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emiT: An apparatus to test time reversal invariance in polarized neutron decay

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We describe an apparatus used to measure the triple-correlation term ($D\hat{\sigma}_n \cdot \mathbf{p}_e \times \mathbf{p}_\nu$) in the beta decay of polarized neutrons. The D coefficient is sensitive to possible violations of time reversal invariance. The detector has an octagonal symmetry that optimizes electron-proton coincidence rates and reduces systematic effects. A beam of longitudinally polarized cold neutrons passes through the detector chamber, where a small fraction undergo beta decay. The final-state protons are accelerated and focused onto arrays of cooled semiconductor diodes, while the coincident electrons are detected using panels of plastic scintillator. Details regarding the design and performance of the proton detectors, beta detectors, and the electronics used in the data collection system are presented. The neutron beam characteristics, the spin-transport magnetic fields, and polarization measurements are also described. © 2004 American Institute of Physics. [DOI: 10.1063/1.1821628]

I. INTRODUCTION

Charge-parity symmetry violation (CP violation) is an important property of nature. Of particular interest is that it is necessary to explain the preponderance of matter over anti-matter in the universe.¹ Thus far, CP violation has been observed only in K and B meson oscillation and decays,²⁻⁴ and can be entirely accounted for by a phase in the Cabibbo-Kobayashi-Maskawa matrix in the electroweak Lagrangian. It can be shown, however, that this phase is insufficient to account for the known baryon asymmetry in the context of Big Bang cosmology,⁵ so that there is good reason to search for CP violation in other systems. CP and time-reversal (T) violation can be related to each other through the charge-parity-time theorem. Experimental limits on neutron and atomic electric dipole moments (T-violating) place strict constraints on some, but not all, possible sources of new CP violation. Tests of nuclear beta decay, and neutron decay in particular, complement these experiments. Some theoretical models that extend the Standard Model, such as left-right

symmetric theories, leptoquarks, and certain exotic fermions could cause observable effects that are as large as the present experimental limits.⁶

The decay probability distribution for neutron beta decay dW , written in terms of the neutron spin direction $\hat{\sigma}_n$ and the momenta (energy) of the electron \mathbf{p}_e (E_e) and antineutrino \mathbf{p}_ν (E_ν) was first described by Jackson, Treiman, and Wyld in 1957,⁷ as

$$dW \propto \left(1 + a \frac{\mathbf{p}_e \cdot \mathbf{p}_\nu}{E_e E_\nu} + A \frac{\hat{\sigma}_n \cdot \hat{\mathbf{p}}_e}{E_e} + B \frac{\hat{\sigma}_n \cdot \mathbf{p}_\nu}{E_\nu} + D \frac{\hat{\sigma}_n \cdot \mathbf{p}_e \times \mathbf{p}_\nu}{E_e E_\nu} \right) dE_e d\Omega_e d\Omega_\nu. \quad (1)$$

The triple correlation D is T-odd. A nonzero value for D above the level of calculable final-state interactions implies a violation of T symmetry. The most sensitive measurement of D in ¹⁹Ne decay is $(1 \pm 6) \times 10^{-4}$,⁸ only about a factor of 3 above electromagnetic final-state effects. The most recent measurements of D in neutron decay, $(-2.8 \pm 7.1) \times 10^{-4}$ and $(-6 \pm 13) \times 10^{-4}$ come from the TRINE collaboration and the first run of the emiT experiment, respectively.^{9,10} Standard Model final-state effects in the neutron system are estimated to be approximately 1.3×10^{-5} , well below the sensitivity of

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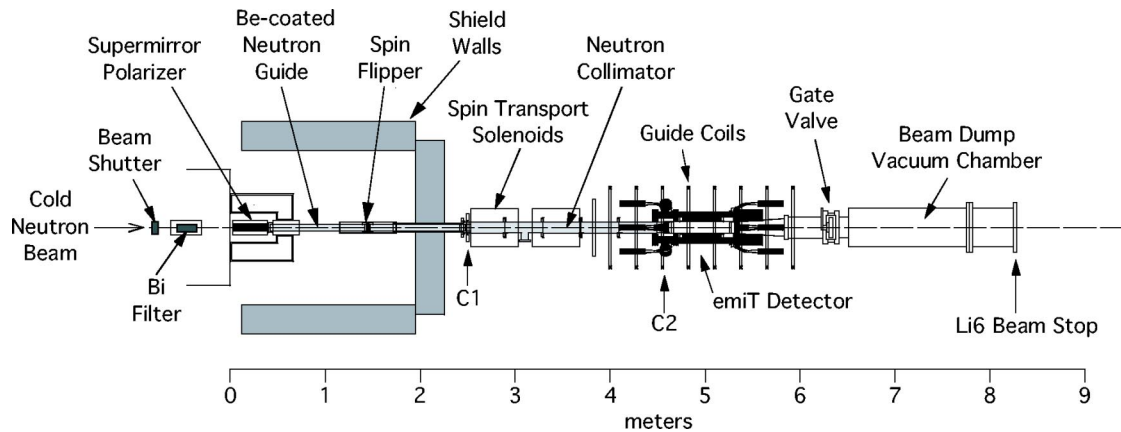


FIG. 1. (Color online) The emiT beam line on NG-6.

current experiments.¹¹ Details of this measurement may be found elsewhere.^{12,13} The focus of this article is the description of the upgraded emiT apparatus. We describe the cold neutron beam line, the spin transport, and specific aspects of an extensively upgraded detector used to perform a second, more sensitive measurement, from October 2003 through January 2004.

II. COLD NEUTRON BEAM

The emiT experiment uses polarized cold neutrons at the National Institute of Standards and Technology Center for Neutron Research (NCNR). The NCNR operates a 20 MW research reactor that provides a source of fission neutrons that have been moderated to thermal energies by the D₂O primary reactor coolant. Cold neutrons are produced by a neutron moderator situated adjacent to the reactor core. The cold source was recently upgraded and consists of an ellipsoidal shell of liquid hydrogen maintained at a temperature of 20 K.¹⁴ Scattering of neutrons in the cold source cools the neutrons to approximately 40 K (they do not reach thermal equilibrium with the liquid hydrogen). Colder neutrons spend a longer time within the sensitive volume of the detector, increasing the probability of an observable decay.

Neutron guides coated with ⁵⁸Ni efficiently transport the cold neutrons approximately 68 m from the cold source to the experimental area at the end of neutron guide 6 (NG-6)¹⁵ on the NCNR Neutron Guide Hall floor. The highly collimated cold neutron beam exits the guide through a thin Mg window and travels through 79 cm of air to an aperture that reduces the beam to a 6-cm-diameter cylinder. Downstream of this aperture is the remote-controlled local beam shutter (see Fig. 1). Upon exiting the guide shutter, the neutron beam passes through a meter-long air gap before entering a 15-cm-thick cryogenically cooled beam filter constructed from blocks of single-crystal bismuth. The filter attenuates fast neutrons and gamma rays originating from the reactor core that would otherwise contribute to the background. Cooling the filter elements to liquid-nitrogen temperatures significantly increases the transmission of cold neutrons through the filter by reducing losses from phonon scattering. The neutrons exit the end of NG-6, pass through a polarizer (Sec. II B), and travel 1 m to the spin-flipper (Sec. II B 2)

through a Be-coated glass neutron guide tube in which a slight helium overpressure is maintained to prevent beam attenuation due to air scattering. The windows on each end of this guide tube are 0.5-mm-thick single-crystal Si. While in the spin-flipper, the beam passes through two parallel sheets of 0.5 mm Formvar®-coated¹⁶ aluminum wire. The main vacuum chamber begins just past the spin-flipper, with a second 1-m-long Be-coated glass neutron guide. The upstream vacuum window of this guide is 0.10 mm aluminum. Following the second guide is the beam collimator section. Two ⁶LiF collimators, C1 (6.00 cm diameter) and C2 (5.00 cm diameter) in Fig. 1, are separated by 2 m, and define the beam. Between C1 and C2 are four ⁶LiF beam “scrapers” with decreasing diameters from 5.90 to 5.32 cm. Backing each collimator and scraper is a thick ring of high-purity lead that removes gamma rays and fast neutrons. Between the scrapers, the collimator tube is lined with ⁶Li-loaded glass to absorb scattered neutrons. Beyond C2, the beam enters the 80-cm-long detector chamber, where the neutron decay products are observed. Downstream of the detector chamber, the beam travels 2.8 m through vacuum to the ⁶Li-loaded-glass beam stop and fluence-monitoring fission chamber.

A. Neutron intensity distribution

Knowledge of the intensity distribution of the neutron beam is essential for understanding potential systematic effects that may give rise to a false *D* coefficient. We employed a neutron imaging technique to profile the beam at three locations along the beam line, thus obtaining detailed information on the beam envelope. In this method, the neutron beam irradiates a metal foil with the requirements of a high thermal neutron absorption cross section, a decay branch into beta particles, few competing decay modes, and a convenient half-life. Although there are a number of suitable metals for use as the transfer foil, we used natural dysprosium, the relevant isotope being ¹⁶⁴Dy. After irradiation, the decay electrons from the activated foil expose a film that is sensitive to beta particles and can be read out by an image reader. Typically, the pixel resolution of the images obtained was 200 μm by 200 μm. The intrinsic resolution of the image can be better, but is not needed for this application. This

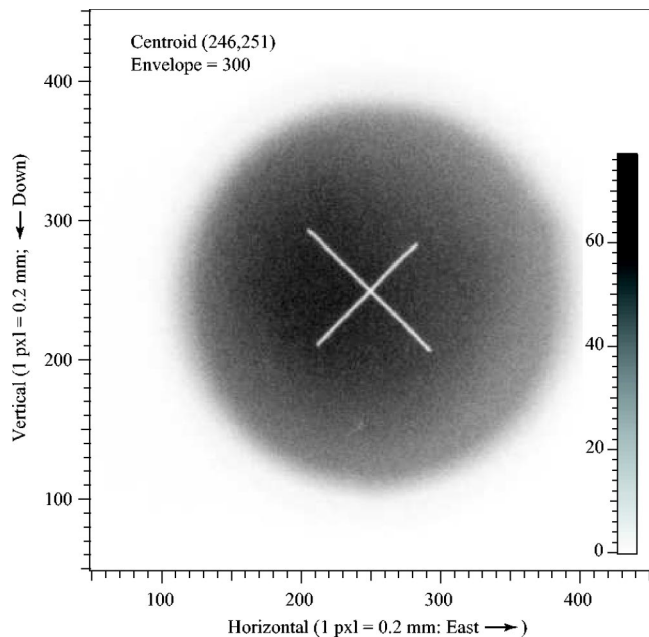


FIG. 2. (Color online) An image plot of the neutron beam intensity profile obtained from a dysprosium foil. The “X” in the center of the beam indicates the mechanical axis of the detector and is centered at position (250,250). The centroid of the image occurs at position (246,251).

technique has not been commonly used for neutron imaging; however, further examples may be found in Refs. 17–19.

Beam images were obtained at the axial center of the emiT detector as well as 18 cm upstream and downstream. These images allow a rendering of the beam envelope sufficient for our purposes. Figure 2 shows an example of one of the images. The intensity scale, referred to as photostimulable luminescence, is linearly proportional to the neutron fluence. The film is initially read out on a logarithmic scale, which covers about four decades of dynamic range (making it ideal for sensitive neutron measurements). One converts to a linear scale through a function supplied by the manufacturer of the film reader. The “X” in the center of the beam indicates the mechanical axis of the detector. It was obtained by sighting with a theodolite and mounting thin Cd wire on the dysprosium; it is centered at position (250,250). The centroid of the image was obtained by weighting each position by its intensity. The centroid defines the beam axis. For all three images, the centroid occurs within ± 1 mm of the mechanical center (detector axis). Figure 2 indicates that the peak of the beam is not coincident with the centroid. This asymmetry arises from the reflection of neutrons from the polarizing supermirror (PSM) discussed in Sec. II B. It is possible to force the centroid and peak to coincide by rotating the PSM; unfortunately, the beam profile remains asymmetric, and there is an undesirable 25% loss in polarized neutron fluence (neutrons/cm²). The maximum neutron fluence rate corresponds to matching of the phase space of the beam with PSM acceptance. Since the PSM is curved, this places the beam axis at an angle to the PSM so that the beam divergence is asymmetric.

Because the precise wavelength distribution of the polychromatic beam is unknown, one uses the capture fluence to quantify the neutron density ρv_o , where $v_o = 2200$ m s⁻¹. Us-

ing a calibrated fission chamber, the capture fluence rate was measured to be at the entrance to the polarizer and 1.7×10^8 cm⁻² s⁻¹ at C2.

B. Neutron polarization

Spin polarization of the neutron beam is achieved using a PSM^{20,21} obtained from the Institut Laue-Langevin in Grenoble, France. Supermirrors produce a high degree of polarization, typically greater than 95%, and are quite stable. The PSM consists of forty 0.2 mm \times 6 cm \times 33 cm Pyrex® plates with coatings on each side that maximize the reflection of the desired spin state while absorbing nearly all of the other.²² Both sides of each plate are covered with several reflecting layers of cobalt and titanium, each layer a few angstroms thick. Beneath those are layers of gadolinium and titanium, which further refract and absorb the neutrons of the undesired spin state. Each plate is slightly curved with a radius of 10 m so that there is no line of sight through the polarizer; each neutron transmitted reflects at least once.

The PSM is positioned within the gap of a magnet assembly formed by two rows of permanent magnets that are rigidly mounted with steel plates. This entire assembly is kinematically mounted on precision translational and rotational stages, allowing it to be precisely aligned relative to the neutron beam line. The permanent magnets produce a field within the gap of approximately 20 mT, transverse to the direction of neutron flight. Neutrons of the desired spin state are reflected via the spin-dependent scattering cross section from the magnetic layer, while neutrons of the opposite spin state are captured on the gadolinium. In this manner, the emergent neutron beam is spin polarized to better than 90%. The polarizer has an overall transmission of 24% of the neutron fluence incident on the PSM. Because neutron capture in gadolinium results in the emission of a large number of capture gamma rays, the PSM polarizer is shielded with 18 cm of lead in order to minimize the gamma-ray background present at the emiT detector.

1. Polarimetry

The neutron beam polarization was measured during construction of the emiT beam line. An analyzing supermirror (ASM), similar in design to the PSM but with supermirror coatings on only one side of each glass plate, was set up at the position of the second collimator C2. A fission chamber was mounted on the downstream side of the analyzer. The product of the beam polarization (P) and the analyzing power of the ASM (A) is given by

$$AP = \frac{N_u - N_f}{sN_u + N_f}, \quad (2)$$

where N_u is the number of counts obtained with the beam polarization in one spin state (“no-flip”), and N_f is the number of counts obtained with the beam polarization in the opposite spin state (“flip”). The spin-flip efficiency s is the absolute value of the ratio of polarizations for the two states of the spin-flipper. This was not measured, but our calculations indicate $s = 0.95 \pm 0.05$.¹³ Single-sided bender polarizers are known to have a smaller polarizing power than the

double-sided²¹ so that we can reasonably assume that $A < P$. We measured

$$\frac{N_u}{N_f} = 10.820 \pm 0.02. \quad (3)$$

Using the extreme values of $s=1$ and $A=P$, we obtain a lower limit on the beam polarization of $P > 0.91$.²³ Incomplete polarization simply reduces the sensitivity of the measurement, and uncertainty in the polarization leads to a measurement uncertainty proportional to D . Precise polarimetry is therefore unnecessary.

2. Spin transport

The magnetic fields downstream of the supermirror are designed to allow the neutron polarization to be flipped, to maintain the neutron polarization into the detector region, and to provide a precisely aligned quantization axis in the detector region. Exiting the PSM, the neutrons proceed through a double current-sheet spin-flipper. The current sheets are $30 \text{ cm} \times 12 \text{ cm}$ (vertical \times horizontal) with horizontal currents and are wound with close packed 0.45 mm Al wire. The return wires for each current sheet are 30 cm upstream/downstream with the central 10 cm of windings bent vertically to allow space for the guide tubes and spin transport solenoids. Iron plates are used to maintain the vertical fields between the supermirror and the upstream current-sheet.

The current in the downstream current-sheet can be in the opposite direction as the upstream one so that the magnetic field at the 1 mm transition is largely determined by the return coils of each current sheet (no-flip state). Alternatively, its current can be in the same direction, causing a sharp reversal in the field direction between the two current-sheets (flip state). In the no-flip state, the fields are aligned and the neutrons see no change of field going through the spin-flipper. In the flip state, the neutrons see an abrupt transition from 2.5 to -2.5 mT when they cross the gap between the solenoids (there is a maximum residual field of 0.2 mT at the edge of the neutron beam). A 0.4-nm neutron traverses the field flip in approximately $1 \mu\text{s}$. Thus, the field rotation exceeds the Larmor precession rate, and the direction of the field is reversed, but the spin direction is not. In this way the polarization along the magnetic field is reversed. The spin-flip efficiency is estimated to be 95% from numerical integration of the Bloch equations describing the evolution of free spins in a magnetic field. (This integration also shows that any residual transverse magnetization left from an incomplete spin-flip quickly averages to zero over the neutron decay region because of the polychromatic beam.)

Once the neutrons exit the downstream flipper solenoid, their spins are adiabatically rotated into the axis of a solenoid 70 cm long by 9.5 cm in diameter that is concentric with the beam line. The neutrons travel through three loops and two more axially aligned solenoids ($50 \text{ cm} \times 41 \text{ cm}$ diameter) before entering the detector region. The 41-cm solenoids provide a smooth transition into the primary field in the detector region that is formed by eight 0.82-m-diameter coils equally spaced along 2 m of the beam line. The guide field in the detector region is approximately 0.5 mT. Figure 3 shows the

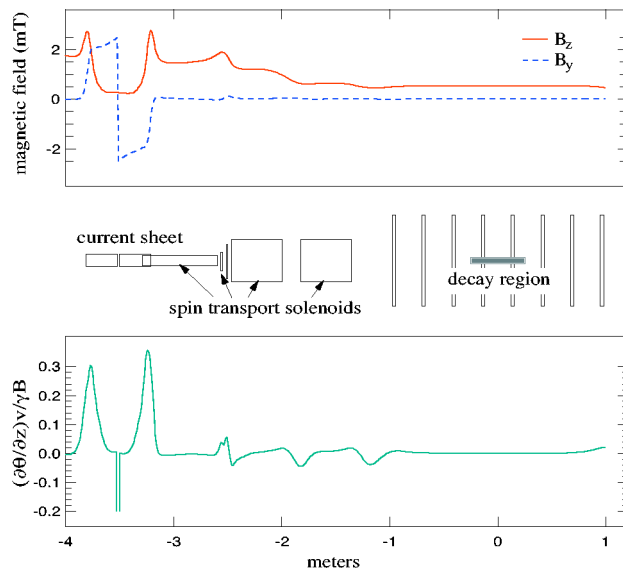


FIG. 3. (Color online) Calculated spin-transport fields. The top two traces show the y (vertical) and z (along the beam line) components of the spin transport field, respectively. The bottom trace shows the adiabaticity parameter $(\partial\theta/\partial z)v/\gamma B$. At the center of the figure is a layout of the spin-transport components.

guide fields as a function of position along the beam line. Also shown is the value of the adiabaticity parameter comparing the gradient of the magnetic field to the Larmor precession rate.

3. Field alignment

Precise alignment of the beam axis, the detector axis, and the magnetic field is critical to minimizing systematic effects. A misalignment between the detector axis and the neutron spin axis can mimic a time-reversal violating signal if the beam is not centered in the detector. This false signal is due to a combination of the spin-electron and spin-antineutrino coefficients, solid angle, and decay kinematics. To reduce systematic effects to acceptable levels, both the detector and the field are aligned to the beam line to within a few milliradians. The detector could be physically aligned using crosshairs temporarily mounted in the ends of the decay chamber, but the field required a more complicated alignment procedure described below.

The beam axis is established as described in Sec. II A. The alignment of the magnetic field is accomplished using a Bartington *Mag-03MS1000* three-axis fluxgate magnetometer. As the internal alignment of this magnetometer is specified to only 1.8 mrad, an alternative method of alignment was developed. Using an alignment tube with crosshairs, a V-block is aligned to within 1 mrad over the length of a 0.6 m rail mounted in the decay region. The magnetometer is mounted in a square carriage that could be placed in the aligned V-block. The square sides of the carriage allowed the fluxgate to be mounted in four orientations representing precise 90° rotations around the V-block axis. By comparing the transverse field measured in two positions 180° apart, it is possible to determine the actual transverse field.

By reversing the current in an individual coil, as well as rotating the magnetometer about the V-block axis, it is pos-

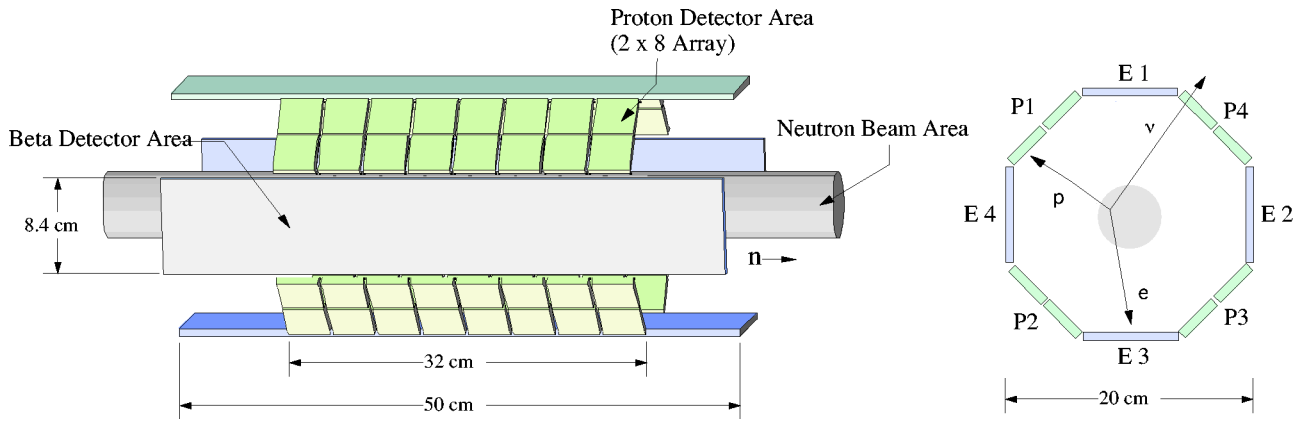


FIG. 4. (Color online) A schematic of the emiT detector illustrating the alternating electron and proton detector segments.

sible to determine the misalignment of each coil and align the field in the center of each coil with respect to the V-block axis to within 1 mrad. However, we also discovered that the fields from each coil are distorted by steel pieces in a trench that crosses the floor approximately 1 m below the middle of the detector. Even with the individual coils aligned, the magnetization induced in this steel causes a marked field misalignment in the decay region. Since this misalignment depends on the field strength in the guide field coils, all further corrections to the magnetic field are done with the 0.5 mT field in the detector region to keep the induced field constant.

Once each guide field coil is aligned, there remain transverse fields associated with ambient guide hall fields and with the induced fields described above. Uniform transverse fields are canceled using six rectangular coils placed in a beam-centered array around the detector. Each coil consists of 208-cm-long straight sections 90 cm off axis with split semicircles of 90 cm diameter on either end. The semicircular sections allow space for the detector assembly. By independently varying the currents in these coils a uniform transverse magnetic field can be established at any azimuthal angle. The residual transverse field components that cannot be compensated by these coils are broken down into polynomial moments, and individual correction coils were wound for the largest of these moments: dB_x/dz , dB_y/dz , d^2B_y/dz^2 , and dB_y/dy , where y is vertical, x is horizontal, and z is along the beam line. Although the actual fields from these correction coils are mostly orthogonal, an iterative procedure is used to produce the best cancellations possible with all the coils and the guide field coils turned on. The resulting field is measured to be aligned within a few milliradians throughout the detector region. Unfortunately, it is not possible to check the alignment of the fields with the detector in place due to the difficulty of aligning the V-block inside the detector.

4. Field monitoring

To insure stability in the magnetic systems, the current through each of the coils is monitored several milliseconds after every spin flip. Two fluxgate magnetometers in fixed positions near the detector are also monitored every 100 s. These data, along with other detector parameters, are fed directly into the data stream. In addition, five unaligned V-blocks designed to reproducibly position a fluxgate mag-

netometer are fixed to the detector frame in several places between 30 cm and 1 m from the detector region. These V-blocks allow for additional checks of the magnetic field.

III. THE EMIT DETECTOR

The emiT detector consists of an octagonal array of four electron and four proton detectors concentric to a beam of longitudinally polarized neutrons. The detector configuration is shown schematically in Fig. 4. Monte Carlo evaluation of various detector arrangements led to a detector geometry that is simultaneously optimized for sensitivity to the D coefficient and insensitivity to most systematic effects, as discussed in following sections.²⁴ The highly symmetric arrangement allows for the approximate cancellations of systematic effects stemming from detector efficiency and solid-angle variations as well as from beam and polarization misalignments.

A. Detector design

As discussed in Sec. I, the T-violating term is expressed in terms of the neutron spin, electron momentum, and antineutrino momentum as $\hat{\sigma}_n \cdot \mathbf{p}_e \times \mathbf{p}_\nu$. The decaying neutron is approximately at rest ($\mathbf{p}_n/\mathbf{p}_p \approx 0.001$). The effect of the small neutron velocity is to shift the proton velocity vector slightly in the detector frame, effectively changing the solid angle of the proton detectors. This can be understood as a slight longitudinal shift in the relative proton–electron detector positions. The analysis methods used are insensitive to such shifts; therefore, we may treat the neutron as though it is at rest and use momentum conservation to rewrite the triple correlation in terms of \mathbf{p}_p .

Short of tracking the individual particles, one can place beta detectors and proton detectors about a beam of polarized neutrons and measure coincidence events from decays within the polarized neutron beam. One can define left-handed or right-handed events based on the sign of the triple product, $\hat{\sigma}_n \cdot \mathbf{p}_e \times \mathbf{p}_p$. Although the particle detectors subtend finite solid angles, they can be placed such that nearly all of the neutron decays are correctly identified as either right-handed or left-handed. Monte Carlo studies indicate that while the sensitivity to D relative to other terms in the decay distribu-

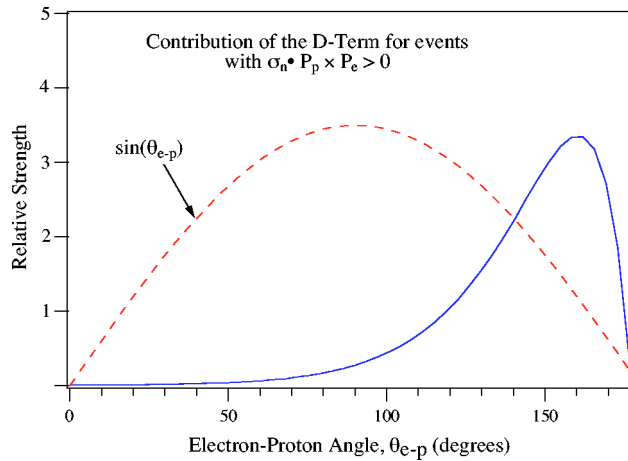


FIG. 5. (Color online) Monte Carlo results for the contribution of the D coefficient as a function of the beta-proton angle θ_{e-p} for right-handed events in zero-radius beam. The solid curve is a fit to the Monte Carlo data. The dashed curve shows the sine of θ_{e-p} , which would be the contribution to the D coefficient if it had only the sine dependence of the cross product.

tion is dependent upon detector geometry, the primary concern should be arranging the coincidence pairs such that the coincidence rate is maximized.

The octagonal geometry used in emiT places pairs of beta and proton detectors at an average angle of 135° rather than at 90° as was typical in earlier experiments. This choice of angles increases the coincidence detection efficiency because with little decay energy available the electron preferentially recoils from the proton. The momenta are thus highly anticorrelated and the coincidence rate increases greatly as the angle between the proton and electron approaches 165° . This situation is clearly illustrated in Fig. 5, which shows a Monte Carlo simulation of the contribution of the triple correlation from Eq. (1) for a zero-radius beam. The difference in rate is dependent on the beam diameter, decreasing for larger beams. To properly cancel systematic effects, the detector must have rotational symmetry, limiting the number of sides to multiples of 2. While a detector with a 24-sided geometry would place electron and proton detectors at a relative angle of 165° and yield a coincidence rate somewhat larger than one with eight sides, the modest gain is not worth the added complexity and cost. However, a detector with coincidence pairs subtending the same solid angles but arranged 135° does have a significantly greater coincidence count rate than a right-angle geometry. For the 6-cm emiT beam, this enhancement is approximately a factor of 3.

1. Determining D

Since several systematic effects can give rise to a false value of D , it is useful to outline briefly how one measures the D coefficient. More detailed discussions are found elsewhere.^{24,25} Note that the analysis presented here assumes that the detector segments have uniform detection efficiency. This was *not* the situation during the run in 1997,²⁶ and thus, an analysis method was developed to analyze data in which the detector has a high degree of nonuniformity.^{12,13} The problems that led to this situation have largely been resolved, and the following discussion illustrates a possible analysis approach.

A majority of the possible systematic effects can be eliminated by utilizing a detector with the appropriate symmetry and by reversing the direction of the neutron polarization during the measurement. Consequently, the emiT experiment is performed by periodically reversing the polarity of the neutron spin, and then comparing the number of coincidences for events with opposite signs of the triple correlation in otherwise identical coincidence pairs of proton and electron detectors. Using this approach, one can construct a ratio of the number of coincidence events in which all the factors in the numerator favor events with one sign of the triple correlation, and those in the denominator with the opposite sign. For example, the factors in such a ratio for the geometry shown in Fig. 4 are

$$R = \frac{N_{e_1 p_3}^\uparrow N_{e_2 p_4}^\uparrow N_{e_3 p_1}^\uparrow N_{e_4 p_2}^\uparrow N_{e_1 p_2}^\downarrow N_{e_2 p_3}^\downarrow N_{e_3 p_4}^\downarrow N_{e_4 p_1}^\downarrow}{N_{e_1 p_2}^\uparrow N_{e_2 p_3}^\uparrow N_{e_3 p_4}^\uparrow N_{e_4 p_1}^\uparrow N_{e_1 p_3}^\downarrow N_{e_2 p_4}^\downarrow N_{e_3 p_1}^\downarrow N_{e_4 p_2}^\downarrow}, \quad (4)$$

where $N_{e_i p_j}^\sigma$ represents the number of coincidences in the i th electron detector and the j th proton detector with $\sigma = \uparrow (\downarrow)$, indicating that the neutron polarization is parallel (antiparallel) to the neutron beam. Each factor can be written as

$$N_{e_i p_j}^\sigma = C^\sigma \Omega_{e_i}^\sigma \Omega_{p_j}^\sigma \epsilon_{e_i}^\sigma \epsilon_{p_j}^\sigma \epsilon_{e_i p_j}^\sigma (1 \pm \vec{K} \cdot \vec{P}D), \quad (5)$$

where C^σ is proportional to the beam flux for the given neutron polarization direction, the Ω terms are the solid angles subtended by the indicated detectors, the ϵ terms are the overall efficiencies of the electron and proton detectors, $\epsilon_{e_i p_j}^\sigma$ is the correlated coincidence efficiency, and \vec{P} is the average neutron polarization. The instrumental constant \vec{K} reflects the reduction in sensitivity to the triple correlation due to finite detector solid angles and can be calculated by Monte Carlo simulation for a specific detector geometry. The ratio is constructed so that the sign on the $\vec{K} \cdot \vec{P}D$ term is “positive” for all of the factors in the numerator and “negative” for those in the denominator. The purpose in constructing such a ratio is that the solid angles, individual detector efficiencies, and beam flux factors cancel, separately, for each of the two polarization directions. Only correlated efficiencies do not cancel exactly. These will be discussed in the next section. The measured D coefficient can be extracted from Eqs. (4) and (5) to yield

$$D = \frac{1}{\vec{K} \cdot \vec{P}} \frac{(R^{1/8} - 1)}{(R^{1/8} + 1)}. \quad (6)$$

2. Minimizing false D -coefficient effects

Correlated efficiencies arise primarily because the spin-antineutrino and spin-electron decay coefficients in Eq. (1) are nonzero. These decay correlation coefficients couple the neutron spin direction and the momenta of the decay products. The momenta are in turn coupled to each other via limitations in the available phase space. Because correlated efficiencies do not cancel exactly, they can give rise to a nonzero D . This effect has been observed in a previous experiment.^{27,28} There are two important contributions to this type of false asymmetry. The first can arise from spatial variations in the polarization direction of an extended beam.

This effect limits the maximum size of the beam and places constraints on the uniformity of the polarization direction. The second effect arises from nonuniformities of the individual detector efficiencies. Efficiencies can vary either as a function of panel position or the angle at which the decay particles strike the detector faces. Segmentation of the detector panels helps to reduce these effects by essentially allowing multiple simultaneous experiments.

Known effects contributing to the systematic uncertainty associated with the experiment were evaluated both analytically and with Monte Carlo simulations.²⁴ As a result of these studies, strict requirements were placed on the symmetry of the detector system and on the accuracy of the alignment of all beam-line components. Beam-line components are aligned to better than 2 mrad and mounted kinematically in order to retain the integrity of the alignment when components are removed for access or repairs. The detector alignment was checked after final beam-line buildup and detector placement using a theodolite and temporary crosshairs. The magnetic field was aligned prior to detector placement using a fluxgate magnetometer mounted on a translation stage. The alignment of both the proton and beta detector segments relative to their mounts was set precisely during assembly. Using measured values of A and B and simulating all possible asymmetries, we estimate that the alignment criteria above generates a maximum systematic uncertainty of approximately 10^{-4} . This can be confirmed by *in situ* systematic tests similar to those performed in the 1997 run.¹⁰

3. Statistical considerations

The emiT apparatus has a limiting statistical sensitivity of $1/(\vec{K} \cdot \vec{P} \sqrt{N})$, where N is the total number of coincidences, and \vec{P} and \vec{K} are as defined previously. Because the available beam is limited, it is necessary to maximize the counting rate, which is strongly affected by detector acceptance and configuration. A larger beam diameter (such as would be obtained with a larger collimator) increases the decay rate by allowing more of the available flux into the detector region. However, larger beam diameters increase the probability of misidentifying the sign of the triple correlation and thus decrease the sensitivity per decay; this effect manifests itself quantitatively as a smaller \vec{K} and is the reason behind the beam-related reduction in sensitivity discussed previously. A beam diameter of 6 cm was chosen as an acceptable compromise between these considerations and results in $|K| \approx 0.3$.

It is also important to maximize the solid angle of each detector segment. In the final detector design, the sensitive volume of the array is significantly longer than in previous experiments; moreover, the detector segments are configured with virtually no dead space between them so that both the proton and electron detectors cover nearly π radians.

A final important consideration regarding system sensitivity is the rate of background counts. Subtracting a large background increases the statistical error in the total number of counts and may also impact the counting rate itself by limiting the livetime of the system. Given the compact configuration of the detectors around the beam and the fact that

both the spin-flipper and current-sheet are activated by neutrons, beam-related backgrounds are a serious concern. These backgrounds are reduced greatly by a compound collimator design and the careful use of lead, concrete, and neutron-absorbing plastic shielding, particularly around the current-sheet spin-flipper. In addition, the beam stop is located as far from the detector region as possible. Other sources of noise in the detectors, such as high-voltage-related particle emission and thermal noise are addressed by careful electrode polishing and cooling to approximately -100 °C, respectively. Hardware energy and software timing cuts further reduce background rates. The overall beam-related background rate in all four beta detectors combined is below 300 s⁻¹, while the total rate of background events in the proton detectors is below 2 s⁻¹. Ultimately, a signal-to-background of better than 100 to 1 is achieved by requiring proton–beta coincidence.

B. Beta detector design

The sensitive region of the emiT beta detectors was fabricated from slabs of Bicron BC408 plastic scintillator cast to a thickness of 0.64 cm and diamond milled to a rectangular prism measuring 50 cm by 8.4 cm. The thickness of 0.64 cm is sufficient to stop a 1-MeV electron and is therefore adequate for detecting neutron decay betas, which have an endpoint energy of 782 keV. Scintillation photons are transported to either end of the scintillator by total internal reflection at the smooth surfaces, where they are ultimately detected by Burle 8850 photomultiplier tubes (PMTs). Although a greater scintillator thickness would have had the advantage of presenting lower light loss (the photons make fewer reflections during travel to the PMTs), this apparent advantage is outweighed in our case by the reduction in sensitivity to gamma ray background presented by a thinner section scintillator.

Each end of the scintillator is adhered to an ultrapure Lucite™ light guide with optical epoxy. The light guides adiabatically curve and transform to a circular cross section, so that they may be optically coupled to the PMTs. The guides curve and pass through an opening in an aluminum housing, which forms a vacuum-tight compression seal against the light guide with a buna o-ring. This design permits detector operation with the scintillator positioned inside the detector vacuum chamber while the attached PMTs remain external to the vacuum. Figure 6 presents a side view of a beta detector assembly.

During the first run of the emiT detector, it was observed that the beta detector exhibited large, continuous rates with occasional large spikes that correlated with breakdown of the proton acceleration electrodes. Subsequent tests determined that the majority of this rate was from electron field emission at points on the proton detector electrodes. This effect was mitigated by wrapping the scintillators in a layer of aluminum foil thick enough to stop a 40 keV electron. In addition, a wrapping of aluminized Mylar™ was placed beneath the foil. Grounding of both wrappings prevented the detectors from becoming charged.

PMTs do not function properly in magnetic fields. Since the uniformity of the guide field in the detector region is

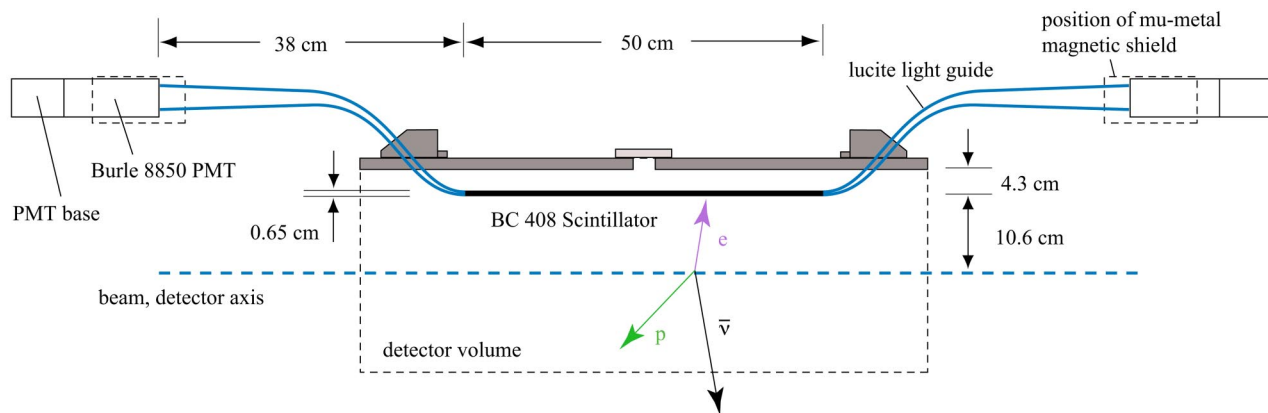


FIG. 6. (Color online) Side view of a beta detector.

critical, both mu-metal cylinders and active shielding were used on the PMTs to minimize stray magnetic fields. The active shields surround the mu-metal and are configured as a pair of nested, coaxial solenoids of equal length but differing in diameter. The current passing through each solenoid (in any pair) flows in opposite directions, and its value was chosen so that the resultant magnetic field at the PMT positions is nearly zero. Outside the solenoid pair, the field drops off rapidly since they are designed to have equal and opposite dipole moments. Thus, the field distortion they create at the detector center is an order of magnitude smaller than the distortion the mu-metal shields would otherwise create. An air-cooling system was installed around the tubes and bases inside the active magnetic shields to maintain temperature stability.

C. Proton detector design

Each of the four proton segments allowed for the placement of a 2×8 array of silicon surface-barrier diode detectors (Ortec AB-020-300-300-S). The detectors have an active layer $300 \text{ mm}^2 \times 300 \mu\text{m}$ and are positioned behind proton acceleration and focusing cells. Each cell consists of a grounded box with the top and the upper half of the sides covered by a grounded wire mesh (94% transmitting) through which the recoil protons enter. Once inside the box, the protons are accelerated and focused down the center of a cylindrical tube held at a high negative potential that was normally between -25 and -32 kV. A schematic representation of a focusing cell is shown in Fig. 7. Surface-barrier detectors have a room-temperature leakage current on the order of $1 \mu\text{A}$ and must be cooled to -100°C to achieve the necessary resolution. Located behind each detector is a pre-amplifier and cooling attachments. A fiber-optic (F/O) link was used to transmit analog signals from the preamps to the data acquisition electronics (see Secs. III C 1 and III C 2).

The focusing scheme serves two purposes: accelerating protons (750 eV maximum kinetic energy from neutron beta decay) to the energy needed to penetrate the dead layer and to be resolved adequately from the detector noise, and reducing the area of silicon needed to collect the protons. This reduction of the total diode area by a factor of 7 significantly reduces the noise generated by the detectors as well as the

associated cost. Monte Carlo simulations based on the SIMION²⁹ electrostatic modeling code indicate that the recoil protons that enter a cell are focused onto the detectors with very high efficiency (approximately 90%). Those protons not successfully focused enter very near a cell wall or at shallow incident angles. A few percent of these scatter, yet still strike the detector and add a small low-energy tail to the proton peak. The focusing efficiency is independent of the decay position within the beam and is not expected to be a source of systematic errors. Each proton panel ground plane is segmented longitudinally into eight pairs of square cells 4.0 cm on a side, providing the longitudinal segmentation required to further reduce the magnitude of the systematic effects.

An electronics rack is maintained at the same high voltage as the proton focusing system. This rack is isolated by a

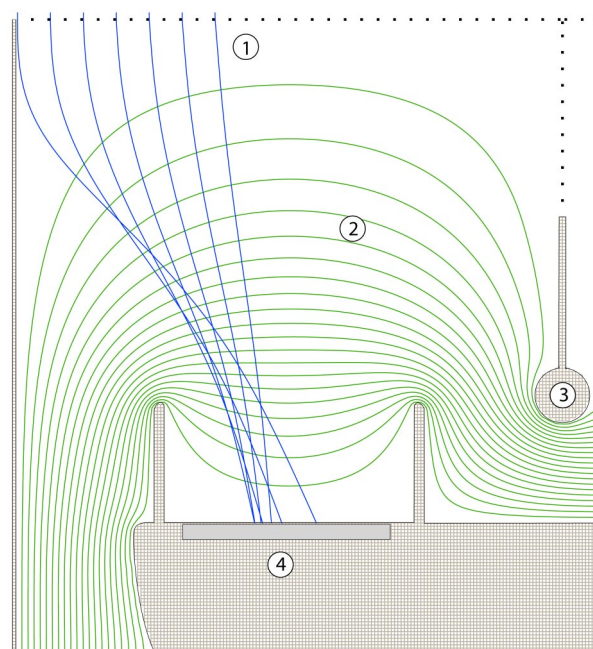


FIG. 7. (Color online) Schematic of a proton focusing cell showing (1) sample proton trajectories, (2) equipotential surfaces, (3) ground plane assembly, and (4) location of the surface-barrier detector in the high-voltage electrode. Protons entering the cell at a shallow angle can strike closer to the edge of the detector.

large transformer and housed inside a Faraday cage and protected by an interlock system. Contained in this high-voltage rack are the power supplies for the proton detector preamplifiers and F/O links as well as the detector bias voltage supply. The rack also contains a protection interlock for the detector bias leakage current as well as analog F/O outputs that allow low-voltage monitoring of both the total detector leakage current and bias voltage.

1. Analog optical link

Analog signals from the preamps are transmitted through F/O directly to the Shaper analog-to-digital Conversion (ADC) cards (see Sec. IV B). This allows the Shaper-ADCs, along with their VME crate and NIM electronics, to be at ground potential with only the power supplies held at high voltage. These electronics are then completely immune to potential damage resulting from high-voltage breakdown. This approach also reduces the size of the apparatus being floated at high voltage, decreasing its capacitance and the inductance of the lines connecting the high-voltage crate to the proton paddles. Both tend to reduce the odds of preamp damage.

The analog F/O link is built around the Hewlett-Packard HFBR 1526 light-emitting diode (LED) transmitter and HFBR 2526 receiver. A fast amplifier (LT1191) is used to drive the LED, and a second one to buffer the receiver into $50\ \Omega$ for the Shaper-ADC cards. The transmitter can be driven directly from the existing preamp output, and a receiver was incorporated into the custom Shaper-ADC boards with the option of either F/O or BNC input.

To minimize the contribution of the F/O link to the total noise level, the largest possible gain ahead of the F/O transmitter was desirable consistent with the dynamic range of the receiver and of the expected signals (see Sec. III C 2).

2. Proton detector preamplifiers

The proton signals generated by the silicon surface-barrier diode detectors are relatively small (approximately 8300 ion pairs for a proton acceleration potential of 30 kV); moreover, the capacitance of the surface barrier is approximately 80 pF when fully depleted. Accordingly, it was necessary to design and build low-noise preamplifiers for use with high-capacitance detectors. The emiT preamp has two gain stages. The input stage is a folded cascode amplifier with an Interfet IF4501 input field-effect transistor (FET), which has a capacitance of 35 pF and g_{fs} of 15 mS. A 1 pF capacitor in parallel with a $1\ \text{G}\Omega$ resistor provide negative feedback. The second stage consists of a bipolar folded cascode amplifier buffered with a Darlington emitter follower. The preamp has an overall gain of approximately $9.5\ \text{V}\ \text{pC}^{-1}$ with a 60 ns rise time.

Due to the potential for damage from high-voltage breakdown, care was taken to provide the preamps with some protection against impulse currents. The output stage was clamped to the $-6\ \text{V}$ supply and to ground through a Zetex BAV99 dual diode. In addition, a $50\ \Omega$ resistor was added in series with the output line. Finally the input FET gate was clamped to the $-6\ \text{V}$ power supply through an In-

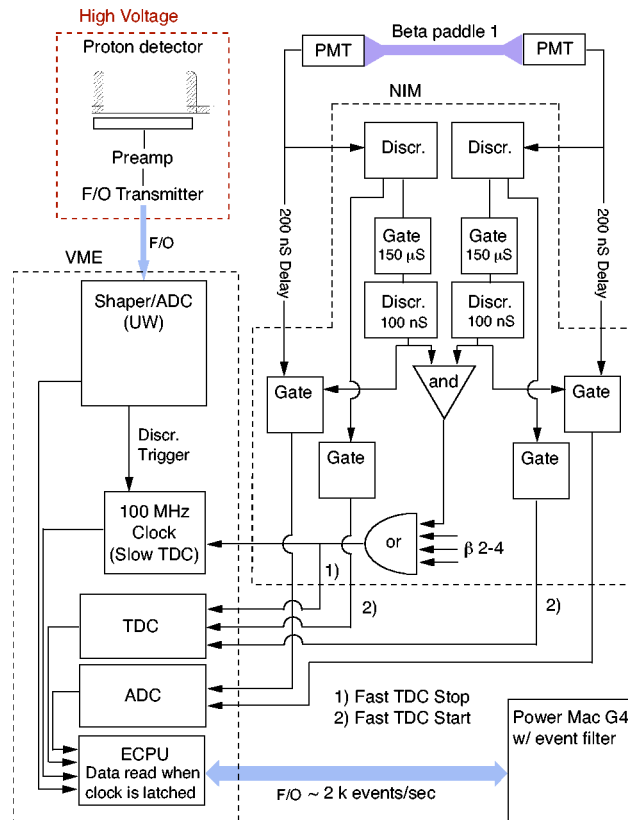


FIG. 8. (Color online) A schematic representation of the emiT data acquisition system.

terfet PAD1 low leakage diode and self-clamped to ground through the intrinsic gate–source junction of the FET.

As the leakage current, and hence the performance, of surface barrier detectors is strongly temperature dependent, considerable attention was given to minimizing the power consumption. Heat dissipation in vacuum (approximately 15 mW per channel) was aided by the use of high thermal conductivity ceramic substrates (Rogers RO4350B). The overall proton paddle design is a 16-channel motherboard mounted behind the focusing tubes that clamps the detectors in place. The majority of components are surface mount on interchangeable in-line modules.

IV. ELECTRONICS AND DATA ACQUISITION

The electronics used to run emiT consist of VME and NIM electronic modules. A block diagram of the hardware setup is shown in Fig. 8. Analog signals from the proton segment preamplifiers are carried by four F/O bundles directly to custom VME-based shaping and ADC cards. Two NIM bins contain the logic electronics for the beta and proton detectors, spin-flip control, and the hardware triggers. The beta detector PMTs are read out by VME-based charge integrating ADCs and relative timing of the PMTs are recorded in time-to-digital conversion (TDC) units. A Motorola MVME 167 embedded computer (EPCU) provides real-time readout of the proton detector and beta detector electronics, scalars, and also the slowly varying analog signals (e.g., magnet currents and applied high voltages) used to monitor the status of the experiment.

A. Proton detector signal processing

The Shaper-ADC boards used to collect data from the surface barrier arrays are custom-built eight-channel modules. Each channel has a four-stage integration shaping network and an independently controlled level-crossing discriminator. The peak detection circuit consists of a transistor-buffered, dual-differentiating network. Shaped pulse conversion is accomplished via a 12-bit ADC and read out through the standard VME bus. Each board also contains scalars that can be used to monitor trigger rates on individual channels as well as the total board trigger rate. The boards support an external inhibit as well as a fast clear function. The boards are controlled through an Altera 9480 series field programmable gate array (FPGA) and can be run independently or in parallel with additional boards.

The VME boards were designed to accept negative pulses from 5 to 3000 mV in amplitude, depending upon the gain setting. In order to allow adjustment of the dynamic range of the boards, a Maxim MAX 7524 multiplying digital-to-analog (DAC) converter is inserted between the first and second shaper stages. This allows for 254 steps of individual channel gain adjustment via VME control. Individual channels can also be remotely disabled by setting the gain to zero.

The on-board shaping network consists of four successive 0.5 μ s integrators and a 50 μ s preamplifier tail cancellation circuit. The integration operations are done primarily by op-amps. Peak detection is accomplished with a transistor-buffered network. This circuit provides a steep-sloped bipolar pulse, centered on the peak of the shaped signal. The differentiated signal is amplified using an op-amp and fed to a comparator. The shaped signal is first compared to a dc level provided by a programmable buffered Analog Devices AD7226 DAC. A signal of sufficient amplitude then results in the assertion of a sample and hold (S/H) when the differentiated shaped pulse crosses zero. This method allows for user-defined pulse height discrimination with minimal S/H timing walk.

The logic to run the VME interface is programmed directly into the Altera FPGA. Only VME line buffers are required outside of the FPGA. The interface to VME uses 16 address and 16 data lines. The board design does not include on-board memory and so must be operated in a polling read-out mode.

B. Beta detector signal processing

The individual PMTs charge information as well as the relative timing between the two PMTs are recorded for each beta scintillator paddle. Charge information is recorded using CAEN Model V862 12-bit individually gated charge to digital converters (QDCs). The relative timing between the PMTs is measured using CAEN Model V775 8-bit TDCs. Signals from the phototube bases are passively split and one-half is delayed in cable by 200 ns (β_{Delayed}). The other half goes through a discriminator whose threshold is set to be just above the single photoelectron peak. The output of the discriminator is double gated: the first gate of approximately 150 μ s reduces the effect of after-pulsing, and the second

gate of 100 ns allows for the transit time of a photon across the length of a beta paddle. This signal is then split, with the first half starting a TDC (CAEN Model V775 8-bit TDCs). The second half is used to require a coincidence (β_{AND}) between the two ends to the paddle (a 100 ns window coming from the previous gate). A logic fan-in of the β_{AND} s from each paddle is used to form a logic or (β_{OR}). β_{OR} is used as a trigger for latching a register on the latched clock trigger board, as a global stop for the TDCs, and as a gate for QDC conversion of β_{Delayed} .

C. Hardware and trigger logic

A VME-based 100 MHz latched clock trigger board was designed to provide relative timing of both proton and electron singles events. Two Altera programmable logic devices (PLDs) were used. An EPM9320, 208-pin 20 ns chip is used to provide the 32-bit VME interface. An EPF10K10 series 144-pin 3 ns chip is used for the 56-bit 100-MHz counter and five individually latched 56-bit registers. Four of these registers are latched by transistor-transistor logic inputs from either the electron, proton, spin-flip, or monitoring logic, and one register is latched by a software command. Each register has an inhibit output that is asserted when the register has been latched. This inhibit output is used to disable further proton or beta signal conversions, until the conversion hardware has been read out. Once the latched register is read the inhibit signal returns to logic zero and the conversion of the proton or beta signals is once again enabled. Logic outputs reflecting any discriminator level crossings in the Shaper-ADC boards are combined in a logical OR to provide a trigger for latching the proton register on the timing board. Data is acquired as follows. A hardware trigger, for example a coincidence between two ends of a beta paddle, causes a latch of the beta register of the latched clock trigger card. This sets an inhibit that blocks further triggers in the beta logic. The EPCU polls the timing board on a regular basis and if any register has been latched, a read of the appropriate QDCs and TDCs is initiated. The inhibit is then cleared and data acquisition is resumed. A similar process is followed for proton events. Data are written into a local VME dual-port memory configured as a circular buffer. The dual-port memory, which is located on the SBUS Model 620 VME to PC controller is simultaneously read out by the data acquisition user interface computer, a Macintosh G4. This computer then displays real-time monitoring information and records the data to disk.³⁰

D. Monitoring and spin-flip control

An XYCOM 200 with programmable I/O lines and built-in counter timers is programmed to generate two periodic timed outputs that initiate either a spin-flip sequence or a full monitoring readout throughout the data collection run. Monitoring of hardware is accomplished using VME-based 12-bit ADCs (Acromag IP 220) and scaler counters (LeCroy 1151). Rates in the beta detectors, proton detectors, and beam fission monitor are tracked in the scalars. In addition, proton paddle temperature, detector bias, and leakage current are converted to frequency for optical transmission from

high voltage, and are also tracked in the scalars. Magnetic coil currents, LN₂ fill controls, and vacuum status are monitored using the ADC modules. Time stamping is accomplished using the latched clock trigger card discussed earlier. These data are then output into the event mode data stream. Of the 50 parameters, 35 are used for alarms. When a value exceeds acceptable bounds a pager-based alarm system is activated, allowing for a timely maintenance response.

V. BETA DETECTOR PERFORMANCE

The four beta detectors were initially tested off-line using radioactive sources to determine the optimal operating voltages of their respective pairs of PMTs. Once operating at the appropriate voltage, the detectors were characterized to obtain parameters for energy calibration, detector light loss, energy and timing resolution, and uniformity of both the hardware trigger and energy response.

For each detector, an initial calibration was obtained from the 976 and 200 keV conversion electron peaks of ²⁰⁷Bi and ¹¹³Sn sources, respectively. The significant Compton continuum present with the ²⁰⁷Bi source was suppressed by requiring a coincidence with pulses from a thin (0.5 mm) scintillating disk placed between the source and the beta detector. All incident electrons from the conversion source passed through this disk, but only a small fraction of Compton electrons produced a coincidence signal. In order to obtain an accurate calibration, the energy loss in this disk must be accounted for. This energy loss (94 keV for 976 keV electrons) was measured in a separate experiment using a calibrated surface-barrier detector to determine the shift in the peak position with and without the disk in place.

After matching PMT gains with the source positioned at the detector's center, each source (in turn) was scanned with two orthogonal linear translation stages across the face of each detector to measure the response as a function of position. The variation of the efficiency as a function of position was shown to be less than a few percent. In addition, data from this scan were used to measure the light-collection efficiency and attenuation lengths.

A pulsed nitrogen laser system was used to verify the stability of the beta detectors over time. The laser light output was normalized through an optical fiber coupled to a separate scintillation detector with an attached ²⁰⁷Bi reference source. During testing, no PMT drift larger than the 5% accuracy of the monitor was observed.

To test the beta detector timing response, we used the laser coupled to an optical fiber and a ⁹⁰Sr source that was encased in a brass howitzer and released a narrow beam of electrons through a small tunnel on one end. Both sources illuminated only a very small region of the scintillator. We measured the full width at half-maximum (FWHM) of the end-to-end relative time for various energies as a function of discriminator level and saw that a minimum was reached at all energies for thresholds of 100 mV and below. For higher energies near the neutron beta endpoint, this minimum width (Δt) was approximately 0.5 ns and increased to about 1.3 ns at 200 keV. Measuring the shift of the time peak as we moved the source gave an effective velocity v_{eff} for the scin-

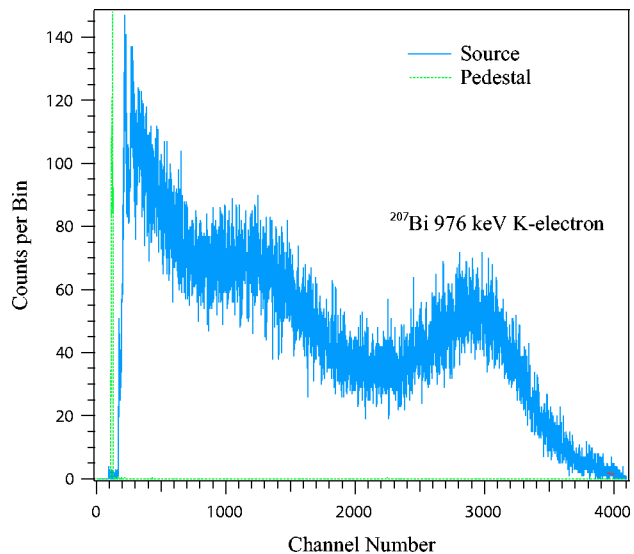


FIG. 9. (Color online) A ²⁰⁷Bi calibration spectrum from a single beta detector taken *in situ*. The higher energy peak is at 976 keV with a resolution of approximately 18%. The structure that peaks at approximately channel 1100 is due to a combination of a conversion electron line at 481 keV and Compton scattering from 569 keV gammas.

tillation light of about 16 cm ns⁻¹, which allowed us to extract beta position with a resolution between 4 and 10 cm, given by $\Delta x = \frac{1}{2} v_{\text{eff}} \Delta t$.

Due to mechanical restrictions, the response of the segments was measured *in situ* using only the ²⁰⁷Bi conversion source without an external trigger. The PMT gains were set to place the 976 keV conversion electron peak at about channel 3000 of the 4096-channel 12-bit ADCs. Measurements showed a resolution of about 18% at this energy. A typical spectrum is shown in Fig. 9.

A random trigger that forced integration of the background noise was used to determine the position of the pedestal. Using a calibration based on the pedestal and the 976 keV conversion electron peak, the beta energy thresholds were determined to be about 35 keV for three of the paddles and 50 keV for the fourth. The fourth paddle required a higher threshold because the dark current in one of the phototubes was higher than expected.

When installed on the beam line, each beta detector had a trigger rate of about 40 s⁻¹ with the local beam shutter closed and the proton detector high voltage set to zero. This background was due primarily to reactor related backgrounds that penetrated the shielding, but also came from cosmic rays and dark current in the PMTs. Opening the local beam shutter increased the total singles rates to about 300 s⁻¹ including decay electrons. In contrast to the first run of emiT, the background was not dependent on the proton detector acceleration voltage.

VI. PROTON DETECTOR PERFORMANCE

The surface-barrier detectors were specially manufactured to have an entrance window of 20 μg cm⁻² Au, half the normal thickness. This was important because it reduced the energy loss in the insensitive region (dead layer) of the detector. The reduced energy loss allowed the use of lower

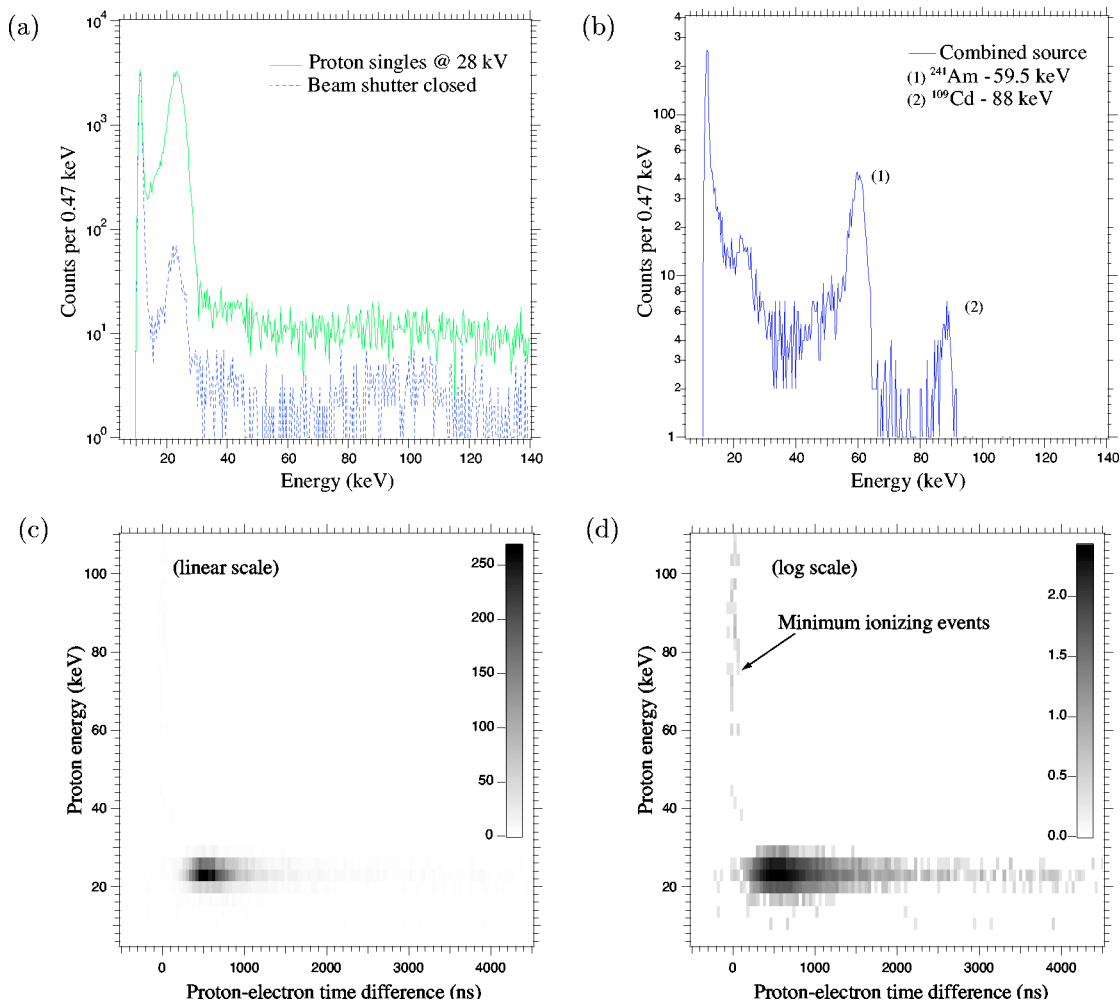


FIG. 10. (Color online) Proton energy calibration data from one of the highest resolution surface-barrier detectors. (a) Pulse height singles spectra for a typical 4 h run with beam-on (solid line) and beam-off data (dashed line). For the beam-on data, the peak at 25 keV is dominated by neutron decay protons accelerated by the applied 28 kV potential. For the beam-off data, the much reduced peak at 25 keV arises from background protons created by high-voltage emission; the total rate for these background protons is below 0.06 s^{-1} for all detector channels. (b) Spectrum from ^{241}Am and ^{109}Cd sources. The FWHM is 4.8 keV at the 59.5 keV line. (c) Surface barrier-scintillator coincidence data from a typical 4-h run showing proton energy vs delay time. (d) Log plot of the data shown in (c); events near $\delta t=0$ are prompt coincidences due primarily to beam-related backgrounds. The very low background rate is also apparent.

acceleration voltages, decreasing the rate of high-voltage breakdown and reducing high-voltage associated backgrounds. Surface-barrier detectors were chosen to replace the PIN diodes used in the first run because low-energy protons lose a calculated 2 keV in the $20 \mu\text{g cm}^{-2}$ gold front entrance window (electrical contact), compared to 12 keV in the same thickness of Si.³¹ Clearly this also helps to mitigate potential high-voltage related problems by allowing operation at lower acceleration voltages. To verify the performance and dead-layer thickness of the proton detectors prior to moving the apparatus to the neutron beam line, we constructed a duo-plasmatron source to produce a low-energy (zero to a few hundred eV) proton beam. The source attached to the downstream end of the detector. The proton beam was collimated and entered the chamber where it Rutherford scattered off a movable Al target and struck the selected detectors.³²

In addition to careful characterization of the surface-barrier detectors, an extensive investigation of the unexpected high-voltage related background seen during the first

run was carried out. It was found that high electric fields around the edge of the focusing tubes caused electron field emission. This resulted in two sources of background: bremsstrahlung and ionization of adsorbed hydrogen on the focusing assembly ground plane. These ions are accelerated back into the detectors in exactly the same manner as a decay proton, yielding a background that cannot be removed by cuts on proton energy. To eliminate this background, the focusing tubes were redesigned to produce lower electric fields and carefully polished. As a result, this source of background was nearly eliminated. This is clear from Fig. 10(a), which shows a typical 28 kV proton energy spectrum (taken without the requirement of an electron coincidence) and a typical beam off spectrum. The peak is made up of protons originating almost entirely from neutron decay. The singles rate in each proton detector is approximately 3 s^{-1} . The rate of the high-voltage-related background varied somewhat from channel to channel; however, during typical running conditions it was never above 0.06 s^{-1} per channel.

During testing and early running a large number of

surface-barrier detectors suffered from a variety of unexplained problems including abnormally high leakage current and breakdown at voltages well below nominal operating voltage. However, after biased operation in vacuum for times on the order of a month, most detectors behaved well. Energy resolution ranged from 4.5 to 8 keV and was sufficient for our purposes. Typical dead-layer energy loss was about 5 keV. This is larger than the calculated value based on the thickness of the gold contact because of additional losses in inactive silicon directly below the gold contact.

Figure 10(b) shows an energy calibration spectrum using an ^{241}Am source together with a ^{109}Cd source. The FWHM of the 59.5 keV line is 4.8 keV. Figures 10(c) and 10(d) show proton events correlated with a beta trigger. In Fig. 10(d) (logarithmic scale), one can see a prompt background signal (vertical stripe) that is associated with the neutron beam. These events are typically above 80 keV and are very well separated from the decay protons. At the same energy as the proton peak, but not clearly resolved in the plot due to its small amplitude, is a band of recoil protons for which the coincident electron was not detected. This band makes up the dominant background in the recent run. The coincidence efficiency varies across the front face of the proton paddle but was calculated to be approximately 20%. Coincidence event rates were measured to be in the range of 0.55 to 0.62 s^{-1} for the paddle end and center, respectively. The overall coincidence rate is greater than 30 s^{-1} with a signal-to-background of better than 100 to 1.

It is clear that the performance of the detector has been greatly improved since the first run. As shown above, the data quality is high and all known systematic effects are under control. We expect that the current run will reach a statistically limited sensitivity to D of 2×10^{-4} . Systematic uncertainties should be below 1×10^{-4} .

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