8								
0.87	F	FFFF	EEE	DDD	CCC	BBB	AAAA	0000 11 22 33 4 5 7 0								
0.69	IIII	HH	GG	FF	EE	DD	CC	BB	AAA	0000 1111 222 3 4 5 6 7 90						
0.50	L	KK	JJ	I	H	GG	F	EE	DD	CC	BB	A	000 111 222 33 44 5 6 7 8 0			
0.31	OO	N	M	L	K	J	I	H	G	F	E	D	C	B	A	00 11 22 333 44 55 6 7 89 0 23 9
0.12	S	R	QP	ON	M	K	J	I	H	F	E	D	C	B	A	0 1 2 33 44 55 66 77 8 9 0 1 23 567890
-0.06	W	TS	PO	LK	IH	GF	ED	C	B	A	00 1 2 33 4 55 66 7 8 9 00 1 3 45 7890123 7					

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CLEARY HILL AREA A ZINC VALUES HEINER & WOLFF

PLOT OF ORIGINAL DATA (Z-COORDINATES)

PLOTTING LIMITS

MAXIMUM X = 9.000000 MINIMUM X = 0.0
 MAXIMUM Y = 5.000000 MINIMUM Y = 0.0

PLOTTED VALUES HAVE BEEN MULTIPLIED BY A FACTOR OF 10 TO THE 1 POWER

X-SCALE IS HORIZONTAL

X-VALUE = 0.0 + 0.1125 X (SCALE VALUE)

Y-SCALE IS VERTICAL

0123456789 123456789 123456789 123456789 123456789 123456789 123456789 123456789

5.00								
4.81								
4.63		+1250					+1750	
4.44								
4.25		+1750	+1000	+500	+750	+1750	+1250	+1750
4.06								
3.88		+1750	+750	+750	+2000	+1500	+3500	+2000
3.69								
3.50		+1750	+1250	+750	+500	+2000	+1250	
3.31								
3.13		+2000	+750	+2000	+500	+1750	+1500	+1750
2.94								
2.75		+2000	+2500	+500	+2000	+750	+2000	+2000
2.56								
2.38		+1750	+2000	+500	+1250	+2000	+1000	+3500
2.19								
2.00								
1.81		+1250	+10	+2000	+1500	+1000	+1250	+1250
1.63								
1.44		+1250	+500				+3500	
1.25								
1.06								
0.88								
0.69								
0.50								
0.31								
0.13								

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CLEARY HILL AREA A ZINC VALUES HEINER & WOLFF

PLOT OF FIRST-DEGREE RESIDUALS

PLOTTING LIMITS

MAXIMUM X = 9.000000 MINIMUM X = 0.0
 MAXIMUM Y = 5.000000 MINIMUM Y = 0.0

PLOTTED VALUES HAVE BEEN MULTIPLIED BY A FACTOR OF 10 TO THE 1 POWER

X-SCALE IS HORIZONTAL

X-VALUE = 0.0 + 0.1125 X (SCALE VALUE)

Y-SCALE IS VERTICAL

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5.00								
4.81								
4.63		+136					+61	
4.44								
4.25		+621	-210	-874	-707	+210	-453	-35
4.06								
3.88		+606	-475	-639	+528	-54	+1781	+199
3.69								
3.50		+592	+9	-654	-986	+430	-483	
3.31								
3.13		+827	-505	+580	-1001	+166	-248	-80
2.94								
2.75		+812	+1230	-934	+483	-848	+236	+154
2.56								
2.38		+547	+715	-949	-281	+386	-778	+1639
2.19								
2.00								
1.81		+32	-1289	+535	-46	-628	-543	-625
1.63								
1.44		+17	-814					+1609
1.25								
1.06								
0.88								
0.69								
0.50								
0.31								
0.13								

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