# The effect of chemical dispersant concentration on hydrocarbon mobility through permeable North-East Scotland sands

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## 30 Highlights:

- Chemical dispersant increased the mobility of hydrocarbons through permeable sands.
- Chemical dispersant enhanced entrainment of oil below manufacturer recommended
   dosing.
- Chemical dispersant selectively entrained hydrocarbons based on their solubility in
   water.

## 36 Abstract:

37 Accidental releases of oil to the marine environment can reach sensitive shorelines resulting in a wide range of environmental impacts. Chemical dispersant is a response tool employed to 38 39 minimise damage to coastal ecosystems by facilitating dispersal of oil slicks before they reach 40 shores. However, chemical dispersants may increase entrainment of hydrocarbons into coastal 41 sediments following an oil spill, resulting in higher hydrocarbon residence times in sediments. 42 Here, the effect of dispersant concentration on the entrainment capability of hydrocarbons in 43 permeable coastal sands from North East Scotland (United Kingdom) was evaluated. 44 Hydrocarbon entrainment into sands was facilitated by dispersant application at concentrations 45 below manufacturer-recommended dosage. Percolation of water-soluble hydrocarbons beyond 46 10 cm deep was not affected by chemical dispersant application and water-insoluble 47 component concentrations increased with dispersant concentration. Results highlighted that the 48 application of dispersant readily mobilised less water-soluble hydrocarbons through coastal 49 sands but did not affect pore-water transport of more water-soluble hydrocarbons.

50 Keywords: oil, transport, percolation, sediment, dispersant

# 51 **1 Introduction**

Accidental oil releases to the marine environment result in a wide variety of environmental impacts. These are partly determined by the extent to which the oil evaporates, disperses and biodegrades in the water column, settles on the seabed and reaches shores, among other fates (Bandara et al., 2011; Davies and Tibbetts, 1987; Ramseur, 2010). Documented accidents such as the *Deepwater Horizon (DwH)*, *Prestige* and *Exxon Valdez* oil spills resulted in extensive coastal oiling and subsequent environmental impacts which are detectable to this day (Beyer
et al., 2016; Levine et al., 2017; Payne et al., 2008).

59 Chemical dispersants were widely used during DwH response operations in an attempt to 60 mitigate its environmental impacts, with 5.3 million litres of dispersant applied at the sea 61 surface and 2.9 million litres at the wellhead (~1500 m deep). Dispersant use remains 62 controversial but has been shown to be beneficial under specific circumstances (Prince 2015). 63 The aim of dispersant application is to disperse insoluble and persistent hydrocarbons by 64 dispersing and dissolving oil as small droplets to increase their surface area with the end goal 65 of accelerating physical, chemical and biological oil degradation (Fingas, 2002). Additionally, dispersant was applied at the wellhead during DwH to facilitate the removal of volatile 66 67 hydrocarbons from surfacing oil and reduce the risks of uncontrolled ignition of volatile hydrocarbons on surface waters and inhalation by oil spill responders (International 68 Association of Oil & Gas Producers, 2015). Dispersant increases oil bioavailability by 69 70 increasing its accessible surface area and enabling microbes to access and utilise oil faster 71 (Hazen et al., 2010). However, by increasing oil bioavailability, dispersant also facilitates the 72 uptake of hydrocarbons by fauna such as filter feeders, marine mammals, seabirds and 73 commercially harvested fish, and can thus result in negative effects for both the marine 74 environment and reach humans through accumulation in the food chain (Beyer et al., 2016). 75 Moreover, dispersants have been found to be toxic to marine organisms and be more persistent 76 than previously thought (White et al., 2012).

77 Dispersed oil, whether mechanically or chemically dispersed, that reaches shorelines can be 78 entrained into sediments where it can persist for decades and act as a reservoir from which contaminants can enter the food chain (Payne et al., 2008). If polyaromatic hydrocarbons 79 80 (PAHs, hereafter) reach anoxic sediments biodegradation may be limited and consequently 81 higher PAH half-life in sediments could be expected (Widdel et al., 2010). Whilst the mobility 82 of PAHs is especially relevant due to their carcinogenicity and persistence, entrainment of 83 hydrocarbons from other fractions (such as aliphatics and Benzene, Toluene, Ethyl benzene 84 and Xylene, BTEX hereafter) is relevant as these have been shown to induce an environmental 85 response, particularly in microbial communities (Phelps and Young, 1999). BTEX components 86 are far more water-soluble than PAHs, potentially being carried into permeable sediments more 87 readily.

88 Oil contact with sediments is particularly undesirable because of the well-known 89 environmental impacts it causes, the difficulty involved in restoring habitats and the damage 90 to the reputation of the responsible party (Beyer et al., 2016; Zuijdgeest and Huettel, 2012). 91 Consequently, understanding the potential entrainment of spilled oil into sediments in coastal 92 environments is relevant. During DwH, the shorelines of Louisiana and other southern states 93 of the United States were severely affected by beached oil (Nixon et al., 2016). Zuijdgeest and 94 Huettel (2012) assessed the entrainment potential of mechanically and chemically dispersed 95 MC525 oil (using Corexit 9500A) and found that mobility of Total Petroleum Hydrocarbons 96 (TPH, hereafter) and PAHs was increased when a 1:100 Corexit 9500A to oil ratio was applied 97 due to Corexit increasing the solubility of hydrocarbons.

98 Over 70% of the seabed of the North Sea is characterised as fine sand (Paramor et al., 2009). 99 Sandy seabeds are highly permeable and therefore facilitate pore-water flushing. Permeable 100 continental shelf sediments contribute significantly to benthic biogeochemical cycling and 101 primary production (Huettel et al., 2014). This highlights the importance of understanding the 102 capability of hydrocarbons to entrain permeable sediments, which may affect upstream 103 ecological processes should a large-scale oil spill take place.

104 The aims of this work were to evaluate the potential of spilled hydrocarbons to be entrained 105 into permeable sands and the effect of concentration of a commercially available dispersant 106 stockpiled in the United Kingdom (Superdispersant-25, SD25 hereafter) on this process using 107 Schiehallion crude oil and a synthetic oil (model oil, hereafter). A synthetic oil was used as it 108 gives a good intermediate between a single hydrocarbon and a crude oil. Additionally, the use 109 of a synthetic oil enabled a constant mixture that could be replicated and compared between experiments. A further objective was to elucidate if SD25 selectively mobilised components of 110 111 different fractions of hydrocarbons at increasing SD25 concentration. The hypotheses of this 112 study were: (1) The effects of SD25 on hydrocarbon entrainment into sediments would be 113 observable from below manufacturer recommended application doses, (2) increasing SD25 114 concentration would increase the entrainment of hydrocarbons and would be less effective in 115 facilitating entrainment of the more soluble components of the model oil (such as BTEX and 116 naphthalene) and (3) Oils would readily entrain permeable sands and may do so to different 117 extents due to the difference in composition of the Schiehallion crude and model oils.

# 119 2 Materials and methods

## 120 2.1 Study site

- 121 The present study was conducted using intertidal sandy sediment collected at the mouth of the
- 122 Ythan estuary (57°18'25.2"N 1°59'13.2"W), which is located 10 km to the north of Aberdeen,
- 123 North East Scotland (United Kingdom, Figure 1).



124

Figure 1. Location of sampling station (purple pin), Ythan estuary, North East Scotland, UnitedKingdom.

The estuary's intertidal area has been estimated at  $1.85 \text{ km}^2$ , with a tidal flushing time between </br/>
<14 hours (Balls, 1994) and 5–12 days (Leach, 1971). The sampling location chosen for this study was at the front-face of the beach. Samples were collected on December 2015 using acrylic cores (internal diameter = 3.6 cm, length = 30 cm) (small cores, hereafter) for sediment analysis and percolation experiments. Further samples were collected using larger cores (internal diameter = 10 cm, length = 30 cm) (large cores, hereafter) to measure permeability. Seawater was collected from the site and UV-filtered (0.5  $\mu$ m filter). Salient salinity and *p*H of water used were 35 and 7.5, respectively. The Ythan estuary has been chosen as the study site for this work due to its proximity to oil and gas offshore installations in the North Sea. These sands are representative of Scottish intertidal sands. Moreover, the Ythan Estuary is classified as a Special Protection Area under Article 4.1 of the Birds Directive (79/409/EEC, code: UK9002221, Natura 2000 network), highlighting the importance of understanding the implications of oil beaching in this region.

## 140 2.2 Sediment characterisation

All analyses detailed below were conducted on three replicate cores each, which were sectioned 141 into four 2.5 cm sections (i.e. 0-2.5, 2.5-5, 5-7.5 and 7.5-10 cm). Each section was 142 143 homogenised and subsamples subsequently oven dried at 60°C for three days and mechanically 144 milled to ensure uniform grain size. Total carbon content (TC) was determined using an 145 NA2500 elemental analyser (Carlo Erba Instruments). Total organic carbon content (TOC) was 146 determined by acidification of sediment samples with 10% HCl acid, overnight drying at 60°C 147 and subsequent carbon content quantification. Total inorganic carbon (TIC) content was 148 determined as the difference between TC and TOC.

For analysis of grain size distribution, a separate set of subsamples was dried overnight at 105°C and subsequently sieved through decreasing mesh sizes (diameter = 2000, 1000, 500, 250, 125 and 63  $\mu$ m). Statistical analyses for the particle size distribution were performed using Gradistat v.8 (Blott and Pye, 2001).

Saturated hydraulic conductivity ( $K_s$ ) was measured using a UMS KSat benchtop saturated hydraulic conductivity instrument using the falling head method (Head, 1982). Three large cores were divided into two sections of depth ranges 0–5 cm, and 5–10 cm. Sectioned sediment samples were saturated with degassed, deionised water prior to recording of the  $K_s$  value to ensure no air bubbles were retained within the sediment, which might otherwise distort the measurement. Triplicate measurements were taken for each sample to ensure representative  $K_s$ values. Permeability (k) was derived from  $K_s$  by the equation:

160 
$$k = \frac{K_{\rm s} m}{\rho g}$$

161 Where  $\rho$  and *m* are the water density (g cm<sup>-3</sup>) and viscosity (g cm<sup>-1</sup> s<sup>-1</sup>), respectively, and *g* is 162 gravity (9.81 m s<sup>-2</sup>).

## 163 2.3 Critical Micelle Concentration of Superdispersant-25

164 The apparent critical micelle concentration (CMC) of SD25 was measured following a similar 165 approach to that used by Gong et al. (2014). Briefly, three stock solutions of SD25 in seawater 166 were prepared  $(327 \pm 1 \text{ mg l}^{-1})$  and these were diluted with several volumes of seawater and 167 were measured for surface tension using a tensiometer (Attension, Sigma 700) fitted with a Du 168 Noüy ring (triplicate measurements for each sample). Surface tension was then plotted against 169 logSD25 concentration (mg l<sup>-1</sup>). A value of zero was allocated to log(SD25 concentration=0) 170 (mg l<sup>-1</sup>) for the purposes of establishing the apparent CMC. Thereafter, the change in gradient 171 was used as a boundary to calculate two linear regressions and establish their intersection point 172 which was inferred to be the CMC (Gong et al., 2014).

#### 173 2.4 Oils used in percolation experiments

174 A North Sea crude oil (Schiehallion) and a model oil were used in this investigation. The SARA 175 analysis of the Schiehallion crude oil was undertaken externally (Intertek, ITS Testing 176 Services, United Kingdom) and the mass percentage of the four fractions was found to be: 177 saturates 51.33%, aromatics 32.20%, resins 14.87% and asphaltenes 1.5%.  $C_{10-30}$  were the most 178 abundant hydrocarbon chain-lengths in the Schiehallion crude oil (Supplementary Figure 1). 179 The model oil was composed of 21 hydrocarbons including BTEX, aliphatic, PAH and resin 180 fractions (Ferguson et al., 2017). The model oil was based on the Schiehallion crude oil to 181 enable a comparison to the crude and analyse the fate of all its components individually. The 182 model oil contained hydrocarbons larger than C<sub>8</sub> because these are more readily deposited on 183 the seabed. Details of the percentage composition by component and fraction can be found in 184 Table 1.

- 186 Table 1. Synthetic oil composition and selected properties of its components. Octanol-water coefficients
- 187 were obtained from literature: (a) Sangster et al. (1989), (b) Mackay et al. (2006), (c) ChemSpider
- 188 website, (d) Sigma Aldrich website.

Hydrocarbon	Hydrocarbon class	Molecular weight (g mol <sup>-1</sup> )	Octanol- water coefficient (log Kow)	Percentage composition	Sonication extraction efficiency (%)	Liquid-liquid extraction efficiency (%)
Ethyl-Benzene	DTEV	106.165	3.15 <sup>b</sup>	6.1	$97.4 \pm 0.1$	$88.5 \pm 7.3$
m-Xylene	DIEA	106.165	3.20 <sup>b</sup>	6.0	$97.9\pm0.1$	$88.7\pm7.2$
o-Xylene	(18.0%)	106.165	3.12 <sup>b</sup>	5.9	$99.3\pm0.7$	$89.5\pm7.0$
Decane		142.282	6.25 <sup>a</sup>	9.0	$99.1\pm0.0$	$89.2 \pm 7.0$
1-Decene		140.266	4.70 <sup>b</sup>	9.1	$98.2\pm0.6$	$88.7\pm7.2$
Dodecane		170.334	$6.80 \pm 1.00^{a}$	9.0	$99.9\pm0.0$	$89.4 \pm 7.1$
Tetradecane		198.388	$8.00^{a}$	9.2	$100.3\pm0.1$	$88.7\pm6.9$
Pentadecane	Alimbotion	212.415	7.50 <sup>b</sup>	6.2	$101.0\pm0.2$	$89.0\pm7.0$
Hexadecane	Anphaucs (580()	226.441	8.00 <sup>b</sup>	8.8	$101.2\pm0.2$	$88.3\pm6.8$
Heptadecane	(38%)	240.468	8.50 <sup>b</sup>	1.5	$101.1\pm0.0$	$88.7\pm7.1$
1-Octadecene		252.478	9.81°	1.4	$101.2\pm0.7$	$88.0\pm6.9$
Eicosane		282.547	10.0 <sup>b</sup>	1.6	$101.6\pm0.5$	$87.5 \pm 7.2$
Docosane		310.601	12.44 <sup>c</sup>	1.4	$101.8\pm0.4$	$88.1\pm7.0$
Tetracosane		338.654	12.0 <sup>b</sup>	1.5	$102.4\pm0.2$	$87.8\pm7.8$
Naphthalene		128.171	3.43 <sup>b</sup>	5.4	$99.9\pm0.7$	$89.3 \pm 6.9$
Fluorene		166.219	4.18 <sup>a</sup>	3.1	$101.1\pm0.4$	$89.3\pm6.2$
Phenanthrene	PAHs	178.229	4.52 <sup>a</sup>	3.0	$100.4 \pm 1.3$	$89.2 \pm 6.0$
Anthracene	(18.2%)	178.229	4.50 <sup>a</sup>	0.7	$84.9\pm4.0$	$86.9\pm6.4$
Fluoranthene		202.251	5.20 <sup>a</sup>	3.1	$101.7\pm1.0$	$89.7 \pm 6.4$
Pyrene		202.201	5.17°	3.0	$101.8 \pm 1.1$	$89.6 \pm 6.5$
Dibenzothiophene	Resin (4.9%)	184.257	4.38 <sup>a</sup>	4.9	$101.0\pm1.7$	$89.2\pm6.4$

189

## 190 2.5 Percolation experimental set-up

191 Solutions of SD25 in seawater were prepared by adding SD25 to seawater in one-litre 192 volumetric flasks. Thereafter, SD25-seawater solutions were magnetically stirred at room 193 temperature for 24 h to allow equilibration of SD25 in seawater. Immediately before 194 percolations were performed, 100 ml of each solution was spiked with 1 g of oil and sonicated 195 (45 kHz) in a USC-TH Ultrasonic bath (VWR) for 3 min to produce a proxy oil in water mixture 196 to emulate the consequences of mechanical mixing of oil and water by waves and tides. The 197 percolation experiment was based on a short column experiment by Zuijdgeest & Huettel 198 (2012) with some modifications (Figure 2).





200 Figure 2. Percolation experiment setup.

201 Samples were extruded from the small cores used for collection and transferred to Pyrex cores 202 of the same dimensions. Care was taken to avoid alteration to the sedimentary structure. The cores were then fitted with a gauze-lined stopcock to prevent blockage by sand. Sediment in 203 204 cores was then saturated with uncontaminated seawater, after which mixtures of oil and SD25 205 at various concentrations (Table 2) were added to the cores avoiding sediment resuspension. The highest concentration (333.3 mg l<sup>-1</sup>) corresponds to the lower boundary of the 206 207 manufacturer's recommendations (1:30 dispersant to oil ratio). Immediately after the addition 208 of the mixtures, the stopcock was opened to allow percolation of the mixtures through the sand 209 until the water level reached the sediment surface. Washout water was collected and a further 210 100 ml of non-contaminated water were percolated through the cores using the same method. 211 The combined washout oil-dispersant-seawater solution was collected in separating funnels 212 and hydrocarbons were extracted within minutes. Sediment was then extruded and sectioned 213 by depths (0.0-1.0, 1.0-3.0, 3.0-5.0, 5.0-7.5, 7.5-10.0 cm) for hydrocarbon extraction and 214 analysis. The use of natural, undisturbed sediments was decided following preliminary 215 experiments where mixed sand from the upper 10 cm were carried out and showed that mixing 216 (homogenising) sand resulted in enhanced entrainment and therefore overestimated 217 entrainment in Ythan estuary sands (Supplementary Figure 2).

218	Table 2. Superdi	spersant-25 (SD25	) concentrations	applied to the	oils used.
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Oil type		SD25 concentration (mg l <sup>-1</sup> )					
Control	0	-	-	-	-	-	
Schiehallion crude oil		-	-	-	-	333.3	
Synthetic oil	0	9.8	21.1	42.0	150	333.3	

## 219

## 220 2.6 Hydrocarbon extraction and analysis

221 Hydrocarbon extractions from sediment were performed by sonicating each sediment section 222 in 50 ml of dichloromethane for 10 min for model oil-contaminated samples. The procedure 223 was performed in triplicate for the Schiehallion crude oil-contaminated sediment extractions. 224 Extractions from washout water were performed by liquid-liquid extraction with  $3 \times 25$  ml 225 dichloromethane for both oil type-contaminated sediments. Hydrocarbons were quantified 226 against external standards containing known concentrations of the model oil components. 227 Hydrocarbon recovery efficiencies for each component can be found in Table 1. Schiehallion 228 crude oil extractions were subsequently rotary-evaporated at 40°C until all dichloromethane 229 had evaporated. Model oil extracts were analysed by gas chromatography (GC, hereafter) with 230 flame ionizing detection using a previously described system (Ferguson et al., 2017). When no 231 hydrocarbons were detected by GC, extracts were further concentrated by rotary evaporating 232 to 10 ml and reinjected into the GC. Schiehallion crude oil was analysed gravimetrically as 233 TPH.

Calibration curves (6-point) were determined for each compound of the model oil. Laboratory control samples were analysed to establish the effect of the sediment matrix and extraction procedure on the recovery of model oil compounds. Toluene was added (1  $\mu$ l ml<sup>-1</sup>) as an internal standard to correct for injection error in the GC analysis. The limits of detection (LOD) and quantification (LOQ) were defined as chromatographic signal to noise ratios (S:N) of 3 and 10, respectively. When chromatographic peaks had a S:N between the LOD and LOQ were assigned a value of LOQ/2.

## 241 2.7 Chemicals

All model oil components (Table 1), toluene (99.8%), dichloromethane (99.8%) and hydrogen
peroxide (30%) were purchased from Sigma Aldrich. SD25 was purchased from Oil Technics
(Aberdeenshire). Sodium hexametaphosphate (technical grade) was purchased from Alfa
Aesar.

## 246 2.8 Calculations and statistical modelling

To establish valid comparisons across SD25 treatments, hydrocarbon concentrations in
sediment were normalised to the total mass of hydrocarbon accounted for in all sediment layers
and washout as follows:

250 
$$C_{i,j,k} = \frac{\frac{m_{i,j,k}}{t_{i,k}}}{\frac{s_{j,k}}{s_{j,k}}}$$

Where  $C_{i,j,k}$  is the normalised concentration in sediment of hydrocarbon *i* in section *j* in core *k*, *m*<sub>i,j,k</sub> is the mass of hydrocarbon *i* in section *j* in core *k*, *t*<sub>i,k</sub> is the total mass of hydrocarbon *i* in all sediment layers and washout of core *k* and *s*<sub>j,k</sub> is the mass of sediment in section *j* in core *k*. Washout hydrocarbon mass was normalised to total hydrocarbon mass in sediment and washout mixture as follows:

$$W_{i,k} = \frac{m_{i,k}}{t_{i,k}}$$

257 Where  $W_{i,k}$  is the normalised mass of hydrocarbon *i* in the washout of core *k* and  $m_{i,k}$  is the 258 mass of hydrocarbon *i* in the washout mixture of core *k*. Depth and SD25 were expected to 259 have non-linear effects and interactive effects on C. Therefore, a generalised additive mixed 260 effects model (GAMM) was therefore fitted to the data including, for each individual 261 hydrocarbon, a bivariate tensor product smooth of depth and SD25 (Wood, 2006). Core identity 262 (k) and Hydrocarbon identity (i) were specified as crossed random intercepts which allowed 263 for variation in average C between cores and between model oil components. A lag-1 264 continuous autoregressive residual correlation term was included in the model to account for the lack of independence between depth segments due to the movement of hydrocarbon from 265 266 the surface of the sediment to the segments underneath, such that C at one depth segment was allowed to depend on C of the same hydrocarbon at the depth segment directly above it. Due 267 268 to the much higher concentration of hydrocarbons in the 0–1 cm layer compared to the rest of 269 the sediment column (89.5  $\pm$  6.8%), the data from this layer was omitted from the GAMM. The 270 response variable C was square root transformed prior to fitting the model to improve 271 homoscedasticity of residuals, and a Gaussian distribution was assumed for the data. The model 272 formula was:

273 
$$C \sim te(z, SD25, by = i)$$

274 Where C is normalised hydrocarbon concentration, te represents tensor product smooths, z is 275 the sediment depth (cm), *SD25* is SD25 concentration (mg l<sup>-1</sup>), *by* estimates a separate smoother 276 for each hydrocarbon *i*. Assessment of  $W_i$  as a function of SD25 concentration was modelled 277 using locally weighted regression where  $W_i$  was the response variable and SD25 concentration 278 was the explanatory variable. The model fits a polynomial surface determined by SD25 279 concentration as a predictor using local polynomial regression fitting (Cleveland et al., 1992). 280 W<sub>i</sub> and SD25 concentration were log-scaled for ease of visualisation. For comparisons between 281 Schiehallion and model oil, TPH mass percentages retained at each sediment depth and 282 washout a locally weighed regression was also used where mass percentage was the response 283 variable and depth was the explanatory variable. Models were developed for SD25 284 concentration = 0 and 333.3 mg  $l^{-1}$  separately, and mass percentage was log-scaled for ease of 285 visualisation. Where pair-wise comparisons were carried out, two-way ANOVAs are used to 286 establish if SD25 application and oil type showed significant effects. All statistical analyses 287 were carried out using the statistical software R (R Development Core Team, 2017) and the 288 libraries ggplot2 (for the locally weighed regression analysis) and mgcv (for the GAMM 289 analysis) (Wickham, 2009; Wood, 2011).

# 291 **3 Results**

# 292 3.1 Sediment properties and SD25 characterisation

The sediments analysed were classified as sands and were found to be highly permeable (Table 3). The intersection of linear response of surface tension to SD25 concentration, the apparent CMC of SD25 in seawater, as 21.1 mg l<sup>-1</sup> (Figure 3).

296 Table 2. Ythan intertidal sediment characteristic. Permeability was measured at larger depth intervals

than the other properties shown due to the size requirement of the instrument used. Errors represent standard deviation (n = 3). D50, TC, TIC and TOC refer to mass-median-diameter, total carbon, total

299 inorganic carbon and total organic carbon, respectively.

	Sediment size and sorting		Carbon content			Permeability	
Depth (cm)	D <sub>50</sub> (µm)	Sorting	TC (%)	TIC (%)	TOC (%)	Depth (cm)	Permeability (m <sup>2</sup> )
0.0–2.5	299.1 ± 11.4	Moderately Well Sorted Medium Sand	$0.072 \pm 0.024$	$0.043 \pm 0.028$	$0.029 \pm 0.006$	0050	$4.04\times10^{\text{-}11}\pm$
2.5-5.0	$\begin{array}{r} 309.8 \pm \\ 6.6 \end{array}$	Moderately Well Sorted Medium Sand	$0.052 \pm 0.045$	$0.038 \pm 0.033$	$0.014 \pm 0.012$	0.0–3.0	$2.25 \times 10^{-12}$
5.0–7.5	334.5 ± 20.3	Moderately Well Sorted Medium Sand	0.086 ± 0.012	$0.061 \pm 0.018$	$0.026 \pm 0.006$	_	4 54 × 10-ll
7.5–10	328.7 ± 5.3	Slightly Very Fine Gravelly Medium Sand	$\begin{array}{c} 0.038 \pm \\ 0.010 \end{array}$	$\begin{array}{r} 0.019 \pm \\ 0.008 \end{array}$	$\begin{array}{r} 0.019 \pm \\ 0.005 \end{array}$	5.0–10	$4.99 \times 10^{-12}$



301

Figure 3. Surface tension of Ythan seawater as a function of Superdispersant-25 (SD25) concentration to establish the apparent critical micelle concentration of SD25. Crosses and circles denote the separation of the dataset to calculate linear regressions (solid and dotted lines, respectively) from the change of slope and their intersection (vertical dashed line).

## 306 *3.2 Model oil – Schiehallion crude oil comparison*

The proportion of TPH retained in the top layer (0-1 cm) for model oil was significantly higher 307 308 than that of Schiehallion crude oil aggregating treatments of both oil, and oil and dispersant 309 treatments (89.5  $\pm$  6.8% and 72.4  $\pm$  16.9%, respectively, p-value = 0.04). Dispersant 310 recommended dosage reduced the percentage to TPH retained in the top layer for model oil 311  $(95.1 \pm 2.4\%$  to  $83.9 \pm 4.1\%$ , p = 0.01) but not for crude oil  $(79.9 \pm 17.0\%$  to  $64.9 \pm 16.1\%$ , p 312 = 0.33). Mass percentage decreased exponentially with depth for both oils and treatments. 313 Locally weighed regressions revealed a clear increase in mass percentage as depth increased 314 for model oil but not for crude oil when SD25 was applied at recommended dosage (Figure 4) 315 SD25 did not have a consistent effect on the mass percentage of Schiehallion crude oil retained 316 at any sediment layer but did increase the percentage of oil in the washout  $(3.7 \pm 5.7\%)$  and 0% 317 when SD25 was not applied).



318

Figure 4. Total hydrocarbon mass percentage as a function of depth by treatment. Oils used were crude oil (left) and model oil (right) and treatments were oil only (red dots) and oil and 333.3 mg  $1^{-1}$  Superdispersant-25 (blue dots). Oil (red) and Oil and dispersant (blue) treatment lines bands represent locally-weighed regression values and associated standard errors, respectively. Note mass percentage has been log(x+1)-scaled.

## 322 3.3 Hydrocarbon entrainment into the top 10 cm of sediment

323 The GAMM results indicate that the application of SD25 increased the normalised 324 concentration of all hydrocarbons with depth, even at SD25 concentration below the 325 recommended dosing (Figure 5, Supplementary Figure 3, Supplementary Table 1). Overall, the 326 application of SD25 increased the amount of oil entrained into these sands. The effect of SD25 327 was similar for most hydrocarbons in the top 4 cm. However, differences in the effect of SD25 328 on the entrainment of hydrocarbons became apparent at depths greater than 4 cm.  $C_{10-12}$ 329 aliphatics showed a linear increase in entrainment with increasing SD25 concentration as in 330 the surface layers. The remaining hydrocarbons showed increased entrainment into these sands 331 at SD25 concentration above 42 mg l<sup>-1</sup>. 1-Octadecene showed an unexpected response 332 compared to equivalent length aliphatics (C<sub>17</sub> and C<sub>19</sub>) with no effect of SD25 concentration 333 on entrainment over 5 cm deep. Dibenzothiophene, the only resin in the model oil, showed 334 enhanced entrainment in sediments from low SD25 concentration. Interestingly, entrainment of dibenzothiophene did not increase with dispersant concentration in the range 150–333 mg 335 SD25 l<sup>-1</sup> at depths greater than 7 cm. 336



Figure 4. Generalised additive mixed effects models of hydrocarbon concentration in Ythan intertidal sands following percolation with increasing
 Superdispersant-25 concentrations from sediment depths of 1 to 10 cm. Note hydrocarbon concentrations have been normalised and square-rooted.

## 340 3.4 Hydrocarbon entrainment beyond 10 cm of sediment

 $W_i$  in the washout varied by component and SD25 concentration (Figure 6). For C<sub>10-14</sub> 341 342 aliphatics, the influence of SD25 concentration on  $W_i$  was unclear.  $W_{\text{Pentadecane}}$  (C<sub>15</sub>) was increased at 42 mg SD25 l<sup>-1</sup> but higher concentrations did not result in further increases of 343 344  $W_{\text{Pentadecane}}$ .  $W_{\text{Hexadecane}}$  (C<sub>16</sub>) increased with SD25 concentration. Heptadecane (C<sub>17</sub>) and tetracosane (C<sub>24</sub>) showed a higher  $W_i$  at and above 21.1 mg SD25 l<sup>-1</sup>. Interestingly, SD25 345 346 application did not affect  $W_{1-\text{Octadecene}}$  (C<sub>18</sub>) but affected C<sub>20</sub> and C<sub>22</sub> aliphatics which only 347 increased at SD25 concentration >150 mg l<sup>-1</sup>. For the more soluble components of the model 348 oil such as BTEX and naphthalene, no clear effect of SD25 concentration was observed, with 349 Wi fluctuating as SD25 concentration increased. The response of fluorene to SD25 350 concentration was similar to that of  $C_{10-15}$  aliphatics, but with only a slight increase of  $W_{\text{Fluorene}}$ 351 at SD25 concentration above 21.1 mg l<sup>-1</sup>. Larger PAHs showed increased W<sub>i</sub> from 42 mg SD25 352  $1^{-1}$  except anthracene which only showed increased  $W_{\text{Anthracene}}$  at 333.3 mg SD25  $1^{-1}$ , possibly as a result of its lower percentage composition of the model oil. Dibenzothiophene, showed a 353 354 steady increase in W<sub>Dibenzthiophene</sub> with SD25 concentration.



Figure 5. Normalised hydrocarbon mass in washout mixtures (*W*) as a function of Superdispersant-25 concentration. Points represent raw data and lines with grey bands represent locally-weighed regression values and associated standard errors, respectively. Note *W* and Superdispersant-25 concentration were  $\log(x+10^{-4})$  and  $\log(x+1)$ -scaled, respectively.

# 359 4 Discussion

## 360 4.1 Key findings

361 SD25 application enhanced the mobility of hydrocarbons of the model oil through the top 10 cm of sediment and increased the W<sub>i</sub> of leached hydrocarbons. The effect was most pronounced 362 363 at and above 150 mg l<sup>-1</sup> (half of the recommended dosage in terms of SD25:oil ratio) (Figures 5 and 6). The effect of SD25 application on W<sub>i</sub> varied with hydrocarbon type, with BTEX and 364 365 naphthalene being unaffected and the remaining components showing different degrees of response (Figure 6). Overall, the recommended dosing of SD25 (1:30 SD25:oil ratio, 333.3 mg 366 367 SD25  $l^{-1}$ ) increased the  $W_i$  of most hydrocarbons. Crude and model oil concentrations followed 368 an exponentially decaying trend with depth in the percentage of mass of TPHs retained in the 369 sediment. SD25 application resulted in increased mobility of model oil through sediments but 370 not in the relative amount of oil in the washout. In contrast, SD25 application resulted in an 371 increase (from zero) in the percentage of crude oil present in the washout.

## 372 4.2 Sediment properties and Superdispersant-25 CMC

The sands used in this experiment were highly permeable  $(4 \times 10^{-11} \text{ m}^2, \text{ Table 3})$  and values were in agreement with prior characterisation of the estuary's sands (Zetsche et al., 2011). High permeability in the top 10 cm results in advective pore-water fluxes being the dominant transport mechanism of solutes (Huettel et al., 2014). Consequently, oil deposition on these permeable sands may result in significant hydrocarbon entrainment after an oil spill. This was evidenced here, where oil entrained the permeable sands beyond 10 cm deep (Figure 6) and is undesirable because sediment-entrained oil can persist for years (Lindeberg et al., 2017).

380 The apparent CMC of SD25 was calculated to be 21.1 mg l<sup>-1</sup> (Figure 3), which is close to that reported for Corexit EC9500A (22.5 mg l<sup>-1</sup>), a dispersant widely used during *DwH* (Gong et 381 382 al. 2014), suggesting that the surfactant effect of the dispersants may be similar. The relevance 383 of the CMC has been subject to extensive study within remediation and oil spill science in 384 recent years. The desired effects of dispersant are frequently found above the CMC (Ahn et al., 385 2010; Gong et al., 2014; Zhao et al., 2015). Here, a similar response for SD25 was found for heptadecane and tetracosane leading to increased percolation over 10 cm at SD25 concentration 386 387 = CMC (Figure 6). It has been shown that different commercial dispersants can have different 388 effectiveness on spilt oil deposition. For example, Corexit dispersants accelerate settling of oil-389 mineral aggregates more effectively than SPC1000 (Cai et al., 2017). Furthermore, Corexit

dispersants promote photodegradation whereas SPC1000 inhibits it (Fu et al., 2016). It is therefore important to establish the effects of dispersants such as SD25, which are stored to respond to potential oil spills across the world, to adequately assess the implications of their use and subsequent consequences.

## 394 4.3 Model oil – Crude oil comparison

395 SD25 application resulted in increased mobility of model oil components but the effect on 396 Schiehallion crude oil was less consistent (Figure 4) This may have been due to the greater 397 complexity of crude oil composition (1000s of components) compared to that of the model oil 398 (21 components), which showed a distinct exponentially decreasing percentage retained at 399 increasing sediment depth. Additionally, the method used to establish TPHs for the 400 Schiehallion crude oil may be less robust than that used for the model oil (gravimetry vs. gas 401 chromatography, respectively). However, the use of a simpler oil (i.e. a model oil) facilitated 402 the interpretation of oil-dispersant interaction mechanisms in seawater and highlighted the need 403 for further research to understand the behaviour of multi-component mixtures in a multi-media 404 system such as the oil-dispersant-seawater-sediment system analysed in this work.

## 405 4.4 Hydrocarbon entrainment into the top 10 cm of sand

406 SD25 application had distinct effects on the mobility of hydrocarbons through permeable sands 407 (Figure 5). SD25 concentration below 42 mg SD25 l<sup>-1</sup> had a relatively low impact on the mobility of most hydrocarbons in the top 10 cm. The effect was most apparent at high SD25 408 409 concentration, indicating that SD25 concentration >150 mg l<sup>-1</sup> may be necessary for 410 hydrocarbons to readily entrain into these sands.  $C_{10-12}$  entrainment showed a linear increase 411 with SD25 concentration (Figure 5). These components are of limited concern as they are 412 relatively volatile and are readily biodegraded (Liu and Liu, 2013). Longer-chained aliphatics 413 (C<sub>12+</sub>) responded non-linearly but almost always monotonically to an increase in SD25 414 concentration (Figure 5). C<sub>14–16</sub> were readily mobilised around 4 cm deep at the recommended 415 SD25 dosing compared to in its absence. This suggested that SD25 selectively mobilised 416 aliphatics with long chains more readily than those with short ones. Interestingly, the effect of SD25 application on 1-octadecene entrainment was minimal compared to the C<sub>17</sub> and C<sub>20</sub> 417 418 saturate hydrocarbons of the model oil (Figure 5). A key difference which may influence 1-419 octadecene's interactions with an oil-dispersant-seawater-sediment system with respect to C17 420 and C<sub>20</sub> saturate hydrocarbons is the presence of a double bond, promoting stronger adsorption 421 to sediment surfaces than saturates. Analogue comparisons between decane (C<sub>10</sub> paraffin) and

422 1-decene ( $C_{10}$  olefin) reveal that entrainment of 1-decene is less pronounced than that of decane 423 in the top 4 cm of sediment but not deeper (Figure 5). This suggested that SD25 may be less 424 effective in mobilising olefins compared to paraffin. BTEX components showed a limited 425 increase in entrainment with SD25 concentration up to 150 mg l<sup>-1</sup>, which agrees with previous 426 work on the limited effect of SD25 on the dissolution and dispersion of these components of 427 the model oil in seawater (Perez Calderon et al., 2018). These components were found in higher 428 (normalised) concentrations in the washout hydrocarbon-dispersant-water solution (Figure 6), 429 highlighting the capability of hydrocarbons to be entrained into coastal permeable sediments 430 beyond 10 cm and impact benthic ecosystems. SD25 recommended dosing (1:30 SD25:oil 431 ratio, in this work 333.3 mg l<sup>-1</sup>) resulted in enhanced entrainment of BTEX components (Figure 432 5). However, unless an oil spill occurs nearshore, it is unlikely that these hydrocarbons will 433 reach coastal sediments due their high volatility and low  $K_{OW}$ . Nevertheless, BTEX have been 434 detected in coastal sediment (Phelps and Young, 1999) and consequently, following the 435 precautionary principle, these interactions should be considered in any dispersant application 436 decision-making process. Dispersant-facilitated adsorption has been shown for PAHs using the 437 dispersant Corexit 9500 (Gong et al., 2014; Zhao et al., 2015). In this work, PAHs showed a 438 similar response to C<sub>14+</sub> aliphatics with an increase in hydrocarbon entrainment with SD25 439 concentration in the top 4 cm of sediment and the effect becoming more pronounced over 4 cm 440 deep. Dispersant application is typically carried out offshore where high-energy mixing can 441 take place with the aim of preventing beaching of spilled oil. However, dispersant can enhance 442 the entrainment into permeable sands by increasing the solubility of hydrocarbons and reducing 443 droplet size.

## 444 4.5 Hydrocarbon entrainment beyond 10 cm of sediment

445 Washout of hydrocarbons over 10 cm deep in Ythan estuary sands was enhanced by SD25 446 application for most hydrocarbons (Figure 6). Aliphatic hydrocarbons of specific chain length 447 ranges ( $C_{15-17}$  and  $C_{20-24}$ ) increased their  $W_i$  with SD25 application. In contrast, the effect of 448 SD25 was less apparent on  $C_{10-14}$  and  $C_{18}$  aliphatics suggesting that SD25 may selectively 449 enhance the mobility of certain hydrocarbons in permeable sediments. C<sub>10-14</sub> aliphatics are the 450 most soluble alkanes of the model oil and, therefore, a lesser impact of SD25 was expected. 451 Intertidal microbial communities play an important role in organic carbon processing in marine 452 sediments (Woulds et al., 2016). Facilitated entrainment of these hydrocarbons may result in 453 microbial community succession in intertidal permeable sands shifting the microbial 454 composition to hydrocarbon degrading communities (Lamendella et al., 2014). Furthermore,

455 bacterial oxidation of hydrocarbons may increase their water-solubility, making them more 456 mobile within the sediment. The  $W_i$  of the most water-soluble hydrocarbons of the model oil 457 (BTEX components and naphthalene) varied across the SD25 concentration range analysed 458 and SD25 application did not have a consistent effect on the capacity of these hydrocarbons to 459 entrain sands beyond 10 cm deep. This is may be due to their high water-solubilities which 460 may limit the effect of SD25 application (Perez Calderon et al., 2018). Previous work has 461 shown a reduced effect of dispersant application on the solubilisation of naphthalene, compared 462 to pyrene (Zhao et al., 2015). This suggests that SD25 enhances the mobility of BTEX 463 components and naphthalene into permeable sands but not their dissolution or dispersion in 464 seawater, implying that pore-water transport of dissolved BTEX and naphthalene is less 465 affected by dispersant application than that of larger, less seawater-soluble hydrocarbons. 466 Larger PAHs (>2 rings) showed a similar response with low  $W_i$  values below 42 mg SD25 l<sup>-1</sup>. However, there was an inflexion point between the CMC and 42 mg SD25 l<sup>-1</sup> from which 467 468 hydrocarbon entrainment increases for these PAHs, indicating that a threshold in enhancing 469 solubility in water may exist for SD25 effectiveness on large PAHs. Dibenzothiophene showed 470 a steady increase in W<sub>i</sub> with SD25 concentration, indicating a different response to SD25 than 471 the other PAHs. Dibenzothiophene was the only resin (contains sulphur in its structure) in the 472 model oil, which may explain its higher  $W_i$  at low SD25 concentration. Overall, these results 473 suggested that hydrocarbons within a mixture such as a crude oil entrain permeable sediments 474 and solubilise to different extents and that dispersant application affected this process 475 differently for specific groups of hydrocarbons.

# 476 **5** Conclusions

This work highlighted the capability of a synthetic hydrocarbon mixture (model oil) and a crude
oil (Schiehallion) to entrain permeable sands *via* natural percolation and the facilitation of this
process by dispersant application. The main findings of the work were:

- 480 (1) A positive effect of SD25 concentration on hydrocarbon mobility was observed below
  481 the manufacturer's recommended dosing in permeable sands. Enhanced percolation
  482 beyond 10 cm deep was detectable at as low as SD25 CMC (21.1 mg l<sup>-1</sup>).
- 483 (2) SD25 concentration increased the mobility of model oil through permeable sands and
   484 selectively mobilised larger hydrocarbon components (less water-soluble) than smaller
   485 components (more water-soluble) of the model oil.

(3) Both the model and Schiehallion crude oils readily entrained permeable North East
Scotland sands. The concentration profiles by depth followed an exponential decay
pattern for model oil but were poorly reproduced for crude oil, highlighting the
complexity of interactions in crude oil mobility through permeable media. SD25
application increased the entrainment of model oil but not of Schiehallion crude oil,
again due to high variability.

The findings of this work highlight the potential of oil to readily be entrained into permeable sands in the event of an oil spill and that dispersant application exacerbates the process for some oil components more than others. Further work is needed to understand how different commercial dispersant formulations can affect oil entrainment and how this varies by oil, hydrocarbon and sediment type as well as how seawater moves through sandy sediments and potentially displaces hydrocarbons already present in them.

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