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Augmenting Mask-Based Lithography with Direct Laser Writing to Increase Resolution and Speed

Miles Patrick Lim Bard College, ml8127@bard.edu

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Augmenting Mask-Based Lithography with Direct Laser Writing to Increase Resolution and Speed

A Senior Project submitted to

The Division of Science, Mathematics, and Computing

At Bard College

By

Miles Lim

Annandale-on-Hudson, NY

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DEDICATION

This work is dedicated to my grandfather Lowell C. Parode. He always encouraged me to follow my curiosities and enjoy the world around me. I also greatly thank my parents Lynne and Sterling for their love and support.

ACKNOLEDGEMENTS

I want to thank my advisor Chris LaFratta for being an incredible mentor and friend. I could not be more grateful to have been welcomed into his lab and had the opportunity to work with him on the hybrid lithography project. His commitment to his students and contagious love of science inspires me to strive for excellence every day. In addition to being an incredible professor and advisor, our shared interest in books, podcast, and TED talks has changed the way I see the world forever.

I also owe a big thanks to the Bard Chemistry department and all of the professors for making chemistry available and unintimidating. I am constantly in awe of how dedicated our faculty are to their student's in every possible way. We are so lucky to have all of you.

Lastly, I would also like to thank the Bard Research Fund and the Bard Summer Research Institute for funding this work.

ABSTRACT

We present combined direct-laser-writing and UV Lithography in SU-8F and S1813 as a fast and flexible lithographic technique for the prototyping of functional polymer devices and pattern transfer applications. Direct laser writing (DLW), which is performed by focusing a laser through a microscope objective, is a useful alternative method for patterning photoresists with sub-micron resolution. DLW however, can be time consuming if the pattern density is high since it is a serial technique. Typically, dense patterns are made using conventional mask-based UV lithography, but these masks can be quite expensive if the resolution is high and the mask cannot be modified once created. Here, we combine UV lithography using inexpensive transparency masks, which have modest resolution of about 20 µm linewidths, with DLW to create smaller features. By using the laser to augment an inexpensive mask, high resolution prototypes can be created, tested, and modified quickly to optimize a design. Here we show that this Laser Augmented Microlithographic Patterning (LAMP) method works with both positive- and negative-tone photoresists, S1813 and SU-8, respectively. The laser written features can be registered to within 2.2 µm of the mask created features and we demonstrate the applicability of LAMP by fabricating an interdigitated electrode and a microfluidic device that can capture an array of dozens of silica beads or living cells.

1. INTRODUCTION

Conventional mask-based lithography and direct laser writing (DLW) can be combined into a hybrid technique, which compensates for the drawbacks of each. Photolithography using a mask to expose a photoresist to UV light is commonly used for the production of microelectronics but has applications including microelectromechanical systems (Waggoner et. al. 2007), lab-on-a-chip devices (Xia et. al. 1998), and DNA microarrays (LaFratta et. al. 2008). The power of photolithography lies in its ability to pattern large areas at sub-micron resolution in a matter of minutes. Two issues with photolithography are: i) the initial cost of the mask, which can be substantial if the resolution is high; and ii) the rigidity of the mask since it cannot be altered. These issues can make prototyping a new device via photolithography fairly expensive. An alternative patterning method that does not suffer from these issues is direct laser writing (DLW), in which a laser is focused to a point in a photoresist and moved with respect to the sample to generate the pattern. One issue with DLW is the potentially long time required to cover large areas. The method we describe here is a combined lithographic technique that utilizes the large area patterning abilities of mask lithography and the serial patterning of direct laser writing. which together provide high resolution patterns, in a short amount of time, and at a reasonable cost. This combined lithography system can effectively pattern from sub-micron to millimeter resolution with much higher throughput than DLW on its own, while offering more pattern flexibility than plain mask lithography. This can be used as an alternative means for creation of microfluidic masters and for prototyping microelectronics.

Others have also investigated hybrid lithography schemes such as the pairing of UV lithography with of electron beam lithography (EBL) (Rahman et. al. 2010; Nakano et. al.

2016; Potosky et. al. 1981; Carbaugh et. al. 2017; Steen et. al. 2006; Mollard 200; Benistant et. al. 1996; Jonckheere et. al 1995) or nanoimprint lithography (NIL) (Dhima et. al. 2012; Scheer et. al. 2010; Montelius et. al. 2010; Reuther et. al. 2011; Scheer et. al. 2010). For example, Kristensen et. al. report the patterning of SU-8 with EBL followed by UV lithography resulting in features as small as about 100 nm linewidths (Gersborg-Hansen et. al. 2007). While EBL is most frequently used with positive tone photoresists to open areas for depositing metal contacts, this work shows that by combining with UV lithography EBL can also be used to fabricate relief structure for molds. Nanoimprint lithography (NIL) has also been used as the first step in a sequential technique to pattern 500 nm features in SU-8 followed by a UV exposure to make contacts at the 200 μ m scale (Skjolding et. al. 2009). These are attractive prototyping technologies that offer rapid pattern generation with fine resolution. The use of direct laser writing as part of a hybrid scheme is less common, but Eschenbaum et. al. 2013 and Muluneh et. al. 2015 devised a hybrid DLW and UV lithography schemes for multi-scale patterning. They created high resolution patterns in three dimensions using an ultrafast laser for two-photon polymerization. The results are impressive showing the fabrication of a miniature 45° mirror to view particles from the side while traveling in a microfluidic channel. Shear and coworkers have also demonstrated a DLW system that uses the mirror array from a projector to quickly transfer a high-resolution pattern, thereby increasing the speed of DLW. Such two-photon systems can be very expensive and somewhat difficult to operate compared to a simple continuous wave diode laser, which is what we report here.

In this work, we present a combined DLW and UV lithography scheme that uses both positive and negative photoresists as a fast and flexible lithographic technique, suitable for wafer scale definition of both millimeter and sub-micrometer scale features. Our method, which we call Laser Augmented Microlithographic Patterning (LAMP), first exposes a photoresist through an inexpensive transparency mask and then adds to that exposure using a DLW system before finally developing the pattern (Figure 1). If one already has a microscope, then it can be readily adapted into a DLW system (LaFratta et. al. 2015). LAMP is fairly low cost, straightforward to perform, and requires only a single photoresist layer and development step. We show that we can register the DLW features to within about 2 µm of the mask alignment marks and can achieve sub-micron linewidths. We envision LAMP to be an attractive alternative to expensive masks for prototyping devices for researchers. We demonstrate two simple proof-of-principle devices, a microfluidic cell trap and an interdigitated electrode (IDE), to show the utility of LAMP.



Figure 1: Experimental steps involved in the laser augmented microlithographic patterning (LAMP) procedure for both positive and negative photoresist. The photoresist is first exposed to UV through a transparency mask, then the exposed region changes color, allowing registration for new features to be patterned by direct laser writing (DLW). Development yields positive (S1813) or negative (SU-8F) microstructures that can then be used for additional steps like metal evaporation or molding.

2. EXPERIMENTAL METHOD

2.1 LAMP Procedural Overview

Experimental conditions and the optical components of our system are described in depth in previous publications by our lab (Lafratta et. al. 2015). For positive photoresist, Shipley S1813 (Microchem) was spun on 2" glass wafers to a thickness of approximately 1.5 μm. For negative photoresist, we doped SU-8 2005 (Microchem) with fluorescein in a ratio of 1 mg of fluorescein to 1 mL of SU-8 to yield "SU-8F". The SU-8F was thoroughly mixed before being spun onto 2" silicon wafers to a thickness of 5 µm. The wafers were soft baked according to their data sheets provided by Michrochem and exposed through a transparency mask to a 100 W mercury lamp (Blak-Ray) for 60 s. The wafers were then mounted onto an inverted fluorescence microscope (IX-71, Olympus), which had a motorized X-Y stage (Proscan III, Prior) coupled to a manual rotation stage (Thorlabs). A 405 nm continuous wave diode laser (OBIS, Newport Corporation) was directed through a custom laser port in the filter turret and focused through a 20X numeric aperture (NA) 0.75 objective onto the sample. The X-Y axis of the exposed mask pattern and the microscope stage were made parallel using the rotation stage, the laser spot was then aligned to a registration point on the exposed mask pattern. The desired power, speed, and focal position along the optical axis (Z-axis) could be adjusted to create lines of varying linewidth. The DLW of the photoresist for S1813 was performed using about 300 nW, while the SU-8F required about 500 μ W. These powers were measured before the microscope, but at the sample they were 13% of these values due to reflective loss at the mirror and because the laser overfilled the back aperture of the objective. Following the exposure of the resist in the desired pattern, the sample was submerged in the appropriate developer; S1813 was developed in Microposit 351 for one minute and SU-8F was post baked and developed in propylene glycol monomethyl ether acetate for one minute. Linewidths and registration of patterned features were characterized by scanning electron microscopy, SEM, (MIRA 3, Tescan) for several objective lenses, power, and sample position along the Z-axis.

2.2 Baking, UV Exposure, and Development Testing

The experimental conditions were originally carried out according to their data sheets (Microchem), but because of differences in equipment we optimized the times and temperatures ourselves. Baking temperatures remained at 65°C and 95°C for SU-8F, but were reduced from 115°C to 95°C for S1813. Exposure times between 45 s to 90 s, for both resists, were tested. Additionally, development times between 5 s and 120 s were tested. All baking, exposure, and development tests were performed using the US Airforce Test Mask standard (USAF1951) with features resolution down to 2.19 µm.

2.3 DLW Resolution Testing

DLW of S1813 and SU-8F was tested at various speeds and powers to determine optimal conditions for augmenting mask features. For both resists, six power studies on six individual wafers were prepared and averaged to collected the linewidth data. For negative tone SU-8F, the lines were defined in parallel with two perpendicular lines to help them stand up. Following development, these lines were measured by SEM to determine the linewidth.

2.4 Registration Testing

Registration between the mask exposed pattern and the DLW pattern was tested using a mask having a series of rectangles regularly spaced over 25 mm, that were connected by both horizontal and vertical lines by DLW. Following development, the patterns were imaged by SEM and the position of the laser augmented lines was measured with respect to the center of the target rectangles. When measuring registration data, Δx and Δy were measured at the center (L1,R1) and at the edges (L10,R10).



Figure 2: The image above shows the mask pattern (in purple) that was used to test the laser registration (in blue). L10, L1, R1, and R10 indicate where on the wafer the measurement were taken.

2.5 Interdigitated Electrode Fabrication

The fabrication of the interdigitated electrode (IDE) began with a transparency mask drawn in LayoutEditor and was printed on a Mylar transparency by Advanced Reproductions (N. Andover, MA) and was available in 24 hours for \$50. The mask had contact leads on the order of 250 μ m wide and about a centimeter in length which came together but left a gap of 1.3 mm. In the gap between leads, LAMP was used as previously described with S1813 to add interdigitated lines about 2 μ m wide with a spacing of 12.5 μ m and with a length of 200 μ m. Following development, the samples were placed in a thermal

evaporator (Edwards) and 2 nm of Cr was evaporated followed by approximately 50 nm of Au. Liftoff was performed by soaking the sample in acetone for 1 hour followed by gentle stirring, and the final sample was imaged by both optical and scanning electron microscopy.



Figure 3: The graphic above show the mask pattern that was used to make the contact wire for the interdigitated electrode test structure.

2.6 Microfluidic Cell Trapping Array Fabrication

The microfluidic designed to trap an array of cells was also made using a Mylar mask with a similar pattern to an IDE except it had lines that were 15 µm wide with 15 µm gaps between them and they were 500 µm long. The Si wafer was spin coated with SU-8F, prebaked, and exposed through this mask. Next, a series of lines were drawn perpendicular to the "IDE" pattern. After post-baking and developing, this master structure was silanized with a fluorocarbon to make it non-stick and polydimethylsiloxane (PDMS) (Sylgard 184, Dow Corning) was mixed, degassed, and cast onto the master. After 1.5 hours at 60°C the PDMS was cut off the master, holes were punched, and the PDMS was placed in a plasma cleaner (Harrick) along with a clean glass slide for 1 minute (LaFratta et. al. 2004). The air plasma oxidized both the PDMS and the glass slide. After they were removed from the plasma cleaner the PDMS was gently placed on the glass slide and placed in a 110°C oven for 10 minutes to irreversibly bond (Duffy et. al. 1998). Tubes were then inserted into the previously punched holes and a dilute solution yeast cells or 5 μ m silica beads were flowed into the device. The functional device was positioned on an inverted microscope and images of the array of cells were captured using a CMOS camera (Thorlabs).



Figure 4: The graphic above shows the mask pattern that was used for the cell trapping microfluidic, and the additional laser patterns added to make the microfluidic master. The scheme also shows the flow in and out of fluid to demonstrate the flow of cells or beads and where they would trap.

3. RESULTS AND DISCUSSION

3.1 The LAMP Method is Dependent on the Photochromism of the Resist

When exposed to UV radiation, both S1813 and SU-8F have photochromic properties resulting in contrast between the exposed and unexposed regions. This contrast enables the DLW system to be aligned with the mask exposed patterns and is critical for LAMP. The photos in Figure. 5 shows both S1813 and SU-8F before and after UV exposure. SU-8 generates a photoacid upon exposure, but shows no color or refractive index change. In order to visualize where the pattern that had been exposed, we doped SU-8 with various concentrations of fluorescein, which is a fluorophore and also a pH indicator. We found that at low concentrations of fluorescein the SU-8F was slightly more yellow in the exposed regions but there was not enough contrast to see the difference between exposed and unexposed regions. If the fluorescein concentration were too high, for example 2 mg/mL, then the contrast was excellent but the developed sample would frequently fall off of the substrate, presumably because the fluorescein interrupted the epoxide polymeric network. We found 1 mg/mL to be ideal for providing enough contrast while maintaining the material properties of SU-8. The SU-8F, which is a clear and colorless, turns bright yellow upon exposure due to the generation of acid and the change in the protonation of the fluorescein molecule in acidic environments, which is yellow (Sjöback et. al. 1995). The S1813 can be seen to photobleach upon exposure turning from clear red to clear colorless. To enhance this color change we used a blue LED as an illumination source on our DLW microscope. The yellow SU-8F lines absorb the blue light and appeared dark indicating where the mask exposure took place.



Figure. 5: Both S1813 and SU-8F show a photobleaching/photochromic effect following exposure to UV, which enables registration between features made with a mask and those made with the laser. Images (A) and (B) show 25 mm coverslips coated in SU-8F before and after exposure, respectively. (C) Shows the contrast of SU-8F on the DLW microscope for the area corresponding to the small square in (B). (D-F) are the analogous images for S1813. The scalebars in (C) and (F) are 250 μm.

3.2 The Procedure was Optimized for Reproducible High Resolution Lines

Factors like prebaking time and temperature, UV exposure time, and development time have an impact on the reproducibility of the resolution when working with submicron features. For S1813, the sample was soft baked for 2 minutes at 95°C, exposed for 45 s, and developed for 45 s. This was optimal for the USAF test mask, but for exposing the Mylar mask for the LAMP process an exposure time of 60 s ensured the pattern was defined properly. For SU-8F, the sample was soft baked for 1 min at 65°C and 3 min at 95°C, exposed for 60 s, hard baked for 1 min at 65°C and 3 min at 95°C, and developed for 60 sec.

3.3 The LAMP Procedure Requires Modification of an Inverted Fluorescence Microscope

In order to write accurate laser lines with respect to the mask exposed pattern, the laser and the mask systems need to be squared together. This was achieved with a manual rotation stage (Thorlabs) that was affixed to a custom mount machined to fit inside of the microscope's 96-well plate holder. This held the sample at the proper focal height, while adding adjustability in theta. Using the contrast between exposed/unexposed photoresist and the rotational stage, the pre-exposed pattern could be adjusted so that it was squared with the X-Y axis of the microscope stage.



Figure 6: Shows images of the manual rotation stage mounted to a 96 well pate holder for an Olympus IX-71. The left image shows the clips for mounting the sample and the image on the right shows the rotational nob.

3.4 Mask Design

The mask was designed with an array of features to demonstrate the viability of the LAMP technique. The transparency masks was drawn in LayoutEditor and were printed on a Mylar transparency by Advanced Reproductions (N. Andover, MA). The primary designed had two major features: a bar through the middle of the mask, and a centering dot. The 26,000 µm

bar was used to square the mask pattern as described above. The centering dot was used to tell the program where the center of the mask was. Once the program knew where the center was and the pattern was squared, we could write laser lines in (x,y) coordinates with respect to the existing mask pattern. The mask also included a series of rectangles which were used for registration (Figures 2 & 7) and a series of test structure features. Additional masks included contact wires for IDEs and the base pattern for the cell trapping microfluidic (Figures 3 & 4).



Figure 7: The registration test mask design in LayoutEditor. The "L-shaped" brackets at the edges are 2 inches apart. The inner brackets are 1 inch apart. The smallest feature size is down to $25 \mu m$.

<u>3.5 Sub-micron wide lines can be made by DLW</u>

Using a 20×0.75 numerical aperture (NA) objective, sub-micron features can be created by our DLW system. Figure 8 shows electron micrographs of some typical lines

fabricated at 40 μ m/s for S1813 and 10 μ m/s for SU-8F. The narrowest lines we could reproducibly write were 780 ± 140 nm wide for S1813 and 950 ± 90 nm for SU-8F. The line height was equal to the film thickness, which was close to 1 μ m for S1813 and 5 μ m for SU-8F. Other speeds were tested for both photoresists ranging from 5 - 50 μ m/s. Faster speeds gave smaller lines that were irreproducible and that sometimes did not develop completely down to the substrate (s1813) or resulted in wavy lines that partially delaminated (SU-8F)



Figure 8: Linewidth data for varying powers using a $20 \times \text{NA} = 0.75$ objective. S1813 lines were written at 40 µm/s and SU-8F lines were written at 10 µm/s. The inset show typical SEM micrographs for these samples (scalebars are 10 µm).

<u>3.6 Patterns can be Registered by DLW to Within About 2 µm on Existing Patterns</u>

When performing DLW, the first step is to register the position of existing features that were made during the mask exposure. This is possible because of the contrast between the exposed and unexposed regions and because the DLW system is itself a microscope where we can directly image the sample while simultaneously exposing it. We tested how accurately and precisely we could position the laser beam on the DLW system using a test pattern that contained dozens of rectangles spanning the length of the mask. By drawing lines from the center of one rectangle to the next and measuring the distance of the line from the center point, we obtained measurements for Δx (horizontal) or Δy (vertical). Figure 9 shows a schematic of a portion of the mask and how we define Δx and Δy . Δx (or Δy) is calculated by measuring the distance of the line to both edges of the rectangle then the difference between these numbers is divided by two (Figure. 9c). If the line is perfectly centered then both distances to the edge will be the same and Δx will be 0. We define the radius, Δr , within which we can position the laser focal point as $\Delta r = (\Delta x^2 + \Delta y^2)^{\frac{1}{2}}$. Hundreds of lines were measured on more than a dozen different wafers to give and an average Δr of $1.6 \pm 1.4 \mu m$ for S1813 and $2.2 \pm 1.5 \mu m$ for SU-8F. These numbers are reasonable given the accuracy and precision of the transparency mask. We believe the Δr is slightly smaller for S1813 because its contrast is more pronounced than that of SU-8F, making it easier to pinpoint the edge of an exposed area. Since the use of a mask in LAMP is intended to pattern large features quickly, it is likely the case that registering smaller features to within about 2 μm is sufficiently accurate; if it is not, then more intermediate sized features can be made by DLW better large-scale smaller scale. to marry the pattern to the



Figure 9: (A) Schematic of the rectangles on the mask that were used for registration marks. The thin red lines were drawn with the laser and their distance from the center of the rectangle, either Δx or Δy , was measured by imaging with the SEM. (B) Typical set of laser augmented registration lines. (C) Close-up of a registration rectangle showing how Δx was measured and calculated

<u>3.7 Proof of Principle Structures</u>

In addition to the characterization samples for linewidth and registration we also used LAMP to make two proof-of-principle devices, one each for the positive- and negativetone photoresists. S1813 was used to pattern a simple interdigitated electrode have large contact wires that lead into electrodes that are 3 μ m wide. The SU-8F was used to create a microfluidic chip having both large channels and very small ones that act as a filter to trap objects like beads and cells.

3.7.1 Interdigitated electrode

Interdigitated electrodes (IDEs) are planar capacitors with high surface area and are useful for electrochemical impedance spectroscopy (Ohno et. al. 2013). The IDE we fabricated by LAMP occupies an area of approximately $200 \times 200 \,\mu$ m and took only a couple of minutes to pattern. The IDE was connected to leads that were over a centimeter long and were made by a mask exposure. Had these leads been made with the laser it would have taken hours to expose such a large area even if the speeds and powers were doubled. Following LAMP, the IDE sample was gold coated and liftoff was performed leaving the electrode on glass, which was imaged by reflectance microscopy (Figure 10). The inset image in Figure 10 shows that the individual lines are about 3 μ m wide, 200 μ m long, and spaced 12.5 μ m apart. Such IDEs have been used in microfluidic channels for electrochemical impedance spectroscopy of cells and bacteria (Varshney et. al. 2009; Wang et. al. 2009; Dweik et. al. 2012)



Figure 10: Optical micrograph in reflectance mode of an interdigitated electrode (IDE) patterned by LAMP using S1813 photoresist. The inset shows a close-up view of the same IDE.

<u>3.7.2 Cell Trapping Microfluidic</u>

Another application of LAMP using the negative tone resist SU-8F is for the creation of microfluidic masters. A cell trapping array was fabricated by using a mask for an IDE like pattern and the laser was used to define 2 μ m channels between the prongs. Following development and PDMS molding, the mold was bonded to a glass slide. The result was micron-scale channels in the location where the SU-8F was polymerized. 5 μ m silica beads were flowed in an aqueous solution through these channels and were trapped at the intersection points between the laser drawn channels and the larger mask patterned channels (Figure 11). As with other examples of soft lithography, the master could be used repeatedly to generate new microfluidic molds. We used another mold to trap *S. cerevisia* cells in a similar device. Devices that create arrays like this could be useful for multiplexed single-cell assays, for size sorting particles or cells, or for mechanical deformability assays of cells (Wlodkowic et. al. 2009).

The power of LAMP is that making and testing these types of devices is very quick because the variable features, which are written with the laser, can be made in minutes and the lead-in channels, and the features which are made with the mask, need not change between prototypes. Thus LAMP enables prototyping with the "fail fast" mantra to quickly troubleshoot and optimize a design before committing to an expensive mask for mass production.





Figure 11: The image on the left shows an array of trapped 5 μ m diameter silica beads in a PDMS microfluidic device containing green dyed water (scale bar is 50 μ m). The right image shows an array of trapped *S. cerevisia* cells in a similar device (scale bar is 30 μ m).

4. CONCLUSION

In this work, we demonstrated a new hybrid lithography technique that combines conventional mask-based UV lithography with DLW to compensate for the drawbacks of each. Using Laser Augmented Microlithographic Patterning, LAMP, we showed that submicron laser written features could be registered to larger mask patterns to within about 2 μ m in both positive- and negative-tone photoresist. We demonstrated an interdigitated electrode and a microfluidic device as typical examples of our LAMP technique. We hope that others who have access to a DLW system, will consider using it to augment conventional lithography to increase the speed and efficiency with which they can generate their samples.

6.1 APPENDIX A: S1813 Linewidth Data

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Image Image <t< td=""><td></td><td></td><td>45</td><td>2 033</td><td></td><td></td><td></td><td>45</td><td>1 905</td><td></td><td></td><td></td><td>45</td><td>2 026</td><td></td><td></td><td>4</td><td>5 1 4 1 7</td></t<>			45	2 033				45	1 905				45	2 026			4	5 1 4 1 7
Image <th< td=""><td></td><td></td><td>50</td><td>1 788</td><td>ontic</td><td></td><td></td><td>50</td><td>1 883</td><td></td><td></td><td></td><td>50</td><td>1.861</td><td></td><td></td><td>5</td><td>1 401</td></th<>			50	1 788	ontic			50	1 883				50	1.861			5	1 401
Image: book of the state of the s			00		optio			55	1 785				55	1.755			5	5 1.177
Image: black Image: black <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>00</td><td>1.484</td><td></td><td></td><td></td><td>00</td><td>1.604</td><td></td><td></td><td>6</td><td>1 113</td></t<>								00	1.484				00	1.604			6	1 113
100 25 2.180 0 500 2.65 2.932 0 500 2.32 0 500 2.33 0 30 2.172 0 30 33 101 35 1.327 0 0 33 2.028 0 35 3.172 0 0 33 35 101 102 1.27 0 0 4.05 3.202 0 0.55 3.13 0 0 35 3.13 0 0 35 3.35 101 0.45 1.031 0 0 4.65 1.031 0 4.65 4.65 4.65 1.33 0 0 4.65 4									1.404					1.004				
1 000 1 200 2 200 2 200 <t< td=""><td></td><td>500</td><td>25</td><td>2 169</td><td></td><td></td><td>500</td><td>25</td><td>2 932</td><td></td><td></td><td>500</td><td>25</td><td>2 382</td><td></td><td></td><td>00 2</td><td>5 1.826</td></t<>		500	25	2 169			500	25	2 932			500	25	2 382			00 2	5 1.826
index index </td <td></td> <td>000</td> <td>30</td> <td>1 958</td> <td>ontic</td> <td></td> <td>000</td> <td>30</td> <td>2 339</td> <td></td> <td></td> <td>000</td> <td>30</td> <td>2 172</td> <td></td> <td></td> <td>3</td> <td>1.658</td>		000	30	1 958	ontic		000	30	2 339			000	30	2 172			3	1.658
$ \ \ \ \ \ \ \ \ \ \ \ \ \ $			35	1 327	optio			35	2.000				35	1 99			3	5 1 358
$ \ \ \ \ \ \ \ \ \ \ \ \ \ $			40	1 212				40	1 961				40	1 549			4	1.000
Image: book with the state of the state			40	1.031		-		40	1 738				40	1 334			4	5 1 123
$ \ \ \ \ \ \ \ \ \ \ \ \ \ $			50	0.84				50	1 599				50	1 227	not quite through?		5	1 1 1 5 2
$ \ \ \ \ \ \ \ \ \ \ \ \ \ $			00	0.04				55	1 359				55	1 209	not quite through:		5	5 1.077
								00	1 198				00	1.171			6	1.017
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$									1.100									1.040
0.00 0.00 1.00 0.00		200	25	1.535	ontic		300	25	1 724			200	25	1 729			00 2	1 102
		300	20	1 333	optic		500	20	1.7.54			300	20	1.606			2	1.133
			35	1.049				35	1.466				35	1 498	maybe not quite thr	ough	3	5 1.055
			40	0.799				40	1 209				40	1 166	Indybe not quite this	Jugii	4	0.913
			45	0.712	Not clear if i	ts through		45	1.011				40	0.984			4	5 0.834
			50	0.671	Not clear if i	ts through		50	0.978				50	0.936				0.872
$ \begin temperature relation to the temperature relation$			00	0.071		lo unough		55	0.070				55	0.000			5	5 0.802
A B B								60	0.937				60	0.301			5	0.728
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$								00	0.321				00	0.770				0.720
1 200 0 0.05 / 0		200	25	0.979	not clear		200	25	1 102			200	25	1 159			00 2	5 0.962
Image: Construction of the construction of		200	20	0.379	not clear	-	200	20	0.005			200	20	0.066			2	0.003
Action		-	35	0.699	(definitely no	t through)		35	0.335				35	0.877			3	5 0.771
Action Action<		-	40	0.033	(Gommely ne	/ anough)	-	40	0.941			-	40	0.82			4	0.631
no o.coc no on on <th< td=""><td></td><td>-</td><td>40</td><td>0.556</td><td></td><td></td><td>-</td><td>40</td><td>0.341</td><td>maubo not all</td><td>the ware three</td><td>uab</td><td>40</td><td>0.02</td><td></td><td></td><td>4</td><td>0.051</td></th<>		-	40	0.556			-	40	0.341	maubo not all	the ware three	uab	40	0.02			4	0.051
5 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.		1	40	0.330		-	-	0#	0.77	not though	uno mya uli Ul		60	0.730	not really through		4	, 0.457
33 0.007 33 0.037 33		1	50	0.400		-	-	30	0.667	not tribugil		-	50	0.000	not really unough		3	5
00 0000		1		-		1	-		0.007			-		0.007			5	, ,

Sample	Power	Speed	Linewidth	Sample	Power	Speed	Linewidth		Sample	Power	Speed	Linewidth	4	Average	std dev	Speed	Power	nm	Line Width	Std Dev	100
10 18 17	1100	25	2.837	10 18 17	1100	25	4.56		10 18 17	1100	25	4.493	3	3.840285714	0.68291177	2	5 20	0 1105	1.10500000	0.13778969	137.78969
PS3 2		30	2.681	PS4 1		30	4.025		PS4 2		30	4.131		3.474571429	0.67610146		30	0 1621.71429	1.62171429	0.21969441	219.69440
		35	2.439			35	3.627				35	4.027		3.207428571	0.65838684		50	0 2383.42857	2.38342857	0.41434349	414.34349
		40	2.324			40	3.353				40	3.53		2.909142857	0.52632747		70	0 2987	2.98700000	0.50981201	509.8120
		45	5 1.995			45	3.152				45	3.137		2.737714286	0.48787727		90	0 3503	3.50300000	0.77847892	778,4789
-		50	1 937			50	2.94				50	3.06		2 601285714	0.45581066		110	0 3840 28571	3 84028571	0.68291177	682 91177
		55	1.84			55	2 796				55	2 989		2 415857143	0 42227566			0			
		60	16			60	2 717				60	2 731		2 262571429	0.41748705	3	0 20	0 018 571420	0 91857143	0 1 2 9 9 2 5 8 8	170 0758
																	30	0 1413 57143	1 41357143	0 242254	242 25399
	000	26	0.954		000	25	2 0 2 0			000	25	4.247		2 502000000	0 77947907		50	0 2146 42957	2 14642957	0.20256642	202 56641
-	500	20	2.304		500	20	3.556			500	20	3 785		3.303000000	0.61731672	_	70	0 2656 85714	2.14042837	0.50250042	503 6522
-		25	2.040			25	3.252			-	25	3.400		027714200	0.51731072			0 2030.03714	2 22771420	0.61721672	617 21672
		33	2.311			30	3.332				30	3.405		2.537714200	0.525355557		110	0 2474 571423	3.23771423	0.67610146	676 10146
		40	2.077			40	3.06				40	0.700		2.0440000000	0.33124733		III	0 3474.37143	3.47437143	0.07010140	070.10140
		40	1 700			40	2.81				40	2.723		2.42885/143	0.41210822		5 30	0 973 439571	0 97747957	0 10567065	105 67064
		50	1.700			50	2.5/5				50	2./18		2.2095/1429	0.38850915		20	0 872.428571	0.8/24285/	0.10567965	105.67964
		55	1.009			55	2.00/				00	2.5/9	-	2.113285714	0.41808815		50	0 1349.57143	1.3495/143	0.22609453	226.09452
		60	1.497			60	2.289				60	2.374		1.9423333333	0.42865585		50	0 1/94./1429	1./94/1429	0.386/6341	386./6341
																	//	0 2354./1429	2.354/1429	0.43962752	439.62752
	700	25	2.451		700	25	3.459			700	25	3.52		2.987000000	0.50981201		90	0 2937.71429	2.93//1429	0.52539937	525.39937.
		30	2.182			30	3.038				30	3.03		2.656857143	0.50365227		110	0 3207.42857	3.20/4285/	0.65838684	658.38684.
		35	5 1.969			35	2.655				35	2.76	2	2.354714286	0.43962752			0			(
		40	1.811			40	2.471				40	2.407		2.151142857	0.35884343	4	0 20	0 784.571429	0.78457143	0.13132159	131.32158
		45	5 1.615			45	2.301				45	2.096	1	1.913285714	0.3198144		30	0 1167	1.16700000	0.28529404	285.29403
		50	1.744			50	2.119				50	2.082	1	1.839714286	0.25727463		50	0 1583.85714	1.58385714	0.35566733	355.66733
		55	5 1.676			55	2.089				55	1.974	1	1.742666667	0.29790308		70	0 2151.14286	2.15114286	0.35884343	358.84343
		60	1.484			60	1.835				60	1.856		1.562666667	0.29615316		90	0 2644	2.64400000	0.53124735	531.24735
																	110	0 2909.14286	2.90914286	0.52632747	526.327474
	500	25	5 1.876		500	25	2.653			500	25	2.846	2	2.383428571	0.41434349			C			(
		30	2.012			30	2.475				30	2.411	2	2.146428571	0.30256642	4	15 20	0 716.571429	0.71657143	0.15698408	156.98407
		35	5 1.576			35	2.133				35	2.153	1	1.794714286	0.38676341		30	0 962.285714	0.96228571	0.24524678	245.24678
		40	1.269			40	2.06				40	1.889		1.583857143	0.35566733		50	0 1389.71429	1.38971429	0.34837982	348.37982
		45	5 1.166			45	1.824				45	1.512	1	1.389714286	0.34837982		70	0 1913.28571	1.91328571	0.31981440	319.81439
igh		50	1.187			50	1.717				50	1.409	1	1.304428571	0.30879724		90	0 2428.85714	2.42885714	0.41210822	412.10822
		55	5 1.056			55	1.348				55	1.173	1	1.203666667	0.21032152		110	0 2737.71429	2.73771429	0.48787727	487.877274
		60	1.08			60	1.255				60	1.369	1	1.186000000	0.11513896			0			(
																5	0 20	0 693	0.69300000	0.14045015	140.45015
	300	25	i 1.472		300	25	1.861			300	25	1.829		1.621714286	0.21969441		30	0 921.428571	0.92142857	0.14521966	145.21966
		30	1.29			30	1.542				30	1.615	1	1.413571429	0.242254		50	0 1304.42857	1.30442857	0.30879724	308.79723
		35	i 1.17			35	1.633				35	1.576		1.349571429	0.22609453		70	0 1839.71429	1.83971429	0.25727463	257.274621
		40	1.049			40	1.541				40	1.492	1	1.167000000	0.28529404		90	0 2269.57143	2.26957143	0.38850915	388.5091
		45	0.851			45	1.118				45	1.226	0	0.962285714	0.24524678		110	0 2601.28571	2.60128571	0.45581066	455.81066
		50	0.827			50	1.134				50	1.032	0	0.921428571	0.14521966			a			
-		55	0.799			55	1.091				55	0.952	0	0.912666667	0.12010676	5	5 20	0 655.6	0.65560000	0.12703597	127.03597
		60	0.751			60	0.909				60	0.927	0	836333333	0 11950459		30	0 912 666667	0 91266667	0 12010676	120 10675
													-				50	0 1203 66667	1 20366667	0 21032152	210 32152
	200	25	0.923		200	25	1 207			200	25	1 312		1 105000000	0 13778969		70	0 1742 66667	1 74266667	0 29790308	297 9030
	200	30	0.829		200	30	0.971			200	30	1.012		1 918571479	0.12002588		90	0 2113 28571	2 11328571	0.41868813	418 6881
		35	0.813			35	0.963				35	0.984		1 877478571	0 10567965		110	0 2415 85714	2 41585714	0.42227566	472 27566
-		40	0.728	-	-	40	0.852			-	40	0.904		784571479	0 13132159		III		2.41505/14		
-		40	0.120			40	0.802				40	0.021		716571/20	0 15698408		.n	0 649 333222	0 64933222	0.08321/71	83 214707
-		40	0.00	-	-	45	0.867	not through		-	40	0.530		1 693000000	0.14045015		30	0 836 333333	0.83633333	0.11050450	119 50459
-		60	0.002	-	-	50	0.007	not through			22	0.004		1 655600000	0.12203597		50	0 1100	1 18600000	0.11513206	115 13805
		00	0.400			00	0.649	luct a dat			00	0.084			0.09221471		70	0 1563 66667	1 56366667	0.20615216	206 16216
		60				60	0.648	just a dot			60	U./19			0.003214/1		//	0 1002.00000/	1.00200000/	0.29010316	430.15315
										-			S	andard devi	stions		90	0 1942.33333	1.94233333	0.42865585	428.05584

6.2 APPENDIX B: SU-8F Registration Data

From SEM n	neasurements															
Power	ps2	ps3	ps4													
200		0.74		average	*1000											
300	1.09	1.63	1.07	1.26333333	1263.33333											
400	1.28	1.83	1.36	1.49	1490											
500	1.74	2.12	1.85	1.90333333	1903.33333											
600	2 15	2 32	2 53	2 33333333	2333 33333											
	2.115	2.52	2.55	2.000000000	2000.00000											
300	1263 33333															
400	1/90															
500	1903 33333															
600	2333 33333															
	2333.33333															
ImageJ						a .								*****		
PSZ	1	2	3	4	5	Convert	1	2	3	4	5	Power	avg	*1000		
300uw	0.1	0.087	0.088	0.09	0.1		0.97895252	0.85168869	0.86147822	0.88105727	0.97895252	300	0.91042584	910.425844		
400uw	0.137	0.122	0.121	0.123	0.117		1.34116495	1.19432208	1.18453255	1.2041116	1.14537445	400	1.21390113	1213.90113		
500uw	0.183	0.172	0.18	0.184	0.182		1.79148311	1.68379834	1.76211454	1.80127264	1.78169359	500	1.76407244	1764.07244		
600uw	0.226	0.236	0.246	0.238	0.253		2.2124327	2.31032795	2.4082232	2.329907	2.47674988	600	2.34752814	2347.52814		
PS3	1	2	3	4	5	Convert	1	2	3	4	5	Power	avg	*1000		
300uw	0.092						0.90063632	0	0	0	0	300	0.18012726	900.636319		
400uw	0.145						1.41948116	0	0	0	0	400	0.28389623	1419.48116		
500uw	0.179						1.75232501	0	0	0	0	500	0.350465	1752.32501		
600uw	0.216						2.11453744	0	0	0	0	600	0.42290749	2114.53744		
PS5	1	2	3	4	5	Convert	1	2	3	4	5	Power	avg	*1000		
300uw	0.113	0.09	0.11	0.096	0.103		1.10621635	0.88105727	1.07684777	0.93979442	1.0083211	300	1.00244738	1002.44738		
400uw	0.175	0.179	0.18	0.157	0.156		1.71316691	1.75232501	1.76211454	1.53695546	1.52716593	400	1.65834557	1658.34557		
500uw	0.176	0.187	0.171	0.155	0.164		1.72295644	1.83064121	1.67400881	1.51737641	1.60548213	500	1.670093	1670.093		
600uw	0.234	0.249	0.237	0.22	0.231		2.2907489	2.43759178	2.32011747	2.15369555	2.26138032	600	2.2927068	2292.7068		
FINAL																
ps2 1	2	3	4	5	ps3	ps5 1	2	3	4	5					std dev	
0.97895252	0.85168869	0.86147822	0.88105727	0.97895252	0.90063632	. 1.10621635	0.88105727	1.07684777	0.93979442	1.0083211	300	951.363859	0.95136386		0.08666005	86.6600469
1.34116495	1.19432208	1.18453255	1.2041116	1.14537445	1,41948116	1.71316691	1.75232501	1.76211454	1.53695546	1.52716593	400	1434,61042	1.43461042			
1.79148311	1.68379834	1.76211454	1.80127264	1.78169359	1.75232501	1.72295644	1.83064121	1.67400881	1.51737641	1.60548213	500	1720.28657	1.72028657			
2.2124327	2.31032795	2.4082232	2.329907	2.47674988	2.11453745	2.2907489	2.43759178	2.32011747	2.15369555	2.26138032	600	2301.42838	2.30142838			

6.3 APPENDIX C: S1813 Registration Data

Wafee d	DY	DV	Ave DV	Ave DV		Middle DV	Middle DV		E-d DV					
water 1	DX	DY	AVg. DX	AVg. DY		Middle DX	Middle DY		End DX	End DY				
L10	1.134833333	4.77525	1.217541667	2.38003125		0.970416667	0.63075		1.464666667	4.1293125				
L1	1.160833333	0.89625												
R1	0.78	0 36525												
Dia	4 70.45	0.00020												
RIU	1.7945	3.463375												
Wafer 2	DX	DY												
L10	0.995516667	2.0535	1.560816667	0.9369375		0.705208333	0.5885625		2.416425	1.2853125				
11	0.43925	0.81475												
D1	0.40020	0.00075												
RI	0.971166667	0.362375												
R10	3.837333333	0.517125												
Wafer 3	DX	DY												
1.10	0.500000000	2 2005	0.755145000	1 01005005		0.554075	4 400 4075		0.050046667	4 202075				
	0.353033333	2.2093	0.755145655	1.21003023		0.001070	1.1254373		0.536510007	1.303073				
L1	0.546916667	1.0845												
R1	0.555833333	1.174375												
R10	1.324	0.31825												
Wafee 4	DV	DV												
water 4	DA	DT												
L10	0.831083333	1.10275	1.132104167	0.8993125		1.138583333	0.722625		1.125625	1.076				
L1	1.527416667	1.14175												
R1	0.74975	0.3035												
R10	1 420166667	1 04925												
	1. 120 100007	1.04323												
Wafer 5	DX	DY												
L10	1.03975	1.883125	0.997916667	1.1030625		1.096208333	0.9374375		0.899625	1.2686875				
11	1,263	1.121375												
P1	0.020416667	0 7525												
RI	0.929410007	0.7535												
R10	0.7595	0.65425												
Wafer 6	DX	DY												
1.10	1 257583333	0.83125	0.867708333	0 581625		0.380875	0 2453125		1 354541667	0.9179375				
1.4	0.07005	0.00120	0.001100000	0.001020		0.000010	0.2100120		1.001011001	0.0110010				
L1	0.37825	0.31325												
R1	0.3835	0.177375												
R1 R10	0.3835	0.177375 1.004625												
R1 R10	0.3835 1.4515 \$1813	0.177375 1.004625	dx	dv		dx	dv		dx	dv				
R1 R10	0.3835 1.4515 s1813	0.177375 1.004625	dx	dy	Middlo Ava	dx	dy	End Ava	dx	dy		how to use duite	find thata	
R1 R10	0.3835 1.4515 s1813	0.177375 1.004625 Total Avg	dx 1.088538889	dy 1.186270833	Middle Avg.	dx 0.807111111	dy 0.709020833	End Avg.	dx 1.3699666667	dy 1.663520833		how to use dy to	o find theta	
R1 R10	0.3835 1.4515 s1813	0.177375 1.004625 Total Avg	dx 1.088538889 n=144	dy 1.186270833 n=96	Middle Avg.	dx 0.807111111 n=72	dy 0.709020833 n=48	End Avg.	dx 1.369966667 n=72	dy 1.663520833 n=49		how to use dy to the bar is 26,00	o find theta Oum and is 1.66	um off
R1 R10	0.3835 1.4515 s1813	0.177375 1.004625 Total Avg	dx 1.088538889 n=144	dy 1.186270833 n=96	Middle Avg.	dx 0.807111111 n=72	dy 0.709020833 n=48	End Avg.	dx 1.369966667 n=72	dy 1.663520833 n=49		how to use dy to the bar is 26,00 0.00365811493	o find theta Oum and is 1.66 32 degree	um off
R1 R10	0.3835 1.4515 s1813 SU-8F	0.177375 1.004625 Total Avg	dx 1.088538889 n=144 dx	dy 1.186270833 n=96 dy	Middle Avg.	dx 0.807111111 n=72 dx	dy 0.709020833 n=48 dy	End Avg.	dx 1.369966667 n=72 dx	dy 1.663520833 n=49 dy		how to use dy to the bar is 26,00 0.00365811493 0.00006384615	o find theta 0um and is 1.66 32 degree 0000554 radian	um off
R1 R10	0.3835 1.4515 s1813 SU-8F	0.177375 1.004625 Total Avg	dx 1.088538889 n=144 dx 1.432199135	dy 1.186270833 n=96 dy 1.783013807	Middle Avg.	dx 0.807111111 n=72 dx 1.385958076	dy 0.709020833 n=48 dy 1.385963498	End Avg.	dx 1.369966667 n=72 dx 1.478440193	dy 1.663520833 n=49 dy 2.180064116		how to use dy to the bar is 26,00 0.00365811493 0.00006384615	o find theta Oum and is 1.66 32 degree 0000554 radian:	um off
R1 R10	0.3835 1.4515 s1813 SU-8F	0.177375 1.004625 Total Avg Total Avg	dx 1.088538889 n=144 dx 1.432199135	dy 1.186270833 n=96 dy 1.783013807	Middle Avg. Middle Avg.	dx 0.807111111 n=72 dx 1.385958076	dy 0.709020833 n=48 dy 1.385963498	End Avg. End Avg.	dx 1.369966667 n=72 dx 1.478440193	dy 1.663520833 n=49 dy 2.180064116		how to use dy to the bar is 26,00 0.00365811493 0.00006384615	o find theta Oum and is 1.66 32 degree 0000554 radian:	um off
R1 R10	0.3835 1.4515 s1813 SU-8F	0.177375 1.004625 Total Avg Total Avg	dx 1.088538889 n=144 dx 1.432199135 n=120	dy 1.186270833 n=96 dy 1.783013807 n=80	Middle Avg. Middle Avg.	dx 0.807111111 n=72 dx 1.385958076 n=60	dy 0.709020833 n=48 dy 1.385963498 n=40	End Avg. End Avg.	dx 1.369966667 n=72 dx 1.478440193 n=60	dy 1.663520833 n=49 dy 2.180064116 n=40		how to use dy to the bar is 26,00 0.00365811493 0.00006384615	o find theta 0um and is 1.66 32 degree 0000554 radian:	um off
R1 R10	0.3835 1.4515 \$1813 SU-8F	0.177375 1.004625 Total Avg	dx 1.088538889 n=144 dx 1.432199135 n=120	dy 1.186270833 n=96 dy 1.783013807 n=80	Middle Avg. Middle Avg.	dx 0.807111111 n=72 dx 1.385958076 n=60	dy 0.709020833 n=48 dy 1.385963498 n=40	End Avg. End Avg.	dx 1.369966667 n=72 dx 1.478440193 n=60	dy 1.663520833 n=49 dy 2.180064116 n=40		how to use dy to the bar is 26,00 0.00365811493 0.00006384615	o find theta 0um and is 1.66 32 degree 0000554 radian:	um off
R1 R10	0.3835 1.4515 s1813 SU-8F	0.177375 1.004625 Total Avg	dx 1.088538889 n=144 dx 1.432199135 n=120	dy 1.186270833 n=96 dy 1.783013807 n=80	Middle Avg. Middle Avg.	dx 0.807111111 n=72 dx 1.385958076 n=60	dy 0.709020833 n=48 dy 1.385963498 n=40	End Avg. End Avg.	dx 1.369966667 n=72 dx 1.478440193 n=60	dy 1.663520833 n=49 dy 2.180064116 n=40		how to use dy to the bar is 26,00 0.00365811493 0.00006384615	o find theta Oum and is 1.66 32 degree 0000554 radian	um off
R1 R10	0.3835 1.4515 s1813 SU-8F	0.177375 1.004625 Total Avg Total Avg s1813	dx 1.088538889 n=144 dx 1.432199135 n=120	dy 1.186270833 n=96 dy 1.783013807 n=80	Middle Avg. Middle Avg.	dx 0.807111111 n=72 dx 1.385958076 n=60	dy 0.709020833 n=48 dy 1.385963498 n=40	End Avg. End Avg.	dx 1.369966667 n=72 dx 1.478440193 n=60 SU-8F	dy 1.663520833 n=49 dy 2.180064116 n=40		how to use dy to the bar is 26,00 0.00365811493 0.00006384615	o find theta Oum and is 1.66 32 degree 0000554 radian	um off
R1 R10	0.3835 1.4515 s1813 SU-8F	0.177375 1.004625 Total Avg Total Avg	dx 1.088538889 n=144 dx 1.432199135 n=120	dy 1.186270833 n=96 dy 1.783013807 n=80 Middle Avera	Middle Avg. Middle Avg.	dx 0.807111111 n=72 dx 1.385958076 n=60 Fnd Average	dy 0.709020833 n=48 dy 1.385963498 n=40	End Avg. End Avg.	dx 1.369966667 n=72 dx 1.478440193 n=60 SU-8F Total Average	dy 1.663520833 n=49 dy 2.180064116 n=40	Middle Avera	how to use dy to the bar is 26,00 0.00365811493 0.00006384615	o find theta Oum and is 1.66 32 degree 0000554 radian	um off
R1 R10	0.3835 1.4515 \$1813 SU-8F	0.177375 1.004625 Total Avg Total Avg s1813 Total Average	dx 1.088538889 n=144 dx 1.432199135 n=120 dy	dy 1.186270833 n=96 dy 1.783013807 n=80 Middle Avera dy	Middle Avg. Middle Avg.	dx 0.807111111 n=72 dx 1.385958076 n=60 End Average dy	dy 0.709020833 n=48 dy 1.385963498 n=40 dy	End Avg.	dx 1.369966667 n=72 dx 1.478440193 n=60 SU-8F Total Average dv	dy 1.663520833 n=49 dy 2.180064116 n=40	Middle Avera	how to use dy to the bar is 26,00 0.00365811493 0.00006384615	o find theta Oum and is 1.66 32 degree 0000554 radian End Average	um off
R1 R10	0.3835 1.4515 s1813 SU-8F	0.177375 1.004625 Total Avg Total Avg s1813 Total Average dx	dx 1.088538889 n=144 dx 1.432199135 n=120 dy	dy 1.186270833 n=96 dy 1.783013807 n=80 Middle Avera dx	Middle Avg. Middle Avg. ge dy	dx 0.807111111 n=72 dx 1.385958076 n=60 End Average dx	dy 0.709020833 n=48 dy 1.385963498 n=40 dy	End Avg. End Avg.	dx 1.369966667 n=72 dx 1.478440193 n=60 SU-8F Total Average dx	dy 1.663520833 n=49 dy 2.180064116 n=40 dy	Middle Avera dx	how to use dy to the bar is 26,00 0.00365811493 0.00006384615 ge dy	o find theta Oum and is 1.66 32 degree 0000554 radian 0000554 radian End Average dx	um off
R1 R10	0.3835 1.4515 \$1813 SU-8F	0.177375 1.004625 Total Avg Total Avg s1813 Total Average dx 1.09	dx 1.088538889 n=144 dx 1.432199135 n=120 dy 1.19	dy 1.186270833 n=96 dy 1.783013807 n=80 Middle Avera dx 0.81	Middle Avg. Middle Avg. ge dy 0.71	dx 0.807111111 n=72 dx 1.385958076 n=60 End Average dx 1.37	dy 0.709020833 n=48 dy 1.385963498 n=40 dy dy 1.66	End Avg. End Avg.	dx 1.369966667 n=72 dx 1.478440193 n=60 SU-8F Total Average dx	dy 1.663520833 n=49 dy 2.180064116 n=40 dy	Middle Avera dx	how to use dy to the bar is 26,00 0.00365811493 0.00006384615 ge dy	o find theta Oum and is 1.66 32 degree 0000554 radian 0000554 radian End Average dx	um off
R1 R10	0.3835 1.4515 s1813 SU-8F	0.177375 1.004625 Total Avg Total Avg s1813 Total Average dx 1.09 n=144	dx 1.085538889 n=144 dx 1.432199135 n=120 dy 1.19 n=96	dy 1.186270833 n=96 dy 1.783013807 n=80 Middle Avera dx 0.81 n=72	Middle Avg. Middle Avg. ge dy 0.71 n=48	dx 0.807111111 n=72 dx 1.385958076 n=60 End Average dx 1.37 n=72	dy 0.709020833 n=48 dy 1.385963498 n=40 dy 1.66 n=48	End Avg.	dx 1.369966667 n=72 dx 1.478440193 n=60 SU-8F Total Average dx	dy 1.663520833 n=49 dy 2.180064116 n=40 dy	Middle Avera dx	how to use dy to the bar is 26,00 0.00365811493 0.00006384615 ge dy	o find theta Journ and is 1.66 32 degree 0000554 radian 0000554 radian End Average dx	um off
R1 R10	0.3835 1.4515 \$1813 SU-8F	0.177375 1.004625 Total Avg Total Avg s1813 Total Average dx 1.09 n=144	dx 1.088538889 n=144 dx 1.432199135 n=120 dy 1.19 n=96	dy 1.186270833 n=96 dy 1.783013807 n=80 Middle Avera dx 0.81 n=72	Middle Avg. Middle Avg. ge dy 0.71 n=48	dx 0.807111111 n=72 dx 1.385958076 n=60 End Average dx 1.37 n=72	dy 0.709020833 n=48 dy 1.385963498 n=40 dy 1.66 n=48	End Avg.	dx 1.369966667 n=72 dx 1.478440193 n=60 SU-8F Total Average dx	dy 1.663520833 n=49 dy 2.180064116 n=40 dy	Middle Avera dx	how to use dy to the bar is 26,00 0.00365811493 0.00006384615 ge dy	o find theta Oum and is 1.66 32 degree 0000554 radian End Average dx	um off
R1 R10	0.3835 1.4515 s1813 SU-8F	0.177375 1.004625 Total Avg Total Avg s1813 Total Average dx 1.09 n=144	dx 1.085538889 n=144 dx 1.432199135 n=120 dy 1.19 n=96 Total	dy 1.186270833 n=96 dy 1.783013807 n=80 Middle Avera dx 0.81 n=72 Center	Middle Avg. Middle Avg. ge dy 0.71 n=48 Outside	dx 0.807111111 n=72 dx 1.385958076 n=60 End Average dx 1.37 n=72	dy 0.709020833 n=48 dy 1.385963498 n=40 dy 1.66 n=48	End Avg.	dx 1.369966667 n=72 dx 1.478440193 n=60 SU-8F Total Average dx	dy 1.663520833 n=49 dy 2.180064116 n=40 dy dy	Middle Avera dx Center	how to use dy to the bar is 26,00 0.00365811493 0.00006384615 ge dy Outside	o find theta Journ and is 1.66 32 degree 0000554 radian End Average dx	um off
R1 R10	0.3835 1.4515 s1813 SU-8F	0.177375 1.004625 Total Avg Total Avg s1813 Total Average dx 1.09 n=144	dx 1.088538889 n=144 dx 1.432199135 n=120 dy 1.19 n=96 Total 1.00	dy 1.186270833 n=96 dy 1.783013807 n=80 Middle Avera dx 0.81 n=72 Center 0.91	Middle Avg. Middle Avg. ge dy 0.71 n=48 Outside	dx 0.807111111 n=72 dx 1.385958076 n=60 End Average dx 1.37 n=72	dy 0.709020833 n=48 dy 1.385963498 n=40 dy 1.66 n=48	End Avg.	dx 1.369966667 n=72 dx 1.478440193 n=60 SU-8F Total Average dx	dy 1.663520833 n=49 dy 2.180064116 n=40 dy dy Total	Middle Avera dx Center	how to use dy to the bar is 26,00 0.00365811493 0.00006384615 ge dy Outside	o find theta Oum and is 1.66 32 degree 0000554 radian End Average dx	um off
R1 R10	0.3835 1.4515 s1813 SU-8F	0.177375 1.004625 Total Avg s1813 Total Average dx 1.09 n=144	dx 1.088538889 n=144 dx 1.432199135 n=120 dy 1.19 n=96 Total 1.09	dy 1.186270833 n=96 dy 1.783013807 n=80 Middle Avera dx 0.81 n=72 Center 0.81	Middle Avg. Middle Avg. ge dy 0.71 n=48 Outside 1.33	dx 0.807111111 n=72 dx 1.385958076 n=60 End Average dx 1.37 n=72	dy 0.709020833 n=48 dy 1.385963498 n=40 dy 1.66 n=48	End Avg.	dx 1.369966667 n=72 dx 1.478440193 n=60 SU-8F Total Average dx dx	dy 1.663520833 n=49 dy 2.180064116 n=40 dy Total 1.43 1.43	Middle Avera dx Center 1.33	how to use dy to the bar is 26,00 0.00365811493 0.00006384615 ge dy Outside 1.48	5 find theta Ourn and is 1.66 32 degree 0000554 radian End Average dx	um off
R1 R10	0.3855 1.4515 \$1813 SU-8F	0.177375 1.004625 Total Avg S1813 Total Average dx 1.09 n=144 dx dy	dx 1.088538889 n=144 dx 1.432199135 n=120 dy 1.19 n=96 Total 1.09 1.19	dy 1.186270833 n=96 dy 1.783013807 n=80 Middle Avera dx 0.81 n=72 Center 0.83 0.71	Middle Avg. Middle Avg. dy 0.71 n=48 Outside 1.33 1.66	dx 0.807111111 n=72 dx 1.365958076 n=60 End Average dx 1.37 n=72	dy 0.709020833 n=48 dy 1.385963498 n=40 dy 1.66 n=48	End Avg.	dx 1.369966667 n=72 dx 1.478440193 n=60 SU-8F Total Average dx dx dy	dy 1.663520833 n=49 dy 2.180064116 n=40 dy Total 1.43 1.78	Middle Avera dx Center 1.39 1.39	how to use dy to the bar is 26,00 0.00365811493 0.00006384615 ge dy Outside 1.48 2.18	5 find theta Ourn and is 1.66 32 degree 0000554 radian End Average dx	um off
R1 R10	0.3855 1.4515 \$1813 SU-8F	0.177375 1.004625 Total Avg s1813 Total Average dx 1.09 n=144 dx dy n=	dx 1.088538889 n=144 dx 1.432199135 n=120 dy 1.19 n=96 Total 1.09 1.19 1.44	dy 1.186270833 n=96 dy 1.783013807 n=80 Middle Avera dx 0.81 n=72 Center 0.81 0.71 72	Middle Avg. Middle Avg. dy 0.71 n=48 Outside 1.37 1.66 722	dx 0.807111111 n=72 dx 1.385958076 n=60 End Average dx 1.37 n=72	dy 0.709020833 n=48 dy 1.385963498 n=40 dy 1.66 n=48	End Avg.	dx 1.369966667 n=72 dx 1.478440193 n=60 SU-9F Total Average dx dx dx dx dx x=	dy 1.663520833 n=49 dy 2.180064116 n=40 dy dy Total 1.78 1.20	Middle Avera dx Center 1.33 1.39 60	how to use dy to the bar is 26,00 0.00365811493 0.00006384615 ge dy Outside 1.48 2.18 60	o find theta Ourn and is 1.66 32 dearee 0000554 radian End Average dx	um off
R1 R10	0.3855 1.4515 \$1813 SU-8F	0.177375 1.004625 Total Avg Total Avg s1813 Total Average dx 1.09 n=144 dx dy nx= ny=	dx 1.088538889 n=144 dx 1.432199135 n=120 dy 1.19 n=96 Total 1.09 1.19 1.19 1.14 4 966	dy 1.186270833 n=96 dy 1.783013807 n=80 Middle Avera dx 0.81 n=72 Center 0.81 0.71 0.72 48	Middle Avg. Middle Avg. Middle Avg. dy 0.71 n=48 Outside 1.37 1.66 72 48	dx 0.807111111 n=72 dx 1.385958076 n=60 End Average dx 1.37 n=72	dy 0.709020833 n=48 dy 1.385963498 n=40 dy 1.66 n=48	End Avg.	dx 1.369966667 n=72 dx 1.478440193 n=60 SU-8F Total Average dx dx dx dx dx n=72	dy 1.663520833 n=49 dy 2.180064116 n=40 dy Total 1.43 1.78 1.78 1.20 800	Middle Avera dx Center 1.39 1.39 60 40	how to use dy to the bar is 26,00 0.00365811493 0.00006384615 ge dy Outside 1.48 2.18 60 40	o find theta Oum and is 1.66 32 degree 0000554 radian End Average dx	um off
R1 R10	0.3855 1.4515 \$1813 SU-8F	0.177375 1.004625 Total Avg S1813 Total Average dx 1.09 n=144 dy nz= ny=	dx 1.088538889 n=144 dx 1.432199135 n=120 dy 1.19 n=96 Total 1.09 1.14 1.99 1.14	dy 1.186270833 n=80 dy 1.783013807 n=80 Middle Avera dx 0.81 n=72 Center 0.83 0.71 722 48	Middle Avg. Middle Avg. ge dy 0.71 n=48 Outside 1.37 1.66 722 48	dx 0.807111111 n=72 dx 1.385958076 n=60 End Average dx 1.37 n=72	dy 0.709020833 n=48 dy 1.385963498 n=40 dy 1.66 n=48	End Avg.	dx 1.369966667 n=72 dx 1.478440193 n=60 SU-9F Total Average dx dx dx dx dx n= n= n= n= n= n= n= n= n= n=	dy 1.663520833 n=49 dy 2.180064116 n=40 dy Total 1.43 1.78 1.20 80	Middle Avera dx Center 1.39 60 40	how to use dy to the bar is 26,00 0.00365811493 0.00006384615 ge dy Outside 1.48 2.18 60 40	o find theta Ourn and is 1.66 32 dearee 0000554 radian End Average dx	um off
R1 R10	0.3855 1.4515 \$1813 SU-8F	0.177375 1.004625 Total Avg S1813 Total Average dx 1.09 n=144 dx dy nx= ny=	dx 1.08533889 n=144 dx 1.422199135 n=120 dy 1.19 n=96 Total 1.09 1.19 1.19 1.44 96	dy 1.186270833 n=96 dy 1.783013807 n=80 Middle Avera dx 0.81 n=72 Center 0.81 0.71 0.72 48	Middle Avg. Middle Avg. dy 0.71 n=48 Outside 1.37 1.66 72 48	dx 0.807111111 n=72 dx 1.385958076 n=60 End Average dx 1.37 n=72	dy 0.709020833 n=48 dy 1.385963498 n=40 dy 1.66 n=48	End Avg.	dx 1.369966667 n=72 dx 1.478440193 n=60 SU-8F Total Average dx dx dx dx dx dx dx	dy 1.663520833 n=49 dy 2.180064116 n=40 dy Total 1.43 1.78 1.20 80	Middle Avera dx Center 1.39 1.33 60 40	how to use dy to the bar is 26,00 0.00365811493 0.00006384615 ge dy Outside 1.48 2.18 60 40	o find theta Oum and is 1.66 32 degree 0000554 radian End Average dx	um off
R1 R10	0.3855 1.4515 \$1813 SU-8F	0.177375 1.004625 Total Avg S1813 Total Average dx 1.09 n=144 dy nz= ny=	dx 1.088538889 n=144 dx 1.432199135 n=120 dy 1.19 n=96 Total 1.09 1.144 96	dy 1.186270833 n=96 dy 1.783013807 n=80 Middle Avera dx 0.81 n=72 Center 0.83 0.71 722 48	Middle Avg. Middle Avg. ge dy 0.71 n=48 Outside 1.37 1.66 722 48	dx 0.807111111 n=72 dx 1.385958076 n=60 End Average dx 1.37 n=72	dy 0.709020833 n=48 dy 1.385963498 n=40 dy 1.66 n=48	End Avg.	dx 1.369966667 n=72 dx 1.478440193 n=60 SU-9F Total Average dx dx dx dx n= n= n= n= n= n= n= n= n= n=	dy 1.663520833 n49 dy 2.180084116 n=40 dy 1.43 1.78 1.20 80	Middle Avera dx Center 1.39 60 40	how to use dy to the bar is 26,00 0.00365811493 0.00006384615 ge dy Outside 1.48 2.18 60 40	o find theta Ourn and is 1.66 32 dearee 0000554 radian End Average dx	um off
R1 R10	0.3855 1.4515 \$1613 SU-8F	0.177375 1.004625 Total Avg Total Avg s1813 Total Average dx 1.09 n=144 dy dx dy mx= ny=	dx 1.08533889 n=144 dx 1.422199135 n=120 dy 1.19 n=96 Total 1.09 1.19 1.424 96 0.286257018	dy 1.186270833 n=96 dy 1.783013807 n=80 Middle Avera dx 0.81 n=72 Center 0.81 0.71 72 48 0.623381041	Middle Avg. Middle Avg. Middle Avg. dy 0.71 n=48 0utside 1.37 1.66 72 48	dx 0.807111111 n=72 dx 1.385958076 n=60 End Average dx 1.37 n=72	dy 0.709020833 n=48 dy 1.385963498 n=40 dy 1.66 n=48	End Avg.	dx 1.369966667 n=72 dx 1.478440193 n=60 SU-8F Total Averaged dx dx dx dx dx n=72 dx dx dx dx dx dx dx dx dx dx	dy 1.663520833 n=49 dy 2.180064116 n=40 dy Total 1.43 1.78 1.20 80	Middle Avera dx Center 1.39 1.39 60 40	how to use dy to the bar is 26,00 0.00365811493 0.00006384615 ge dy Outside 1.48 2.18 60 40	o find theta Oum and is 1.66 32 degree 0000554 radian End Average dx	um off
R1 R10	0.3855 1.4515 \$1813 SU-8F	0.177375 1.004625 Total Avg s1813 Total Average dx 1.09 n=144 dy nz= ny=	dx 1.088538889 n=144 dx 1.432199135 n=120 dy 1.19 n=96 Total 1.19 1.14 96 0.286257018	dy 1.186270833 n=80 dy 1.783013807 n=80 Middle Avera dx 0.81 n=72 Center 0.83 0.71 722 48 0.623381041	Middle Avg. Middle Avg. ge dy 0.71 n=48 Outside 1.37 1.66 722 48	dx 0.807111111 n=72 dx 1.385958076 n=60 End Average dx 1.37 n=72	dy 0.709020833 n=48 dy 1.385963498 n=40 dy 1.66 n=48	End Avg.	dx 1.369966667 n=72 dx 1.478440193 n=60 SU-9F Total Average dx dx dx dx dx n= n= n= n= n= n= n= n= n= n=	dy 1.663520833 n49 dy 2.180084116 n=40 dy Total 1.43 1.78 1.20 80	Middle Avera dx Center 1.39 60 40	how to use dy to the bar is 26,00 0.00365811493 0.00006384615 ge dy Outside 1.48 2.18 60 40	o find theta Ourn and is 1.66 32 dearee 0000554 radian End Average dx	um off
R1 R10	0.3855	0.177375 1.004625 Total Avg Total Avg s1813 Total Average dx 1.09 n=144 dx dy nx= ny=	dx 1.08533889 n=144 dx 1.422199135 n=120 dy 1.19 n=96 Total 1.09 1.19 1.424 96 0.286257018	dy 1.186270833 n=96 dy 1.783013807 n=80 Middle Avera dx 0.81 n=72 Center 0.81 0.71 72 48 0.623381041	Middle Avg. Middle Avg. Middle Avg. dy 0.71 n=48 0utside 1.37 1.66 72 48	dx 0.807111111 n=72 dx 1.385958076 n=60 End Average dx 1.37 n=72	dy 0.709020833 n=48 dy 1.385963498 n=40 dy 1.66 n=48	End Avg.	dx 1.369966667 n=72 dx 1.478440193 n=60 SU-8F Total Average dx dx dx dy nx= ny=	dy 1.663520833 n=49 dy 2.180064116 n=40 dy Total 1.43 1.78 1.20 80	Middle Avera dx Center 1.39 1.39 60 40	how to use dy to the bar is 26,00 0.00365811493 0.00006384615 ge dy Outside 1.48 2.18 60 40	o find theta Oum and is 1.66 32 degree 0000554 radian End Average dx	um off
R1 R10	0.3855 1.4515 \$1813 SU-8F	0.177375 1.004625 Total Avg S1813 Total Average dx 1.09 n=144 dy nz= ny=	dx 1.088538889 n=144 dx 1.432199135 n=120 dy 1.19 n=96 Total 1.19 1.14 96 0.286257018	dy 1.186270833 n=80 Middle Avera dx 0.81 n=72 Center 0.83 0.71 727 48 0.623381041	Middle Avg. Middle Avg. ge dy 0.71 n=48 Outside 1.37 1.66 722 48	dx 0.807111111 n=72 dx 1.385958076 n=60 End Average dx 1.37 n=72	dy 0.709020833 n=48 dy 1.385963498 n=40 dy 1.66 n=48	End Avg.	dx 1.369966667 n=72 dx 1.478440193 n=60 SU-9F Total Average dx dx dx dx n= ny=	dy 1.663520833 n=49 dy 2.180064116 n=40 dy Total 1.43 1.78 1.20 80	Middle Avera dx Center 1.39 60 40	how to use dy to the bar is 26,00 0.00365811493 0.00006384615 ge dy Outside 1.48 2.18 60 40	o find theta Ourn and is 1.66 32 dearce 0000554 radian End Average dx	dy
R1 R10	0.3855	0.177375 1.004625 Total Avg s1813 Total Average dx 1.09 n=144 dx dy mx= ny=	dx 108538889 n=144 dx 1.422199135 n=120 dy 1.19 1.09 1.19 1.19 1.09 1.19 0.286257018	dy 1.186270833 n=96 dy 1.783013807 n=80 Middle Avera dx 0.81 n=72 Center 0.81 0.71 72 48 0.623381041	Middle Avg. Middle Avg. ge dy 0.71 n=48 Outside 1.37 1.66 72 48	dx 0.807111111 n=72 dx 1.385958076 n=60 End Average dx 1.37 n=72	dy 0.709020833 n=48 dy 1.385963498 n=40 dy 1.66 n=48	End Avg.	dx 1.369966667 n=72 dx 1.478440193 n=60 SU-8F Total Average dx dx dx dx dx dy mx= ny=	dy 1.663520833 n=49 dy 2.180064116 n=40 dy Total 1.43 1.78 1.20 80 80	Middle Avera dx Center 1.39 1.39 60 40	how to use dy to the bar is 26,00 0.00365811493 0.00006384615 ge dy Outside 1.48 2.18 60 40	o find theta Oum and is 1.66 22 degree 0000554 radian End Average dx	um off
R1 R10	0.3855 1.4515 \$1813 SU-8F	0.177375 1.00425 Total Avg	dx 1.088538889 n=144 dx 1.432199135 n=120 dy 1.19 n=96 Total 1.09 1.144 96 0.286257018	dy 1.186270833 n=80 dy 1.783013807 n=80 Middle Avera dx 0.81 n=72 Center 0.81 0.71 722 48 0.623381041	Middle Avg. Middle Avg. ge dy 0.71 n=48 Outside 1.37 1.66 72 48	dx 0.807111111 n=72 dx 1.385958076 n=60 End Average dx 1.37 n=72	dy 0.709020833 n=48 dy 1.385963498 n=40 dy 1.66 n=48	End Avg.	dx 1.369966667 n=72 dx 1.478440193 n=60 SU-8F Total Average dx dx dx dy nz= ny=	dy 1.663520833 n49 dy 2.180064116 n=40 dy Total 1.43 1.78 1.20 80	Middle Avera dx Center 1.39 1.33 60 40	how to use dy to the bar is 26,00 0.00365811493 0.00006384615 ge dy Outside 1.48 2.18 60 40	o find theta Ourn and is 1.66 32 dearee 0000554 radian End Average dx	um off
R1 R10	0.3855	0.177375 1.004625 Total Avg s1813 Total Average dx 1.09 n=144 dx dy mx= ny=	dx 108538889 n=144 dx 1.422199135 n=120 dy 1.19 n=96 Total 1.09 1.19 1.42 96 0.286257018 Total (S1813)	dy 1.186270833 n=96 dy 1.783013807 n=80 Middle Avera dx 0.81 n=72 Center 0.81 0.71 0.72 48 0.623381041 Center (S1811	Middle Avg. Middle Avg. ge dy 0.71 n=48 Outside 1.37 1.66 72 48 0utside (S18	dx 0.807111111 n=72 dx 1.385958076 n=60 End Average dx 1.37 n=72 Total (SU-8F)	dy 0.709020833 n=48 dy 1.385963498 n=40 dy 1.66 n=48	End Avg.	dx 1.369966667 n=72 dx 1.478440193 n=60 SU-8F Total Average dx dx dx dx dx dx s=0 SU-8F Total Average dx dx s=0 SU-8F SU-	dy 1.663520833 n=49 dy 2.180064116 n=40 dy Total 1.43 1.78 1.20 80 80	Middle Avera dx Center 1.39 660 40	how to use dy to the bar is 26,00 0.00365811493 0.00006384615 ge dy Outside 1.48 2.18 60 40	D find theta Ourn and is 1.66 32 degree 0000554 radian End Average dx	um off
R1 R10	0.3855 1.4515 \$1813 SU-8F	0.177375 1.004625 Total Avg 51813 Total Avg s1813 Total Average dx dx dy n=144 dx dy nx= ny= dx dx	dx 1.088538889 n=144 dx 1.432199135 n=120 dy 1.19 n=96 Total 0.286257018 0.286257018 Total (S1813) 1.09	dy 1.186270833 n=96 dy 1.783013807 n=80 Middle Avera dx 0.81 0.71 72 Center 0.83 0.71 72 48 0.623381041 0.6233810 0.623381041 0.62338100 0.62338100 0.62338100000000000000000000000000000000000	Middle Avg. Middle Avg. ge dy 0.71 n=48 Outside 1.33 1.66 72 48 Outside (S18 1.33	dx 0.807111111 n=72 dx 1.385958076 n=60 End Average dx 1.37 Total (SU-BF) 1.43	dy 0.709020833 n=48 dy 1.385963498 n=40 dy 1.66 n=48 Center (SU-81 1.39	End Avg.	dx 1.369966667 n=72 dx 1.478440193 n=60 SU-9F Total Average dx dx dx dx dx dx dx dx dx dx	dy 1.663520833 n=49 dy 2.180064116 n=40 dy 1.43 1.78 1.20 80 	Middle Avera dx Center 1.39 60 40	how to use dy to the bar is 26,00 0.00365811493 0.00006384615 ge dy Outside 1.48 2.18 60 40	b find theta Ourn and is 1.66 32 dearee 0000554 radian End Average dx	um off
R1 R10	0.3855	0.177375 1.004625 Total Avg s1813 Total Average dx 1.09 n=144 dy dx dy n=144 dy n=144 dy dy dx dy dy dx dy dy dx dy dy dy dy dy dy dy dy dy dy dy dy dy	dx 1088538889 n=144 dx 1422199135 n=120 dy 1.19 n=96 Total 1.09 1.19 0.286257018 Total (S1813) 1.09 1.19 1.09 1.19 1.09 1.19 1.09 1.19 1.09 1.19 1.09 1.19 1.19 1.09 1.19 1.09 1.19 1.09 1.19 1.09 1.19 1.09 1.19 1	dy 1.186270833 n=96 dy 1.783013807 n=80 Middle Avera dx 0.81 n=72 Center 0.81 0.71 722 48 0.623381041 Center (S181 0.81 0.81 0.81 0.81 0.81 0.81 0.81 0	Middle Avg. Middle Avg. ge dy 0.71 n=48 Outside 1.37 1.66 7.2 48 0utside (S18 1.37 1.66	dx 0.807111111 n=72 dx 1.385958076 n=60 End Average dx 1.37 n=72 Total (SU-8F' 1.43 1.78	dy 0.709020833 n=48 dy 1.385963498 n=40 dy 1.66 n=48 Center (SU-81 1.39 1.39	End Avg.	dx 1.369966667 n=72 dx 1.478440193 n=60 SU-8F Total Average dx dx dx dx dx dx n=6 BF)	dy 1.663520833 n=49 2.180064116 n=40 dy Total 1.43 1.78 1.78 1.78 80 	Middle Avera dx Center 1.39 60 40	how to use dy to the bar is 26,00 0.00365811493 0.00006384615 ge dy Outside 1.48 2.18 60 40	D find theta Ourn and is 1.66 32 degree 0000554 radian End Average dx	um off
R1 R10	0.3855 1.4515 \$1813 SU-8F	0.177375 1.004625 Total Avg 51813 Total Avg s1813 Total Average dx dy n=144 dx dy nx= ny= dx dx dy ny=	dx 1.088538889 n=144 dx 1.432199135 n=120 dy 1.19 n=96 Total 1.09 1.19 1.09 1.19 0.286257018 0.286257018 Total (S1813) 1.09 1.19 1.44 1.19 1.19 1.19 1.42 1.19	dy 1.186270833 n=96 dy 1.783013807 n=80 Middle Avera dx 0.81 0.71 72 48 0.623381041 0.62338100 0.62338100 0.62338100 0.62338100000000000000000000000000000000000	Middle Avg. Middle Avg. Middle Avg. Middle Avg. Middle Avg. 0.71 n=48 Outside 72 48 Outside (S18 0.00000000000000000000000000000000000	dx 0.807111111 n=72 dx 1.385958076 n=60 End Average dx 1.37 Total (SU-8F] 1.43 1.78 1.78 1.78	dy 0.709020833 n=48 dy 1.385963498 n=40 dy 1.66 n=48 center (SU-81 1.39 1.39 0.39	End Avg. End Avg.	dx 1.369966667 n=72 dx 1.478440193 n=60 SU-8F Total Average dx dy nx= ny= SF)	1.663520833 n=49 dy 2.180064116 n=40 dy dy 1.43 1.43 1.78 1.20 80	Middle Avera dx Center 1.39 60 40	how to use dy to the bar is 26,00 0.00365811493 0.00006384615 ge dy Outside 1.48 2.18 60 40 40	b find theta Ourn and is 1.66 32 dearee 0000554 radian End Average dx	um off
R1 R10	0.3855	0.177375 1.004625 Total Avg s1813 Total Average dx 1.09 n=144 dy dx dy n=144 dy dy n=144 dx dy n=144 dx dy n=144 dx dy n=144 dx dy n=14 dx dx dy n=14 dx dx dy dy dx dx dx dx dx dx dx dx dx dx dx dx dx	dx 1088538889 n=144 dx 1422199135 n=120 dy 1.19 n=96 Total 1.09 1.19 1.44 96 0.286257018 Total (S1813) 1.09 1.19 1.09 1.19 1.44 2.45 1.09 1.19 1.45 1.09 1.19 1.45 1.09 1.19 1.45 1.09 1.19 1.45 1.09 1.19 1.45 1.09 1.19 1.45 1.09 1.19 1.45 1.09 1.19 1.45 1.09 1.19 1.45 1.09 1.19 1.45 1.09 1.19 1.45 1.09 1.19 1.45 1.09 1.19 1.45 1.09 1.19 1.45 1.09 1.19 1.45 1.09 1.19 1.45 1.09 1.19 1.45 1.19 1.45 1.19 1.45 1.19 1.45 1.19 1.45 1.45 1.19 1.45 1.4	dy 1.186270833 n=96 dy 1.783013807 n=80 Middle Avera dx 0.81 n=72 Center 0.81 0.71 722 48 0.623381041 Center (S181 0.81 0.71 72 2 48	Middle Avg. Middle Avg. Middle Avg. ge dy 0.71 n=48 Outside 1.37 1.66 72 48 Outside (S18 1.37 1.66 72 72 72 72	dx 0.807111111 n=72 dx 1.385958076 n=60 End Average dx 1.37 n=72 Total (SU-8F 1.43 1.78 1.42 1.22 0.22	dy 0.709020833 n=48 dy 1.385963498 n=40 dy 1.666 n=48 Center (SU-81 1.39 0.39 0.00	End Avg. End Avg. End Avg. Outside (SU- 1.48 1.48 2.218 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	dx 1.369966667 n=72 dx 1.478440193 n=60 SU-8F Total Average dx dx dx dx dx n=72 SU-8F Total Average dx dx BF)	dy 1.663520833 n49 dy 2.180064116 n=40 dy Total 1.78 1.70 1.020 80 	Middle Avera dx Center 1.39 60 40	how to use dy to the bar is 26,00 0.00365811493 0.00006384615 dy dy Outside 1.48 2.18 60 40 40	D find theta Ourn and is 1.66 32 degree 0000554 radian End Average dx	um off

6.4 APPENDIX D: SU-8F Registration Data

B Wafer 1	DX		DY	Avg. DX	Avg. DY		Middle D	х	Middle DY	(End DX	(End DY	
L10		1.040875	0.78425	0.917020833	0.8844375			0.793166667		0.984625			1.040875		0.78425
L1		0.793166667	0.984625												
R1															
R10															
B Wafer 2	DX		DY												
L10		1.376	4.048875	0.989833333	3.0761875			0.603666667		2.1035			1.376		4.048875
L1		0.603666667	2.1035												
R1															
R10															
9.21 2	DX		DY												
L10		1.573917931	3.28836425	1.382448004	1.633642496			1.419336706	1	1.385961214		· ·	1.345559303		1.881323777
L1		1.749578415	0.94856661												
R1		1.089094997	1.823355818												
R10		1.117200675	0.474283305												
10.06	DX		DY												
L10		0.920460933	3.319983137	1.22084036	1.920847386			0.95559303	(0.685075885			1.48608769		3.156618887
L1		1.250702642	0.853709949												
R1		0.660483418	0.516441821												
R10		2.051714446	2.993254637												
10.10 1	DX		DY												
L10		3.766160764	0.748313659	2.059443508	1.056597808			1.926644182	1	1.090851602			2.192242833		1.022344013
L1		2.230185497	0.822091062												
R1		1.623102867	1.359612142												
R10		0.618324902	1.296374368												
10.10 2	DX		DY												
L10		1.665261383	3.520236088	2.023608769	2.126370152			2.617341203	2	2.065767285			1.429876335		2.186973019
L1		3.330522766	2.266020236												
R1		1.90415964	1.865514334												
R10		1.194491287	0.853709949									1		1	
				dx	dy		dx		dy			dx		dy	
			I otal Avg	1.432199135	1.783013807	Middle Avg.		1.385958076	1	1.385963498	End Avg.		1.478440193		2.180064116
				n=120	n=80		n=60		n=40			n=60		n=40	
Outlier	-														
9.21 1	DX		DY												
L10		7.51826869	18.23355818												
L1		3.632658797	5.111720067												
K1		7.173974143	1.981450253												
R10		4.503934795	11.59359191												
							1					1		1	

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