

M. W. TINDER COMMISSIONER OF HIGHWAYS

COMMONWEALTH OF KENTUCKY DEPARTMENT OF HIGHWAYS FRANKFORT

December 13, 1954

ADDRESS REPLY TO

ATTENTION: D. 2. 1. D. 1. 7.

MEMO TO: D. V. Terrell Director of Research

Last year when results of the state-wide acid water survey were reviewed from the standpoint of policies governing drainage pipe installations, the permanency of bituminous coatings on metal pipe was a point that remained undecided. No exception was taken to the conclusion that metal was adequately protected as long as the coating or pavement remained intact, but most of those attending the review meeting doubted whether the performance of coatings on a few pipe placed in the main highway system 25 or 30 years ago was representative of performance that could be expected from coatings on a variety of metal pipe placed since the beginning of the Rural Secondary program.

As a result of this concern, Mr. Bray requested that a fairly extensive survey of Rural Secondary projects be made to determine the conditions that existed. This was done by E. M. West during the past summer, and his findings are contained in the attached report. Almost 300 bituminous-coated culverts on 51 Rural Secondary roads were inspected. The roads were in 26 widely scattered counties, and the dates of installation ranged from 1949 to 1952 - about the extent to which a sampling of the R. S. program could be taken. All sizes of pipe and pipe arches were represented, and a few uncoated multiplate arches were included because of the convenience for inspection.

In essence the survey showed that on practically all pipe correctly installed the coatings and pavements were in excellent condition except at the ends, and at points where sustained wetting and drying has occurred. Invariably light - and particularly direct sunlight - has caused cracking of the bituminous material, so that only those pipes with ends shaded are free from severe cracking. This, of course, is mainly a result of exposure to ultra violet light, an influence to which unmodified asphalt cements have notoriously little resistance. Fortunately deterioration of this sort extends into the pipe only a short distance, and on the pipe inspected (maximum age about 6 years) there was no evidence of removal of the asphalt or deterioration in the metal, even though some of the cracks were deep enough to expose the metal. Conditions might have been different had any of the pipe been carrying acid water.

D. V. Terrell

Scaling of the asphalt to slight depths was caused by frequent and sustained wetting and drying. This appeared most often along the elevation of low flow or the "trickle" line in culverts where flow is continuous but variations in the water level are very small except during periods of heavy runoff. Scaling in this manner extended throughout the length of the culvert. Normally the scales adhered and were not removed, particularly where flow was confined to the bituminous pavement. Wherever the culvert had been installed incorrectly and the pavement was not in the invert, scaling damage to the bituminous coating was always severe, provided the wetting and drying conditions prevailed.

Insofar as bituminous coatings and pavements are concerned, I doubt that there is a significant difference between those applied today and the ones applied by comparable manufacturers 25 or 30 years ago. Construction conditions which favored shading, heavy silting in most of the coated culverts that were found, and the installation of pipe in positions that did not permit continuous flow account for the absence of cracking and scaling in the structures which were studied in the acid water survey. All these locations were revisited this fall to correlate circumstances in the earlier and the recent studies.

The report contains some other observations about drainage structures that are worthwhile, and in addition it brings up to date our records of the test installation at Mortons Gap - which was started four years ago in conjunction with the acid water study. Progressive deterioration in some of the sections is evident, and another pipe has been removed since the last report was made. In brief the experiment continues to point up the often-told story about the cleaning power of acids in drainage systems, which closes with the admonition "....don't use sulphuric acid - it eats hell out of the pipes."

Respectfully submitted,

L.E. Stry

L. E. Gregg Assistant Director of Research

LEG:ddc Copies to: Research Committee Mack Galbreath (3) Commonwealth of Kentucky Department of Highways

AN INVESTIGATION OF BITUMINOUS COATINGS AND PAVEMENTS ON CORRUGATED METAL CULVERTS

(Rural Secondary Projects 1949-1951)

by

Eugene M. West Research Engineer

Highway Materials Research Laboratory Lexington, Kentucky

November, 1954

INTRODUCTION

The object of this inspection was to determine the efficacy of bituminous coatings and paved inverts on corrugated metal pipe and culverts installed on Rural Secondary Projects during the past few years. The study originated after earlier investigations had led to recommendations concerning the resistance of various types of pipe and culvert materials in the presence of acid-bearing waters.*

One of the conclusions from the acid-water survey was that "bituminous-coated metal pipe is resistant to acid corrosion as long as the coating insulates the metal from contact with acids." The condition of bituminous-coated pipe located in the primary and secondary roads which were surveyed in 1952 conveyed the impression that these coatings could be relied upon to adhere well and protect the metal for periods upward from 15 years. This was based not only on the few (approximately 30) coated pipe in the roads surveyed that year, but also on information obtained from surveys in other states. The pipe represented in the 1952 survey ranged up to 30 years in age.

When recommendations contained in the report on the work were considered from the standpoint of policies that should be applied to cross drains and entrance pipes on various classes of roads, there was some doubt about the comparability of coatings placed on pipe more than 15 years ago and the coatings applied to pipe in recent years. This was based on occasional observations made by others on Rural Secondary Projects where the pipe had been installed since 1948. Numerous failures of coatings were reported.

* See Report No. 2 on "A Survey of Acidity in Drainage Waters and the Condition of Highway Drainage Installations", by J. H. Havens, Highway Materials Research Laboratory, December 1952.

Inasmuch as the acid-water surveys had not included any roads in the Rural Secondary class, there was no basis for direct comparison between the older and the more recent coatings. As a result, the Division of Research was asked to extend its observations of bituminous-coated pipe to include many of those installed since the beginning of the Rural Secondary program. This is the report of those observations, supplemented by data from the drainage test installation at Morton's Gap which was started in April 1951, and on which the last report was made in December 1952.

GENERAL CONSIDERATION

- 3

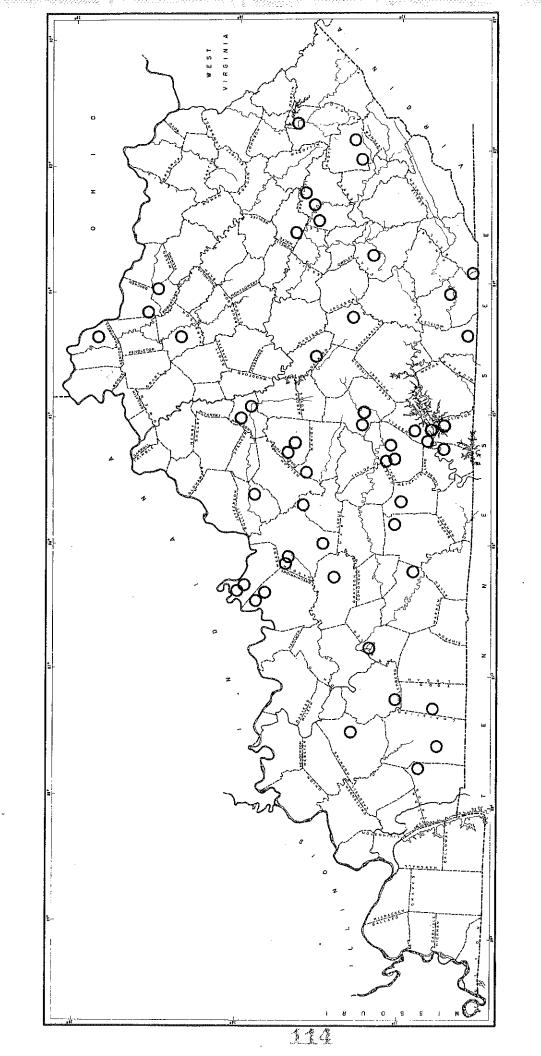
Selection of Culverts

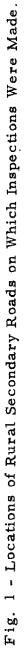
Locations of coated and paved pipes were selected through a review of final estimates on Rural Secondary Projects dating from the beginning of the Rural Secondary program in 1948 to and including 1951. Only those roads for which the records indicated use of bituminous coated corrugated metal (BCCM) pipe were considered.

Inspections were made on the majority of these roads, the principal exceptions being cases where there were more than two or three such projects in a county, or where the projects were very close together. An att empt was made to spread the inspections in order to include reasonably representative samples from all the areas in which culverts of this type had been used. General locations of roads on which inspections were made are shown in Fig. 1.

Inspection Procedure

At the outset it was decided that an analysis of each structure by some physical test on the material or by some definite yardstick of performance would not be feasible. A reasonable alternative was to make a complete inspection of representative culverts on the roads chosen for study, and from that record as much field information as could be obtained through inspections of the inside coating and pavement in its entirety and the outside coating wherever possible. The evaluation included not only visual observations as such, but also a superficial test for adhesion by which attempts were made to peel the coating or pavement. In addition, resistance to penetration was roughly estimated by use of





a knife blade - the result proving some measure of hardness or dryness of the coating material. Photographs showing the general conditions encountered, were taken at each location and kept as a visual record of the inspections.

Whenever the presence of acid water at a culvert site was definitely suspected, the pH was measured with methyl orange or methyl red, and the value recorded. Drops of methly orange were placed in the water for the range of acidity of pH 3.1 to pH 4.4 and methyl red for the range of 4.4 to 6.0. Since the majority of streams associated with the culverts studied were dry at the time of inspection, the pH test had limited application. When possible, these tests were conducted in pools of water elsewhere in the stream, but always close to the culvert involved.

Note was made of any situation thought to have had some influence on the condition of the coating and pavement observed at the time of inspection. In addition, these data included information relating to suggested improvements as well as comments on errors in construction.

Records

Since there was no standard procedure for this type of field study, it was decided that performance of the culverts would be judged according to conditions set forth in an inspection form (See Fig. 2). The form was designed to include: (1) a full description of the structure, (2) the date of installation, (3) general classification of as much of the drainage area that it was feasible to observe in the field, and (4) apparent condition

- 4

1.15

	INSPECTION NO.	Bituminous Coated Coated & Paved Paved Invert
LOCATION		
	Dir. Com	Dine Arch No. Lath
		Pipe Arch NoLgth
GradeEst. C	over(Skewed,	Beveled, Headwall)Gen. Cond
FLOW:	TYPE DRAINAG	E: MAINTENANCE CONDITI
Continuous	Cult. Land	Excellent
Frequent	Pasture	Very Good
Intermit	Hilly Wooded	
Filling	Wooded Swamp	Poor
Erosion:	Farmyard	Pvt. Alin.
Sand	Sewage	Type Soil:
Gravel	Mine Water	Black Loam
Boulders	pH Paper	Clay
Shale	pH Meter	Shale
	Water Sample	Sandy
ASPHALT: Adhesion Exceller Adhesion Good Ashesion Fair Adhesion Poor Coating Checked Percent Missing Average Thicknes Could be Stripped SPELTER: Like New Pin Point Rust Tubercular Rust Spelter Gone Loose Scaly Rust Heavy Pitting	5	Adhesion Excellent Adhesion Good Adhesion Fair Adhesion Poor Longitudinal Cracks Circumferential Cracks Width of Cracks Depth of Cracks Percent Missing Ave. Thickness over Crests INSPECTION DATE INSPECTED BY
Periorated		

Fig. 2 - Sample of Inspection Form used in recording data for the present study. of the coating and pavement. Provision was made for some features that could influence the degree of performance as well as for symptoms of failure.

Even though the spelter coating of metal was not directly related to bituminous coatings, effort was made to note the condition of the spelter where metal had become exposed on BCCM pipe. Also, in a few instances where an uncoated pipe having the same service life was located close to a coated pipe, both were inspected for the purpose of comparison. Another type structure - the uncoated metal arch fabricated on the site - was encountered on several occasions and incidental observations were made at those locations because of its function and similarity to the structures in question.

Information from the inspection forms are summarized in Table 1 in the Appendix. Much of the original material has been abbreviated in the table, particularly in the column headed Remarks, the intent being to save space and eliminate comments in the field notes that had no particular bearing on coatings or pavements for corrugated metal pipe.

- 5

RESULTS OF FIELD OBSERVATIONS

- 6

After inspections had been completed on a few of the roads it was evident that certain features in the performance of the coatings and pavements were common to all the installations. Although deterioration is undoubtedly progressive, the tendency toward development of these features was independent of the age of the pipe, all of which were from 2 to 5 years old at the time. Also it was independent of location in the state, and with the exception of ponding it was independent of location with respect to various features of the stream.

The most significant influences were manner of placement of the culvert at the time of construction, shading or lack of shading at the inlet and outlet, slope of the pipe under some circumstances, and maintenance conditions. This, of course, did not apply to the uncoated structures which were included for reasons previously mentioned.

Condition of the Coating

In all but a few of the BCCM structures the overall condition of the coating ranged from good to excellent. There were a few cases where dripping had occurred (but never to any great extent), indicating that adhesion was reasonably good but temperature susceptibility of the bituminous material was too great. In some culverts there was evidence of slight checking of the coating in the end portion. However, in no instance did this action expose the metal. In many cases, scratching and scarring of the coating (caused by improper handling) was found.

The outside coating of structures of any age was usually cracked and flaking off, except when the exposed part of the pipe was located in a shaded area. Almost invariably the outside coating on that portion of pipe buried within the fill was rapidly deteriorating or completely removed. However, there were no locations where additional deterioration such as removal of the spelter and consequent rusting was noted.

- 7

There were two special cases of extreme deterioration in coatings, which were caused by service conditions for which the coatings were not intended. These are covered specifically later under headings dealing with improper placement and burning of drift.

Condition of Pavement

In approximately 90 percent of the locations the pavement was in an excellent state almost throughout the entire length of the culvert. At the extremities (for varying distances in from the inlet and outlet ends) cracking in the invert was prevalent. Sometimes the cracking pattern extended an appreciable distance back into the pipe - from a few inches in small structures to several feet in large arches.

Deterioration of this type was dependent upon exposure to light, and particularly to direct sunlight. Ends of pipe which were shaded, such as the one shown in Fig. 3, were generally free from cracks in the pavement. On the other hand, end openings that were fully exposed invariably showed pronounced cracking of the pavement. This was so whether the culvert consisted of a circular pipe (Fig. 4 and 5) or an arch (Fig. 6). The extent of cracking was influenced by both the size of opening and the thickness of pavement. As one would expect, cracks extended farther

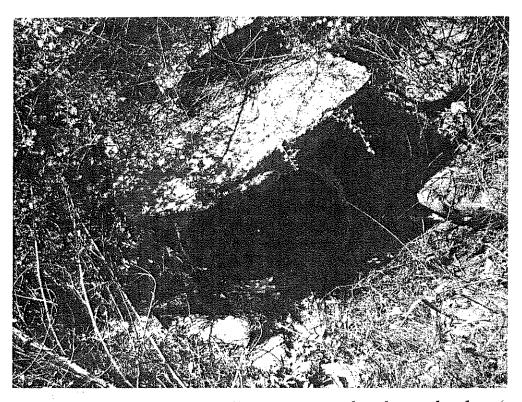
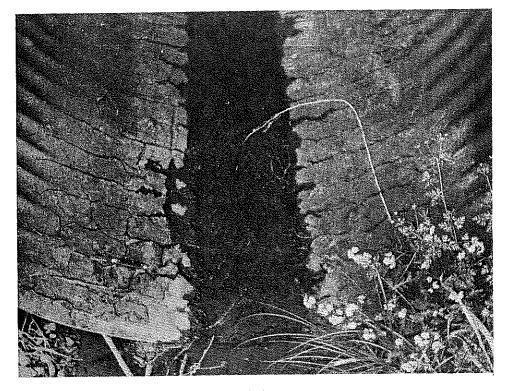
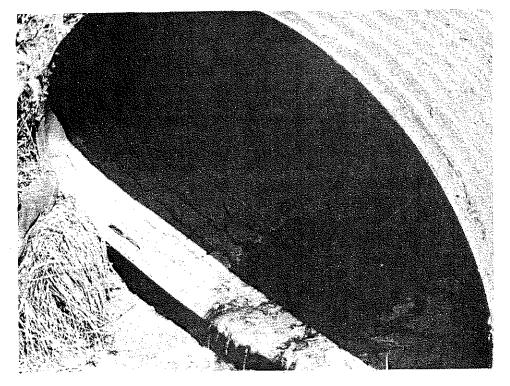


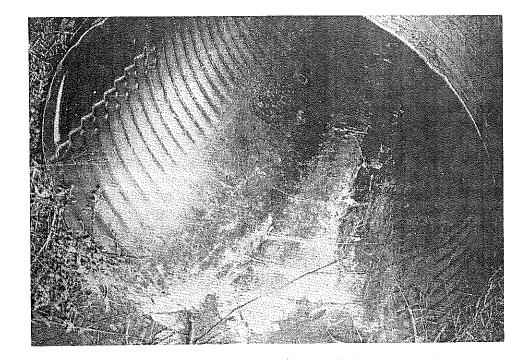
Fig. 3 - Inlet of a 24-in. diameter coated and paved culvert completely shaded by overhanging rock. No scaling was evident, and only minor cracking had occurred for a distance of 3 to 5 in. These conditions were typical of all coated and paved pipe which were shaded and placed on sufficient slopes to prevent ponding of water at the inlet and outlet.

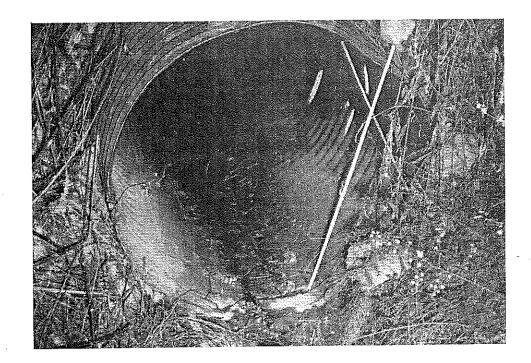




(Ъ)

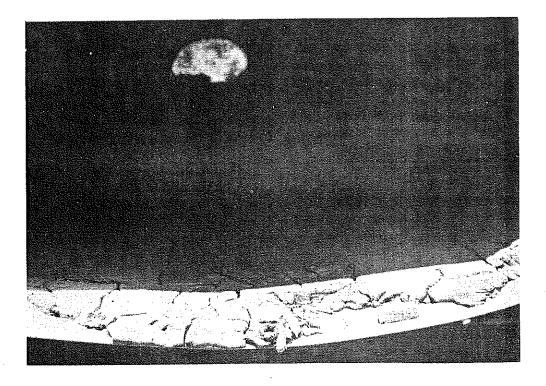
Fig. 4 - Outlet ends of (a) 42-in. diameter pipe and (b) 58x36-in. pipe arch, both installed in 1949. Note the cracking patterns in the paved inverts.

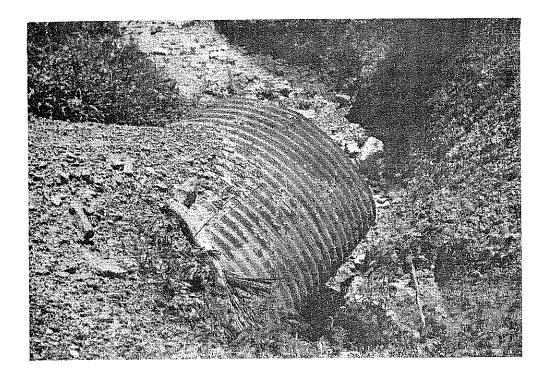




(b)

Fig. 5 - Inlet (a) and outlet (b) ends of a 42-in. diameter coated and paved pipe placed in 1952. Cracking was pronounced, but deterioration had not progressed to the extent indicated for the pipe in Fig. 4 which had a greater period of exposure.





(b)

Fig. 6 - Views of a 34x59-in. coated and paved pipe arch showing (a) cracking of the pavement at the outlet, and (b) scaling of the outside coating at the same end of the arch. Date of installation - 1950.

toward the interior of the culvert as the size increased, and the widths of individual cracks were greater in the pavements having the greater thicknesses.

The direction of cracking was both longitudinal and circumferential, and usually occurred at each corrugation in the end portion that was exposed. At the extreme edge of a large, thickly paved culvert the cracks were as great as 3/8-in. wide, and in some cases deep enough to expose the spelter. This condition receded to the point where cracks became mere lines and disappeared farther back into the pipe. Usually adhesion remained good, even near the outer edge and seldom could these polygons of weathered asphalt be peeled off by hand.

A different type of deterioration, which obviously resulted from ponding of water at an end of the pipe is shown in Figs. 7, 8, and 9. Here scaling is associated with the cracking that occurred through exposure to light. The scaling condition existed invariably where ponding had occurred, and apparently it was dependent upon alternate wetting and drying at a relatively slow rate.

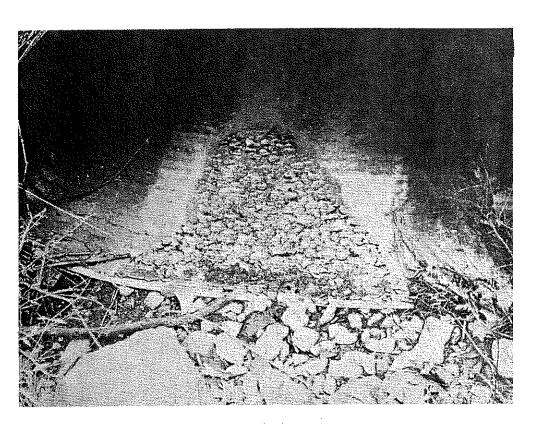
Generally scaling caused by ponded water was localized, since the possibilities for ponding are limited even in a culvert on 0 percent gradient. However, in a pipe having relatively low flow most of the time with slight fluctuations in the water surface, a favorable condition for wetting and drying exists throughout its entire length. Thus, scaling has occurred in several of the pipes at the general level of low flow or the so-called "trickle line". This is illustrated in Fig. 9.

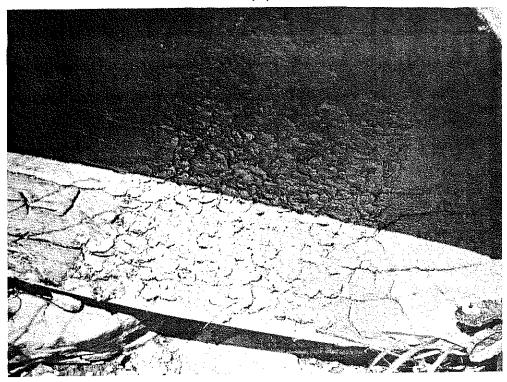
Usually scaling action had progressed for only a slight distance into the bituminous pavement, and the scales were well attached to the

124



Fig. 7 - Combined scaling and cracking at the outlet of a 44x26-in. pipe arch installed in 1949. In some way this end of the structure had been bent upward providing for intermittent ponding to a slight depth, and consequent wetting and drying.





(b)

Fig. 8 - Scaling at both the inlet (a) and outlet (b) of a 65x40in. pipe arch installed in 1949. Associated cracking was more extensive at the outlet than at the inlet, which is not subjected to direct sunlight.

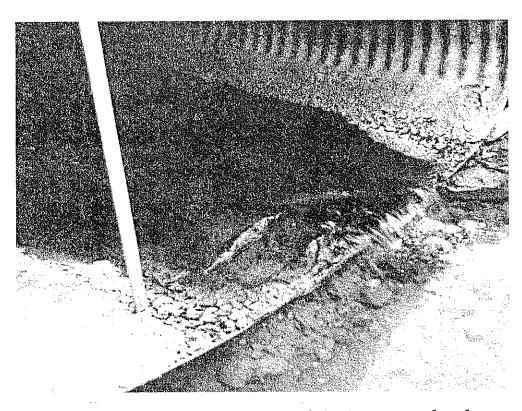


Fig. 9 - Scaling along the edges of the low water level or "trickle line" in the paved invert of a 72x44-in. pipe arch installed in 1949. This condition extended throughout the entire length of the culvert. underlying bituminous material. Still there were indications that the deterioration might be appreciably progressive with time, and that scaling does encourage failure of the underlying pavement. There were some locations where the dry scales had hardened enough to become brittle, and undoubtedly they could be broken off by the scouring action of silt and debris.

At many locations where silting had occurred to appreciable depth the usual symptoms of deterioration were not evident. Obviously the accumulated material has insulated the pavement and prevented exposure to both sunlight and wetting and drying.

Improper Placement of the Paved Invert

In about 30 percent of the culverts inspected, the paved section had not been laid so that it formed the culvert invert. Instead, the pavement was shifted to one side or the other, and sometimes even to the top of the structure. Often this was the apparent cause of coating failure, since there were no cases of failure in the coating when the pavement had been properly placed in the invert.

Abuses of this nature led to peeling and scaling of the coating with subsequent exposure of the spelter. As a rule, when the pavement was positioned incorrectly and there was reasonably continuous low flow, a portion of the bituminous coating was scaled and some of the coating had been completely removed throughout the entire length of the culvert at the trickle line. Damage to the coating was always confined to a strip approximately 4 inches wide in small culverts and as much as one foot wide in large sections. A typical example of misplaced pavement is shown in Fig. 10.

7 C T

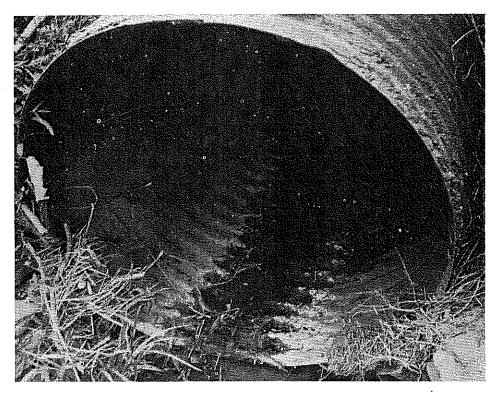


Fig. 10 - Coated and paved pipe placed with the invert shifted almost 90 degrees to the left. The knife (see arrow) marks the lower edge of the pavement. Water has flowed on the coating since installation of the pipe in 1949, and considerable scaling has occurred in the trickle line.

129

Damage to Coating and Pavement Caused by Fire

Although damage to bituminous coatings and pavements caused by the burning of drift has no bearing on the ordinary performance of these materials, some aspects of this type damages are worth recording since two such incidents were encountered during the inspections. In at least one of the two locations there was evidence that the drift was burned by someone other than highway maintenance crews, indicating that probably the drift was blocking drainage to the extent of its becoming a nuisance.

Some of the effects of burning drift are illustrated by Fig. 11 and 12. The structures were installed in 1949, and about two years later the drift was burned. Both ends of the archs are now covered with rust, and much of the protective coating is gone even from the interior of the pipe adjacent to the one in which the burning occurred. Where rusting was severe, even the spelter was no longer available to provide protections.

Plain Multi-Plate Pipe Arches

Inasmuch as they were so easily accessible, a number of uncoated, multi-plate pipe arches were included in the inspection. The condition of the spelter on these structures of uncoated metal was of fundamental concern.

In the majority of cases there was evidence of rusting which generally covered the entire invert portion. As a rule, the rust pattern was a "pin point" type. Occasionally rusting had progressed to a point where scaling of the spelter had spread throughout the invert. Because of the obvious vulnerability of the metal to corrosion by acids whenever they may be present, water at each of the sites inspected was checked for acidity. There was no indication of acid at any of the locations.

- 10

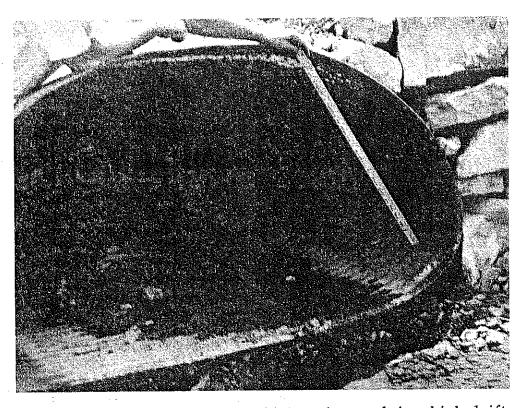


Fig. 11 - Outlet end of 72x44-in. pipe arch in which drift has been burned. Although it is not evident in the photograph, the entire bituminous coating has been destroyed and only fragments of the pavement remain in the invert. Extensive rusting was present throughout the pipe at the elevation indicated by the pointer, and on the inside crown of the structure. Date of installation - 1949.

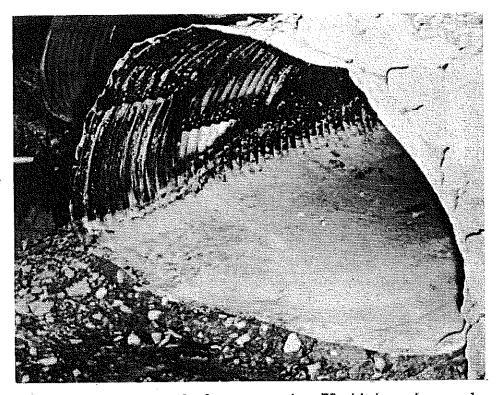


Fig. 12 - Outlet end of a companion 72x44-in. pipe arch placed alongside the arch shown in Fig. 11. The pavement was in good condition, but much of the coating on the left side had been removed by intense heat from fire in the adjacent structure. Even without acid as a factor, the general condition of inverts in these somewhat major structures gave the impression that protective coatings at least similar to those placed on smaller culverts should be developed for the low-flow portions of multi-plate arches.

Miscellaneous Observations of Field Practice

An appreciable percentage of the culverts inspected had ends that were scarred, bent, partially collapsed, or completely broken off. Undoubtedly most of this type damage was caused by graders changing direction while pulling a nearby ditch, or in a few instances it could have been caused by mowing machines. The ends of some pipe are so obscured by their surroundings it is difficult to locate them, especially where there is dense plant growth. Under such circumstances the marking of culverts by posts, or the clearing of vegetation or debris would help avoid damage.

A number of locations illustrated the importance of care in bedding and backfilling at the time of construction. Occasionally large pipe arches were severely deformed and distorted in shape although there was no evidence of collapse. On the other hand, some pipe with insufficient cover were collapsed, and in a few cases the outlet was higher than the inlet indicating poor bedding conditions during construction.

TEST INSTALLATION AT MORTONS GAP

In the course of inspections on Rural Secondary Projects in the western part of the state, the drainage pipe test installation at Mortons Gap was observed and general performance conditions evaluated. This test installation, developed as a part of acid water investigations*, was well over four years old and pipe at that location were at about the median age of projects involved in the coating condition survey.

Because of the general differences in objectives of the studies, and the fact that acidity of water at the Mortons Gap site is almost always very high, no direct comparison between the two sets of conditions was intended. However, a progress report on results from Mortons Gap has not been made in written form within the past two years, and the opportunity thus afforded to combine material of similar nature is convenient.

The test installation originally consisted of 16 sections of 24-in. pipe. Two sections of each of the different types were installed in the following order, beginning at either end (See Fig. 13).

- 1. Reinforced concrete
- 2. Vitrified clay
- 3. Corrugated metal, asbestos bonded bituminous coated and paved
- 4. Corrugated metal, half-coated and paved
- 5. Corrugated metal, plain galvanized
- 6. Corrugated metal, full double coating without paving
- Corrugated metal, full coated and paved according to Kentucky Special Specification No. 1-R
- 8. Corrugated metal, galvanized, asbestos bonded with bituminous seal coat

* See Report No. 2 on "A Survey of Acidity in Drainage Waters and the Condition of Highway Drainage Installations", issued by the Research Laboratory in December, 1952.

134

During the interim, as noted in the summaries of inspection that follow, some of the sections of pipe failed and were removed.

Inspections Previously Reported

Twelve inspections (or events), including the one at the time of the installation, have been reported previously. In essence the results were as follows:

> 1951 - April 25 - Date of installation. Specific resistance of water - 280 ohms.

> > May 22 - Date of first inspection. Specific resistance of water - 260 ohms. Spelter gone from plain galvanized metal pipe.

July 16- Water tested 235 ohms. Invert eaten out of corrugated metal, plain galvanized sections. Concrete pipes showed slight etching.

August 20 - Water tested 240 ohms.

October 18 - Routine inspection; no significant changes.

1952 - March 9 - Water tested 300 ohms.

April 15 - Heavy rain dislodged several sections of pipe and deposited silt in the channel.

April 29 - Installation restored. Galvanized metal sections not replaced. Water tested 290 ohms.

June 18 - Routine inspection; no significant changes.

August 4 - Water tested 268 ohms.

August 28 - Routine inspection; no changes noted.

October 5 - Water tested 265 ohms. Concrete pipe beginning to show visible evidence of progressive corrosion. Aggregate exposed in the invert, but no appreciable reduction in thickness of material observed.

4 4 x 3 4 m

At the inspection on October 5, 1952, the vitrified clay sections and variously coated metal sections remained virtually unaffected, except at those points on metal pipe where the protective coatings had been scarred during placement. The half-coated galvanized metal sections showed some scarring where the uncoated portion was in contact with fill material. This was interpreted as a mild form of corrosion.

Inspections Not Previously Reported

In the period since 1952, inspections have been less frequent than they were prior to that time. This was partially because a basis for estimating the need for attention had been established, and partially because all the inspections were combined with other work by Research Laboratory personnel in the general vicinity of Mortons Gap. Four inspections were made, with the essence of results being as follows:

> 1953 - July 7 - Routine inspection; water tested 267 ohms. No changes noted.

> > September 7 - Full double coating gone in invert of one (upstream) section of pipe No. 6, metal corroding.

1954 - July 22 - Full double coated section(No. 6 from upstream end) removed with invert eaten out.

> August 18 - Water tested 275 ohms. Pipe sections in the lower half of the installation were heavily silted. The pipe removed and reset. Downstream channel cleared to prevent silting if possible.

This being the latest inspection the following conditions observed in the upstream half of the installation are pertinent:



Fig. 13 - Test installation at Mortons Gap

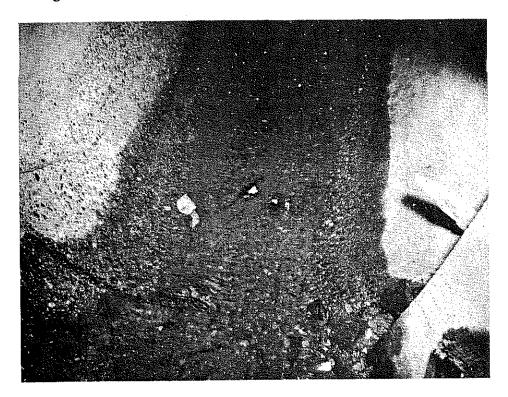


Fig. 14 - Interior of reinforced concrete pipe. Exposure of coarse aggregate has resulted from corrosion and removal of mortar by acid water. Date-August, 1954 Age - 4-1/3 yr.

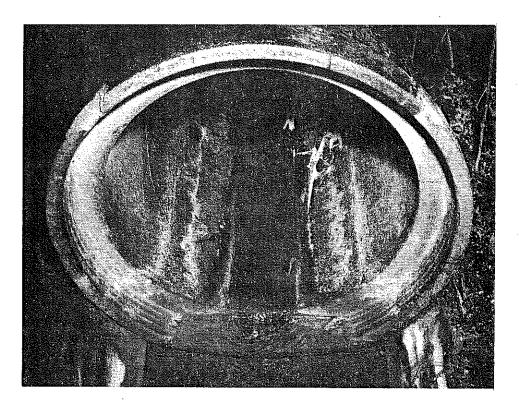


Fig. 15 - Vitrified clay pipe. Although staining and discoloration are evident at the edges of the flow line, structurally the pipe is in excellent condition. Date - August 1954; Age - 4-1/3 yr.

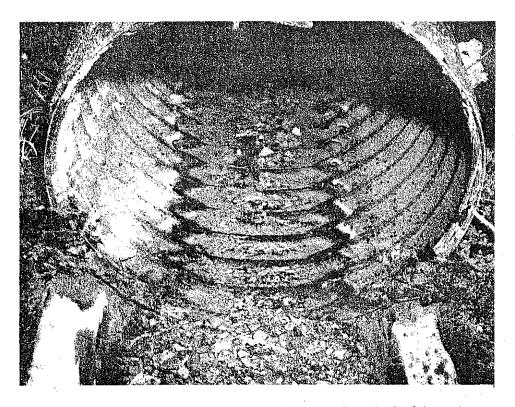


Fig. 16 - Corrugated metal, asbestos-bonded, bituminous coated and paved pipe. The flow line has been obscured by silt but the pavement in the invert has remained smooth and intact. There is no evidence of any deterioration. Date - August, 1954; Age 4-1/3 yr. 1. <u>Reinforced concrete</u> - In these two sections of pipe considerable corrosion has caused removal of mortar and exposure of the aggregate. (See Fig. 14) In this case, the aggregate used was Ohio River Gravel, and in view of other similar inspections, it is believed that corrosion would have progressed further had the coarse aggregate been limestone.

2. <u>Vitrified clay</u> - Both sections of pipe were in excellent condition with no visible deterioration (See Fig. 15).

3. <u>Corrugated metal</u>, asbestos bonded, bituminous coated and <u>paved</u> - Both sections were in excellent condition with no visible deterioration (See Fig. 16).

4. <u>Corrugated metal</u>, half-coated and paved - The pavement and coating in the remaining section was in excellent condition, and there was no evidence of corrosion in the upper portion or crown since that has not been exposed to the acid water flow (See Fig. 17). During periods of high flow the acidity is greatly reduced.

5. <u>Corrugated metal</u>, plain galvanized - Both sections removed and abandoned after two months of service.

6. Corrugated metal, full double coating without paving - Removed July 23, 1954, with invert eaten out (See Fig. 18).

7. Corrugated metal, full coated and paved according to Kentucky Special Specification No. 1-R. - As illustrated in Fig. 19, the coating was peeling at several points in this pipe, and there was evidence of serious rust at places where the coating was removed.

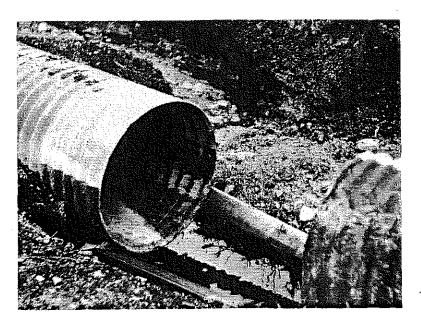


Fig. 17 - Corrugated metal, half-coated and paved pipe. Note that the pavement and coating are in excellent condition. Date -August, 1954; Age 4-1/3 yr.

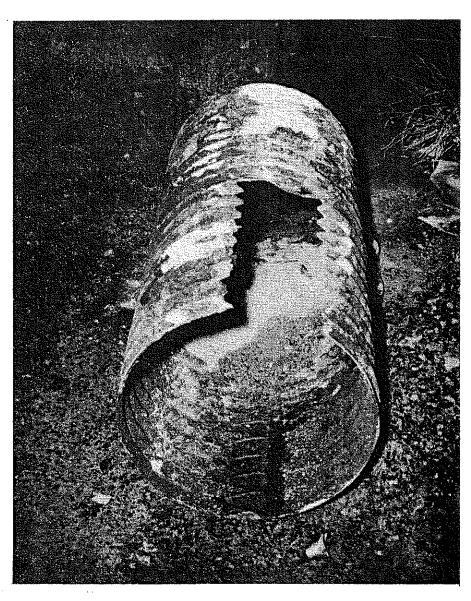


Fig. 18 - Upstream section of corrugated metal pipe, full double coated without pavement. Note that part of the invert has been eaten away by corrosion (pipe is rotated 180 degrees). Date - August 1954. Date of removal - July 1954; Age at failure - 4-1/4 yr.

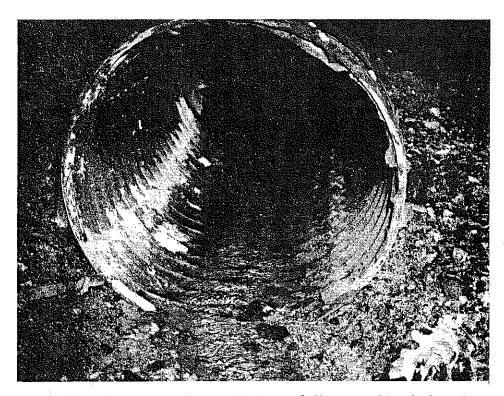


Fig. 19 - Corrugated metal pipe, full coated and paved according to Kentucky Special Specification No. 1-R. The coating has peeled at some points immediately above the pavement in the invert. Rusting has occurred to a minor extent in areas where the coating is missing. Date - August 1954; Age 4-1/3 yr. 8. <u>Corrugated metal</u>, galvanized, asbestos bonded with bitumi-<u>nous seal coat</u> - Although there was no evidence of deterioration whatsoever on the inside of this section, the seal coat outside appeared very dry and tending to flake off or peel.

SUMMARY AND CONCLUSIONS

The performance of coatings on the inside of culvert pipe in the Rural Secondary System was good in every case where the culvert had been properly installed. Coating failures that were observed, resulted from one or more of the following: (1) abuse in handling and transportation, (2) improper positioning of the paved invert during installation, and (3) intentional burning of drift material within or adjacent to the pipe.

Apparently the fairly generalized peeling of coating material on the inside of one section of pipe No. 7 (corrugated metal full coated and paved according to Kentucky Special Specification No. 1-R) at the Mortons Gap installation has no connection with any of the influences mentioned above, and no direct cause is evident at this time. The exposed metal is far enough above low flow to avoid water of high acidity, but there is considerable rusting at places thus exposed.

Coatings on the outside of metal pipe lose adhesion, even when the pipe is covered by earth fill. Inasmuch as the coatings merely become loose but are not removed from pipe within the fill, no particular damage results at least within the period represented by the Rural Secondary projects inspected. Whenever a coated pipe projects beyond the earth fill, cracking, scaling, and removal of the bituminous material occurs within a relatively short period of time particularly if the pipe is exposed to direct sunlight. Even here the loss of protection has no inherently serious consequences, provided the spelter remains undamaged.

145

- 17

Pavements in metal pipe are giving dependable protection to the metal surface, except at the ends where exposure to light is rigorous and at points where ponding or low flow has developed frequent wetting and drying conditions. Cracking results from the exposure to light and scaling results from wetting and drying. Scaling has hardly impaired the protective ability of any of the pavements within the 2-to 6-year period of service, and because of the fact that the material scales to very slight depths, probably the time required to reform and remove several successive layers is great.

On the other hand, cracking starts at a very early age and some of the cracks carry through to the metal within a few years at the most, particularly where the pipe is exposed to direct sunlight. Even when cracks were pronounced there was no visible deteioration of metal beneath. That applies to situations where there was essentially no acidity in the water. Obviously in cases where there is appreciable acidity the chances for serious corrosion of metal at the base of the cracked pavement are great.

A full evaluation of protective coatings on metal drainage pipe would involve more than superficial observations such as those contained in this survey, and probably additional observations at many more culverts would merely confirm the results that have been obtained. The sample in this case is considered representative of the conditions that prevail.

Even though the service conditions are realistic, the lack of uniformity in installation, exposure, and probably manufacture, limit the possibility for estimating what can be expected from this type protective coating, and how it can be improved.

- 18

Inherently asphalts are vulnerable to deterioration under exposure to light, heat, and in some respects moisture. Unfortunately there is no reliable measure of the way or the extent to which deterioration occurs under a given set of circumstances. However, as demonstrated by the performance of asphaltic pavements for roads, by the performance of asphaltic coatings containing asbestos or rock wool fibers (and other features of fabrication), by pipe subjected to considerable depths of silting, or by mineralized asphaltic coatings in roofing materials, there are possibilities for creating favorable insulating conditions under which asphaltic coatings can perform to maximum advantage so far as weathering is concerned.

The extent to which basic concepts can be applied to coatings and pavements for metal pipe is, of course, within the province of manufacturers. Improved treatment for the ends of pipe seems especially needed, and no doubt that is a problem of which the industry is aware. From the standpoint of the Department, better service from drainage structures in the corrugated metal categories would be achieved if:

- 1. More care was used in positioning culverts with paved inverts at the time of construction;
- 2. Pipe were set slightly below grade so that a limited amount of silting (perhaps as much as 6 inches) would occur in the course of subsequent stream action;
- 3. The ends of culverts were plainly marked and guarded against damage from maintenance equipment and passing vehicles; and
- 4. Uncoated metal arches were given a protective coating perhaps a pavement in the invert at the time of installation.

- 19

It was noted during the inspections that corrosion in the inverts and at the base was extensive on most of the metal arches observed. In view of the size of arch culverts and the investment they represent, it appears inconsistent to be unduly concerned with coatings and pavements on several minor conduits when on the same road a single structure having no protection whatsoever is equal to all the minor conduits as a group. Probably the life of several arches now in service could be extended if their inverts were suitably paved and the lower portions of the sides suitably coated.

- 20

. .

. . .

.

APPENDIX

.

INDEX TO CULVERT LOCATIONS (Accompanying Table 1)

		•
		Rural Secondary
	County	Project No.
Inspection No.	County	
	.	82-203-2
1-7	Meade	14-193-6
8-14	Breckinridge	47-453-1
15-18	Breckinridge	47-719-2
	Hardin	43-555-1
19-26	Grayson	
27-35	Larue	62-341-1
36-43	Anderson	3-231-2
44-50	Anderson	3-211-2
51-54	Bullitt	15-351-1
55-64	Duilitt	115-189-2
65-69	Washington	115-269-1
70-76	Washington	49-312-1
77-82	Harrison	19-491-1
83-89	Campbell	12-286-1
90-98	Bracken	101-121-1
90-90 99-105	Robertson	78-362-1
	Marion	
106-110	Casey	23-261-1
111-119	Garrard	40-246-1
120-124	McCreary	74-213-1
125-132	Russell	104-218-1
133-137		104-238-1
138-143	Russell	104-238-1
144-147	Russell	27-206-1
148-152	Clinton	1-330-1
153-156	Adair	1-310-1
157-161	Adair	1-430-1
162-165	Adair	109-348-1
166-169	Taylor	109-288-1
	Taylor	109-200-1
170 - 174	Rockcastle	102-337-2
175-183	Whitley	118 - 740 - 1
184-191	Bell	7-224-3
192-199	Clay	26-145-3
200-207	Metcalfe	85-244-1
208-215		5-452-1
216-222	Barren	114-528-1
223-229	Warren	107-205-1
230-231	Simpson	110-426-1
232-238	Todd	24-665-1
239-246	Christian	101-74-1
247-252	Trigg	54-640-1
253-260	Hopkins	89-543-1
200-200	Muhlenberg	07-04J-1 1/ 05/ 1
261-267	Butler	16-256-1
268-272	Wolfe	119-223-1
273-279	Breathitt	13-407-1
280-287	Breathitt	13-427-1
288-292		60-298-1
293-297	Knott	

TABLE 1 - SUMMARY OF DATA FROM ALL INSPECTIONS

r	- <u>-</u>					—r						1-0			• • • •								PECTI	
				:					r	YPE	:	M	IAIN	п.				N (яL		~ UU	1 1.5.1	
	1	NSTAI	LLATION		FLC	j wc	ERŌ	5'N		AINA			CON	D.	co	AT:	ING			P/	AVE	MEN	r	
	\vdash					\mathbf{T}^{\dagger}	TT	T	TT	TF	TT		11	1	<u> </u>	Π	11	╈	П		T		Γ	
										e e											2			REMARKS
	ved									Book					u len		e e	e llen			Crac	k s	ke	
No.	and Paved	talled	(iii)		8	ţ			ded La	wam					оос Цхс Ц	Fall	hec		Coo	000	nal 11	Crac	Cracks	
ction	d an	EL	Inch	ø	uent	nitta 18	ers		Vare Urbo	led S	ge Wat	tlent	5		1018	1018		a De Bion	810n	uo i e	itudi	, Pof	8	
Inspection	Coated	(car	Size (Inches)	Grade	req	uter	Bould	Grav	Pasture Hilly Wooded	V ood	Mine	e xce	Very Good Good	Line d	Adhe	Adhe	Coat	Adhe	Adhe	Adhe		widt	Depth	
-	11	<u></u>				11		11	111					Ť			5	1			00	Width of Cracks	i i	
12	×	1949 1949	24 24 18	M S F		0							0		0		0				00		Metal Metal	Perement ecoded in flow line Pavement can be stripped to base metal. Silted beyond inspection
345	x	1949 1949 1949	18 18	F M		•	00		0				0	٥	00			0				0	0	Concrete polished in invert - erosion evidence on sill
6		1949 1949	24 24	M M		0						0 0												Concrete excellent condition Concrete excellent condition
89	x x	1949	18 42	F M B		0	0							000	0		ן ווי	ן מ	္စ၀		00	1/4 1/4 3/8 1/8	Metal Metal Metal	Can peel pavement Scaling in invert at inlet - can be peeled Evidence of crosion - checked crack pattern
10 11 12	×		2-36 48 2-42	F M F				16						ŏ	0			1	0	1 1	00	1/в 1/4	Metal	Silting bally
13	x x x	1949	18 24	F F											00			0	0		00	3/8	1/4	Could not peal pavement - No abrasive wear No svidence of deterioration
15 16	x x	1949	24 18	F F		8	0					Π		D	0			0			0	1/32 1/64	1/32 1/64	Evidence of erosion - 50% of flowing gone
17 18	x x		24 66x38	F		0	0	0	200				0	"	0 0				00		00	1/2	Metal Metal	Outlet and inlet 10-20% erosion No erosion at inlet - outlet end severely cracked erosion evident in flow line.
19 20	x	••••	42 42	F F	1	0	┼┾		5	c	11	$\uparrow \uparrow$	1	\dagger		Ħ	\dagger	6	Þ		00	3/8	Metal	Excellent condition
21	X		18 18	F F F										°	0	6	0	ľ	P	1	00		Metal	Can peel - flaking in invert
23	x		18 18	F								$\left \right $		0		0			·					Silted 1/2 full (cannot inspect pavement). Silted 1/2 full (cannot inspect pavement). Percent almost complete pavement.
25	x		18 18	F F		0						$\ $			00			٥			0 0 0 0			Pavement almost completely gone - can peel - pavement and coating appears brittle. Water standing in pipe (slight erosion - 10-20% missing
26 27 28	X	1951	18 30	F F								Ħ	0		00		П	0	o		٥		1/32	Very good condition Abrasion possible - no wear evident
29 30	xx		24 18	F F			0	0	0					0	0		1	0			0	1/32	1/32	Outside coating excellent Small evidence of payment year.
31	×		18	м		•	•	°	0					٥	P			٥						Wear or loss of parement slight - 10% at flow line. Culvert on concrete sill. Sill eroded, (3/6"), more than pavement.
32	x		18 18	г F									0	۰,	0				0					Abrasive materials settling out Pool at outlet and some silt in barrel.
32 33 34 35 36	X X X		18 18 24	F F	9									0	0			0						Silted up No evident wear from abrasion
	x	1949	24	F	0			Т	0	00		Π	0			P	°				00	. 4	Metal	Can peel sheets hand size from pavement. Seems to be chemical disintegration.
37 38	X X		66 x 38 24	ㅋㅋ		•			00	000				0	P				٥	0	00	1/4	Metal Metal	No evident wear from abresion Pavement scaling - can be peoled with fingers. Concrete above shows no abrasion or acid.
39 40			123x77 66x38	F F	٩ -		•	0			Ί			0									.	Possible abrasion on metal (entire invert) Silted half full with sand and gravel.
41	x		66738	F	0		•	٥	0							°	0		0	[• •	3/8	Metal	Coating - inside good - exterior coming off. No erosion wear on pavement (pooled).
42 43	x		24	F		0			0	Щ	Ц.	Ц		0	0				0 0			3712	Metal	Side coating acting as invert. Scaling in flow. Side coating acting as invert. Scaling in flow. Outside coating flaking off with fingers. 40% of
44		1949	30 18	M M			0								0 0 0 0			.	00		이 이 이 이		Metal	pavement eroded at flow line (chemical).
45	x		18	F				ŀ	00						0		0			0	00	-, -	Metal	ing excellent. Pavement - first 4' feet peeling to base metal. Outsid
47			24	м					00					0	00				0	0	• •	3/16		coating 5-6% missing cracking. Pavement flaking off on ends (4).
48	X		24	F		"			0.0			H			00	0	0					1. 3/16	Metal Metal	Pavement - can peel large sections out. Favement dry - shrinkage cracks in weathering. Flaking badly in wet and drying area.
49 50 51	X	1949	72-44 Arch 36	F F F	0 0		。┤┤			0	<u> </u>			+		Ш		0	6				1/4	100' above coating arch. Chemical erosion and trickle line. Outside coating
		-/-/		-								$\left \right $, -		scaling - 25% gone. Pavement scaling - 50% of last 6'. Ends gone. Evidence of full flow.
52 53	×		58x36 36	F						ľ										0				No wear - some abrasion force possible. Pavement not in invert - (side). Spelter gone in invert the entire length. Algae action.
<u>54</u> 55	3	1950	58x36 30	F	0	-	。┼┼	-	0	0	0	H	0	+	0	-	╇					1/2 1/16	Metal 1/16	invert the entire length. Aigas action. Outside coating checked. Trickle line disintegration - 15% on ends only. Algas
56),		18	F				0	0						0				•		00	1/4 1/2		action. Coating on outside checked.
57	×		59 x 34	F		י	• • •	000	°	00	°	$\left \right $	0	^	°				°°		• •	1/2	MetaJ	Trickle line disintegration in entire length. Algae condition.
58 59	×		77x57 18	न्म न				00	0			$\left \right $	0		0				0		• •	1/32	1/32	Silted 2' deep, oversized. First 1' on ends only (cracks). Outlet shaded - no end cracks.
60 61 62	×		24 159 x 96 Arch	r. F	0		•	00	000				,	1	ľ			ľ	ľ					Pooled in invert - oversized - wasted material. Spelter breakdown due to abrasion.
63 64	x		48" 36	F F	•			00				\prod			° °				°.		0 0 0 0	1/4 1/4	Meta Netal	25% erosion length trickle line. Full flow. <u>Pavement 50% gone in trickle line.</u> Wet and dry flakin Trickle line erosion 10-20%. Checked pattern 4' both
65	ľ	1949	42	4	0 0		Ī	0	00	0			0					ľ			。]。[3/8 1/2		ends. Outside coating dry. Peeling off, 20%.
66	ř		42 24	न न		,	۱	0		ľ				•		ŀ					0	1/2		Trickle line erosion 10% . Circumference cracks length of pipe, outside coating peeling off -10% . Outside coating peeling off. Coating in trickle gone
	<u>Î</u>														$\ $									or easily raked off. Spelter gone and pin point rust. Paved invert on sids.
68	×		42	F			•	0	P	0			• •	ŀ	° °		• • •	ì	l l°		6 0	1/4	Metal	Outside coating peeling off. Coating in trickle gone or easily raked off. Spelter gone and pint point rust
		10/2																						Paved invert on side. Pin point rust length of trickle line. Generatic silt must on boilts only
69 70	x	1949 1949	Arch 44x25	F	•			+	0	++0	6	\uparrow	50	-	80	h	0	0	•	††	• •	1/2	Hstal	Galvanic silt rust on boits only. Scaling last 2' of ends (pavement). Outside coating only (stripped).
71 72	x		2-30 44x25	F F						00		ŀ		0	00	l I			00	0	00	1/32	1/32	Fooling in barrel (silting), Chunks of pavement lying in silted culvert.
73	x X		36 50x32	F F		- 1 I I	1	00		0	11		0		1 6	•	000	ן א	•		00	1/2	Metal	Coating acting as invert, scaling to metal. Minor wet and dry scaling.
75	x		1.4 x 25	F										00	ľ	1								Silted 1/2 full (impossible to inspect).
															Ц_			1					1	

TABLE	1	-	(CONT'D.)
-------	---	---	-----------

8 7 0									TAI	SLE	1 - (CON	סיד	.)					· · ·
NETALATION PLOT NLOSS DATING CONT. FATELONT 6 0		·······									CON	DITI	ON	OF	NLE	T & C	DUTL	ET	· · · · · · · · · · · · · · · · · · ·
Normalization Normalinstation Normalization Normalizatio		INSTAL	LATION		FLOW	EROSIN					COA	TING	.		PAV	EME	NT		
State State <th< td=""><td></td><td></td><td></td><td> </td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>~ • • •</td><td></td><td></td><td></td><td></td></th<>															~ • • •				
State State <th< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>\prod</td><td></td><td></td><td>TŤ</td><td>TT</td><td></td><td>Τ</td><td></td><td></td><td></td></th<>										\prod			TŤ	TT		Τ			
$\begin{array}{c c c c c c c c c c c c c c c c c c c $															5				REMARKS
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	ved.						puo/				Ile		ped		raci				
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	No.	fled	Ê		H		L.an led	and a			Sod	Poor Poor	trip	3000		rach		rack	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	tion	1 10 1	ache		ittar	50 L	e ted Vood	d Sw ard Vate	food		55		BeS		adin F				
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	pect		- <u>-</u>	ade	ntin er m fing	ulde avel	ltive stur IV	rmy vage vage		L G	hesi	hesi atin	PIN	hesi	heai	d th			
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		X		ų	Sala	C SHOW	O G H >	N.S.	ώ>ů	ц Ц	PY	2 P P P	ပို	PAA	ΓP Γ	א כ	1	Å	
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $						0 0 0													
1 2 2 3 0		1952	24 18			0 0			°						0		4 Me	tal	Scaling in flow line. Wet and dry coating in pave-
1 1 1 1 0 0 0 1/2 Care is made to be a solution. 1 1 1 0 <				S		0 0			0		00		c	0		5			2-5% erosion in trickle line.
and bis			18		0	0 0	00	0	00	0	o]						32		Cracks inches from end. High cut shade culverts.
6 1 3 7 0	83		123x77		8		00		- 10		0			1					Used as cattle crossing,
B T T O	85 x		24	F	0	0 0	00		00		8	0	1	0		י וי	32		Checked 1' from end inside and out. (Light)
8 9 90 1/20 <td></td> <td></td> <td></td> <td></td> <td>0</td> <td>000</td> <td>000</td> <td></td> <td>00</td> <td>00</td> <td>이</td> <td>00</td> <td></td> <td>2</td> <td>000</td> <td>) 1/</td> <td>4 Me</td> <td>tel</td> <td>Checked coating outside. Sheltered inside and out. Scaling in invert. Outside coating completely miss-</td>					0	000	000		00	00	이	00		2	000) 1/	4 Me	tel	Checked coating outside. Sheltered inside and out. Scaling in invert. Outside coating completely miss-
9 90 </td <td></td> <td></td> <td></td> <td>_</td> <td></td> <td>tion.</td>				_															tion.
90 100											•) °		°	0 0	יי (°	32		Scaling is light. Outside coating off where exposed soil. Fool reflects radiation. Breakdown in ends.
90 x 136 r 000 00		-											Ļ		Щ		<u> </u>		High abrasive force, 50 pound rocks in culvert. Two truck loads of rock inside pipe.
92 24 7 0 <th0< th=""> 0 0 0</th0<>		1949		-								°	٥		°	ין ¹ /	32	ſ	Invert on side, coating in invert off, peel to metal. Coating off adjacent to soil.
90 24 F 0																			Coating and pavement in good condition. Loose scaly rust and scarred sections on end, scarred by machiner
97 24 7 6 0	!										11					–			Scaling and stacking on ends in pavement. Outside coating gone unler ground line.
99 10 0									0						 °	י ןי	16 Me	otal	Invert in top, coating gone in flow line, pin point rust.
9 10 7 10 7 0 <th0< th=""> <th0< th=""> <th0< th=""></th0<></th0<></th0<>	1										11								pavement scaling on ends. Pavement on side.
97 43 7 6 9											0	0	0	ľ	00	2			Costing gone in trickle line only. Pavement cracks on ends only, last foot.
98 36 7 0 <th0< th=""> 0 0 <th0< th=""></th0<></th0<>																	ł		with gravel.
98 30 P 0 <th0< th=""></th0<>	97 I		48	F	l °	0	0			°	P					.			Boulders up to forty pound size, pavement on side at
90 1400 00 7 0 0 0 0 0 0 0 10 7 10 7 0 0 0 0 0 0 0 10 7 10 10 10 10 10 10 10 10 0 0 0 0 0 0 10 10 10 10 10 10 10 10 10 10 10 0 0 0 0 0 10 <th10< th=""> <th10< th=""> 10</th10<></th10<>	98 x		36	r	0	000	0			0	0 0			0					7:00 Pavement not in invert, coating holding up well.
10: 98056 P 0 </td <td>99 x</td> <td>1949</td> <td>30</td> <td>F</td> <td></td> <td></td> <td>00</td> <td></td> <td>0</td> <td><u>ə</u></td> <td></td> <td></td> <td>-</td> <td>0</td> <td>0.0</td> <td>17</td> <td>32</td> <td></td> <td>Foor alignment, no inspection.</td>	99 x	1949	30	F			00		0	<u>ə</u>			-	0	0.0	17	32		Foor alignment, no inspection.
101 x 98066 F x 0 </td <td>100 x</td> <td></td> <td>05,40</td> <td>r</td> <td>Ĭ</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>ľ</td> <td>ľ</td> <td>•</td> <td></td> <td></td> <td>1 1/.</td> <td>4 Me</td> <td>ital</td> <td>missing on the end 3. Outside coating cracked</td>	100 x		05,40	r	Ĭ						ľ	ľ	•			1 1/.	4 Me	ital	missing on the end 3. Outside coating cracked
112 93-64 112 <th< td=""><td>101</td><td></td><td>50-24</td><td>ъ.</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>section.</td></th<>	101		50-24	ъ.															section.
100 x 35477 7 0 </td <td></td> <td></td> <td></td> <td>, i</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>0</td> <td>°</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>tion at flow line.</td>				, i								0	°						tion at flow line.
100 x 18 F 0 <th0< th=""> <th0< th=""></th0<></th0<>			95x64	T														/20	
100 x 30 F 0 0 0 0 0 1/8 Mathematic and good, west and radiation cracks in parameti, lat 3? 106 1940 93x64 F 0				- 1												1	5e 17	2	and outlet submerged.
106 1349 93404 9 107 x 30 0																			scarred by mower,
1.107 1.207 <td< td=""><td>. </td><td>76/6</td><td></td><td>7 17</td><td></td><td></td><td></td><td>a</td><td></td><td></td><td></td><td></td><td>\downarrow</td><td></td><td></td><td>1/1</td><td>B We</td><td></td><td>in pavement, last 2'</td></td<>	.	76/6		7 17				a					\downarrow			1/1	B We		in pavement, last 2'
1008 107×777 F 0 0 0 0 0 0 0 0 0 1/8 1/8 1/8 7 0																	, v.		Trickle flow under arch.
109 x 18 F 0 0 0 0 0 0 0 0 1/8 <th1 8<="" th=""> <th1 8<="" th=""> <th1 8<="" t<="" td=""><td>108</td><td></td><td></td><td>F</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>Ĭ</td><td></td><td>1 1/</td><td>Б</td><td>- LEI</td><td>in flow line. Outside coating gone.</td></th1></th1></th1>	108			F										Ĭ		1 1/	Б	- LEI	in flow line. Outside coating gone.
111 x 14/2 F 0 0 0 0 0 0 0 1 F there shaded <			18	F	0		00		0				8		0				Excellent condition - end shaded - full flow.
112 44x72 P 0 </td <td></td> <td>1929</td> <td></td> <td>-</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>0</td> <td>0</td> <td></td> <td></td> <td>0</td> <td></td> <td>-</td> <td></td> <td></td> <td>where shaded.</td>		1929		-						0	0			0		-			where shaded.
113 x 44x72 F 0 </td <td>112</td> <td></td> <td></td> <td>F</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>]</td> <td></td> <td>1 10</td> <td>· [_/</td> <td>٠ </td> <td>line pavement is good.</td>	112			F]		1 10	· [_/	٠	line pavement is good.
113 x 44x72 F 0 0 0 0 0 1/8				-															Oxidation along pattern of fill on outside. Outside
114 x 4.4x72 F 0<	113 x		44 x 72	F	00		00	0		0				0	0	1/1	1 1.	R I	coated and burnt out
115 x 18 F 0 0 0 0 0 0 0 0 0 1/6 1/6 100 100 100 1/6 100 100 1/6 100 100 100 1/6 100 110 110 111 110 111 110 111 110 111 110 111 110 111 110 111 110 111 110 111 110 </td <td>114 🛪</td> <td></td> <td>ļ</td> <td>P</td> <td></td> <td> _/·</td> <td></td> <td></td> <td>end burnt, inside and outside costing ran of</td>	114 🛪		ļ	P												_/·			end burnt, inside and outside costing ran of
116 159296 F 0<												0	٥			$ \tilde{1}/\epsilon$	Me:		Inlet shaded - excellent condition, Outlet end
127 x 1940 34x59 F 0	116		159396	F	0														and deteriorated in flow line last 3 '.
117 X 1949 34x59 F 0			,																plain arches in this area all rusted. Possibly 5
119 x 34x59 F 0 0 0 0 0 0 0 0 110 118; revenent accellent accellent muler the met = like met. 120 x 1950 52x30 F 0		1949			D O			0		。					00	1//	L Met	tel	Typical weathering on inlet and outlet ends,
119 X 14/2 X 14/2 X 14/2 X 14/2 X 15/2 X 14/2 X 15/2 X <th16 2="" th="" x<=""> <th16 2="" th="" x<=""> <th16 2="" th="" x<=""> 16</th16></th16></th16>													<u>ا</u>						blistering. Pavement excellent under the mud - like
121 x 59x34 F 0 </td <td>119 x 120 x</td> <td>1950</td> <td></td> <td></td> <td></td> <td>- - - c</td> <td></td> <td>╺┨╍┨╍┨╸┨</td> <td>1.0</td> <td>。┼┼</td> <td>-</td> <td></td> <td></td> <td>0</td> <td>000</td> <td>1/2</td> <td></td> <td></td> <td>Typical end condition, radiation weathering.</td>	119 x 120 x	1950				- - - c		╺┨╍┨╍┨╸┨	1.0	。┼┼	-			0	000	1/2			Typical end condition, radiation weathering.
122 x 59x34 F 0 </td <td>121 x</td> <td>-</td> <td></td> <td>F</td> <td></td> <td></td> <td></td> <td>0</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>11/</td> <td>Mat</td> <td>1</td> <td>scaling in invert, ends exposed to radiation.</td>	121 x	-		F				0								11/	Mat	1	scaling in invert, ends exposed to radiation.
125 x 1949 18 F 0 0 0 0 0 1/32	122 x 123 x		59x34	F F			000	o	0		0		0	0	000		Met	tal	Scaling in last 31 in invert - both ends.
122 x 124 174 105 7 000 000 000 00 1/32	124 x			F		c				0			0		00	1/2	Mat		In invert flow line - radiation exposure drift and
127 x 24 p 0	126 🗖		18	F i	000	3 8				0	0			ò o	00	1/	2 1/2	32	Weathering first 6" from end.
129 142x90 F 0<	128 x		24 142	F F		0 0	00	0	0	0		0	0			_		~	Typical weathered ends and erosion and trickle line.
10 1 10 1 10 1 10 1 10 1 10 1 10 1 10 1 10 1	129		142790	F	°		polo			0									Invert advanced tubercular rust 21 up on sides of
131 x 18 M 0 <td< td=""><td>130 x</td><td></td><td>18</td><td>F</td><td></td><td></td><td> • </td><td></td><td>0</td><td></td><td>0</td><td>°</td><td></td><td>•</td><td></td><td></td><td></td><td></td><td>Inlets shaded in excellent condition. Outlet nave-</td></td<>	130 x		18	F			•		0		0	°		•					Inlets shaded in excellent condition. Outlet nave-
32 x 18 N 0<	131 x		18	м	0		0				0	00		。					on end of cuivert.
Coating good - pavement weathered light - 6" from ends.	132 x	l	18	м	000				0	。	0								Outlet exposed typical weathering pattern.
																			ends.
		l			┶┶┙┷┝	444				11	ТŢ	ЦЦ	-		11	L			
									-		i t	39	8						

na shararara 💡 🦿

anada se s

:

, 										+						וידא					
								T	YPE		MAI	1	CON	DIT		OF	INI	ET	& OU	TLET	
	I	INSTA	LLATION		FLOW	ER	osin		INAG		CON		COA	TIN	G		Р	AVE	MEN	r	
										T		7"		Π	П			Π		T	D BY A B WG
Inspection No.	Coated and Paved	r Installed	Size (Inches)	de	Continuous Frequent Intermittant	178 1 1 A P T E	le vel	ture y Wooded Mooded	oded Swarnp myard	age e Water	y Good	6.5	esion Excellent esion Good	esion Foor Her Charled	ld Be Stripped	esion Excellent esion Good	esion Fair esion Poor	gitudinal Cracks cumfer ial Cracks	th of Cracks	th of Cracks	REMARKS
Insp	Coa	Үсаг	Size	Grade	Con Fre Inte	Sand	Sha Gra	Pas	W00 Far	Min	Coo Goo	н Рос	up Adh	Adh	Cou	49Y Adh	4PA	Cition	Width	Depth	
133 134 135 136 137	x x x	1949	48 18 42 93x64 42	9 P P T	0 0 0 0 0	0 0	000		0		000000000000000000000000000000000000000		0 0 0 0 0		00	00		00	3/8	ibtal	Inlet coating as invert peeling - Pavement at 9:00. Outlet exposed cracking and flaking last 2' in pave- ment. Outside coating checking badly. In excellent condition - in shaded and protected by fill and trees from radiation. In shaded from radiation. Wet and dry flaking and paveward in trickle line, Pavement at 7:30. Invert of arch completely runted - tubercular. Spelter completely gone, Acid taste - shows no acid. Abrasion possible. Large spots of rust around bolts insides. Pavement at 5:00.
138 139		1950	77x56 18	F F	0						0		0			0			1/8	Metel	Spelter gons and invert - tubercular rust - No acid - red clay rock area. Abrasive force light.
139 140 141	x		18 60	F	0	0	00	0			00		00		00	00			1/6	Metal	Invert and in excellent condition, sheded. Outlet end pavement radiation bracks, scaling and flaking in invert trickle-line. Excellent condition - both ends shaded. No add - badly weathered cracks in both ends of pavement. Some mag in top - approximately 1'. No
142 143	x		59x34 93x64 93x64	F	0	o	o	00	o			0	00								scaling, but evidence of erosion in flow line. Out- side costing gone under fill. Wet and dry flaking on ends of parcment. Typical where sun radiation load is present. Nust in flow line - left arch bally ieformed at out- let end, due to improper placing - no acid. 1-2' sag due to rock fill.
144 145 146		1950	77x57 77x57 170x104 48	न	0	0 0	o	000	0	0		0	a			0	0	00	1/2	Metal	Right barrel silted 2' deep. Left barrel invert rusted - no soid by test. Some rust - partally protected by gravel bar in structure approximately 6° deep. Pavement badly checked first 4' and last 4'. Typical weathering on outlet scaling and etc. Flaking and poor adhesion at outlet. Outside coating dry and scaly.
147	x	1950	24 18		0	00	0	0			0		0 0	$\downarrow \downarrow$	╁╢	P					Excellent condition - inlet and outlet protected by deep fill and out, 1/2 full of silt - no pavement inspection.
149 150 151	X X X	1990	18 18 54	F F T T	0000	000	00	000			0										1/2 1011 of sitt - no payment inspection. Excellent condition - inlet and outlet shaded. Excellent condition - inlet and outlet shaded. No erecks - no peeling - excellent condition - ends in shade. Some ovidence of deterioration in trickle line - no acid outside coaching good. Excellent in every way. As good as day installed.
153 154 155 156	x x	1949	24 24 16 18	F F F F	0 0 0	00	0 0 0 0 0 0 0						0 0 0	c	0	0 0 0] [0 0 0 0 0 0	3/8 1/8 1/8	Metal Metal Metal	Sheded by trees and fill. Outside coating good - typical weathering at water- line on ends by radiation. Pavement at 3:00. Both ends exposed - typical cracking of pavement and scaling in flow line. Cover insufficient. In excellent condition - vines covered both ends. shielded from weather and high enough to avoid water from standing in pipe. Coating missing where pavement invort is not in bottom. Outlet pavement at 8:00. Typical weathering
157 158 159 160 161		1949	24 52x30 18 59x34 54	F F F F	0 0 0 0		c	00	0		0					0 0 0		> 0 > 0	1/8 1/2	Metal	To spelter - spelter inll. Sag in culvert 1). Water starding in center, Last 2' paving cracked and scaling. At end foot coating good except where paving slightly coated. Pavement at 6-30 - paving in top of inlet. Outside coating good except where mistreated in handling. Coating good - Pavement silted. Impossible to inspect. Typical flaking at outlet - inlet good - shielded by shaie and vegetation. Typical weathering - both ends scaling; crack ing first and last 3'. Typical cracking first and last three feet. Sag in
162 163 164 165 166	x x x x	1949	18 52x30 36 72x44 77x57	F F F		0 0	000		0		0		0	00	0	0 0 0			1/8 3/8 1/2	Metal Metal Metal	<pre>top = 11. Outlet = silted = not inspect pavement outside. Coating peeling outside of inlet - pavement eroded at trickle line - coating good. Typical pattern, but silght outlet due to light deposit of sand. Coating good inside and outside. Flaking in pavement (ends) Outside coating good - aide indicates full flow and possible overflow. Typical in ends - cracked badly - scaling in trickle line. Outlet coating good. Deep hole in dutlet. Silted - outlet end. Heavy abrasion action -</pre>
167 168 169	x x x		18 24 24	F F NO	o	0	0 0 0 0		0		00	0	0			000	Ħ	0	1/32 1/32	· .	calcarious limestone and shale. Large gravel deposits. Slight cracks at outlet cracks - no peeling. Inlet partially silted. Outlet slited - inlet very slight cracking. Excellent condition - no cracking. Continues flow from spring house and ends are protected by shade.
170	x	1950	59x34 24	Р М.	00 0	0	0	0 0	0		000		0		C	0		00	1/32 1/32	·	hilst excellent condition - shaled by heavy trees. Outlet partly shaded. Cracked and scaling last 6°. Parament Flaking in the ends. Cracking first foot on ends. Exposed to weather, and wet and dry conditions.
172 173 174	x x		107x72 18 94x46	F M F	0 0 0	0	00	0 0 0	0		00	E L	0			0				-	Beavy rust in flow line. Considerable gravel in rock bottom channel, Channel fairly steep. Excellent conditions - emis shaded. No wet or dry action. Outlet emis too low. Silted 1/2 full. Coating and Determine excellent on inlt with out the work of
175	x	1950	18	ĸ	0	╫		ő	++	P			0	+		6-	$\left \right $				pavement excellent on inlet end. Outside coating very good. Pavement completely gone and trickle line - not through scaling and cracking but through decimal
																					through scaling and cracking, but through chemical action or chem, disintegration. Excellent rough stone headwall protection.
												1	ףיייין פּ }	ţ							

TABLE 1 - (CONT'D.)

1	1		. <u></u>			<u> </u>	1						co	ND	ITIC	NC	OF	INI	LE'	тьо	UTLET	
		INSTA	LLATION		FLOW	EROS	И		YPE INAGE	2	MAD COM		со	AT	ING			P	νA	(EME)	nТ	
	-			1			+					Π	łΤ	Π	T		Π	1	Π			-
	ed							Wooded					lent			ed			ZCKB	racks		REMARKS
No.	and Paved	Installed	(a)				uravel Cultivated Land	ded Wa	wamp	Ŀ			t Excellent Good	Fair	hecked	Stripp	Cood	Poor	51 191	Cracks	Crack	
Inspection No		5	Size (Inches)	ę	tinuou quent rmitte	le te	vel	ture y Woo ntaind	o di a	6			ceion ceion	c a l on	ting C	d Be		C 210D	gitudin	ž v	Ч	
	Coated	Year	Size	Grade	Con Trife	San Bou Sha	╉		Far Sew	Min	Ver Goo	Far Poo	4bA AdbA	ЧРV	AGA Coa	100 0		Adh	Ton	Width	Depth	
	x x		. 18 18	м м	0	0	0	0 0	٥	C) 0		0				00			0 1/32 0 1/8	1/32 Metal	Last foot of pavement hardening with slight cracking. Inlet end in excellent condition. Trapical cracking in outlet exposed 21. Chemical
178	x		24	м	o			0 0			00		00		·lo	0	0			1/8	Metal	erosion in trickle line.
	x		24	м	0			00		•	0 0		0		0		0		0	1/8	Metel	Outside coating cracked in fair condition.
	x x		123x77 24	F M	00 0	0	,[]	0					00				0		00	1/32	1/32	Rust, no acid from test - Abrasion possible. Rust in the invert. Slight cracking at outlet, samistons erosion, sag in
182	x		34#59	м	o	0 C	,	0			0			00		0		11	1	1/8	Metal	the middle. Outside coating excellent. Inside pavement at inlet shaded, weathered outlet end. Cracked heavily, pavement very soft with loss adhesion.
																						Outside coating has no adhesion, flakes off easily. It appears that coating was placed over oil. High run off, scour possible; no evidence of rust.
	x	1950	<u>66738</u> 66x38	F	0	<u> c</u>	0		┽┼┦	+	00	┥	0	1	╁┼	╀	0	╢	0 0	> 1/8	1/8	12' soon possible; ho evidence of rust. 12' of sag in center; slight weathering at inlet end, oracking alight at outlet - some erosion in flow line.
185 186	x		107x72 107x72 24	F	00		0	0												,		No acid by pH test.
187 188	×		36 72x44	F	00			00				0	°	ø	00	>						Collapsed - slited half full. Outside coating almost gone. Laid on side. One arch slited half full other arch rusted over entire
189	×		72x44 18	F	o			0					0	0	0		0		0 0	1/8	Metal	Invert. No acid indicated by test.
	x x		66 х38 24	F F	00						0		00			0	0 0		0 0	1/4	Metal	no acid - eroded trickle line. Scaling in pavement on ends, deep fill, sheltered still Shaded excellent condition
193 194	X X X	1950	18 18 18	S S	000	0 0		000			000	,	8	T	a		0 0 0	۱ĸ	0	1/8 1/8 1/8	Metal Metal Metal	End cracks on pavement. Outside coating badly scarred. Pavement end cracks, exposed.
196	X X X		24 36 18	S S	00	o 0		0			o		000			0	0		ļ			Half collasped at end, silted up. Excellent condition, no gracks and no wear. Inlet collasped - scarred - rock blocking end. Coating
198 199	x		18 48	s s	0	o 0	c	, e			00				00	0	00		0	1/4	Metal	good. Coating in pavement excellent - shaded. Pavements ends cracking. Outlet velocity very high -
200	x		24	- 5	0	> 0		0	┥┦┤		00		0	1.	00	$\left \cdot \right $	0		5 8	1/8	Metal	has been send bagged at outlet to prevent erosion. Outside coating ecouring dff. Typical weathering cracks in inlet pavement - outside
201	×		36	м	0			o			00		0		0		٩		•			coating dull and peeling on exposed ends. Pavement at 7 o'clock - typical conditions where coating acts as pavement. Coating peeling in trickle
202			36		0	0	。				c	0			0		0		0			line - elsewhere costing is excellent. Outside good. Typical weathering on outlet pavement exposed to sun. Pavement at 3 o'clock. Severe weathering. Pavement
203 :	, ,		48		0			0			0		0		0		0	a	,			peeling - coating peeling in trickle line - spelter good, Outside coating peeling. Severe weathering on emis for 2'. Coating weathered
204 1			42	м	000			0			0		0		0		•	4	c			where exposed to sun, dull and dry. Typical weathering. Pavement at 11 o'clock - coating gone in flow line. (Tuberculin in flow line).
205 1 206 1	×		36 36	F	0	0	0		0		0		Î		0		٩					Inlet on excellent condition. Outlet end - costing gone or never coated, spelter gone with rust. Pavement at 2 o'clock. Costing asting as paving - out.
207	×		66x33	м	0			0	0		00		0				。	0				side costing.fair- some oracking. Outlet end not costed. Tuberculin rust, advanced stage. Typical weathering - cracking and scaling - outside
208 3	-	1950	59x34	F	•	0	-	0 0			00	╟	ö	$\left - \right $	0		-	ö	0	3/8	Metal	coating good - slight rust on hip where coating is scarred. Some sag in center. Wetting and drying flaking in
209	ĸ		24	F	•			0			0		0		`		0					trickle line, at inlet and outlet. Outside coating - dull and cracking. No metal showing. Farement at 5 o'clock typical weathering condition at
210 2			18 18	M F	0 0 0	0		0		,	000	c	0			0						outlet. Inlet paving and coating good. Typical - coating good - some slight checking and saaling a few feet on ends in invert.
212 7			18	F	0		0	0			00		0									Partly collapsed at inlet. Coating good - silt over pavement at outlet - pavement good at inlet. Overflaws roadway - cultort half full of silt. Pare-
213 7	×		72 x 44	м	00		°	0			0		0			d					1/8	ment good - coating good. Few cracks first 2' - overall pavement condition excellent - no chacks or peeling - outside coating
214 215 x	2		18 18	M F	0		0				00		0			4		٥	0	1/4	2/4	excellent. Typical weathering on ends. Coating good outside. Some weathering and paving at inlet end. Faving good
216 2		1950	30 18	F F	00		0	0			٩	Ť	0	Ħ	T	2				1//	Max -	in shaded outlet end. Pavement typical - invert slightly off. sink hole topography. Typical weathering.
218 7			30	и	0 0		0				0 0		0							1/4	Metal Metal	Outside coating. Adhesion poor - spelter good - typical weathering.condition. Inlet and outlet exposed.
			-																	24 10	200 681	Typical weathering conditions. Outlet high and exposed has 5' free fall at outlet. Dug large hole. One joint of concrete pipe at inlet end. No weathering on metal.
219 x 220 x 221 x	¢ l		24 18 18	F F M	0 0 0 0	0	0	0	•		000		000									Pavement not in invert. Water standing in pipe - some silt. Silted up - outlet end burned out. Silted badly at let
			-				ľ					Ĭ										811teC up ~ 1/3.
			ĺ																			
							Ц															

	1	INSTA			ł								1		- 1	CONT			nn	TATE	.FT	& OU	TI 57	
	1	INSTA			1					-	330777		1.		L –		DIT	ION	UF	<u>п</u> ят			T THE L	
			LLATION		FI	LOW	ER	OS'	N		YP. AIN	e Age		IAIN CONI		COA	TIN	a		Р.	۸VJ	SMEN'	г	
on No.	and Paved	talted	ches).		ous f	ttant			Cultivated Land	ooded	121	rd	nt.	000		n Excellent n Good n Fair	n Poor	trip	on Excellent on Good	n Poor	iinal Cracks er'ial Cracks	Gracks	Cracks	REMARKS
Inspection No	Coated.	Year Ins	Size (Inches)	Grade	Continuou	Intermi	Sand	Shale	Cultivat	Hilly W	Wooded	Sewage Mine W	Excelle	Good Good	Роог	Adhesion 7 Adhesion C	Adhesio	Could B	Adhesio	Adhesio	Circum	Width of	Depth of	
222	×		18	s		0			0			•		0		٥			0		ľ			No cracks - ends fairly shielded. Pavement slightly off invert.
223 224 225 226	× × ×	1950	18 18 18 18	к M S	U	00	0	I E						000		0 0 0 0 0			0 0 0			1/4 1/8	Metal Metal	Paving good - shielded by silt and gravel. Full flow. Typical weathering at outlet - cracks. Cracking through in very good shielded condition - erosion in pavement - outlet end and no chance of wetting and drying in outlet end. Inlet collapsed. Outside coating good. Good - no weathering - shielded - Outside coating good. Coating in pavement good - in excellent shape.
228	x x x	-	36 36 42	P F		000	0		00					00		000			00					Outside conting good, Typical weathering, excessive scaling and fulking in trickle line, Extreme flaking in outlet. Costing perfect - all exposed - spolter good. Shaded - excellent condition both ends due to shade. Typical weathering, extremes flaking condition - no evidence of wetting and drying. Small crack s inlicates material may be too dry, last 3' to 4'.
230 231	x x	1949	18 18	г ř		0	0		00	0						0			0	1 1		1/8 1/8	Metal Metal	Outlet end free and 3' of fall. Some boulders in harrels. Invert at 5 o'block. Typical weathering on ends. Yery little drainage on this road. Paving st outlet at 5 o'clock. Typical weathering
232 233	x	1949	42x28 42x28 66x38	м		0			00 000	11				0 0		00			0			1/4	Metal	outlet end shaded - in excellent shape. No rust. Outside coating fairly good. Typical cracks on pave- ment on ends. No scaling - no wet and dry action.
235	x x		18 18	м		0	o		200 20	0				0 0 0	11	00		c	0					No ponding. Shielded ends - No cracks in pavement. Excellent condition. Excellent condition - shielded by vines and vegetat- ion.
	x x x		18 18 18	M M M		0 0						>		0	0	0 0			0					Good condition. Shielded at inlet - typical weather- ing at outlet - exposed end. No cracks at shielded inlet. Protected inlet and outlet - size good. Full flow due to silted inlet - Inlet end torn and
239	x	1949	24	F	┢┼╾	o			9		+-+-			o		0		┼┼			00	1/4	Metal	partially collapsed. Inlet pavement fair. Weathered inlet - cracking and peeling at inlet. Pavement at 7 o'clock at outlet. Outside coating
241	×	1949	18 30x17		0 0	0			000					0 0					0					good. No rust on exposed spelter, Costing good. Typical weathering at inlet. Outside conting good. Silted in perement - and impossible to inspect pave- ment - coating good.
243 244	x x x		59x34 30x17 30x17	F F F		0			0					0		000			000	1.10	olo		1/32 Metal	Outside costing good - inside very good. Silted - impossible to inspect pavement. Typical weathering. Small cracks on end of pavement. Free out fall - outlet pavement cracked - outside costing good.
246	x x	1949	66x38 66x38 39x34 39x34 24	F F M		0 0 00			00 00 x 0					0		0			0				Metal Metal	no wet or dry condition.
248 249 250	x	-147	93x64 77x57 30x17 30	FF	.0	0 0	0	0	000		00			0 0 0 0	o	0			0					silted No evidence of rust. Cut off on skew, Rust in invert. No acid. Wet and dry flaking scaling at inlet and outlet. Culvert low and pooled at outlet. Coating good. Typical weathering on ends. Coating good inside and
252 253		1949	77x57 18	F F		0			00		$\left \right $	\square			0		+	┞╢	+	-	50	1/2	Metal	out with slight evidence of erosion. Helf full of silt and md - looks good elsewhere. Outlet and inlet ends partially collapsed. Severe
254	x		18	F		0			0					00		0	1		0					cracking of pavement, Feeling in large squares. Outside costing scarred off. Severe cracking in pavement; outlet which is exposed. Indit sheltered and therefore, nd cracking so severely. Outlet end damaged by grader. Full flow.
255 256 257	x		77x57 18 24	y M F		00			0	00				00		0			00		• •	1/2	Metal	No rust - some slit and outlet. Culvert laid too low. Severe cracking in pavement. Pavement in culverts on this section of road are thicker than usual. Cracking very wide.
258		1949	18	F		00			00					0	0	0		d						Standing full of water. Coating good. Payment impossible to inspect. Extreme cracking - payment peeling in large chunks.
	x		24 18	F			00	0	0	0	0			а 0		0		0						Pavement peeling off. Costing adhesion some to be bad. Pudding in culvert deteriorating costing. Wetting and drying affect. Culvert partially collapsed at inlat. Fipe cut by grader. Mas insufficient cover. Fave-
						0					Ĭ													mont in pipe deeply cracked. Extremely bad - as has been typical of this road. Wide cracks penetrates to metal. Pavement seems to be thicker causing more severe cracking. Paving meens very dry. Outside coating mostly come.
261 262	x	1949	77x57 18	F		0 0	00		00				0	0	• •				0	Π				Scour action. Complete rust in trickle line. Outside spelter good. No acid. Typical weathering at outlet. Gracking and scaling in trickle line. Costing excellent. Inlet end meeds
264	x x		18 18	S F		00	0	0	D	0	0			0	•	0			0				-	cleaning. End projects too far into the cut. Perfect condition. Shielded by cut and vegetation. Outside coating good. Paving good. Coating fair - protected by clay silt and invert. Outside coating gone.
265	X		18	M		00			00		0			00		0			°			1/8	Metal	Coating good. Typical weathering. Flaking outside

1911

100038-

a de la construction de la constru

ł

· [T		<u></u>						<u> </u>			-1							OF		ET	٤ 0	UTLE	
		INSTA	LLATION		FLC	w	ERO	s'N		TYI AIN	PE IAGI	2	MA CC		. c	r A C	'ING	;		P	AVE	CME	T	
.on No.	and Paved	Installed	chea)						D Cultivated Land Pasture Hilly Wooded	chous Wooded Swamp	<u> </u>	ater	ut Dod		in Excellent	DI GODE	un Poor Checked	te Stripped	m Excellent m Good	Adhesion Poor	dinal Gracks ferial Gracks	f Cracks	f Gracks	REMARKS
Inspection No	Coated	Year In	Size (Inches)	· · · · · ·	Continuo Frequent	FILLER	Boulder	Gravel	Pasture HINV W	Wobded	Earnya Sewage	Mine W	Very Go	Fair	Poor Adhesid	Adhesto	Adhesio	Could B	Adhesio	Adhealo	Circum	Width of	Depth af	
266 267	x		30 18	F		0			00					0	o	0			0	2	• •	3/8	Metal	Wetting and drying. flaking. Typical eracking pattern. Outside coating good. culvert set low on grade. Puddling at outlet allowing wetting and dry- ing for weathering. Parement at 3 o'clock at outlet. Severe weathering of pavement. Costing excellent. Inlet good condition abidided. Outlet high and exposed.
268 269 270	X X X	1949	24 72x44 58x36	F		,							٥	0		0			0	5	-			shielded. Outlet high and exposed. Typical weathering. Slight flaking in trickle line. Pavement flaking in large chunks. Typical weathering conditions. Some wetting and dry- ing; flaking in flow line. Coating good. Outlet eracking sovers. Large sheets of pavement missing. Spelter dull. Pinpoint rust where exposed. Typical weathering of pavement of both order Met
271 272	x x		19 36	M F		>			00 00 00	,	0.			0	0				00					Typical weathering of payement at both ends. Wet and dry flaking. Small amount of algae growth. Pin- point rust where exposed. Excellent condition. Ends are shielded and no wet or dry action. Typical weathering - cracks not as severe as usual. Some chemical action - not acid. Coating good.
273 274 275	x x x	1949 1949 1949	24 24 18	F M F	0	>			0 0 0 0 0				(H	_ [[0 0 0		c	0		00		Netal	<u>Guivert is 1/2 corrugated metal and 1/2 concrete.</u> Cracking first 6". Otherwise shaded. In deep fill. Pavement slightly out of invert. Excellent condition, Inlet shaded - coating and pavement best condition. Outlet silted 1/2 full and is high. Last 6' exposed. Outlet trickle line cracked to metal.
276 277 278 279 280	x x x x x x	1949 1949 1949 <u>1949</u> 1949	18 30 59x34 52x30 77x57	M F M M			>						1	2000		0000			0		00	3/8	Metal	Silt in bottom seems to be protecting pavement. Slightly weathered. Coating not in invert. Coating is checking and peel- ing in flow line. Favement good. Typical weathering and scaling in invert. Excellent condition. No cracks or peeling.
281 282 283 283 284	x x x	1949 1949 1949 1949 1949	65x44 48 24 77x57	F M T	00 0 0	11			000					0	000	0		ſ						Very good condition. Excellent condition. No creacks or peeling. Spelter excellent - exception - one piece is missing and a spot is rusted. Invert at 9 of clock. Costing and pavement excellent. Advanced stage of tuberculin rust on entire flow line. No mine water. 30% gone.
285 286 287 288 289	***	1949 1949 <u>1949</u> 1949 1949	30 74x57 74x57 <u>48</u> 48 42	F F M M		20			000						0000	2					00	1/8		Excellent condition. Excellent condition at inlet. Outlet typical cracks. Good condition. Excellent condition. Excellent condition.
290 291 292 293	x x	1949 1949 1949	18 18 48 142x90 142x90 48	м	00 00				0 0 0 0 0 0				ľ	0	0				0					Excellent condition. No cracking, checking or scaling. Typical checking at outlet, where exposed to afternoon sun. Inlet excellent. One arch completely rusted in invert. The other is slited 1/3 full. Recommend paying this out, Perfect condition. No cracks or checks, Best seen
	x x x x x	1949 1949	24 24 18 24	M F S	0000				0000						00000			000			00			so far. In good condition. Slight evidence of checking. Cracks present in protruding outlet. Good shape - no cracks. Good shape - no cracks. Outside excellent.
																								4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
and the second sec																								
re por sta . A d'auto da a																		L.						
		-																						
																		-						
					Ш		Ц.	ĻĻ		Ц				\square	Щ	Ш	Щ		Ш				l <u></u>	

TABLE 1 - (CONT'D.)

000000

· ~....