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November 25, 1985

Mr. R. E. Johnson Division Administrator Federal Highway Administration 330 West Broadway Frankfort, Kentucky 40601

Dear Mr. Johnson:

Subject: Implementation Statement for UKTRP Report No. 85-15, "Effectiveness of Traffic Noise Barrier on I-471 in Campbell County, Kentucky"

The traffic noise measurements and data analyses summarized in the subject report show that the I-471 noise barrier has resulted in a substantial reduction in traffic noise for the affected homes. The success of this noise barrier in providing its predicted insertion loss proves that noise barriers provide an effective traffic noise abatement alternative.

The results of this study are now being used in public meetings to illustrate the potential effectiveness of proposed noise barriers.

The construction of additional barriers will be considered in the future as a viable noise abatement measure.

The funds allotted and used for this particular research study can well be justified.

Very truly yours,

K. Capito

R. K. Capito, P.E. State Highway Engineer

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The objective of this study was to evaluate the effectiveness of the traffic noise barrier on I 471 in Campbell County, Kentucky. Since the barrier coincided with con- struction of I 471, it was necessary to predict noise levels that would exist if no barrier were present utilizing the FHWA STAMINA 2.0 computer model. This was com- pared to actual noise level measurements at the barrier site to determine the barrier insertion loss. After calibration of the STAMINA 2.0 model, noise measurements were conducted at 39 receiver locations during off-peak and peak traffic conditions. The noise barrier reduced the noise level reaching adjacent residences substantially. Twenty-one residences (20 percent of the total in the study area) experienced a peak L10 insertion loss of 10 dBA or more, while another 63 residences (58 percent) were estimated as receiving an insertion loss of 5.0 to 9.9 dBA. Comparison of insertion loss using levels predicted by the STAMINA 2.0 model with the barrier in place and measured levels were very close. Analyses indicated that insertion loss values predicted by the STAMINA 2.0 model with coise barrier. A survey of community perception of the noise barrier was performed. Of 103 question- naires delivered, 66 (64 percent) were returned. The community perception of the barrier was favorable, as 64 percent of the respondents generally liked the noise barrier and 95 percent felt it was effective in reducing traffic noise.						
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Research Report UKTRP-85-15

EFFECTIVENESS OF TRAFFIC NOISE BARRIER ON I 471 IN CAMPBELL COUNTY, KENTUCKY

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and

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> in cooperation with Transportation Cabinet Commonwealth of Kentucky

> > and

Federal Highway Administration US Department of Transportation

The contents of this report reflect the views of the authors who are responsible for the facts and accuracy of the data presented herein. The contents do not necessarily reflect the official views or policies of the University of Kentucky, the Kentucky Transportation Cabinet, nor the Federal Highway Administration. This report does not constitute a standard, specification, or regulation.

May 1985

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Table of Contents

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		Page
Introduction	•	1
Data Collection Procedure	•	1
Technique for Determining Insertion Loss	•	1
Model Development and Calibration	•	2
Insertion Loss Measurements	•	5
Results	•	5
Model Calibration	•	5
Field Measurements	•	6
Measured versus Predicted Insertion Loss	•	7
Survey of Community Perception	•	8
Summary	•	9
Implementation	•	10
References	•	10
Appendix A Receiver Coordinates	•	33
Appendix B Output from STAMINA 2.0	•	37
Appendix C Traffic Volume Count Summaries	•	43
Appendix D Summary of Data by Location	•	47
Appendix E Cover Letter and Survey Questionnaire	•	57

INTRODUCTION

Traffic noise may reach such excessive levels at locations near major highways that noise abatement measures are necessary. One noise abatement measure used frequently across the United States involves a noise barrier constructed along the highway. These barriers are vertical walls made of wood, metal, concrete, or earth berms. They are designed to reduce noise levels at sensitive receivers adjacent to the highway and to break the line of sight between vehicles on the highway and receivers adjacent to the highway.

Currently, only one noise barrier has been constructed in Kentucky. This barrier is located on Interstate 471 in Campbell County (Figure 1). This barrier is 15 feet high and is of metal construction. It is located adjacent to the shoulder of the interstate and has a total length of 2,550 feet. It was constructed in 1981, and its construction coincided with the construction of I 471. The cost of the metal noise barrier itself was \$357,000 or \$9.33 per square foot or \$140.00 per linear foot. The total cost of the noise barrier construction project was \$392,277.

The noise barrier was designed to shield traffic noise from a residential neighborhood adjacent to I 471. The objectives of this study were to determine the insertion loss provided by the barrier and to determine if noise reduction estimates were achieved. Since this barrier was the first to be constructed in Kentucky, a determination of barrier effectiveness will aid in future decisions regarding when and how additional noise barriers should be constructed. The construction of noise barriers is expensive, which means that the most efficient design must be used to minimize the amount of barrier area required while achieving the needed noise reduction. Any improvement in design would result in reduced construction costs as well as reductions in noise levels for the affected receivers.

Since the noise barrier was part of the construction of I 471, beforeand-after data could not be obtained. This report describes the procedure used to determine the barrier field insertion loss. Modeling of the site is detailed along with the calibration procedure. Results of field measurements are presented. A survey developed to determine community perception of the noise barrier is also shown and results are presented.

DATA COLLECTION PROCEDURE

TECHNIQUE FOR DETERMINING INSERTION LOSS

Since construction of the noise barrier coincided with construction of I 471, before-and-after noise measurements could not be obtained. Also, there was not a similar site along the highway where there was no noise barrier where measurements could be taken and compared to those behind the barrier. Therefore, it was decided to use the procedure described in Section 5.5 of FHWA report FHWA-DP-45-1R (1). That procedure utilizes the FHWA STAMINA 2.0 model to determine insertion loss by comparing actual "after" sound level measurements to predicted "before" levels. The STAMINA

2.0 model considers highway traffic noise in relation to a roadway source, which is approximated by a series of straight-line segments, and estimates the acoustic intensity at receiver locations resulting from the roadway source. Source characteristics are defined by speed-dependent noise emission levels and by traffic density by vehicle type. Site geography is described by a three-dimensional coordinate system. Source-receiver path characteristics are then considered, taking into account effects of noise barriers, topography, vegetation, and atmospheric absorption.

Two locations (behind the noise barrier) were selected and measurements were taken to calibrate the model. Thirty-nine locations were then used in the data collection procedure. Once the calibration process was completed, "before" sound levels were predicted by the model. The insertion loss was determined by taking the difference between the calculated "before" and measured "after" noise levels.

MODEL DEVELOPMENT AND CALIBRATION

The first step in the model calibration process was the physical modeling of the study site. This was done by quantifying physical characteristics of the microphone or receiver locations, vehicles, the roadway, and the barrier. Using maps, an aerial photograph, and a preliminary field inspection, locations for the two microphones (study site and reference microphones) necessary to the calibration process were selected.

To locate the study site microphone, it was necessary to first establish a baseline perpendicular to the centerline of the near traffic lane, passing through the study site microphone location. The study site microphone had to be on the receiver side of the barrier (i.e. the barrier had to stand between the microphone and roadway) and had to be at least 10 feet from any vertical reflective surface. The geometry between the microphone and roadway was to be as simple as possible.

The reference microphone was located on the baseline in such a way that the noise barrier had no effect on it; it required an unobstructed view of the roadway through a subtended arc of at least 160 degrees. Due to the closeness of the noise barrier to the edge of the roadway, the only way to satisfy requirements for locating the reference microphone was to place it behind the noise barrier along the baseline and elevate it in such a manner that the barrier would have no effect (Figure 2). The reference microphone had to have a perpendicular clearance of 5 feet from a line originating at the near edge of the pavement and passing through the top front edge of the noise barrier. Using a tripod constructed of 1-inch diameter galvanized pipe, it was necessary to raise the microphone to a height of 28 feet to obtain the required perpendicular clearance (Figure 3). Locations of the microphones were expressed in terms of x, y, and z coordinates, with the z coordinate indicating the elevation of the microphone.

Vehicle types were grouped into four categories: automobiles (AUTOS), light trucks (LT), medium trucks (MT), and heavy trucks (HT). In terms of noise emission levels, all passenger cars, pickup trucks, and 12- or 15-passenger vans were grouped into the automobile category. The light truck category consisted of delivery-type trucks larger than a van in addition to pickup trucks having two axles and six tires. Single-unit trucks having two axles and six tires, as well as buses, were considered as medium trucks. Motorcycles were included in that category because they had similar noise emission levels. Single-unit trucks having three or more axles and all combination trucks were grouped into the heavy truck category. Corresponding source heights of 0.0, 0.0, 2.3 and 8.0 feet, respectively, were assigned to the categories and input into the STAMINA 2.0 model. Noise emission levels for cars, medium trucks and heavy trucks based on results from nationwide studies are incorporated into the STAMINA 2.0 model, but it was decided to use noise emission levels for different types of Kentucky vehicles derived in a previously issued report (2). The STAMINA 2.0 model allows for input of additional vehicle types; thus, parameters for Kentucky autos, light trucks, medium trucks and heavy trucks were added to the model as Vehicle Types 4, 5, 6, and 7, respectively. Traffic flow conditions for vehicle type, volume, and speed were then input into the model. The "Cars," "Medium Trucks," and "Heavy Trucks" vehicle types, based on nationwide emission levels, were all assigned traffic volumes of one vehicle per hour and speeds of 30 miles per hour (minimum values accepted by the model) so that they would effectively not be considered in the prediction process. Speeds and volumes were input for Vehicle Types 4, 5, 6, and 7 for prediction of traffic noise based on emission parameters for Kentucky automobiles, light trucks, medium trucks and heavy trucks, respectively. The STAMINA 2.0 User's Manual (1) did not specify what speeds were to be The 85th-percentile speed, which is the speed used to set speed used. limits, was used in this study.

A model of the roadway was constructed mathematically using a threedimensional coordinate system to describe a string of sequentially connected This presented a complex situation because the straight-line segments. roadway running in each direction consisted of a mainline and an entrance or exit ramp, all within the study site location. It was decided to model the ramps, the mainline section before the ramp, and the mainline section after the ramps all as individual roadways with corresponding traffic volumes. For example, the southbound lanes of I 471, which are adjacent to the noise barrier, are comprised of the mainline section and an entrance ramp. The ramp was considered as one roadway and its traffic volumes recorded. The mainline section just prior to the entrance ramp was considered as a separate roadway and its traffic volumes recorded. Finally, the mainline section just past the entrance point of the ramp was considered as a roadway itself; the ramp traffic volumes and the previous mainline section volumes were added to obtain combined traffic volumes for the third roadway. A similar technique was used for the northbound lanes. The exit ramp and mainline section traffic volumes were added to obtain combined traffic volumes for the section just prior to the exit ramp. Thus, there were three individual roadways for each direction, or a total of six. The individual roadways making up the northbound or southbound roadways contained common terminal points in order to connect the individual sections. STAMINA 2.0 allows the user to adjust the emission levels for heavy trucks moving up grades, but does not allow the user to define traffic flow direction. However, a grade ad justment factor may be included in the roadway model and was taken into account in the prediction process for the upgrade southbound lanes.

The noise barrier was modeled physically in the same manner as the roadway, using a three-dimensional coordinate system to describe the barrier as a string of sequentially connected straight-line segments. The height of the top of the barrier was input into the model as well as its elevation at ground level. Barrier coordinates were inserted into the model during the calibration process for the purpose of predicting the present conditions and comparing those predicted noise levels to those actually measured. After calibration of the model, noise barrier coordinates are removed from the model to predict conditions that would exist if the barrier were not present.

A decision was made to model the concrete median barrier as a small noise barrier. Though it was not intended to be a noise barrier and its effect would be minimal, it was decided to include the concrete median barrier in the model to approximate the actual site as closely as possible. For the same reason, three hills in the study site considered to be sufficiently large to provide a significant amount of protection from traffic noise for some of the residences were included in the model. STAMINA 2.0 recognizes three types of barriers: absorptive, reflective, and structural. The noise barrier wall and the concrete median barrier were considered to be reflective barriers, while the three hills were modeled as absorptive earth barriers.

Other factors recognized by STAMINA 2.0 in the modeling process are alpha factors, which concern the effect of hard or soft ground on the noise propagation rate between the source and receiver, and shielding factors, which account for the additional attenuation of noise due to shielding by buildings, rows of houses, trees, or other terrain features. The hillside behind the noise barrier was covered with thick vegetation, leading to the use of the 4.5 dB per distance doubling propagation rate for soft ground between the roadway and the study site microphone. A propagation rate of 3 dB per distance doubling was used for the hard pavement surface between the roadway and the reference microphone. There were no shielding factors between the roadway and reference and study site microphones to cause additional noise attenuation in the model calibration process.

Noise measurements were taken at the reference microphone location by a microphone atop the 28-foot tripod and connected via cable to a B & K Model 4426 Noise Level Analyser. The microphone at the study site was supported on a smaller 5-foot tripod and was connected to another B & K Noise Level Analyser.

The final step in the calibration process was to obtain noise measurements at selected microphone reference and study site locations. During this time period, traffic volumes and speeds were recorded. Using this information, noise levels at the two receiver locations were predicted by the STAMINA 2.0 program. Those levels were then compared to the actual recorded levels at the receiver locations for the same time periods in order to test the validity of the model.

INSERTION LOSS MEASUREMENTS

After calibration of the STAMINA 2.0 model, noise data were collected for peak and off-peak traffic conditions to estimate the barrier insertion Study site locations were selected throughout the neighborhood loss. adjacent to the barrier and "after" noise level measurements were obtained at those locations using 1) a B & K Noise Level Analyser, and 2) a B & K Impulse Precision Sound Level Meter with a Portable Graphic Level Recorder. Measurements for peak traffic conditions were made between 3:55 p.m. and 6:05 p.m.; off-peak data were collected between 10:30 a.m. and 3:00 p.m. Noise data were collected on 21 different days with off-peak data collected on 10 days and peak data collected on 13 days. Noise level measurements were made at 10-minute intervals and corresponding traffic volumes were recorded. To obtain the "before" noise levels, the x, y, and z coordinates of the receiver locations were input into the STAMINA 2.0 model as described in the model calibration. A listing of those coordinates for the 39 receiver locations is in Appendix A. Receiver locations are noted on the map in Figure 4. The receiver locations varied from as close as 135 feet from the noise barrier to as far as 740 feet. Receiver elevations varied from 5 feet above the top of the barrier to 76 feet below the bottom of the barrier. Appropriate alpha and shielding factors were also input.

Coordinates of the noise barrier were excluded from the model to simulate the situation that would exist if no barrier were present. Corresponding traffic volumes and speeds were input into the model and the STAMINA 2.0 program was run to predict the noise levels that would exist for the study site receiver locations without the noise barrier. A sample output including noise barrier coordinates from calibration of the STAMINA 2.0 model is in Appendix B. The barrier insertion loss for each receiver location was calculated to be the difference between the "before" and "after" noise levels.

RESULTS

MODEL CALIBRATION

To calibrate the model, noise level measurements were obtained and corresponding traffic volumes and speeds were recorded for the reference location and the initial study site location. Data were collected over seven 10-minute intervals, resulting in seven separate "runs". For each run, the traffic volumes and speeds were entered into the STAMINA 2.0 model; the model used those volumes and speeds to predict the noise level. The predicted noise levels were then compared to measured traffic noise levels. For the reference microphone location, the allowable difference in Leq could not be more than 1.0 dBA. For seven runs, the average difference in Leq was 0.8 dBA. The difference ranged from 0.2 to 1.6 dBA. The average difference in L10 at the reference microphone was 0.2 dBA with a range of 0.0 to 0.5 dBA.

The allowable difference in Leq for the study site microphone location was 2.0 dBA. For seven runs, the average difference was 0.9 dBA, which also was acceptable. The differences ranged from 0.2 to 2.0 dBA. The average difference in L10 at the study site microphone was 0.9 dBA with a range of

0.0 to 2.3 dBA. Therefore, it was assumed that the STAMINA 2.0 model of the noise barrier site was calibrated properly and could be used to predict traffic noise levels for the situation where no noise barrier existed.

FIELD MEASUREMENTS

Traffic noise data were collected during off-peak and peak traffic conditions at 39 receiver locations. The receiver locations were selected to cover an area adjacent to I 471 which could be affected by the noise barrier. Maps and visual inspections were used to select this area. An attempt was made to select a sufficiently large area such that any residences that may have been impacted by the noise barrier would be included. The receiver locations covered an area that included 108 residences.

The data were summarized separately for off-peak and peak conditions. Traffic volumes were counted during each measurement period. The volumes are summarized in Appendix C. Volumes were counted by direction and by mainline and ramp. The measured noise levels were compared to noise levels predicted by the STAMINA 2.0 model for the situation that would exist if no barrier were present. The barrier insertion loss was calculated to be the difference between the measured existing noise levels and the predicted noise levels. The numbers of residences within certain noise level and insertion loss ranges were estimated. The measured noise data and corresponding traffic volumes for off-peak and peak traffic conditions are contained in Appendix D.

Off-Peak Conditions

Predicted and measured L10 and Leq average noise levels and insertion loss estimates for off-peak traffic conditions are summarized in Table 1. Average off-peak hourly volumes for I 471 are given in Table C-1. Over the data collection period, total off-peak volumes averaged 2,052 automobiles per hour, 7 light trucks per hour, 84 medium trucks per hour, and 64 heavy trucks per hour. Shown in Figures 5 and 6 are average predicted L10 and Leq noise levels, respectively, at each receiver location for the conditions that would exist if no barrier were present. Figures 7 and 8 show average measured L10 and Leq noise levels, respectively, at each receiver location, while insertion loss estimates for L10 and Leq noise levels are shown in Figures 9 and 10, respectively.

The effect of the noise barrier on traffic noise reaching residences (for off-peak traffic conditions) is shown in Table 2. For the situation with no noise barrier, 51 of the 108 residences (47 percent) were predicted to experience an L10 noise level of 60.0 dBA or greater; none of the residences were found to experience off-peak L10 noise levels of 60.0 dBA or more based on measured data for existing conditions. Similarly, 36 of 108 residences (36 percent) were predicted to experience an Leq noise level of 60.0 dBA or more with no barrier compared to no residences receiving Leq noise levels of 60.0 dBA or more for existing conditions with the barrier present.

Insertion loss estimates for residences throughout the study site for off-peak traffic conditions are given in Table 3. For L10 noise levels, 24 of 108 residences (22 percent) were found to have experienced an insertion loss of 10.0 dBA or more, while 61 of 108 residences (57 percent) had an insertion loss of 5.0 to 9.9 dBA. Similarly, 20 residences (18 percent) were estimated to receive an Leq insertion loss of 10.0 dBA or more, while 57 residences (53 percent) experienced an Leq insertion loss between 5.0 and 9.9 dBA.

Peak Conditions

Predicted and measured L10 and Leq average noise levels for peak traffic conditions are given in Table 4. Corresponding average hourly volumes for I 471 are given in Table C-2. Total peak traffic volumes over the data collection period averaged 4,592 automobiles per hour, 2 light trucks per hour, 68 medium trucks per hour, and 35 heavy trucks per hour. Figures 11 and 12 show average predicted L10 and Leq noise levels, respectively, if no barrier were present. Figures 13 and 14 show average measured L10 and Leq existing peak noise levels, respectively. Insertion loss estimates under peak traffic conditions for L10 and Leq noise levels are shown in Figures 15 and 16, respectively.

The effect of the noise barrier on traffic noise reaching residences for peak conditions is shown in Table 5. For noise levels predicted by the STAMINA 2.0 model if no barrier were present, 12 of 108 residences (11 percent) would experience an L10 noise level greater than or equal to 70.0 dBA, while another 46 residences (43 percent) would experience L10 levels from 60.0 to 69.9 dBA. For the existing situation with a barrier, no residences had peak-hour L10 levels measured at 70.0 dBA or more; only 5 residences (5 percent) had measured L10 levels between 60.0 and 69.9 dBA. Similarly, 46 residences (43 percent) had predicted Leq levels for peak conditions from 60.0 to 69.9 dBA, while there were no residences with measured Leq levels of 60.0 dBA or greater with the barrier present.

Peak hour insertion loss estimates for study site residences are given in Table 6. Twenty-one residences (20 percent) experienced a peak L10 insertion loss of 10.0 dBA or more, while another 63 residences (58 percent) were estimated to receive an L10 insertion loss of 5.0 to 9.9 dBA. Simalarly, 15 residences (14 percent) experienced an Leq insertion loss of 10.0 dBA or more, while 58 residences (54 percent) experienced a peak Leq insertion loss of 5.0 to 9.9 dBA.

MEASURED VERSUS PREDICTED INSERTION LOSS

One objective of this study was to determine whether computer estimates of insertion loss were being achieved. Field measurements were used to check the accuracy of predicted insertion losses. To compare predicted with measured insertion loss, the STAMINA 2.0 model was used to predict noise levels with the noise barrier in place.

A summary of insertion loss using both field measurements and STAMINA 2.0 to determine noise levels with the barrier is shown in Table 7. Comparisons are given for both L10 and Leq noise levels and for both peak and off-peak traffic conditions. Average insertion loss is given for each noise level and time period.

In three of four cases, the insertion loss using measured values was more than that using predicted values. However, there were only small differences between the compared values with the largest being 2.0 dBA.

There were only small differences between peak and off-peak and L10 and Leq insertion loss values. The L10 insertion loss values were slightly higher than the Leq values. The insertion loss for off-peak was slightly higher than peak using measured values while peak was slightly higher than off-peak using predicted values.

This analysis shows that insertion loss values predicted by the STAMINA 2.0 computer program will be achieved by the noise barrier.

SURVEY OF COMMUNITY PERCEPTION

A survey of community perception of the noise barrier was conducted among residents of the homes included in the analysis. A questionnaire and accompanying cover letter explaining the purpose of the survey, along with a postage-paid return envelope, were mailed to residents in the study area. Those were the same residences included in the area covered by the field measurements.

The questionnaire consisted of common questions asked of residents in similar noise-barrier evaluations (3, 4, 5, 6, 7, 8). Questionnaire topics included awareness of the barrier, highway-related problems with the barrier, activities affected by the barrier, and the general effectiveness of the noise barrier as perceived by residents of the neighborhood. The cover letter and questionnaire are contained in Appendix E.

Of 103 questionnaires delivered, 66 (64 percent) were returned; 49 (48 percent) were returned initially and 17 of 54 follow-up questionnaires (31 percent) were returned by residents who did not respond initially.

Responses showed that the affected homes were in an old and established neighborhood. The average length of residence was 18 years with an average of three persons per home. Ninety-eight percent of the respondents owned their homes.

Ninety-six percent of the respondents described the neighborhood as quiet or very quiet before the roadway and barrier were constructed, while only 34 percent felt it to be quiet or very quiet after construction of the roadway and barrier. Ninety-eight percent of the respondents were aware the -barrier existed; of those, 63 percent learned about the barrier by observing its construction, while 19 percent learned of the barrier from the newspaper.

Concerning the effect of the noise barrier on highway-related problems, 78 percent of the respondents felt that the barrier made an overall improvement in reducing highway noise and 71 percent felt the barrier improved their privacy. In addition, 56 percent felt the barrier reduced highway dust and dirt accumulation and litter from vehicles, 54 percent felt it reduced headlight glare, 52 percent felt it reduced road vibrations, and 48 percent felt it reduced road fumes.

In relation to various activities, 57 percent thought relaxing outdoors was less difficult due to the presence of the barrier and 56 percent felt that conversation outdoors was less difficult. Also, 48 percent thought sleeping was less difficult, 46 percent thought conversation indoors was less difficult, 44 percent thought relaxing indoors was less difficult, and 42 percent thought telephone use was less difficult. Fifty-seven percent stated the barrier did not affect the amount they used their yards, but 40 percent felt they would have used their yards less if the barrier had not been constructed.

Thirty-three percent felt the barrier limited or restricted their view, 17 percent thought the barrier was unsightly, 15 percent felt it created a closed-in feeling, and 15 percent felt it had a detrimental effect on the environment. It should be noted that many respondents seemed to have difficulty discriminating the benefits of the noise barrier from the impact of the roadway, since their construction was coincidental. Thus, many of the negative answers and comments directed toward the noise barrier were actually directed toward construction of the roadway.

Seventy-eight percent of the residents who responded to the survey considered the appearance of the barrier to be acceptable; 12 percent thought it to be unsightly, while 10 percent thought it to be attractive. Compared to having no noise barrier, 50 percent felt the barrier was very effective in reducing traffic noise and 45 percent thought it was somewhat effective. In relation to property values, 57 percent felt the barrier had no effect, while 27 percent felt their property decreased in value and 16 percent felt that it increased. Overall, 64 percent of those responding generally liked the noise barrier, 13 percent disliked it, and 23 percent had no opinion.

SUMM ARY

The STAMINA 2.0 computer program was calibrated using a model of the study site so that it could be used to predict noise levels assuming the noise barrier was not present. Noise measurements were then obtained at 39 receiver locations during both peak and off-peak traffic conditions. That allowed insertion loss estimates to be made.

The noise barrier reduced noise levels reaching the adjacent residences substantially. For example, 21 residences (20 percent of the total in the study area) experienced a peak L10 insertion loss of 10 dBA or more, while another 63 residences (58 percent) were estimated to receive an L10 insertion loss of 5.0 to 9.9 dBA. Also, the STAMINA 2.0 model predicted (with no barrier present) that 12 residences (11 percent) would experience peak L10 noise levels greater than or equal to 70 dBA while another 46 residences (43 percent) would experience levels from 60.0 to 69.9 dBA. Measurements found that no residences had peak L10 levels of 70 dBA or more and only 5 residences (5 percent) had levels between 60.0 and 69.9 dBA. Noise levels with the barrier in place were predicted using the STAMINA 2.0 model. Comparisons of insertion loss using both measured levels and predicted values were close. The analysis indicated that insertion loss values predicted by the STAMINA 2.0 computer program will be achieved by the noise barrier.

Of 103 questionnaires mailed to residences to determine their perception of the barrier, 66 (64 percent) were returned. The community perception of the barrier was favorable. Overall, 64 percent of those responding to the survey generally liked the noise barrier, 13 percent disliked it and 23 percent had no opinion. Compared to having no noise barrier, 50 percent felt the barrier was very effective in reducing traffic noise and 45 percent thought it was somewhat effective.

IMPLEMENTATION

Traffic noise measurements and data analyses summarized in this report show that the I-471 noise barrier has resulted in a substantial reduction in traffic noise for the affected homes. The success of this noise barrier in providing its predicted insertion loss proves that noise barriers provide an effective traffic noise abatement alternative. The construction of additional barriers should be considered as a viable noise abatement measure. Results of this study may be used in future public hearings to illustrate the potential effectiveness of proposed noise barriers.

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Figure 1. Noise Barrier, Interstate 471, Campbell County, Kentucky.



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Figure 2. Elevated Reference Microphone.



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Figure 4. Field Measurment Receiver Locations.



Figure 5. Average Predicted Off-Peak LIO (No Barrier).







Figure 7 Average Measured Off-Peak LIO (Barrier Present).



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Figure 8. Average Measured Off-Peak Leg(Barrier Present).





Figure 10. Average Off-Peak Leg Insertion Loss.



Figure II. Average Predicted Peak LIO (No Barrier),



Figure 12. Average Predicted Peak Leg (No Barrier).



Figure 13. Average Measured Peak LIO (Barrier Present).

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Figure 14. Average Measured Peak Leg (Barrier Present).



Figure 15. Average Peak LIO Insertion Loss.


Figure 16. Average Peak Leg Insertion Loss.

			AVERAGE	NOISE LEVEL	(dBA)	
RECEIVER	MEASUR	ED	PRE	DICTED	INSERTION	LOSS
NUMBER	L10	Leq	L10	Leq	L10	Leq
002	63.0	59.4	50.8	49.2	12.1	10.2
003	59.7	56.1	52.4	50.2	7.3	5.9
004	54.7	51.2	47.7	45.4	7.0	5.8
005	69.3	65.9	56.2	53.6	13.1	12.3
006	65.0	61.5	52.8	50.5	12.2	11.0
007	58.5	55.0	52.3	50.0	6.2	5.0
008	55.3	51.8	47.3	47.5	8.0	4.3
00 9	64.1	60.4	52.5	50 .9	11.6	9.5
010	64.3	60.8	55.6	53.6	8.7	7.2
011	64.5	60.9	54.9	52.7	9.6	8.2
012	68.2	65.0	56.6	54.8	11.6	10.2
013	60.6	57.4	53.6	51.2	7.0	6.2
014	64.6	61.5	55.3	53.5	9.3	8.0
015	56.8	53.2	49.4	47.1	7.4	6.1
016	60.7	57.4	54.2	52.2	6.5	5.2
017	52.0	46.0	48.7	46.0	3.3	0.0
018	49.9	46.4	48.3	45.9	1.6	0.5
019	56.5	53.2	49.0	47.1	7.5	6.1
020	5 9. 0	55.5	49.7	47.9	9.3	7.6
100	63.1	59.5	52.8	51.1	10.3	8.4
101	64.0	60.5	54.5	52.8	9.5	7.7
102	67.1	63.9	55.4	53.6	11.7	10.3
103	66.8	63.6	55.3	53.8	11.5	9.8
104	60.7	57.2	53.3	51.0	7.4	6.2
105	52.8	49.3	47.0	45.1	5.8	4.2
106	50.0	46.4	45.3	43.5	4.7	2.9
107	53.0	49.5	49.7	47.7	3.3	1.8
108	62.9	59.7	51.0	49.2	11.9	10.5
109	66.9	63.7	54.2	52.2	12.7	11.5
110	52.0	48.7	49.7	47.4	2.3	1.3
111	56.0	52.5	48.2	46.5	7.8	6.0
112	60.6	57.4	50.8	49.0	9.8	8.4
113	63.3	60.6	58.4	56.0	4.9	4.6
114	65.4	62.4	56.8	54.5	8.6	7.9
115	68.8	65.3	55.2	53.0	13.6	12.3
116	70.4	67.1	5 9. 0	57.0	11.4	10.1
117	71.5	68.1	59.7	57.2	11.8	10.9
118	64.9	62.1	59.4	57.1	5.5	5.0
119	67 . 5	64.2	55.6	53.4	11.9	10.8

TABLE 1. OFF-PEAK INSERTION LOSS MEASUREMENTS

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NOISE LEVEL (dBA)		PREDICTED (N	O BARRIER)	MEASURED (BARRIE	ER PRESENT)		
		NUMBER RESIDENCES	PERCENT	N UMBER RESIDENCES	PERCENT		
L10	70.0 or above	0	0	0	0		
	65.0 - 69.9	18	17	0	0		
	60.0 - 64.9	33	30	0	0		
	55.0 - 59.9	28	26	17	16		
	50.0 - 54.9	16	15	43	40		
	Less than 50.0	13	12	48	44		
Leq	70.0 or above	0	0	0	0		
-	65.0 - 69.9	10	9	0	0		
	60.0 - 64.9	26	24	0	0		
	55.0 - 59.9	27	25	10	9		
	50.0 - 54.9	22	21	42	39		
	Less than 50.0	23	21	56	52		

TABLE 2. EFFECT OF NOISE BARRIER ON TRAFFIC NOISE REACHING RESIDENCES (OFF-PEAK)

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TABLE 3. NUMBER OF RESIDENCES RECEIVING GIVEN INSERTION LOSS (OFF-PEAK)

	L10		 Leq	
AVERAGE INSERTION LOSS (dBA)	NUMBER RESIDENCES	PERCENT	NUMBER RESIDENCES	PERCENT
10 or above	24	22	20	18
5.0 - 9.9	61	57	57	53
Less than 5.0	23	21	31	29

.

		AVERAGE NOISE LEVEL (dBA)						
RECEIVER	MEAS	URED	PRED	ICTED	INSERTION	LOSS		
NUMBER	L10	Leq	L10	Leq	L10	Leq		
002	64.4	61.2	54.9	52 . 4	9.5	8.8		
003	61.6	58.6	55.5	53.9	6.1	4.7		
004	56.1	52.8	49.9	47.9	6.2	4.9		
005	71.2	68.5	56.8	55.0	14.4	13.5		
006	66.3	63.9	55.9	54.7	10.4	9.2		
007	60.5	57.8	55.8	54.0	4.7	3.8		
008	57.3	54.5	51.2	48.5	6.1	6.0		
00 9	65.7	62.6	55.0	53.0	10.7	9.6		
010	65.2	62.3	56.1	54.2	9.1	8.1		
011	66.5	63.3	58.9	56.6	7.6	6.7		
012	69.7	67.4	60 .9	59.3	8.8	8.1		
013	61.9	59.2	56.5	54.9	5.4	4.3		
014	64.9	62.4	58.1	56.4	6.8	6.0		
015	57.6	54.5	52.1	50.8	5.5	3.7		
016	61.9	59.5	56.3	54.4	5.6	5.1		
017	51.5	48.1	49.0	47.5	2.5	0.6		
018	51.6	48.4	47.9	46.2	3.7	2.2		
019	57.8	55.3	51.0	49.5	6.8	5.8		
020	60.6	57.7	52.6	51.0	8.0	6.7		
100	64.1	61.0	57.3	55.7	6.8	5.3		
101	64.9	62.1	57.9	55.8	7.0	6.3		
102	69.1	66.9	60.0	58.4	9.1	8.5		
103	68.3	65.8	59.3	57.8	9.0	8.0		
104	62.5	59.3	52.9	51.3	9.6	8.0		
105	53.0	49.8	48.8	47.1	4.2	2.7		
106	51.8	48.5	47.4	44.9	4.4	3.6		
107	54.5	51.6	50.8	48.8	3.7	2.8		
108	64.7	62.3	54.4	52.6	10.3	9.7		
109	69.1	66.6	56.7	54.8	12.4	11.8		
110	54.3	51.4	51.4	49.8	2.9	1.6		
111	56.1	53.3	51.3	49.8	4.8	3.5		
112	61.4	58.9	54.7	53.2	6.7	5.7		
113	63.7	61.6	57.7	55.0	6.0	6.6		
114	67.0	65.1	60.0	58.3	7.0	6.8		
115	71.3	68.6	57.5	55.8	13.8	12.8		
116	72.4	69.9	60.3	58.4	12.1	11.5		
117	72.8	70.4	61.1	59.4	11.7	11.0		
118	66.0	64.0	63.7	61.1	2.3	2.9		
119	68.8	66.5	56.3	54.3	12.5	12.2		

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 TABLE 4. PEAK INSERTION LOSS MEASUREMENTS

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		PREDICTED (NO) BARRIER)	MEASURED (BARR	IER PRESENT)
NOISI	E LEVEL (dBA)	NUMBER RESIDENCES	PERCENT	NUMBER RESIDENCES	PERCENT
L10	70.0 or above	12	11	0	0
	60.0 - 64.9 55.0 - 59.9	31 27	29 25	5 44	5 41
	50.0 - 54.9 Less than 50.0	18 5	16 5	37 22	34 20
Leq	70.0 or above 65.0 - 69.9 60.0 - 64.9 55.0 - 59.9 50.0 - 54.9 Less than 50.0	0 17 29 27 16 19	0 16 27 25 15 17	0 0 32 36 40	0 0 30 33 37

TABLE 5. EFFECT OF NOISE BARRIER ON TRAFFIC NOISE REACHING RESIDENCES (PEAK)

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TABLE 6. NUMBER OF RESIDENCES RECEIVING GIVEN INSERTION LOSS (PEAK)

	L10 Le		Leq	эd	
AVERAGE INSERTION LOSS (dBA)	NUMBER RESIDENCES	PERCENT	NUMBER RESIDENCES	PERCENT	
10 or above	21	20	15	14	
5.0 - 9.9	63	58	58	54	
Less than 5.0	24	22	35	32	

TABLE 7. MEASURED VERSUS PREDICTED INSERTION LOSS

	AVERAGE INSERTION LOSS (dBA)				
	L10		Leq		
	PEAK O	FF-PEAK	PE AK	OFF-PE AK	
Measured	7.5	8.6	6.6	7.1	
Predicted	7.2	6.6	7.2	6.4	
Difference	0.3	2.0	0.6	0.7	

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APPENDIX A

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RECEIVER COORDINATES

TABLE A-1.	RECEIVER	COORDINATES
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RECEIVER				
LOCATION	Х	Y	Z	SHIELDING
NUMBER	COORD	COORD	COORD	FACTOR (dBA)
		1050		
002	4327	1252	659	3.0
003	4302	1424	639	3.0
004	4287	1553	624	7.0
005	3723	1223	668	0.0
006	3895	1334	664	1.0
007	4006	1531	657	4.0
008	4068	1666	644	5.0
009	3350	1445	732	3.0
010	3078	1490	729	3.0
011	2917	1465	719	3.0
012	2671	1410	709	0.0
013	2613	1593	718	4.0
014	2286	1580	744	1.0
015	2808	1743	709	5.0
016	2440	1687	734	3.0
017	3038	1913	684	7.0
018	3048	1834	694	7.0
019	2266	1720	748	6.0
020	2665	1722	714	4.0
100	3330	1494	731	3.0
101	3204	1487	730	3.0
102	2771	1445	712	0.0
103	2616	1454	709	0.0
104	4333	1305	654	3.0
105	4302	1619	617	8.0
106	4264	1743	614	9.0
107	4119	1766	633	6.0
108	3891	1368	664	2.0
109	3783	1280	667	0.0
110	3011	1770	701	5.0
111	2919	1735	708	5.0
112	2593	1685	718	3.0
113	2303	1640	746	1.0
114	2289	1508	738	0.0
115	2326	1316	690	0.0
116	2986	1342	721	0.0
117	3467	1261	704	0.0
118	4346	1334	679	0.0
119	4052	1224	629	0.0

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APPENDIX B

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OUTPUT FROM STAMINA 2.0

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STAMINA 2.0/BCR FHWA VERSION (MARCH 1982) TRAFFIC NOISE PREDICTION MODEL DEVELOPED UNDER CONTRACT BY BBN

ROADWAY 1 SOUTHBOUND I-471 MAINLINE (COMB)

(INPUT UNITS- ENGLISH + OUTPUT UNITS- ENGLISH)

EVALUATION OF TRAFFIC NOISE BARRIER 1-471 CAMPBELL CO.

PROGRAM INITIALIZATION PARAMETERS

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- 22

HEIGHT	CDDE	DESCRIPTION
0.0	1	RECEIVER HEIGHT ADJUSTMENT
1.00	2	A-WEIGHTED SOUND LEVEL ONLY
0.0	3	HEIGHT ADJUSTMENT FOR PASSENGER CARS (CARS)
8.00	4	HEIGHT ADJUSTMENT FOR HEAVY TRUCKS (HT)
2.30	5	HEIGHT ADJUSTMENT FOR MEDIUM TRUCKS (MT)
0.0	6	HEIGHT ADJUSTMENT FOR TYPE4 VEHICLES (VEH4) *AUTOS*
		CO = 20.44 CI = 30.32 SO = 3.11
0.0	7	HEIGHT ADJUSTMENT FOR TYPES VEHICLES (VEH5) •LT TRKS•
		CO = 21.86 CI = 31.08 SO = 3.41
2.300	8	HEIGHT ADJUSTMENT FOR TYPE6 VEHICLES (VEH6) •MED TRKS
		C0 = 26.98 C1 = 31.37 S0 = 3.89
8.000	9	HEIGHT ADJUSTMENT FOR TYPE7 VEHICLES (VEH7) •HEAV TRKS
		C0 = 36.52 C1 = 28.20 S0 = 3.44

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	VEHICLE TYPE	VEHICLESZHOUR	SPEE)
	CARS	1.	30.	
	HT	1.	30.	
	MT	1.	30.	
	VFH4	1170	60.	
	VEHS	0.	55.	
	VEH6	30.	55.	
	VEH7	30.	55.	, ,
		-COORDINATES		
	X	¥ _	Z	GRADE
RS-1	1179.	772.	779.	1
RS-2	1551.	920.	768.	1
R5-3	1834.	1027.	758.	1
RS=4	2126.	1113.	749.	ī
RS-5	2428.	1169.	739.	1
RS-6	2727.	1188.	730.	1
RS-7	3037.	1174.	720.	ī
RS-8	3338.	1120.	710.	1
RS-3A	3414.	1102.	707.	1

ROADWAY 2 SOUTHBOUND I-471 MAINLINE (SEP)

	VEHICLE TYPE	VEHICLES/HOUR	SPEED	
	CARS	1.	30.	
	HT	1.	30.	
	MT	1.	30.	
	VEH4	990.	60.	
	VEHS	0.	55.	
	VEH6	30.	55.	
	VEH7	30.	55.	
		-COORDINATES		
	X	Y	Z	GRADE
RS-8A	3414.	1102.	707.	1
R5-9	3827.	1004.	694.	1
RS-10	4315.	882.	678.	1
RS-11	4799.	763.	662.	1
RS-12	5288.	662.	646.	1

Figure B-1. Output from STAMINA 2.0

		VEHICLE TYPE CARS HT VEH4 VEH5 VEH6 VEH7	VEHICLES/HOUR 1. 1. 180. 0. 0. 0.	SPEED 30. 30. 55. 50. 50. 50.	
			-COORDINATES		
RF-1 RF-2 RF-3 RF-4 RF-5 RF-6 RF-7		3419. 3523. 3719. 3919. 4117. 4315. 4515.	1130. 1109. 1062. 1036. 1010. 984. 961.	707. 704. 697. 690. 682. 672. 662.	1 1 1 1 1 1 1
RF-8 RF-9 RF-10 RF-11		4713. 4913. 5111. 5313.	936. 912. 840. 886.	653. 643. 633. 623.	1 1 1
ROADWAY	4	NORTHBOUND I-471	MAINLINE (COMB)		
		VEHICLE TYPE CARS HT MT VEH4 VEH5 VEH6 VEH7	VEHICLES/HOUR 1. 1. 990. 0. 36. 66.	SPEED 30. 30. 65. 65. 60. 60.	
			-COORDINATES		
RN-1 RN-2 RN-3 RN-4 RN-5 RN-6		x 1212. 1585. 1864. 2147. 2440. 2728.	Y 689. 838. 944. 1027. 1081. 1100.	2 779. 768. 758. 749. 739. 730.	GRADE 0 0 0 0 0 0
ROADWAY	5	NORTHBOUND I-471	MAINLINE (SEP)		
		VEHICLE TYPE CARS HT MT VEH4 VEH5 VEH6 VEH7	VEHICLES/HOUR 1. 1. 1. 774. 0. 36. 66.	SPEED 30. 30. 65. 65. 60. 60.	
		X	Y	 Z	GRADE
RN-6 RN-7 RN-8 RN-9 RN-10 RN-11 RN-12		2728. 3030. 3323. 3809. 4296. 4783. 5276.	1100. 1092. 1046. 929. 809. 688. 586.	730. 720. 710. 694. 678. 662. 646.	0 0 0 0 0 0 0

Figure B-1. Output from STAMINA 2.0 (Cont.)

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	VEHICLE TYPE	VEHICLES/HOUR	SPEED)
	CARS	1.	30.	
	HT	1.	30.	
	MT	1.	30.	
	VEH4	216.	60.	
	VEHS	0.	60.	
	VEH6	0.	55.	
	VEH7	0.	55.	
		-COORDINATES		
	X	Y	Z	GRADE
RE-1	2818.	1079.	725.	0
RE-2	3069.	1041.	716.	0
RE-3	3264.	993.	708.	0
RE-4	3457.	942.	701.	0
RE-5	3650.	889.	694.	0
RE-6	3843.	837.	687.	0
RE-7	4036.	785.	680.	Ō
RE-8	4229.	730.	675.	Ō

BARRIER	1	TYPE(R)	TRAFF	IC NOISE	BARRIER	
		CO	DRDINATES		-	
		X	Y	Z	ZO	DELZ
8-1		1822.	1063.	774.	759.	0.
8-2		2117.	1149.	766.	751.	
B-3		2527.	1217.	753.	738.	
8-4		2939.	1219.	739.	724.	
8-5		3144.	1200.	733.	718.	
3-6		3351.	1165.	727.	712.	
8-7		3547.	1124.	719.	704.	
8-8		3698.	1090.	713.	698.	
8-9		3872.	1063.	705.	690.	
8-10		4343.	1007.	688.	673.	

BARRIER 2 TYPE(R) CONCRETE MEDIAN BARRIER -----COORDINATES------

		X	Y	6	20	UELZ	P
8M-1		1196.	731.	781.	779.	0.	0
8M-2		1755.	951.	764.	762.		
AM-3		2136.	1071.	752.	750.		
BM-4		2434.	1126.	744.	742.		
BM-5		2728.	1144.	732.	730.		
8 M-6		3033.	1129.	723.	720.		
BM-7		3331.	1083.	713.	710.		
8 - -M8		3818.	967.	697.	694.		
BM-9		4693.	749.	668.	666.		
8M-10		5282.	624.	649.	647.		
BARRIER	3	TYPE(A)	EARTH	BARRIER NO	0.1		
	-	C0	ORDINATES				
		X	Y	Z	Z 0	DELZ	Р
EA-1		4525.	1113.	705.	689.	0.	0
EA-2		4586.	1105.	707.	686.		
EA-J		4637.	1098.	707.	683.		
EA-4		4738.	1087.	704.	678.		
EA-5		4837.	1075.	702.	673.		
BARRIER	4	TYPE(A)	EARTH	BARRIER NO	. 2		
		coc	RDINATES				
		X	Y	Z	Z 0	DELZ	Ρ
E8-1		4293.	1110.	678.	667.	0.	0
EB-2		4319.	1100.	680.	664.		
EB-3		4343.	1104.	680.	665.		
E8-4		4374.	1107.	680.	663.		
EB-5		4400.	1101.	680.	661.		

Figure B-1. Output from STAMINA 2.0 (Cont.)

BARRIER 5 TYPE (A) EARTH BARRIER NO. 3

1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 -1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 -

	C(DORDINATES-				
	X	Y	Z	Z 0	DELZ	Ρ
EC-1	2631.	1576.	713.	711.	0.	0
EC-2	2724.	1600.	715.	707.		-
EC-3	2815.	1620.	719.	705.		
EC-4	2993.	1608.	725.	699.		
EC-5	3078.	1580.	725.	698.		
EC-6	3180.	1571.	725.	695.		
EC-7	3257.	1573.	725.	690.		
EC-8	3391.	1549.	733.	684		
EC-9	3626.	1503.	745.	677.		

RECEIVER DATA

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COORDINATES						
X 4119.	Y 1766.	Z 633.				
	C x 4119.	COORDINATES x y 4119. 1766.				

ALPHA FACTORS - ROADWAY ACROSS, RECEIVER DOWN

1 * 0.5 0.5 0.5 0.5 0.5 0.5

SHIELDING FACTORS - ROADWAY ACROSS.RECEIVER DOWN 1 * 3.0 3.0 3.0 3.0 3.0 3.0

 EVALUATION OF TRAFFIC NOISE BARRIER I-471 CAMPBELL CO.

 RECEIVER
 LEQ(H)
 SIG
 L10
 L50
 L90

 P107
 48.1
 5.5
 51.6
 44.6
 37.6

Figure B-1. Output from STAMINA 2.0 (Cont.)

APPENDIX C

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TRAFFIC VOLUME COUNT SUMMARIES

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TABLE C-1. SUMMARY OF OFF-PEAK I-471 TRAFFIC VOLUMES

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======			=====	======	TRAFFIC	VOLUME (V	===== РН)	=====	=====	
	100 AC 100 100 AC AC AC	MAINLINE					RAMP			
DIRECTION	AUTOS	LT	MT	HT	TOTAL	AUTOS	LT	MT	HT	TOTAL
Southbound	822	4	34	29	889	186	1	4	2	193
Northbound	829	2	39	31	901	215	0	7	2	224
Both	1,651	6	73	60	1,790	401	1	11	4	417

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TABLE C-2. SUMMARY OF PEAK I-471 TRAFFIC VOLUMES

				 T	RAFFIC V	DLUME (VP	н)			
	MAINLINE					RAMP				
DIRECTION	AUTOS	LT	MT	HT	TOTAL	AUTOS	LT	MT	HT	TOTAL
Southbound	2,943	0	30	20	2,993	286	0	2	0	288
Northbound	1,122	2	32	15	1,171	241	0	4	0	245
Both	4,065	2	62	35	4,164	527	0	6	0	533

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APPENDIX D

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SUMMARY OF DATA BY LOCATION

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		- 10 miles

TABLE D-1. SUMMARY OF OFF-PEAK DATA BY LOCATION

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			NOISE	LEVEL	TOTAL	VOL	===== UMES ((VPH)
RECEIVER NUMBER	DATE	TIME	L10	Leq	AUTOS	LT	MT	нт
2	4-23-85	12:05-12:15	51.0 50.2	49. 0	1896 1896	36 36	54 54	120 120
	4-29-85	12:20-12:30	51.3	49.8	2310	0	66	192
3	6-06-84	12:25-12:35	51.5 53.0	49. 6	1956 1986	0	78 84	66 70
	2-21-85	1:15-1:25	53.5	51.2 49.6	1890 2058	0	66 42	60 54
	4-29-85	12:35-12:45	52.5	50.1	2526	0	78	156
4	4-29-85	12:50-1:00 12:50-1:00	47.8 47.5	45.5 45.3	2200 2200	6 6	78 78	108 108
5	6-11-84	10:55-11:05 11:10-11:00	51.8 54.5	54.9 52.3	1596 1494	0 0	100 60	84 90
6	6-11-84 4-23-84	1:05-1:15 1:18-1:28 1:18-1:28	55.8 52.0 50.7	53.1 49.8 48.7	1960 1540 1540	18 54 54	84 48 48	54 108 108
7	6-11-84	1:25-1:35 1:40-1:50	52.0 50.5	49.6 50.4	1986 2010	6 0	96 96	48 66
8	4-23-85 10-16-84	1:45-1:55 1:45-1:55	46.0 48.5	43.9 46.5	1416 2112	18 0	78 132	78 84
9	6-18-84 7-09-84 12-17-84	11:10-11:20 11:05-11:15 11:00-11:10 11:15-11:25	52.0 54.0 51.5 52.5	50.8 52.3 49.9 50.5	1890 1926 1752 1968	6 12 18 12	138 90 96 96	54 72 42 78
10	6-18-84 12-17-84 2-21-85	11:45-11:55 11:35-11:45 11:10-11:20 11:25-11:35	55.8 54.2 55.5 54.3	53.5 56.3 53.8 52.3	1890 1986 2046 1866	0 0 0 6	108 84 72 54	48 103 78 84
1 1	4-29-85 6-18-84	2:00-2:10	56.2	54.0	2370 1920	0	90	90 48
11	12-17-84	12:00-12:10 12:20-12:30 1:05-1:15 1:20-1:30	55.8 54.2 54.5	53.4 52.3 52.5	2166 2100 2052	12 0 6	96 48 66	48 48 60 72
12	6-18-84	1:35-1:45 1:50-2:00	56.3 56.5	54.7 54.5	2286 2172	12 6	60 78	42 54
	12-17-84	1:40-1:50	56.1 57.5	54.8 55.0	2376 2154	6 12	72 132	48 72

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			NOISE	LEVEL	TOTAL	TOTAL VOLUMES(VPH)			
RECEIVER									
NUMBER	DATE	TIME	L10	Leq	AUTOS	LT	MT	нт 	
13	6-18-84	2:10-2:20	55.3	52.9	2154	6	84	30	
		2:25-2:35	56.3	53.0	2280	12	54	60	
	12-17-84	2:15-2:25	50.7	48.8	2376	6	54	48	
		2:30-2:40	52.2	50.2	2934	18	78	72	
14	6-18-84	3:00-3:10	57.3	55.2	2508	6	126	96	
	4-25-85	10:45-10:55	54.2	52.8	2214	30	102	108	
		10:45-10:55	54.2	52.6	2214	30	102	108	
15	7-09 - 84	10:45-10:55	50.8	48.5	1866	6	54	66	
	4-23-85	2:40-2:50	50.3	47.4	2136	18	36	102	
		2:40-2:50	47.0	45.3	2136	18	36	102	
16	6-21-84	11:25-11:35	54.3	52.2	2010	0	84	60	
		11:40-11:50	54.0	52.1	2118	6	102	102	
17	6-21-84	1:10-1:20	48.0	45.3	2334	6	54	60	
		1:25-1:35	49.3	46.7	21 9 0	6	66	78	
18	6-21-84	1:45-1:55*	49.5	46.6	2268	12	120	48	
		2:00-2:05	48.0	45.7	2118	0	114	48	
		2:00-2:05	47.5	45.3	2118	0	114	48	
19	2-21-85	10:50-11:00*	50.2	48.7	1848	12	9 0	48	
	4-25-85	10:30-10:40 _*	47.5	45.9	1944	18	66	78	
		10:30-10:40	49.2	46.7	1944	18	66	78	
20	7 - 09-84	1:55-2:05	49.8	47.8	1872	6	78	36	
		2:10-2:20	47.9	47.9	2280	0	96	66	
100	10-16-84	10:45-10:55	51.2	49.9	1968	24	48	30	
		11:00-11:10	52.0	50.3	1836	12	78	102	
	12 - 17-84	11:00-11:10	53.3	51.0	1752	18	96	42	
		11:15-11:25	54.5	53.3	1968	12	96	78	
101	10-16-84	10:45-10:55	53.8	52.2	1968	24	48	30	
		11:00-11:10	54.8	53.0	1836	12	78	102	
	12-17-84	11:35-11:45	54.2 55.2	52.6 53.4	1986 2322	0 18	84 96	108 90	
102	10-16-84	11:20-11:30	55.7	54.1	1938	6	102	48	
	10 17 0/	11:35-11:45	56.0	54.9	1/94	12	/8	66	
	12-1/-84	1:05-1:15	55.0	52.8	2100	0	48	60	
		1:20-1:30	JJ.U	22.2	2052	b	00	12	

TABLE D-1. SUMMARY OF OFF-PEAK DATA BY LOCATION (Cont.)

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			NOISE	======== LEVEL	TOTAL	TOTAL VOLUMES(VPH)			
DECEIVED									
NUMBER	DATE	TIME	L10	Leq	AUTOS	LT	MT	нт	
103	10-16-84	11:20-11:30	57.3	55.8	1938	6	102	48	
		11:35-11:45	56.8	55.3	1794	12	78	66	
	12-17-84	1:40-1:50	53.2	51.6	2376	6	72	48	
		1:55-2:05	53.8	52.4	2154	12	132	72	
104	10-16-84	12:55-1:05	52.5	50.8	1602	12	9 0	60	
	4-23-85	12:23-12:33	54.3	51.5	1632	54	36	114	
		12:12-12:33*	53.2	50.8	1632	54	36	114	
105	4-29-85	1:05-1:15	47.8	45.7	2184	6	72	96	
105	, .,	1.05 1.15	46.2	44.5	2184	6	72	96	
106	4-29-85	1:20-1:30	45.0	43.0	2070	6	9 0	78	
107	10-16-84	1:30-1:40	49.5	48.2	1944	18	78	60	
107	10 10 01	1:45-1:55	51.0	48.5	2152	0	132	24	
	4-29-85	1:40-1:50	48.5	46.4	2160	Ő	66	96	
108	10-16-84	2.05-2.15	52 2	50 /	1482	٥	126	54	
100	10 10 04	$2 \cdot 20 - 2 \cdot 30$	49 7	48.0	2340	0	90	36	
	2-21-85	11.45-11.55	51.2	49.2	1812	6	42	48	
	2 21 05	12:00-12:10	51.0	49.0	2256	6	84	42	
109	10-16-84	2.05-2.15	57.0	54.6	2082	0	126	54	
105	10 10 04	2.05 2.15	5/ 0	52 1	2340	ñ	90	36	
	2-21-85	11.45-11.55	52.8	50 3	1812	6	42	48	
	2 21 05	12:00-12:10	52.8	51.8	2256	6	84	42	
110	11-29-84	10.45-10.55	513	48 9	1902	24	78	70	
110	11 25 04	11.00 - 11.10	48.0	45.9	1728	30	70	18	
		11.00 11.10	10.0		1, 20	50	, 2	10	
111	11-29-84	11:20-11:30	48.3	45.9	2052	48	114	102	
		11:35-11:45	48.0	47.0	2112	24	9 0	120	
112	11-29-84	12:55-1:05	50.3	48.4	2040	36	96	84	
		1:10-1:20	52.8	51.0	1 9 80	18	9 0	9 0	
	12-17-84	2:15-2:25	49.3	47.6	2376	6	54	48	
113	11-29-84	1:30-1:40	58.3	55.5	2136	54	9 0	9 0	
		1:45-1:55	57.3	54.7	2352	30	66	60	
	4-29-85	2 : 15-2:25_	59.3	56.8	29 58	0	126	84	
		2:15-2:25	58.7	56.8	2958	0	126	84	
114	11-29-84	2:05-2:15	60.3	57.8	2220	42	66	96	
		2:20-2:30	60.0	57.4	2670	30	120	60	
		11:00-11:10	53.0	51.2	1728	48	66	54	
		11:00-11:10	53.8	51.6	1728	48	66	54	

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TABLE D-1. SUMMARY OF OFF-PEAK DATA BY LOCATION (Cont.)

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			NOISI	TOTAL VOLUMES(VPH)				
RECEIVER NUMBER	DATE	TIME	 L10	Leq	AUTOS	LT	 MT	- - нт
115	3-27-85 4-25-85	12:30-12:40 11:40-11:50 11:40-11:50	56.2 55.0 54.5	54.2 52.4 52.3	1932 2004 2004	0 42 42	48 78 78	84 30 30
116	3-27 - 85	12:55-1:05 1:10-1:20	60.2 57.7	57.9 56.1	1938 1914	6 12	96 84	72 36
117	3-27-85 4-25-85	1:35-1:45 12:00-12:10* 12:00-12:10	62.5 58.5 58.2	60.0 56.1 55.7	2064 1770 1770	0 24 24	108 102 102	114 114 114

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TABLE D-1. SUMMARY OF OFF-PEAK DATA BY LOCATION (Cont.)

* Data taken simultaneously with analyzer and meter and recorder

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			NOISE	LEVEL	TOTAL	VOLU	JMES(VPH)
RECEIVER NUMBER	DATE	TIME	 L ₁₀	- Leq	AUTOS	LT	MT	HT
2	4-17-85 4-22-85 4-22-85	5:15-5:25 5:30-5:40 5:30-5:40	54.2 56.8 53.8	51.5 54.3 51.5	5352 4830 4830	0 6 6	102 36 96	66 72 72
3	4-02-85	5:11-5:21 * 5:11-5:21 *	54.8 56.2	53.3 54.5	5380 5388	0 0	56 56	54 54
4	4-25-85	4:25-4:35* 4:25-4:35*	49. 5 50.2	48.1 47.6	3270 3270	36 36	144 144	84 84
5	3-20-85	3:55-4:05 4:10-4:20	56.5 57.0	54.9 55.1	3570 5184	0 6	138 36	60 36
6	3-20-85	4:30-4:40 4:45-4:55	55.7 56.0	54.8 54.5	4110 4932	0 0	84 66	36 30
7	3-20-85	5:05-5:15 5:20-5:30	56.0 55.5	54.4 53.6	5220 5196	0 0	60 109	24 30
8	3-20-85	5:05-5:15 5:20-5:30	51.5 50.8	48.5 48.4	5220 5196	0 0	60 109	24 30
9	2-27-85	3:55-4:05 4:10-4:20	55.0 55.0	52.6 53.4	3798 5052	6 0	78 84	30 48
10	3-06-85	4:30-4:40 4:45-4:55	55.0 57.2	52.9 55.5	3990 4914	0 12	72 36	36 6
11	3-06-85	3:55-4:05 4:10-4:20	59.3 58.5	56.9 56.3	3942 4932	12 0	72 66	36 42
12	2-27-85 3-06-85	5:05-5:15 5:20-5:30 3:55-4:05 4:10-4:20	60.8 60.5 61.7 60.5	59.8 58.9 60.0 58.6	4956 4710 3942 4932	12 12 12 0	60 72 72 66	30 48 36 42
13	2-27-85	5:40-5:50 5:55-6:05	56.2 56.7	54.9 54.8	4650 3708	12 6	66 48	36 30
14	3-14-85 4-25-85	3:55-4:05 4:10-4:20 5:30-5:40	57.0 57.7 59.5	55.3 56.4 57.4	3510 4848 4068	6 0 12	78 96 108	66 54 18

TABLE D-2. SUMMMARY OF PEAK DATA BY LOCATION

			NOISE	NOISE LEVEL		TOTAL VOLUMES(VPH)			
RECEIVER NUMBER	DATE	TIME	L ₁₀	L eq	AUTOS	LT	MT	HT	
15	3-14-85	5:40-5:50 5:55-6:05	52.0 52.2	50.6 50.9	4668 3666	0 0	66 42	42 30	
16	3-06 - 85	5:05-5:15 5:20-5:30	55.8 56.8	53.9 54.8	4842 5280	0 0	54 60	54 18	
17	3-14-85	5:05-5:15 5:20-5:30	49.2 48.7	47.7 47.3	5184 50 34	6 6	60 72	30 42	
18	3-14 - 85	5:05-5:15 5:20-5:30	47.5 47.3	46.6 45.6	5184 5034	6	60 72	30 42	
19	4-25-85 3-14-85	4:30-4:40	49.0 50.2	46.4	4392	6	60 70	42 36	
20	3-06 - 85	4:43-4:55	51.7	50.0 50.3	5142 4140	6	42	24 54 30	
100	4-49-85	6:10-6:20 [*] 6:10-6:20	58.0 56.5	56.8 54.6	3660 3660	0	90 90	24	
101	2-27-85	4:30-4:40	57.0 58.8	54.6 57.0	3990 4914	0	72 72	- · 36 48	
102	2-27-85	5:05-5:15 5:20-5:30	60.2 59.7	58.8 58.0	4956 4710	12 12	60 72	30 48	
103	2 - 27 - 85	5:40-5:50 5:55-6:05	59.0 59.5	57.6 58.0	4650 3708	12 6	66 48	36 30	
104	4-17 - 85	5:00-5:10 [*] 5:00-5:10	53.2 52.3	51.4 51.7	4230 4230	12 12	66 66	24 24	
	4-25 - 85	4:50-5:00 [*] 4:50-5:00	52.3 52.7	51.2 50.9	4050 4050	6 6	126 126	54 54	
105	4 - 25-85	4:10-4:20 [*] 4:10-4:20 [*]	49.0 48.5	48.0 46.1	3762 3762	36 36	54 54	48 48	
106	4-17 - 85 4-25 - 85	4:00-4:10 3:55-4:05 3:55-4:05	46.5 48.3 47.5	45.0 44.9 44.9	3870 4062 4062	0 54 54	138 72 72	108 72 72	
107	3-20-85 4-22-85 4-29-85	5:55-6:05 4:30-4:40 5:15-5:25	51.5 51.2 49.7	49.5 48.7 48.1	3636 5256 5442	6 0 0	36 108 84	12 3 42 42	

TABLE D-2. SUMMMARY OF PEAK DATA BY LOCATION

			NOISE LEVEL		TOTAL VOLUMES(VP)			VPH)
RECEIVER NUMBER	DATE	TIME		Leq	AUTOS	LT	MT	HT
108	3-20-85	4:30-4:40 4:45-4:55	54.3 54.5	52.6 52.5	4110 4932	0 0	84 66	36 30
109	3-20-85	3:55-4:05 4:10-4:20	56.8 56.6	55.0 54.5	3570 5184	0 6	138 36	60 36
110	4-10-85	3:55-4:05 4:10-4:20	52.7 52.5	51.2 51.2	3810 4614	0 0	108 66	60 24
	4-29-85	5:35-5:45 5:35-5:45	50.0	48.4 48.4	5340 5340	6 6	78 78	84 84
111	3-14-85 4-10-85	5:40-5:50 4:30-4:40 4:45-4:55	52.0 50.7 51.2	50.5 49.5 49.5	4668 4332 5046	0 0 0	66 90 48	42 6 42
112	3-06-85 4-29-85	4:30-4:40 5:50-6:00 5:50-6:00	55.3 54.0 54.7	53.4 52.9 53.2	4140 4506 4506	6 0 0	42 84 84	54 24 24
113	3-06-85 3-14-85	5:05-5:15 4:30-4:40 4:45-4:55	61.5 55.5 56.0	56.4 53.5 55.0	4842 4074 5142	0 6 0	54 60 72	54 36 24
114	4-10-85	5:05-5:15 5:20-5:30	59.5 60.5	58.1 58.5	5304 5148	6 0	54 90	30 30
115	4-03-85	3:55-4:05 4:10-4:20	57.5 57.5	55.7 55.9	3828 5172	0 0	72 84	48 30
116	4-03-85	4:30-4:40 4:45-4:55	60.0 60.5	58.1 58.6	4170 5064	0 6	90 96	36 48
117	4-03-85	5:05-5:15 5:20-5:30	61.7 60.5	60.0 58.8	5418 5232	0 0	78 42	42 36
118	4-17-85 4-29-85	5:30-5:40 4:00-4:10 4:00-4:10	62.5 64.3 64.2	60.3 61.3 61.7	5184 4716 4716	6 0 0	60 192 192	24 66 66
119	4-17-85 4-29-85	5:45-5:55* 5:45-5:55* 4:40-4:50* 4:40-4:50*	56.0 55.3 56.8 57.0	53.7 53.3 54.9 55.2	4614 4674 5400 5400	0 0 0 0	36 36 66 66	60 60 48 48

TABLE D-2. SUMMMARY OF PEAK DATA BY LOCATION

* Data taken simultaneously with analyzer and meter and recorder

APPENDIX E

COVER LETTER AND QUESTIONNAIRE

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KENTUCKY TRANSPORTATION RESEARCH PROGRAM

UNIVERSITY OF KENTUCKY

College of Engineering Transportation Research Building 533 South Limestone Lexington, Kentucky 40506-0043 Telephone: 606-257-4513

Dear Resident:

The University of Kentucky Transportation Research Program, in conjunction with the Kentucky Transportation Cabinet, is conducting a research study to evaluate the effectiveness of the traffic noise barrier located on Interstate 471 in Campbell County. As part of this study, it is important to obtain the opinion of the affected residents concerning the noise barrier.

Enclosed is a questionnaire and a self-addressed, postage-paid return envelope. Please fill out the questionnaire and return it at your earliest convenience. All information will be kept confidential. Information from the questionnaires will be used in determination of traffic noise barrier effectiveness and as an aid in future decisions regarding location and construction of noise barriers. Thank you for your assistance.

Sincerely,

Tom Creasey Transportation Research Engineer

TRANSPORTATION RESEARCH PROGRAM

UNIVERSITY OF KENTUCKY

EFFECTIVENESS OF TRAFFIC NOISE BARRIERS QUESTIONNAIRE

Please complete and return this questionnaire in the enclosed self-addressed, postage-paid envelope. Thank you for your cooperation.

1.	How long have you	lived at this addre	ss? <u> Y</u> ears	Months
	What is your stree	et address:	·	
2.	How many persons 1	live at this residen	ce?	
3.	Do you own your re	esidence, or do you	rent? Own	Rent
4.	How would you desc construction of I barriers?	cribe your neighborh 471 and the accompa	ood before and aft nying traffic nois	cer Se
		Before Construction (Check one)	After Construction (Check one)	
	Very quiet			
	Quiet			
	A little noisy			
	Noisy			
	Very Noisy		- talk - the spectra spectrum	

5. Are you aware that a noise barrier, which was constructed at the same time as I 471, stands between your residence and the interstate? Yes No

(If you answered "No" to the above question, please stop here and return the questionnaire; if you answered "Yes", please continue).

6. How did you learn about the noise barrier?

Television/Radio

Newspaper

Public	hearing notice
Letter	from a political representative
Observe	ed construction of barrier
Other	

7. How do you feel that the presence of a noise barrier has affected these highway-related problems compared to the situation where no noise barrier was present?

	Worse	No Effect	Slight Improvement	Significant Improvement	No Opinion
Highway dust and dirt				·	<u> </u>
Headlight glare					
Litter from vehicles					- <u></u>
Highway noise			·····		
Road vibration					
Road fumes	·				
Privacy					
Other					
8. How do you fe the following noise barrier	eel that g activiti g was pres	the presence les compared sent?	of a noise to the situa	barrier affects ation where no	
	More Difficult	t No Effect	Less Difficult	Significantly Less Difficult	No Opinion
Conversation indoors					
Conversation outdoors					
Telephone use					
Relaxing indoors				·	
Relaxing outdoors					
Sleeping					
Leaving windows open					
Other					

9. Indicate if you feel that the noise barrier has created any of the following disadvantages:

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Yes No	No Opinion
Creates closed-in feeling	
Hurts area environment	
Limits or restricts view	
Requires more yard maintenance	·····
Visual eyesore; unsightly	
0ther	
10. How do you feel about the appearance of the barrie	er?
AttractiveOKUnsightly	
11. Compared to having no noise barrier at all, how effect the noise barrier has been in reducing the to	ffective do you raffic noise?
Very Somewhat EffectiveNo EffectiveNo Effective	ct
12. How do you feel the presence of the noise barrier the value of your property?	has affected
DecreasedDecreasedNoIrSignificantlySomewhatEffectSomewhat	ncreased omewhat
13. If the noise barrier had not been built, do you fe would use your yard more, less, or the same amount	eel that you t?
MoreLessSame Amount	
14. How do you feel about the noise barrier in general	1?
LikeDislikeNo Opinion	
Please feel free to submit any further comments al barrier here. Thank you. Your help is sincerely appre	bout the noise eciated.