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ADDRESS REPLY TO

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H-2-21

MEMO TO: A. O. Neiser, State Highway Engineer

'Chairman, Research Committee

SUBJECT: Research Report (Final), "Determination

of Traffic Parameters for the Prediction,

Projection, and Computation of EWL's"

KYHPR-64-21, HPR-1(4), Part II

The design of pavements is, in reality, two problems: one pertains to the capabilities of the pavement structure to withstand a certain amount of traffic, and the other pertains to forecasting traffic. Although a structural design may be adequate for a stated summation of traffic, if the traffic forecast is in error, "design life" and "actual life" of pavements will differ. If "traffic age" exceeds the "chronological age", traffic is accumulating at a higher rate than was predicted. For instance, if a pavement designed for a 20-year forecast of traffic actually accumulates that much in 10 years, the forecast was obviously in error. If, in the same instance, the pavement developed concomitant distress, its structural design would not be suspect.

A method of estimating or predicting EWL's for the design of bituminous pavements was recommended to the Department in 1949. It was revised in 1954. A 1958 statistical evaluation of predicted versus actual accumulations of traffic, on approximately 57 projects designed and constructed between 1948 and 1957, indicated that 68 percent of those roads did or would accumulate their 10-year quota of traffic between 6.8 and 16.8 years.

The prediction of equivalent wheel loads (or equivalent axleloads) is much more complicated than predicting gross traffic volume - although, any error in predicting gross traffic compounds the error in equivalent loadings. For instance, the composition of traffic and the spectral distribution of truck types and axle weights are extremely elusive and variable factors - even in retrospection. Presumably, this inability to predict with accuracy exists because we do not have sufficient historical knowledge of the past - that is to say: traffic counts and classification data have not provided true and complete representation of trends in traffic, on either a constitutive or time basis.

The study report transmitted herewith presents an inquiring analysis of available traffic data. From the standpoint of resolving a predictive criterion, subjective parameters were introduced and tested for statistical significance. Even so, residual or unaccountable variances persist. In still another sense, the inherent or natural variability remains high and so does the error of estimate. This does not mean that all predictions will be hopelessly in error: it does mean that in some instances the actual accumulation may be somewhere between half and twice the predicted value but in the majority of cases will conform much closer.

The method or criterion we are proposing for adoption (Appendix F of the report) is quite different from the one now in use. The new method provides factors which offer the best estimate of Kentucky EWL's and(or) AASHO, 18-kip, equivalent axleloads per 1000 vehicles; these may be projected over the design period. Inasmuch as the AASHO basic axle is gaining preminence throughout the country and inasmuch as certain planning statistics are already required by the Bureau of Public Roads to be reported in terms of 18-kip, equivalent loadings, we believe that our pavement design criterion should be converted eventually to that basis. In the meantime both Kentucky EWL's and AASHO axles should be entered on design records. We suggest that each axle of a tandem pair continue to be considered as an individual axle.

This study was a long time "maturing". Much of the effort was consumed in compiling and verifiying the data. The data systems are now amenable to updating again on future occasions.

The study has not been extended to include urban situations as was originally planned - and is concluded with this submission.

Respectfully sabmitted,

Jas. H. Havens

Director of Research

JHH:em

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#### Attachments

#### Research Report

# DETERMINATION OF TRAFFIC PARAMETERS FOR THE PREDICTION, PROJECTION, AND COMPUTATION OF EWL'S

FINAL REPORT
KYHPR-64-21: HPR-1(4)

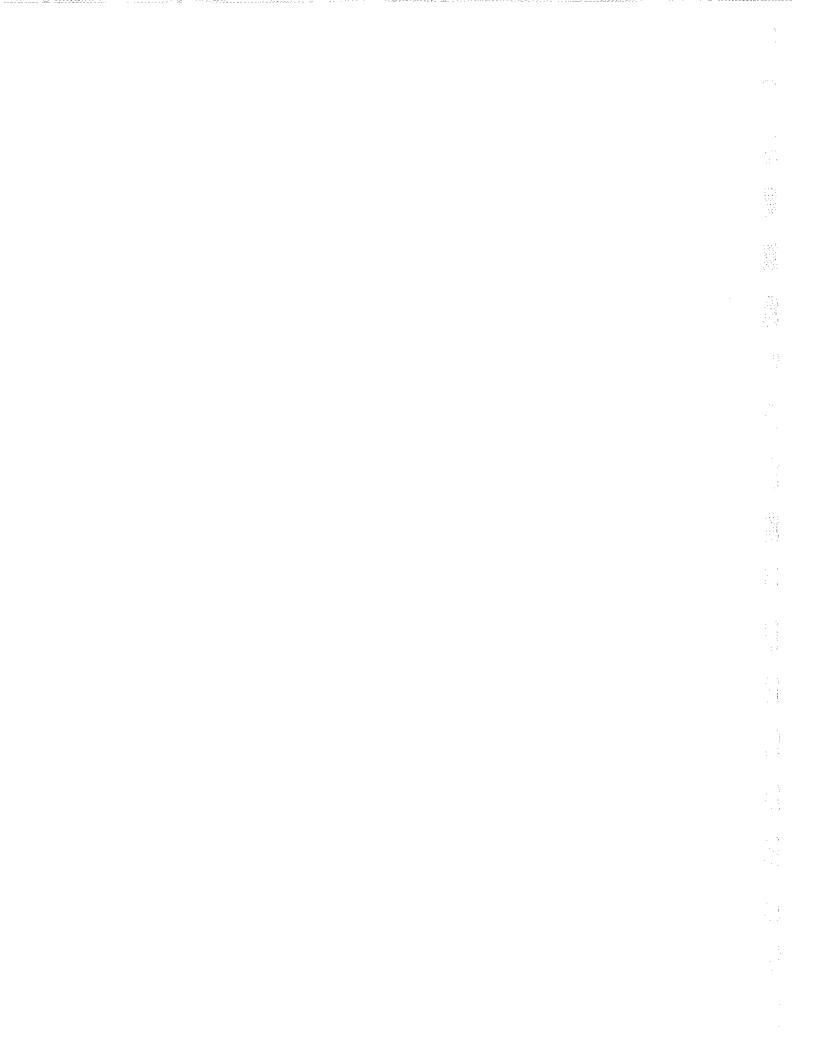
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in cooperation with the
U.S. Department of Transportation
Federal Highway Administration
Bureau of Public Roads

The opinions, findings, and conclusions in this report are not necessarily those of the Department of Highways or the Bureau of Public Roads.



# TABLE OF CONTENTS

Pa	ag:
LIST OF TABLES	V
LIST OF FIGURES	vi
INTRODUCTION	1
PROCEDURES FOR PREDICTING EWL'S	5
COMPARISON OF KENTUCKY AND AASHO METHODS CURRENT KENTUCKY PROCEDURE CALIFORNIA PROCEDURE RECENT INVESTIGATIONS IN TEXAS PURDUE UNIVERSITY CONCLUDING REMARKS	
PROPOSED METHODOLOGY	15
LOCAL CONDITIONS	18
DATA ACQUISITION AND ASSIMILATION	23
APPLICABLE SURVEYS DATA SOURCES DATA FORMAT EXTENT OF AVAILABLE DATA	
SUMMARY OF AVAILABLE DATA	34
SUMMARY OF PARAMETERS USED IN PRESENT METHOD SUMMARY OF PARAMETERS USED IN PROPOSED METHOD EFFECTS OF LOCAL CONDITIONS	
PREDICTION OF TRAFFIC PARAMETERS	39
METHODS PREDICTING VEHICLE-TYPE PERCENTAGES PREDICTING UNIT EWL'S EXTENSIONS OF METHODOLOGY	

ACCURACY VERIFICATION	58
SUMMARY	65
RECOMMENDATIONS	66
REFERENCES	68
APPENDIX A - HISTORICAL SUMMARY - AVERAGE PERCENT TRUCKS AND AVERAGE NUMBER OF AXLES PER TRUCK	71
APPENDIX B - HISTORICAL SUMMARY - AVERAGE AXLELOAD DISTRIBUTION	75
APPENDIX C - HISTORICAL SUMMARY - AVERAGE EWL'S FOR 1,000 VEHICLES AND FOR 1,000 TRUCKS	81
APPENDIX D - AVERAGE VEHICLE-TYPE PERCENTAGES AS A FUNCTION OF LOCAL CONDITIONS	87
APPENDIX E - AVERAGE UNIT EWL'S AS A FUNCTION OF LOCAL CONDITIONS	90
APPENDIX F - WORK SHEETS FOR PREDICTING DESIGN EWL'S	97
APPENDIX G - EXAMPLE PROBLEM	106

# LIST OF TABLES

Table		Page
1	ORIGINAL LOAD EQUIVALENCY FACTORS	2
2	CURRENT LOAD EQUIVALENCY FACTORS	7
3	KENTUCKY GROWTH ADJUSTMENT FACTORS FOR EWL ESTIMATES	9
4	KENTUCKY DESIGN TRAFFIC CATEGORIES	10
5	CALIFORNIA EWL CONSTANTS FOR DUAL-TIRED COMMERICAL VEHICLES	12
6	EQUIVALENCY COEFFICIENTS BY ROUTE CLASS	14
7	CODIFICATION OF LOCAL CONDITIONS	19
8	CODIFICATION OF VARIABLES OTHER THAN LOCAL CONDITIONS	27
9	WEIGHT-CATEGORY CODES	29
10	EFFECT OF WEIGHTING ON MEAN KENTUCKY UNIT EWL'S	36
11	WEIGHTING BY GROUPS	36
12	ILLUSTRATION OF DUMMY VARIABLES	42
13	ILLUSTRATION OF VALUES OF DUMMY VARIABLES	42
14	METHODS FOR CORRELATION OF TRAFFIC PARAMETERS WITH LOCAL CONDITIONS	44
15	ACCURACY OF VEHICLE-TYPE PERCENTAGE ESTIMATES	49
16	UNIT EWL'S OF BUSES	53
17	ACCURACY OF UNIT EWL ESTIMATES	54
18	ACCURACY OF ESTIMATES OF EWL'S PER 1,000 VEHICLES	58

# LIST OF FIGURES

Figure		Page
1	Form for Estimating 20-Year EWL's, 2000-2999 vpd	11
2	Four Geographical Areas	22
3	Example of Station-Location Descriptions	25
4	Example of Index by Route	26
5	Example of Index by County	26
6	Example of Basic Classification Data	<b>3</b> 0
7	Example of Modified Classification Data	31
8	Example of Basic Weight Data	32
9	Example of Modified Weight Data	33
10	Influence of Year on Additive Correction Factors	47
11	Relationship Between Additive Correction Factor and Year (Unit EWL Estimates for C-4A Trucks)	51
12	Relationship Between Additive Correction Factor and Maximum Allowable Gross Weight (Unit EWL Estimates for C-4A Trucks)	51
13	Example Effect of Maximum Allowable Gross-Weight on AASHO EAL's per 1,000 Vehicles	56
14	Comparison of Actual and Predicted Kentucky EWL's per Day for 225 Individual Counts	59
15	Variability in Kentucky Daily EWL's at Station 8	60
16	Percent Error in Kentucky Cumulative Daily EWL's as a Function of Time	62
, 17	Actual Versus Predicted 20-Year Design EWL's for All Stations	63
18	Flexible Pavement Thickness Based on Actual	64

#### INTRODUCTION

One of the first published methods for the structural design of highway pavements was called the Massachusetts Rule and was presented in the eighth annual report of the Massachusetts Highway Commission in 1901 (1). The essence of this procedure was a rather intuitive assumption concerning the distribution of vertical pressures beneath a loaded area. For design purposes, this required the selection of a design load which, since failure was assumed to be catastrophic and not cumulative, could be taken as the largest load that could reasonably be anticipated during the design life of the pavement. The prediction of such a design load was in itself a rather formidable task.

However, as early as the late 1930's, pavement designers began to appreciate that pavements could become distressed not only catastrophically as a result of the single application of a very large load but also cumulatively as a result of the repetitive application of loads of lesser magnitudes. In 1938, Bradbury (2) hypothesized that portland cement concrete pavements could fail as a result of the conventional mechanisms of fatigue. The primary type of failure in flexible pavements was identified by Porter in 1942 (3) as resulting from progressive plastic deformation of the foundation as large repetitions of load were accumulated. Soon thereafter, Hveem and Carmany (4) postulated that repetitive load applications on flexible pavements could cause fatigue-associated distress in the asphalt-bound layers in addition to distress associated with the accumulation of irrecoverable plastic deformations. To apply this knowledge in any gainful way required that the cumulative destructive effects of the diverse spectrum of traffic loads be evaluated and, for design purposes, predicted. This greatly magnified the problems associated with traffic predictions, which heretofore had concentrated on the design-load concept.

A first indication as to how the destructive effects of various repetitive traffic loads might be reduced to a single measure was that made by Bradbury (2). He introduced the problem of flexural-fatigue failure in portland cement concrete pavements and proposed a design procedure based on the linear summation of cycle ratios concept (5) whereby estimates could be made of the age of a pavement at which fatigue cracking would be initiated. Furthermore, he illustrated the practical application of this technique by means of an example problem based on necessary assumptions concerning the distribution of traffic loads, the geometry of the pavement slab, and characterizations of material behavior.

One of the first investigators to be significantly influenced by Bradbury's work was Grumm (7), who, in the early 1940's, sought a means whereby the destructive influence of the magnitude and number of applications of any particular wheel load might be expressed in terms of an equivalent number of applications of a standard or base wheel load. A standard wheel load of 5,000 pounds was selected since it was felt that high-type pavements could

<sup>&</sup>lt;sup>1</sup>Investigators of the fatigue of metals have commonly termed this concept "Miner's hypothesis" (6).

withstand an almost unlimited number of applications of wheel loads of smaller magnitudes without exhibiting distress. Grumm introduced the concept of equivalent wheel load (EWL) or load equivalency factors, the number of applications of the standard 5,000-pound wheel load which is equivalent in destructive effect to one application of a wheel load of different magnitude. These factors, which were derived from an analysis of Bradbury's illustrative example and subsequently modified on the basis of observed flexible pavement performance inservice, are shown in Table 1. Note particularly that these factors represent a simple geometric progression for the stipulated wheel loads.

Grumm further suggested that, by using these equivalency factors and traffic estimates that yielded the total number of applications of each wheel load anticipated during a given design period, one could estimate, by summation the total equivalent number of applications of the standard 5,000-pound wheel load — that is, the total number of EWL's — that would be anticipated during the design period. Thus, if two different traffic estimates yielded identical estimates of total EWL's, the composite destructive effects of the traffic in the two circumstances were assumed to be the same.

The California investigators were the first to incorporate this means for traffic evaluation into empirical methods for flexible pavement design (7). Their use of the concept, though in a somewhat different form, has continued to the present (3). The Kentucky Department of Highways adopted a modification of the California curves for the structural design of flexible pavements in the mid-1940's (9). In 1949 (9), design curves were published which utilized, as the traffic parameter, the predicted accumulations of EWL's during the design period. On the basis of these predictions, traffic was placed in one of five categories which enabled the selection of an appropriate design curve. In 1959 (10), the number of traffic categories had been increased to 11 and the design curves were modified on the basis of an extensive pavement performance reevaluation.

TABLE 1
ORIGINAL LOAD EQUIVALENCY FACTORS (7)

Wheel Load (1bs)	Equivalency Factor
5,000	1
6,000	2
7,000	4
8,000	8
9,000	16
10,000	32

A nationwide resurgence of interest in the load equivalence concept followed analyses of the AASHO Road Test results (11-14). These analyses focused attention on the validity of expressing the destructive effects of traffic in terms of equivalent loadings, at least insofar as empirical design procedures are concerned. The standard or base load, the method for deriving the equivalency factors, the factors themselves, and some of the methods of analysis were changed to reflect the vast amounts of data from the road test and improved capabilities for analysis. However, the equivalency concept was verified and retained in the interim design guides (13,14).

During the several years immediately prior to 1963, Kentucky had been experiencing some difficulties in obtaining reliable estimates of design EWL's. Average estimates obtained at several locations had been found to agree remarkably well with the actual average EWL's that had been accumulated. However, when EWL estimates at specific locations were compared with actual accumulations, an unacceptably large variation was found. This comparison illustrated the need for a more proper determination of the effects of local conditions on significant parameters of the traffic stream. In addition, the Kentucky procedure offered no basis whatsoever for extrapolation of data to a wide variety of routes — for example, secondary roads — for which limited historical data were available.

These observations were largely responsible for the initiation of the current study in September 1963. The major purpose of the study is the reevaluation of traffic parameters used for predicting EWL's for use in pavement-thickness design procedures with the intent of more properly incorporating the influence of local conditions. The more specific objectives of the study are as follow:

- 1. to establish a proper methodology for obtaining estimates of design EWL's,
- 2. to identify those characteristics of a particular route or locale which affect the composition and axleload distributions of traffic,
- 3. to develop a means for relating significant traffic parameters to local conditions, and
- 4. to provide a means whereby estimates of EWL's by both the Kentucky and AASHO procedures can be compared and the differences evaluated.

Three specific limitations on the scope of this study are worthy of mention. First, the study is basically a traffic study. No attempt has been made to ascertain whether the equivalency factors are of proper magnitude, whether it is essential to distinguish between single and tandem axles, and so forth. Second, the traffic characteristics in rural areas have been found to differ significantly from those in urban areas. It was decided to restrict the scope of this report to rural areas within which the bulk of applicable data have been accumulated. Third, it was decided to assume that accurate estimates of average daily traffic (ADT) would be available to the designer. This assumption appears reasonable since:

1. Reasonably accurate predictions of ADT are currently available on request from the Division of Planning,

- 2. An extensive study of ADT-prediction procedures is currently programmed in Kentucky (15), and
- 3. It appears plausible that separate procedures can and should be evolved for predicting traffic volumes and the composition and weight characteristics of the traffic.

#### PROCEDURES FOR PREDICTING EWL'S

An analysis of the available literature reveals that there are apparently few, if any, procedures for properly relating EWL predictions to local conditions. However, before some of this literature is examined, it is well to review some of the fundamental differences between the Kentucky and AASHO methods of computation.

### COMPARISON OF KENTUCKY AND AASHO METHODS (10,13,14)

The major differences in the two methods are described as follow:

- 1. Base load. Kentucky has retained the 5,000-pound wheel load as the base or standard load. Converting to axleload format, the standard axleload used in Kentucky is the 10,000-pound single axleload. AASHO uses as a standard the 18,000-pound single axleload which is the maximum legal single axleload in many states  $(\underline{16})$ . For empirical correlations, the actual magnitude of the base load is of little practical significance since conversions from one base load to any alternate can readily be made. Of much more significance are the relative magnitudes of the load equivalency factors.
- 2. Axle types considered. Kentucky considers all axles as single axles while AASHO applies different sets of equivalency factors to single and tandem axles. It is well known that the destructive effects of loads acting singly and in tandem are not identical (16). The matter of ascertaining the importance of this distinction cannot be properly debated here. It should be mentioned, however, that Kentucky defines a tandem axle as the composite of two single axles whose centers lie between 42 and 120 inches (17). At the same time, AASHO specifies that this measurement should be 40 inches or less (13). Whether this distinction is relevant, considering the axle configurations which pass over Kentucky highways and those employed in the AASHO road test, is unknown. However, if it is, the Kentucky procedure may be more in order for Kentucky conditions since the axleloads tend to act separately as the distance between them increases.
- 3. <u>Derivation of load equivalency factors</u>. Kentucky's equivalency factors are based on the illustrative example of Bradbury and modified as required for compatibility with experience. The factors suggested by AASHO were determined from a statistical analysis of the performance of the road test pavements.
- 4. Factors affecting load equivalency factors. Kentucky's factors are a function of the magnitude of the single axleloads and are applicable only to flexible pavement design. AASHO's factors are a function of: (1) axleload magnitude, (2) type of pavement (flexible or rigid), (3) type of axle (single or tandem), (4) terminal serviceability rating (an index of the extent of distress at failure), and (5) the structural number (an index representing the composite structural capacity of the pavement). It is reasonable to assume that each of the determining factors selected by AASHO do theoretically affect the magnitudes of the load equivalency factors. For example, Yoder (16) has

pointed out that the equivalency factors depend upon the type and thickness of the pavement. However, recent work at Purdue University (18) indicates that for practical purposes variations in pavement thickness and terminal serviceability have little effect on equivalency factors and can possibly be neglected for pavement design purposes.

- 5. Two-axle, four-tired vehicles. In the past, only trucks have been considered by Kentucky to contribute to the accumulation of destructive loadings. A truck is defined as a motor vehicle having six or more tires and designed primarily as a freight carrier. Furthermore, all truck axles weighing less than 9,000 pounds are assumed to have negligible effect. AASHO considers all vehicles as contributing to the cumulative destructive effect although the contribution by passenger cars is extremely small.
- 6. Design EWL's. A minor distinction in terminology is necessary since Kentucky expresses traffic in terms of equivalent wheel loads, and AASHO in terms of equivalent axleloads (EAL's). This presents no difficulty since Kentucky's results can be interpreted in terms of a base single axleload of 10,000 pounds, and AASHO's results in terms of a base wheel load of 9,000 pounds. Both recommend use of a traffic evaluation period of 20 years. A major difference with regard to design procedures is that Kentucky uses total EWL's in all lanes and in both directions. AASHO identifies a single design lane for heavy-duty, multilane facilities and computes EAL's only for that lane. The results are equivalent only when the average annual directional split is 50-50 and when, on multilane facilities, all contributing, onedirectional traffic utilizes the same lane. The AASHO approach is perhaps more reasonable, especially due to the rapidly increasing mileage of multilane facilities. For this reason, the approach taken herein is to provide the capability for considering directional splits of other than 50-50 and lane distributions of other than 100 percent of the significant traffic in the design lane.

Table 2 is presented to compare the equivalency factors currently used by Kentucky and AASHO. In studying this table, one should keep clearly in mind the aforementioned distinctions between the two methods.

#### CURRENT KENTUCKY PROCEDURE

The four parameters of the traffic stream that enter the EWL computations are (1) ADT, (2) average percent trucks, (3) average number of axles per truck, and (4) the average load distribution of truck axles (axleload distribution). For purposes of estimating EWL's, these four parameters must be representative of the average conditions during the design life. Estimates must be made on the basis of data gleaned from traffic volume counts, vehicle classification counts, and weight studies at loadometer stations. Special surveys may be taken if necessary for a particular design project but most often data are obtained from the routinely conducted surveys or from special, statewide surveys.

Estimates of ADT are thought to pose no significant problems. An extensive network of automatic traffic recording (ATR) stations is located within the Commonwealth, and information obtained from these is annually supplemented by numerous counts made for more specific purposes.

TABLE 2

CURRENT LOAD EQUIVALENCY FACTORS 1

Single Axles				Tandem Axles	
Load (kips)	Kentucky	AASHO <sup>2</sup>	Load (kips)	Kentucky <sup>3</sup>	aasho <sup>2</sup>
1-3 3-5	0 0	0.0002 0.002	2-6 6-10		
5-7	ō	0.01	10-14		0.01
7-9	0	0.03	14-18		0.05
9-11	1	0.09	18-22		0.12
1113	2	0.19	22-26		0.26
13-15	4	0.36	26 <b>-3</b> 0		0.50
15-17	8	0.62	30-34		0.86
17-19	16	1.00	34-38		1.38
19 - 21	32	1.51	38-42		2.08
21-23	64	2.18	42-46		3.00
2325	128	3.03	4650		4.17
25-27	256	4.09	50-54		5.63
27-29	512	5.39	5458		7.41
29-31	1024	6.97	58-62		9.59

<sup>1</sup>The factors used by AASHO relate to truck axles. In addition, two-axle, four-tired vehicles are assumed to contribute 0.0002 EAL's per vehicle.

<sup>2</sup>These factors relate to flexible pavements having a terminal serviceability index of 2.5 and a structural number of 5.

 $^{3}$ Kentucky does not identify tandem axles separately for purposes of computation.

Accurate estimates of percent trucks are slightly more difficult to obtain. As will be shown later, the percentage of trucks is very much affected by season; the lowest value for rural stations is normally recorded during the summer months when the volume of passenger cars is large. It is essential, therefore, to obtain an annual weighted average of percent trucks. Furthermore, it must be recognized that estimates of percent trucks are made solely on the basis of vehicle classification counts. There apparently has been some tendency in the past to select as a basis for estimation only those counts taken at the loadometer stations. This practice ignores a wealth of data available from other vehicle classification counts and limits consideration to those traffic patterns representative of primary highways on which the bulk of loadometer stations have been operated.

Estimates of the average number of axles per truck likewise should be made on the basis of vehicle classification counts. Accordingly, the above remarks apropos to restricting the basis of estimates to loadometer-station data are equally relevant here. A further consideration is also important. One must not restrict determinations of the average number of axles per truck to those trucks that are actually weighed at a particular loadometer station. The rationale here is obvious since the average number of axles per truck is sensitive only to the relative percentages of the various vehicle types in the traffic stream: the vehicle sampling for weighing purposes is not necessarily in the true proportion.

Estimates of the load distribution of truck axles must be made on the basis of data obtained from loadometer stations. However, caution must be exercised to assure that both vehicle classification and weight data enter the computations unless the weight sampling by vehicle type is in the same proportion as the vehicle types exist in the traffic stream.

As summarized above, estimates of average percent trucks, average number of axles per truck, and axleload distribution have generally been based on vehicle classification and weight data obtained from loadometer stations. To account for the effects of local conditions, the analyst generally exercises his discretion in the selection of a relevant basis for evaluation. Normally considerations would include (1) the nearest loadometer station, (2) the loadometer station with the most similar traffic characteristics, and (3) statewide averages for all loadometer stations falling within a designated volume group. Under many circumstances, the effect of local conditions could be much better assessed if the analyst would extend his range of consideration to include any relevant vehicle classification counts from which estimates of average percent trucks and average number of axles per truck might be made.

With this basic information in mind, Kentucky's current procedure for estimating design EWL's is summarized by the following step-by-step procedure:

- 1. Estimate the initial ADT (total, two directional).
- 2. Estimate the average percent trucks. It is assumed that this percentage will not change significantly during the design life. The validity of this assumption is borne out by an analysis of the data assembled herein. While random variations in percent trucks are evidenced from year to year, no overall trend can be noted.
- 3. Find the initial average daily number of trucks by taking the product of initial ADT and average percent trucks.
- 4. Find the average daily number of trucks over the 20-year design period. It is assumed in most cases that the annual increase in the number of trucks is constant over the period and equals 4.65 percent of the initial number. The average number then equals the initial number increased by 46.5 percent. In special cases, other percentages may be chosen at the discretion of the analyst. For low volume groups the average increase is taken to be 20 percent. Table 3 summarizes these adjustments.

TABLE 3

KENTUCKY GROWTH ADJUSTMENT FACTORS FOR EWL ESTIMATES

#### Volume Group

	0-399 (vpd)	400-999 (vpd)	1000-1999 (vpd)	2000-2999 (vpd)	3000+ (vpd)
Multiplicative factors to adjust initial daily truck traffic to average over design period	1.200	1.200	1.465	1.465	1.465
Additive factors to adjust initial average number of axles per truck to average over design period		0.04	0.08	0.14	0.19
Additive factors to adjust initial axleload distribute to average over design perfor following axle load categories (kips)					
9-11	<del>lum</del>	0.01	0.04	0.08	0.09
11-13	break	0.01	0.04	0.11	0.13
1315		0.04	0.11	0.23	0.27
15-17	Hos	# <b>G</b>	0.04	0.12	0.15
17-19	1779	0.01	0.04	0.09	0.11
19-21	_		0.01	0.04	0.05
21-23	-15	Pricts	-	4=m	***
23-25	0.4	•	maces	_	074

- 5. Estimate the initial average number of axles per truck.
- 6. Adjust the initial average number of axles per truck to an average over the design period. This is accomplished through the use of additive adjustment factors shown in Table 3. These adjustments are based on an analysis of trend data and reflect increasing utilization of truck types having larger numbers of axles.
- 7. Estimate the total number of truck axles anticipated during the 20-year design period. This is obtained by taking the products of the adjusted average daily truck traffic (step 4), the adjusted average number of axles per truck (step 6), 365, and 20.

- 8. Estimate the initial axleload distribution for truck axles. This is the percentages of truck axles which fall within designated axleload intervals. Axles weighing less than 9,000 pounds may be neglected.
- 9. Estimate the average axleload distribution during the design period by applying the additive corrections shown in Table 3. These corrections are based on an analysis of trend data which indicate that average weights of truck axles have generally increased with time.
- 10. Find the total number of truck axles expected within each axleload category during the design life. These are obtained by multiplying the total number of truck axles (step 7) by the adjusted percentages within the various load categories (step 9).
- 11. Compute the EWL's within each axleload category by multiplying the total axles in that category (step 10) by the appropriate equivalency factor (Table 2).
- 12. Sum the EWL's of step 11 to obtain the final estimate of the total, two-directional EWL's anticipated during the design period.
  - 13. Determine the appropriate traffic category using Table 4.

Figure 1 illustrates one of the forms used to facilitate the computational process embodied in the above procedures.

TABLE 4
KENTUCKY DESIGN TRAFFIC CATEGORIES

Category	Two-Directional EWL's (millions)
IA	Less than 0.5
I	0.5-1
II	12
III	2-3
IV	<b>3</b> –6
V	6-10
VI	10-20
VII	20-40
VIII	40-80
IX	80-160
X	160-320

#### TRAFFIC VOLUME GROUP 2000-2999

COUNTY _		ROAD NAME				E NO	
PROJECT LIMITS PROJECT NO.							
LOADOME	TER \$1	TATION REFE	ERENCE_				
(1) Percen	t Truci	cs					
(2) Avg. A	xles pe	r Truck					
(3) Avg. 24	4-Hr. '	Traffic			, , , , , , , , , , , , , , , , , , ,		
(4) Avg. 24	4-Hr.	Truck Traffic	= (1) x (3)				
(5) Avg. 24	4-Hr.	Truck Traffic	for 20-Yr	.Period = 1.4	65 x (4).		
(6) Avg. A	xles pe	r Truck for Z	0-Yr. Per	iod = (2) + 0.1	14		
(7) Total A	xles in	20 Yrs. = (5	) x (6) x 36	55 x 20 ,			
(A) Axle Load (tons)	(B) Total Axies (7)	(C) % Total Axles, From Load, Sta.	(D) Correct-	(E) % Corrected Total Axles (C) + (D)	(F) Total Axles by Wt. Class (B) x (E)	(G) EWL Factor	EWL's 2 Direct (F)x(G)
4.5-5.5			0.08			1	
5.5-6.5			0,11			2	
6.5-7.5			0.23			4	
7.5-8.5			0,12			8	
8, 5-9, 5			0.09			16	
9.5-10.5			0.04			32	
10.5-11.5			0			64	
			. 0			128	

Figure 1. Form for Estimating 20-Year EWL's, 2000-2999 vpd.

#### CALIFORNIA PROCEDURE

A review of the California procedure for evaluating EWL's (8,19) provides the opportunity for introducing the concept of unit EWL's which are defined as the average EWL's per vehicle and which are a function of vehicle type. For pavement design purposes, California predicts the accumulated equivalent number of 5,000-pound wheel loads on the design lane during a 10-year period. This design EWL is converted to a Traffic Index for entry into the pavement design charts.

First it is necessary to predict the present and future, two-directional, average daily volumes of the various types of dual-tired commercial vehicles. These types are classified according to number of axles per vehicle, and buses are treated as commercial vehicles. These average daily numbers of vehicles are multiplied by EWL-conversion factors for each vehicle type, and the results are summed over all vehicle types to obtain the average annual design EWL in one direction. These conversion factors are shown in the second column of Table 5. These factors automatically convert from two-directional to one-directional volumes and from daily to annual accumulations. For special conditions of traffic, adjustments in the EWL-conversion factors

TABLE 5

CALIFORNIA EWL CONSTANTS FOR DUAL-TIRED COMMERCIAL VEHICLES

Type of Vehic	cle Annual Design EWL per Vehicle per Day	Unit EWL
2-axle truch 3-axle truch 4-axle truch 5-axle truch 6-axle truch	k 815 k 965 k 2385	1.37 4.47 5.28 13.08 8.09

may be warranted. Corresponding average unit EWL's for the various vehicle types are shown in the third column of Table 5. After the average annual one-directional design EWL has been obtained, it is multiplied by the number of years in the design period and adjusted, if necessary, for lane distribution on multilane facilities.

The important fact to emphasize here is that California largely separates the problem of estimating the composition of the traffic stream (by vehicle type) from the problem of estimating the axle-weight distributions of the various vehicle types. It is apparently assumed, furthermore, that there is some consistency in the average unit EWL's among the various types of highways even though provision is made to adjust these if necessary.

#### RECENT INVESTIGATIONS IN TEXAS

Two rather recent investigations conducted in Texas shed additional light on both methodology and the effects of local conditions. The first of these (20) was concerned primarily with methodology. The proposed methodology does not seem to differ greatly from that used in Kentucky and is outlined briefly in the following manner:

- 1. Predictions are made of the average daily traffic (ADT) anticipated throughout the design period.
- 2. The percentage of trucks can then be estimated using a curve derived from an analysis of past data which relates percent trucks with ADT. Percent trucks are not used directly in the analysis but are computed primarily for use in geometric design and as input to steps 3 and 4.
- 3. The numbers of both single and tandem axles per 100 vehicles are obtained from a tabulation based on volume group, percent trucks, and highway classification. Multiplication of these numbers by the ADT expressed in hundreds yields the total numbers of single and tandem axles anticipated.

4. Axleload distributions for both single and tandem axles are related to percent trucks. Given these distributions and the numbers of axles obtained in step 3, the numbers of each type of axle in each weight category can be determined. Equivalency factors are then applied and the results summed to obtain the design EAL's.

The second investigation (21) employed a slightly different methodology but focused attention primarily on how to relate axleload distributions at one location to those at other locations. This represented an attempt to ascertain and describe the effect of local conditions on axleload distributions. Data obtained from loadometer stations operated from 1960 through 1963 were grouped by each of the following three classification sets: (1) percent trucks, (2) highway system classification (a composite indication of geometric design standards and percentage of through trucks), and (3) statewide averages.

It was concluded that axleload distributions for design purposes should be obtained from measurements at a nearby loadometer station if such measurements are available and if design and traffic conditions are nearly identical. If not, the statewide average axleload distributions should be used except for highways approaching interstate design standards. For these facilities, average axleload distributions for stations of this high-type design should be used.

#### PURDUE UNIVERSITY

Recently, Ulbricht  $(\underline{18})$  has devised an approximate method for estimating EAL's based on a knowledge of ADT and an equivalency coefficient. The equivalency coefficient is the average EAL per vehicle and considers the proportions and weights of all vehicle types in the traffic stream. Using multiple regression techniques, an equivalency coefficient of this type was related to various parameters in the traffic stream including percent trucks and percent multiple-unit trucks. Data from 22 loadometer stations accumulated over a three-year period were utilized and the resulting correlations were found to be most acceptable.

It was suggested, however, that, since the percentages of trucks on highways of the same class are approximately constant, the equivalency coefficient could be related to a classification of highway type by truck usage. The three classes of truck routes are:

- 1. Class I truck routes all interstate routes and US-numbered routes connecting major population centers,
  - 2. Class II truck routes all other primary highways, and
  - 3. Class III truck routes all secondary state highways.

The equivalency coefficients, based on AASHO's computational procedures, are shown in Table 6.

TABLE 6
EQUIVALENCY COEFFICIENTS BY ROUTE CLASS

Class of Truck Route		y Coefficients per vehicle)
	Rigid	Flexible and Overlay
· I	0.22	0.16
II	0.10	0.07
III	0.03	0.01

To estimate EAL's, it is recommended that vehicle weight and classification data be used directly. However if such data are unavailable, a reasonbly accurate estimate may be made by obtaining the product of the average ADT, the equivalency coefficient, the number of years, and 365. The significance of this work is embodied in use of the equivalency coefficient and the ability to consider local conditions only in terms of the highway class.

#### CONCLUDING REMARKS

Other organizations (22-24) have also sought appropriate means for estimating EWL's for pavement-design purposes. In addition, still others (25,26) have been concerned with related aspects of the problem-including sampling procedures, methods for obtaining measurements, and so forth. Apparently, however, there has been very little in-depth study of the various effects of local conditions on the pertinent traffic parameters. For example, the effects of time and such a crucial variable as the maximum allowable gross weight have generally remained unknown. It is primarily to this problem that the current study is directed.

#### PROPOSED METHODOLOGY

During the search for a responsive procedure for predicting EWL's for pavement-design purposes, it was necessary to investigate whether the methodology currently used in Kentucky is sufficiently responsive to both present and future requirements of the design problem. The following criteria were established to enable a proper assessment of both current and possible alternate methodologies:

- 1. The method must be simple to apply to design situations. It was felt that any refinements requiring laborious and time-consuming computations would be unacceptable to the designer unless significant improvements in accuracy could be realized.
- 2. If a new methodology is proposed, it must be reasonably simple and straightforward in its development.
  - 3. Full use must be made of all available, relevant data.
- 4. The methodology should be rational, or at least intuitively appealing, and should lend insight as to the basic relationships entering the design computations.
- 5. The methodology should yield sufficiently accurate estimates of design EWL's.
- 6. The methodology should maximize the amount of valid data useful for other than pavement-design purposes.
- 7. The methodology should be adaptable to possible future considerations of lane and directional distributions.
- 8. The methodology should be sufficiently general so as to permit use of any chosen set of equivalency factors and to permit separate identification of single and tandem axles.
- 9. The methodology must be structured so that the effects of local conditions may be properly evaluated.

A review of Kentucky's current method led to the conclusion that it generally satisfied most of the above criteria or, with some modifications, could satisfy most of them. However, certain deficiencies were noted which made attractive the consideration of possible alternatives. In the first place, Kentucky's procedure uses the load distribution of truck axles which, as has been mentioned previously, is dependent on both vehicle classification and weight data. This means that weight data is meaningless in itself without corresponding classification counts. At first glance, this poses no significant problems since the procedures could be modified to use the axleload distributions of the various vehicle types. However, the axleload distributions are difficult to manipulate statistically and a much simpler method would be to collapse the relevant information into a single measure such as unit EWL's.

The average number of axles per truck is a variable related only to the percentages of the various vehicle types in the traffic stream. This manner of viewing these percentages seems to cloud the basic relationships which are contributing to the changing traffic stream. A somewhat arbitrary, additive correction factor (Table 3), applied to adjust for changing basic conditions with time, is not intuitively appealing and lends little insight into the mechanisms at work within the changing system.

Furthermore, the variable, percent trucks, has been examined in some detail and has been found to be relatively insensitive to local conditions and, therefore, rather difficult to predict. For example, percent trucks, though extremely variable from year to year, does not seem to demonstrate significant trends with time. However, the percent of individual truck types are greatly dependent upon year. It was felt, therefore, that benefits would be realized by predicting the percentage of each vehicle type. This would provide a built-in checking procedure as well as additional information to those concerned with the composition of the traffic stream on a designated route.

Finally, Kentucky considers only truck traffic in its analysis. At the same time, weight data obtained from loadometer stations indicate that some two-axle, four-tired, freight vehicles have axles weighing in excess of 9,000 pounds and, therefore, contribute to the accumulation of EWL's. Furthermore, some buses also have a destructive effect on pavement performance. If non-zero equivalency factors for single axle loads under 9,000 pounds are used, the effects of these omissions are somewhat magnified.

A semi-theoretical approach of the type alluded to by Larson (25) was first suggested as an alternate to the Kentucky procedure. Such an approach would be based on postulations of intercity interactions (27) extended to encompass the necessary range of vehicle types. While such an approach is intuitively appealing, development of the procedures and characterization of the system seemed to be rather monumental tasks. This is further complicated by the fact that a significant portion of the traffic in Kentucky is generated from terminals alien to Kentucky. The necessary resources for such an effort were not available and significant advantages over less tedious procedures were not assured.

It was decided, therefore, to adopt an empirical approach which relied on the correlation of significant parameters of the traffic stream with those local conditions of potential importance which could be identified and evaluated rather easily. Gross measures, such as the equivalency coefficient of Ulbricht, were rejected primarily on the basis that much significant data would be lost, the basic relationships entering the design computations would be obscured, and it would be difficult to account at some future time for lane and directional distributions. Significant parameters of the traffic stream chosen to be evaluated were the percentages of the various vehicle types and their average unit EWL's. After these characteristics were predicted for a design situation, the design EWL's were computed as follows:

Design EWL's = 
$$\Sigma\Sigma$$
 365(ADT<sub>j</sub>)(P<sub>i</sub>)(D<sub>i</sub>)(L<sub>i</sub>)(UEWL<sub>i</sub>) (1)

 $<sup>^{1}\</sup>mathrm{The}$  sum of the percentages would have to equal 100 percent.

where j = the jth year,

i = the ith vehicle type,

 $ADT_{i}$  = the average daily traffic in the jth year,

P<sub>i</sub> = the predicted percentage of the total traffic stream which is of vehicle type i,

D<sub>i</sub> = the annual average percentage of type i vehicles which travel in the critical direction,

L<sub>i</sub> = the annual average percentage of type i vehicles traveling in the critical direction in the design lane, and

UEWL; = the predicted average unit EWL's for vehicle type 1.

The design EWL's predicted from Equation 1 represent the predicted accumulations of EWL's in the design lane. This equation can be simplified somewhat when it is possible to predict an average or effective ADT during the design period and when the basis for design is the total accumulation of EWL's in both directions and all lanes. Equation 1 then reduces to

Design EWL's = 365 (N)(ADT<sub>eff</sub>) 
$$\Sigma$$
 (P<sub>i</sub>)(UEWL<sub>i</sub>) (2)

where N = the design period in years and

 $ADT_{eff}$  = the average or effective ADT during the design period.

Equation 2 provides valid estimates for use with Kentucky's current flexible pavement-design procedure.

The proposed methodology, which is embodied in Equations 1 and 2, is found to reasonably satisfy the previously enumerated criteria. It is simple both in development and application. Full use can be made of all relevant data since unit EWL's need only be derived from weight data and the percentages of the vehicle types from classification data. While maximum use is made of classification information, some information is lost when unit EWL's are substituted for axleload distributions. This problem is partially alleviated herein by the subsequent presentation of unit EWL's computed by Kentucky's procedure, by AASHO's procedure, and by a modified AASHO procedure which is explained subsequently. Local conditions enter the analysis in the determination of the traffic parameters of interest—namely, the vehicle percentages and the unit EWL's.

#### LOCAL CONDITIONS

Having thus established the proposed methodology and identified the traffic parameters of interest, it was then necessary to identify those local conditions thought to be significantly related to the composition of the traffic stream and to the weights of the vehicles included therein. The process used in this identification was largely intuitive since at this stage the available data were not in proper format for analysis.

Several rather general guidelines were available to aid in this selection. Any apparently relevant local condition would have to be amenable to analysis — that is, it would be necessary to be able to classify each condition both to enable the analysis of past data and to enable subsequent predictions. Furthermore, some rationale would have to be formulated to tentatively substantiate the relationships between the traffic parameters and the local condition. It was soon recognized that many of the relevant conditions could not be treated as continuous variables but would have to be treated as classification sets to which an integer number would be associated for data—processing purposes. Finally, it would be desirable to exclude from the set of local conditions any predictive characteristics of the traffic stream itself except ADT.

The set of local conditions chosen for analysis is shown in Table 7, which also gives information relative to the coding scheme. The data bank code is the code found on the basic data records. The second code is a transformed code used to facilitate the analyses reported herein. For convenience, all local conditions have been treated as classification sets and none as continuous variables.

- 1. Road type. The road-type category was originally intended to provide an indication of the percentage of through vehicles most notably, through trucks in the traffic stream. As such it was felt to be indicative of the local— or through—service nature of the route. It was felt that the vehicle weight and composition characteristics would greatly depend on such a classification. However, difficulties were soon apparent in attempting to devise a coding scheme which could, within a reasonable time frame, be applied for all data obtained within the study period (1950-1966). Accordingly, a compromise scheme was adopted which classified the route by the manner in which it was numbered.
- 2. Direction. Kentucky is geographically situated so that the bulk of interstate truck traffic travels on primarily north-south routes. It was felt, therefore, that the principal direction of a high-type facility might be a significant factor in determining the type of traffic traveling thereon. Accordingly, each route was classified as to its predominant direction. As an aid in making this assessment, terminal or quasi-terminal points were selected and a decision made as to whether north-south or east-west traffic would make major use of the route. Distances separating the quasi-terminal points were extended as the adjuged importance of the route increased. The potential significance of route direction was felt to greatly diminish as the local-service nature of the route increased.

TABLE 7
CODIFICATION OF LOCAL CONDITIONS

Local Condition	Data Bank Code	Code for Subsequently Reported Analyses		Description
Road Type	1 2 3 4 5 6	1 2 3 None 4 None		Interstate-numbered rural US-numbered rural KY-numbered rural Toll rural Other rural Urban
Direction	1 2	1 2		North-South East-West
Alternate Route	1 2 3	1 2 3		Alternate route is inferior No alternate or alternate of same quality Alternate route is superior
	1	1		Primarily provides service to major recreational activities
	2 3	3		Provides significant service to major recreational activities Provides some service to recreational activities
Service Provided	4 5	4 5	:	Ordinary Provides some service to mining activities
	6	6		Provides significant service to major mining activities
	7 8	7 8		Primarily provides service to major mining activities Provides more than ordinary
	9	9		service to industrial activities Primarily provides service to major concentrations of industrial activities
Volume (ADT)	None None None None None None	1 2 3 4 5 6 7 8		0-499 500-999 1000-1999 2000-2999 3000-3999 4000-5999 6000-7999

TABLE 7 (Cont'd.)

Local Condition	Data Bank Code	Code for Sebsequently Reported Analyses	Description
Volume (Cont'd.)	None None	9 10	10,000-13,999 14,000 or more
Maximum Allowable Gross Weight	None None None	1 2 3 4	30,000 lbs 42,000 lbs 59,640 lbs 73,280 lbs
	1	1	Western Kentucky (Highway Districts 1 and 2)
Geographical Area	2	2	South Central Kentucky (Highway Districts 3, 4, and 8)
	3	3	North Central Kentucky (Highway Districts 5, 6, and 7)
	4	4 .	Eastern Kentucky (Highway Districts 9, 10, 11, and 12)
	None	1	1950-1951 1952-1953
	None None	2 3	1952-1955
	None	4	1956–1957
Year	None	5	1958-1959
1000	None	6	1960-1961
	None	7	1962-1963
	None	8	1964–1965
	None	9	1966
	1	. 1	Winter (Jan - Mar)
	1	$rac{1}{2}$	Spring (Apr - June)
Season	2 3	3	Summer (July - Sept)
5692011	<b>3</b> 4	4 ·	Fall (Oct - Dec)
	5	None	Annual average for all seasons

3. Alternate route. The significance of alternate routes became apparent when traffic parameters on certain routes were studied during a time period in which alternate routes having superior geometric design standards were opened to traffic. It was apparent that, if an alternate route is available, through truck traffic tends to become channelized on that route offering the superior service. As an aid toward the classification of particular locations in this regard, the quasi-terminal-point approach was found to be particularly useful. As the importance of the route increased, it was necessary to extend the parallel band within which possible alternate routes were

considered. While three different codes were chosen to represent this local condition, it was felt that codes 1 and 2 would yield similar results and that only code 3 would be significantly different.

- 4. Service provided. A large number of routes in Kentucky provide service to areas in which rather unusual activities take place in terms of the types of traffic generated. Most notable among these are those mining areas of the Commonwealth in which the bulk of coal is carried over some segment of the high-way system. In fact, inability of current EWL-prediction procedures to adequately treat this important factor was responsible in part for initiation of the current study. It was decided, therefore, to classify each route according to the major activities which it serviced. These activities were classified as recreational, ordinary, mining, and industrial. Mining activities include not only coal mining but also aggregate production and processing. A distinction had to be made between the western and eastern coal-producing regions since much of the coal produced in the western region is transported directly from the mines by rail. As an aid to the classification of routes according to service provided, locations of coal mines, aggregate quarries, and recreational areas were carefully pinpointed.
- 5. <u>Volume</u>. Traffic volume has long been associated with other significant parameters of the traffic stream. While the expressed intent of this study was to exclude from the set of local conditions any predictive characteristics of traffic, volume was thought to be of such importance that it had to be included. An appropriate measure of volume is the ADT. This seemed not only a logical but also an expedient choice since ADT must be independently projected as a part of the proposed methodology.
- 6. Maximum allowable gross weight. Kentucky has had four different maximum allowable gross weights during the study period. Even now, different highways are assigned different maximum allowable gross weights to reflect their varying structural capabilities. Composition of the traffic stream is greatly affected by maximum allowable gross weight. As this allowable weight increases, percentages of the larger combinations tend to increase while percentages of the smaller combinations tend to decrease. It was felt that much of the variability which has been attributed to a time factor is in reality a reflection of the changing maximum allowable gross weights. Maps classifying the highway system into trucking categories were extremely useful in codifying historical data in this regard.
- 7. Geographical area. It was assumed, somewhat arbitrarily, that different geographical areas of the Commonwealth might exhibit somewhat different traffic patterns. This could not be considered as a very basic determinant of traffic characteristics but must be considered as one which, if omitted, could possibly lead to distortions of the predictions. Accordingly, four geographical areas were delineated based on intuitive considerations of the nature of the areas. The delineations were made to coincide with the boundaries of current administrative highway districts in order to facilitate their use in the predictive process. Figure 2 depicts the boundaries of these four areas.
- 8. Year. Past procedures have considered year as a major independent variable in the analysis and have relied on the application of annual correction factors to the various traffic parameters. It was felt that the apparent effects

of year might be greatly diminished if proper consideration could be afforded to other conditions such as maximum allowable gross weight. However, year was still retained as a possibly significant variable affecting pertinent traffic parameters. Year was progressively coded so that the beginning of the study period was given a code of 1 and the end a code of 9. Subsequent investigation has suggested the possibility that the effects of time might better have been expressed as that interval following a change in maximum allowable gross weight.

9. Season. Season is known to have a significant effect on the composition of the traffic stream. For example, on rural routes serving normal traffic, percent trucks is lowest during the summer and largest during the winter. Since annual averages are required for predictive purposes, it might be reasoned that season should not be included as a part of the predictive procedure. However, since the correlations of traffic parameters with local conditions must be based on historical data and since such data are not necessarily representative of the annual average conditions, season must be considered as a separate part of the analysis.

The above nine items represent that set of local conditions which was chosen for correlation with the significant traffic parameters, unit EWL's and percentages of the various vehicle types. While other local conditions may be equally as significant, they simply have not been identified in this study as being of importance in Kentucky. Data which indicate the actual relative significance of these conditions are presented in the following sections. The relative importance of each local condition varies according to the parameter which is being evaluated.

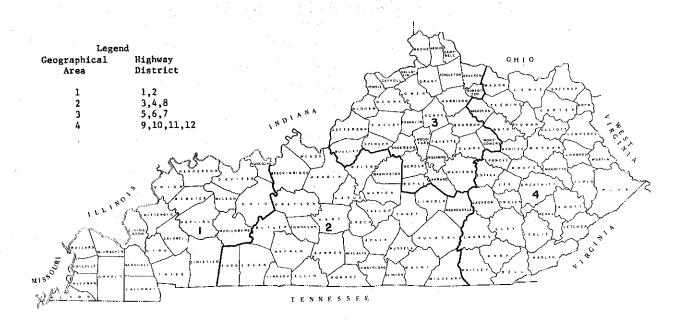


Figure 2. Four Geographical Areas.

#### DATA ACQUISITION AND ASSIMILATION

The proposed methodology not only enabled but also required separate evaluations of vehicle classification and weight data. This requirement greatly expanded the extent of available data on which the analysis was based. It also required an extensive and prolonged search through existing data files. While much assistance in this endeavor was rendered by personnel of the Division of Planning, significant efforts were directed to the identification of data sources and the transformation of available data into formats amenable to analysis by computer.

#### APPLICABLE SURVEYS

#### Loadometer Surveys

The Division of Planning has operated loadometer stations throughout the Commonwealth since 1942 (28). Locations of these stations were revised in 1950, at which time ten permanent stations were established. Since 1950, station locations have been changed periodically to reflect changing needs and travel patterns; none of the original stations is currently in operation. In 1966, ten loadometer stations were operated on rural primary highways and two on urban facilities (29). The permanent loadometer stations have always been located on the higher volume and more important routes.

Both vehicle classification and weight data are available from the load-meter stations. In general, four 24-hour classification counts are taken annually at each station, one during each season. Weight data are generally taken only once a year during the summer months. The scales are usually operated at each station for 16 hours. During this period, they are alternated between the two directions every two hours yielding a total of eight hours of operation in each direction. All freight vehicles including two-axle, four-tired vehicles are sampled for weighing in approximately the same proportions as they exist in the total traffic stream.

#### Special Weight Surveys

During the spring and summer months of 1957 and 1964, special vehicle weighing operations were conducted at many locations throughout the Commonwealth. These locations were chosen primarily to extend coverage to low-volume, secondary routes for which virtually no weight data had been otherwise obtained. Vehicle classification counts were conducted in conjunction with the weighing operations. These special weight surveys provide the bulk of weight data available for low-volume facilities.

#### Toll Roads

Extensive records are kept concerning the types and numbers of vehicles using the toll facilites in Kentucky. Of use to a study such as this would be information concerning the percentages of the various vehicle types using the

facilities. Unfortunately, vehicle types are identified solely with respect to the number of axles per vehicle. It is thus impossible to distinguish, for example, between single-unit and combination three-axle trucks. Since this method was not directly compatible with the vehicle-classification scheme adopted for this study, no toll records have been analyzed.

#### Other Classification Studies

Additional vehicle classification data are available from the ATR stations, from special classification surveys, and from origin-and-destination (O&D) studies. Data prior to 1950 were not suitable for evaluation, however, since trucks were classified only in three categories light, medium, or heavy (28). All available classification data obtained since 1950 have been included in the basic data bank.

#### DATA SOURCES

While suitable data were available from these various studies, they had not generally been summarized in a form amenable to analysis. The vehicle weight and classification data obtained from the permanent loadometer stations had generally been published in report or tabular form (29). However, the weight data had not been reported by individual station and, therefore, were useless for a detailed study of the effects of local conditions. Other published data (9,10,28) were likewise deficient.

Fortunately, all weight data obtained from the permanent loadometer stations after 1949 had been placed on punched cards. Each card contained information concerning the axle weights of one vehicle. These original cards became the primary source of available weight data.

Vehicle classification data in summarized form were virtually non-existent except for those data taken at the permanent loadometer stations and reported in the W-tables of the vehicle-weight-and-classification-study reports. The bulk of classification data were obtained through a manual search of available files of the Division of Planning.

The study period was chosen to include the years of 1950 through 1966. It is recalled that, for prior years, the weight data were not available on punched cards and that the classification data were not in proper form.

#### DATA FORMAT

With the exception of toll-road data, all available vehicle classification and weight data obtained from all sources during the study period have been assembled as a part of this study. The resulting data set includes both rural and urban data even through the urban data has yet to be analyzed.

#### Station Locations

Each location at which data were obtained was assigned a specific station number. Rather extensive efforts were made to assure that each location was

assigned only one number even though surveys may have been taken at that location for different purposes and at different times. To assure consistency in the numbering scheme, all past numbers which had been assigned to specific locations were discarded. The stations were then assigned word descriptions as illustrated by Figure 3. Reasonable efforts were made to assure consistency in the descriptions among the many station locations.

#### Indexes

Two indexes have been provided to assist in the identification and location of relevant vehicle classification data. The first of these is an index by route which lists the station numbers located on a specific route. Figure 4 illustrates this type of index. The second type of index, which is illustrated by Figure 5, enables the identification of those particular locations within each county at which classification data have been obtained and summarized

NEW	OLD	
STA	STA	DESCRIPTIONS OF STATION LOCATIONS
NUM	NUM	
<u> </u>	L 4	US27 At SCIENCE HILL IN PULASKI CO
	L, 10	US60 JUST E OF MOREHEAD AND W OF KY32 IN ROWAN,CO
3	L 27	US60 JUST W OF JCT OLD US41 IN HENDERSON CD
4	L 31	US41 2.0 MI S OF HOPKINS CO LINE IN CHRISTIAN CO
5	L 40	US60 JUST E OF JCT K#395 AT PEYTINA IN SHELBY CO
6	L 41	US31W APPROX 5.0 MES OF FRANKLIN IN SIMPSON CO
7	L 42	US25 AT LILY IN TOUREL CO
8	L 43	US25 APPROX 0.75 ML N OF GEORGETOWN CL IN SCOTT CO.
9	L 44	US27 APPROX 3-0 MI S OF ALEXANDRIA IN CAMPBELL CO.
10	L 45	US42 JUST W OF WARSAW IN GALLATIN CO
11	L 46	US51 2.4 MI NOR FULTON CL AND 0.5 MI S OF JCT KY94 IN FULTON CO
12	L 47	US41 AT NCL OF HOPKINSVILLE IN CHRISTIAN CO
13	L 48	US31W 3.0 MI S OF ELIZABETHTOWN AND APPROX 1.0 MI 5 OF JCT KY61 IN HARDIN CD
14_	1 49	US42 0.25 MI W OF JCT KY55 AND APPRUX 2.0 MI W OF CARROLLTON CL IN CARROLL CO
15	L 50	US27 L.1 MI S OF JCT KY22 AND APPROX 1.1 MI S OF FALMOUTH IN PENDLETON CO
16	<u>  51</u>	USGO 1.0 MI E OF JCT KY32 AND APPROX 2.5 MI E OF MOREHEAD CL IN ROWAN CO
17	L 52	US25 2.0 MI N OF LONDON CL ON SPUR OLD US25 1.0 MI N OF JCT KY80 In Laurel Co
_18_	1 53	US27 4.9 MI N OF WHITLEY CITY CL AND 1.0 MI S OF KY1045 IN MCCREARY CO
19	L 54	165 BTWN INTERCHANGES AT KY222 AND KY61 APPROX 2.0 MI S OF ELIZABETHTOWN IN HARDIN CO
-20	1 55	164 BIWN INTERCHANGES AT KY53 AND KY395 APPROX 4.0 ML E OF SHELBYVILLE IN SHELBY CO

Figure 3. Example of Station-Location Descriptions.

RFIL	) T E	CGUNTY	STAT	LUN NUT	MBERS	4ITH}N	COUNTY	,						
	54	BUAD	195											
		CLASK	285	287	312									
		FAVETTE	377		,112									
		EU VVK FIVI	441	442										
		SHELRY	70	76	gen									
		SHELKY	711	115	A.F.									
I	0.5	HAPPIN	19											
		HAPITY	1											
			-10-											
	7.5													
		GD AMT	7.7											
		KENTIJV		6.33										
		SCETT	1.5											
	C for file	JEFFERSON	1148											
		941.4.421.4	040											
		14-57												
υ	23	PUND	188	129										
			97		432	434								
		F ( +)YD	196	431 572	504	505	504	507	50A	500	512	513	514	
		(. P <u>F</u> F 4(1) P			- Ti - Ti	31.3	26		4,	4,,	712	, ,	31.4	
		TUHYZUN	674 06	<u> </u>	657									
		F V P F M C E			וכיז									
		LETCHER	/,50	764	706	7119								
		PIKE	67	(84	100	7/14								
	2 0													
		ционе	170	620		-								
		FAYETTE	366	368	36.0	370	371	372	372	374	778	34?	3.94	39
		FAYETTE	393	304	209	400	472	403	406	407	410	411	412	41
		LANCTEC	414	415	416	417	418	410						
		GP AMT	71	463	494	485	407	441	400					. –
		KENTON	454	6.71	624	440	631				1			
	-	LSURFL	7	17	193	20.5	445	645	650	553				
		14 A4) [ 511N	400	763	704									
		POCKCYZILI	1.0	28.23	435	837								
		SCOLE	p	864	265	R 7 3	974							

Figure 4. Example of Index by Route.

COUNTY	ŞIAI	ION NU	MBERS_	HITHIN	COUNT	Υ								
ADAIR	100	101	102	103	104	105	106_	107	106	859				
ALLEN	109	110	111	112	113	114	115	116	117	118				
ANDERSON	119	120	121	122	123	443								
BALLARD	124	125	126	127	129			·						
BARREN	29 148	135 149	136 150	137 151	138 152	139	140 154	141 155	142 362	143	144	145	146	147
RATH	156	157	158	159	160	161								
3ELL	R 5	162	163	164	165	166	167							
ROONE	168	169	170	171	172	.477	629			-				
BOURBON	47 550	80	173	174	175	176	177	178	179	190	161	182	183	184

Figure 5. Example of Index by County.

#### Codes

Numerous codes are used to identify and describe the assimilated data. Table 7, which has been presented previously, describes the codes used to classify local conditions of each station at which classification or weight data had been obtained. In addition, use was made of codes to describe other relevant information and variables. These codes are summarized in Tables 8 and 9.

TABLE 8

CODIFICATION OF VARIABLES
OTHER THAN LOCAL CONDITIONS

Variable	Data Bank Code	Code for Subsequently Reported Analyses	Description
Source	1 2 3 4 5	None None None None None	Permanent loadometer station O & D survey Special weight survey Toll records ATR classification surveys Special classification surveys
Classification Data Availability	1 2	None None	Corresponding classification data are available Corresponding classification data are <u>not</u> available
Loadometer Data Availability	1 2	None	Corresponding weight data are available Corresponding weight data are not available
Vehicle Types	1 2 3 4 5 6 7 10 11 12 13 14 15	None None 1 None None 2 None None 3 4 5	Unclassified vehicles Passenger cars (in-state) Passenger cars (out-of-state) All passenger cars Buses (school) Buses (other) All Buses SU-2A-4T (less than 1 1/2 ton) SU-2A-4T (greater than 1 1/2 ton) All SU-2A-4T SU-2A-6T SU-3A SU-4A (or more)

TABLE 8 (Cont'd.)

Variable	Data Bank Code	Code for Subsequently Reported Analyses	Description
	20 21	6 None	C-3A C-4A (2A Trac., 2A T1r.)
Vehicle	22	None	C-4A (3A Trac., 1A Tlr.)
	23	None 7	A11 C-4A
Types (Cont'd.)	23 24	, None	C-5A (3A Trac., 2A Tlr.)
(Cont d.)	25 25	None	C-5A (2A Trac., 3A Tlr.)
	26	8	A11 C-5A
	27	9	C-6A (or more)
	27	,	o on (or more)
	1	None	Single empty
		None	Single loaded
	2 3	None	All singles
	4	None	Bi-tandem empty
	5	None	Bi-tandem loaded
Axle	6	None	All bi-tandems
Туре	7	None	Tri-tandem empty
• •	8	None	Tri-tandem loaded
	9	None	All tri-tandems
	10	None	All axles (empty)
	11	None	All axles (loaded)
	12	None	All axles (total)
Data	1	None	Partial count
Limitation	2	None	Partial count, location uncertain
	3	None	Location uncertain

The source code provided a means for identifying the type of survey used to obtain the data. The classification-data-availability and loadometer-data-availability codes were used to correlate the two types of data. The vehicle-type codes were established so that codes from 1 to 9 represent passenger vehicles, 10 to 19 represent single-unit trucks, and 20 to 29 represent truck-semitrailer combinations. These codes were selected in order to provide maximum flexibility for possible future use. Experience accumulated during the study, however, dictated a reduction in the number of significant vehicle types to eight for purposes of analysis.

The axle-type code distinguished the type of axle and the condition of the vehicle, that is, empty or loaded. The "all axles" categories treat all axles as if they are single axles. The data-limitation code was used to identify those data obtained from other than 24-hour surveys and/or stations whose locations are uncertain. Finally, it was desirable to codify certain

TABLE 9
WEIGHT-CATEGORY CODES

# Axleload Interval (kips)

Code	Si	ngle Axles	Bi-Tandem Axles	Tri-Tandem Axles
1		0-7	0-14	021
2		79	14-18	21-27
3		911	18-22	27-33
4		11-13	22-26	<b>33–39</b>
5		13-15	26-30	<b>3</b> 9–45
6	•	15-17	30-34	45-51
7		17-19	34-38	<b>51</b> 57
8		19-21	38-42	57-63
9	•	21-23	42-46	<b>63</b> –69
10		23-25	46-50	69-75
11		25-27	5054	75-81
12	•	27-29	54-58	81-87
13		29-100	58-100	87-100

standard axleload intervals. The codes chosen to accomplish this are shown in Table 9.

# Classification Data

The classification data were placed on punched cards with one card summarizing the results of each count. Figure 6 illustrates the format of the basic data cards. Note that for urban stations (road type 6) most of the local conditions have not been codified. Note also that for partial counts two additional numbers are given. The first represents the length of the count, in hours, and the second represents the hour the count was begun. The daily traffic is the total number of vehicles that were counted.

While the format illustrated by Figure 6 is useful for storing all of the relevant data, it was rather inconvenient for data processing purposes. Therefore the data set was purged of unwanted data and reproduced on punched cards as shown in Figure 7. The local-condition codes shown in Figure 7 are those used for purposes of analysis.

## Weight Data

The summarized weight data were placed on magnetic tape for convenient storage and processing. Data for each weighing operation were stored on 96 sequential records. One record was required for each combination of eight vehicle types which were weighed, and the 12 axle types. Figure 8 illustrates the 96 records for one particular operation. The percentages shown represent integer tenths of a percent. Thus the number 1000 represents 100 percent. The

NO E O I D I E LALLOW O OF A U D D G R T GROSS LOCAL FOR SING SING SING SOMB COMB COMB BUS BY S R A A H T E V WT. O EIGN UNIT UNIT UNIT TRU- TRU- TRU- TRU- D C T T W Y C R F CARS TRU- TRU- TRU- TRU- TRU- TRU- TRU- TRU-	
OCTTWYCR F CARS TRU-TRU-TRU-TRUCKS-CKS-CKS-CKS	
	AET
NEAAAPTPO -CKS-CKS-CKS-CKS	RI D
Y E I R U L CARS LESS TWO TWO TRI- TRI- FOUR FIVE SIX-	<u> </u>
A A O O T A THAN AXLE AXLE AXLE AXLE AXLE AXLE AXLE AXLE	М Д
A A I I E TONS TIRE TIRE	H
LL T E	
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275 49 4 2 1 2 3 2 1 4 2 42000 2 847 181 217 0 137 3 11 0 0 0 6	3 1405
627 49 2 2 1 2 3 6 10928 4297 1095 0 832 6 509 0 0 0 21	13 17874
628 49 2 2 1 2 3 2 1 4 2 42000 2 4934 2034 611 0 701 0 426 0 0 0 0 24	40 8946 1 16 14
629 49 2 2 1 2 3 6 6970 2774 876 3 755 8 417 14 0 0 3 31	14 12134 1 16 6
125 50 1 2 1 2 1 2 2 4 1 42000 4 330 179 103 0 68 3 19 6 0 0 2	6 716 1 8 8
126 50 1 2 1 2 1 2 1 4 2 42000 2 202 404 66 0 97 4 37 6 0 0 0	8 824 1 8 8
127 50 1 2 1 2 1 3 2 4 3 42000 2 45 14 25 0 19 0 1 1 0 0 2	0 107 1 8 8
7	6 1320 1 16 6
275 50 2 6 1 2 1 3 2 4 2 30000 2 243 19 118 0 60 1 2 0 0 0 2	0 445 1 8 8
313 50 2 2 1 2 2 3 1 2 2 30000 2 77 19 66 0 108 0 3 0 0 0	0 273
	0 123
460 50 4 6 1 2 3 6 4643 717 543 0 480 24 291 15 0 0 14 6	55 6792
461 50 4 6 1 2 3 6 6466 855 795 0 667 26 328 20 0 0 20 9	99 9276
462 50 4 6 1 2 3 6 2339 194 315 0 243 3 70 7 0 0 23 3	33 3227
<u>478 50 4 2 1 2 3 2 1 3 2 42000 2 976 545 182 0 303 25 163 6 0 0 20 3</u>	30 2250
598 50 4 6 1 2 1 6 2478 282 470 0 196 9 113 6 0 0 0 2	24 3578 1 8 6
<u>599 50 4 6 1 2 1 6</u> 2468 270 484 0 212 9 117 6 0 0 0 3	32 3598 1 8 6
600 50 4 6 1 2 1 6 1392 55 271 0 115 0 9 1 0 0 0 6	67 1910 1 8 6
601 50 4 6 1 2 1 6 1584 64 273 0 100 0 11 1 0 0 0 7	<u>'3 2106 1 8 6</u>
602 50 4 6 1 2 1 6 2232 409 619 0 295 9 120 3 0 0 1 3	35 3723 1 B 6
603 50 4 6 1 2 1 2 1 4 2 42000 2 2223 416 645 , 0 281 9 120 3 0 0 1 3	3 3731 1 8 6
604 50 4 6 1 2 1 6 527 26 125 0 96 0 0 0 0	4 778 1 8 6

Figure 6. Example of Basic Classification Data.

RDASVMHYS		PERC	ENTAGES					
TIRPGGDRE R W A	CARS BUSE	5 5U-2A- 5U-2A	- SU-3A	C-3A	L-4A	/C-5A	<u>C-6</u> Ā	TRAFFIC
2 2 1 5 5 2 4 2 2	67.37C 1.81	4T 6T 9 16.473 12.28	3 0.237	1.529	0.264	0.026	0.0	3794
221562423	71.956 1.78	9 12.749 10.54	3 0.482	2.178	0.275	0.023	0.0	(4361
2 2 1 5 5 2 4 2 4	62.066 2.68	5 15.961 16.48	7 0.175	2.422	0.204	0.0	0.0	3427
2 2 1 5 4 2 4 2 1	64.199 3.33	1 14.973 13.45	9 0.437	2.894	0.707	0.0	0.0	2972
2 2 1 5 5 2 4 2 2	66.892 3.35	4 16.400 9.66	2 0.031	3.538	0.092	0.031	0.0	3250
2 2 1 5 6 2 4 2 3	7i.510 l.78	5 13.166 10.19	1 0.843	2.108	0.397	0.0	0.0	4033
221552424	73.567 2.55	9 13.204 7.42	0.358	2.226	0.537	0.128	0.0	3908
221552431	59.971 3.39	1 18.290 15.18	3 0.174	2.754	0.232	0.0	0.0	3450
2 2 1 5 5 2 4 3 2	67.323 2.43	1 17.784 9.46	0.128	2.252	0.461	0.154	0.0	3908
221562433	73.092 1.65	1 12.757 9.97	0.472	1.522	0.536	0.0	0.0	4664
2 2 1 5 5 2 4 3 4	69.770 2.26	9 12.520 11.55	5 0.522	2.634	0.678	0.052	0.0	3834
2 2 1 5 6 2 4 3 1	70.667 2.10	8 12.244 11.1C	9 0.122	3.000	0.710	0.041	0.0	4933
2 2 1 5 6 2 4 3 2	67.565 1.82	1 16.315 10.29	4 0.437	2.573	0.947	0.049	0.0	4119
221562433	78.727 1.14	4 10.827 6.42	4 0.705	1.716	0.400	0.057	0.0	5246
2 2 1 5 6 2 4 3 4	67.156 1.91	0 14.328 11.85	4 1.151	2.572	0.931	0.098	0.0	4083
2 2 1 5 4 2 4 4 1	66.271 2.66	1 14.815 11.25	0.791	3.812	0.396	0.0	0,0	2781
2 2 1 5 5 2 4 4 2	69.560 1.21	8 15.104 9.89	6 0.207	2.979	0.881	0.155	0.0	3860
2 2 1 5 6 2 4 4 3	76.286 0.36	7 12.249 7.17	3 0.441	2.401	0.955	0.122	0.0	4082
221462113	73.214 0.46	0 11.450 9.86	2 0.334	4.325	0.272	0.084	0.0	4786
221462114	72.661 0.61	3 9.219 12.44	3 0.396	3.976	0.633	0.059	0.0	5055
2 2 1 4 6 2 1 1 1	75.627 1.16	4 9.078 9.15	7 0.257	4.144	0.355	0.217	0.0	5067
2 2 1 4 6 2 1 1 2	77.227 0.56	9 8.891 8.89	0.368	3.717	0.251	0.084	0.0	5972
2 2 1 4 7 2 1 1 3	83.221 0.58	0 5.719 6.78	0.324	3.062	0.270	0.040	0.0	7414
221462114	75.643 0.74	0 8.388 10.70	3 0.303	3.799	0.420	0.0	0.0	5949
221462121		5 10.097 9.05		4.357	0.359	0.068	0.0	5853
2 2 1 4 6 2 1 2 2		4 8.911 10.66				0.141	0.0	5656
2 2 1 4 7 2 1 2 3		2 7.745 9.21				0,190	0.0	6314
221472124	-	1 8.033, 8.93				0.089	0.0	6772
2 2 1 4 6 2 1 2 1		8 8.277 8.88				0.018	0.0	5473
2 2 1 4 7 2 1 2 2		9 9.099 8.14			0.495		0.0	6671
2 2 1 4 7 2 1 2 3	80.138 0.85	9 8.573 7.00	3 0.277	2.701	0.443	0.0	0.0	7220

Figure 7. Example of Modified Classification Data.

Figure 8. Example of Basic Weight Data.

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"number of axles" represents the number of axles actually weighed.

The basic information summarized in Figure 8 is the axleload distributions by vehicle and axle types. Subsequent to the decision to treat the weight data in terms of unit EWL's, the basic data were transformed as illustrated in Figure 9. Figure 9 shows the data format as used herein for purposes of analysis.

## EXTENT OF AVAILABLE DATA

It should be emphasized that, with one exception, all vehicle classification and weight data known to be available for the 17-year study period have been incorporated into the data bank. The one exception is the vehicle-classification data obtainable from toll-road records.

Classification data were available from approximately 730 different rural locations. A total of 1871 counts were taken at these locations and approximately 6,100,000 vehicles were counted. The number of different rural locations at which vehicles were weighed is 51. The total number of vehicles weighed at these locations was approximately 69,000.

UNIT EMLS									
R D A S V M H Y S T I R P G G D R E	VEH TYPE	KENTUCKY EWL/VEH	AASHO, EWL/VEH	MODIFIED AASHO	NUMBER OF				
R W A	· · · · · · · · · · · · · · · · · · ·			EMT\AEH	AXLES				
213434393	7	1.9920	0.2080	0.2220	24				
2 1 3 4 3 4 3 9 3	8	2.3400	0.1703	0.2459	15				
213434393	<u>9</u>	0.0	0.0	0.0	0				
221564493	3	0.0	0.0040	0.0040	54				
221564493	4	2.0020	0.1584	0.1584	158				
2 2 1 5 6 4 4 9 3	5	5.6610	0.3470	0.5079	27				
2 2 1 5 6 4 4 9 3	6	2,4600	0.2401	0.2401	54				
2 2 1 5 6 4 4 9 3	7	9.3360	0.6435	0.7517	136				
2 2 1 5 6 4 4 9 3	8	9.3850	0.5452	0.8048	320				
221564493	9	0.0	0.0	0.0	0				
212394493	3	0.0	0,0056	0.0056	34				
212394493	4	5.2340	0.2723	0.2723	292				
212394493	5	24.6720	0.6710	0.9992					
212394493	6	8.7750	0.6668	0.6668	78				
212394493	7	23.9600	1.0649		348				
212394493	8	32.0150	1.1882	1.9208	630				
212394493	9	0.0	0.0	0.0	.0.				
212344293	3	0.0	0.0040	0.0040	60				
212344293	4	2.4500	0.1623	0.1623	98				
212344293	5	89.2439	0.5923	1.7203	9				
212344293	6	6.8820	0.5272	0.5272	27				
212344293	7	19.7600	0.8838	1.1994	104				
212344293	8	47.7550	1.6340	2 = 5468	330				
212344293	9	0.0	0.0	0.0	0				
112474293	3	0.0	0.0040	0.0040	34				
1 1 2 4 7 4 2 9 3	4	1.8380	0.1467	0.1467	186				
1 1 2 4 7 4 2 9 3	5	2.6160	0.1792	0.2358	24				
1 1 2 4 7 4 2 9 3	6	7.7940	0.5816	0.5816	204				
112474293		10.3320	0.6727	0.7803	800				
1 1 2 4 7 4 2 9 3	8	13.1700	0.7154	1.0674	2245				

## SUMMARY OF AVAILABLE DATA

The extensive data compilations of this study presented the unique opportunity for obtaining summary statistics of traffic parameters used in estimating EWL's. Such statistics are presented herein for both those parameters currently used in Kentucky and those proposed for future use.

### SUMMARY OF PARAMETERS USED IN PRESENT METHOD

The current EWL-prediction procedure requires evaluation of the following traffic parameters: (1) ADT, (2) the average percent trucks, (3) the average number of axles per truck, and (4) the average axleload distribution. One of the difficulties that has been encountered in making EWL estimates in the past has been the lack of a detailed summary of these parameters over a sufficiently long span of time. With the exception of ADT, the data assembled as a part of this study made possible the compilation of such a summary.

The parameters which are summarized include: (1) the average percent trucks, (2) the average number of axles per truck, (3) the average axleload distribution, (4) the average EWL's per 1,000 vehicles, and (5) the average EWL's per 1,000 trucks. Weighted averages of these parameters were computed as a function of year, traffic volume, and geographical area. These three variables were chosen as a basis for the grouping since (1) they have historical significance (10), (2) they are known to influence the magnitudes of the parameters, and (3) they are easily evaluated. The averages were weighted according to the number of vehicles counted at each location. Thus if 12 percent trucks was observed at a location where the 24-hour count was 3,000 vehicles and 18 percent trucks where the corresponding count was 6,000 vehicles, the weighted average would be 16 percent trucks.

Appendix A shows the average percent trucks and the average number of axles per truck as a function of year, traffic volume, and geographical area. Also shown are the statewide averages of these parameters. The average rural traffic in the Commonwealth over the 17-year period consisted of 18.26 percent trucks and the average number of axles per truck was 2.911. A truck was defined in the conventional way as being any freight vehicle having six or more tires. Thus pickup trucks are excluded from these and subsequent tabulations. The tabulations are based on all vehicle classification data including, in part, those obtained at the loadometer stations. Average values of both parameters are highly influenced by traffic volume and somewhat less by geographical area. The influence of year on percent trucks is sporadic and inconsequential -- it is of extreme importance, however, for average number of axles per truck. The statewide average annual change in the number of axles per truck was 0.034 for the lowest volume group and 0.085 for the highest (compare with Table 3).

 $<sup>^1\!</sup>$ An early attempt to estimate EWL's that had been accumulated on Kentucky highways was based on the use of these three variables. The results proved to be highly successful and useful.

Average axleload distributions for truck axles are shown in Appendix B. These distributions were computed on the basis of those stations for which both classification and weight data were available. Thus a large number of entries are zero, especially for the lower volume groups. The total number of axles which were counted are shown in the last columns of the tabulations. Appendix B shows that the percentage of heavier axles generally increased as the traffic volume increased and as the year became more recent. Slight differences in the axleload distributions can be observed among the four geographical area.

Two parameters which incorporate the combined effects of vehicle composition and weight characteristics are the average EWL's contributed by 1,000 vehicles and by 1,000 trucks. These parameters are summarized in Appendix C. The basis for computation was again data obtained from the permanent and special loadometer surveys. As such the statistics are representative only of summer and late spring conditions. EWL's were computed by three different methods: the Kentucky method, the AASHO method, and a modified AASHO method. The modified AASHO method used the AASHO equivalency factors for single axles and treated each tandem axle as two single axles. For any given traffic condition, the modified AASHO EAL's are equal to or slightly greater than the corresponding AASHO EAL's. When computing the Kentucky EWL's, contributions by all four-tired vehicles were assumed to be negligible. These parameters were significantly influenced by year, volume, and geographical area.

### SUMMARY OF PARAMETERS USED IN PROPOSED METHOD

The parameters proposed for future use include the percentages of the various vehicle types and their unit EWL's. Weighted means and weighted standard deviations of these parameters were computed as a function of each of the local conditions identified in Table 7. Appendices D and E show the resulting tabulations for the vehicle-type percentages and the unit EWL's, respectively.

Since means and standard deviations were computed, some technique for weighting the raw data had to be selected. Three possible techniques included: (1) weighting by the exact number of vehicles counted or weighed, (2) weighting by a group number based on the number of vehicles counted or weighed, and (3) giving equal weight to each counting or weighing operation. Table 10 shows the effect on mean Kentucky unit EWL's of the three weighting schemes. The weights assigned to the groups in the second method are given on Table 11.

Distinct differences in the mean unit EWL's computed by these three schemes may be noted from Table 10. The third or unweighted method was immediately rejected since it was felt that more importance should be attached to data obtained from a large number of vehicles than to that obtained from a smaller number. The second method of weighting by groups was ultimately selected for the following reasons: (1) it gave more weight to data obtained from larger numbers of vehicles, (2) it could be applied in the multiple regression analysis that was to follow, and (3) it did not give excessive weight to the extremely high-volume stations. Table 11 gives the weights which were assigned and which were used in preparation of Appendices D and E. These weights were used in all subsequent data analyses.

One observation immediately apparent from the tabulations of Appendices D and E is that the data are extremely variable. Coefficients of variation in

TABLE 10

EFFECT OF WEIGHTING ON MEAN KENTUCKY UNIT EWL'S

Mean Unit EWL's Weighted by

Vehicle Type	Exact Number of Vehicles Weighed	Groups by Number of Vehicles Weighed	Unweighted
SU-2A-4T	0.02	0.04	0.09
SU-2A-6T	3.31	3.19	3.09
SU-3A	12.55	10.04	8.24
C-3A	9.80	8.89	8.76
C-4A	15.77	15.25	13.40
C-5A	18.92	18.33	15,24

TABLE 11
WEIGHTING BY GROUPS

Vehicle-Type Per	centages	Unit EWL's	
Traffic Volume (ADT)	Weight	Number of Vehicles Weighed	Weight
0-499	1	0-15	1
500-999	2	16-30	2
1000-1999	3	31-60	3
2000-2999	4	61-120	4
3000-3999	5	121-240	5
4000-5999	6	241 or more	6
6000-7999	7		
8000-9999	8		•
10,000-13,999	9		
14,000 or more	10		

excess of 100 percent are not uncommon.

### EFFECTS OF LOCAL CONDITIONS

A first indication of the relative effects of the various local conditions on the traffic parameters can be obtained from Appendices D and E. One must be cautious, however, in interpreting average results such as these because of the non-random nature of the sampling and because of the interactions which exist among many of the local conditions.

The effect of road type on the various traffic parameters is quite pronounced. The road-type classification delineated in this report is not only a functional classification system but also is indicative of the quality of service provided. This results in a larger percentage of the larger types of vehicles using the higher quality highways and a larger percentage of cars on the lower type facilities. Because different highways in Kentucky are classified at different legal gross weights, the larger trucks can be operated efficiently only on the higher quality roads which have the larger weight limits. Interestingly, the average unit EWL's are generally larger for the lower classes of highways. This reflects, in part, a more efficient utilization of vehicle capacities on these roads.

The percentage of passenger cars using north-south routes is not significantly different from that using east-west routes. However, slightly more of the larger trucks use the north-south routes and their unit EWL's are significantly greater. This difference in unit EWL's may be due to the degree to which these vehicles are loaded, the density of the cargo, and significant differences in the average local conditions such as road type and maximum allowable gross weight.

The data support the conclusions that larger vehicles tend to use the superior of two alternate routes and that these vehicles are also more heavily loaded on the superior routes. The vehicle-type percentages and the unit EWL's are not significantly different for routes in which there is no alternate, there is an alternate of equal quality, or there is an alternate of inferior quality.

Service provided also yielded some significant indications as to traffic characteristics. Recreational roads carried much larger percentages of passenger cars and mining roads carried larger percentages of SU-2A-6T and SU-3A trucks, which are the vehicle configurations most often used for hauling coal and aggregates. Furthermore, the SU-2A-6T and SU-3A trucks were loaded much more heavily on the mining roads. Beyond this, the effects of service provided are unknown due to the limited data available for many of the codes and the difficulties associated with evaluating this local condition.

The percentage of passenger cars generally increases as the traffic volume increases. The percentages of the larger vehicle types seem to peak in the range of 4,000 to 6,000 vehicles per day. The weights of the vehicles, as indicated by their average unit EWL's, seem to reach a minimum in this same range.

Maximum allowable gross weight is a significant determinant of the

percentages of the various vehicles types. The maximum percentages of C-5A, C-4A, and C-3A vehicles occurred at maximum allowable gross weights of 73,280 pounds, 59,640 pounds, and 42,000 pounds, respectively. These represent legally allowable weights at which the respective vehicle capabilities can be most effectively utilized. The effects of maximum allowable gross weight on average unit EWL's is significant but not readily explainable. A part of the difficulty stems from the relative scarcity of data. Independent data analyses have shown, however, that the mean unit EWL's for the four largest vehicles are essentially constant when the ratio of the vehicle weight capacity to the maximum allowable gross weight is less than one. When the ratio exceeds one, the mean unit EWL's are significantly reduced.

The effects of year are significant on both the vehicle-type percentages and the unit EWL's. However, it is felt that much of the yearly influence is due to changing maximum allowable gross weights, a condition which makes evaluation of these average statistics particularly difficult.

Finally, detection of possible seasonal differences in unit EWL's is impossible since loadometer surveys have been taken only during the summer and later spring months in Kentucky. Significant differences were detected, however, in the vehicle-type percentages with the maximum percentage of cars occurring during the summer months for these rural highways.

### PREDICTION OF TRAFFIC PARAMETERS

The proposed methodology requires evaluation of the percentages of the various vehicle types and their unit EWL's. For the sake of simplicity and to assure compatibility between the available classification and weight data, the number of vehicle types was limited to eight. These include (1) cars, (2) buses, (3) single-unit, two-axle, four-tired (SU-2A-4T) trucks, (4) single-unit, two-axle, six-tired (SU-2A-6T) trucks, (5) single-unit, three-axle (SU-3A) trucks, (6) combination, three-axle (C-3A) trucks, (7) combination, four-axle (C-4A) trucks, and (8) combination, five-axle (C-5A) trucks. Unit EWL's were evaluated by each of three methods including the Kentucky method, the AASHO method, and the modified AASHO method. The modified AASHO method uses the AASHO equivalency factors but makes no special recognition of tandem axles.

The approach for relating the traffic parameters with the local conditions was empirical in nature. Each parameter was separately treated as the dependent variable and the local conditions as the independent variables. Each parameter was quantified as a continuous variable while each local condition was codified on the basis of classification sets. The various methods which were considered for correlating the traffic parameters with local conditions are detailed in the following section. Each method was judged with regard to its accuracy, its simplicity, its reasonableness, and its predictability.

### **METHODS**

## Combinatorial Analysis

It was recognized at the onset that strong interactions might exist among many of the local conditions. For example, route direction was thought to be significant only for the higher type facilities. Such interactions can be properly treated, when the independent variables are characterized by classification sets, by grouping the available data into categories representative of each possible combination of the independent variables. The average values of the dependent variables within each combination would then serve as the best estimates of future traffic if the future state of each of the relevant local conditions could be established.

Such a scheme proved to be extremely valuable in some preliminary investigations in which the number of local conditions was limited to three: namely, year, geographical area, and traffic volume. The purpose of these investigations was to derive a simple means for estimating past accumulations of EWL's on selected rural highways in Kentucky. The number of possible combinations of the local conditions in this analysis was 340. Unfortunately when the number of local conditions increases, the number of possible combinations of these conditions increases rapidly. In fact the number of possible combinations for all of the local conditions enumerated herein, excluding year and season, exceeds 40,000. Since the available data could not support such a detailed categorization, the combinatorial analysis could not be a feasible approach for this problem.

# Means and Correction Factors

Perhaps the easiest way to predict the traffic parameters is to compute their mean values from the available data and to use these values for predictions. This is basically the approach chosen by California in their unit EWL tabulations (Table 5). One way to consider the effects of local conditions is simply to modify the gross means based on intuition and judgement. Since this procedure was judged to be unsatisfactory, the gross-means approach was not pursued further.

If it can be assumed that interactions among the local conditions are inconsequential, then the effects of local conditions can be evaluated by applying a series of correction or adjustment factors to the gross means. There is one correction factor for each local condition and its value is determined by the local-condition code. To apply this procedure, the gross means are first computed. Then average residuals between the actual parameter values and the gross means are computed for each value of one selected local condition. The process is repeated for the second and subsequent local conditions by computing average residuals between actual values and those predicted from the gross means and the correction factors from previously analyzed local conditions. The entire process is iterated to reduce the effect of the chosen sequence of local conditions.

Computer programs for derivation of correction factors verified the feasibility of this approach. It was found that the correction factors converged after a maximum of about five iterations. Furthermore it was shown that the order in which the local conditions were evaluated had no effect on the values of the correction factors.

A very relevant question is whether the correction factors should be additive or multiplicative. It is apparent that the final choice should be based largely on the accuracy attained. However a special problem arose through the use of additive factors — due to the prediction of several negative percentages and negative unit EWL's. While adjustment procedures can be derived which assure no negative predictions, such procedures are rather arbitrary and are unnecessary if multiplicative factors are used.

The correction-factor approach may be somewhat deficient because consideration of interactions among the local conditions is precluded. This deficiency can be partially alleviated if it is possible to identify two or three local conditions having strong interactions. Average values of the traffic parameters are then computed for all possible combinations of this restricted set of local conditions. The effects of the remaining local conditions are treated independently as correction factors applied to the average basic percentages in much the same manner as outlined above. The primary difference is that in the former case the correction factors are applied to the gross means while in the latter case they are applied to classified means computed for various combinations of the interacting local conditions.

The two immediately preceding methods are based on iterative procedures designed to eliminate the effects of the order in which the correction factors are applied. Accuracy can possibly be improved not only by maintaining a

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The two immediately preceding methods are based on iterative procedures designed to eliminate the effects of the order in which the correction factors are applied. Accuracy can possibly be improved not only by maintaining a

specified sequence of correction-factor application but also by selecting values of the correction factors based on both the coded values of the local conditions and on the prior predictions. This approach was also successfully programmed. The prior prediction of percent trucks was used as a determinant of the value of the corrective factor.

# Multiple Regression

Detailed study of the data in Appendices D and E led to the identification of another possible method of analysis. Average values of the parameters could be taken from these tables for each of the local conditions. These averages could in turn be averaged over all the local conditions to obtain the desired estimates. This procedure would give equal weight to the importance of each of the local conditions. Since the validity of such a weighting scheme was highly suspect, methods were sought in which a different weight, which would be indicative of the relative importance of the local condition, could be assigned to the averages for each local condition.

Conventional multiple regression techniques were found to provide a suitable answer to the problem. Use was made of a standard, stepwise, multiple regression program in the University of Kentucky statistical library of computer programs (30). This program, called MULTR, satisfactorily established the weights to be applied to the average estimates for each local condition. The weights were found to depend on the particular traffic parameter being evaluated.

One final method was evaluated for correlating the traffic parameters with local conditions. This is a multiple regression technique using dummy variables which is useful in those situations in which the independent variables are treated as classification sets (31). For this problem, the jth local condition, represented by n, codes, is replaced by (n,-1) dummy variables. For example, if there are only two local conditions, road type and traffic volume, the dummy variables, which are independent variables, would be as shown on Table 12. No dummy variable is assigned to one category for each local condition in order to make estimates of the constant term and all the coefficients in the regression equation mathematically determinant. The dummy variable is assigned a value of either one, if the local condition is characterized by the corresponding code, or zero if it is not. Table 13 illustrates this procedure for the two local conditions of Table 12. Thus for road-type 2 and trafficvolume 8, dummy variables  $X_2$  and  $X_{11}$  would assume values of one and the remaining dummy variables, zero. For road-type 4 and traffic-volume 10, all dummy variables would assume values of zero.

If the effects of the various local conditions are additive, the corresponding regression equation is

$$Y = a_0 + a_1 X_1 + a_2 X_2 + \dots + a_{12} X_{12}$$
 (3)

where Y = the traffic parameter of interest,

 $a_0$  = regression constant,

 $a_{i}$  = regression coefficients, and

TABLE 12

ILLUSTRATION OF DUMMY VARIABLES

Local Condition	Code	Dummy Variable
Road Type	1 2 3	X <sub>1</sub> X <sub>2</sub> X <sub>3</sub>
	1 2	None X <sub>4</sub> X <sub>5</sub>
Traffic Volume	3 4 5 6	X6 X7 X8 X9
	7 8 9 10	X10 X11 X12 None

TABLE 13

ILLUSTRATION OF VALUES OF DUMMY VARIABLES

Local Condition	Code	<sup>x</sup> 1	х <sub>2</sub>	×3	X4	*	and the		rial <sup>X</sup> 8		X10	× <sub>11</sub>	<sup>X</sup> 12
Road Type	1 2 3 4	1 0 0 0	0 1 0 0	0 0 1 0									
	1 2 3				1 0 0	0 1 0	0 0 1	0 0 0	0	0 0	0 0	0 0 0	0 0 0
Traffic Volume	5 6 7 8 9				0 0 0 0 0	0 0 0	000000	1 0 0 0 0 0	0 1 0 0 0 0	0 0 1 0 0 0	0 0 0 1 0 0 0	0 0 0 1 0 0	0 0 0 0 1
	10				0	0	0	0	0	0	0	0	0

X<sub>i</sub> = dummy variable.

It may be seen, therefore, that  $a_0$  becomes the best estimate of the traffic parameter in the above example for road-type 4 and traffic-volume 10. If the effects of the various local conditions are multiplicative, the relation between the traffic parameter and the local condition is shown as follows:

$$Y = b_0 b_1^{X_1} b_2^{X_2} \dots b_{12}^{X_{12}}.$$
 (4)

The corresponding regression equation becomes

$$Z = c_0 + c_1 X_1 + c_2 X_2 + \dots + c_{12} X_{12}$$
 (5)

where  $Z = \ln Y$  and

 $c_i = \ln b_i$ .

The above procedures and equations can be generalized to include the nine local conditions of Table 7, in which case there are 40 dummy variables. It may further be generalized to include interactions among two or more of the local conditions by redefining the dummy variables so that each dummy variable corresponds to one combination of the interacting local conditions. This greatly increases the number of dummy variables and was not attempted due to program limitations which restrict the number of dummy variables to 50.

## Summary

Several possible methods for correlating the relevant traffic parameters with local conditions have been outlined above. The feasibility of each of these has been established as a part of this study. The selection of a particular method must be based, however, on the aforementioned criteria of accuracy, simplicity, reasonableness, and predictability. Following sections of this report present a discussion relative to the selection of appropriate methods. Table 14 summarizes the candidate methods which have been discussed herein. Also presented in Table 14 are abbreviated names of the various methods designed to facilitate future reference. It should be emphasized that most of these methods are readily adaptable to either multiplicative or additive adjustments.

It should also be emphasized that the multiple regression technique using dummy variables is quite similar to the iterative correction factor technique. Differences relate only to the manner in which the various factors and coefficients are established. The multiple regression technique is supported by sound mathematical and statistical theory while the correction factor technique is based more on intuition and judgement.

### TABLE 14

# METHODS FOR CORRELATION OF TRAFFIC PARAMETERS WITH LOCAL CONDITIONS

Description	Nomenclature
Combinatorial means	None
Gross means	None
Correction factor based on gross means, no interaction, iterative	FACT1
Correction factor based on classified means, limited interaction, iterative	FACT2
Correction factor based on classified means, limited interaction, prior knowledge	FACT3
Multiple regression, averages	MULTRA
Multiple regression, dummy variables	MULTRD

## PREDICTING VEHICLE-TYPE PERCENTAGES

## Selection of Predictive Methodology

With the exception of combinatorial means, each of the possible methods of Table 14 for correlating the vehicle type percentages with the local conditions was investigated. The gross means approach was immediately rejected since all other methods were found to yield superior accuracies. The remaining methods were compared on the basis of the four criteria of relative simplicity, reasonableness, accuracy, and predictability and a recommended method was developed.

Of interest first was whether there were significant differences in accuracy between the correction factor techniques and the multiple regression techniques. The other criteria for comparison were assumed to be identical for both of the techniques. Using additive factors (similar to Equation 3) for predicting the percentage of C-4A trucks, correlation coefficients of 0.78, 0.78, and 0.79 were obtained by FACT1, MULTRA, and MULTRD, respectively. The C-4A truck was chosen for this analysis since it has been the largest single contributor to EWL accumulations on rural highways in Kentucky. All available vehicle classification data were used in this and subsequent analyses. Similar estimates of the percentage of cars using FACT1 and MULTRD yielded correlation coefficients of 0.62 and 0.60, respectively. It was, therefore, concluded that there were no significant differences between the correction

factor and multiple regression techniques and that an intelligent selection of the best of these techniques would have to be based on other considerations. Similarly no significant difference was observed between the dummy variable (MULTRD) and the averages (MULTRA) multiple regression techniques.

One factor which would dictate a choice of the correction factor techniques would be to verify the necessity for including interaction effects among two or more of the local conditions. Thus estimates were made of the percentages of cars and C-4A trucks using FACT1 and FACT2. In both cases, all nine local conditions were considered and additive factors were used. FACT2 used road type, direction, and alternate route as the three interacting local conditions. Estimates of the percentage of cars yielded correlation coefficients of 0.62 and 0.63 for FACT1 and FACT2, respectively. Similar estimates of the percentage of C-4A trucks yielded correlation coefficients of 0.78 and 0.80 for FACT1 and FACT2, respectively. Since the three interacting local conditions of FACT2 had not been shown to be optimal and since slightly larger accuracies were achieved with IACT2, it was concluded that interaction might well be significant. This led to the immediate rejection of the multiple regression techniques since sufficient program capability was not available for handling even a limited number of interactions. Subsequent analyses showed that the three interacting local conditions used by FACT2 were not optimal and that larger correlation coefficients would have been achieved with FACT2 if other interacting local conditions had been specified.

Having decided that interactions among at least three of the local conditions were significant, it was then necessary to ascertain whether the remaining local conditions should be represented by correction factors (1) which were order independent and derived using iterative procedures or (2) which were order dependent and responsive not only to the local conditions but also to the prior predictions. The variable representing prior predictions was percent trucks: three conditions were chosen depending on whether the prior predictions of percent trucks were less than 15 percent, between 15 and 19 percent, or greater than 19 percent. Additive factors were used and the three interactive local conditions were, as before, road type, direction, and alternate route. Predictions of the percentage of cars yielded correlation coefficients of 0.63 and 0.66 for FACT2 and FACT3, respectively. Predictions of the percentage of C-4A trucks yielded correlation coefficients of 0.80 and 0.82 for FACT2 and FACT3, respectively. These results indicated the slight superiority in accuracy for predictions based on a specified sequence of correction-factor application and prior estimates. At the same time, use of the procedures required by FACT3 were considerably more complicated and susceptible to increased human error. Therefore, FACT2 was chosen for use in predicting the vehicle type percentages.

Remaining to be decided was whether the correction factors should be additive or multiplicative. The criterion of reasonableness weighed heavily in favor of the specification of multiplicative factors since their use negates the possibility of negative predictions. Data were already at hand from previous results of MULTRD with which to ascertain the superior of the two techniques with regard to accuracy. Correlation coefficients of 0.79 and 0.86 for cars and 0.60 and 0.57 for C-4A trucks had been obtained for additive and multiplicative factors, respectively. Since these accuracy determinations were inclusive and since multiplicative factors were superior on the basis of reasonableness, multiplicative factors were selected.

# Final Predictive Technique

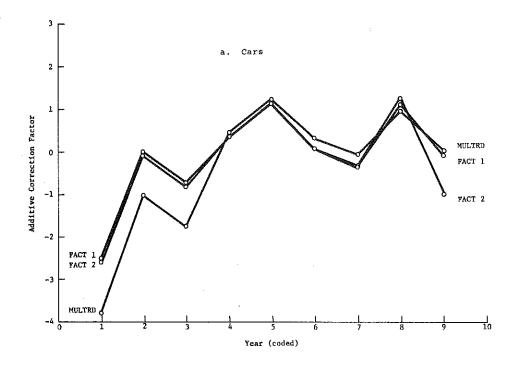
The method that had been chosen to relate the vehicle type percentages to the local conditions was the correction-factor technique considering interactions among some of the local conditions and applying independent multiplicative correction factors to account for the remainder. However, several remaining items had to be considered in order to establish the viability of the technique as a predictive tool.

Not minor among these was the manner in which the time variable, year, was to be considered in the predictive process. Prior work as summarized in Figure 10 showed how various additive correction factors had been affected by year during the 17-year study period. Certainly data such as these furnished no reasonable basis from which to predict the possible effects of future years. The most promising solution was to exclude year from the analysis and to ascertain how the accuracy was thereby affected. Data were available from prior use of MULTRD and FACT3 which showed that exclusion of year caused a reduction in the correlation coefficients for predictions of the percentages of cars and C-4A trucks of less than 5 percent. It was obvious that this slight decrease in accuracy had to be tolerated and year was subsequently excluded from the analysis.

Remaining to be determined was which of the eight local conditions should be established as those among which interactions are of most significance. Based on the number of possible combinations of the local conditions and the number of available data sets, it was considered feasible to include a maximum of three interacting local conditions. For reasons discussed later, season was excluded as a possible candidate for evaluation. From the remaining seven local conditions, eight of the most promising combinations of three conditions were selected intuitively and analyzed jointly on the basis of relative accuracy and predictability. As a result of this analysis, road type, maximum allowable gross weight, and traffic volume were adjudged to exhibit the most significant interactions among those investigated.

A set of basic percentages were derived for all possible combinations of these three local conditions. Also derived were a set of multiplicative correction factors for each of the remaining five local conditions to be applied independently to the basic percentages. Sheets 3 and 4 of Appendix F show the final set of basic percentages and multiplicative correction factors recommended for use in predicting vehicle type percentages.

It may be noted from Sheet 4 of this appendix that correction factors are given for the various seasons. These factors have been retained primarily to enable comparisons of vehicle type percentages estimated by the proposed methodology with those observed from specific surveys. To be useful for predicting the annual averages that are desired, however, the seasonal factor must be eliminated. To do this, all 1967 traffic volume data obtained from 42 ATR stations in Kentucky were summed by season. An annual average of the seasonal correction factors weighted by the seasonal traffic volumes was computed. These weighted averages, which are shown in the computational portions of Sheet 4, are recommended for use in the predictive process. The fact that these averages approach unity suggests that classification counts have been taken in approximately the same proportions as actual traffic volumes by season.



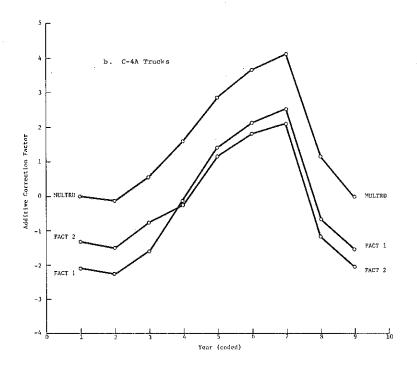


Figure 10. Influence of Year on Additive Correction Factors.

Finally, the criterion of reasonableness dictates that the sum of the predicted percentages must equal 100 percent. Since the percentage of each vehicle type is predicted independently of the remaining vehicle types, the total percentages will rarely equal 100 percent. For this reason, the initial predictions must often be appropriately modified. Several methods for accomplishing this were suggested. However since all preliminary estimates were close to 100 percent, an elaborate adjustment procedure was felt to be unwarranted. It is recommended, therefore, that the adjustments to 100 percent be made by multiplying each initial prediction by 100 divided by the sum of the initial predictions. This procedure is summarized on Sheet 4 of Appendix F.

# Accuracy

The procedures described above, together with the basic percentages presented on Sheet 3 of Appendix F and the multiplicative correction factors presented on Sheet 4, were used to estimate vehicle-type percentages for comparison with the actual percentages obtained from past vehicle classification counts. The results of this accuracy comparison are summarized in Table 15.

The accuracy of the proposed predictive technique, as indicated by the correlation coefficients, is not good. Some slight decrease in accuracy resulted from the exclusion of year from the set of local conditions. However, this was necessary in order to establish the technique as a valid, predictive tool. Despite the relative inaccuracy of the technique, it was found superior to others of those investigated on the basis of the four criteria of accuracy, simplicity, reasonableness, and predictability. Table 15 also shows that slight increases in accuracy for most vehicle types were achieved by correcting the initial estimates to a total of 100 percent.

## PREDICTING UNIT EWL'S

## Selection of Predictive Methodology

In comparison with the vehicle classification data, the available weight data were much less extensive. Most of the weight data had been obtained from rural, primary routes having relatively high-volume, ordinary types of traffic. All had been obtained during the late spring or summer months. Because of this rather limited data, consideration of interactions among even a limited number of local conditions was felt to be unwarranted. In spite of this, however, analyses of Appendix E and other data indicated that an approach such as gross means would be inappropriate since the local conditions did measurably affect the average unit EWL's. Consideration was limited to multiple regression techniques since possible interactions were not to be investigated and since the correction-factor techniques offered no known advantages over the multiple regression techniques.

Only a cursory analysis was made to ascertain the superior of the MULTRA and MULTRD techniques. Kentucky unit EWL estimates using MULTRA were made for the SU-3A trucks which yielded a correlation coefficient of 0.44. Similar estimates were also made using MULTRD, additive techniques and which eliminated year and service provided as independent variables. These yielded a correlation coefficient of 0.59. It was therefore decided that MULTRD was superior to

TABLE 15

ACCURACY OF VEHICLE-TYPE PERCENTAGE ESTIMATES

Vehicle Type	Mean Percent	Standard Deviation	Standard	l Error	Correlation	Number of Vehicles	
råħe.	Tercent	Unc		$\mathtt{Corrected}^{1}$	Uncorrected	$\mathtt{Corrected}^{1}$	Counted
Cars	71.6 <b>71</b> 8	7,1262	5.7059	5,6479	0.5984	0.6098	4,159,168
Buses	0.8592	0,6164	0,4842	0.4843	0.6187	0.6186	46,953
SU-2A-4T	9.0922	3,8732	2,6203	2.5744	0.7364	0.7471	474,626
SU-2A-6T	8.5095	3.8990	3.2277	3,2297	0.5610	0.5602	456,745
SU-3A	1.0016	2.3819	2.1307	2.1244	0.4470	0.4522	52,264
C-3A	3.9378	4.1526	2,6852	2,6831	0.7628	0.7632	239,123
C-4A	4.1038	4,3735	2,6848	2,6772	0.7894	0.7907	263,847
C-5A	0.8230	2.1582	1.5584	1,5448	0.6918	0,6983	56,805

 $<sup>^{1}</sup>$ Estimates of vehicle-type percentages were corrected to a total of 100 percent.

MULTRA for the unit EWL predictions. MULTRA did allow a determination of the order of importance of the local conditions with regard to the unit EWL parameter for SU-3A trucks. It rated service provided as the most influencial condition followed in decreasing order of importance by maximum allowable gross weight, volume, road type, direction, geographical area, year, and alternate route.

The next item to be considered was whether the factors should be additive (Equation 3) or multiplicative (Equation 4). Estimates were made of Kentucky unit EWL's for C-4A trucks using MULTRD with both additive and multiplicative factors. The C-4A truck was chosen for this analysis since it has been the single most important contributor to EWL accumulations on rural highways in Kentucky. The additive factors yielded a correlation coefficient of 0.76 and the multiplicative, 0.72. Additive factors were chosen, therefore, not only on the basis of their superior accuracy (which was verified for other of the vehicle types as well) but also because they are slightly easier to derive and use. Some reasonableness was sacrificed because of the possibility for predicting negative unit EWL's but this is overshadowed in part by the slight increases in overall accuracy resulting when negative estimates are set equal to zero.

The method which was finally selected for relating unit EWL's with local conditions was, therefore, additive factors derived using multiple regression with dummy variables. The next problem was to assess its reliability as a predictive tool. The most important local condition with regard to future predictions is year. Estimates of unit EWL's for C-4A trucks were made both including and excluding year as an independent variable. These yielded correlation coefficients of 0.76 and 0.72, respectively. Thus the inclusion of year was found to slightly increase the accuracy with which past unit EWL's for this vehicle type could be estimated. But could year serve as a basis for future predictions? Figure 11 was constructed to ascertain an answer. If attempts were made to extrapolate the data of this figure to future years, the additive correction factor would have to be taken as approximately zero. Thus it would be impossible to discriminate among the effects of future years. Furthermore, because of the interrelationship between year and maximum allowable gross weight, the correction factors for maximum allowable gross weight appear incongruous when year is included as an independent variable. This is apparent from Figure 12. Year was, therefore, excluded as an independent variable for predictive purposes.

Each of the remaining seven local conditions contributed to the analysis, and all were amenable to future predictions with the exception of service provided. Data were available to establish valid correction factors only for service-provided codes of 3, 4, and  $5^{1}$ . Therefore due to lack of data, service provided was also eliminated as an independent variable — causing a further reduction in the correlation coefficient from 0.72 to 0.62. This represents a significant reduction in accuracy and suggests that more accurate future estimates may be partially dependent on the weighing of vehicles on road representing each of the service-provided categories.

<sup>&</sup>lt;sup>1</sup>See Appendix E.

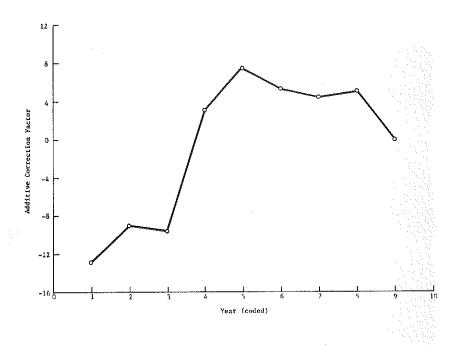


Figure 11. Relationship Between Additive Correction Factor and Year (Unit EWL Estimates for C-4 $\Lambda$  Trucks).

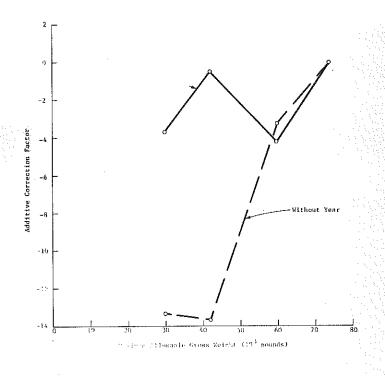


Figure 12. Relationship Between Additive Correction
Factor and Maximum Allowable Gross Weight
(Unit EWL Estimates for C-4A Trucks).

Sheet 5 of Appendix F shows the final additive correction factors for all vehicle types and all types of unit EWL's. The factors for road-type 4 were assumed the same as those for road-type 3 since no weight data had been obtained for the "other rural roads" category. Furthermore, it was necessary to obtain the factors for volume-group 10 by extrapolation since no data were available for this volume group. The base conditions for the predictions are road-type 2, direction 2, alternate-route 3, volume 5 (except for C-5A where it is 7), maximum-allowable-gross-weight 4, and geographical area 4. Thus the constant term in each case represents the unit EWL predictions for this set of local conditions.

# Cars and Buses

To enable valid predictions of EWL accumulations, the predictive methodology must recognize all EWL contributions regardless of their source. This reasoning prompted, for example, the separate consideration of SU-2A-4T vehicles since weight data indicated that these vehicles did make slight contributions to the EWL accumulations. The remaining vehicle types which have not yet been considered herein because no weight data were available for analysis are cars and buses. Each must be investigated with regard to its possible effect on EWL accumulations.

Since the gross weights of typical passenger cars are so small, it must be assumed that cars have zero unit EWL's when evaluated by Kentucky's procedure. This is necessitated by the fact that Kentucky equivalency factors for axleloads less than 9,000 pounds are zero. For such small axleloads, however, the AASHO equivalency factors are not zero. In lieu of valid weight data for car axles, the unit EAL's for cars by AASHO and modified AASHO procedures are assumed to be 0.0002 EAL's per car. This follows from the recommendations of the AASHO Committee on Design (13). This unit EAL is assumed to be constant for all possible sets of local conditions.

Buses, and in particular commercial, intercity buses, pose more significant problems in that their unit EWL's may be rather large. Fortunately with regard to EWL predictions, the numbers of commercial buses on rural highways are rather small so that errors in unit EWL predictions are relatively insignificant in terms of the total EWL accumulations. However, a large percentage of school buses are found on some rural, low-class roads (as much as 6 percent). Assuming the unit EWL contribution of school buses is equal to that of commercial buses, this means that as high as 50 percent of the total EWL's on some rural roads result from school buses.

Information supplied by Southern Greyhound Lines relative to the axle weights of its commercial buses operated in Kentucky enabled the preparation of Table 16. Since none of these buses has, at present, a tandem axle, the estimates for AASHO and modified AASHO unit EAL's are identical. Unfortunately the data of Table 16 fail to represent the entire problem since school buses and buses operated by other agencies and for other purposes are not included. Furthermore, no information is readily available concerning the average loading of these buses and the percentages of the various bus types. Also shown in Table 16 are arbitrary estimates of unit EWL's which have been chosen to represent the average conditions in Kentucky for all types of buses. These estimates are recommended for use in the predictive equations until such time as more

TABLE 16

## UNIT EWL'S OF BUSES

	Commercial Buses <sup>1</sup> (Empty)	Commercial Buses (Fully loaded)	Estimate Including Other Buses	
Kentucky Unit EWL	3.6	16.0	5	
AASHO Unit EAL	0.31	1.06	0.4	
Modified AASHO Unit EAL	0.31	1.06	0.4	

1From information supplied by Southern Greyhound Lines.

valid data become available. Like the unit EWL estimates for cars, these estimates are not responsive to variations in local conditions.

# Accuracy

The procedures described above, together with the additive factors presented on Sheet 5 of Appendix F, were used to estimate unit EWL's for comparison with actual unit EWL's obtained from past weight data. The results of this accuracy comparison are summarized in Table 17.

A brief glance at the tabulated correlation coefficients is sufficient to reveal that the accuracy of the estimates leaves much to be desired. However, no other technique investigated herein yielded superior accuracy as long as it was stipulated that the technique had to represent a valid, predictive procedure. Furthermore, it is apparent from Table 17 that this method of accounting for the effects of local conditions is superior to the gross means approach.

Three other points relative to this accuracy comparison are important:

- 1. The best accuracy was generally achieved for those vehicle types which contribute most significantly to the EWL accumulations.
- 2. Generally, estimates of Kentucky unit EWL's are more accurate than either AASHO or modified AASHO unit EAL's.
- 3. The procedure for correcting negative unit EWL's to zero only slightly improved the accuracy of the estimates. The magnitude of the improvement was greatest where the mean unit EWL was lowest, that is, for the SU-2A-4T vehicle.

 $\begin{array}{c} \text{TABLE 17} \\ \text{ACCURACY OF UNIT EWL ESTIMATES}^{1} \end{array}$ 

Vehicle	EWL Type	Mean Unit EWL	Standard Deviation	Standard Error		Correlation Coefficient		Number of
Type				Uncorrected	Corrected <sup>2</sup>	Uncorrected	$Corrected^2$	Vehicles Weighed
SU-2A-4T	KY AASHO MAASHO <sup>3</sup>	0.0415 0.0061 0.0061	0,644 0,030 0,030	0.632 0.030 0.030	0.630 0.030 0.030	0.192 0.190 0.190	0.212 0.198 0.198	12,349
SU-2A-6T	KY AASHO MAASHO	3,1945 0,1787 0,1787	4.121 0.088 0.088	3,758 0,081 0.081	3.752 0.081 0.081	0.411 0.377 0.377	0.414 0.377 0.377	23,389
SU-3A	KY AASHO MAASHO	10.0445 0.3391 0.5290	16.129 0.289 0.440	12.973 0.235 0.363	12.867 0.234 0.362	0.594 0.578 0.564	0.603 0.583 0.568	2,180
C-3A	KY AASHO MAASHO	8.8944 0.6071 0.6071	6.560 0.270 0.270	6.109 0.253 0.253	6.106 0.253 0.253	0.364 0.351 0.351	0.366 0.351 0.351	12,143
C-4A	KY AASHO MAASHO	15,2519 0,8076 0,9872	9.848 0.328 0.435	7.766 0.227 0.302	7.759 0.226 0.301	0.615 0.723 0.721	0.615 0.723 0.721	14,321
C-5A	KY AASHO MAASHO	18.3338 0.7865 1.2088	15.225 0.452 0.705	11.478 0.347 0.530	11.471 0.347 0.530	0.658 0.639 0.659	0.658 0.639 0.659	4,302

 $<sup>^{1}</sup>$ No weight data were available for cars or buses.

<sup>&</sup>lt;sup>2</sup>Negative estimates were transformed to zero.

<sup>&</sup>lt;sup>3</sup>Modified AASHO procedures were used.

## EXTENSIONS OF METHODOLOGY

The legal maximum allowable gross weight on Kentucky highways increased three times during the 17-year study period. Each increase has greatly affected the EWL accumulations on those particular highways to which the increase applied. Such effects are due to (1) a redistribution of the relative vehicle-type percentages, (2) an increase in the loading of vehicles having weight capacities near to or greater than the prior maximum allowable gross weight, (3) the utilization of heavier vehicles which, prior to the change, were either prohibited or were uneconomical to operate at reduced payloads, and (4) a reduction in the ADT. The underlying rationale is that the choice of vehicle type by a carrier is dependent both on the characteristics of the shipment and on the efficiency with which various vehicle types may be operated within the legal constraints of maximum allowable gross weights and permissive vehicle types.

Inability of past procedures to consider the effects of maximum allowable gross weight has doubtlessly led to underestimates of design EWL's. This current reevaluation endeavor offers a means for rectifying this situation in the future. Two distinct problems immediately emerge.

The first relates to how and when the maximum allowable gross weight may be expected to change. Since these are legislative and administrative matters, they are largely beyond the purview of the engineer. At the same time, it is the engineer's responsibility to predict design EWL's based upon all the information that is available to him. While the matter is not dealt with in depth herein, it is recommended that estimates of design EWL's for high-type, multilane facilities be based on a maximum allowable gross weight of 89,000 pounds. This is approximately equal to the allowable gross weight of a C-6A truck. As an alternate suggestion, the current maximum allowable gross weight might be considered to govern the first 10 years of the design life and an increased allowable weight, the second.

The second problem, which is within the scope of this study, is how to modify the proposed methodology to incorporate a maximum allowable gross weight which lies outside the range of historical experience. Preliminary attempts to establish relationships between the maximum allowable gross weight and the traffic parameters of interest, namely, the vehicle-type percentages and the unit EWL's, were unsuccessful. Two pertinent variables that were identified, however, included the ratio of vehicle gross weight to the highway maximum allowable gross weight and the payload capacities of all competing vehicle types. Complicating the analysis were time lags occurring after a change in maximum allowable gross weight. These were thought to be caused by (1) a delay in the introduction of new equipment and (2) a delay in administering the change for specific routes. It was felt that the entire study period was represented by unstabilized traffic redistributions.

<sup>1</sup> These changes may be too small to be actually detected. To illustrate the point, however, fewer C-5A trucks would be required for a given shipment than C-4A trucks due to their increased payload capacity.

A simplified procedure can be used, however, to obtain estimates of the EWL's per 1,000 vehicles for different maximum allowable gross weights. The EWL's for 1,000 vehicles would be predicted for each of the four maximum allowable gross weights and the results plotted as illustrated by Figure 13. The curve would be extrapolated to the future maximum allowable gross weight and the result multiplied by the total number of vehicles expressed in thousands to obtain the final estimate. Figure 13 is based on predictions of AASHO EAL's for the following situation: road-type 2, direction 2, alternate-route 2, service-provided 4, volume 4, and geographical-area 4. The above procedure is recommended for use in the absence of a more refined method.

### SUMMARY

Several empirical methods have been investigated for predicting the pertinent traffic parameters on the basis of anticipated local conditions. These methods were compared with respect to the criteria of accuracy, simplicity, reasonableness, and predictability. The chosen method for predicting vehicle type percentages considers three interacting local conditions which establish the base percentages and multiplicative correction factors for independent analysis of the remaining conditions. Year was excluded as an independent variable for predictive purposes. The chosen method for predicting unit EWL's considers additive factors for the independent analysis of each of six local conditions. Year, season, and service provided were excluded as independent

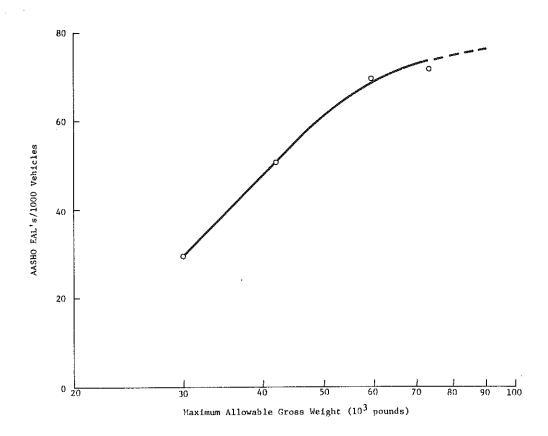


Figure 13. Example Effect of Maximum Allowable Gross Weight on AASHO EAL's per 1,000 Vehicles.

variables for predictive purposes.

Work sheets for predicting design EWL's are included as Appendix F. As such, Appendix F summarizes the recommended procedures and presents the necessary data for computational purposes. These data represent averages over the 17-year study period weighted by the factors of Table 11. An example problem is presented in Appendix G to demonstrate implementation of the recommended procedures.

Appendix F should be used to estimate EWL's for purposes of pavement design except where appropriate data are available for the specific route in question. A method has been given for predicting design EWL's when the anticipated maximum allowable gross weight is in excess of that stipulated in the past. The data of Appendix F may be extended by extrapolation or interpolation as necessary in order to obtain valid estimates. For example, missing entries may have to be obtained by extrapolation or interpolation. Judgment may have to be exercised in other instances, such as for a location at or near the boundary of two geographical areas.

Accuracy of the individual estimates of the traffic parameters, as indicated by Tables 15 and 17, was somewhat discouraging. Nevertheless, the recommended technique represents the best available among those investigated and satisfies the basic requirement for a valid prediction procedure which accounts for the effects of local conditions. A portion of the observed errors is doubtlessly due to inappropriateness of the model. At the same time, other errors remain which could not be diminished by any model. These include (1) errors in obtaining and recording data in the field, (2) errors in coding data and local conditions in the office, (3) errors due to large inherent variabilities in the traffic stream, and (4) errors due to non-random nature of the basic data. In addition, the data are representative only of average weekday conditions and the weight data have been obtained only during the spring and summer months.

The true validity of the proposed model can not be assessed solely on the basis of estimates of the individual traffic parameters. Of considerably more significance is the accuracy of estimates of design EWL's or of estimates of pavement thickness resulting therefrom. These matters are considered in the following section.

## ACCURACY VERIFICATION

EWL's were estimated using the proposed method and then compared to actual EWL's for all stations at which both vehicle classification and weight data had been obtained during the study period. There were 51 such stations representing a total of 225 counts for an average of approximately four annual counts per station. Of these, nine were stations for which 11 or more years of data were available and 18 for which seven or more years were available. Thirtyone of the stations were represented by only one or two years of data.

The first comparisons were made on the basis of EWL's per 1,000 vehicles for the 225 individual counts. Table 18 summarizes the results of these accuracy comparisons. The correlation coefficients are relatively small, which indicates that a large portion of the variability in EWL's per 1,000 vehicles for individual counts remains unexplained.

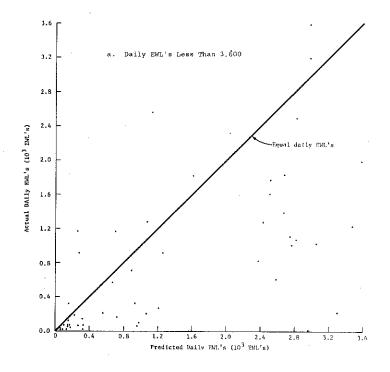
The actual and predicted total daily EWL's were then computed and compared. Figure 14 shows the results of this comparison for Kentucky EWL's. This figure depicts visually the accuracy of estimates of daily EWL's for individual counts.

Table 18 and Figure 14 indicate that the proposed method for predicting EWL's, while superior to all methods investigated herein, does not enable high accuracy in predicting EWL's for individual counts. This is due in large part to the extreme variability in the actual EWL's that are accumulated at individual stations from year to year. Such variability is depicted on Figure 15a for

TABLE 18

ACCURACY OF ESTIMATES OF EWL'S PER 1,000 VEHICLES
FOR 225 INDIVIDUAL COUNTS

Type of EWL	Actual Mean	Standard Deviation	Standard Error	Correlation Coefficient
Kentucky (EWL's/1,000 vehicles)	1535.4	1405.3	1173.1	0.55
AASHO . (EAL's/1,000 vehicles)	82.4	54.5	42.4	0.63
Modified AASHO (EAL's/1,000 vehicles)	96.9	70.8	52.2	0.68



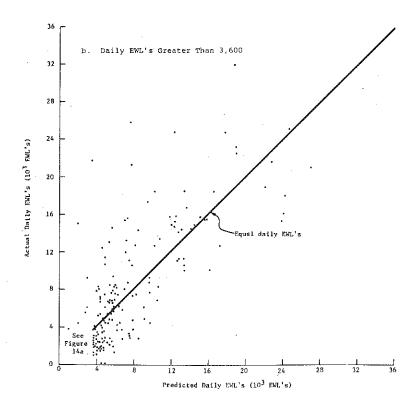
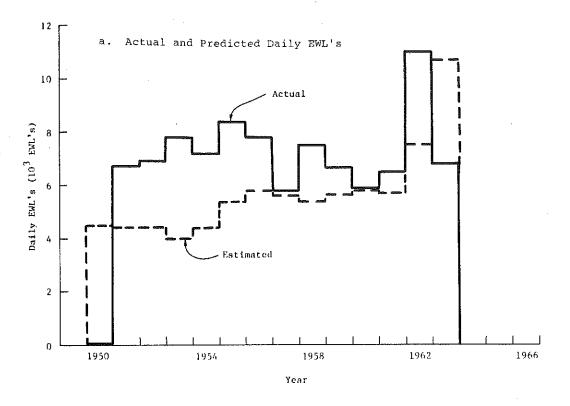


Figure 14. Comparison of ACtual and Predicted Kentucky
EWL's per Day for 225 Individual Counts.



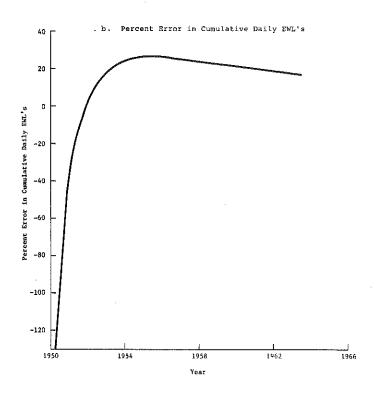


Figure 15. Variability in Kentucky Daily EWL's at Station 8.

Station 8, for which 14 years of data are available. Certainly no predictive procedure can be conceived that would be able to duplicate the actual year-to-year variations that are obvious from this figure. Figure 15a suggests, however, that, if the daily EWL's were accumulated over a period of years, the actual and predicted accumulations might tend to converge. This led to the construction of Figure 15b which shows, for the same station, the percent error in cummulative daily EWL's as a function of year. The percent error was computed by dividing the difference between the actual and predicted values by the actual value. Following a six-year period of initial instability, the percent errors tend to be reduced as the number of years increased. By extrapolation, the percent error at the end of a 20-year design period would be about 6 percent, which certainly represents a tolerable error.

Figure 15b lends support to the hypothesis that the proposed predictive methodology becomes more accurate as the predictive period increases. This is of extreme significance since most flexible pavement designs in Kentucky are based on a 20-year period. Curves similar to that of Figure 15b are shown in Figure 16 for six of the nine stations for which 11 or more years of data have been accumulated. This figure also shows that the percent errors tend to become stablized and reduced as the time increases.

As a further means for validating the proposed methodology, the influence of the accuracy of the EWL estimates on the accuracy of the design pavement thicknesses was also investigated. First the actual and the estimated EWL's for each of the 51 locations were extrapolated to 20-year accumulations. These are shown in Figure 17. Then the combined flexible pavement thicknesses including base and pavement were determined (10). These determinations, which are summarized in Figure 18, were based on an arbitrarily-selected design CBR of 5. Differences in the thicknesses based on estimated actual and predicted EWL's seem rather large at first glance. However, it should be recalled that actual data were available for periods of only one or two years for 31 of the 51 stations. This would, of course, decrease the reliability of the estimates of 20-year accumulations of EWL's. Figure 18b suggests that the percent error for stations with data for a 20-year period would be about 2 percent.

In summary, it is concluded that the proposed method for predicting design EWL's is sufficiently accurate for use in designing flexible pavements. It satisfies the remaining criteria of simplicity, reasonableness, and predictability and provides a suitable means for ascertaining the influence of local conditions.

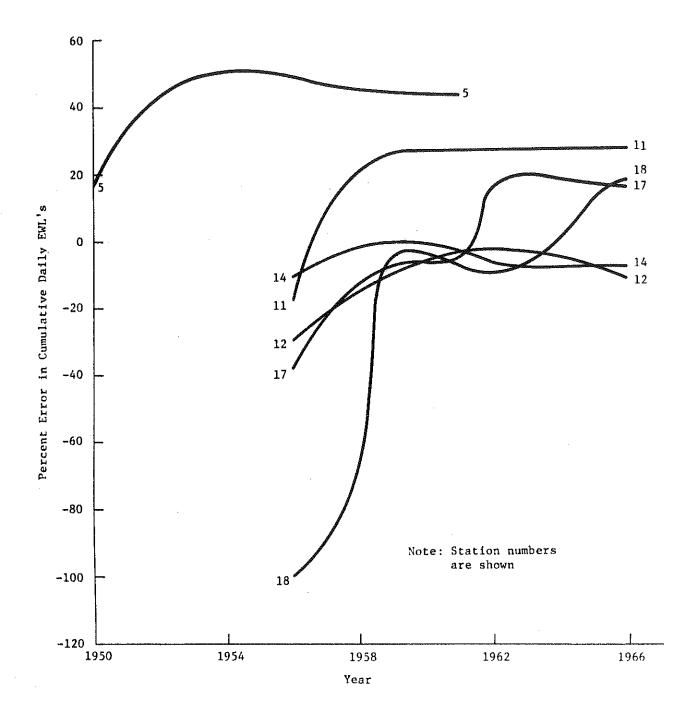
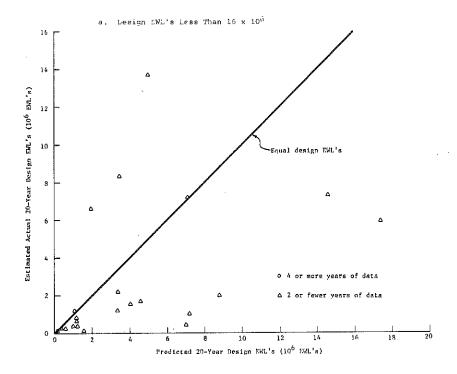


Figure 16. Percent Error in Kentucky Cumulative Daily EWL's as a Function of Time.



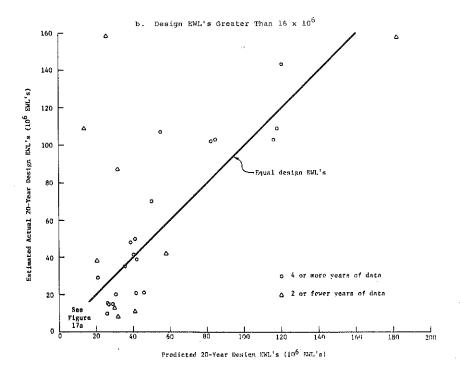
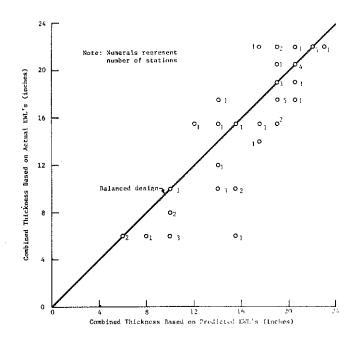
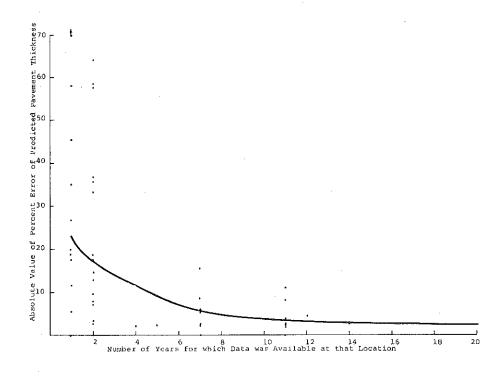


Figure 17. Actual Versus Predicted 20-Year Design EWL's for All Stations.



(a)



(b)

Figure 18. Flexible Pavement Thickness Based on Actual and Predicted 20-Year EWL Accumulations.

### SUMMARY

Difficulties in obtaining reliable estimates of EWL accumulations for flexible pavement design purposes led to the initiation of this study in 1963. When EWL estimates at specific locations were compared with actual EWL accumulations, major discrepancies were often noted. These discrepancies were believed to be associated with the inability of the predictive procedure to differentiate among many of the routes in other than a qualitative manner.

The prerequisites which were established as a basis for comparing alternate predictive procedures included the following:

- 1. The predictive model should consider as many of the relevant local conditions which determine the composition and weights of the traffic stream as possible,
- 2. The predictive model should make full use of all available vehicle classification and weight data, and
- 3. The predictive model should possess the qualities of simplicity, reasonableness, predictibility, and accuracy.

Evaluation of the methodology currently used in Kentucky led to the search for a more responsive empirical method of prediction. It was assumed that sufficently accurate estimates of ADT would be available and, therefore, could be excluded from consideration. Furthermore, the analyses was restricted to rural areas for which the bulk of data was available. The significant traffic parameters were identified as the percentages of the various vehicle types and their unit EWL's. The local conditions which were found to significantly affect the traffic parameters included road type, direction, alternate route, service provided, traffic volume, maximum allowable gross weight, geographical area, year, and season. Analyses were then made to find a suitable empirical method for predicting the traffic parameters on the basis of an analysis of the pertinent local conditions.

The chosen method for predicting vehicle-type percentages consists of a set of basic percentages determined jointly by road type, volume, and maximum allowable gross weight and a series of multiplicative correction factors determined independently by direction, season, alternate route, service provided, and geographical area. Independent predictions are made of the percentage of each vehicle type and the results adjusted so that the sum equals 100 percent. The chosen method for predicting unit EWL's is based on a multiple regression model that considers all of the above local conditions, except year, season, and service provided, in an additive fashion. Adjustments are made so that no estimate yields a negative value. Procedures are provided for estimating Kentucky, AASHO, or modified AASHO unit EWL's.

The recommended methodology, which is presented in Appendix F, was found to provide a suitable means for predicting EWL accumulations. In no case, however, should the recommended methodology be used if valid traffic data are available for the specific route in question.

### RECOMMENDATIONS

The following recommendations for implementing and extending the efforts of this study are presented for consideration.

- 1. The proposed methodology for predicting EWL's for rural highways in Kentucky should be adopted for purposes of flexible pavement design. This method has been shown to be a valid predictive tool which can account for the effects of local conditions.
- 2. Twenty-year predictions of design EWL's should incorporate the effects of probable changes in maximum allowable gross weight on high-type, multilane highways. Maximum allowable gross weight has been found to significantly affect EWL accumulations. Four different maximum allowable gross weights have been in effect on Kentucky highways during the 17-year study period and future changes are likely to occur.
- 3. Analogous methodologies should be developed to enable valid predictions of EWL's and associated traffic parameters in urban areas. No method currently exists for accurate predictions of design EWL's in these areas.
- 4. The data banks developed as a part of this study should be continually and routinely updated and maintained. This is essential not only to facilitate future reevaluations of EWL predictions but also to provide the capability for immediate and accurate recall of traffic data for a multitude of engineering purposes.
- 5. Responsibility for the maintenance of up-to-date data banks should be assumed by the Division of Planning which now has overall responsibility for data collection systems.
- 6. Formats of the data banks should be thoroughly reviewed and revised to be compatible not only with past data but also with possible future innovations and changes and to provide a rapid means for future updating. The formats now used were selected primarily to facilitate the objectives of the current study. Certainly the capability for handling new vehicle types such as double bottom trucks and new axle types such as tri-tandem axles must be provided. This might also require certain changes in the current data collection systems.
- 7. A comprehensive review of current methods for acquiring vehicle classification and weight data appears desirable. The analysis reported herein was hampered by the non-randomness of data caused, in part, by the emphasis which has been placed on the permanent loadometer stations. A minimal number of permanent, fixed stations used to ascertain long-term trends supplemented by additional randomly selected stations used to provide maximum coverage appears advantageous.
- 8. Investigations should be conducted to ascertain the seasonal variations, if any, of average vehicle weights and unit EWL's.

- 9. An independent means should be sought for predicting changes in vehicle type percentages and unit EWL's anticipated as a result of future increases in the legal maximum allowable gross weight. Not only would this increase the credibility of future predictions but it would also promote improved understanding of the evolving structure of the traffic stream.
- 10. The current EWL-calculation procedure which neglects the possible effects of differential lane and directional distributions should be subjected to close scrutiny. Neglect of lane distribution can possibly lead to overdesign on multilane facilities while neglect of directional distribution can possibly lead to both overdesign and underdesign depending on the direction of flow. Both the Asphalt Institute (24) and the Portland Cement Association (23) provide a means of correcting for the effects of lane distribution in their design methods.
- 11. It is imperative that the contribution to EWL accumulations by buses be studied in some detail. Despite the fact that fully loaded, commerical buses contribute significantly to EWL accumulations, no detailed data on average bus weights are available.
- 12. Future reevaluations of flexible pavement design procedures must provide a sound basis for justifying or altering the procedure for neglecting to distinguish between single and tandem axles. Both theory (16) and the results of road tests (11) have shown that the destructive effects of single and tandem axles are not identical.
- 13. Periodic maps of annual EWL accumulations on Kentucky highways would be useful for providing an up-to-date source of information for analysis and design purposes. While the preparation of such a map would currently require excessive expenditures, such an effort would be a small task for a computerized system. It is, therefore, recommended that increasing use be made of high speed data processing systems for the storage and analysis of traffic data. Such a system would provide immediate and accurate information concerning a variety of traffic parameters.

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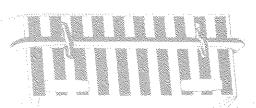
# APPENDIX A

HISTORICAL SUMMARY - AVERAGE PERCENT TRUCKS AND AVERAGE NUMBER OF AXLES PER TRUCK

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4000-7999 VPD 1000 DR MDRE VPD	11.07	15.08	16.78	12.99	15.26	14.78	14.34	13.34	11.95	11.10	16.19	14.44	1,2	17110		T-HA /	17.56	
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JZ.BI	12.62	76.91	54.71	21.20	77 6 E	:05 61	97.61	35.83	58.71	30.15	71.02	60.81	75 91	77 71	99 81	16.51	65.19	4000-7999 VPD
9.91	84.71	75.91	24,61	70.71	36 7T	47 .81	114.71	£8.61	11.81	15.41	11.11	58.91	12,11	20 91	11.51	11.73	05.5	s day eeee-oods
										16.81								
										19.21								
8.01	92.0	91.10	4.4	50.51	2.0	01.01	85.EE	3-0	FF.9	G1*11	U-U	FE782	97781	£9.01	0.0	0.0	0.0	OdΛ 66∌÷0
																		IBNCKZ
																		AVERAGE PERCENT
ирчү	9961	496T			2961	1961	3961	76661	6651	1681	9561	3661	7961	1623	2561	1561	0561	
סרר																		
					e North Co Horsenson	gradeni Nggara		unity) Tieta	515	MH9 DT	าษากษา			randirida Albaniai		a yara Wasan		
								21 ONV		ŭ lo		510 X4	нісін					
					18.0	i seri			1 1 20	N KENI	Matera							



HISTORICAL SUMMARY - AVERACE
AXLELOAD DISTRIBUTION

APPENDIX B

.228020 .228020 .2234 .21294	10 0 10 0	10.0 10.0 10.0	50.0 50.0 40.0 60.0	10.0 20.0 E1.0 80.0	\$1.0 \$1.0 \$5.0	12°1 12°1 12°1 1°29	50.2 20.2	10.8 10.22 55.01	81.9 91.8 77.8	56.1 56.1 70.1	19.6 56.6 50.7	81,51 81,61 81,61 81,54 81,54	51.18 60.44 94.84	# 1000 1000 1000 1000 1000 1000 1000 10	
81101 9506	50.0	2010	0.18	0.16	01.1	16°Z 1'25	11.8	96 ° 5	10.5	92°5 26'5	16.2 64.2 74.2	02.11 87.51	06.42	666=005 669=0	
616	0.0	0.0	0.0	0.0	0.0	26-1	85.1	96.1	68.5						VEARS.
12624	0.0	0.0	10.0	60°0	0*25	79°1	58 °5	11.30	46.01	10.6	21.51	86.91	85.05	8000 PR MURE \$000 PR MURE \$1000-138	
05EST	8:0	0.0	90.0	12.0	26.0	07.0	06,5	60.51	11.11	66.0	11,20	95 R1	26.45 26.45	\$662-0007 \$000-1000	
805	0.0	0.0	0.0	0.0	0.0	0,0	0.0	65 0	87.5 0.0	0.0 0.0	01 9 0 0	9°0	0.0	665-005 665-0	
0.0	0°0 .	0.0	60.0	0°0 50°0	0°0	59-1	0.0	51-11	70*01	87.8	84.11	69*8I	22.16	SHATTA TIV	9961
81551 79271 8777E	0°0	0.0 0.0	40.0	0.0 0.0	65.0	17.1	17.2	11.01	61.61 16.6	10.26	10.59	17,81	89.75 97.56	3ADM SO 0008	
*1251	70.0	0.0	70.0	0.0	0.0	85.5	15.8	78.5 54.11	60.5	50.1	15.90	29'6T 95'6T 0'0	71,58 71,58	6665-0007 6661-0001 666-005	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	9.0	0.0	664-0	596T
0797E	0.0	0.0 E0.0	0.0 0.0	81.0 85.0	. 99'0 -	49°1	0219	£Z*6	56'8 £7'6	15.1	59°01_	55°21	80,86 80,7£	SOOD OR HORES	
4553	0'0	0.0	0.0	0.0	21.0	96*0	16.9	07.51 6.50	66 21	68 9	25. 21 E5 D1	18.38	18.8E	5662-0005	
*9262 *DSET	11.0	90.0	05.0 08.0 61.0	£1.0	55.0	52*T	26.1	50.4	25.7	92.5	25.7 13.7	17,21	24.67 67.88	666-005 666-0	
*569 *2002£	0.0	0.0	0.0	0.0	75.0 0.0	70.5 71.5	92:1	92.01	47.6	87.5		69°41		אלד אַסרמאָנּבּ פססס מאַ אסענּבּ	*96T
d*n	0.0	0.0	0.0	86.0	05.0 05.0	D.0	9,36 13,7 0,0 7,83	0.0 20.0	47.6 6.0	05.7 0.0	95.01 0.0 58.01	0.0	61.5E 0.0 85.45	666Y-0005	
9118 9118 92828	0.0	0.0	0.0	80.0	0.0	86.5 86.1	D.0	10.01	0.0 0.7	0.0	U.0	0.0 25.71	0.0 0.0	\$000-7666 \$00-7666	
0.0 0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	667-0	E961
5023*	€0.0 €1.0	70.0	50*0	91*0	80.0	72°0	00*5	96.8	91.6	25 °8	95.11	66.71	99.76	BOOD OR HORE ALL VOLUMES	
1619 LE19	50.0	0.0	50.0 50.0 85.0	20.0	91.0	- 05*0	64.2 64.2	16.1	59°6	98.6	17,51	98.81	99'9E 98'9E	666E-0007	
0.0	0 0	0.0	0°0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	6661-0001 666-009 665-0	
0*0	.0.0	0.0	0.0	0-0	0.0	0.0	0.0	0-0	D*6	55.7	0.0	0.0	65.00	SEMPLE VOLUMES	Z961
56318 11328 11328	0.0	0 0 0 0	20°0.	60.0	02°0	91.1 91.1	48.4 19.4	57.8 88.6	90.7 64.8	57.8	17'9	51.71 51.61	11.95	8000 OS MORE	
6795	0.0	0.0	0.0	0.0 11.0 0.0	0.0	6.0 56.1 70.2	10.E1	15.11	45.E	ZE *B SB * 7	90.7 52.11	£0.01	9E SE	666E-0002 666T-0001	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.9	0.0	0.0	0.0	0.0	0.0	0.0	964-00e	1961
2524	0 0	90°0	10.0	90.0	0.0 0.0	81,1	10.4	57.6	96 5 27 DT	15 1	96.6	69 51	44.99	BOOD OR MORE	
265 7 L 265 7 L	0.0	10.0	60.03	01.0	50°0	11.1	66.5	75.8	16 6	7H - 0	76.8	£9.21	26 66	9995-0005	
0*0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	6.0	1000-1488 200-888	
D*0	0.0	0.0	0.0	0.0	0.0	0*0	00	0*0	0.0	0.0	0.0	0.0	0.0	665-0 VIT ADCOMES	0961
1846TS	0.0	0.0	0.0	01.0	9E.0	95°2	06.4 22.7	96'8 96'8	99.T 50.P	70 L	11.2	28 ET	95'27 95'6E	980 AD 0008	
11961 11961	0.0	0.0	0.0	£0.0	2.0 52.0	87-1	18.8	57.01	Z7'6	F0.8	40.4	57.21	68'E' 1E'85	666E-000Z 666E-0001 666-005	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	665-005 665-0	6561
26338.	0.0	0.0	10.0	90°0	11.0	66*1	14.6	76.01	GE "H	65.63	66.0	98'81	0.0	SOOO OR HORE	2701
* 5564 I	0.0 0.0	0.0	20.0 0.0	10.0 E0.0	41.0 9.0	0°0 60°2	0°0 59°6 51°6	69.01	£5*9	72.8 12.8	50.8	55'61	64.25	666E-0005	
1067L 1706	0.0	0.0	0-0	0.0	0.0 25.0	69.1	76*9	21-01	55.0	17.9	51.0	25,51	08.62	5661-0001 566-005	
0,0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 ° D	0.0	0-0	669-0 971 AUTONES	2561
*59E0E *0*0 *18951	0.0	0.0	90.0	0.0	0.0	0°0 98°1	0.0	0.0 88.7	0.0 0.0	0.0	0.0 21.9	0.0	0.0	980H RD 0008	
9968	50.0	ED .D	11.0 0.0	0.0 60.0	91.0	87.1 88.1	49.E	46.6 44.7 66.2	£6,8	15.7	25.8	0Z 71 0Z 71 20 11	55'85	5000-3444 1000-1444	
9071	0.0	0.0	71.0	0.0 01.0 71.0	69.0	65"1 17"0	49°1	57°2	3.02	59°5	66.4	15°8 19'8	18,5T	666-009 667-0	
BOSEE	0.0	10.0	0.0	20.0	01.0	66.0	61.9	19'9	68 '8	50.5	14.2	10.90	15.02	BGGO DR HDRE ALL YOLUNES	1261
12754 163664 123,	0.0	0.0 50.0	0.0	20.0 50.0	£0.0	98.0 20.1	25.7	60.8 0E.9	16.8	92.49 17.8	91.6	66 DT	£9°05	6662-0007	
0.0 0.0	0.0	0.0	0.0	0.0	0.0	57.1	46.8	78.8	01.01	11.4	65 E	0.0	0.0	6661-0001 666-009	
0.0	0.0	0.0	0,0	p.*o	0.0	0,0	0.0	0.0	0.0	0.0	0.0	0.0	26,88	0-499 VII AUFINEZ	9961
0°0	0.0	0.0	0.0	90.0	60.0	0.0	0.0	0.0	0.3	98.2	0.0	p.0	0.0	9804 AD 0008	
0.0 .0S72 .18021	0.0	0.0	0.0	90°0 60°0	0.0	9E*T	99.4	86-9 86-9	57°L	76.2	0.0 10.2	87.01 87.01	60.82 0.0	666F-0008 6661-0301	
0.0	0.0	0.0	0.0	0.0	0.0	0.0 0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	665-005 665-0	****
12981	0.0	6.0	0.0	CD-0	91.0	D6.0	16.9	21'8	91.9	06.4	27.e	59*9	55.05	SEMMIDA TIV	STET
0°0	0.0	0.0	0.0	6,0	0.0	0,0	9.0	80.8 0.0	0°0	9.0	0.0	0.0	0.0	9967-000A 3ADM AD 0008	
9868	0.0	0.0	010 .	0.0	EE'O.	20'1	98'9	0.0	11.1	0.0 82.4	96'5	0.0	0.0	5665-0007 5661-0001	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	665-005 665-0	7561
18119	0.0	0.0	10°0	50.0	90.0	0.0	61'9 0'0	06.1	0.0	98*5 0*0	55.2	0.0	05.92	SODD DR MORE	
, EEOT	0.0	0.0	20.0	80.0	11.0	46.0	96°5	24.7 01.7	7.71 7.21 0.0	90°9	££*5	91.6	SE 65	9904 - 0004 9000 - 9008	
0.0	0.0	0 0 0 0	0.0	0.0	0.0 0.0	0.0	0.0 0.0	0.0	0.0	0.0	0.0 0.0	0.0 0.0	0.0 0.0	6667-0001 666-005	
******	0.0	0.0	0.0	50.0	\$1.0	77.0	65*5	78'1	40.7	05-5	81.2	00.7	86.08	0-444 VEF ADERHES	E 561
9866	0.0	0.0	0.0	0.0	0.0	0.0	0*0	0.0		91.5	0.0	Q*D	72, 42 72, 54	9000 DB WDME	
*9668 0*0 0*0	0 0	0.0	0.0	90.0	91.0 81.0	11.1	68 S	0.0	51.7	0.0	16 7 D'0	0.0	0-0	5665-0005 1666	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0,0	0.0	0.0	0.0	665-309 667-0	766*
0.0 18731	0.0	0.0	0.0	10.0	0.0	1°03 1°57	0.0 56.2	15.1	0.D	95.4	10.0.	05.9	80.23	ALL VOLUMES BOOD ON MORE	256t
0.0 PE2P	0.0	0.0	0.0	0,0 0,0	E0.0	58*0	3.87	52.T 02.T	£7.7	00 9 89 9	17 S	1211	20.E8	6661-0007 6661-0001	
0.0	0.0	0.0	0.0 0.0	0.0	0*0 0*0	0.0	0.0 0.0	0.0	0.0	0.0	0.0	0.0	0.0	666-0DS	
*0*161	0.0	0.0	0.0	0.02	60.0	26.0	05.1	0.0	96*1	15.5	0.0	0.0	0.0	665-0 53H010A 119	1561
9271	0.0	0 0	0.0	6.03	6-0 F1-0	0.0	0.0	0.0	28.1	0°0	0.0	0°D	92.61	8600 GR NORE	
11511 0'0 0'0	0.0	0.0	0.0 0.0	9.0 9.0	90.0	0.0 TE.D	. 18°0	0.0	5,06	0.0	1.53	95.9	9.0	6665-0007	
0.0	0 0	0.0	0.0	9.0	0.0	0.0	0.0	0.0	0'0	0.0	0.0	0.0	0.0	664-005 664-0	04.1
a sister	86666	66687		66692	66627	66607	6668T	66691	5669T	15668	66601	8444	DGOT		Ideg
\$ 3 1 2 4	04	0.1	01	oï -			000TJ				01	OT.			

ZYAHAIN JARUP

.4E67P	0.0	10°0 0°0 10°0	0.0	90°0 0°0 21°0	61.0 6.0 65.0	0'0 9''1 76''I	8,22 9,0 0,0 5,5	05,11 0.0 18,01	10,01 0.0 9,22	0.0 27.1 27.1	67'8 0"0 67'6	95.61 0.0 85.61	0.0 11.00 90.52 90.52	8000 OK HOKE 4000-1466 2000-1466	
96517 1,991 0.0	0.0	0.0	0.0	0.0 0.0 55.0	0.0 0.0 0.0	95°1 0'0 25°0	85.5 82.5	09'II 56'5 0'D	19'5 0'0	09.5	0.0 17.8	46.1 0.0	0.0 64.88	6661-0001 666-009 669-0	FARSI
						68.1	7E *9	17°E.L		ÇŖ ₽	12.18	20,11	15.85	VIT ADEQUES	ALL YEARS
*1694 0*0 *9915	0.0	0*0 0*0	0.0	0.0	0'0 52'0	0.0	0.0	0°0 55°21	0.0	0°0	0'0 89'1	0.0 67.31	28.75 28.96 0.0	2000-3999 4000-7999 8000 08 HORE	
0.0 0.0 2466.	0.0	0.0	0.0	0.0	0.0 ET.0	0.0	86'E 62'11 0'0	0.0	0.0	0.0	0.0 0.0	0.0	0.0	6661-0001 666-009	
0.0	0.0	0.0	_0.0	0.0	0.0	0-0	82"7	25.11	29'11	0.0	0.0	9.01	9.0	0-466 VICT AUF INE 2	9961
*1508 *E505	0.0	0.0	0.0	0.0	61.0 12.0	26.0 50.0	0.0	0°0 20°01	0°0 71.21 0°0	0.0 EE.D1	0.0	0.0	52.55 70.75	\$000 OB HOKE \$000-1666	
0.0 0.0	0.0	0.0	0.0 11.0	0.0 0.0	0.0	0.0	0.0	0.0	0.0	0.0 85.8	0.0 72.51	0.0	0.0	6661-0001 666-005	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0:0	27.51	32.91	53H01DA 11Y	596 T
.96711 .96511	6.0	90'0	0.0	0.0	0.0 0.0	0.0 0.0 11.1 0.0	0.0 18.7	0.01 51.01	12,79	0.0 0.0 0.0	0.0	0.0	79.85 0.0	980# 8D 0008	
9615	0.0 0.0	0.0	0.0 0.0	0.0	0.0 0.16 0.16	0.0 E0.1	0°0	95.1 20.15	70.8 70.8	77.7	50°24 0'15	65.21 25.25 71.79	99.1E	566E-000Z 566T-000T 666-004	
4011	0.0	0.0	D*0	0.0	0.0	81-1	0_	0.0	17.2	14.1	£1.5	. 00°5 E9°51	05.85 DE.01	214 VOLUHES.	596I
0,0 0,0 18ST	0.0	0.0	0.0	0.0	0.0 0.0	\$8.5 0.0 61.5	0.0 61.01	0.0 15.21	0.0 0.0	0°0 0°1	0.0 0.0	0°0 10'51	0.0	8000 06 MD8E	
0.0	0.0	0.0	0.0	0.0 91.0	0.0 26.0	0.0	0.0 70.0	96,21 0,0	0.0	0.0 0.0	0.0	0.0 ET.31	0.0	1000-1666 200-1666	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	VIL VOLUMES	£951
0769	0.0	0.0	0.0 0.0	0.0	0°0	0.0	0.0 0.0	0.0	0.0 22.11	0.0	85.9 0.0	0.0 E3.81	\$5.0E 50.0 0.0	8000 ON HORE	
2505 .888£	0.0	0.0	0.0	0.0	0.0 0.0	0.0	0.0	69°ET	0.0 0.0	0.0 0.0	0.0 2.0	99*91 95*91 0*0	0.0 42.2£	566E-000Z 566-1660 500-666	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	9.0	0.0	664-0	<u>296</u> ₹
. 2868	0.0	0.0	0.0	0.0	0.0	0.0	99-01	09'51 0'0 50'51	92.91	10.7	0.0 0.0	0.0 0.0 16.54	90*0£ 0*0	SECO DE MORE SECO DE MORE VOCO DE MORE	
. 6581 . 7526	0.0	0.0	0.0 0.0 0.0	0.0	0.0 6.0	0.0 0.0	95.V 67.51	0.0	76.51 41.6	76'9	0.0 7.59	E1.81	88.62 81.08	5000-1466 1000-1466	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	665-005 665-0	1961
9605	0.0	0.0	0.0	0.0	0.0	0.D 9.0	0.0	92*51	65°01	91 9 0 0 77 /	0 0	17.46 13.20	0,0 86,66	8000 OR MORE 8000 OR MORE \$10 A000-1999	
10961	0.0	0.0	0.0	0.0	0.0	0.0	72.E1 ST.E	0,0 11,63	99'1 99'1	01.7	56.6 56.6	74.61	0.0 91.15	1000-1466	
0*0 0*0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0,0	666-005 665-0	0961
*8615	0°D	0.0	D*0	0.0	72.0	5.26	*!*!1 0*0	0,0 E8,E1	15.01	16.2	65.2	11.21	9875E	BEGG OR MORE	
*6555 *6951 0*0	0.0	0.0	0.0	0.0	0.0 78.0	86.E	66.0 76.11	09.41 04.41	67:Z1 92:9 0:0	2.83	61 5 0 D	65.E1	95.5E	5000-3444 5000-3444 1000-1444	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	666-005 664-0	696t
*E*15	0.0	0.0	0.0	50.0	0.0	72°Z	65*41	16.41	20.8	26.0	96.4	12.21	0.0 PE.9E	SOOO ON WORE	0301
*+982 *8427	0.0	0.0	0.0	0.12	0.0	92-1 95-1	71.55 71.55	0.0 0.0	65.T	96.4 94.5	00 9 E9 C	85 21 9 0	19'15 56'96	5000-13466 5000-13466	
0.0	0.0	0.0 0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	666-00⊆ 66 <del>7</del> -0	8561
8 t o 8	40.0	£0.0	11.0	Z1:0	0.0	E6-1	0.0	0.0 67.7	11.8	0.0 0f.7	55.7	50.61	91.00	BOOG OR MORE	0301
	90.0	0.0 0.0	0.0	01.0	1.22 1.22	65.5 2.59	88.7 87.7	50.6 76.1	75°85 0°69 1°95	50.7 80.2 80.2	61.1 ES.1	10.28	16 °C v	5000-3888 5000-3888 7000-1888	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	950	0.0	0.0	0.0 94.0	0 0 56 5	9.01 0.9	0.0	666-005 665-0	1561
0.0 .03£7	0.0	0.0	0.0	E0.0	11.0	58.0	96-9	19.6	6.0 0.0	0.0	0.0	91.01	87'67 0'0 54'15	POGG OF HORE	5901
*82++ *1962 *0*0	0.0	0.0	0.0	0.0	0.0	58.0 78.0	81.a 70.1	67.6	25.6 0.0	61°8 0°0	0.0 ES.7	26 11 0 0	57.12 80.32	5661-0007 5661-0007	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 0.0	0.0	0.0	0.0	0.0	0.0	0.0	666-009 669-0	4213
3920	0.0	0.0	0.0	0.0	90.0	66.0	96.€	0.0	010	15.6	18.0	71.8	0 D	SOOO OF HORE	1956
18917 19917	0 0	0.0	0.0	0.0	-51.0	02.1	57.5 0.0	19.4	81'8 0'0	88.2	50.0 75.8	66.8 76.8	65 15 0 0	1000-1999 2000-1999	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	666-009 664-0	
**156	0.0	0.0	0.0	0.0	79.0	50*1	SE*E	05.2	01.1	8-67	46.8	62.0	£0.82	VET ADEDNES	566T
0°6 '516I	0.0	0.0	0.0	0.0	0.0	0.0 1.51 0.86	55.5 55.5	0°0 65°5	65.4	13.P 85.6 0.0	0°D 09'9 92'5	97.9 0.0	26'19 86'65	8000 06 HORE \$000-1666	
0-0 0-0	0.0	0.0	0.0	0.0	0.0 0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 ° 0 D.1 0	0.0	666-005	
0.0	0.0	0.0	0.0	0.0	90.0	82.0	0.0	0.0	51.2	0.0	0.0	08.7	0.0	665-0 \$3W010X 11V	<del>5</del> 661
. 2871 0,0	0.0	0.0	0.0	0.0	0°0	0.0	0.0	26.5	0.0	0.*0	0.0 56.57 76.52 9.0	0.0	56.14 0.0	4000 0K WORE 4000-3666	
0.0	0 0	0.0	0.0	0.0	0.0 6.0 6.0	0°0	0.0 79.E	0.0	0.0 0.0	96'S 22'9 0'0	0.0	6 0 0 0	0.0	6661-0001 666-005	
*8558	0.0	0.0	0.0	0.0	7 £ * 0	08.1	65.5	0.0	0.0	66.T	19.9	7E.0	0.0	24U JOV JJA	1953
0.0	0.0	0.0	0.0	0.0	0.0 0.0	95.0	61.1	10*7	66.0	08.7	76.1 0.0	19.5	0.0 0.0 0.0	8000 08 HOSE	
0*0 0*0	0.0	0.0	0.0	0'0 0'0	0'0	0.0 0.0	0°0 0°0	0.0 0.0	0.0 0.0	0.0	0.0	0.0	0.0	566E-0007 6661-0001 666-005	
*8266	o*b	0.0	0.0	0.0	0.0	0°0	0.0	19.8	0.0	0.0	0.0	0.0	0.0	0-466 VET ANTONES	7561
0.0	0.0	0.0	0.0	0.0	61.0	22.0	0.0	10.6	52.2	0.0	60.6	91.8	0.0	9804 AD 0008	
0*0 0*0	0.0 0.0	0.0	0.0	0.0	0.0	0.0 0.0 18.0	0.0	0.0	0°0	0.0	0.0	0.0	0.0	6661-0001 666-005	
0°0 	0.0	0.0	0.0	0.0	01.0	0.0	0°0 0°0	0°0 65°2	80.E	0.0	0.0 0.0	0.0	0.0	667-0 \$390704 179	1661
19991	0.0	0.0	0.0	0.0	6.0	0.0 0.0 0.0	0.0 17.0 10.1	96.1	1.30	1616	0.0	95.T 0.0 T0.T	0.0 62.81 0.0	9900 DR MORE 4000-1499	
1882° 0°0	0.0 0.0	0.0	0.0	0.0	0.0	0.0 75.0	0.0 8E.1	0.0 E1.E	0.0	16 °C	0.0 0.0	0.0 88.4	0.0 TT TT	5000-3888 1000-1888 200-888	
0.0	0.0	0.0	0.0	0.0	6.0	0.0	0.0	0.0	0.9	0.0	0.0	0.0	0.0	667-0	DS6I
	66665	66682	56692	66697	66622	56602	66681	8669T	666+1	66621	66601	666B	1000		

1985	*95196	0°0	10.0	2010	£0.0	16.0	77°1	££*5	89-8	29*6	T0.8	01.6	05.21	91.14	ALL VOLUMES	
The column   The	29390	0.0	10.0	20 0	40.D E0.0	01.0	9£.5	/115	15.7	62.T	15.6	55.9	70*11	51.56 94.52 91.52	\$000~3888	
Color	• 9£ L	0.0	0.0	E5.0	0.0	79.0	12.0	1111	15°Z	70°E	56°E		42.01	\$3.03	666-005	AEVHZ
The color	,2119	0.0	0.0	+0*0	70.0	65.0	25'1	15'7	00-11	56.51		55.51	94*12	67 tZ	ALL VOLUMES	Tiv
Color	0.0	0.0	0.0	0.0	0.0	60.0	62.0	BI.E	96.01	16*21	10.38	0°0 65°EL	55°2Z 06°51	21.25	6664-0009	
Color	. 6.0	0.0	0.0	0.0	0.0	0.0	9.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	666-D05	
The color   The		0.0						11.9	61.21		95*01	50*21	80.81	26.42		9961
Color	*5955	0.0	0.0	0.0	0.0	0.0	0.0	0°0	0.0	0.0	0.0	0.0	21.01 0.0	PZ.ES	6667-0002	
99 99 99 99 99 99 99 89 109 99 89 129 699 895 895 895 895 895 895 895 895 895 8	6*0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.3	0.0	0.0	0.9	0.0	666-0091 666-009	· -
The color   The	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0	0.0				596 l
The color   The	0.0	0.40	0.0	0.0	0 0	9.0	61°D	g-p	D*D	0.0	0.0	12,29	0.0	0.0	9997-000+ 390M 90 0008	
**************************************	*666	0.0	60.0	0.0	£2.0	00	E 5" 1	£8.6 64.0	69-1	69.4	5*86	97.8	15° 51	88.12	6661-0001	
Test	611	0.0	0.0	0.0	0.0	0.0	05**	98-Q	15'2	74.0	17"2	4,90		B1 \$4		<del>5</del> 961
Color	6.0	0.0	0.0	0*0 90*0	0.0	0.0	0.0	0.0	O.D	0.0	4116	0.0	68.05	11.92	6661-0007	
\$\frac{1}{2} \begin{align*}{c c c c c c c c c c c c c c c c c c c	6*6	0.0	0.0	0.0	0.0	0.0	0.0	6.0	0.0	0.0	0.0	0.5	0.0	0.0	666T-000T	
The color   The	0.0	0.0	0.0	0.0	0.0	0.0	D-0	D-0	0.0	0.0	0.0	0*0	0.0	0.0	669-0	£961
1.   1.   1.   1.   1.   1.   1.   1.	0.0	0.0	D.D	0.0	0.0	0.0	51'0 0'0	0.0	0.0	0.0	0.40	0.0	0.0	0.0	3AUM RD 0008	
Color	19671	0.0	0.0	0.0	0.0	75,0	55,0	40.5	£1-9.	0.9	0.0	75.11	68.91	0.0	5000-3333 1000-1333	
Test	0.0	0.0	0.0	0.0	0.0	0,0	0.0	Ð-D		0.0	0.0		0.0	0.0	666-00S	Z961
GEO. 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	0.0	0.0	6:0	-0.0	0,0		D.D	0.0	0.0	0.0	52.01	. 0.0	0.0	0.40	3 AON 90 0008	
Post	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0°0	0.0	0.0	68.4	0.0	0.0	0°D	5000-3000	****
No.   Color	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.D	0.0	0-0	0.0		0.0	0.0	666-005	1967
Section   Color   Co	0.0	0° D	0.0 10.0	0.0 10.0	91.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3000 DR MURE	
\$\frac{900}{900}   \$\frac{900}	+E801	0.0	0.0	0.0	0.0	62.0	58.6	29.5	61'4	21.01	89"5	98*9	54151	V/ 10	6661-0003	
**************************************	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	666-005	
\$1.00   \$1.0	.6912	0.0	0.0	0.0	0.0	24.0	0.0	10.0	£5°8					95.25		0961
0	0.0	0.0	0.0	0.0	0.0	0.0	54.1	68.4	15.6	56.51	10*9	56.7	65,71	80°15	4000-1666 S000-366	
***  ***  ***  ***  ***  ***  ***  *	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	666-009	
1915   0'10	**109		0.0	90.0		60.0	65*7				16'5				ALL VOLUMES	656I
979 079 070 070 070 070 070 070 070 070	0.0	0.0	0.0	10.0	0.0	90.0	64.5	67-11	78,51	7.31	25.2	6E*9	72°54 U*0	38.28	566E-0007	
1980	0.0	0.0	0.0	0.0	0.0	0,0	6°0	0.0	0.0					0.0		
\$46.65	*9909	0.0	0.0	ED*0	a'p				29*01		1119	29*5	04.51	21.64	VIE ADEOUES	8561
1246	*666E	0.0	0.0	0.0	0.0	10.0	1.36	75,11	75'51	10.24	51.8	29*5	11.51	16,95	6664-0007	
1561	1059	0.0	0.0	92.0	0.0	25,0	0.0	EE'5	51.5	10.1	61.9	09'9	10.96	80.ET	1000-1444 200-444	<u>.</u>
1415	.85.41	0*0		0.0	0.0	E0.0	Z8*0		4*54	£9*01	09*9	25*5	92.51	12.Bp		1961
	*519E	9:0	0.0	0.0	0.0	0.0	92.0	22.0	19*6	65*11	91.9	84.7		90172 0.0	666L-ODD+	
The color   The	0.0	<u>0.0</u> -	0.0	0.0	0.0	0.0	57.1	79.e	6.87	0.0	0.0	65.€	0.50	0.0	6661-0001 666-005	
**   **   **   **   **   **   **   *	*55.65			0.0	5110	0.0	61.1	19'5	68.7							9561
0*0 0*0 0*0 0*0 0*0 0*0 0*0 0*0 0*0 0*0	1667	0.0	0.0	0.0	11.0	0.0	98.0	0*0 15**	64.6 0.0	61.8	78.2	67.6	0.0	92.E2	6664-0007	
**************************************	- 0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0°0	0.0	0.0	0.0	0.0	6661-0001 666-005	
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		u-0	<u> 0-0</u>	0.6	p.0	0.0	0*6	0.0	0.0	0.0	0.0	0.0	0-0	0.0	665-0	1822
Feet   Color	0.0	0.0	0.0	0.0	<u>a*a</u>	Đ*0	0.0	70.0	78.8	0.0	0.0	0.0	0.0	0.0	SUDO DR MURE	
1	0.0 .SEEE	0.0	0.0	0.0	0.0	65.0		D*0	78*B		11.6	29-5	65*R	B.S. SS	666E-0007 6661-0001	
010	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0	0.0	666-009	
****   ****	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	D*0	0.0	0.0	0.0	01 E9 D 0	B000 OH MORE	_ c #. \$1.
0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0		0.0	0.0	0.0	0.0	16.0	75.0	11.7 20.0	0.0	0.0	0.0 15.E	0.0	41.7	חים	9995-0005 99970005	
0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0	0.0	0.0	0.0	0,0		0.0	0.0	0.0	0.0	0.0	0-0	0.0	0.0	666-006	
	0.0	0.0	0 0	0.0	0.0	6.0	66.0	0.0	O-0	0.0	0-0	0.3	0.0	0.0	8000 ER MORE .	-501
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	3420	0.0	0.0	0.0	60.0	0.0	66.0	50.0	0'0 11'8	0.0	00.T 0.0	99.5	O*D	99*09	666E-000Z	
010 010 010 010 010 010 010 010 010 010		0.0	0.0	0.0	D*0	0.0	0.0	0.0	0.0	0.0	0.6	0.0	_ D * D	0.0	666-005	
1952   0   0   0   0   0   0   0   0   0	0.0	0.0	0.0	D*0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0	0.0	BOCO OR MORE	4561
. 0'0 0'0 0'0 0'0 0'0 0'0 0'0 0'0 0'0 0'	1967	0.0	-0.0	0.0	0'0	0.0	96.0	05.5	10°5	98.5	0.0	0.0	.0.0	50.28 0.0	~ 6995-DD05 6691-0004	
155E   0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.0	a.p	8.0	0,0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	a-a	0.0	666-VD5	
*155E 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	0.0		0.0		5.0	0.0	0.40	0.0	99*1	0.3	00.5	15.1	14.9	09.58		1981
0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0'0	0.0	0.0	0.0	0.0	0.0	70-0 2.0	0.0	49.1	0.3	0.0	17*1	0.0		9995-0005 9997-0004	
	0.0	0.0	0.0	аO	0.0	0.0	0,0	0.0	0.0 0.0	0.0	0.0	0.0	0.0	0 0 0 0	6661-0001 666-005	
9561 9561 96665 96667 96667 96667 96667 96667 96667 96667 96666 96666 96666 9676 96666 9676 9676	VXFE2			66692	666.7											0561
14101 00095 00015 00025 00015 00015 0001 0001 0001			00015 01	01	DŦ	OT	01	Di	(1)		O.T	O.T.	0.1		TGA	HA3*
PERCENT OF TOTAL TRUCK AXLES BY NEIGHT GROUP						สกอรอ เ	нэтэй д	yxrez e.			אכנאו מו	13 ai				

BURREL MEHNAYS

FILGHERY BISTRICES 3, 4, AND B

SOUTH CENTREL MENTICES

.8531 .80502 .60967 .71866 .640271	0.0 0.0 0.0 0.0	TO'0 ZO'0 TO'0 O'D O'O	0.0 0.0 0.0 0.0 10.0	0.0 60.0 60.0 60.0 60.0	41°0 61°0 60°0 0°0	25.1 06.0 40.0 81.1 81.1	85.4 26.4 26.4 46.2 85.4	60.8 60.1 60.1 60.1	26.8 54.7 24.7 24.8	50.6 18.4 21.6 20.7 20.7 20.7	67.3 67.4 61.7 61.7 61.7 81.7	95.61 95.61 13.61 85.61 85.61	72.24 94.54 99.74 55.94 88.84	53W0107 114 6001-0005 6061-0001 606-1-0001 606-1-0001 606-005 606-005	
5662	0.0	0-0	o*o		0.0	54-0									ALL RAA3Y
61691 61691	0.0	0.0	0.0	50°0	60°D	0.7.0	21.€ EB.€	30.11	10.11	66 6 66 6	16.51	19.72 19.72	0.0 49.95	PER AGENCES PRODUCTORES #000 OF HORE	
\$2172 0.0	0.0	<u>p*n</u>	0.0	11.0	0.0	0:0 1:44	0 0 11 2 67 0	65.0 65.0	0°0 0°6 89°7	05 °01	62.41	12.19 12.19	0.0 6.13	566E-000Z T000-1666	
0°0	0.0	0.0	0.0	0.0	0,0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	665-005 685-0	9961
*****************	0+0	0.0	\$0.0 E0.0		51°0	10.0	48.5		07.01 89.01	D7.8	50°71	18.95	76'1E	SOUD OR HORE	9961
15921	0.0	0.0	0.0	90°0 0°0	21.0	0.4	05.2	0°D	0.0	0.0	0.0	0.0	0.0	5000-3000	
0.0	0.0	0.0	0.0	0.0	0.0	86.5 0.0	15.8	76.5	60.45	20.1	6.0	89°ZZ 95'51 0'0	0°0	666-009	
0.0	0.0	0.0	0.0	D*0	0.0	99*0	25.5	11.6	1Z*6	96°L	07.01	91.81	0,0E	0-434 VIL VOLUMES	596T
**************************************	0.0	0.0	0.0	0.0 0.0 0.0	60.0 60.0	0.0 64.0	0.0 45.4	62.01	90.01	0.0 70.8	0.0	0°D	0.0 64.7£	4000 DR MURE \$3MUL VOLUMES	
.T#SZ 0.0	0.0	0.0	0.0	15.0	0.0	51-1 0-0	16.2	11.01	R 7 Z	91.16 5117	2, 14 2, 14	85'71 86'71	17.95	666E-0007 666E-0001 666-009	
.518 .116.	0.0	0.0	0.0	0.0	27.0	0.0	19.1	0.0	19.1	11.7 E2.E	56 8	SI'EI	42.17	665-0	<del>&gt;</del> 961
*56011 0*0	0.0	0.0	0.0	0°0	84.0	91.1	60.0	0.0	0.0 4E.6	0.0	26.01	0.0	0.0 E0.7E	8000 GR MORE 8000 GR MORE \$3M010A 114	
.557E .67ET	0.0	0.0	70°0	80.0	0.0	98.0 0.0	55.5	10.01	91'6	86.9 86.1	17,01 17,01	73.91	91.4E	5000~3666 1000-1666	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.0	0.0	0.0	0.0	0.0	0.0	666-005 667-0	
1+901 0 0	£0*0	0.0	£0.0	50.0	21.0	79-0	95*6	7.80	9176	16.T	52.11	11.61	16-15	8000 OR HORES	€961
0*0 5516 "2651	0.0 E0.0	0.0	0.0 0.03	6.0 0.0	0.0 0.17	79.0	₽8.€ 0.0	92°L 0'0	81.P 0.3	0 0 6E 8	97.11	55.81 70.81	24.52	2000-3999	
0'0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	010	0.0	0.0	0.0	0.0	6661-0001 666-009	
0.0	0.0	0.0	0.0	0.0	0,0	0.0	0.0	0.0	0.5 2.8	25.9	0.0	0.0	16.04	23MU30V 11A	2961
12105.	0.0	90°0	0.0	0.0	05.0 11.0	84.5 06.1	66.8 18.8	51.6	26 9 96 9	9.80	F 6 8	25. 41	12.12 12.12	990M AU 0098	
E 29E	0.0	0.0	0.0	0.0	0.0 05.0	0.0	56.4	0.5 58.8	0.0	50.6	68.8	8£'81	0.0	565E-000Z 6651-0001	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0'0	0.0	0.0	0.0	0.0	0.0	665-005	1961
115031	0.0	40.0	0.0	80-0	60.0	41.1	0.0	C. D	62'6	06*9	f Y . 8	76°51	88.52	3900 98 0008 24 VOLUMES	
.197£ .0047 0.0	0.0	0.0	0.0	60.0	40.0	17.0	£6.2	56.F	97°11	46.8	99 S	19.61	05.64 61.65	9991-0001 9995-0002 9997-0003-	
0.0	0.0	0.0	0.0	0.0 0.0	0.0	0.0 0.0	0.0	0.0	0.0	0.0	0.0	0.0 0.0	0.0	665-005 665-0	
*45ETT	0.0							24.6	86.8	69.9	59.0	65.5I	92.54	ארד אמוחאנצ	0961
0*0	0.0	0.0 £0.0	0.0	0.0 0.0 50.0	0.0	05'Z 0'0 10'5	0.0 ET.T	16.3	67.01 67.01	25.9 0.0	£7.8 62.8	0°0 75°91 69'91	B*0 58*75 69*15	\$000 GB HGRE	
0.0 0.0 .ERT2	0.0	0.0	0.0	0.0	0.0	0.0 0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	666T-000T	
_0.B	0.0	0.0	9:0	G*0	0*0 .	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	569-0	6961
0.0 7E90	0.0	0.0	0.0	50.0	2.0	0,0	0.0	0.0 8.39	0 J 95 L	0.0	0.0	0 0 61.21	0.0	8000 DK MCKE 8000 DK MCKE 8000 DK MCKE	
09D+	0.0	0.0	0.0	0.0	15.0 55.0	0.0 07.1	54.0	91.6 17.8	59.6	27.7	00 S	26 91	0.0 62.12 62.12	666E-000Z 6661-0001	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	665-005 665-0	9561
4554P	0.0	0.0	60.0	6.0 0.0	91 0	21°Z	19 <u>*1</u> _	84.1	98.8	96.4	40.6	55.51	52.67	PEE ADENEZ	9501
16986	0.0	0.0	-0.0	22.0	61°0	46.5	91.8 91.8	11.B	60.E1	67.5	67.6	17.00	99 JS	2000 - 1999	
207	0.0	O*D	0.0	0.0	D*0	0.0	08.1	34.5	74.E	24.9	29°5 60°5 09°5	66 9 99 8	15.07	6661-0001 666-009 664-0	
.81801 .E81	0.0	10.0	0.0	0.0	6.0	F1.1 - Ha.0	19"4_	86 <u>*0</u>	6E'S	78.E		62.11 62.11	99'69	VEE AUCONES	£\$6T
.1817 0.0	0 0	0.0 10.0	0.0	0.0	0.0	0°0 I 1°3	0.0 18.8	0.0	81.8 0.0	65*9	05 S 0 0 22 S	76'01	BE*64	9000 CR MBRE	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.0 0.0	0.0	0.0	0 0 0 0	6661-0001 666-005	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	9,0	664-0	9561
0.0 6998	0.0	0.0	0.0 50.0	0.0	6.0 6.0	0.0	0.0	91.7	0.0	07.5 0.0 85.5	0.0	0.0	99.02 69.52	BODD OR MORE BODD OR MORE ALL YOLUNES	
2125	0.0	0.0	6.0	6.0	51.0	9 E 1 9 T T	04.2	6F:1 0'0	0.0	77'5 0'0	99.9 12.2	0.0 0.0 0.0	9,86	\$900-3900 1000-1444	
0.0	0.0	0.0	0.0	0.0	0.0 0.0	9.0	0.0	0.0	0.3	0.0 0.0	0,9	0.0	0.0	666-305 665-0	5561
.eze.	D' 0	D-D	0.0	90*0	50*0	59*0	84.6	91'8	29*9	£1.2	88.4	05.5	10.42	ALL VOLUMES	3341
0,0	0.0	0.0	0.0		Q*D	0.0	0*0 85*D(	01.6 94.8	0.0	0.0	12.2	0.0	0.0	980H #0.0038	
0.0	0.0 0.0	0.0	0.0 0.0	0.0	0 0 0 0	65.0 6.0	0°0 0°0	0.0	0.0	0.0	0.0	0.0	0.0	1000-1338 200-1338	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0-0	0-0	0.0	0.0	0.0	669-0	756T
0.0 0.0 .PS.3T	0.0	0.0	6.0 6.0	20 0 0 0	0.0	72.1	0.0 0.0	0.0	86.9	05.5	91'S	51.6	75.45	RODD ON HOME 2	
0.0 .8ES.	0.0	0.0	9.0	0.0	0.0 0.0	79.1 18.1	86.8 28.51	18.7	51°9 59°4 0°9	59'S 0'0	45.2 94.7	69.6 0.0	92 25 55 55 0 0	6661-0001 6667-0002	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0-5	0.0	0.0	0.0	0.0	666-009	
0.0	0.0	0.0	0.0	0.0	02.0	54.0	£6.8	70.8	57*9	84.4	57.7	6E,7	29.05	BODO OR MORE	
9856	0.0	0.0	0.0	0.0	0.0 6.23 0.0	85.0 93.0 0.0	52.8 9.75	10.8 2.0	0.0 54.0	0°0	65°5	51.9	0°0 69°85 €7°09	9904 90 0008	
0.0	0.0	0.0	0.0	0.0	0.0	0.0 0.0	0.0 0.0	0.0	0.7 0.9 0.9	0.0	0.0	0.0 0.0	0.0 0.0 0.0	665-305 665-0	
*210L	0.0	0.0	0.0	20.0	0.12	621t	ES -5	86*9	66.70	96*9	78.2	12.7	20'09	5807 AD 2008	7561
0.0	0.0	0.0	0.0	6.0	0.19	0.0	0.0	0.0	0.0	0.0	99.5	97.0	0.9	8664-0307	
0.0 0.0 .EE8E	0.0	0.0	0.0	0.0	0.0	81.1 0.0	0.0	0.0	05.9	0.0 52.0	0.0	0.0	16 09 0 0 .0 0	666E-000Z 666E-0001 666-009	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0,0	0.6	0.0	A b to m O	1961
9665 1867 1867	0.0	0.0	0.0	0.0	60 0 0 0	0.0	0.0 50.1	2,04	29°1	52.5	1.14	B + F	85 58 0 0	SOCO DE HORES	
0.0	0.0	0.0	0.0	0.0 10.0	0.0 0.0	0.0 22.0	0.0 7.4.E	0.0 0.0 84.2	0.0 7.0.6	87.7 0.0	0.0 64.5	0.0 65.1 9.39	16,59 85,15	6661-0001 6661-0004	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0*0	0.0	0.0	0.0	0.0	0.0	0.0	699-00ē	
 537xv	66666		56692		46+70										3561
-2.04	. 01	ODOTS OT	D.A.		66672 UL	66607 D1 00061		01	10	10	10466 TD 4060	8888 10 1000	<u>наомо</u> <u>Боо</u> т		AEVE

MINCH CENTRAL KENTOCKY
HICHARY DISTRICTS 5, 6, 1400 7

RUNAL HICHARYS 

.016 .016 .016 .016	56£	10°0 0°0 0°0 10°0	£0*0 50*0 10*0 6*0 61*0	90'0 20'0 40'0 40'0	01.0 01.0 01.0	66.0 72.0 72.0 72.0 72.0	1,47 1,47 1,35 1,135 1,135	56.1 65.2 54.7 11.6	56.6 07.1 95.9 88.1	08.1 12.4 12.4 08.1	86.0 67.8 69.8 73.6	77.4 04.4 26.4 20.8	10.51 10.51 16.61 18.61	89.64 £5.04 £1.42 51.52 51.52 61.54	5000-1444 5000-1444 TD00-1444	
280	01	0.0	0.0	56.0	80°5 11°0 0°0	0.0 0.0	10 E	18.1	78 .5	69 E	75.4	18.5 50.2	09.8 86.11	16.69	666-305 669-0	Z E A E S
163	18	0.0	0.0	0.0	50°0	10 ° I 87 ° I	P7.5	68.2 69.7	54.0 97.0	15.51 9.54 16.51	61.9 61.9	68.8 69.01	19,81	70,16 70,16 70,16	\$3H0104 1 <u>174</u> 8000 00 0008 6661-0005	
0.0	T.S.	0.0 0.0	0.0 0.0 0.0	0.0	0.0 0.0	0.0	0'0 0'0	0.0 0.0	0.0	0.0	0.0	0.0	0.0	0.0	666E-0007 6661-0001	
0.0	00	0.0 0.0	0.0	0.0	0.0	0.0	97'5	0.0	61.6	0.7	00.0	0.0	<u>0'0</u>	05166	23MULD V 11X	9961
101	55	0.0 0.0	0.0	0.9 9.0 10.0	0.0	91.0 7£.1	11.1	16 4	0.0 01.6 95.01	_55 <u>*8</u> _	0.0 61.6	0.0 TE.SI E2.1	90°81 65°61 0°0	95.96 75.75 71.84	5666-3009	
0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 0.0	0.9	0.0	0.0	0.0	0.0	1000-1884 200-888 200-888	5961
*694 *609		6.0 80.0	64.03 0.40	0.0	91.0	0.0 16.1	37.5	8,52 6,52 6,0	9.0 91.9 88.6	26'9	60.0 80.4	42.01	85-91 51-51	95°65 55'86 <u>0'</u> 0	8000 DR WD86 8000 DR WD86 8000 TJV	
.618 ,208	9	95.0 0.0	75.0 0.0	0°0 67°0 67°1	0.0 24.2 0.0	901	89°1 6'02 0'0	26 E	7,00 51.0	41.6 48.1	24.5 28.1	65.8 64.8 76.8	9.0 82.11 01.61	45.02 17.64 35.12	5000-3046 500-3046 500-3046	
-0£		9.0 0.0	0.9 0.0	0.0 0.0	0.0	0'0	0'0 58.8	19.4	9.0	99.9	06.6	21.01	0.0 89.21	_00°09.	8000 GK MOKE ALL VOLUMES 0-449	596 T
1856	8+	0.0 0.0	0.0	0.0	0,0 91.0	0°0	3.0 28.1	9 9 50 5 0 0	0.0 0.0	16.6 0.3 55.9	15.2 72.2	69.11 0.0	55.61 E8.41	9°55 11'85	6667-0002	
0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0,0 0,0	0.0	0.0	6661-0301 666-005 667-2	£961
123	06	01.0	16.0	02.0	88.0 07.0	90.0	- <u>69*1</u> - 11 * 1	86 ' 9	0.0 00.0	71.6 0.0	51.1	59"6 59"01	65.73 64.73	99*55	\$000 CS MORE \$000 CS MORE	
0 0 0 0	71	0.0 0.0	0.0	0.0	0.0 0.0 0.0	0.0 0.0	0.0 0.0	0 0 15 E 0 0	3.0	20 OT	0.0 01.0	0.0	09°51 0°0	0*0 95*05 0*0	666-0002 666-10001 666-305	
0.0		0-0	9.0	0.0	0*0 50*6	0-b	2.4	6.0	0.0	0.0	3-q_	0.0	0.0	11.54	665-0 57.F KOLUMES	296 E
665 651	75 75 21	0.0 0.0 0.0	0.0 0.0	0,0 0,0 75.0 15,0	6.0 70.0	0°12 0°0 0°0	65 0 29 6 67 0 0 0	10.6 46.7	51.6" 17.8	82.1 87.1	55.4 54.1	61-1 0.0	0,0 70,81	12.26	2000-3999 2000 CR MORE	
0.0		0.0	0.0	0.0	0.0 0.0 0.0	0.0	0.0	0.0	3.0 3.0 0.0	0.3	0 D 0 D	0.0	0.0	0.0	566-0001 666-000	
05	25	0.0	0.0	0.0	0.0	0.0	68'0 59'0	05.2	9.06	76 °5	95'9	25°L	90*51	56 9 6 66 9 9	2000 AD 0008 2000 AD 0008 21,1 VOLUNES	1961
0.0	11	0.0	0.0	0*0 0*0	0.0	0.0 0.0	0.0 66.1	0.0 14.5 0.0	0,0 70,6	0.7 6.43	5, , 6 0, 0	0.0 62.8	15:21	0.0 19.58	6662-0007 6661-0007 6661-0007	
0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0 0	0.0	0.0	0.0	664-0	0961
. 0.0 114.	44	0.0 0.0	0.0 0.0 0.0	0.0 0.0	0.0 0.0 10.0	51.0 0.0 76.0 76.0	55.5 56.1 67.1	0.0 00.0	9 ' B	0,7 9,7 80.9	70.0 70.7 70.4	16.8 0.0	0,0 15,81	66.42 24.74 0.0	2000 CB HORE 2000 CB HORE 5000-3030	
0°0	21	0.0 0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0'0 0'0	0.0 0.0	0.0	9.6	0.0	6661-000T 666-006 667-0	
	25 .	0.0	0.0	6.0	50*0.	0-0_	RA. I	19-9	88.6	8816	79.9		19'51	18*55 0*0	390M NO 0008 23MUJOV JJA	6561
0.0 .IT.	0 <del>5</del> 11	0.0	0.0 0.0	0.0 0.0	0.0 55.0	0.0	0°0 67'7 67'8	6 A . S F8 . T	39.9	95 11 11 7	9E.8	0.0	69.41 69.41	0.0 0.0	5661~0007 5660-3666 1,000-1666	
0.0		0°0	0.0	0.0	0.0	0.0	D.0 D.0	0.0	0.0	0.3	0.0	0-0	0.0	0.0	669-0	8561
0.0	86	0.0 0.0	0.0 0.0	0,0 80,0	56*6 0*0	0.0 81.0	0.0	0.0	01.0 1.0	0.0 0.1	8,18 0,0 58.8	0.0 75.6	12.84 0,6	0.6 71.42	4000-7999 6000 GR MURE 711 VOLUMES	
0.41 9.21	٤	0.0 0.0	0.0	91.0 0.0 \$1.0	0.0	59.0 50.0 51.0	51°1 86'E 28'E	71.1 71.1	20 S	45.5 48.8	95°5 98°2 21°5	19-5 67.5	15.¢ 46.0) 11.51	56.51 71.53 77.17	5000-3666 5000-666	
-09	91	0.0 0.0	0.0	0.0	60.0	6.0	01.1	01.2	PE 1	2.20	76.d [2.d	19.5	66.01 0.9	13*61 26*88 16*61	0-444 900 CB WORE	1561
.151 .61	11 92	0.0	0'0 0'0	0.0	0.0 10.0 0.0	11.0 90.0 11.0	20°I 20°I 20°I	02 1 06 2 91 2	50.7 86.2	591	48.1	90**	74.0	12*99	5000-3000 5000-3000 1000-1000	
0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 0.0	0.0	0,0 0,0	0.0	666 <b>-</b> 005 665-0	9961
0.0	65	0.0 0.0	0 ° 0 0 ° 0	0°0 0°0	£1'6 0'6 £1'0	0.0 10.0	05.1 0'6 05.1	6'0 6'0	9.0	90.9	0.0 15.7 0.0	0.0 67.4 0.0	9.0 9.0 9.0	46*15 0.0	VII AGE PMES 4000 CB WOSE 4000-1444 5000-3444	
0.0		0.0	0°0	0.0	0.0	0.0	0.0 0.0	0.0	0.0	0.2	9.0	0.0	0,0	0.0 0.0	5661-3001 566-305	
0.0		0.0	0.0	0.0	D*6	0.0	a.b.	0.0	0.0	0.9	9.0	0.0	9.0	9'0	664-0	5561
0.0	15	0.0	0.0 0.0	0.0 0.0	0.0 0.0	80.0 80.0	99 0 99 0	98.2 98.2	58'6 50'6	15 9 9 3 15 9	95.5 0.0	25.2 . 0.0 . 5.32	60.7 .0.0 £9.1	91.09	9000 UR HORE 4000-1006 5000-2006	
0.0		0.0 0.0	0.0 0.0	0.0	0.0 0.0	0.0	0.0	0.0	0.0	0.0	0.0	0,0	0.0 0.0 0.0	0.0	666-000T	
112	16	0.0	0.0	0.0	0,c	80.0	01.0	03.0	99.F.	51,7	0.0 8E.7	76.0	11.9	70°09	ארר אמרחאב א	
0.0	11	0.0	0.0	0.0	0.0 0.0	0.0	0.0 DE.0	0.0	9.0 9.1	0.7 57.7	0.0 0.0 85.1	0.0	0.0 77.4	0.0	5000-3000 5000-3000 1000-1000	
0.0		0,0	0.0	0.0	0.0	0.0	0.0	0.5	3,0	0.7	0,0	0.0	0.0	0.0 b,0	664-J	E561
0.0	96	0.0 0.0 0.0	0.0 0.0 0.0	0,0 0.0	80.0 80.0 80.0	0,0 0,0 0,0	6.0 6.0 6.0	68.5 64.5	95 B	7 94 7 94 7 94	87 V 0 D	66°7	27.0 2.0 27.6	72.79 0.0 72.79	2 3 MO D D D D D D D D D D D D D D D D D D	
0.0		0.0	9.0	0.0 0.0	0.0	0.0	0.0 0.0	0.0	0.0	0.0	0.0	0.0	3.0 2.0	0.0 0.0	6661-0002 6661-0001 666-005	
167	EE	0.0	0.0	0.0	0.0 0.0	71.D	55*1 0*0	0.0	10.5	25.5	56.5	79*5	0675	62.66	ALE VCLUMES ADD OF MORE	7561
0.9 15 0.9	21	0.0 0.0	0.0	0.0 0.0	0°0	0.0 85-0	90'0 96'0 88'T	0.3 02.2	0 0 0 0	0.0 20.4 0.0	0°0 10°4 25°9 0°0	0°0 7°5 7°0	0.0 41.1 0.0	55,87 F1,98	5000-3446 5000-3446 1000-1466	
0.0		0.0	3*0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	-0.0	0.0	0.0	9.0	664-3	1551
0.0	92	C.0	0.0	0.0	0.0	0.0 0.0 0.0	3 B	6.0 0.0	0.0 3.0 70.5	80.4 0.0 0.0 ET.1	01°1 0°0	0.0 0.0	12.8 12.6	6.0 0.0	######################################	
0.0 0.0		0.0	0.0 0.0 0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0 0 0	T 9 Z J 0 J 0	0.0 6.0	0.0 0.0	- 0.0 0.0 	66-2007 666-206 66-206	
0.0		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6		0.0	0.0	0.6	- 0.0	667-0	0961
341		00005 01	00012 01	01 00057	56666 10 54648	0017 01 0017	160 16 14006	00071 01 99981	1 2000 1 2000	000£1	15444 11000	0006 61 66601	6565 0381	8.36NU 0031	TUA.	A4.3Y
						anges .	інотон ,	rktes av	14UCK	79101 :	0 1741 OE	яза				

EASTERN KENTIGKY HIGHWAY DISTRICIS 9, 19, 71, AND 12 BURAL HIGHWAYS

LOW T'000 AEHICFES PND LOW T'000 LENCKS HISLOWICET SOMWERK - VAERGE EMF.S

VBBENDIX C

51 F2A 86 E27 12,854	25.561 28.111	12.252 01,004 40,952	92°V6 92°901 50'101	77,5410 77,78151 70,0986	95.9271 85.4815 69.4514	9997-0009 990M 90 000B	
22,612 52,192 191,90	50.68 TS.101	19.584 16.085	85,88 91,88	75,422 20161 54,524 54,524	75,4281 72,4281	666-0007 666-0001 666-009	
Z1-091	19.51	39.851	65.51	59,8981	24.471	669-0	ALL YEARS
68.0T8	99*691		110.27	17.95351 90.2951	P1.8555 21.89ES	23MULOV 11A	
16,911 16,911 16,911	12, 825	24'699 06'608 90'801	50.11 46.851 46.851	85°0566 21°98161 E1°9221	47.5012 00.5954 18.2621	5662-0007 5000-3666 1000-1666	
0.0	0.0	0.0	0°0	0.0	6-0	665-005	
19*/9#	52*09T	11.954	96.911 21.901	13446.36	66,6825	NODO ON HORE	9951
92.288 97.538 11.198	96 '51 96 '51 66 '51	16,000 16,000 21,000	60.551	15,6561 HT,15051	88.106.4	\$000-3668	.,
51.48£	11'75 0'0	15.628 0.0	0.0 0.0	0.0	58*859 0*0 0*0	6661-0001 666-005 665-0	
0.0	110.96	£J 965	67.76	96.72921	96'5912	ALL VOLUMES	5961
22,868 69,559 89,865	16.191 16.191	60,001 86,117	60.201 82.201	15.5821.21 12.5821.21	21,0825 21,0825	9808 90 0008 666E-0005	
56*659 10*525	38.08	90.465		26 * 52617 64 * 11109	15.0055 57.000	6661-0001	
67,081	90,751	28.556	65'EE 20'IET	19,19551	18,2552	2540 ACLUMES	<del>59</del> 61"
97 ,6 28	14.27 I	0.0	6'6 55'05!	75'6IZEI	20.3EFS 9,0	2000 - 1999 4000-1999 4000-1999	
0.0 0.0 24.281	0,0	187929 0°0	97'11'1 6'0	0.0 EY.80#11	0.0 57.1115	666-009	
0*4	0,0	0.0	0.0	0,0	0.0	664-0	£961
50.018 59.856	12.591	16'995 61'697 61'969	96,801 96,801	84.65.41 27.55.111	04.1634 06.21534	380M 93 0008 380M 93 0008	
0.0 28.000	65*821 65*88	0.0	86.18	0.0 0.0 0.0	0.0 AE.11EL	5000-3444 T000-1444	
0.9	0°0 0°0	0,0	0.0	0.0	0.0	665-305 669-0	2961
64,586	19'92I	04.818	25 '50 ( 61 '91 (	1041444 1041444	VB*8681	ארר אמרחאב2 8000 מע אמצר	
62*169 62*169	18'601	59,049	99166	28 '6668 TO 99511	11,0641	666L-0005	
17.088	21,52,	0,080	10.0	97 3E181	51-5292 0*0 0*0	000-1888 000-1888 000-888	
9°0 98°989	0,0	0.0	£7.76 D.0	16.5849	T 100 A4	SELUNES ACTURES	1961
56*955	11.50	50,668 50,688	81,501 81,501	87,8280 81,5200 80,8867	86.9951 86.9951	2000-1999 4000-1999	
0.0 0.0	70.Tij	10°054 0°0 0°0	0.0	6.0 d.B	0.0	666-009	
0.0	0.9	0.0	0,0	0'0	0,0	0-466 VII VOLUMES	0.96 )
98-951	76*071 11*101 92*511	50'529 67'556	16'611 10'56 49'951	11205,17	41,4565 50,1541	940M AG 0004	
60.969 01.948 62.691	05.705 25.011	11,258 12,512 17,188	25,26	88 , 484 £	65 8091 95 2605	\$666-0002 1000-1666 200-666	
0.0	0.0 0.0	0.0	0.0	0.0	0.0	664-0	6561
65,E6T	134.12	29 * 8 + 9	99'81I	EV. EEE11	66°5'L07	BODO OR HORE WORE	
	81.EF1	61,726 81,726	87*171 2112°17	58,12511 98,11811	15,8721 68-7105 77,6515	7000-1086 7000-1086 700-1086	
63*295 0*0	0.0	0.0	01'56 0'0 0'0	52,542& 0,0	0.0	666-009 669-0	8561
14.518	100.22	0.0 0.0	49°63	85'6686	96-6191	SEMULOV DIA	
06.50T	77 55 E 55 EG (	27'109	50, 51,1	95,1840f	1907	5662-0007 5662-0002 5661-0001	
399,63	10*95	99.96E	62,11 57,04	19,261 68,6196 19,261	57.621 10.088	566-009 669-0	
50°1E1	92°II	79°205	67.0b	51.8967	27,0851 1280,75	VIL VOLUMES BOOD OR MORE	156
10,592	53.99 £1.5n	70,152 55,090	95.ET 67.88 60.25	42 4111 42 4118 45 4111	61*1991 UE*5111	2005-3999 0001-3999	
7E,072	61.27 61.27	65"65"	92*59	87.15.46	0.0	6661-0001 666-005 669-0	
0*0	0'0	22.014	64,61	71.11.02	1515.96	WIF AGENES	956
12'989 0'0 71'115	97.4n	0.0	0.0	81,521a 71,8127 0.0	29.2981 29.2981	999E-0005 999T-0004 3ADM 93 0008	
	0.0 95.80	0.0 0.0	0.0 57.40	0.0	0.0	1000-1000 2006-444	.—
0.0	6.7 0.0	0.0	0.40	0.0	0.0	669-0	555
·				10.8474	29*2811	ALL YOLUMS	
0*0 0*0 05°05%	0.0	0.0	0.0 17.41 98.10	0.0 08.8644 51.0127	0.0 121,157 0.0 0.0	9000 OK HOKE \$000-1464 \$000-1446	
0.0	0.0 0.0 55.58	0.0	0.0	0.40	0.0	666-009 666-0	
	ייט יי	75-25	0.0	0.0 0.0	10,9201	ALL VOLUMES	556
0.0 0.0	0.0 41.51	9.052	0*0 0*0	0.0	0.001 1042,93	2000~3999 4000~3999 8000 DR HDRE	
£1.25.2	80.21	<u>"G"E%</u>	0.0 60.81	0.0	0.0	5000-1446 1000-1446 200-066	
ਹ* 0 ਰ*0	0.0	0.40	0.0	0.0	77.9401	554010A 77V	£5.6
74.414	0.0 Ra.4T	0.0 0.0 50.04	0.0 11,51	0.0 0.0 12.2792	0.0 54.5E9	BOOD ON HOME	
E1.940	65,58 50,44	***6E*	84.18	78*5657	90*£221 0*0	\$600-3999 1000-1999 200-999	
0.0	0-0	0.0	0.0	0.0	0-0	666-009 669-0	255
	D*0	0.0 0.177£	6.64	0.0 46,2962	0.0 0.0 0.1.10e	8000 AB 0008 8000 BR MORE 23MULLY 11A	
25.012 7.0	90*84	99,12E	97.04 90.14	19*5865 56*565	40.548	5000-3888 1000-1888	
0.0	0.0	0.0	0*0 0*0	0.0	0.0	666-005	
0+0		TSU-BT	72.25	75*20ZT	0.0 44.54E	SENT DA FTY	
0.0	0.0	20*0 20*50t	95,55 28,01: 0,0	14-1902 14-1951	0.0 66.574 16,516	2000-3449 6667-0004	
51°901	£9'ZŽ	9.0	0*0	0.0	0.0	666-009 669-0	
0*0	<del>0</del> •0		9-0				05
Fano isacka	A NEW CHILD AND A NOW NO. 1	VIODO TRUCKS	AASHD.ENLS	VYOOD LUNCKS	VIDDO AEH	TGA	HA

01,008 .26,124 .0,0 .86,261	0.0 E2.1E1	56*065 0*0 61*195	0,0 0,0	60*98E11 9*0 91*E966	0.0 0.0 2036.06	9297-0004 8000 90 0008 2390,004 114	
52.852	55°05	60.440 55.855	- 96*12T	01.8027	58,2945 94,5945	5000-3888	
	0,0	0.3	0.0	25.4011	0°0 90°94	666-005 665-0	
05.869	550,99	49 ° E 69	99'691	P£"89551	27.00SE	SEMOJDA TIV	YEAR5
3'0 56'858	6' 0 62' 59 I	£P,E03	0.0 90.661	0*0 64*15811	0.0	4 DEG-1699	
17,1361	50.165	6.0 8P.8R8	0.0 21.891	0.0 66.81105	65,116P 65,116P 6.0	\$000-3000 \$000-1000	
0.0	e.0 e.0	6,0	0.0	0,0	0*0	666-005 665-0	
69.988	19*761	69,714	22*961	52,0ETEI	01*07+E	VET ADEMIES	9961
81.456	10°C	0.0 01.454	0.2	0°0 59°858ET	0°0 22*8052	4000 00 0008 8000 00 0008	
2.0 78.158	0°0	6*0 6*0	0.0	0.0 0.9 0.5PP81	0.0	666E-000Z 6661-0001 666-009	
7-0	0.0	0.0	0-0	a.p	o•n	664Q	3961
27.456	96*V+t	F0'185	98'E01	98-89941	50*8052	4000 ER MURE \$900 ER MURE \$140.704 174	
0.25 92,39	25.081	26.61T 28.783	05.011	1216,13	***Z6+Z	566E-0002	
9.0	6.6	19.275	0*0	0*0 11.4965	0.0 41.852	, 999-002	
115.23	25°L	62-511 19*629	56,161	98.8121	99*195E		596T
27,7201 27,7201	28,725 0.0 24,025	0.0	0.0 0.0	46,99441 0,0 21,18411	0.0 17.826£	9000 CB WGEE 4000-1469	
27.0ES1	95.25	E9 E69	RE SUT	95-00261	TB . EUP E	566E-0007	
0.0	0 · 0	*** 2*5 **** 0*6	6.0	0.0	9.0	666-009 664-0	
96*120	48,891	58' 451	95*951	12728,92	74-8645	VEE ADEDHES	E96I
3°0 21°956 81°948	91.521 88.491 0.6	11.301	0.0	16,28051 19,280E1	70.0 70.1945	9000 -1999 4000-7999 7000-7999	
4'0	0.0	D*0	0.0	0.0	0.0	666-005	
3.3	(-t)	0.0	6.0	0*0	. D.0	664-3	7961
Teen's1	95.751	12.220	12:061	19:616:41	91'619Z	NOOD OH WINES	
15,1701 11,479 3,1	86,195. 81,811 9,9	18,45H 64,45H 0.9	59*29T 26*951	44,655481	86,1895 84,8455	5000-3446 5000-3446	
9.0	0.0	0.0	0.0 0.0	6.0	0.0	566 -005	
9.6	٥٠٤ .		0.0	6.0	0.0	665-0	1961
0.0 07,504	96,591	11,567	9.0 48.18.1	11.0821	0.0 TA.TASS	BOOD OR HORE	
71.11A	135,79	75 II H	113.92	11525111	0.0 302,13 34,5881	*000-1888 5000-3888 7000-1888	
9.9	0.0	0 0 0 0 6 3	0*0 0*0	0.0	0.0	666-005 665-0	
0°0 09°256	18,48I 0,9	n1,307	BZ*051	92*9[66]	29*6712	SEMOTON TIV	0961
0.0	0 °0	0.0	0,0	08.82451	0.0	9997~000 <i>p</i> 3#3# #0 0008	
9,9 60,850 98,849	16.891	U.1	85,061	0.0 0.0 14.05621	0.0	5000-3888 7000-1888	
0.0	0.0	0 ° 0	0.0	0,0	0.0	666-009 665-0	6561
92,9231	ms.avi	20'558	10.841	19354.95	11.8895	8000 OF MORE	
9Z*6+8 9Z*6+8 1Z\$6*33	47.3E1	61.0C1	05,711	12159,39	05°5561 58°5°13	9999	
0.7 16.9951	25.852	52.6501	0.0 87.991	9.0	0.0	6661-0001 666-005	
3.0	9.0	0.0	0°D	0.0	· 0.0	664-0	1429
61.617 9.0	64,151	9£ '985	0.0	13050*51	0.0 8.45ES	3800 DO 0006	
15,487	145*16	87.653	55102T	95,09801	2052.74	7000-1000 5000-2000 1000-1000	
95*125	96,94	92.854	0.0	88.747 0.0 81.47001	91,02 0.0 74,5481	666-005 665-0	
61.ET	16.5	01'405	77'5 81 88	51.0718	Db*ZE†I	VIT ADLONES	TERT.
- U-J 54,568	99*26	0.0	0.0	9.4567	67.02E1	9994 90 0008	
15.053	68.611	0'0	16*6E 16*6E	F1.112h	0.0 18.1531	1000-1000	
0*0 0*0	0*U	0.0	0.0	0.0	0.0	666-005 669-0	956T
17.288	49*21	#1.ETE	EE.OT	56'5EZG	12.766	BODO OR HURE ALL VCLUMES	
24,272 24,272 3;0	5°0	0°0 50°097	0.0 84.85 86.111	96*715E	12.812 96.4001	6666-0002	
0.0	0*0	0.0 FE.SEA	0.0	9.0	0.0	1000-1666 200-666	
0.0	0.0	0'5	ū.o	0.0	0*0	669-0	5561
01*615	96*59		A1.50	05.6568	65*526	VIL. VOLUMES	
72.275 0.0	12.54	0.0	4.70	42,1417 24,2216 40,0	58.882 20.0	2000-3999 4000-7999	
16,518	71.00	95*505	60'27 57'86	0.0	0.0	666-009	
0.0	0.0	0.0	0.0	0*0	0.0	667-G	966 T
42.E95	35-09		PT . PE	ET SERE	95,652 0.0 85,652	BOOG OR MORE	
0,0	56.55 62.05	79.49f	75.48 20.30	554,13 2554,13 0.0	62.951I	*000-1888	
3*6 0*0 0*0	0.0	6.0	0.0	0.0	0.0	5661-000T 666-005	
D*0	0.0	0,0	0.0	0.0	12,719	53H01DA 11V	£561
0.0 -58.20r	09*69 0*0	0.0 0.0	92.85	0.0 0.0 64.190E	51,8881 67,858 0,0 15,719	480H HD 0008	
17.155	90"711	\$6.840 \$7.155	717.96 90.511	29.41801	0.0	5000-3666 1000-1666	
0*0 0*0	0°0	0.0	0.0	0.0	6.0	565-005 569-0	
378	75.44	52.556	48 • E+	92*9665	26 585	BOOD OR WORE	2561
. 69*9EE 3*0 52*894	0.6 15.44	0.0		10.0EEE	42.012 0.0	666 E-0005	
19,952	96.48	427,19	99.28	97.4012	6.0 0.0	566E-000Z T000T-666 666-00S	
טיט	0.0	0-0	0.0	0.0	0.0	664-0	1961
99*291	#E+06	62*291	P.0	0.0	74*16E	BOOD DR MORE	
0*0 95*211 97*691	91.91	47.641 68.111.	94.91 0.0	65,5421 62,5421	56.915	5662-0005 566E-0005	
0.0	0°0	0.0	0.0	0.0	0.0	6661-000T 666-005	
0*0	0.0	0.0	0.0	0.0	0.0	664-0	0561
	1901/ HAA 0001/	/1000 IRUCKS	H3A 0001/	/1000 1KUCKS	11000 AER		8437
TRIICKS			AASHO ENLS	KY EMLS.			

61.25.73 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0	0.0 0.0 50,621	0.0 0.0 11.892 10.872	86.18 E7.751 0.0 49.201	. D*0 . 59*2296 - E0*7106	10,5341 11,2115 0,0 65,7281	2006–3999 8000 OR NORE ALL VELURES
86,150	41, E91	61,646	7E.71	\$6*E65DT 88*815E	01.0251	6661-0002 6661-0001 666-005
\$2*U91	65.21	15.121	15,00	82'98+2	11.165	0-499 911
01.096		19.889	0°D	16*22151	94.5916	VEL VOCUMES
59.28 - 01.1881 - 0.0	20,005 81',191	28,019 21,403	65,091	10364,28	76.1272	\$000-3999 \$000-1999
0.0	0.0	0.0 0.0	0.0 0.0	0.0	0*0 0*0	665-005 665-005
21.46101	****572	91 664	99*181	11111501		9961
00*556 00*556	\$0.205 0.0	£8,207	0.0 15,121	0.0 80,4851 11,5554	0.0 6.42376 0.0 0.0 0.0	4000-1999 4LL VOLUMES ALL VOLUMES
0.0	0.0 0.0 £4.626	0,0 0.0 0.0	D*0	0.0 0.0	0.0 0.0	5000-3000 1000-1000 200-200
3.0	ú*s	0.0	0.0	9,0	0.0	665-0 5961
58'14 <i>L</i>	96°£11	99,118	0.0 0.0	55*007ZT	0*0 5L*0481	SOOD OF MORE
85.84T	11,505	68.657	\$8,87 88,621	57°2551 51°50551 55°9259	11.47.81 41.1781	5000-3888 4000-3888
21 *850 E3 *862 OE *923	67.45 53.61 97.54	44, 815 41, 855 44, 116	15.75 14.23 24.10	20,0222 20,8042 24,4754	65.215 65.215	666-009 666-009 665-0
86.660	58*561	11'589	LL*09T	151/8621	21.1165	1894 VET AGEOMES
96.2EB	# £ * 66 E	683.22	65.641	89.17981 97.58811 0.0	25.46BS	9000 00 HORE 4000-1944
0.0 E2,TSB	0,0 79,281	0.0	25"651	0.0	0.0 SE.FSIE	666 T~DDD1
0.0	0'0	0.0	0,D	0,0	0.0	665-005 665-0
31,752	15:001	P.E.ETE	04,18	86,2002	91°1111	Z SKUJUY JJA
19.254	801	14,516	E0*56 .	55'ST87 60'72'95	£1.6001	6662-0007
0.0 0.0	0.0	0.0	0°0	0*0 0*0	0*0 0*0	666 - 0001 666 - 005 667 - 0
16,410	29*421	96.858	£17£01	49*5298	59*6521	2961 2961 7961 40104E3
50.4696	29'12'L 99'511	28.084	ET.EGI G.O. TI.TGI	89,059a	0.0 18,0721	9000 00 WORE 4000-1666
77,038 0.0	27.521	05.066	0.0	47.46121 0.0	41,2535 0,0	6661-0001
0.0	0.0	0.0	0,0	0.0	0.0	666-005 667-0 1961
PP.0E.0	65.451	92.094	61,811	\$6,20T01	0.0 22.85.74	SOOO OF WORES
08.EPE	95.551	26.868	55,611	02-58001 T0945-20	5284.09	666E-0007
0*0	0.0	0'3	0.0	0.0	0.0	665-0001
0.0	0.0	0-0	0.0	0.0	0-0	665-0 0961
28,752 0.0 28,807	12.421 0.0 129.01	19,022 10,0 10,152	55'671 0"0 99'511	0.0 0.0 01.0111	0.0 0.0 0.0	4000-1999 4000-1999 4000-1999
50,050 24,754	0.0	71,258	06,181	0°0 #8*59581	0°0 95°5605	5661-000Z T000-1666
3.0	0.0	0.0	0.0	0.0	0.0	665-009 665-0
06.E68	00.251	£9.0ET	15***1	72.113E1	T4.1445	FASA VET AGENHES
7L*996	16'691	11,987 0.0	0'0 20'551 0'0	0.0 85.097+1	0.0	2000 4000-3999 380M AU 0008
63°296	99.701 0.6	05 96	- 01'56	6Z*Z5Z9	12,8522	666-005
0*0	0.0	0.0	0.0	0.0	0.0	669-0 8561
97.759	194*58	96.082	0.0	90.6546 0.0	B.0 86.8721	8000 GR.HORE ALL VOLUMES
87.294 87.298	0°0 0°0 26°59	51.657 0.3 55.504	0.0	0.0 0.0 0.0	0.0 SE.61TS	6664-0007 6664-0007 6661-0001
10,78 E5,021	6Z.BI	65-85T	12.26-	19.528 17.7255	59.285	666-005
₽6.4EB2	56°E01	75'675	92,78	£4.1241	1410.22	FART AUTONE? BOOD ON HOME
0°0 75°665	0'0 70'50'5	95,452	95 ° 06	66,848T 0,0	0.0 80.85EI	9904 an quos
76.05. A1.262	56.51 74.13	65.4654 0.0	85 69 0*0	0.0	05,6201	665-0001 665-005
<u>5•a</u>	0-5	0.0	0.0	0.0	0*0	665-0
61 ****	12*68 12*801	12.964	09.7k	0.0	0.0 0.0 01.00E1	8000 DE HOEE 4000-118 HOEE
91,944	QA_£A	62'15' 58'56F 0'0	61.401 07.50	71.2453 0.0	98,8001	5000-3666 5000-3666
0.0	0.0	0.0	0.0	6.0	0.0	666-009 669-0
						5561
0.0	0,0 14,59	0,0 90,152	20,56	0.0 E1.2281	9.0 0E.78EL	9000 08 HORE 9000 08 HORE 9000-1848
0.0 98.86	17.59	0°0 125	50.5e 0.0	0.0 E1.228% 0.0	0.0	5000-3333
0.0	0,0	0.0	0.0	940	0.0	666-005
57.545	65*19	88 486	50.04	95.4055	E>*488	5561 53W0 70K 17V
99*16€	91'6Z	010 16'98E	19.47	12 5995	95.5801 0.0	2000-3999 - 4000-3999 - 4000-3999
26.895	95*69	29.985	0.0 0.0	0.0	0.0	5661-0001
0*0	0.0	0*0	0.0	0,0	0.0	666-006 667-0 6567
98*69€	26,41	0.0 E0.545	0.0 5£.2T	0.0 87.4212	10ee-e0	9000 EE WORE 9000 EE WORE 9000-1666
99.646	26,47	60,58E	SE.87 0.0	87.0518 0.0	0°0 0°0°0	5000-1666 5000-1666 5000-1666
0.0	0.0	0.0	0.0	0.0	0.0	666-009 689-0
99*65E	50-59	0.0	75''59	11-0295	05*5E8	SES VOLUMES
0.0 0.0	0.0	0.0	0.0	0.0	0.0	350M 80 0008
89.68£	50*59	17.825	75,44	0.0	85°5ER 0°0	5606-0007 6661-0001 660-009
0.0	0.0	0.0	0.0	0.0	0.0	669-0
91*98	49.61	0.0 27.18	60.81	50.622	0.0	8000 OR MORE
0.0	5°0	0.0	78°03	999982	04 . T S.S.	2000-3466 5000-3466
0.0	0.0	0.0	0.0	0.0	0.0	665-000T 666-006
	0.0	0.0	0-0			02.6.
/1000 TRUCKS	#3V 0001\	/1000 TRUCKS	VIGDO AEH	VIDDO IBNCKS	V1000 ASH RX EMTZ	104 843
HID AASHO EVLS.						

00,407 85,867 54,504	99.F51	94.5£2 96.878 91.412	24.011 52.011 10.46	88.9659 18.21401 50.5078	28,0005 54,5261	2000 OD WORE \$600 OD WORE	
244,30 244,30	30.0E 30.0E	14.855 16.855 31,145	28,09 28,65 18,55	62,7236 02,7236 90,0427	78.1E2 E3.619 25.7051	5000-3666 10001 200-666	
£5.611	15-11	35'611	ZĞ'ET	าเมาห์ได้เ	96-121	667-0	VEARS ALL
65.28T E4.48T	02*5E1 68*8E1	05'895 65'895	100,92	10270,57	54.50F4 72.5781 54.50F4	BOOD EN HORE 4000-1999	
T8.211 	EB.881.	66,801 66,800	07'171 20'11	1222,04	18,251	5000-3666 1000-3666	
0.0	0.0	0.0	0.0	0.0	0.0	666-005 667-0	7961
10,811	11.111	54.808	65*501	68.12101 68.12101	26.7981 56.7981	ALL VOLUMES ROOD OR MORE 4000-7999	7401
27,828 85,858 0,0	0.0	12,056 0.0	0*0 LE*951	0506111	48.848 01.1725 0.0	5000-3666	
0.0	11'7' 0'0 0'0	0.0	0,0 0,0 64,8E	0°0 0°0	0.0	6661-0001 666-009 667-0	
91 *965	15'66	96,1BA	01,18	90*5918	58*85ET	SOUD CR HORE	5961
0.0	0°0 89'651	0'0 45 185	95'611	0'0	0*0 64*7661	9995-0005	
92.025	56.5E 50.01	81,285 81,285 56,785	28.80 28.80 58.50	56-6166 58-6166	47.ES1 68.048 EB.174	666-009 664-00 664-0	
47 .E44	E9'811	ST.042	22.001	89,7539	16.5211	ALL VELUMES	, 26.5 1.56.5
55°249.	0.0	0*0 HE *845	71, E01 71, E01	0.0 14,28001 50.0816	08.0581 08.0581	380H 80 0008 666E-0002	
90°199 9°0	0.0 6.211	91*9*5 0*0	0.0	0.0	0.0	6661-0001 666-006	
0'0	0.0	0.0	0*6	9.0	65.90at 6,0	VIL VOLUMES	£961
0*0 6**815	98-501 0*0 16*131	61,584 0,0 05,024	71.26 0.0 96.65	0°0 71°9508	12.0271 0.0	980M SO DOOR	
0.9	26.58	0,0	0.0	0.0 0.0 11.0851	0.0 12.5801	5664-0002 5664-0001 566-005	
ú.0	0.0	0,0	0.0	0.0	0.0	669-0	Z96 1
58.46A 94.76A	06,161	06,948 95,884	EZ*Z11	12.66.03 10.66.89	96 ° 660 E	SODE OR HORE	
EL*109	6£*99 90*90) 0*0	11'595 0'0	82'89 0'68	05*5998 20*1596 0*0	29*9921	5561-0002 5000-3666 1000-1666	
0.0	0.0	0.0	0.0	0.0	0*0 0*0	664-0	1961
66.582	0.0 48.4701	68.405	10.50	TT.ETPR	76.52.52	SODO OR HORES	(36)
66*595 #0*029	10,101 70,101	60,484	51.19 16.20	15.462B	1645.34	7000-1944 5000-3944	
0*0 0*0	0.0	0*0 0*0	0.0 0.0 0.0	0.0	0.0	6661-0001 666-005 667-0	
£1.851	60*4*1	££*129	15521	E5'5[5]]	88,6065	BOOD OF MORE	0961
16.45B	14.605 17.605	80,148 88,978 0.0	0.57 00.00 0.00	6*0 08*56051 £0*1660	0°0 67'087E	\$000-1000	
0.0	0.0	0*0	0.0	0.0	0.0	566-005	
91.844	78,711	66'875	61.501	CS.DIE6	90,5571	664-0 SƏWOTDA 77V	1959
19.650	0°-3-	94.55.8 94.55.8 0.0	0.0	0 0 B£ 6076	0.0 0.0 0.0	2000-3999 4000-3999 300M AD 0008	
28*559 0*0	0*0 0*0	0.0	0°0 0°0	0.0 0.0	0.0	6661-0001 666-009	
0.6	0.0	0.0	0.0	75.0£70 0.0	0°0 52°155T	569-9 528077A 77V	8561
67,488 0.0 18,154	0.0 0.0	55.852 0.0 9.942	17.101 B5.28	70960T 70960T 9675200T	0.0	9000 OB WORE 4000-1436	,,
19.661	65'011 65'11	13,614	69°11	16"2EST 26"3EST	96'9551 66'161 82'865	5600-3005 1000-1948	,
17.421 11.425	98'51	98.321	14.85	58 19902	05'561	665-0	1561
56*585 U*U 0*U	04.0 04.0 118,91	99'926 91'989	09°L01	99*09EB 0*0 9E*6056	0.0 0.0 51.9551	PTT ADDOMES #000-1000 #000-1000	•
0.0	50,00 FD,90	0.0 AL-514	18.50	0.0	O. O. Let	5000-3666 1000-1666	
0*0	0.0	0.0	0.0	0.0	0.0	666-005 669-0	9561
£6*185	02.501	75.042	6£'86	15.2078	77.8521	ACCOUNTS ACCOUNTS	
88.085 87.788	58*££1 62*99 .0*0	64.5£ 64.84£	0,0 65.24 72.51	99.6466 96.4346 9.0	0.0 15.6605	1000-1666 1000-1666	
0*0 0*0	0*0 0*0	0.0	0.0	0.0	0.0	666-003 664-0	5561
	99*55	08.4225	58*26	£9,2777	98.5861	VFF AGFOWEZ	2501
25.572 0.0 21.652	15.57 26.601 0.0	D*0	0.0	0°0 91'98'78 18'9971	0°0 89°4212 1018°06	8000 DE HOEE ***********************************	
0*0 0*0	0.0	98'565 0'0 0'0	0.0 0.0 00.0	0.0	0.0	7000-3000 7000-1000 700-000	
0+0	0.0	G.D.	0*0	0.0	0.0	0-488 VII AOFINES	<b>7561</b>
0.9 A8.1AP	60°651	0,0	0*0 0*0 124°10	0.0	0.0	8000 DR HORE	
18*915	55,58	E5*205	0.0	65*95EL 0*0 0*0	0.0 0.0	5000-3888 1000-3888 200-888	
0*0	0.0	0.0	6°0	0.0	0.0	666-005 666-0	£561
69°069	0.0 60.89	95°575 0°0	0°0	0.0 0.0 88.8F01	99°58°1 0°0 1888°58°1	BOOD OR HORE ALL VOLUMES	
0.644 18.644	71,77	02.16A 02.16A	0.0 80.87 08,581	86.0866	TS. 401.1	5000-1999 1000-1999	
6*0	0.0	0.0	0.0	0.0	0.0	666-005 669-0	1952
0.0	0°0	71.0s2	0.0 0.15	0.0	0.0	POOD DE NOSE	
15*525	01.88 01.88	12.21. A1.P5.	5E*ETT 76*E9 0*0	98.720a 38.2264	97.9E0	6662-0007 660E-0007	
0.0	0.0	0.0	0.0	0.0	0.0	666-005 669-0	1
		(P.TS)	96*52	21°5E81		BOOD OR HURES	1661
0.0 55.075	1,86 74,04 0,0	11,99 -264,32	50.51	95*5666	0.0 95.4201 0.0	5662-0005 2000-1999	
0.0	0.0	0.0	0.0	0.0	0.0	666-005 667-0	
0.0	0*0	8*0					0561
MOD &&SHO. EWLS 11000 TRUCKS	NOD 445HD, EMIS.	VIBOD TRUCKS	VIOOD KEH	KY ENLS /1000 TRUCKS	KY EMLS	TOA	86.32

00,00£ 80,282 80,737 63,274	75*15 75*971 75*87 15*55	67.948 22.584 70.154 63.984	00,84 00,91 85,501 98,61	64.48.4 01.145.7 50.49916.1 17.4899	40,20P 12,6011 64,5155 68,9461	8000 CH WURE 8000 CH WURE \$000-3888	
67.645 47.746 94.6401 00.066	19*95 80*95 E6 61	62,435 62,456 64,605 61,446	26.051 04.52 56.051	11.050+ ->0.80+ ->0.80+ ->0.60+ ->0.60+ ->0.60+	62,791 62,791 62,811 60,8584	6661-0001 666-005 665-0	
							YEAR'S
14,774 29,7201 88,778	59 E11 52 651	20,235 59,235 60,198	17.251 71.301	24,67,82 36,45,91 36,75,41	0.0 67.889 60.5606 05.7865	8000 OB NURE 8000 OB NURE 7000 PT NURE	
0.0	0'0	0.0	0,0 0,0 0,0	0.0	0.0 0.0 0.0	\$000-3666 \$00-366	
0°0	0.0	0.0	0 · D	0.0	0.0	669~0	7951
75,620 15,620 15,168	99°921 71°051 89°921	42.458 65.101	06'86 14'011 91'55	36,1584 26,1584 16,89881	£8.40P E4.1783 E6.410s	ANDO DO BENEVALES	~~
7,0	0.2	- 6.5°	0.0	0.0 0.0	0.0 0.0 0.0	6664-0002 6661-0001 660-009	
0.0	0.0		٠٠٠	0*0	0.0	669-0	6961
168,16 10.48 168,16	66.811 0.9 69.811	#\$ '556 	0.0 61.601 TI.00	0.0 5.10651 5.10651	0.0 (5.0015 86.0185	6647-0004 8984 90 0008 8980-104 114	
96-559	95.025 94.01	10.0501	66 85 06 681 66 75	90.69044	96*8111 65'8811	5000~3000 100001	
50,435 46,986	90, e 50, e 2	16,881 AB.016	16.8	91,8121 1415,14	29,511	666-005 664-0	<del>9951</del>
82*628	21.621 0.0 25.481	0+,0E1 0+0 20.4+4	67.541 0.9 E7.541	21.597£1	07'1E+8 0'0 61'10+16	9000 EE MURE 4000 EE MURE	
3°167	15,12	0.0 115.00£	D.U.	0.0	0.0 41.0416 9.10416	566E-0002	
0.9	6.0	0.0	0°0	0.0	0.0	665-005 665-0	£961
7.0.27 B	17.581. 77.851	02.583	76'211		0.0 Re-1600 67.2526	P897-000A BDM AJ 0098 SHUJOV JJA	
	0.0	0'3 78'FU7 0'0	0.0 T2.4A C.0	0.0 0.0 65.6644 0.0	66,525T	1000-1999 1000-1999	
0 °0	0,1 0,0	0.0	0.0	0.0	0.0	664-006 664-0	2961
50°215	88.71	11.082 	52'79 26'08	34,4250	59*15Z1 15*0951 50*99*	VEL VELUMES BODO OR MORE	
3*3 0*0	0.0 E2.48	22+962	15'2E 0'0 0'0	00'1977	0.0	4060-0005 6666-0002 1000-000 200-006	
7.0	0.0	0.0	0.0	0.0 0.0 0.0	0.0	666-009 665-0	1961
56.118	52,87 58,88	70'ESV	61,18	1948,05	05*7501	MOOD DE MORE	
9.0 9.0	0'0	0*0	0*0 61*15*	0,0 0,0	67.653	5000-3333 5000-3333	
0*0 0*0	0.0	0,0 0,0	0,0	0.0	8*0 6*0	5551-0001 656-005 567-0	7890
15*245	16.00	11.716	10.22	11,295g 00,197g	45.95.1	SOUD OR MURE	0 4 9 1
00.51.4 7.7 56.61.4	U*U E5*E9	U*0	25,15	0.0	0.0	6662-0005 5000-3666 1000-1666	
3*0 3*0 3*0	0.0	0.0 0.0	0.0	0,0 0,0 0,0	0.0 0.0	665-005 665-0	
36,564	25'611 0'0	55.822	£9'15	87,9519	+5 ' £65 T	PUR ANTINES	6561
78-355 PP,157 0.0.	61,951	19'059 58'960	56.551 67.54	10648169	0.0 27.080 76.005	6661-0005	
3*0	0°0 0°0	0'0 0'0	0.0	0.0	0.0	6661-0001 666-005 669-0	
51'95v	49°07.	44.814	5£'59	81,1917	£9'VIII	ALL VOLUMES BOOD OR NORE	8561
03*196 55*19E	95'861 95'861	0°.005 66'005	18.49	*D*Z5Z0	10,2621	9995-0004	
78.29E 78.29E 26.02S	21.FC 15.24 21.56	19.46£ 19.46£	27,20 20,50 76,60	19*18% 87 '2057 00' 0695	981.394 21.489 21.489	6661-0001 666-005 665-0	
†U*€8†	ZB.43	#2*69b	61,50	25.8125 25.2857	05*B30I	WIT ADENWES	1561
95°859	£1.44 £8.44 £7.48	50,214 25,000 25,000	- 66.66	91,1888	59.585	6661-0007 6661-0001	
0.0	0.0	0.0	6*D 0*0 0*0	0.0	0.0	664-009 664-0	
0°0 (0'2£†	09*99	14,210	05'EG 0'0	99.1099	67,E58	ALL VOLUMES	9961
0°0. 53°255	0°0 09°55	14,812	0.0	99'1059	67,478	6000-3333 5000-3333 7000-1333	
3,0	0*0 0*3	0*0 0*0	0.0 0.0	0.0	0.0	666-809 667-0	
J*ü	0.3			16,0103	65,859	SHULDV 11A	9561
95°5E7	81.70 0.0 81.70	61.854 0.0 01.854	0'0 66'59"	0.0	65 556	9804 80 0009 4667-0009	
\$5*SE+	5*D	0.0	0.0	0.0	0.0	5686-0007 1000-3888 200-888	
	0°0	0.0	0.0	T0.8262	0.0	Sawnada 11V	<b>456</b> 1
9*0 9*0	71.50 0.0 11.50	0,5 0,5 K1,605	10,14 0,0 10,14	0,0	88.158	2000 08 HORE	
3.0	0.0	0.0	0.0	0*0 0*0	0.0	6661-0001 666-009	
0 '0 0 '0	D.0.	0.0	0.0	0.0	0.0	665-0 5200704 778	ESST
3.9	6.0 14.02	0°0 16°52E	76.64 0.0 76.64	49.086.4 0.0 0.0	0.0	240M AD 0008	
0,0 La.5SE	0.0	0*U	0.0	0.0	0°0	566E-000Z 1000-1288	
0.0	0.0	0.0	0.0	0 * D	0.0 0.0	665-005 665-0	7625
0.0 0.0	0 * 0	45.524 0.0 16.22£	0.0 6.82	0.0 PT.4852	0,0	8000 08 HORE	
24.908 00.521	25.25 73.28	02*151	60.25	0.0 0.0 0.0	0.0 0.0	6661-0007 6661-0001 666-009	
0.0	0.0	0.0	0.0	0.0	0.0	565-0 534673A-115.	1561
TS+251	0,0	0.0 A6.551	0.0	0.0 0.0	0.0 0.0 47.5£4	9801-0004 9804 90 0008	
240,23 12.21	60.82 10.5	25.045 62.045	+0°86 0°0	\$5.14PE	66.62	5000-3888 1000-1888 200-888	<del></del>
0*0 0*0	0.0	0.0	0.0	0.0	0.0	669-0	DS6T
/1000 TRUCKS	/ TOOD AEH	VIODO INDEKS	\TOOD AEH	/1000 IRUCKS	\1000 AEH	TOA	. AABY
	Z IN 3 OFFS VV ORF	SANA DH244	SAME GHEA.	XX EMLS	2 102 44		

## APPENDIX D

AVERAGE VEHICLE-TYPE PERCENTAGES AS A FUNCTION OF LOCAL CONDITIONS

LOCAL   CODE   CARS   BUSES   SU-ZA-41   SU-ZA-61   SU-3A   C-3A   C-4A   C-5A   C-6NOTITION				,,,,,,	RURAL K	ICLE TYPE ENTUCKY HI 1950-1966					
ROAD 1 70.993 0.311 4.838 5.387 0.700 2.363 11.092 4.316 TYPE 2 71.523 0.920 8.542 8.450 1.043 4.508 4.255 0.740 3 72.692 0.649 13.848 9.981 0.864 0.992 0.830 0.190 4 774.697 1.045 14.707 7.769 0.329 1.037 0.210 0.000 DIREC- 1 71.648 0.884 8.614 8.302 0.885 4.255 4.472 0.930 TION 2 71.697 0.016 9.902 8.861 1.198 3.399 3.418 0.610 DIREC- 1 71.648 0.884 8.614 8.302 0.885 4.255 4.472 0.930 TION 2 71.697 0.016 9.902 8.861 1.198 3.399 3.418 0.610 DIREC- 1 71.658 0.885 8.812 8.459 1.072 4.120 4.360 0.908 RDUTE 2 71.366 0.855 8.812 8.459 1.072 4.120 4.360 0.908 SERVICE 1 79.656 0.365 11.118 5.097 0.312 2.363 0.741 0.349 RCOVIDED 2 74.003 0.325 11.766 7.911 1.598 0.868 2.293 1.235 TION 3 71.501 0.923 8.967 8.364 0.827 3.704 4.858 0.858 4 73.096 0.789 8.333 8.067 0.747 3.997 4.152 0.809 5 6 6.00105 0.739 12.656 13.171 7.373 1.472 2.813 1.492 5 6 6 0.0105 0.739 12.656 13.171 7.373 1.472 2.813 1.492 T 7 11.687 1.468 1.380 0.393 1.2056 13.171 7.373 1.472 2.813 1.492 T 7 11.687 0.884 1.897 0.303 1.197 0.253 0.979 0.255  VOLUME 1 6.9.057 1.123 17.709 10.870 0.228 0.775 0.187 0.187 0.909 T 7 7 11.687 0.884 1.8777 11.929 0.668 2.293 1.035 0.187 0.187 0.188 1.997 0.750 0.188 0.779 1.057 0.750 0.188 0.779 0.774 0.774 0.775						1420-1466					
ROAD 1 70,993 0.311 4.8385 5.387 0.700 2.365 11.092 4.316  TYPE 2 71.523 0.920 8.5942 8.5450 1.053 4.506 1.205 0.740 3 72.692 0.6049 13.648 9.981 0.864 0.942 0.830 0.100 4 776.997 1.095 14.707 7.769 0.329 1.037 0.210 0.005  DIRECT 1 71.648 0.884 8.614 8.302 0.885 4.255 4.772 0.930  TION 2 71.697 0.016 9.902 8.861 1.198 3.399 3.478 0.614  ALI 1 71.502 0.933 9.370673 0.837 4.297 3.624 0.759  ROUTE 2 71.366 0.855 8.872 8.459 1.072 4.120 4.360 0.902  SERVICE 1 79.656 0.365 11.118 5.097 0.312 2.363 0.741 0.349  ROUTE 2 75.003 0.325 11.766 7.911 1.598 0.868 2.293 1.235  SERVICE 1 79.656 0.365 11.118 5.097 0.312 2.363 0.741 0.349  ROUTE 2 75.003 0.325 11.766 7.911 1.598 0.868 2.293 1.235  4 73.096 0.789 8.333 8.067 0.747 3.997 4.125 0.809 5 66.629 0.894 9.554 9.402 1.271 4.714 4.72 0.859 6.604 9.504 9.		CODE	CARS	BUSES	SU-2A-41	SU-ZA-6T	SU-3A	C-3A	C-4A	C-5A	TOTAL VEH
THE STATE OF THE S	ROAD	1								4.316	341175
DIREC- 1 71.648 0.884 8.614 8.302 0.885 4.255 4.472 0.930  TION 2 71.697 0.816 9.902 8.861 1.198 3.399 3.478 0.691  ALT 1 71.502 0.933 9.370 3.673 0.837 4.297 3.624 0.799  ROUTE 2 71.346 0.855 8.872 8.459 1.072 4.120 4.360 0.908  3 74.825 0.717 10.293 8.538 0.796 1.491 3.079 0.250  SERVICE 1 79.656 0.365 11.118 5.097 0.312 2.363 0.741 0.349  ROVIDED 2 74.003 0.325 11.766 7.911 1.598 0.868 2.293 1.235  4 73.096 0.789 8.333 8.067 0.747 3.997 4.152 0.809  5 68.629 0.894 9.534 9.402 1.271 4.914 4.421 0.930  6 6 60.105 0.733 12.655 13.717 7.573 1.472 2.815 1.464  7 71.867 1.465 13.809 8.333 1.001 1.360 1.369 9.167  8 8 60.579 1.030 5.209 5.888 0.277 1.446 1.275 0.295  9 65.532 0.089 1.957 8.768 0.358 0.277 1.446 1.275 0.295  4 73.096 0.739 12.655 13.717 7.573 1.472 2.815 1.466 1.525  VOLUME 1 69.057 1.123 17.709 10.870 0.828 0.775 0.187 0.059  5 7 7.1867 1.465 13.809 8.333 0.067 0.779 10.556 1.552  VOLUME 1 69.057 1.123 17.709 10.870 0.828 0.775 0.187 0.059  5 7 7.728 0.884 15.777 1.429 0.689 2.2192 2.551 0.350  4 7 7.928 0.889 15.777 1.429 0.689 2.2192 2.551 0.350  5 7 7.728 0.889 15.777 1.828 0.768 0.776 0.308 0.779 0.508 0.750  5 7 7 7 1.867 0.885 15.777 1.429 0.689 2.2192 2.551 0.350  4 7 7 1.973 0.629 6.644 7.222 0.969 3.414 6.967 0.187 0.050  7 7 1.973 0.629 6.644 7.222 0.969 3.414 6.967 0.187 0.258  4 7 1.973 0.629 6.644 7.222 0.969 3.414 6.967 0.190  7 7 1.973 0.629 6.644 7.222 0.969 3.414 6.967 0.190  7 7 1.973 0.629 6.644 7.222 0.969 3.414 6.967 0.190  7 7 1.973 0.629 6.644 7.222 0.969 3.414 6.967 0.190  7 7 1.973 0.629 6.644 7.222 0.969 3.414 6.967 0.190  7 7 1.973 0.629 6.644 7.222 0.969 3.414 6.967 0.190  7 7 1.973 0.629 6.644 7.222 0.969 3.414 6.967 0.190  7 7 1.973 0.629 6.644 7.222 0.969 3.414 6.967 0.190  7 7 1.973 0.629 6.640 9.916 7.988 1.339 3.448 4.704 1.241 0.790  7 7 1.984 0.895 7.995 7.825 0.968 0.492 3.611 2.688 1.349 0.258 0.759 0.248 0.759 0.248 0.759 0.248 0.759 0.248 0.759 0.248 0.759 0.248 0.759 0.248 0.759 0.248 0.759 0.248 0.759 0.248 0.759 0.259 0.259 0.259 0.259 0.259 0.250 0.251 0.	TYPE										5196622
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SERVICE 1 79.656 0.365 11.118 5.097 0.312 2.363 0.741 0.349 ROVIDED 2 74.003 0.325 11.766 7.911 1.598 0.668 2.293 1.255 3 71.501 0.923 8.967 8.364 0.827 3.704 4.658 0.828 4 73.096 0.789 8.333 8.067 0.77 3.704 4.658 0.828 5 68.629 0.884 9.534 9.504 1.271 4.914 4.621 0.930 6 0.0015 0.739 12.656 13.171 7.573 1.472 2.815 1.464 7 711.867 1.465 13.809 8.933 1.010 1.360 1.369 0.187 8 8 80.579 1.030 5.209 3.888 0.277 1.446 1.275 0.256 9 65.532 0.085 11.557 8.766 0.553 0.979 10.596 1.552  VOLUME 1 69.057 1.123 17.709 10.870 0.228 0.775 0.187 0.596 1.0016 0.005	ROUTE										4340900
NOVIDED   2		3	74. 825	0.717	10.293	8,538	0.796	1.491	3.079	0.250	486325
71,501 0,923 8,967 8,364 0,827 3,704 4,858 0,855 4 73,096 0,788 8,333 8,067 0,774 3,997 4,152 0,809 5 88,629 0,894 9,534 9,402 1,271 4,914 4,421 0,930 6 6 60,105 0,739 12,656 13,171 7,573 1,472 2,815 1,466 1,369 0,187 7,71,867 1,465 13,809 8,933 1,010 1,360 1,369 0,187 8 8 80,579 1,030 9,209 5,888 0,277 1,446 1,275 0,286 9 5,532 0,085 11,957 8,766 0,555 0,979 10,596 15,532 0,085 11,957 8,766 0,555 0,979 10,596 1,532 0,085 11,957 8,766 0,555 0,979 10,596 1,532 0,085 11,957 8,766 0,555 0,979 10,596 1,532 0,085 11,957 8,766 0,555 0,979 10,596 1,532 0,085 11,957 8,768 0,265 1,343 0,610 0,100 3 0,728 0,899 12,148 10,780 0,662 2,182 2,531 0,359 1,535 0,579 1,064 0,967 10,027 8,788 1,125 3,607 3,606 0,750 5 70,762 1,026 8,661 8,537 1,266 5,341 3,949 0,453 0,610 0,100 1,0										0.349	12717 67011
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5 68,629 0,894 9,524 9,402 1,271 4,4914 4,421 0,930 7 7 71,867 1,465 13,809 8,933 1,010 1,360 1,369 0,187 8 8 80.579 1,030 9,209 5,888 0,277 1,464 1,275 0,256 9 65,532 0,085 11,557 8,766 0,553 0,979 10,596 1,532											3343836
6 60.105 0.739 12.656 13.171 7.573 1.472 2.815 1.406 7 71.867 1.465 13.809 8.933 1.010 1.300 1.369 0.168 8 80.579 1.030 9.209 5.888 0.277 1.446 1.275 0.296 9 65.532 0.085 11.957 8.766 0.553 0.979 10.596 1.532  VOLUME 1 69.057 1.123 17.709 10.870 0.228 0.775 0.187 0.051 2 69.167 0.884 15.777 11.429 0.669 1.343 0.610 0.100 3 70.238 0.899 12.148 10.780 0.462 2.182 2.531 0.359 4 71.064 0.967 1.027 8.788 1.126 3.667 3.606 0.755 5 70.762 1.026 8.661 8.537 1.266 5.341 3.949 0.453 6 71.297 0.750 8.327 8.281 0.974 4.537 4.920 0.908 7 71.973 0.629 6.644 7.522 0.969 3.444 6.967 1.611 8 77.004 0.763 6.423 4.244 0.643 3.083 4.320 1.520 9 800.251 0.681 5.884 5.058 0.462 3.611 2.688 1.344 10 78.998 0.526 7.328 6.415 0.453 4.114 2.539 0.228  MAGW 1 74.125 0.529 14.967 9.145 0.469 0.404 0.313 0.048 2 71.018 1.153 9.261 9.771 0.870 7.009 0.879 0.032 3 71.763 0.791 8.435 8.101 1.079 2.978 6.598 0.224 4 72.032 0.556 8.702 6.943 1.208 1.289 5.679 3.586  AREA 1 70.693 0.641 9.916 7.998 1.339 3.458 4.704 1.241 2 72.032 0.556 8.702 6.943 1.208 1.289 5.679 3.586  VEAR 1 69.257 1.348 9.349 11.227 0.521 7.810 0.467 0.010 3 70.252 1.111 9.188 9.807 1.190 7.329 1.018 0.036 4 71.554 0.889 9.709 7.095 7.625 0.836 4.912 4.421 0.755 5 73.498 0.704 8.905 7.669 0.651 7.359 0.958 4 71.554 0.858 8.805 0.651 7.359 0.958  VEAR 1 69.257 1.348 9.349 11.227 0.521 7.810 0.467 0.010 5 73.498 0.704 8.905 7.669 0.655 2.549 5.994 0.002 5 73.498 0.704 8.905 7.669 0.655 2.549 5.994 0.002 6 71.554 0.858 8.807 8.807 1.190 7.329 1.018 0.030 6 71.554 0.858 8.807 8.807 1.190 7.329 1.018 0.030 6 71.554 0.858 8.807 8.807 1.190 7.329 1.018 0.030 6 71.554 0.858 8.807 8.807 1.190 7.329 1.018 0.030 6 71.554 0.858 8.807 8.807 1.190 7.329 1.018 0.030 6 71.554 0.858 8.807 8.807 1.190 7.329 1.018 0.030 6 71.554 0.858 8.807 8.807 1.190 7.329 1.018 0.030 6 71.554 0.858 8.807 8.807 1.190 7.329 1.018 0.030 6 71.554 0.858 8.807 8.807 1.190 7.329 1.018 0.030 6 71.554 0.958 8.807 8.808 0.916 4.225 4.025 0.955 6 72.487 0.562 0.913 9.048 8.268 0.916 4.225 4.025 0.955										0.930	1370128
## 8				0.739	12.656	13.171	7.573	1.472	2.815	1.469	74622
VOLUME 1 69.057 1.123 17.709 10.870 0.228 0.775 0.187 0.051 2 69.167 0.884 15.777 11.429 0.689 1.343 0.610 0.100 3 70,238 0.899 12.148 10.780 0.862 2.182 2.531 0.359 4 71.064 0.967 10.027 8.788 1.126 3.607 3.606 0.750 5 70.762 1.026 8.661 8.537 1.266 5.341 3.949 0.453 6 71.297 0.750 8.327 8.281 0.974 4.537 4.920 0.908 7 71.973 0.629 6.644 7.522 0.969 3.484 6.967 1.811 8 77.004 0.763 6.423 5.244 0.643 3.1083 4.320 1.520 9 80,251 0.681 5.884 5.058 0.482 3.611 2.688 1.344 1.0 780 0.750 8.327 8.241 0.974 4.537 4.920 0.908 9 80,251 0.681 5.884 5.058 0.482 3.611 2.688 1.344 1.0 78.398 0.526 7.328 6.415 0.455 4.114 2.539 0.228 4.2 71.018 1.153 9.261 9.771 0.870 7.009 0.879 0.228 4.2 71.018 1.153 9.261 9.771 0.870 7.009 0.879 0.032 3 71.763 0.791 8.435 8.101 1.079 2.978 6.598 0.248 4.72.032 0.556 8.702 6.943 1.208 1.289 5.679 3.566 4.728 6.945 0.885 0.482 3.611 2.884 6.967 1.728 6.729 0.728 4.72.032 0.899 7.095 7.825 0.685 4.912 4.421 0.785 4.72.032 0.556 8.702 6.943 1.208 1.289 5.679 3.566 6.7028 6.943 1.208 1.228 6.228 6.949 6.940											251972
VOLUME         1         69,057         1.123         17,709         10.870         0.228         0.775         0.187         0.051           2         59,167         0.884         15,777         11.429         0.689         1.343         0.610         0.100           3         70,238         0.899         12,148         10.780         0.862         2.182         2.331         0.359           4         71,064         0.967         10.027         8.781         1.126         3.667         3.060         0.750           5         70,762         1.026         8.661         8.537         1.266         5.341         3.949         0.453           6         71,297         0.750         8.227         8.281         0.974         4.537         4.920         0.908           7         71,973         0.629         6.644         7.522         0.969         3.484         6.967         1.811           8         77,004         0.763         6.423         6.244         0.643         3.603         4.220         1.529           9         80,251         0.681         5.884         5.086         0.469         0.404         0.313         0.046 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>84805 2350</td></t<>											84805 2350
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5 6.512 0.588 3.713 3.065 1.113 1.947 4.599 0.116 796518 6 7.7797 0.488 3.857 3.562 4.465 1.629 4.785 0.759 761350 7 6.568 0.539 3.811 4.941 1.722 1.070 5.205 1.430 758579 8 6.803 0.515 3.968 2.788 2.391 0.787 3.369 3.094 804565 9 5.714 0.492 4.000 2.452 0.824 0.800 2.184 4.581 360840  SEASON 1 7.621 0.626 3.820 4.097 3.217 4.619 4.889 2.141 1183755 2 5.501 0.601 3.824 3.136 1.599 4.375 4.318 1.439 1460505 3 6.715 0.566 3.963 4.171 2.790 3.337 3.568 2.268 2061552 4 6.539 0.603 3.839 3.740 1.260 4.163 4.865 2.574 1385446		CONTRACTOR CONTRACTOR									
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7 6.568 0.539 3.811 4.941 1.722 1.070 5.205 1.430 758579 8 6.803 0.515 3.968 2.788 2.391 0.787 3.369 3.094 804565 9 5.714 0.492 4.000 2.452 0.824 0.800 2.184 4.581 360840  SEASON 1 7.621 0.626 3.820 4.097 3.217 4.619 4.889 2.141 1183755 2 5.501 0.601 3.824 3.136 1.599 4.375 4.318 1.439 1460505 3 6.715 0.566 3.963 4.171 2.790 3.337 3.568 2.268 2061552 4 6.539 0.603 3.839 3.740 1.260 4.163 4.865 2.574 1385446											
8 6.803 0.515 3.968 2.788 2.391 0.787 3.369 3.094 804565 9 5.714 0.492 4.000 2.452 0.824 0.800 2.184 4.581 360840  SEASON 1 7.621 0.626 3.820 4.097 3.217 4.619 4.889 2.141 1183755 2 5.501 0.601 3.824 3.136 1.599 4.375 4.318 1.439 1460505 3 5.715 0.566 3.963 4.171 2.790 3.337 3.568 2.268 2061552 4 6.539 0.603 3.839 3.740 1.260 4.163 4.865 2.574 1385446		7									
SEASON         1         7.621         0.626         3.820         4.097         3.217         4.619         4.889         2.141         1183755           2         5.501         0.601         3.824         3.136         1.599         4.375         4.318         1.439         1460505           3         6.715         0.566         3.963         4.171         2.790         3.337         3.568         2.268         2061552           4         6.539         0.603         3.839         3.740         1.260         4.163         4.865         2.574         1385446			6.803	0.515	3.966	2.788	2.391	0.787	3.369	3.094	804565
2 6.501 0.601 3.824 3.136 1.599 4.375 4.318 1.439 1460505 3 6.715 0.566 3.963 4.171 2.790 3.337 3.568 2.268 2061552 4 6.539 0.603 3.839 3.740 1.260 4.163 4.865 2.574 1385446		9	5.714	0.492	4.000	2,452	0.824	0.000	2.184	4.581	360840
2 6.501 0.601 3.824 3.136 1.599 4.375 4.318 1.439 1460505 3 6.715 0.566 3.963 4.171 2.790 3.337 3.568 2.268 2061552 4 6.539 0.603 3.839 3.740 1.260 4.163 4.865 2.574 1385446	SEASON		7.621	0.626	3.820		3.217	4.619	4.889	2.141	1183755
3 6.715 0.566 3.963 4.171 2.790 3.337 3.568 2.268 2061552 4 6.539 0.603 3.839 3.740 1.260 4.163 4.865 2.574 1385446							1.599				1460505
									3.568	2.268	2061552
A V E B A C E S 7,123 A.A14 3,87A 3,80G 2,382 4,183 4,274 3,165		•	76599	0.000	26029	39140	16600	44103	4.800	4.514	1303446
	AVEDA	2 F C	7,123	0.616	3.874	3.899	2.382	4.153	4.374	2.158	

FOCYT CONDITIONS
VAEKYGE NNIL EMF.8 V8 V ENNCLION OE

APPENDIX E

UNIT EWL'S

## VEHICLE TYPE SU-2A-4T

			CKY					TOTA
CONDITION		MEAN	STD DEV	МЕАМ	STD DEV	MEAN	STD DEV	VOLU
ROAD	1	0.0	0.0	0.0040	0.0	0.0040	0.0	19
TYPE	2	0.0406	0.7016	0.0063	0.0331	0.0063	0.0331	1046
	3	0.0533	0.2558	0.0054	0.0061	0.0054	0.0061	172
	4	0.0	0.0	0.0	0.0	0.0	0.0	
DIRECT-	1	0.0475	0.8253	0.0065	0.0389	0.0065	0.0389	657
ION	. 2	0.0329	0.1679	0.0055	0.0055	0.0055	0.0055	577
ALT	1	0.0945	1.0063	0.0084	0.0471	0.0084	0.0471	562
ROUTE	2	0.0052	0.0279	0.0045	0.0022	0.0045	0.0022	663
	3	0.0	0.0	0.0042	C.0007	0.0042	0.0007	<u> </u>
SERVICE	1	0.0	0.0	0.0	C.O	0.0	0.0	
PRCVIDED	2	4.0000	6.9282	0.1925	0.3265	0.1925	0.3265	ě
	3	0.0095	0.0378	0.0049	0.0031	0.0049	0.0031	204
	4	0.0106	0.0589	0.0049	0.0040	0.0049	0.0040	553
	5	0.0039	0.0128	0.0044	0.0011	0.0044	0.0011	423
	6	0.0	0.0	0.0040	0.0	0.0040	0.0	12
	7	0.4062	0.5828	0.0145	0.0133	0.0145	0.0133	35
	8	0.0 0.0	σ.0 0.0	0.0	0.0	0.0 0.0	0.0	
NOT UNE	,	0.0	0.0	0.0041	0.0004	0.0041	0.0004	52
VOLUME	2	0.0	0.0113	0.0041	0.0004	0.0041	0.0014	87
	3	0.1053	0.3329	0.0072	0.0085	0.0072	0.0015	111
		0.1625	1.5534	0.0121	0.0003	0.0121	0.0732	205
	5	0.0035	0.0104	0.0044	0.0010	0.0044	0.0010	282
	6	0.0083	0.0435	0.0047	0.0034	0.0047	0.0034	359
	ř	0.0272	0.1079	0.0060	0.0068	0.0060	0.0068	93
	. 8	0.0	0.0	C.0040	0.0	0.0040	0.0	36
	ğ	0.0	0.0	C.0046	0.0008	0.0046	8000.0	4
	10	C.C	0.0	0.0	0.0	0.0	0.0	
MAGW		0.0	0.0	0.0041	0.0003	0.0041	0.0003	134
	2	C.0159	0.0663	0.0052	0.0046	0.0052	0.0046	525
	3	0.0258	0.1656	0.0050	0.0043	0.0050	0.0043	457
****	4	0.2042	1.7772	0.0139	0.0837	0.0139	0.0837	116
AREA	1	0.1220	1.3475	0.0100	0.0635	0.0100	0.0635	283
	2	0.0055	0.0340	0.0045	0.0026	0.0045	0.0026	231
	3 4	0.0118	0.0625	0.0050	0.0041	0.0050 0.0053	0.0041 0.0048	310 409
YEAR	1	0.0143	0.0388	0.0052	0.0030	0.0052	0.0030	171
	2	0.0033	0.0110	0.0043	0.0010	0.0043	0.0010	189 118
	3	0.0425	0.1222	C.0072 0.0041	0.0082	0.0072 0.0041	0.0082 0.0003	118 374
	<u>4</u> 5	0.0151	0.0515	0.0054	0.0040	0.0054	0.0003	90
	6	0.0151	0.0	0.0042	0.0003	0.0054	0.0003	85
	7	0.0	0.0	0.0042	0.0006	0.0042	0.0006	44
	é	0.2749	1.8140	0.0041	0.0849	0.0157	0.0849	135
	<u> </u>	0.0078	0.0202	0.0051	0.0023	0.0051	0.0023	25

UNIT ENL'S
VEHICLE TYPE SU-2A-6T

LOCAL CONDITION	CODE	KENT MEAN	UCKY STD DEV	AAS HEAN	HO STD DEV	MODIFI MEAN	ED AASHO STD DEV	TOT: VOLUE
COMBILION		ILLEHA	01.1 21.1	7.23, 2.				
ROAD	1	2.2685	0.5453	C.1587	0.0281	0.1587	0.0281	153
TYPE	2	3.1048	3.3595	0.1807	0.0858	0.1807	0.0858	2041
	3	4.5115	8.4677	0.1751	0.1189	0.1751	0.1189	14
,	4	0.0	0.0	0.0	0.0	0.0	0 - 0-	
DIWECT-	1	3.0705	3.1701	C.1807	C.C888	0.1807	0.0888	1340
ION	2	3.3920	5.2869	0.1756	0.0855	0.1756	0.0855	99.
ALT	1	3.3950	5.4725	C.1759	0.0894	0.1759	C.0894	91
ROUTE	2	3.0805	3.1475	0.1796	0.0860	0.1796	0.0860	138
	3	3.1264	1.8013	C.1995	0.0966	0.1995	0.0966	3
SERVICE	1	0.0	0 • G	0.0	0.0	0.0	C.0	
PROVIDED	2	1.9257	C.0881	0.1292	0.0293	0.1292	0.0293	1.
	3	3.8928	4.9832	C.1977	0.1188	0.1977	C.1188	460
	4	2.6179	1.5532	0.1688	0.0664 0.0641	0.1688 0.1701	0.0664	119
	5	2.6471	1.4473 0.0	C.1701 C.2422	0.0041	0.2422	U=U641 C=0	04
	6 7	4.4380 25.9040	15.0036	0.4497	0.1615	0.4497	0.1615	2
w-v	8	C+0	0.0	0.0	0.0	0.0	0.0	
	9	0.0	0.0	0.0	0.0	0.0	0.0	
VCLUME -	1	1.8008	1.7673	0.1271	0.0908	0.1271	C.0908	3:
*CEOFC	2	3.2372	2.2850	0.1858	0.0963	0.1858	0.0963	8
	3	5.8139	10.0731	0.2202	0.1576	0.2202	0.1576	11
	4	2.5431	1.6875	0.1563	0.0753	0.1563	0.0753	31
	5	2.8495	3.7822	0.1714	0.0897	0.1714	0.0897	50
	6	2.8852	1.5332	C.1783	0.0580	0.1783	C.0580	65
	7	2.9626	1.2014	0.1871	0.0456	0.1871	0.0456	384
	8	5.3893	7.5039	0.2159	0.1100	0.2159	0.1100	22
	9	3.7450	1.4890	0.2202	0.0521	0.2202	0.0521	21
	1 C	0.0	0.0	0.0	0.0	0.0	0.0	
PAGW	1	2.8900	2.5882	C.1641	0.1049	0.1641	0.1049	102
	2	2.1692	1.1340	C.1489	0.0632	0.1489	0.0632	919
	3 4	3.9911 3.5293	5.6487 4.0008	0.1983 0.1973	0.0946 0.0871	0.1983 0.1973	C.0946 O.0871	894 42
					0.0(15			
AREA	1 2	2.5419	1.1985 2.5915	0.1673	0.0615 0.1038	0.1673	C.C615 0.1038	463
	3	2.6522	1.3028	C.1758	0.0651	0.1758	C.0651	86)
	4	4.9630	7.7775	0.1992	0.1148	0.1992	0.1148	613
YEAR	1	1.8375	1.2318	C-1277	0.0743	0.1277	0.0743	318
	2	2.2072	0.7977	0.1569	0.0458	0.1569	0.0458	291
	3	2.3002	1.1231	0.1601	0.0611	0.1601	0.0611	254
	4	2.7588	1.6759	0.1714	0.0713	0.1714	0.0713	479
	5	3.8248	2.5026	0.2304	0.1132	0.2304	0.1132	206
	6	3.4185	2.1679	0.1863	0.0660	0.1863	0.0660	204
	7	4.4785	6.8524 7.6833	C.2007 C.2025	0.1049 0.1099	0.2007 0.2025	0.1049 0.1099	179
	<u>8</u> 9	4.7680 2.6030	1.2171	C.1725	0.0511	0.1725	0.1099	313 91
					A 0.02			
VERAGE	: (	3,1945	4.1207	C.1787	0.0876	0.1787	C.0876	2338

UNIT EML'S
VEHICLE TYPE SU-3A

LOCAL CONDITION	CODE	KENTU HEAK	CKY STD DEV	AASH FEAT	O STD DMV	110DIFII PEAN	STD DEV	TOTAI
	,	6.1290	5.5267	0.2661	0.1553	0.4151	C.268C	140
RGAD TYPE	2	5.1080	12.9214	0.3260	0.2476	0.5116	0.3824	1890
1116	3	23.1424	35.4535	0.5358	0.5667	0.8017	0.8447	150
	4	0.0	O • C	0.0	0.0	0.0	0.0	(
				0.3370	0.2560	0.5169	0.3558	129
DIRECT-	1	9.4560	14.4354	0.3279 0.3573	0.2300	0.5486	C.5024	88.
(CN	2	10.9966	18.5041	(19212				
ALT	1	10.6581	18.5923	C.3481	0.347C	0.5304	0.5199	89 131
RCUTE	Ž	9.7835	14.3797	C.3367	0.2503	0.5319	0.3900	31
	3	6.5808	4.2205	0.2450	0.1177	0.4059	C.1714	
			0.0	0.0	0.0	0.0	0.0	
SERVICE	1 2	C.O 5.4435	0.4339	0.2649	0.0141	0.3755	C.0103	4
PROVIDED	3	14.3703	22.6647	0.3578	0.3261	0.5663	0.5063	39
	4	7.6126	6.2635	C.3207	0.2091	0.5064	0.3202	113
	5	5.6740	5.5134	0.2671	0.2039	0.4113	C.3198	47
	- 6	4.9920	0 • C	0.3640	0.0	0.4494	0.0	1.2
	7	58.8783	37.4635	1.1404	0.5208	1.6980	0.7850	12
	8	0.0	0.0	0.0	0.0	0.0	0.0	
	5	6.0	0.0	C+0	0.0	0.0	U = U	
	•	1.3986	1:7418	C.0830	0.0969	0.1355	0.1615	
VOLUME	1	3.6633	4.9677	0.1931	0.2266	0.2837	0.3245	4
	3	25.2502	36.2287	0.5347	0.5813	0.8314	C-8531	14
	4	8.3661	15.4769	0.2863	0.3027	0.4476	0.5016	23
	Ś	7.0448	7.3153	C.2930	0.2356	0.4646	0.3569	43
	6	7.2825	3.9445	0.3271	0.1519	0.5152	0.2367	63 41
	7	9.3329	7.4444	0.3650	0.2036	0.5749	0.3332 0.4581	23
	8	20.7772	27.7086	C-4686	0.3234	0.6967	0.0834	3
	ç	19,9960	6.6129	C.6245	0.0658	0.9402	C.0	
	10	G • O	0.0	0.0	0.0	0.0		
P. A G W	1	2.0433	2.2627	0.1366	C.1446	0.1880	0.1941	2
1:	ž	5.6330	4.3851	0.2550	0.1746	0.4105	0.2758	78 94
	3	14.0285	21.5711	C.4228	C.3502	0.6516	0.5204 0.4249	43
	4	10.6706	14.3586	0.3453	0.2578	0.5392	0.4247	
1054	1	7.6802	6.9326	G.3311	0.2309	C.5062	0.3570	43
AREA		7.4554	14.7594	0.2429	0.2599	0.4021	0.4370	26
	3	7.5774	5.6396	0.3226	0.1918	0.5135	0.3014	92
	4	18.5590	28.1782	C.4510	0.4288	0.6762	C•6332	55
			X 3505	0.1967	0.2055	0.3242	C.3185	13
YEAR	1	4.4404	4.7505 4.3604	0.2538	0.1710	0.4121	0.2751	24
	2 3	5.6077 6.2953	3.5361	0.2852	0.1161	0.4620	C.1947	29
	4	5.9575	6.1718	C.2543	0.1856	0.3936	0.2931	48
		10.2700	8.4896	0.4069	0.2595	0.6461	C.3971	16
	6	12.3121	16.0816	0.4554	0.3120	0.6866	0.4653	23
	7	17.6219	23.3043	0.4529	0.3081	0.6884	0.4615	18
	8	16.0872	26.7364	0.4312	0.4453	0.6464	0.6632	33 10
	5	15.4322	22.6324	0.3591	0.2158	0.6207	0.4438	
				v				
							0.4399	218

UNIT EWL'S
VEHICLE TYPE C-3A

LOCAL CONDITION	CODE	KENT MEAN	UCKY STD DEV	AAS MEAN	HO STD DEV	MODIFI MEAN	ED AASHO STD DEV	TOTAL VOLUME
ROAD	1	6.7608	2.2514	0.5077	0.1167	0.5077	0.1167	705
TYPE	2	9.0137	5.8794	0.6159	0.2394	0.6159	0.2394	11376
	3	10.4281	17.8593	0.5984	0.7486	0.5984	0.7486	62
	4	0.0	0.0	0.0	0.0	0.0	0.0	0
DIRECT-	1	9.3428	7.6731	0.6280	0.2913	0.6280	0.2913	7105
ION	2.	8.1347	3.9101	0.5718	0.2256	0.5718	0.2256	5038
ALT	1	8.4253	6.3817	0.5821	0.2917	0.5821	0.2917	4929
ROUTE	2	9.2079	6.6523	0.6241	0.2545	0.6241	0.2545	7167
	3	5.5420	4.7296	0.4132	0.2985	0.4132	0.2985	47
SERVICE	1	0.0	0.0	0.0	0.0	0.0	0.0	0
ROVIDED	2	5.6940	0.0636	0.4366	0.0419	0.4366	0.0419	29
	3	9.7485	9.6735	0.6483	0.2595	0.6483	0.2595	2197
	4	9.2643	6.3190	0.6245	0.3051	0.6245	0.3051	6569
	5	7.7847 7.2180	3.5523 0.0	0.5547	0.2013	0.5547	0.2013	3319 6
	7	7.3890	2.9251	0.5536	0.2384	0.5536	0.2384	23
	8	0.0	0.0	0.0	0.0	0.0	0.0	
	9	0.0	0.0	0.0	0.0	0.0	0.0	Ö
VOLUME	1	19.9770	30.3074	0.9099	1.1607	0.9099	1.1607	17
AGEOUSE	2	16.2083	28.6535	0.6966	0.7156	0.6966	0.7156	42
	3	7.3226	5.0268	0.5110	0.3181	0.5110	0.3181	169
	4	7.9436	3.5492	0.5534	0.2332	0.5534	0.2332	1227
	5	8.9645	4.0120	0.6320	0.2284	0.6320	0.2284	3508
	6	8.9114	4.2455	C-6118	0.2388	0.6118	0.2388	4092
	7	8.5588	3.0719	0.6002	0.1719	0.6002	0.1719	2384
	8	8.7348	2.7545	0.6101	0.1431	0.6101	0.1431	614
	9	6.1510	1.8555	0.5118	0.1096	0.5118	0.1096	90
	10	0.0	0.0	0.0	0.0	0.0	0.0	0
MAGW	1	12.8738	20.5063	C.7000	0.8534	0.7000	0.8534	45
	2	9.6780	7.7532	0.6449	0.2886	0.6449	0.2886	6571
	3	8.5961	3.4246	0.5947	0.1778	0.5947	0.1778	4217
	4	7.0790	3.0314	0.5299	0.1814	0.5299	0.1814	1310
AREA	1	6.9609	3.2860	0.5066	0.1929	0.5066	0.1929	1846
	2	10.0704	11.7014	0.6292	0.3517	0.6292	0.3517	2108
	3	9.3217 8.5918	4.5760 3.9560	0.6455 0.5982	0.2564	0.6455 0.5982	0.2564	6278 1911
VETT.		2 8889	A 5340	0.6613	0.2981	0 (412	0 2001	100
YEAR	1 2	6.0827 9.8519	4.5240 3.7674	0.4413 0.6809	0.2163	0.4413 0.6809	0.2981 0.2163	1586 2428
	3	11.6798	3.1798	0.7797	0.1775	0.7797	0.1775	2508
	4	9.8127	9.6333	0.6215	0.2470	0.6215	0.2470	2569
	5	8.7034	2.7507	0.6090	0.1455	0.6090	0.1455	811
	6	7.0257	3.3398	0.5028	0.1429	0.5028	0.1429	717
	7	6.4242	2.2730	0.4913	0.1428	0.4913	0.1428	588
	8	9.5955	10.9791	0.6356	0,4598	0.6356	0.4598	618
	9	6.7403	3.5619	0.5265	0.2183	0.5265	0.2183	318
ERAGE	_	8.8944	6.5605	0.6071	0.2702	0.6071	0.2702	12143

UNIT EWL'S
VEHICLE TYPE C-4A

LOCAL	CODE	KENT		AAS			ED AASHO	TOTA
CONDITION		MEAN	STD DEV	MEAN	STD DEV	MEAN	STD DEV	VOLU
D.G.L.D.		13. 5/76	D 7521	0.7101	2.1402		2.1027	
ROAD	1	11.5470	3.1531	C.7181	0.1480	0.8419	0.1827	315
TYPE	2	15.4852	9.3296	0.8218	0.3289	1.0090	0.4381	109
	3	21.5461	22.1746	0.7775	0.5681	0.9627	0.7273	2:
	4	0.0	0.0	0.0	0.0	0.0	0.0	
DIRECT-	1	16.9244	10.8113	0.8775	0.3361	1.0784	0.4500	93
ION	2	11.9912	6.4898	0.6712	0.2619	0.8092	0.3396	49
ALT	1	13.3289	12.6905	0.6862	0.3333	0.8306	0.4306	30:
ROUTE	2	16.0684	8.3921	0.8596	0.3108	1.0547	0.4190	109
	3	12.7608	7.7463	0.6295	0.3381	0.7407	0.4039	3
SERVICE	1	C+0	0.0	C = C	0.0	0.0	0.0	
PROVIDED	2	58.6528	24.3714	1.6165	0.4985	2.1276	0.6607	
	3	16.4054	8.0706	0.8791	0.2929	1.0907	0.4059	284
	4	15.1038	9 4972	0.7882	0.3024	0.9566	0.4002	814
	5	13.1598	7.3966	0.7602	0.3488	0.9217	0.4434	324
	6	0.0	0.0	0.0420	0.0	0.0360	0.0	•
	7	16.0787	7.3192	0.7129	0.1243	0.9165	0.2513	
	8	0.0	0.0	0.0	0.0	0.0	0.0	
	9	C.O	0.0	0.0	0.0	0.0	0.0	
VOLUME	1	2.4000	3.3226	0.2196	0.2473	0.2476	0.2937	
	2	23.9338	24.4528	0.8037	0.4604	0.9274	0.5300	9
	3	19.4607	11.7079	0.8820	0.4056	1.1488	0.5731	23
	4	21.3722	15.7455	0.9466	0.4386	1.2020	0.5954	149
	5	12.6771	6.2434	0.7406	0.3017	0.8961	0.3886	235
	6	12.9852	6,9260	0.7584	0.3277	0.9114	0.4175	350
	7	15.0196	5.4130	0.8271	0.2134	1.0047	0.2874	422
	8	14.9399	3.8819	0.8371	0.1341	1.0072	C.1951	217
	9	16.3311	6.8235	0.8478	0.1941	1.0357	0.2701	27
	10	0.0	0.0	0.0	0.0	0.0	0.0	
MAGW	<u>1</u>	13.7774	18.6630	0.4636	0,5245	0.5769	0.7028	4
	2	8.0703	12.4310	0.4174	0.3652	0.4864	0.4588	97
	3	16.3872	5.2233	0.9053	0.1975	1.1073	0.2764	844
	4	17.4440	11.6178	0.8797	0-2940	1.0869	0.4095	484
AREA	1	19.8425	13.0430	C.9628	0.3858	1.2106	0.5133	287
	2	15.3652	9.8347	0.8192	0.3744	1.0128	0.5095	295
	3	13.1103	5.1497	0.7402	0.2212	0.8865	0.2784	627
	4	13.7991	10.5943	0.7401	0.3117	0.8883	0.3965	221
YEAR	1	2.057C	3.0218	0.1502	0.1530	0.1624	0.1737	12
	2	5.3724	4.7603	0.3600	0.2272	0.4053	0.2544	29
	3	4.8393	2.5664	0.3420	0.1147	0.3824	0.1340	37
	4	16.4120	7.2948	0.8705	0.2376	1-0629	C.3147	298
	5	18.3276	5.7624	0.9859	0.2045	1.2163	0.2929	228
	6	16.1736	5.5891	0.9015	0.2127	1.1048	0.3104	252
	7	16.2239	6.7317	0.8827	0.2431	1.0707	0.3332	266
	- 8	19.5410	16.3683	0.8885	0.3677	1.1092	0.4963	217
	9	13.9525	6.3093	0.7586	0.1993	0.9315	0.2894	91
				1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -			//	
	S	15.2519	9.8483	0.8076				

UNIT EWL'S
VEHICLE TYPE C-5A

LOCAL CONDITION	CODE	KENTI MEAN	JCKY STD DEV	AASI MEAN	HO STD DEV	MODIFI MEAN	ED AASHO STD DEV	TOT
COMPLICA					p	1.20		
RCAD	1	14.1246	3.4435	0.7327	0.1480	1.1051	0.2335	24
TYPE	2	19.9525	17.3973	0.8094	0.5165	1,2548	0.8035	18
	3	16.9600	15.7222	0.7266	0.5043	1.0556	C.7961	
	.4	0.0	0.0	0.0	0.0	0.0	0.0	
DIRECT-	1	22.1451	16.6855	C.8960	0.4594	1.3887	0.7212	30
ION	2	11.3953	8,5081	C.5872	0.3605	0.8812	0,5377	12
ALT	1	13.5862	13.5004	0.6378	0.4999	0.9682	C.7514	4
ROUTE	2	20.2235	15.4663	0.8473	0.4195	1.3078	0.6645	38
	3	9.2112	9.3769	0.4344	0.3237	0.6181	0.4793	
SERVICE	ı	0.0	0 • C	0.0	0.0	0.0	0.0	
PROVIDED	2	59.1900	0.0	1.9175	0.0	2,9333	0.0	
	3	24.6747	14.9258	C.97GO	0.4662	1.5137	0.7405	6
	4	16.6637	14.7646	0.7391	0.3791	1.1254	0.5895	28
	5	14.5289	12.5650	0.6784	0.4702	1.0425	0.7208	7
	6	0.0	0 . C	0.0	0.0	0.0	0.0	
	7	2.0000	0.0	0.2000	0.0	0.3100	0.0	
	8	0.0	0.0	0.0	0.0	0.0	6.0	
				2.6	0.0	0.0	C+0	
VGLUME	1	6.0	0.0	0.0	0.0	1.1102	0.9673	
	2	19.6875	18.7011	C.7495 C.7503	0.4722	1.1102	0.7039	
	3	16.5100	12.1248 23.3535	1.1061	0.5303	1.7054	C.8374	4
	4	30.7183	14.8700	0.5638	0.4782	0.8716	0.7228	ż
	5 6	14.0957 13.3145	10.0277	0.6597	0.417C	1.0157	C.659C	4
	7	15.5617	7.6670	C.7677	0.3216	1.1701	C.4890	15
	8	16.7488	10,1251	0.7653	0.3218	1.1738	C.5259	11
	ç	24.3595	6.5884	1.0246	0.1493	1.6212	0.2735	4
	10	C.O	C . C	C . C	0.0	0.0	0 - 0	
MAGW	1	19.1883	14.8582	C.8583	0.5144	1.1931	C.7380	
, , , , ,	ž	13.1143	18.5255	C.5579	0.6282	0.8543	0.9559	
	3	9.5589	11.0585	0.5092	0.4859	0.7660	C.7453	2
	4	22-4187	14.6691	0.9208	0.3413	1.4250	C.5408	40
AREA	1	24.4670	19.3083	0.9349	0.4542	1.4566	C.7138	9
	2	21.5264	16.6279	0.9135	0.4929	1.3842	0.7660	12
J	3	12.5637	7.7264 13.7429	0.6330	0.3491	0.9617	0.5227 0.7466	16
	4	1142143						
YEAR	1	26.0000	0 • C	0.9820	0.0	1.8140	0.0 1.1120	
	2	10.9571	22.9561	0.3820	0.7675	0.6030 1.0941	C.3089	
	3	12.4667	3.3519	0.8251 0.5671	0.1991 0.4504	0.8490	0.7072	
	4	11.1105	11.3202 15.4840	C.6465	0.6853	0.9249	1.0180	
	5 6	11.9062 5.9875	6.5137	C.3427	0.3171	0.5229	0.5173	
	7	15.5248	7,5415	0.7105	0.2798	1.1140	0.4360	- 4
	8	24.4939	17.4904	0.9531	0.3848	1.4735	0.6083	20
	9	20.3362	11.1413	0.8969	0.3209	1.3849	0.5251	17
VERAGI		18.3338	15.2253	0.7865	0.4518	1,2088	C.7051	

DESIGN ENT.2 MOKK SHEELS BOK BKEDICLING

VLLENDIX L

PREDICTION OF DESIGN (RURAL ONLY)	FWLS	SHEFT DATE-	- 1 OF 5
DESCRIPTION OF PROJECT AND	COMPUTATIONS		RATOR-
DESCRIPTION OF PROJECT			
ROUTE NAME-	RO	UTE NUMBER-	
PROJECT NUMBER-	co	UNTY-	
PROJECT LIMITS-			
LOADCMETER STATION REFERE	NCE (IF ANY)-	· · · · · · · · · · · · · · · · · · ·	1 1 104:00/03/03/03/03/03/03/03/03/03/03/03/03/0
DESCRIPTION OF TRAFFIC AND DES	IGN PERIOD		
DESIGN PERIOD (INCLUSIVE	DATES)-		
DESIGN PERIOD (YEARS)-			
DESIGN OR EFFECTIVE ADT (	VEHICLES PER DAY	) -	
TYPE OF EWL (CIRCLE)-	KY AASHO M	OCIFIED AASHO	
COMPUTATIONS			
ADJUSTE VEHICLE FRACTIO		UNIT EWLS	
TYPE (FROM SHE	FT 4) (FROM	SHEET 5)	
CARS	X	NEW TOTAL TO	
BUSES	X	=	
SU-2A-4T	X	=	
SU-2A-6T	X		
SU-3A	X		
C-3A	X		
C-4A	X	=	
C-5A	X	=	
	AVERAG	F UNIT FWL =	= SU
DESTON EWLS = 365 X		X	AUMON MINERAL MINERA MINERA MINERA MINERA MINERA MINERA MINERA MINERA MINERA M
PER	IGN ADT	SUM	DESIGN EWLS
(YE	ARS) PER DAY)		
COMPARISON WITH REFERENCE STAT	TON		

## PRECICTION OF DESIGN EWLS SHEET- 2 OF 5 (RURAL ONLY) DETERMINATION OF LCCAL CONDITIONS PREPARATOR-

## \*\* FOR EACH OF THE FOLLOWING LOCAL CONDITIONS, CIRCLE THE APPROPRIATE CODE \*\*

LOCAL	CODE	DESCRIPTION
CONDITION		
	1	INTERSTATE-NUMBERED RURAL ROUTE
ROAD	<del></del>	US-NUMBERED RURAL ROUTE
TYPE	3	KY-NUMBERED RURAL ROUTE
	4	OTHER RURAL ROUTE
*	•	
DIRECTION	ļ	SERVES PREDOMINANTLY NORTH-SOUTH TRAFFIC
	2	SERVES PRECOMINANTLY EAST-WEST TRAFFIC
ALTERNATE	1	ALTERNATE ROUTE PROVIDES INFERIOR SERVICE
ROUTE	2	NO ALTERNATE ROUTE OR SAME QUALITY OF SERVICE
	3	ALTERNATE ROUTE PROVIDES SUPERIOR SERVICE
	1	PRIMARILY PROVIDES SERVICE TO MAJOR REGREATIONAL ACTIVITIES
	2	PROVIDES SIGNIFICANT SERVICE TO MAJOR RECREATIONAL ACTIVITIES
A F B 1 (1)	3	FROVIDES SOME SERVICE TO RECREATIONAL ACTIVITIES
SERVICE	4	ORDINARY
PROVIDED	5	PROVIDES SOME SERVICE TO MINING ACTIVITIES
•	6 7	PROVIDES SIGNIFICANT SERVICE TO MAJOR MINING ACTIVITIES
	8	PRIMARILY PROVIDES SERVICE TO MAJOR MINING ACTIVITIES  PROVIDES MORE THAN ORDINARY SERVICE TO INDUSTRIAL ACTIVITIES
	9	PRIMARILY PROVIDES SERVICE TO MAJOR INDUSTRIAL ACTIVITIES
		LUTUALTEL LUCATOES SENATCE IN MAJOR THANDSINTAL WATTEL
	1	C-499 VEHICLES PER DAY
	2	
	3	1000-1999 VEHICLES PER DAY
-#	4	2000-2999 VEHICLES PER DAY
VCLUME	5	3000-3999 VEHICLES PER DAY
TOTAL	6	40CO-5999 VEHICLES PER DAY
	7	6000-7999 VEHICLES PER DAY
	8	8000-9999 VEHICLES PER DAY
	.9	10000-13999 VEHICLES PER DAY
	10	14000 OR MORE VEHICLES PER DAY
**************************************		
MAXIMUM	1	30,000 POUNDS
ALLCHABLE	2 3	42,000 PCUNDS
GRUSS ⊯EIGhT	3 4	59,640 PCUNDS 73,280 POUNDS
# CAUFF	CTHER	13,280 PUONDS PGUNDS
	CHIER	t an una
		WESTERN THIGHWAY DISTRICTS 1 AND 2)
GEOGRAPHICA	_	SOUTH CENTRAL (HIGHWAY DISTRICTS 3, 4, AND 8)
AREA	3	NORTH CENTRAL (HIGHWAY DISTRICTS 5, 6, AND 7)
	4	EASTERN (HIGHWAY DISTRICTS 9, 10, 11, AND 12)
	1	WINTER (JANUARY-MARCH)
SEASCN	2	SPRING TAPRIC-JUNE )
	3	SUMMER (JULY-SEPTEMBER)
**	.44	FALL (OCTOBER-DECEMBER)

MAY 1968

 1+1*1	428 <b>.1</b> 8401 YA₩	249*0	982 *0	77£**	L L 5 * L	861.0	ZZT *98	01	<b>b</b>	г
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680 * 0	707 * 6	£41.5	788.0	£16.6	10*008	54 I I	627°69	ξ	٤	Z
. 705.0 170.0	755 Z	702.0 E72.5	105°1	906°01	528*21 151*21	561°1 100°0	270 .47 197 .63	Z †	£	S
 680 *0	051.1	578.2	8£5 *0	855*5	221*9	158.0	958.67	DΥ	5	z
 410.0	269.0	091.7	074.0	LES *9	4E1 *9	69B "O	78° T80	6	2	Z
 0.023	2 2 8 . 0	298.1 7.974	0.57.0	9* 620	199*5 068*9	926°0	158.FT	8	<u> </u>	2
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 820.0	505.1	997.0 885.0	712.1 266.0	780.01 EET.0	987 .e	99E * T	007.07 078.83	5	2 2	7
 670°0	659.0	875.4	688.0	12.356 12.356	877.11	160 1	69*250	£	- <u>s</u>	z
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 100 *0	890 *0	986*1	100 0	996 °8	15.319	251 * I	£65.2T	7	Ţ	Z
0.001	564.0 927.0	284.0 0.422	791.0	117.8 594.8	516*ZI	98T 0 029 0	767 #38	S E	1	2
E11*0	9EE*0	1.682	£18 °0	ESE 6	75Z*71	S78.0	72,804	ĭ	i	2
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 585*8 852*9	917.4	196*1	965 °0	169*t	515*5 585*5	255.0 786.0	668.2FF	5 9	<del>"</del>	Ţ
19E.T	8*115	198*1	9ZL *0	991°9	906*7	916.0	925*11	L	7	ι
157°£	910 E1	796°Z	067.0 277.0	9 E O * 9	148.2 178.2	27 Z • 0 2 Z Z • 0	991 *89 879 *EL	9	* *	I I
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7.0000000000000000000000000000000000000									6.	<b>*</b>	E
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	628.0	1,325	877*0	£69*0	797.8	15*634	912*0	99E*LL	9	4	E E
	6ZB*1	198.1 505.5	744.0	707.0 278.0	9*586 9*623	111.21 520.61	55E 0 567 0	421.17 421.17	E E	*	E
	601°0 100°0	699 °0	100.0 805.0	579°0 215°0	605°8	1+5*91 5+5*81	1.225 458.0	SZT.ST ETE.ST	Ş	<b>b</b>	£
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	Z+0 *0	BYE .0	615*0	126.0	906 €	\$66°L	508.0	551°98	0 T	£	E
	960°0	685.0	906.0	806 0	061.6	E+5 *II	1001	50Z*5Z	B .	£ E	E
	910°0	969 0	<u> +€+•0</u>	199 0	T66 *9	13,882	945 0	915*94	9	٤	Ē
	Z9+*D	769.0	447.0 488.0	975.0	464.9 E44.T	798°II 008°II	477.0 417.0	865.67 73.298	5 4	8	E
	0.53.0 0.53.0	116*1 900*1	E87.0 EE1.1	1.029 1.029	020*21 959*6	169*ET 78*935¢	866.0 887.0	151.7a	S E	E	Ę
	1.208	1, 206	505°0	1.812	£75.01	15.207	201.0	B80*69	Ť	ε	E
									01		£
									6 B	2 2	E
	900 *0	916.0	0.802	3*248	764.0I	692*81	157.0	090*12	9	2	E
	800 °0	407.0 141.0 475.0	691*I 10+*T	512°2 0°480	826.0I	960°E1	7£7.0	25,27 72,446 71,060	- <del>'</del> 5	2 2	E
	1ZO *0	1/2 0	90L*Z	606*0	6£0**I	13.882	098 *0	E16.74	E	Z	3
	811.0	059.0	750.5 755.1	909 *0 490 *0	300 £1 13,006	851 *91 116 *11	011*1 9EE*1	£88*+9	Z I	2	E
									01	I.	٤
									6	······	E
									8	i	<u> </u>
	910*0	161.0	1E1*0	791°0	099*91 912*9	015*11 195*11	0.252	600*1 <i>L</i> 509*£8	9	I I	E
	0.0140	971.*0	905*0 965*0	1ES *0	582.e	209**1 669**1	199°0	405 * SL	4	i	٤
	920 0	071.0	692.0	922.0	965*01	616 91	095 *0 TT6 *0	7.42.17	5 E	· τ	E
	750.0	960 0	7.E.S.,D	870 40	11.924	E11.61	116.0	550.70	ī	τ	ε
									andaa	GR WEIGHT	IAbE
	¥90	₩ <b>5</b> -0	A & - 3	AE-US	10 87 00	19-42-0S	Sasua	CARS	7140704	MAX ALLOW	OAOA

<u> </u>	/001	CENTAGES =	чизтеп нек	GAMU 90 MUZ	BHT YA GAGI	100 DIA	SIMENT FACTOR	u L d A	
= X		= I00*0	- 966°D	×	x	×	х	×	
•						158*+		6	
						7*598 0*451		7 8	
						3*383 7*092		6 3 5 SHEET	∀:
,,,,			6+6*0 050*1	857.0		£55*0 \$66*0	550°I	3 4 FRDM	
			80 I • 1 2 7 8 • 0	£06 *0 Z£9 * 1	691 *1 £06 *0	095°0 668°0	826.0	<u>z</u>	
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			0* <del>04</del> 5	680 • I	0*611 5*02¢	0.770 0.770	1°009	Z I	
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= X		= 100*0	- E00°T	X	X	X 714°0	Х	<u>x</u>	
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· · · · · · · · · · · · · · · · · · ·			696°0	1 025 0 98 90	960°T	056°0 961°1	990°1	<u> </u>	
			1.057	1*525	1 76 0	856.0	928 0	Ţ	
		= 100*0	- 800°T	X	X	x	Х	<u>x</u>	
						407.0 268.0		6	
						+81•1 €78•0		<u>£ 9</u>	
			1.122	1.172		1 • 008		FEET 5	T3-AS
			906*0	Z+6 *D 866 *O	910*1	£56*0	456°0	ξ.	
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= X		= 100°0	- Z00°I	X	X	X	X	X	
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			710.0 £10.1	756°0 101°1	670.1 640.1	950 <b>*</b> 1	750°T 700°T 046°0	<u>z</u>	
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INTONAL MATERIA	1417007		996*0	466°0	866*0	1,028	110.1	ī	
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				111CM2	OR LUCAL CCAO	a inamizut	DA DN	\$3\$N8
0307*0	//			2 NO1 11	סא רסכער כסעט	элгиеит е	NO AE	CARS
0309*0								
	GECGRAPHICAL ASSA	GR WEIGHT	AGF OWE	∃TANA∃T JA ∃TUOS	DIRECTION	RCAE	adoo a	1APE VEHICLE

DESIGN UNIT EALS 0.0002 0.4000 GECGRAPHICAL AREA. -0,0166 -0,0036 -0,0075 -0.0847 -0.0847 0.0138 0.0392 0.0054 0.0033 0.0033 \*\* SELECT THE APPROPRIATE FACTORS AND PERFORM THE INDICATED CALCULATIONS \*\* SHEET- 5C OF 5 DATE-PREPARATOR-MAX ALLON GR NEIGHT -0,0471 -0,0622 -0,0160 -1.0956 -0.1770 0.0005 0.0 -0.0085 -0.0110 -0.0105 0.0 0,1924 0,0792 0,0184 0,0 -0.0034 0.0018 0.0048 0.0082 0.0018 0.0018 0.0019 0.0019 VOL UME 0.0150 0.0150 0.0120 0.0212 0.0120 0.0150 0.0150 0.0457 0.0457 0.0270 0.2000 -0.0668 0.0 0.0739 0.1118 0.2420 0.4745 0.3328 0.1140 -0.0527 -0.0137 0.0495 0.0495 -0.0195 ALTERNATE ROUTE 0.0087 -0.0026 0.0 0,0104 -0,0030 0,0 0.4541 0.5409 0.0 0.1549 0.1676 0.0 PREDICTION OF DESIGN EALS (RURAL ONLY) MODIFIED AASHO UNIT EALS NO ADJUSTMENT FOR LOCAL CONDITIONS
NC ADJUSTMENT FOR LOCAL CCNDITIONS DIRECTION -0.0617 0.0067 0.0101 0.0897 -0.3421 0.0 0.8838 0.8838 -0.0054 0.0 -0.0004 -0.0004 -0.0684 0.0 0.0164 0.0164 -0.1476 0.0 -0.1686 -0.1686 0,3093 + + 6560.0 0.0042 0.2053 VEHICLE TYPE SU-2A-4T SU-24-6T RUSES SU-3A CARS C-3A

** TRAMSFER DESIGN UNIT EMLS TO SHEET 1, A NEGATIVE ESTIMATE SHOULD BE TRANSFERRED		MAY 1968	
LS TO SHEET 1. A NEGA			
** TRAMSFER DESIGN UNIT EML	AS ZERD A*		

0.3417 +

0.3229 0.2472 0.1670 0.0

-0,8691 -0,7595 -0,1122 0,0

0.3778 0.3329 0.0

0.1498

- G. 4230 0.0 0.4594 0.4594

C-4A

0.2304 0.2304 0.0944 0.1464 0.0369 0.0369 0.0913 0.2378 0.2378 0.2764 0.3063 0.1134 0.0

-0.4514 -0.5495 -0.6707 0.0

0.8240 0.6346 0.0

0,3980

-0,4868 0,0 0,1140 0,1140

C-5A

0.5147 +

0.0 0.0507 0.0968 0.3610 -0.3156 -0.01018 0.3658 0.4506 EXAMPLE PROBLEM

VAPENDIX G

(RUR/	OF DESIGN EWLS AL ONLY)		DA	TE-	1 OF 5 8-15-68
DESCRIPTION OF PE	ROJECT AND COMP	NOITATU	S PR	EPAF	PATOR-LYNCH
DESCRIPTION OF PROJE	FCT _				
ROUTE NAME-		ADDRESS. POSSESSESSESSESSESSESSESSESSESSESSESSESSE	ROUTE NUMBER	- 4	5 27
PROJECT NUMBER-	KYHPR-21		COUNTY- Mac	2RE	MRY
PROJECT LIMITS-	2 TO 4 MI	<u>'LES</u> ,	NORTH OF M	HIT	LEY CITY
LOADCMETER STAT	ILON REFERENCE	(IF ANY	1- 4,9 MILES	NE	RM OF WHITE
DESCRIPTION OF TRAFF	C AND DESIGN	PERIOD			
DESIGN PERIOD (	INCLUSIVE DATE	s1- 19	70-1990		
DESIGN PERIOD (	YEARS)- 20				
DESIGN OR EFFEC	TIVE ADT (VEHI	OLES PET	R DAYI- 2900		107
TYPE OF EWL (CI	RCLE)- RY	) AASH	C MODIFIED AA	sho	
COMPUTATIONS					
VEHICLE	ADJUSTED FRACTION		UNIT EWLS		
TYPE	(FROM SHEFT 4	)	(FROM SHEET 5)		
CARS	.7045	χ	0	.=	0
BUSES	10094	Х	5,0000	=	0,0470
SU-2A-4T	.0893	X	0,3199	=	0.0286
SU-2A-6T	.0713	X	3,0593	-	0.2/8/
SU-3A	,0160	Х	8,5954	3	0.1375
C-3A	.0184	Х	9,0301	जन	0,1662
			01 0010	-	1.5228
C-4A	.0614	X	24,8012		
C-4A C-5A	.0614	Х Х	37,9646	**	1,1275
		Х			1, 1275 3,2477= SUM
C-5A	.0297	Х	<i>37.9646</i> VERAGE UNIT EWL	= ,	3.2477= SUM 68.750.000
	,0297  365 X 20 )  DESIGN PERIOD	X AV ADI (VEHIC	37.9646  VERAGE UNIT EWL  20 X 3.2477  T SUM  CLES	= ,	3.2477= SUM
C-5A  DESIGN EWLS =	,0297  365 X 20 )  DESIGN PERIOD (YEARS)	X A\ X 290 ADI	37.9646  VERAGE UNIT EWL  20 X 3.2477  T SUM  CLES	= ,	3.2477= SUM 68.750.000
C-5A	,0297  365 X 20 )  DESIGN PERIOD (YEARS)	X AV ADI (VEHIC	37.9646  VERAGE UNIT EWL  20 X 3.2477  T SUM  CLES	= ,	3.2477= SUM 68.750.000

(RUR	OF DESIGN EWLS AL ONLY)			SHEFT- 1 OF 5 DATE- 8-15-68
DESCRIPTION OF P	ROJECT AND COMP	UTATION		PREPARATOR-LYNCA
DESCRIPTION OF PROJ	FCT			
ROUTE NAME-	H0 (SERIANA) (SERIANA)		ROUTE NUMB	ER- US 27
PROJECT NUMBER	- KYHPR-21		COUNTY- NA	CREARY
PROJECT LIMITS	- 2 TO 4 MILE	ES NO	ATH OF WH	ITLEY GITY
LOADOMETER STA	TION REFERENCE	(IF ANY	1-4.9 MILES	NORTH OF WHITLE
DESCRIPTION OF TRAF				
DESIGN PERIOD	(INCLUSIVE DATE	si- 19	70-1990	
DESIGN PERIOD	(YEARS)- 20			
DESIGN OR EFFE	CTIVE ADT (VEHI	CLES PE	R DAY)- 290	0
TYPE OF EWL (C			50h.	
COMPUTATIONS				
VEHICLE	ADJUSTED FRACTION		UNIT FWLS	
TYPE	(FROM SHEFT 4	)	(FROM SHEET 5	)
	um			
CARS	.7045	х	0,0002	= ,000/4/
CARS BUSES	,7045	х х	0,0002	
				= 1003760
BUSES	.0094	Х	0,4000	= ,003760 = ,001768
BUSES SU-2A-4T	,0094	X	0,4000	= ,003760 = ,001768 = ,013376
BUSES SU-2A-4T SU-2A-6T	.0094 .0893 .0713	x x x	0,4000	= ,003760 = ,001768 = ,013376 = ,004045
BUSES SU-2A-4T SU-2A-6T SU-3A	.0094 .0893 .0713	x x x	0,4000	= ,003760 = ,001768 = ,013376 = ,004045 = ,010895
BUSES SU-2A-4T SU-2A-6T SU-3A C-3A	.0094 .0893 .0713 .0160	X X X X	0,4000 0,0198 0,1876 0,2528 0,5921	= ,003760 = ,001768 = ,013376 = ,004045 = ,010895 = ,066109
BUSES SU-2A-4T SU-2A-6T SU-3A C-3A C-4A	.0094 .0893 .0713 .0160 .0184	x x x x	0,4000 0,0198 0,1876 0,2528 0,5921 1,0767	= ,003760 = ,001768 = ,013376 = ,004045 = ,010893 = ,066109
BUSES SU-2A-4T SU-2A-6T SU-3A C-3A C-4A C-5A	.0094 .0893 .0713 .0160 .0184 .0614	X X X X X	0,4000 0,0198 0,1876 0,2528 0,5921 1,0767 1,3150 VERAGE UNIT E	= ,004045 = ,010893 = ,066109 = ,03905 WL = ,139156 SUM
BUSES SU-2A-4T SU-2A-6T SU-3A C-3A C-4A	.0094 .0893 .0713 .0160 .0184 .0614 .0297	X X X X X X X	0,4000 0,0198 0,1876 0,2528 0,5921 1,0767 1,3150 VERAGE UNIT E	= ,003760 = ,001768 = ,013376 = ,004045 = ,010893 = ,066109
BUSES SU-2A-4T SU-2A-6T SU-3A C-3A C-4A C-5A	.0094 .0893 .0713 .0160 .0184 .0614 .0297	X X X X X X X	0,4000 0,0198 0,1876 0,2528 0,5921 1,0767 1,3150 VERAGE UNIT E	= ,003760 = ,001768 = ,013376 = ,004045 = ,010893 = ,066109 = ,03905
BUSES SU-2A-4T SU-2A-6T SU-3A C-3A C-4A C-5A	.0094 .0893 .0713 .0160 .0184 .0614 .0297 = 365 X 20 DESIGN PERIOD (YEARS)	X X X X X X X A X X P AO (VEHI	0,4000 0,0198 0,1876 0,2528 0,5921 1,0767 1,3150 VERAGE UNIT E	= ,003760 = ,001768 = ,013376 = ,004045 = ,010893 = ,066109 = ,03905

		OF DESIGN EWLS			SHEFT- 1 OF 5 DATE- 8-15-68
D	ESCRIPTION OF PR	DJECT AND COMP	UTATIONS	S	PREPARATOR-LYNCH
DESC	RIPTION CF PROJE	СТ			
	ROUTE NAME-			RCUTE NUMB	ER- US 27
	PROJECT NUMBER-	KYHPR-21		COUNTY- N.	le CREARY
	PROJECT LIMITS-	2 to 4 MILE	ES NON	TH OF WH	ITLEY CITY
					NORTH OF WHITEY B
DESC	RIPTION OF TRAFF	IC AND DESIGN	PERIOD		
	DESIGN PERIOD (	INCLUSIVE DATE	si- 19:	70-1990	
	DESIGN PERIOD (	YEARSI- 20			
·	DESIGN OR EFFEC	TIVE ADT (VEHI	CLES PET	R DAYI- 290	00
	TYPE OF EWL (CI	RCLE) - KY	AASH	C (MORIFIED	AASHO
COMP	UTATIONS				
		ADJUSTED		UNIT	
	VEHICLE TYPE	FRACTION : (FROM SHEFT 4	)	FWLS (FROM SHEET 5	1
<u> </u>	£40£	.7045	~	0,0002	
	CARS		Х	· · · · · · · · · · · · · · · · · · ·	= ,000141
	BUSES	,0094	X	0,4000	= ,00 3760
	SU-2A-4T	,0893	· <b>X</b>	00198	= ,001768
	SU-2A-6T	,0713	Х	0.1876	= ,0/3376
	SU-3A	,0160	X	0.4236	= ,006778
·	C-3A	,0184	X	0.5921	= ,010895
	C-4A	.0614	Х	1.3910	= ,085407
	C-5A	,0297	Х	2,0416	= ,060636
<del></del>			Α'	VERAGE UNIT E	WL = 18276/ = SUM
	CESTON EWLS =	345 V 20	× 290	O x./827	61 - 3 870 000
	CESTGN EMES -	DESIGN	AD	r sum	16/ = 3 870,000 DESIGN EWLS
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COMP	ARISON WITH REFE	RENCE STATION			
AND THE RESIDENCE OF THE PERSON OF THE PERSO		4_4-4-41-41-41-41-41-41-41-41-41-41-41-41-			<u>^</u>
	•				MAY 1968

## PRECICTION OF DESIGN EHLS (RURAL ONLY) DETERMINATION OF LCCAL CONDITIONS

SHEET- 2 OF 5
DATE- 8-15-68
PREPARATOR- LYNCH

## \*\* FOR EACH OF THE FOLLOWING LOCAL CONDITIONS. CIRCLE THE APPROPRIATE CODE \*\*

	CODE	DESCRIPTION
CONDITION		
	1	INTERSTATE-NUMBERED RURAL ROUTE
ROAD	(2)	US-NUMBERED RURAL ROUTE
TYPE	3	KY-NUMBERED RURAL ROUTE
	4	OTHER RURAL ROUTE
DIRECTION	<u>ā</u>	SERVES PREDOMINANTLY NORTH-SOUTH TRAFFIC
	4.	SERVES PRECCMINANTLY EAST-WEST TRAFFIC
ALTERNATE	1	ALTERNATE ROUTE PROVIDES INFERIOR SERVICE
ROUTE	(2)	NO ALTERNATE ROUTE OR SAME QUALITY OF SERVICE
	3	ALTERNATE ROUTE PROVIDES SUPERIOR SERVICE
	_	COLUMN TO THE PROPERTY OF THE PROPERTY ACTIVITIES
	1	PRIMARILY PROVIDES SERVICE TO MAJOR RECREATIONAL ACTIVITIES PROVIDES SIGNIFICANT SERVICE TO MAJOR RECREATIONAL ACTIVITIES
	(3)	PROVIDES SOME SERVICE TO RECREATIONAL ACTIVITIES
SERVICE	4	CROINARY
PROVIDED	5	PROVIDES SOME SERVICE TO MINING ACTIVITIES
	6	PROVIDES SIGNIFICANT SERVICE TO MAJOR MINING ACTIVITIES
	7	PRIMARILY PROVIDES SERVICE TO MAJOR MINING ACTIVITIES
	8	PROVIDES MORE THAN ORDINARY SERVICE TO INDUSTRIAL ACTIVITIES
	9	PRIMARILY PROVIDES SERVICE TO MAJOR INDUSTRIAL ACTIVITIES
	1	C-499 VEHICLES PER DAY
	2	50C-999 VEHICLES PER DAY
	3_	ICOC-1999 AFHICES DEK DAY
	(4)	2000-2999 VEHICLES PER DAY
ACTAWE	5	3000-3999 VEHICLES PER DAY
	6 7	4000-5999 VEHICLES PER DAY 6000-7999 VEHICLES PER DAY
	8	OAGO COOO VELIVELLE DEU DAM
	9	10000-13999 VEHICLES PER DAY
<del></del>	10	14000 OR MORE VEHICLES PER DAY
MUMIXAM	1	30,000 POUNDS
ATTCHARTE	2	42,000 PCUNDS
GRUSS	(4)	59,640 PCUNDS 73,280 POUNDS
ME1GhT	CHER	131280 POUNDS
	<b>U</b> 111211	, , , , , , , , , , , , , , , , , , , ,
	1	WESTERN (HIGHWAY DISTRICTS 1 AND 2)
GEOGRAPHICAL	$\mathcal{O}$	SOUTH CENTRAL (HIGHWAY DISTRICTS 3, 4, AND 8)
AREA	3	NORTH CENTRAL (HIGHWAY DISTRICTS 5, 6, AND 7)  EASTERN (HIGHWAY DISTRICTS 9, 10, 11, AND 12)
	4	EASTERN (HIGHWAY DISTRICTS 9, 10, 11, AND 12)
	1	WINTER (JANUARY-MARCH)
SEASCN	2	SPRING (APRIL-JUNE)
	3	SUMMER (JULY-SEPTEMBER)
<del> </del>	.4	FALL (OCTOBER-DECEMBER)

MAY 1968

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ROAD TYPE	MAX ALLOW GR WEIGHT	VOLUME GROUP	CARS	BUSES	SU-2A-4T	SU-2A-6T	AE-UZ	C-3A	C-4A	C-5A
3	1	11	67,622	0.911	19.113	11.924	0.078	0.237	0.096	0.027
3.	1	2	71.247 73.944	0.560 0.351	16.919 14.699	10.596 9.282	0 • 228 0 • 865	0.263 0.436	0.170 0.360	0.025 0.071
3	ī	4	75.504	0.641	14.607	7.493	0.531	0.408	0,715	0.109
3	1 1	5	83.605 71.009	0.252	11.461 11.510	4.214	0.162	0.160	0.137 0.131	0.016 0.001
3	1	6 7 8								
3	ī	9								
3	1	10								
3	2	1	66.133	1.336	17.311	13.006	0.067	1.534	0.620	0.001
3	2 2	2 3	64+883 67+313	0.860	16.148 13.882	14.708	0.606	2,037	0.339	0.118 0.027
3	2 2	<u>. 4</u> 5	76.486 72.275	0.737	11.591 13.036	8.586 10.328	0.480 2.215	1.401	0.704	0.022
3	2	6	71.060	0.751	13269	10.497	3.248	0.802	0.376	0.006
3	2 2	7 8								
3	2	9		•						
3	2	. 10								
3	3 3	2	67.131	0.705	15.207	10.273 9.656	1,812	0.504	1.005	1.208 0.186
3	3	3	69.209	0.783	13.691	12.020	1.029	1.133	1.911	·0.230
3	3 3	4 5	73.298 78.092	0.471 0.714	11.800 11.862	9.634 7.463	1.355 0.276	0.744 0.886	2.244 0.697	0.462 0.016
3	3	6 7	76.516	0.576	13.882	6.991	0.557	0.434	0.898	0.154
3	3	B	75.709	1.031	11.543	6.130	0.908	0.306	0.283	0.095
3	3 3	10	86.144	0.805	7.992	3,906	0.321	0.419	0.378	0.042
3			72 202	1 226	10 5/5	( 00/	0.611	0.001	0.001	0.001
3	4	1 2	72.722 72.373	1.225 0.834	18.545 16.541	6.994 8.409	0.517 0.645	0.001 0.208	0.001 0.889	0.001 0.109
3	4	3	71.124 70.993	0.495 0.355	15.111 13.922	9.623 9.286	0.707 0.875	0.186 0.447	1.597 2.303	1.164.
3	4	5								
3	4	7 7	77.766	0.216	12.934	5.797	0.697	0.448	1.375	0.825
3	4	9								
3	4	10								
4	1.	1	72.020	1.120	17.667	9.029	0.073	0.080	0.016	0.001
4	1	2	76.173 82.974	0.688 0.214	13.379 9.889	7.277 3.389	1.493 0.001	0.658 2.459	0.306 1.080	0.035 0.001
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4	2 2	6 7	76.911	1.607	9.879	7.203	0.536	3.845	0.025	0.001
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4	2 2	9								
4	3	1	72.918	3,126	12.501	11.459	0.001	0.001	0.001	0.001
4	a	2	(2.710	3,120	12.501	11.439	0.001	0.001	4+001	0.001
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