## Research Report

KTC 96-10

# EVALUATION OF SUPERIOR PERFORMING PORTLAND CEMENT CONCRETE PAVEMENTS IN KENTUCKY 

by

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and
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May 10, 1996

Mr. Paul E. Toussaint<br>Division Administrator<br>Federal Highway Administration<br>330 West Broadway<br>Frankfort, Kentucky 40602-0536

SUBJECT: Implementation Statement KYHPR 94-156, "Evaluation of Superior Performing Portland Cement Concrete Pavements in Kentucky," NCP Code 4C1C

Dear Mr. Toussaint:
The vast majority of Portland cement concrete (PCC) pavements constructed in Kentucky during the past forty years have been confined to the Interstate and Parkway Systems. Initially, 78 percent of the $1,215-\mathrm{km}$ ( $755-\mathrm{mi}$ ) Interstate System and 50 percent of the $1,040-\mathrm{km}$ ( $646-\mathrm{mi}$ ) Parkway System was PCC pavement. Performance of PCC pavements, designed using 1960s and 1970s criteria, has varied considerably. However, substantial lengths of the original PCC pavements are still performing satisfactorily. Research Report KTC 96-10 entitled "Evaluation of Superior Performing Portland Cement Concrete Pavements in Kentucky," describes inventories and analyses undertaken during the course of this research study to determine if there are common factors which have contributed to the superior performance of certain sections of Kentucky's PCC pavements. An extensive inventory of Kentucky's interstate, parkway, and other primary routes was performed to determine locations of PCC sections over fifteen years old that had demonstrated excellent performance. Selection of PCC pavement sections for evaluation was based on longevity and traffic accumulations. Both on-site and laboratory evaluations were performed.

The primary distresses of these PCC pavements were transverse joint deterioration and joint faulting. Intermediate span transverse cracking, with occasional faulting, was observed to be the predominant type of PCC cracking. Common factors which would contribute positively to the outstanding performance of these PCC pavements were the concrete's high compressive strengths and high moduli of elasticity. Other factors determined during the evaluations would contribute negatively to any pavement's performance. These factors include very low California Bearing Ratios (CBR's) in both the dense-graded aggregate base and subgrade layers underlying the concrete pavement, relatively high amounts of minus $75 \mu \mathrm{~m}$ (No. 200) sieve material in the dense-graded aggregate base, and high moisture contents and fairly low unconfined compressive strengths of the soil subgrade layer.

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One task, Task F, was not performed by researchers due to time and budget constraints. The Study Advisory Committee (SAC) for this study recommended the study be extended to complete the task of evaluating adjacent PCC sections that had exhibited poor performance. Information from this task would have enhanced final conclusions and recommendations. Additionally, the SAC recommended that the researchers use the extension to:

- Incorporate data from the Kentucky Department of Highways' Pavement Management Group, including distress surveys, soil and design data,
- Backcast ESAL's from ADT and \%TRUCK data -- this information is needed to effectively analyze pavement performance. The design CBR, pavement thickness design and design traffic should be used to determine when the pavements selected for study should have failed,
- For design purposes, drainage should be quantified in terms of the AASHTO drainage coefficient,
- Evaluate the workmanship of the pavement sections by the falling weight deflectometer (FWD) by determining the load transfer capabilities of selected pavement joints within the pavement sections studied.

The Kentucky Department of Highways concurs with the recommendations of the SAC and supports the efforts of the researchers to fully complete this study. However, current PCC pavement designs, including thicker PCC slabs, drainable bases, shorter joint spacings, skewed joints and improved jointfiller materials have contributed to improved joint quality and minimized intermediate span transverse cracking and faulting. Also, improved construction and inspection methods and adherence to presently accepted mix design and production parameters, including screening of potentially reactive aggregates, acceptance of pozzolanic materials and tighter standards on mix variations, have provided a more consistent product. It is conceivable that if present design, construction, and inspection processes had been in use in the 1960s and 1970s, an even higher percentage of the original PCC pavements would be performing satisfactorily with only minimum lengths requiring overlays or reconstruction. It is logical to expect that the improved design, construction and inspection methods of today will provide a consistent 30-year, or longer, pavement life with the only maintenance activities involving joint resealing and diamond grinding to restore surface smoothness and ride quality.

Sincerely,

J. M. Yowell, P.E.<br>State Highway Engineer

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## EXECUTIVE SUMMARY

This research report describes a program of study directed at determining common factors which have contributed to the superior performances of selected sections of Portland cement concrete (PCC) pavements in Kentucky. This involved an extensive inventory of Kentucky's interstate, parkway, and other primary routes to determine locations of PCC pavement sections greater than 15 years old that had performed satisfactorily with minimal maintenance. Twelve of the best performing PCC pavements with long service and heavy traffic were selected for detailed evaluations. A series of in-situ pavement tests were conducted followed by core drilling and sampling pavement material. Laboratory tests were conducted on the pavement samples to ascertain basic physical properties. No evaluations were made of PCC pavements exhibiting poor performance.

The vast majority of the PCC pavements constructed in Kentucky during the past forty years is confined to the Interstate and Parkway systems. Initially, 78 percent of the 1,215km ( $755-\mathrm{mi}$ ) Interstate system and 50 percent of the $1,040-\mathrm{km}$ ( $646-\mathrm{mi}$ ) Parkway system was PCC pavement. These values have been significantly reduced in recent years as substantial mileage of PCC pavement has been overlain with asphaltic concrete. Nevertheless, 890 km ( 553 mi ) of PCC existed in early 1994 on Kentucky's combined Interstate and Parkway systems, and only 93 km ( 58 mi ) of the 890 km ( 553 mi ) was reconstructed PCC pavement. Historically, PCC pavements have been selected infrequently for non-Interstate and nonParkway routes in Kentucky. Although the performance of PCC pavements on Kentucky's Interstate and Parkway systems has varied considerably, substantial mileage of the original PCC pavements, designed from criteria in effect during the 1960 s and 1970 s , is performing satisfactorily. The primary source of PCC pavement distress observed was transverse joint deterioration and faulting. Intermediate span transverse cracking with occasional faulting was the only significant type of PCC cracking observed.

Based on the testing program, the only common factors which would contribute in a positive manner to the superior performance of the 12 PCC pavements were the high compressive strengths and moduli of elasticity of the PCC slabs. The values greatly exceed design criteria. The other common factors determined from the testing program would be expected to contribute in a negative manner; these being very low in-situ CBR values and high percentages of minus $75 \mu \mathrm{~m}$ (No. 200 sieve) material in the dense graded aggregate (DGA) bases; and, high moisture contents, low in-situ CBR values and low unconfined compressive strengths of the underlying subgrades.

PCC pavement designs in common use today -- thicker PCC slabs, drainable bases, shorter joint spacings, skewed joints and improved joint-filler materials -- will contribute to improved joint quality and minimized intermediate span transverse cracking and faulting. Also, adherence to presently accepted mix design and production parameters including improved screening of potentially reactive aggregates, acceptance of pozzolanic materials and tighter standards on mix variations will provide a more consistent product. It is conceivable that if designs presently in use had been specified during the 1960 s and 1970 s , an even higher percentage of the original PCC pavements would be serving satisfactorily. It is logical to anticipate that the improved designs in common use today will provide a consistent 30-year or longer pavement life, with the only maintenance consisting of joint resealing and diamond grinding to restore surface smoothness and ride quality.

## INTRODUCTION

The primary uses for Portland cement concrete (PCC) on high-type, heavy-duty pavements in Kentucky during the past forty years have been for the Interstate and Parkway systems. Approximately three-fourths of the Interstate system and one-half of the Parkway system were initially constructed with PCC wearing surfaces. These percentages have been significantly reduced in recent years as numerous PCC pavement sections developed distress or served their useful life and were subsequently overlain with a structural layer of asphaltic concrete (AC). It has been common practice during the past ten years to break and seat the PCC prior to overlaying with AC. A few of the PCC sections have been rubblized or removed prior to paving with AC. Only a small percentage of the PCC pavements have been replaced with PCC.

The uses of PCC on other Primary (mainly U.S.) routes have been infrequent and comprise a relatively small percentage of the high-traffic primary routes. The sections are generally fairly short in length and located in the vicinity of the larger urban areas, either approaches to or within the urban area. As these develop distress, or serve their useful life, the typical practice is to overlay with AC. The vast majority of the other primary routes has been initially AC and continues to be constructed with AC.

Few PCC pavement sections are presently being constructed in Kentucky. The contributing factors are quite complex. The early deterioration, particularly joints, of several PCC sections on the Interstate system and to a lesser extent on the Parkway system, influenced designers in the choice of pavement systems. However, several 15- to 30 -year old, or older, PCC pavement sections still remain in service on major highways in Kentucky and have performed satisfactorily with minimal maintenance.

The objective of this study was to determine if there were identifiable factors common to these PCC pavements which had contributed to their superior performance on high-traffic primary routes in Kentucky. The findings should be useful for optimizing design practices when specifying PCC pavements.

## PROCEDURE

The PCC pavement portions of the Interstate, Parkway, and other significant Primary routes were inventoried during 1993. Pertinent observations of physical conditions and performances were recorded. Photographs depicting typical conditions were taken.

- Twelve test projects comprising the combination of the best performing, longest service and
heaviest traffic PCC pavements were selected from the inventory for detailed evaluations. The projects included three Interstate sections, ranging from 25 to 33 years old, six Parkway sections, ranging from 22 to 31 years old, and three other Primary (U.S.) Route sections, ranging from 12 to 34 years old. A listing of the projects is contained in Table $I$ and the locations are depicted in Figure 1.

Two sites were selected on each of the 12 test projects for coring, in-situ testing and sampling. The sites were chosen in areas where the pavement was in essentially perfect condition with no cracks, spalls or other types of distress. Due respect was given to select sites with adequate sight distance to ensure an increased margin of safety for the test crews.

Three tests were typically conducted at each site, or six for each project. The tests were at mid-span, $305 \mathrm{~m}(1000 \mathrm{ft})$ apart in the outside wheel path of the outside traveled lane, approximately 1070 mm ( 42 in .) from the outside shoulder. Therefore, one lane closure and flagging protection sufficed for all three tests at a site. The other site was chosen in the opposite direction of travel and required another lane closure sequence.

The same sequence of coring, in-situ testing and sampling was followed at each test location. The sequence was:

- Take $150-\mathrm{mm}$ (6-in.) diameter core of PCC (ASTM C42) and measure thickness;
- Conduct in-situ CBR test (ASTM D4429) on base through core hole;
- Remove base material, place in sealed container for subsequent laboratory tests, and measure thickness of base;
- Conduct in-situ CBR test (ASTM D4429) on subgrade through core hole;
- Collect sample from the top 50 mm ( 2 in .) of the subgrade and place in sealed container for subsequent laboratory tests;
- Take Shelby tube sample of the subgrade for subsequent laboratory tests; and - Fill holes with base material and PCC.

Care was taken during the coring process to minimize contamination of the base with water from the core barrel. The truck used as a test platform for the CBR tests weighed $9,525 \mathrm{~kg}$ ( $21,000 \mathrm{lb}$ ) and was supported on blocks. A $50-\mathrm{mm}$ ( 2 -in.) diameter piston was forced at a constant rate into the subject material while measuring the load and corresponding penetration. Views of typical pavement testing and sampling are shown in Figures 2 through 4.

1-164 in Fayette County
2-175 in Laurel County
3-164 in Shelby County
4-BG Parkway in Nelson County
5 - WKY Parkway in Hopkins County
6 - Pennyrile Parkway in Hopkins/Christain County
7 - Pennyrile Parkway in Hopkins County
8 - GR Parkway in Ohio County
9 - Audubon Parkway in Daviess County
10 - US 127 in Owen County
11 - US 27 in Pulaski County
12 - US 119 in Pike County
$\omega$


Figure 2. Core samples were obtained from the PCC pavements.


Figure 3. In-situ California Bearing Ratio tests were performed on the surface of the dense graded aggregate base and the underlying soil subgrade.


Figure 4. Undisturbed soil subgrade samples were obtained for laboratory testing.

Laboratory tests were conducted on the PCC cores, base samples, subgrade samples directly below the base, and subgrade tube samples. The specific tests and sequences were:

## PCC Cores

- Core ends faced and capped with sulfur mortar (ASTM C617);
- Compressive strength tests conducted on four cores (ASTM C39); and,
- Static modulus of elasticity tests conducted on another two cores (ASTM C489);


## Base Samples

- Moisture content tests conducted (ASTM D2216);
- Minus $75 \mu \mathrm{~m}$ (No. 200 sieve) material tests conducted (ASTM D1140); and,
- Plasticity indices tests conducted (ASTM D4318);


## Disturbed Soil Subgrade Samples

- Moisture content tests conducted (ASTM D2216);


## Undisturbed Soil Subgrade Samples

- Moisture content tests conducted (ASTM D2216);
- Wet densities of the undisturbed samples determined;
- Unconfined compressive strength tests conducted (ASTM D2166);
- Particle size analysis tests conducted (ASTM D422);
- Specific gravity tests conducted (ASTM D854);
- Plasticity indices tests conducted (ASTM D4318); and,
- Classification of soils performed (ASTM D2487).


## DATA PRESENTATION AND FINDINGS

## Inventory

The 1993 inventory of Kentucky's Interstate, Parkway, and other Primary routes indicated that the vast majority of the PCC pavements constructed during the past 40 years is confined to the Interstate and Parkway systems.

As noted in Table II, $78 \%$ of the $1,215 \mathrm{~km}$ ( $755-\mathrm{mi}$ ) Interstate system was originally PCC. Table III indicates that $50 \%$ of the $1,040 \mathrm{~km}(646-\mathrm{mi})$ Parkway system was originally PCC. These values have been significantly reduced in recent years as substantial mileage of PCC pavement has been overlain with asphaltic concrete (AC). Nevertheless, 890 km ( 553 mi ) of PCC existed as of January 1994 on Kentucky's combined Interstate and Parkway systems, and only 93 km ( 58 mi ) of this was reconstructed PCC pavement.

Appendix A contains information for pavement types by mileposts for each section of each Interstate highway in Kentucky. The left date indicates original construction and dates to the right of the slash marks indicate overlays or major rehabilitation activities. Appendix B contains similar data for the Parkway system.

PCC pavements have been selected infrequently for non-Interstate and non-Parkway routes in recent years. Most of the PCC pavements on these other Primary routes are fairly short in length and located either on approaches to or within urban areas.

## Early Designs

The typical Interstate thickness design for the majority of the routes was 250 mm ( 10 in .) of PCC on $150-\mathrm{mm}$ ( $6-\mathrm{in}$.) dense graded aggregate (DGA) base. The first few designs in the early 1960's had only 125 mm ( 5 in .) DGA base. Joint spacing was 1.5 m ( 50 ft ) for limestone aggregate. The few sections containing gravel aggregate typically had $7.5-\mathrm{m}$ ( $25-\mathrm{ft}$ ) joint spacing. Welded wire fabric was placed at the mid-depth of the slab. Joints were sawed at $90^{\circ}$ to the direction of travel. Joints were sealed with hot-poured asphalt. Dowel bars were used for load transfer at the joints. Continuously reinforced concrete pavement was placed on a total of $13 \mathrm{~km}(8 \mathrm{mi})$ of I-71 and I-275; however, performance of the continuously reinforced concrete sections was considered to be inferior.

The typical Parkway thickness design was $225-\mathrm{mm}$ ( $9-\mathrm{in}$.) PCC on $100-\mathrm{mm}$ (4-in.) DGA base. Jointing and fabric details were the same as the Interstate designs.

Thickness designs for other Primary (US) routes were typically 200-mm (8-in.) PCC on 100mm (4-in.) DGA base. Jointing and fabric details were the same as the designs for the Interstates and Parkways.

## Later Designs and Actions

After 1976, joint spacings were reduced for new construction. A variable spacing was common, typically $3.7,4.0,5.2,5.5 \mathrm{~m}(12,13,17,18 \mathrm{ft})$, averaging about $4.6 \mathrm{~m}(15 \mathrm{ft})$. Welded wire fabric was not used. A $90^{\circ}$ or a skewed joint pattern was used. Joint sealants were either hot-poured asphalt, neoprene or silicone.

Since 1982, several PCC pavements have been rehabilitated with edge drains. Normally joints were re-sawed and widened and sealed with silicone. Some sections had slabs or portions of slabs replaced during the edge drain installation and the re-jointing operation. Many of these pavements are approaching 30 years of service.

Substantial mileage of PCC pavements has been overlain with AC. Prior to 1982, the AC was placed directly on the PCC pavement. Reflective cracking at the joints was common in
a few years. Since 1982, breaking and seating of the PCC pavement prior to overlay with AC has been the common practice.

The original 1,215-km ( $755-\mathrm{mi}$ ) Interstate system had $78 \%$ ( 953 km ( 592 mi )) of the mileage in PCC pavement. By January 1994, about $40 \%$ of that mileage had been overlain with AC, leaving 547 km ( 340 mi ) with a PCC wearing surface.

The original 1,040-km ( $646-\mathrm{mi}$ ) Parkway system had $50 \%$ ( 523 km ( 325 mi )) of the mileage in PCC pavement. By January 1994, about $33 \%$ of that mileage had been overlain with AC, leaving 346 km ( 215 mi ) with a PCC wearing surface.

Since 1991, approximately 32 km ( 20 mi ) of PCC pavement has been diamond ground on I$65, \mathrm{I}-75, \mathrm{I}-275$ and I-471. Ride quality has been substantially improved as a result of diamond grinding.

By January 1994, the average age of the PCC pavements on Kentucky's Interstate and Parkway systems at the time of an AC overlay had been 21 years. The weighted average for the Interstate system was 19.6 years and the Parkway system was 24.6 years. Table IV contains the average age of overlays for Interstates and Parkways that had overlays as of January 1994. With exception of I-71, most of the Interstate and Parkway PCC pavements served the 20-year design life before being overlaid.

The average age of the PCC pavements initially on Kentucky's Interstate and Parkway systems that were still in service as of January 1994 and had not required an overlay had been 24.0 years. The weighted average for the Interstate system was 22.2 years, which included sections of I-24, I-265, I-275, and I-471 constructed rather recently, and the Parkway system was 26.4 years. Table V contains the average age for the original Interstate and Parkway PCC pavements still in service as of January 1994. All had served the 20-year design life.

## Recent Designs

Present design practices for PCC pavements have changed substantially from those used during the massive interstate/parkway construction phase of the 1960s and 1970s. Typical thickness design is 280 mm (11 in.) PCC, although the thickness can range from 255 mm ( 10 in.) for lightly traveled routes to 325 mm ( 13 in .) for heavy coal-haul routes.

Base thicknesses are typically 200 mm ( 8 in .), consisting of a $100-\mathrm{mm}$ ( $4-\mathrm{in}$.) treated drainage layer over a $100-\mathrm{mm}$ (4-in.) DGA base which has a lower percentage of minus 75
$\mu \mathrm{m}$ (No. 200 sieve) fines than previously used. Longitudinal drains are installed along the shoulder.

Distances between joints are random (variable), averaging about $4.5 \mathrm{~m}(15 \mathrm{ft})$ with a range of 3.5 m ( 1.2 ft ) to 5.5 m ( 18 ft ). Joints are typically skewed.

Welded wire fabric is not used. The PCC is non-reinforced. Dowel bars are still used for load transfer at the joints.

Neoprene is the typical choice for joint sealing for new construction and silicone is normally selected for joint repair.

Table VI shows the general comparison of the design details used during the 1960s and 1970s and those in the current use. The only common design parameter is the use of dowel bars at the joints for load transfer. All other basic design parameters have changed.

## Pavement and Laboratory Tests

Table VII contains average values for each project for the pavement and laboratory tests. Appendix C contains more detailed information in summary form for each project including. ranges of values. Individual test results on each sample are given in Appendix D.

## PCC Pavement Cores

Thicknesses are very close to original designs. Average for the Interstate projects is 254 mm ( 10.0 in .); Parkway projects, 231 mm ( 9.1 in .); and the three U.S. route projects, 211 mm ( 8.3 in.). The range in values is small for the individual Interstate and Parkway projects.

Compressive strengths vary considerably ranging from 39.6 to $57.2 \mathrm{MPa}(5,740$ to $8,300 \mathrm{psi})$, while averaging $46.0 \mathrm{MPa}(6,680 \mathrm{psi})$. These values greatly exceed the accepted design value of $24.1 \mathrm{MPa}(3,500 \mathrm{psi})$.

Static modulus of elasticity values likewise vary considerably ranging from 25.7 to 35.0 GPa ( 3.73 to 5.08 million psi), while averaging 30.8 GPa ( 4.47 million psi). The average is commensurate with the average compressive strength value. An estimate of the modulus of elasticity ( E ) value may be obtained using the following accepted relationship:

$$
\mathrm{E}=4.73 V_{\mathrm{f}_{\text {cyl }}^{\prime}}\left(\text { or } \mathrm{E}=57,000 V_{\mathrm{f}_{\text {cyl }}^{\prime}}\right)
$$

where E is in GPa (or psi) and $\mathrm{f}^{\prime}$ cyl is the compressive strength in MPa (or psi) determined through standard tests. Inserting the average compressive strength value obtained from tests on the PCC cores of $46.0 \mathrm{MPa}(6,680 \mathrm{psi})$ yields an estimated E value of 32.1 GPa ( 4.66 $\left.\times 10^{6} \mathrm{psi}\right)$, close to the measured average of $30.8 \mathrm{GPa}\left(4.47 \times 10{ }^{6} \mathrm{psi}\right)$.

## Base Samples

The base material directly under the concrete is limestone dense graded aggregate on 11 of the projects, the only exception being a sandstone base on the US 119 (Pike County) project: Thicknesses are very close to original designs; averaging 150 mm ( 5.9 in .) for the Interstate projects, 100 mm ( 4.0 in .) for the Parkway projects and 94 mm ( 3.7 in .) for the three U.S. route projects.

In-situ CBR values ranges from 8 to 20 (excluding the sandstone base project) with an average of 13 . These values are significantly lower than those assumed in structural design calculations.

Average moisture contents range from 4.7 to $9.3 \%$, averaging 6.4\%. These are typical for obtaining maximum compacted densities.

The minus $75 \mu \mathrm{~m}$ (No. 200 sieve) values range from 9.2 to $17.0 \%$, averaging $12.2 \%$. Current specifications limit this value to a maximum of $10 \%$, with acceptable values between 2 and $10 \%$. At the time these pavements were constructed, the specification was 12 to $15 \%$.

## Disturbed Soil Subgrade Samples

The in-situ CBR values range from 2 to 9 , (excluding the sandstone project) with an average of 4.0. This is the value most often assumed for design purposes at that time, but now would require subgrade modification prior to construction.

Moisture contents range from 13.8 to $26.3 \%$, (excluding the sandstone project) with an average of $19.7 \%$. The values are reasonably high and indicate subgrades in weakened conditions.

## Undisturbed Soil Subgrade Samples

The unconfined compressive strengths of samples extracted from Shelby Tubes range from 92 to 280 kPa (13.4 to 40.6 psi ) averaging 184 kPa ( 26.7 psi ).

Moisture contents range from 13.3 to $28.0 \%$ (excluding the sandstone project) with an average of $19.0 \%$. These are essentially the same as those obtained from samples directly below the base.

Wet densities vary considerably reflecting the influence of soil type, prevailing moisture content, and relative compaction.

The subgrade soils generally classify as clay with low plasticity (CL). On four projects, the soil type varies considerably at the different test sites. The sandstone project is an exception.

## SUMMARY, CONCLUSIONS AND RECOMMENDATIONS

The objective of this research study was to determine common factors contributing to the superior performance of selected sections of PCC pavements in Kentucky. An extensive inventory of the highway system was conducted followed by selection of 12 projects for subsequent in-situ pavement and laboratory testing.

Performance of PCC pavements on Kentucky's Interstate and Parkway systems and other Primary routes has varied considerably; however, the majority has performed beyond their design lives. The primary source of PCC pavement distress observed was transverse joint deterioration and faulting. This combination generally results in substandard ride quality. The overall concrete quality is quite satisfactory, except in the vicinity of the distressed joints. Aggregate popouts and small alligator (or crazing) cracks were evident on several sections, but neither appears detrimental.

Intermediate span cracking was the only significant type of cracking observed. These were generally at mid-span or occasionally at third points. Faulting of intermediate span cracks was observed on a portion of the sections.

The basic design parameters, excepting pavement thickness, for the 12 projects selected for detailed evaluations were essentially the same -- dowel bars for joint load transfer, hotpoured asphalt joint filler, welded wire fabric reinforcement, $90^{\circ}$ jointing pattern, $15-\mathrm{m}$ (50ft) joint spacing and DGA limestone base with high fines content.

PCC slab and DGA base thicknesses were common for the particular route classifications, i.e., $250-\mathrm{mm}(10-\mathrm{in}$.) PCC/ $150-\mathrm{mm}$ ( $6-\mathrm{in}$.) base for Interstates, $225-\mathrm{mm}$ ( $9-\mathrm{in}$.) $\mathrm{PCC} / 100-\mathrm{mm}$ (4-in.) base for Parkways and $200-\mathrm{mm}$ ( $8-\mathrm{in}$.) PCC/ $100-\mathrm{mm}$ ( 4 -in.) base for other Primary
routes. Measurements of the extracted PCC cores and base thicknesses confirmed conformance to original design specifications.

The PCC compressive strengths and moduli of elasticity greatly exceeded design parameters for all projects. Obviously, this commonality would contribute in a positive manner to the superior performance of the pavements.

The moisture contents of the DGA bases were typical and therefore have no particular influence. However, the in-situ CBR values were very low and the minus $75 \mu \mathrm{~m}$ (No. 200 sieve) material values were very high; which would be expected to impact negatively to the superior performance of the pavements.

Subgrade moisture contents were quite high, in-situ CBR values low and unconfined compressive strengths low; which would contribute in a negative manner to the performance of the pavements. Present pavement designs would require subgrade modification prior to pavement construction for most of the sections evaluated.

Substantial mileage of the original PCC Interstate and Parkway designs is still performing satisfactorily. However, it is conceivable that if the design presently in use had been specified during the 1960s and 1970s, an even higher percentage of the original PCC pavements would be serving satisfactorily with minimum mileage requiring overlays or reconstruction except for geometric improvements. The designs in use today -- which presumably are superior to the designs for the 1960s and 1970s-have thicker PCC slabs, drainable bases, shorter joint spacings, skewed joints, and improved joint-filler materials. Also, certain mix design and production parameters have changed, such as improved screening of potentially reactive aggregates, acceptance of pozzolans and tighter standards on mix variations. It is logical to anticipate that the improved designs in common use today will provide a consistent 30 -year or longer pavement life, with the only maintenance consisting of joint resealing and diamond grinding to restore surface smoothness and ride quality.

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TABLE I. PCC Pavement Sections Selected for Study

| Route | County | Milepost | Date Constructed |
| :--- | :--- | :--- | :--- |
| Interstate 64 | Fayette | $82.32-89.48$ | $1963 / 87^{*}$ |
| Interstate 75 | Laurel | $40.70-46.95$ | $1969 / 84^{* * *}$ |
| Interstate 64 | Shelby | $38.18-43.33$ | $1961 / 84^{*}$ |
|  |  |  |  |
| Bluegrass Parkway | Nelson | $24.24-32.60$ | $1965 / 84^{* * *}$ |
| Western KY Parkway | Hopkins | $25.64-35.50$ | 1963 |
| Pennyrile Parkway | Hopkins/Christian | $22.48-29.91$ | $1968 / 93^{* * *}$ |
| Pennyrile Parkway | Hopkins | $45.00-53.11$ | 1968 |
| Green River Parkway | Ohio | $32.64-42.27$ | $1972 / 87^{* *}$ |
| Audubon Parkway | Daviess | $15.88-23.46$ | $1970 / 87^{* *}$ |
|  |  |  |  |
| US 127 | Owen | $16.96-24.69$ | 1973 |
| US 27 | Pulaski | $10.48-15.46$ | 1960 |
| US 119 | Pike | $24.81-29.75$ | 1982 |

*Edge Drains $\quad{ }^{* *}$ Edge Drains and Joint Seals $\quad{ }^{* * *}$ Edge Drains, PCC Repairs, and Joint Seals

TABLE II. Kentucky Interstate Highway System, Initial and Present Pavement Types

| KENTUCKY INTERSTATES - PAVEMENT TYPE (km [mi]) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Initially |  |  | Presently |  |  |  |
| Interstate | AC/DGA | FDAC | PCC | AC/DGA | AC/PCC | FDAC | PCC** |
| 1-24 | 71 [44] | 0 | 77 [48] | 71 [44] | 0 | 0 | 77 [48] |
| 1-64 | 109 [68] | 0 | 182 [113] | 109 [68] | 58 [36] | 0 | 124 [77] |
| 1-65 | 32 [20] | 3[2] | 183 [114] | 32 [20] | 58 [36] | 3 [2] | 126 [78] |
| 1-71 | 0 | 0 | 126 [78] | 0 | 126 [78] | 0 | 0 |
| 1-75 | 43 [27] | 0 | 264 [164] | 43 [27] | 159 [99] | 0 | 105 [65] |
| 1-264 | 3 [2] | 0 | 34 [21] | 0 | 5 [3] | 0 | 32 [20] |
| 1-265 | 0 | 0 | 40 [25] | 0 | 3 [2] | 0 | 37 [23] |
| 1-275 | 0 | 0 | 39 [24] | 0 | 0 | 0 | 39 [24] |
| 1-471 | 0 | 0 | 8 [5] | 0 | 0 | 0 | 8 [5] |
| Total km $\qquad$ | $\begin{gathered} 258 \\ {[161]} \\ \hline \end{gathered}$ | $\begin{gathered} 3 \\ {[2]} \end{gathered}$ | $\begin{gathered} 953 \\ {[592]} \end{gathered}$ | $\begin{gathered} 255 \\ {[159]} \end{gathered}$ | $\begin{gathered} 409 \\ {[254]} \end{gathered}$ | $\begin{gathered} 3 \\ {[2]} \end{gathered}$ | $\begin{gathered} 548 \\ {[340]} \\ \hline \end{gathered}$ |
| \% | 22\% | 0\% | 78\% | 21\% | 34\% | 0\% | 45\% |
| *Muitiply by $\approx 4.05$ to convert to lane kilometers [miles] <br> ${ }^{* *}$ Includes 37 km ( 23 mi ) [148 lane kilometers ( 92 lane miles)] of PCC Grinding Includes 183 km ( 114 mi ) [ 734 lane kilometers ( 456 lane miles)] of PCC Repairs |  |  |  |  |  | Prep | 1/94 |

TABLE III. Kentucky's Parkway Highway System, Initial and Present Pavement Types

| KENTUCKY PARKWAYS - PAVEMENT TYPE (km [mil]* |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Initially |  |  | Presently |  |  |  |
| Parkway | AC/DGA | FDAC | PCC | AC/DGA | AC/PCC | FDAC | PCC** |
| Mountain*** | 51 [32] | 0 | 69 [43] | 51 [32] | 63 [39] | 0 | 6 [4] |
| Western KY | 74 [46] | 0 | 146 [91] | 74 [46] | 68 [42] | 0 | 79 [49] |
| Bluegrass | 56 [35] | 0 | 56 [35] | 56 [35] | 23 [14] | 0 | 34 [21] |
| Pennyrile | 0 | 0 | 114 [71] | 0 | 26 [16] | 0 | 90 [56] |
| Aububon | 0 | 0 | 37 [23] | 0 | 0 | 0 | 37 [23] |
| Daniel Boone ${ }^{* * *}$ | 40 [25] | 16 [10] | 39 [24] | 40 [25] | 0 | 16 [10] | 39 [24] |
| Green River | 40 [25] | $11[7]$ | 61 [38] | 40 [25] | 0 | $11[7]$ | 61 [38] |
| Jackson Purchase | 84 [52] | 0 | 0 | 84 [52] | 0 | 0 | 0 |
| Cumberland | 56 [35] | 87 [54] | 0 | 56 [35] | 0 | 87 [54] | 0 |
| Total km <br> [mi] | $\begin{gathered} 401 \\ {[250]} \\ \hline \end{gathered}$ | $\begin{array}{r} 114 \\ {[71]} \\ \hline \end{array}$ | $\begin{gathered} 522 \\ {[325]} \\ \hline \end{gathered}$ | $\begin{aligned} & 401 \\ & {[250]} \end{aligned}$ | $\begin{gathered} 180 \\ {[111]} \end{gathered}$ | $\begin{aligned} & 114 \\ & {[71]} \end{aligned}$ | $\begin{gathered} 346 \\ {[215]} \\ \hline \end{gathered}$ |
| \% | 39\% | 11\% | 50\% | 39\% | 17\% | 11\% | 33\% |
| *Multiply miles by $\approx 3.9$ to convert to lane kilometers [miles] <br> **Includes 154 km [ 96 mi ( 618 lane kilometers [ 384 lane miles]) of PCC Repairs Prepared 1/94 <br> ***Portions are 2- and 3-lanes |  |  |  |  |  |  |  |

TABLE IV. Average Age (Years) of PCC Pavements at the Time of An Asphalt Overlay

| Route | Kilometers [Miles] | Average Age at Overlay (Years) |
| :---: | :---: | :---: |
| $\mathrm{l}-64$ | $58[36]$ | 21 |
| $\mathrm{l}-65$ | $58[36]$ | 21 |
| $\mathrm{I}-71$ | $126[78]$ | 15 |
| $\mathrm{I}-75$ | $159[99]$ | 22 |
| $\mathrm{I}-264$ | $5[3]$ | 21 |
| $\mathrm{I}-265$ | $3[2]$ | 30 |
| Average for Interstates |  | 19.6 years |
|  |  |  |
| MP | $63[39]$ | 26 |
| WKP | $68[42]$ | 26 |
| BGP | $22[14]$ | 21 |
| PRP | $26[16]$ | 22 |
| Average for Parkways |  | 24.6 Years |

TABLE V. Average Age (Years) of Original PCC Pavements Still in Service

| Route | Kilometers [Miles] | Average Age (Years) |
| :---: | :---: | :---: |
| $1-24^{*}$ | 77 [48] | 17 |
| 1-64 | 113 [70] | 25 |
| 1-65 | 72 [45] | 27 |
| 1-75 | 93 [58] | 27 |
| 1-264 | 13 [8] | 24 |
| 1-265* | 37 [23] | 12 |
| 1-275* | 32 [20] | 14 |
| 1-471* | 8 [5] | 14 |
| Average for Interstates |  | 22.2 years |
| MP | 6 [4] | 32 |
| WKP | 85 [53] | 31 |
| BGP | 34 [21] | 29 |
| PRP | 88 [55] | 27 |
| AUDP | 37 [23] | 24 |
| DBP | 39 [24] | 21 |
| GRP | 60 [37] | 22 |
| Average for Parkways |  | 26.4 Years |
| *More recent construction |  |  |

TABLE VI. General Comparison of the Design Details for PCC Pavements Used During the 1960s and 1970s and Those in Common Use Today

| Factor | 1960s \& 1970s | Currently |
| :---: | :---: | :---: |
| PCC Slab Thickness | 200 mm (8 in.) Primary (standard) 225 mm (9 in.) Parkway (standard) 250 mm (10 in.) Interstate (standard) | 250 mm to 325 mm (10 in. to 13 in .) (variable depending on traffic, etc.), 275 mm (11 in.) normal |
| Base Thickness | 100 mm (4 in.) Primary (standard) <br> 100 mm (4 in.) Parkway (standard) <br> 125 mm to 150 mm ( 5 in . to 6 in . Interstate (standard) | $200 \mathrm{~mm}(8 \mathrm{in}$.$) (consisting of 100-$ mm (4-in.) drainable base and 100 mm (4 in.) of DGA) |
| Base Material | Dense graded aggregate (high \% of fines) | Stabilized, drainable base on a DGA base (lower \% of fines) |
| Joint Spacing | 15.2 m ( 50 ft ) for limestone aggregate (most) <br> $7.6 \mathrm{~m}(25 \mathrm{ft})$ for gravel aggregate | Random (variable) spacing, averaging $4.6 \mathrm{~m}(15 \mathrm{ft})$ |
| Joint Pattern | $90^{\circ}$ | Skewed |
| Reinforcement | Welded wire fabric | None |
| Joint Filler | Hot-pour asphalt | Neoprene or Silicone |
| Joint Load Transfer | Dowel bars | Dowel bars |
| Mix Parameters | — | More screening for potentially active aggregate, fly ash permitted |
| Mix Production | - - | Tighter standards on mix variations |

Table VII. Pavement and Laboratory Test Results

| PROJECT IDENTIFICATION | $\begin{gathered} \text { AGE } \\ \text { AT } \\ \text { TEST } \\ \text { (YEARS) } \\ \hline \end{gathered}$ | PORTLAND CEMENT CONCRETE CORES |  |  | DENSE GRADED AGGREGATE* |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | AVERAGE THICKNESS (mm) [in.] | AVERAGE COMPRESSIVE STRENGTH (MPa) [psi] | AVERAGE MODULUS OF ELASTICITY (GPa) [psi x 10 ${ }^{6}$ ] | AVERAGE <br> THICKNESS (mm) [in.] | AVERAGE MOISTURE CONTENT (\%) | AVERAGE IN-SITU CBR | AVERAGE MINUS NO. 200 SIEVE SIZE (\%) |
| 1-64; FAYETTE | 32 | 250 [10.0] | 51.2 [7,430] | 35.0 [5.08] | 155 [6.2] | 6.1 | 20 | 10.6 |
| 1-75; LAUREL | 26 | 250 [10.0] | 40.0 [5,800] | 31.2 [4.52] | 135 [5.4] | 6.1 | 12 | 9.2 |
| 1-64; SHELBY | 34 | 250 [10.0] | 47.0 [6,810] | 31.2 [4.53] | 150 [6.0] | 6.2 | 16 | 10.4 |
| BGP/NELSON | 30 | 225 [9.0] | 57.2 [8,300] | 35.0 [5.08] | 105 [4.2] | 5.9 | 14 | 11.2 |
| WKP/HOPKINS | 32 | 230 [9.2] | 48.7 [7,060] | 32.2 [4.67] | 108 [4.3] | 7.9 | 9 | 12.7 |
| PRP/HOPKINS \& CHRISTIAN | 27 | 230 [9.2] | 48.7 [7,060] | 30.2 [4.38] | 88 [3.5] | 4.7 | 11 | 12.4 |
| PRP/HOPKINS | 27 | 225 [9.0] | 39.6 [5,750] | 28.1 [4.07] | 103 [4.1] | 5.7 | 12 | 12.3 |
| GRP/OHIO | 23 | 225 [9.0] | 45.4 [6,580] | 31.6 [4.58] | 103 [4.1] | 5.4 | 17 | 10.6 |
| AUP/DAVIESS | 25 | 225 [9.0] | 39.6 [5,740] | 25.7 [3.73] | 100 [4.0] | 5.8 | 16 | 17.0 |
| US127/OWEN | 23 | 205 [8.2] | 41.3 [ 5,990$]$ | 28.3 [4.10] | 88 [3.5] | 9.3 | 8 | 11.3 |
| US27/PULASKI | 35 | 188 [7.5] | 51.3 [7,440] | 33.4 [4.85] | 93 [3.7] | 8.1 | 9 | 12.1 |
| US119/PIKE | 13 | 230 [9.2] | 42.3 [ 6,140$]$ | 27.9 [4.05] | 98 [3.9] | 5.6 | 24 | 16.9 |
| RANGE | 13-34 | $\begin{array}{r} 188-250 \\ {[7.5-10.0]} \\ \hline \end{array}$ | $\begin{gathered} 39.6-57.2 \\ {[5,740-8,300]} \\ \hline \end{gathered}$ | $\begin{array}{r} 25.7-35.0 \\ {[3.73-5.08]} \\ \hline \end{array}$ | $\begin{array}{r} 88-155 \\ {[3.5-6.2]} \\ \hline \end{array}$ | 4.7-9.3 | 8-24 | $9.2-17.0$ |
| AVERAGE | 27 | 250 [10.0] Int. <br> 228 [9.1] Pkwy <br> 208 [8.3] US | 46.1 [6,680] | 30.8 [4.47] | 5.9 lnt . 4.0 Pkwy 3.7 US | 6.4 | $14(13)^{* *}$ | 12.2 |

[^0]Table VII (Continued)

| PROJECT IDENTIFICATION | SUBGRADE SAMPLES |  | SUBGRADE TUBE SAMPLES ( $0-175 \mathrm{~mm}$ ) [0 to 7 in .] |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AVERAGE MOISTURE CONTENT BELOW DGA (\%) | AVERAGE IN-SITU CBR | AVERAGE MOISTURE CONTENT (\%) | AVERAGE UNCONFINED STRENGTH (kPa) [psi] | AVERAGE WET DENSITY ( $\mathrm{kg} / \mathrm{m}^{3}$ ) [pcf] | $\qquad$ |
| I-64; FAYETTE | 24.8 | 2 | 23.2 | 240.6 [34.9] | 2,119 [132.3] | CL |
| 1-75; LAUREL | 15.5 | 3 | 15.1 | 157.2 [22.8] | 2,223 [138.8] | VARIABLE |
| 1-64; SHELBY | 22.8 | 3 | 23.4 | 156.5 [22.7] | 2,102 [131.2] | CL |
| BGP/NELSON | 23.6 | 2 | 22.2 | 161.3 [23.4] | 2,135 [133.3] | CL |
| WKP/HOPKINS | 21.1 | 4 | 16.2 | 131.0 [19.0] | 2,199 [137.3] | VARIABLE |
| PRP/HOPKINS \& CHRISTIAN | 14.8 | 4 | 18.3 | 233.0 [33.8] | 2,191 [136.8] | CL |
| PRP/HOPKINS | 15.2 | 6 | 15.0 | 248.2 [36.0] | 2,211 [138.0] | CL |
| GRP/OHIO | 13.8 | 7 | 11.4 | 200.6 [29.1] | 2,223 [138.8] | VARIABLE |
| AUP/DAVIESS | 14.5 | 9 | 13.3 | 279.9 [40.6] | 2,182 [136.2] | CL |
| US127/OWEN | 24.6 | 2 | 22.6 | 92.4 [13.4] | 2,138 [133.5] | CL |
| US27/PULASKI | 26.3 | 2 | 28.0 | 128.9 [18.7] | 1,978 [123.5] | CH |
| US119/PIKE | 8.1 | 13 | 9.8 | NA | NA | SM-SC |
| RANGE | 8.1-26.3 | 2-13 | 9.8-28.0 | $\begin{array}{r} 92.4-279.9 \\ {[13.4-40.6]} \\ \hline \end{array}$ | $\begin{gathered} 1,978-2,223 \\ {[123.5-138.8]} \\ \hline \end{gathered}$ |  |
| AVERAGE | 18.8 (19.7)** | $4.8(4.0)^{* *}$ | $18.2(19.0)^{* *}$ | 184.1 [26.7] | 2,154 [134.5] |  |

${ }^{*}$ All base samples were non-plastic $\quad{ }^{* *}$ Excluding sandstone base project

## APPENDIX A

## PAVEMENT TYPES FOR EACH SECTION OF EACH INTERSTATE HIGHWAY IN KENTUCKY AS OF DECEMBER 1993

| INTERSTATE -24-PAVEMENT TYPE |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Initially |  |  | Presently |  |  |  |
|  |  |  | AC | FDAC | PCC | ACIDGA | AC/PCC | FDAC | PCC |
| County | Mileposts | Dates | km [mi] | km [mij] | kmi [mi] | km [mi] | km [mi] | km [mi] | km [mi] |
| McCracken | 1.00-4.33 | 74/89 | 5.36 [3.33] |  |  | 5.36 [3.33] |  |  |  |
| * | $4.33-10.32$ | 78/90 | 9.64 [5.99] |  |  | 9.64 [5.99] |  |  |  |
| " | 10.32-13.80 | 78/90 | 5.60 [3.48] |  |  | 5.60 [3.48] |  |  |  |
| n | 13.80-16.16 | 78/90 | 3.80 [2.36] |  |  | 3.80 [2.36] |  |  |  |
| McGracken/Marshall | 16.60-22.04 | 77/85/93 | $9.46 \mathrm{~EB}[5.88]$ |  |  | 9.46 [5.88EB] |  |  |  |
| " | 16.60-22.04 | 77/83/93 | $9.46 \mathrm{WB}[5.88]$ |  |  | 9.46WB [5.88] |  |  |  |
| Marshall | 22.04-26.56 | $77 / 86$ | 7.27 [4.52] |  |  | 7.27 [4.52] |  |  |  |
| " | 26.56-27.55 | 79/90/93 | 1.59 [0.99] |  |  | $1.59[0.99]$ |  |  |  |
| " | 27.55-29.14 | 79/90/93 | 2.56 [1.59] |  |  | 2.56 [1.59] |  |  |  |
| Livingston | 29.54-30.55 | 79/90/93 | 1.63 [1.01] |  |  | 1.63 [1.01] |  |  |  |
| " | 30.55-33.88 | 80/91 | 5.36 [3.33] |  |  | 5.36 [3.33] |  |  |  |
| Lyon | 33.88-39.51 | 79/87 | 9.06 [5.63] |  |  | 9.06 [5.63] |  |  |  |
| " | 39.51-41.60 | 80/87 | 3.36 [2.09] |  |  | 3.36 [2.09] |  |  |  |
| " | 41.60-45.20 | 80:87 | 5.79 [3.60] |  |  | 5.79 [3.60] |  |  |  |
| Lyon-Caldwell | 45.20-55.63 | 80 |  |  | 16.78 [10.43] |  |  |  | 16.78 [10.43] |
| Caldwell-Trigg | 55.63-65.35 | $80^{*}$ |  |  | 15.64 [9.72] |  |  |  | 15.64 [9.72] |
| Trigg-Christian | 65.35-76.07 | 75/85** |  |  | 17.25 [10.72] |  |  |  | 17.25 [10.72] |
| Christian | 76.07-85.56 | 75/85** |  |  | 15.27 [9.49] |  |  |  | 15.27 [9.49] |
| " | 85.56-93.30 | 75/85** |  |  | 12.45 [7.74] |  |  |  | 12.45 [7.74] |
| Totals |  |  | $\begin{aligned} & 70.47 \\ & {[43.80]} \end{aligned}$ | 0 | $\begin{aligned} & 77.39 \\ & {[48.10]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 70.47 \\ & {[43.80]} \\ & \hline \end{aligned}$ | -0 | 0 | $\begin{gathered} 77.39 \\ {[48.10]} \\ \hline \end{gathered}$ |
| ${ }^{*}$ Edge Drains <br> ${ }^{* * E d g e}$ Drains, PCC Repairs, Joint Seals |  |  |  |  |  |  |  |  |  |


| INTERSTATE 1-64-PAVEMENT TYPE |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | initially |  |  | Presently |  |  |  |
|  |  |  | ACIDGA | FDAC | PCC | ACIDGA | ACPPCC | FDAC | PCG |
| County | Mileposts | Dates | km [mi] | km [mi] | km [mi] | km [mi] | km [mi] | km [mi] | km [mi] |
| Jefferson | 0.72-1.34 | 69/88*/94 |  |  | $1.00[0.62]$ |  |  |  | 1.00 [0.62] |
| * | 1.97-2.06 | 70182194 |  |  | $0.14[0.09]$ |  |  |  | 0.14 [0.09] |
| " | 2.25-3.26 | 71/88*/94 |  |  | 1.63 [1.01] |  |  |  | 1.63 [1.01] |
| * | 4.95-5.50 | 70/85 |  |  | 0.88 [0.55] |  | 0.88 [0.55] |  |  |
| " | 5.50-6.45 | 70/84BS ${ }^{*}$ |  |  | 1.53 [0.95] |  | 1.53 [0.95] |  |  |
| " | 6.45-8.20 | 68/848S ${ }^{*}$ |  |  | 2.82 [1.75] |  | 2.82 [1.75] |  |  |
| " | 8.20-9.46 | 70 |  |  | 2.03 [1.26] |  |  |  | 2.03 [1.26] |
| " | 9.46-12.58 | 69 |  |  | 5.02 [3.12] |  |  |  | 5.02 [3.12] |
| " | 12.58-14.89 | 64/89BS/94 |  |  | 3.12 [2.31] |  |  |  | 3.12 [2.31] |
| " | 14.89-18.86 | 64/88BS |  |  | 6.39 [3.97] |  | 6.39 [3.97] |  |  |
| Jefterson/Shelby | 18.86-25.09 | 61/84BS ${ }^{*}$ |  |  | 10.02[6.23] |  | 10.02 [6.23] |  |  |
| Sheiby | 25.09-31.84 | 61/84BS* |  |  | 10.86 [6.75] |  | 10.86 [6.75] |  |  |
| " | 31.84-38.18 | $62 / 84 \mathrm{BS}^{*}$ |  |  | 10.20 [6.34] |  | 10.20 [6.34] |  |  |
| . ${ }^{\circ}$ | 38.18-43.33 | $61 / 84^{*}$ |  |  | 8.29 [5.15] |  |  |  | 8.29 [5.15] |
| Shelby-Franklin | 43.33-47.76 | 62/80/88 |  |  | 7.13 [4.43] |  | 7.13 [4.43] |  |  |
| Franklin | 47.76-53.12 | 62180188 |  |  | 8.62 [ 5.36$]$ |  | 8.62 [5.36] |  |  |
| " | 53.12-57.90 | 62/88** |  |  | 6.76 [4.20] |  |  |  | 6.76 [4.20] |
| Franklin-Woodiord | 57.90-65.27 | 72/91* |  |  | $11.86[7.37]$ |  |  |  | $11.86[7.37]$ |
| Woodford-Scott | 65.27-68.55 | 73/91* |  |  | 5.28 [3.28] |  |  |  | 5.28 [3.28] |
| Scott-Fayette | 68.55-75.20 | 73/91* |  |  | $10.70[6.65]$ |  |  |  | $10.70[6.65]$ |
| $1-64$ combines with $1-75$ for approximately $9.25 \mathrm{~km}(5.75 \mathrm{ml})$ in Fayette County |  |  |  |  |  |  |  |  |  |
| Fayelte | 80.95-82.32 | $81^{*}$ |  |  | 2.20 [1.37] |  |  |  | 2.20 [1.37] |
| $\pi$ | 82.32-89.48 | $63 / 87^{*}$ |  |  | $11.16[7.16]$ |  |  |  | 11.16[7.16] |
| Clark | 89.48-94.23 | $63 / 3 / 84$ | 7.64 [4.75] |  |  | 7.64 [4.75] |  |  |  |
| * | 94.23-101.74 | $61 / 73 / 84$ | 12.08 [7.51] |  |  | 12.08 [7.51] |  |  |  |
| " | 101.74-104.26 | 61/73/84 | 4.05 [2.52] |  |  | 4.05 [2.52] |  |  |  |
| Montgomery | 104.26-172.30 | $6173 / 84$ | 12.94 [8.04] |  |  | 12.94 [8.04] |  |  |  |
| Montgomerry-Bath | 112.30-123.02 | 68/84** |  |  | 16.60[10.32] |  |  |  | 16.60 [10.32] |
| Bath | 123.02-128.96 | 68/84** |  |  | 9.56 [5.94] |  |  |  | 9.56 [5.94] |
| Howan | 128.96-137.28 | 68/84** |  |  | 13.39 [8.32] |  |  |  | 13.39 [8.32] |
| " | 137.28-146.10 | 69/84** |  |  | 14.19 [8.82] |  |  |  | 14.19 [8.82] |
| Rowan-Carter | 146.10-154.22 | 69/82 | 13.07 [8.12] |  |  | 13.07 [8.12] |  |  |  |
| Carter | 154.22-161.45 | $69 / 82$ | 11.63 [7.23] |  |  | 11.63 [7.23] |  |  |  |
| " | 161.45-168.50 | 68/82 | 11.34 [7.05] |  |  | 11.34 [7.05] |  |  |  |
| " | 168.50-171.61 | $69 / 82$ | 5.00 [3.11] |  |  | 5.00 [3.11] |  |  |  |
| * | 171.61-180.81 | $73 / 82$ | $14.80[9.20]$ |  |  | 14.80[9.20] |  |  |  |
| Boyd | 180.81-185.47 | 64/81/90 | 7.50 [4.66] |  |  | $\begin{gathered} 7.50[4.66] \\ \text { SAMI } \\ \hline \end{gathered}$ |  |  |  |
| " | 185.47-191.30 | 64/81/90 | 9.38 [5.83] |  |  | $\begin{gathered} 9.38[5.83] \\ \text { SAMI } \end{gathered}$ |  |  |  |
|  | Totals |  | $\begin{aligned} & 109.44 \\ & {[68.02]} \end{aligned}$ | 0 | $\begin{gathered} 182.32 \\ {[113.31]} \\ \hline \end{gathered}$ | $\begin{aligned} & 109.44 \\ & {[68.02]} \\ & \hline \end{aligned}$ | $\begin{gathered} 58.44 \\ {[36.32]} \\ \hline \end{gathered}$ | 0 | $\begin{aligned} & 123.88 \\ & {[76.99]} \\ & \hline \end{aligned}$ |
| *Edge Drains <br> *Edge Drains, PCC Repairs, Joint Seals |  |  |  |  |  |  |  |  |  |


| INTERSTATE I-65 - PAVEMENT TYPE |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Intitally |  |  | Presently |  |  |  |
|  |  |  | ACIDGA | FDAC | PCC | ACIDGA | AC/PCC | FDAC | PCC |
| County | Mileposts | Dates | km [mi] | km [mi] | kmimi] | km [mi] | km [mi] | km [mil] | km [mi] |
| Simpson | 0.00-1.98 | 69/87* |  |  | 3.19 [1.98] |  |  |  | 3.19 [1.98] |
| " | 1.98-12.81 | 65/87 ${ }^{\text { }}$ |  |  | 17.43 [10.83] |  |  |  | 17.43[10.83] |
| Simpson-Warren | 12.81-22.35 | 65/82 |  |  | 15.35 [9.54] |  | 15.35 [9.54] |  |  |
| Warren | 22.35-28.01 | 66/87* |  |  | $9.11[5.66]$ |  |  |  | $9.11[5.66]$ |
| n | 28.01-33.00 | 661/87* |  |  | 8.03 [4.99] |  |  |  | 8.03 [4.99] |
| " | 33.00-35.56 | 66/87* |  |  | 4.12 [2.56] |  |  |  | 4.12 [2.56] |
| * | 35.56-42.61 | $69187^{*}$ |  |  | 11.34 [7.05] |  |  |  | 11.34 [7.05] |
| Warren/Edmonson/Barren | 42.61-46.88 | 69/87* |  |  | 6.87 [4.27] |  |  |  | 6.87 [4.27] |
| Barren | 46.88-51.90 | 68/87* |  |  | 8.08 [5.02] |  |  |  | 8.08 [5.02] |
| Barren-Hart | 51.90-58.20 | 68/88BS |  |  | 10.14 [6.30] |  | 10.14 [6.30] |  |  |
| Hart | 58.20-61.20 | $67 / 87^{*}$ |  |  | 4.83 [3.00] |  |  |  | 4.83 [3.00] |
| " | 61.20-64.15 | $67 / 84$ | 4.75 [2.95] |  |  | 4.75 [2.95] |  |  |  |
| " | 64.15-70.41 | 65/84 | 10.07 [6.26] |  |  | 10.07 [6.26] |  |  |  |
| Hart-Larue | 70.41-76.10 | $65 / 84$ | $9.16[5.69]$ |  |  | 9.16 [5.69] |  |  |  |
| Larue | 76.10-78.66 | 63/84*BS |  |  | 4.12 [2.56] |  | 4.12[2.56] |  |  |
| Hardin | 78.66-85.58 | 59/84*BS |  |  | 11.13 [6.92] |  | 11.13 [6.92] |  |  |
| * | 85.58-90.58 | 59/84*BS |  |  | 8.05 [5.00] |  | 8.05 [5.00] |  |  |
| " | 90.58-93.69 | 85/86 | 5.00 [3.11] |  |  | 5.00 [3.11] |  |  |  |
| " | 93.69-95.12 | $84 / 86$ | 2.30 [1.43] |  |  | $2.30[1.43]$ |  |  |  |
| * | 95.12-97.58 | 83/86/93 |  | 3.96 [2.46] |  |  |  | 3.96 [2.46] |  |
| " | 97.58-101.98 | 83/86G |  |  | 7.08 [4.40] |  |  |  | 7.08 [4.40] |
| Hardin-Bullitt | 101.98-103.57 | 85 |  |  | 2.56 [1.59] |  |  |  | 256 [1.59] |
| Bullitt | 103.57-105.18 | 85 |  |  | 2.59 [1.61] |  |  |  | 2.59 [1.61] |
| * | 105.18-107.26 | 85 |  |  | 3.35 [2.08] |  |  |  | 3.35 [2.08] |
| n | 107.26-110.71 | 87 |  |  | 5.55 [3.45] |  |  |  | 5.55 [3.45] |
| " | 110.7t-115.82 | 87 |  |  | 8.22 [5.11] |  |  |  | 8.22 [5.11] |
| . | 115.82-118.68 | 86 |  |  | 4.60 [2.86] |  |  |  | 4.60 [2.86] |
| " | 118.68-121.38 | 86 |  |  | 4.34 [2.70] |  |  |  | 4.34 [2.70] |
| " | 121.38-123.18 | 86 |  |  | $2.90[1.80]$ |  |  |  | $2.90[1.80]$ |
| Jefferson | 123.18-126.12 | 87 |  |  | 4.73 [2.94] |  |  |  | 4.73 [2.94] |
| " | 126.12-127.57 | 87 |  |  | 2.33 [1.45] |  |  |  | 2.33 [1.45] |
| Jefferson | 127.57-128.13 | 89 | 0.80 [0.56] |  |  | $0.90[0.56]$ |  |  |  |
| " | 128.13-128.84 | 89 |  |  | 1.14 [0.74] |  |  |  | 1.14 [0.71] |
| " | 128.84-131.37 | 88 |  |  | 4.07 [2.53] |  |  |  | 4.07 [2.53] |
| * | 131.37-136.72 | 71/81/86 |  |  | 8.61 [5.35] |  | 8.61 [5.35] |  |  |
|  | Totals |  | $\begin{array}{r} 31.18 \\ {[20.00]} \\ \hline \end{array}$ | $\begin{gathered} 3.96 \\ {[2.46]} \\ \hline \end{gathered}$ | $\begin{gathered} 183.84 \\ {[114.26]} \\ \hline \end{gathered}$ | $\begin{gathered} 32.18 \\ {[20.00]} \\ \hline \end{gathered}$ | $\begin{gathered} 57.39 \\ {[35.67]} \\ \hline \end{gathered}$ | $\begin{gathered} 3.96 \\ {[2.46]} \\ \hline \end{gathered}$ | $\begin{aligned} & 126.45 \\ & {[78.59]} \\ & \hline \end{aligned}$ |
| ${ }^{*}$ Edge Drains <br> Note: New alignment Sta 90.58-131.37 |  |  |  |  |  |  |  |  |  |


| INTERSTATE 1-71-PAVEMENT TYPE |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Initially |  | Presently |  |  |
|  |  |  | AC/DGA | PCC | AC/DGA | AC/PCC | PCC |
| County | Mileposts | Dates | km [mi] | km [mi] | km [mi] | km [mi] | km [mi] |
| Jefferson | 0.08-1.75 | 67/88BS* |  | 2.69 [1.67] |  | 2.69 [1.67] |  |
| " | 1.75-5.55 | 68/88BS* |  | 6.12 [3.80] |  | 6.12 [3.80] |  |
| " | 5.55-9.06 | 68/84BS* |  | 5.65 [3.51] |  | 5.65 [3.54] |  |
| Jefferson-Oldham | 9.06-21.38 | 69/84BS* |  | 20.10 [12.49] |  | 20.10 [12.49] |  |
| Oldham-Henry | 21.38-27.71 | 69/84BS* |  | 10.19 [6.33] |  | 10.19 [6.33] |  |
| Henry | 27.71-37.18 | 69/84BS** |  | 15.24 [9.47] |  | 15.24 [9.47] |  |
| Henry-Trimble-Carroll | 37.18-44.08 | 68/82 |  | 11.10[6.90]** |  | 11.10 [6.90] |  |
| Carroll-Gallatin | 44.08-56.67 | 68/84BS* |  | 20.26 [12.59] |  | 20.26 [12.59] |  |
| Gallatin | 56.67-61.77 | 68/82BS*** |  | 8.21 [5.10] |  | 8.21 [5.10] |  |
| " | 61.77-69.89 | 68/82BS |  | 13.07 [8.12] |  | 13.07 [8.12] |  |
| Boone | 69.89-77.72 | 68/84BS* |  | 12.60 [7.83] |  | 12.60 [7.83] |  |
|  | Totals |  | 0 | $\begin{aligned} & 125.22 \\ & {[77.81]} \end{aligned}$ | 0 | 125.22 [77.81] | 0 |
| *Edge Drains <br> **GRCP <br> ***Research Test Section, Different Size Breaks |  |  |  |  |  |  |  |


| INTERSTATE 1-75-PAVEMAENT TYPE |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Initially |  | Presentiy |  |  |
|  |  |  | AC/DGA | PCC | AC/DGA | AC/PCC | PCC |
| County | Mileposts | Dates | km [mi] | km [mi] | $\mathrm{k}[\mathrm{n}$ [mi] | km [mi] | km [mi] |
| Whitley | 0.00-0.48 | 62/84 |  | 0.77 [0.48NB] |  | 0.77 [0.48NB] |  |
| " | 0.00-0.48 | 62/84** |  | 0.77 [0.48SB] |  |  | 0.77 [0.48SB] |
| " | 0.48-3.68 | 62/84** |  | 5.15 [3.20] |  |  | 5.15 [3.20] |
| " | 3.68-10.55 | 65/84** |  | 11.06 [6.87] |  |  | 11.06 [6.87] |
| " | 10.55-15.46 | 66/84** |  | 7.90 [4.91] |  |  | 7.90 [4.91] |
| " | 15.46-20.20 | 68/84** |  | 7.63 [4.74] |  |  | 7.63 [4.74] |
| " | 20.20-21.88 | 68/84*/91BS |  | 2.70 [1.68] |  | 2.70 [1.68NB] |  |
| " | 21.88-23.38 | 68/84S* |  | 2.41 [1.50] |  | 2.41 [1.50NB] |  |
| " | 23.38-24.66 | 68/86BS* |  | 2.06 [1.28] |  | 2.06 [1.28NB] |  |
| " | 20.20-24.66 | 68/84** |  | 7.18 [4.46SB] |  |  | 7.18 [4.46SB] |
| Whitley-Laurel | 24.66-28.85 | 68/84** |  | 6.74 [4.19] |  |  | 6.74 [4.19] |
| Laurel | 28.85-34.40 | 69/84**/91G |  | 8.93 [5.55] |  |  | 8.93 [5.55G] |
| " | 34.40-40.70 | 69/84**/91G |  | 10.14 [6.30] | . |  | 10.14 [6.30G] |
| " | 40.70-46.95 | 69/84** |  | 10.06 [6.25] |  |  | 10.06 [6.25] |
| " | 46.95-48.95 | 69/84** |  | 3.22 [2.00] |  |  | 3.22 [2.00] |
| " | 48.95-50.77 | 69/84 |  | 2.93 [1.82] |  | 2.93 [1.82] |  |
| Rockcastle | 50.77-55.80 | 69/78/90 | 8.10 [5.03] |  | 8.10 [5.03] |  |  |
| " | 55.80-58.95 | 69/78/90 | 5.07 [3.15] |  | 5.07 [3.15] |  |  |
| " | 58.95-62.01 | 68/78/90 | 4.92 [3.06] |  | 4.92 [3.06] |  |  |
| " | 62.01-65.22 | 68/78/90 | 5.17 [3.21] |  | 5.17 [3.21] |  |  |
| " | 65.22-68.31 | 68/88BS* |  | 4.97 [3.09] |  | 4.97 [3.09] |  |
| " | 68.31-70.20 | 67/88BS* |  | 3.04 [1.89] |  | 3.04 [1.89] |  |
| RockcastleMadison | 70.20-75.52 | 67/88BS* |  | 8.56 [5.32] |  | 8.56 [5.32] |  |
| Madison | 75.52-77.00 | 66/88BS* |  | 2.38 [1.48] |  | 2.38 [1.48] |  |
| " | 77.00-84.66 | 66/89BS* |  | 12.33 [7.66] |  | 12.33 [7.66] |  |
| " | 84.66-87.32 | 66/89BS* |  | 4.28 [2.66] |  | 4.28 [2.66] |  |
| " | 87.32-89.80 | 64/72/84 | 3.99 [2.48] |  | 3.99 [2.48] |  |  |
| " | 89.80-97.54 | 62/72/84 | 12.46 [7.74] |  | 12.46 [7.74] |  |  |
| Fayette | 97.54-100.32 | 63/72/84 | 4.47 [2.78] |  | 4.47 [2.78] |  |  |
| " | 100.32-103.89 | 63/89* |  | 5.75 [3.57] |  |  | 5.75 [3.57] |
| " | 103.89-110.25 | 64/89* |  | 10.24 [6.36] |  |  | 10.24 [6.36] |
| Fayette | 110.25-111.82 | $81^{* / 94}$ |  | 2.53 [1.57] |  |  | 2.53 [1.57] |
| " | 111.82-117.80 | 64/81 |  | 9.62 [5.98] |  | 9.62 [5.98] |  |
| Fayette-Scott | 117.80-122.29 | 63/86*/92BS |  | 7.23 [4.49] |  | 7.23 [4.49] |  |
| Scott | 122.29-126.83 | 63/86*/92BS |  | 7.31 [4.54] |  | 7.31 [4.54] |  |
| " | 126.83-130.25 | 62/86*/93BS |  | 5.50 [3.42] |  | 5.50 [3.42] |  |
| " | 130.25-134.08 | 62/86*/93BS |  | $6.16[3.83]$ |  | 6.16 [3.83] |  |
| " | 134.08-136.47 | 62/86*/94BS |  | $3.85[2.39]$ |  | 3.85 [2.39] |  |
| " | 136.47-138.00 | 63/86*/94BS |  | 2.46 [1.53] |  | 2.46 [1:53] |  |
| " | 138.00-143.24 | 63/84*BS |  | 8.43 [5.24] |  | 8.43 [5.24] |  |
| Grant | 143.24-154.47 | 63/84*BS |  | 18.07[11.23] |  | 18.07 [11.23] |  |


| " | 154.47-158.54 | 62/85*BS |  | 6.55 [4.07] |  | 6.55 [4.07] |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| " | 158.54-165.79 | $61 / 85 * B S$ |  | 11.67 [7.25] |  | 11.67 [7.25] |  |
| Grant-KentonBoone | 165.79-173.50 | 61/78/85*BS |  | 12.41 [7.71] |  | 12.41 [7.71] |  |
| Boone | 173.50-179.20 | 61/78/86/ 93*BS |  | 9.17 [5.70] |  | 9.17 [5.70] |  |
| * | 179.20-180.00 | 61/78/86/89 |  | 1.29 [0.80] |  | $1.29[0.80]$ |  |
| " | 180.00-182.46 | 61/80/86BS/89 |  | 3.96 [2.46] |  | 3.96 [2.46] |  |
| " | 182.46-183.18 | 62/80/85/93 |  | 1.16 [0.72] |  | 1.16 [0.72] |  |
| Boone-Kenton | 183.18-184.72 | 78 |  | 2.48 [1.54] |  |  | 2.48 [1.54] |
| Kenton | 184.72-187.95 | 62/76/80/90/93 |  | 5.20 [3.23] |  | 5.20 [3.23] |  |
| " | 187.95-191.20 | $\begin{array}{\|c\|} \hline 90 \\ \text { (Temporary)*** } \\ \hline \end{array}$ |  | 5.23 [3.25] |  |  | 5.23 [3.25] |
|  | Totals |  | $\begin{array}{r} 44.18 \\ {[27.45]} \\ \hline \end{array}$ | $\begin{gathered} 263.19 \\ {[163.54]} \end{gathered}$ | $\begin{gathered} 44.18 \\ {[27.45]} \end{gathered}$ | $\begin{aligned} & 159.31 \\ & {[98.99]} \\ & \hline \end{aligned}$ | $\begin{aligned} & 104.22 \\ & {[64.76]} \end{aligned}$ |
| *Edge Drains <br> **Edge Drains, PCC Repairs, Joint Seals <br> ***Presently being rebuilt with PCC on new alignment |  |  |  |  |  |  |  |


| INTERSTATE I-264 - PAVEMENT TYPE |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Initially |  |  | Presently |  |  |  |
|  |  |  | AC/DGA | FDAC | PCC | AC/DGA | AC/PCC | FDAC | PCC |
| County | Milaposts | Dates | km [mi] | km [mi] | km [mi] | km [mi] | km [mi] | km [mi] | km [mi] |
| Jefferson | 0.00-0.48 | 68/88*/94** |  |  | 0.77 [0.48] |  |  |  | 0.77 [0.48] |
| " | 0.48-1.89 | 68/87* |  |  | 2.27 [1.41] |  |  |  | 2.27 [1.41] |
| " | 1.89-2.86 | 70/87* |  |  | 1.58 [0.97] |  |  |  | 1.58 [0.97] |
| " | 2.86-3.78 | 70/87* |  |  | 1.48 [0.92] |  |  |  | 1.48 [0.92] |
| " | 3.78-4.54 | 70/87* |  |  | 1.22 [0.76] |  |  |  | 1.22 [0.76] |
| " | 4.54-5.96 | 70/87* |  |  | 2.29 [1.42] |  |  |  | 2.29 [1.42] |
| " | 5.96-7.18 | 71/87* |  |  | 1.96 [1.22] |  |  |  | 1.96 [1.22] |
| " | 7.18-8.03 | 73/87* |  |  | 1.37 [0.85] |  |  |  | 1.37 [0.85] |
| " | 8.03-9.23 | /90** |  |  | 1.93 [1.20] |  |  |  | 1.93 [1.20] |
| " | 9.23-10.15 | $190 * *$ |  |  | 1.48 [0.92] |  |  |  | 1.48 [0.92] |
| " | 10.15-12.68 | $190^{* *}$ |  |  | 4.07 [2.53] |  |  |  | 4.07 [2.53] |
| " | 12.68-14.20 | /93** |  |  | 2.45 [1.52] |  |  |  | 2.45 [1.52] |
| " | 14.20-18.40 | /93** |  |  | $6.80[4.20]^{* * *}$ |  |  |  | $6.80[4.20]^{* * *}$ |
| " | 18.40-20.13 | 194** | 2.78 [1.73] |  |  |  |  |  | 2.78 [1.73] |
| " | 20.13-21.93 | $61 / 83^{*} \mathrm{BS}$ |  |  | 2.90 [1.80] |  | 2.90 [1.80] |  |  |
| " | 21.93-22.65 | 68/83*BS |  |  | 1.16 [0.72] |  | 1.16 [0.72] |  |  |
| " | 22.65-23.24 | 68/88*BS |  |  | $0.95[0.59]$ |  | 0.95 [0.59] |  |  |
|  | Totals |  | $\begin{gathered} 2.78 \\ {[1.73]} \\ \hline 1 \end{gathered}$ | 0 | $\begin{gathered} 34.62 \\ {[21.51]} \end{gathered}$ |  | $\begin{gathered} 5.01 \\ {[3.11]} \end{gathered}$ | 0 | $\begin{gathered} 32.40 \\ {[20.13]} \\ \hline \end{gathered}$ |
| *Edge Drains <br> **Replaced with PCC |  |  |  |  |  |  |  |  |  |


| INTERSTATE 1-265-PAVEMENT TYPE |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Initially |  |  | Presently |  |  |  |
|  |  |  | AC/DGA | FDAC | PCC | AC/DGA | AC/PCC | FDAC | PCC |
| County | Mileposts | Dates | km [mi] | km [mi] | km [mi] | km [mi] | km [mi] | km [mi] | km [mi] |
| Jefferson | 10.25-11.46 | 85 |  |  | 1.95 [1.21] |  |  |  | 1.95 [1.21] |
| " | 11.46-13.92 | 86 |  |  | 3.96 [2.46] |  |  |  | 3.96 [2.46] |
| " | 13.92-15.66 | 87 |  |  | 2.80 [1.74] |  |  |  | 2.80 [1.74] |
| " | 15.66-18.80 | 87 |  |  | 5.05 [3.14] |  |  |  | 5.05 [3.14] |
| ${ }^{\prime}$ | 18.80-23.26 | 87 |  |  | 7.18 [4.46] |  |  |  | 7.18 [4.46] |
| " | 23.26-25.35 | 69 |  |  | 3.36 [2.09] |  |  |  | 3.36 [2.09] |
| " | 25.35-26.84 | 61/91 |  |  | 2.40 [1.49] |  | 2.40 [1.49] |  |  |
| " | 26.84-29.83 | 84 |  |  | 4.81 [2.99] |  |  |  | 4.81 [2.99] |
| " | 29.83-32.66 | 78 |  |  | 4.55 [2.83] |  |  |  | 4.55 [2.83] |
| " | 32.66-34.73 | 70 |  |  | 3.33 [2.07] |  |  |  | 3.33 [2.07] |
|  | Totals |  | 0 | 0 | $\begin{gathered} 39.40 \\ {[24.48]} \end{gathered}$ | 0 | $\begin{gathered} 2.40 \\ {[1.49]} \end{gathered}$ | 0 | $\begin{gathered} 37.00 \\ {[22.99]} \end{gathered}$ |


| INTERSTATE I-275 - PAVEMENT TYPE |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Initially |  |  | Presently |  |  |  |
|  |  |  | AC/DGA | FDAC | PCC | AC/DGA | AC/PCC | FDAC | PCC |
| County | Mileposts | Dates | km [mi] | km [mi] | km [mi] | km [mi] | km [mi] | km [mi] | km [mi] |
| Kenton | 0.00-1.09 | 77/93 |  |  | 1.75 [1.09]* |  |  |  | 1.75 [1.09]* |
| Kenton-Boone | 1.09-4.06 | 73/91*** |  |  | 4.78 [2.97]*WB |  |  |  | 4.78 [2.97] ${ }^{\text {W }} \mathrm{WB}$ |
| " | 1.09-4.06 | 77 |  |  | 4.78 [2.97] [EB |  |  |  | 4.78 [2.97] EB |
| Boone | 4.06-7.15 | 77 |  |  | 4.97 [3.09] |  |  |  | 4.97 [3.09] |
| " | 7.15-13.50 | 77 |  |  | 10.21 [6.35] |  |  |  | 10.21 [6.35] |
| Campbell | 73.55-75.39 | 80/91 $\mathrm{G}^{* * * *}$ |  |  | 2.96 [1.84] |  |  |  | 2.96 [1.84] |
| " | 75.39-77.22 | 80 |  |  | 2.95 [1.83] |  |  |  | 2.95 [1.83] |
| Campbell-Kenton | 77.22-78.76 | 76 |  |  | 2.48 [1.54] |  |  |  | 2.48 [1.54] |
| Kenton | 78.76-79.80 | 77 |  |  | 1.67 [1.04] |  |  |  | 1.67 [1.04] |
| " | 79.80-82.48 | 77 |  |  | 4.31 [2.68] |  |  |  | 4.31 [2.68] |
| " | 82.48-83.58 | 76/94 |  |  | 1.77 [1.10] |  |  |  | 1.77 [1.10] |
| " | 83.58-83.78 | 77/94 |  |  | 0.32 [0.20]* |  |  |  | $0.32[0.20]^{*}$ |
|  | Totals |  | 0 | 0 | $\begin{gathered} 38.19 \\ {[23.73]} \\ \hline \end{gathered}$ | 0 | 0 | 0 | $\begin{array}{r} 38.19 \\ {[23.73]} \\ \hline \end{array}$ |
| *CRCP <br> **PCC Reconstructed <br> ***With Drainage Layer <br> ****With Repairs and Joint Seals |  |  |  |  |  |  |  |  |  |


| INTERSTATE 1-471 - PAVEMENT TYPE |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Initially |  |  | Presently |  |  |  |
|  |  |  | AC/DGA | FDAC | PCC | AC/DGA | AC/PCC | FDAC | PCC |
| County | Mileposts | Dates | km [mi] | km [mi] | km [mi] | km [mi] | km [mi] | km [mi] | km [mi] |
| Campbell | 0.00-1.75 | 80/92G* |  |  | 2.82 [1.75] |  |  |  | 2.82 [1.75]G |
| " | 1.75-3.23 | 80/92G* |  |  | 2.38 [1.48] |  |  |  | 2.38 [1.48]G |
| " | 3.23-4.55 | 81/92G* |  |  | 2.12[1.32] |  |  |  | 2.12 [1.32]G |
| " | 4.55-4.75 | 81 |  |  | 0.32 [0.20] |  |  |  | 0.32 [0.20] |
|  | Totals |  | 0 | 0 | $\begin{gathered} 7.64 \\ {[4.75]} \\ \hline \end{gathered}$ | 0 | 0 | 0 | $\begin{gathered} 7.64 \\ {[4.75]} \\ \hline \end{gathered}$ |
| *With Repairs and Joint Seals |  |  |  |  |  |  |  |  |  |

## APPENDIX B

PAVEMENT TYPES FOR EACH SECTION OF EACH PARKWAY HIGHWAY IN KENTUCKY AS OF DECEMBER 1993

| MOUNTAIN PARKWAY. PAVEMENT TYPE |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Initially |  | Presently |  |  |
|  |  |  | AC/DGA | PCC | ACIDGA | ACPCC | PCC |
| County | Mileposts | Dates | km [mi] | km [mi] | km [mi] | km [mi] | km [mi] |
| Clark | 0.00-3.68 | 62 |  | 5.92 [3.68] |  |  | 5.92 [3.68] |
| \% | 3.68-10.58 | 62/86BS* |  | 11.10 [6.90] |  | 11.10 [6.90] |  |
| Clark-Powell | 10.58-16.02 | 62/86BS* |  | 8.75 [5.44] |  | 8.75 [5.44] |  |
| Powell | 16.02-19.15 | 62/89BS* |  | 5.04 [3.13] |  | 5.04 [3.13] |  |
| " | 19.15-22.31 | 62/898S ${ }^{*}$ |  | 5.09 [3.16] |  | 5.09 [3.16] |  |
| " | 22.31-26.12 | 62/88BS* |  | 6.13 [3.81] |  | 6.13 [3.81] |  |
| " | 26.12-29.30 | 62/88BS ${ }^{*}$ |  | 5.12 [3.18] |  | 5.12 [3.18] |  |
| " | 29.30-32.90 | 62/89BS* |  | 5.83 [3.62] | , | 5.83 [3.62] |  |
| * | 32.90-36.00 | 62/908S* |  | 4.96 [3.08] |  | 4.96 [3.08] |  |
| Wolfe | 36.00-39.51 | 62/908S* |  | 5.65 [3.51] |  | 5.65 [3.51] |  |
| " | 39.51-43.20 | 62/918S** |  | 5.94 [3.69] |  | 5.94 [3.69] |  |
| " | 43.20-49.80 | 63/75/91 | 10.62 [6.60] |  | 10.62 [6.60] |  |  |
| " | 49.80-55.43 | 63/75/92 | 9.06 [5.63] |  | 9.06 [5.63] |  |  |
| Wolle-Morgan | 55.43-59.50 | 63/75/88 | 6.55 [4.07] |  | 6.55 [4.07] |  |  |
| Morgan | 59.50-63.08 | 63/75/89 | 5.76 [3.58] |  | 5.76 [3.58] |  |  |
| Magoftin | 63.08-67.40 | 63/75/87 | 6.95 [4.32] |  | 6.95 [4.32] |  |  |
| " | 67.40-71.65 | 63/75/88 | 6.84 [4.25] |  | 6.84 [4.25] |  |  |
| " | 71.65-74.58 | 63/75/86 | 4.72 [2.93] |  | 4.72 [2.93] |  |  |
| " | 74.58-75.63 | 63/75/85 | 1.69 [1.05] |  | 1.69 [1.05] |  |  |
|  | Totals |  | $\begin{array}{r} 52.19 \\ {[32.43]} \\ \hline \end{array}$ | $\begin{gathered} 69.52 \\ 143.201 \\ \hline \end{gathered}$ | $\begin{array}{r} 52.19 \\ {[32.43]} \\ \hline \end{array}$ | $\begin{gathered} 63.60 \\ {[39.52]} \\ \hline \end{gathered}$ | $\begin{gathered} 5.92 \\ {[3.68]} \end{gathered}$ |
| Drains |  |  |  |  |  |  |  |



| BLUEGRASS PARKWAY - PAVEMENT TYPE |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Initially |  | Presentry |  |  |
|  |  |  | AC/DGA | PCC | AC/DGA | ACPCC | PCC |
| County | Mileposts | Dates | km [mi] | km [mi] | km [mi] | km [mi] | km [mi] |
| Hardin-Nalson | 0.45-9.04 | 65/79/88/93 | 13.82 [8.59] EB |  | $13.82[8.59]$ EB |  |  |
| Neison | 9.04-16.54 | 65/79/88/92 | 12.07 [7.50] EB |  | 12.07[7.50] EB |  |  |
| n. | 16.54-24.24 | 65/79/88/92 | 12.39 [7.70] EB |  | 12.39[7.70]EB |  |  |
| Hardin | 0.45-4.90 | 65/99/88 | 7.16[4.45] WB |  | 7.16 [4.45] WB |  |  |
| Hardin-Noison | 4.90-9.52 | 65/79/88/93 | 7.44 [4.62] WB |  | 7.44 [4.62] WB |  |  |
| Nelson | 9.52-10.17 | 65/79/88/92 | 1.05 [0.65] WB |  | 1.05 [0.65] WB |  |  |
| " | 10.17-16.54 | 65/79/88 | 10.25 [6.37] WB |  | $10.25[6.37]$ WB |  |  |
| " | 16.54-24.24 | 65/79/88 | 12.39 [7.70] WB | - | 12.39 [7.70]WB |  |  |
| Nelson | 24.24-32.60 | 65/91** |  | 13.46 [8.36] |  |  | 13.46 [8.36] |
| " | 32.60-34.91 | 65/91** |  | 3.72 [231] |  |  | 3.72 [2.31] |
| - | 34.91-39.27 | 65 |  | 7.02 [4.36] |  |  | 7.02 [4.36] |
| Washington | 39.27-41.79 | 65/37BS* |  | 4.06 [2.52] |  | 4.06 [2.52] |  |
| WashingtonAnderson | 41.79-47.69 | 65/858S ${ }^{*}$ |  | 9.50 [5.90] |  | 9.50 [5.90] |  |
| Anderson | 47.69-51.84 | 65/86BS* |  | 6.68 [4.15] |  | 6.68 [4.15] |  |
| Anderson-Mercer | 51.84-59.59 | 65 |  | 12.47 [7.75] EB |  |  | 12.47 [7.75] EB |
| Anderson-Mercer | 51.84 .56 .29 | 65 |  | 7.16 [4.45] WB |  |  | 7.16 [4.45] WB |
| Anderson | 56.29.59.59 | 65/938S* |  | 5.31 [3.30] WB |  | 5.31 [3.30] WB |  |
| AndersonWoodford | 59.59-71.13 | 65/82 | 18.57 [11.54]EB |  | 18.57 [ 11.54 ] EB |  |  |
| " | 59.59-67.00 | 65/82/93 | 11.93 [7.41] WB |  | 11.93 [7.41] WB |  |  |
| Woodiord | 67.00-71.13 | 65/82/92 | 6.65 [4.13] WB |  | 6.65 [4.13] WB |  |  |
|  | Totals |  | $\begin{gathered} 56.86 \\ {[35.33]} \\ \hline \end{gathered}$ | $\begin{array}{r} 56.89 \\ {[35.35]} \\ \hline \end{array}$ | $\begin{gathered} 56.86 \\ {[35.33]} \end{gathered}$ | $\begin{gathered} 22.97 \\ {[14.27]} \\ \hline \end{gathered}$ | $\begin{array}{r} 33,94 \\ {[21.09]} \\ \hline \end{array}$ |
| ${ }^{*}$ Edge Drains <br> ${ }^{*}$ Edge Drains, Repairs and Joint Seals |  |  |  |  |  |  |  |


| PENNYRLLE PARKWAY - PAVEMENT TYPE |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Initially |  | Presently |  |  |
|  |  |  | ACIDGA | PCC | ACIDGA | AC/PCC | PCC |
| County | Miloposts | Dates | km [mi] | km [mi] | km [mi] | km [mi] | km [mi] |
| Christian | 6.77-10.77 | 68 |  | 6.44 [4.00] |  |  | 6.44 [4.00] |
| * | 10.77-16.50 | 68 |  | 9.22 [5.73] |  |  | 9.22 [5.73] |
| " | 16.50-22.48 | 68 |  | 9.62 [5.98] |  |  | 9.62 [5.98] |
| ChristianHopkins | 22.48-29.91 | 68/92 ${ }^{\text {+4* }}$ |  | 11.96 [7.43] |  |  | 11.96[7.43] |
| Hopkins | 29.91-32.94 | 63 |  | 4.88 [3.03] NB |  |  | 4.88 [3.03] NB |
| $\cdots$ | 29.91-31.36 | $63 / 90^{*}$ |  | 2.33 [1.45] SB |  | 2.33 [1.45] SB |  |
| * | 31.36-32.94 | 63/90* |  | 2.54 [1.58] SB |  | 2.54 [1.58] SB |  |
| " | 32.94-37.07 | 63 |  | 6.65 [4.13] NB |  |  | 6.65[4.13]NB |
| * | 32.94-35.55 | 63/90* |  | $4.20[2.61] \mathrm{SB}$ |  | $4.20[2.61]$ SB |  |
| " | 35.55-37.07 | 63/90BS* |  | 2.45 [1.52] SB |  | 2.45 [1.52] SB |  |
| " | 37.07-41.00 | 63 |  | 6.32 [3.93] |  |  | 6.32 [3.93] |
| " | 41.00-45.00 | 63 |  | 6.44 [4.00] |  |  | 6.44 [4.00] |
| " | 45.00-53.11 | 68 |  | 13.05 [8.11] |  |  | 13.05 [8.11] |
| HopkinsWebster | 53.11-61.84 | 69187BS ${ }^{*} / 90$ |  | 14.05 [8.73] NB |  | $14.05[8.73] \mathrm{NB}$ |  |
| , | 53.11-61.84 | 69/92** |  | 14.05 [8.73] SB |  | 14.05 [8.73] SB |  |
| Webster- <br> Hendersort | 61.84-65.50 | 69/88BS ${ }^{*}$ |  | 5.89 [3.66] |  | 5.89 [3.66] |  |
| Henderson | 65.50-70.35 | 69 |  | 7.81 [4.85] |  |  | 7.81 [4.85] |
| " | 70.35-78.25 | 68 |  | 12.71 [7.90] |  |  | 12.71 [7.90] |
|  | Totals |  | 0 | $\begin{gathered} 115.04 \\ {[71.48]} \end{gathered}$ | 0 | $\begin{gathered} 25.54 \\ {[15.87]} \\ \hline \end{gathered}$ | $\begin{array}{r} 89.48 \\ {[55.60]} \\ \hline \end{array}$ |
| *Edge Drains <br> **Edge Drains and PCC Repairs <br> "*Edge Drains, PCC Repairs, Joint Seals |  |  |  |  |  |  |  |


| AUDUBON PARKWAY - PAVEMENT TYPE |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Initially |  | Presently |  |  |
|  |  |  | AC/DGA | PCC | AC/DGA | ACPCC | PCC |
| County | Mieposts | Dates | km [mi] | km [mi] | km [mi] | km [mi] | km [mi] |
| Henderson | 0.00-8.75 | 70/87** |  | 14.08 [8.75] |  |  | 14.08 [8.75] |
| * | 8.75-15.88 | 70187** |  | 11.47 [7.13] |  |  | 11.47 [7.13] |
| Daviess | 15.88-23.46 | 70/87** |  | 12.20 [7.58] |  |  | 12.20 [7.58] |
|  | Totals |  | 0 | $\begin{gathered} 37.76 \\ {[23.46]} \\ \hline \end{gathered}$ | 0 | 0 | $\begin{array}{r} 37.76 \\ {[23.46]} \\ \hline \end{array}$ |
| *Edge Drains and Joint Seals |  |  |  |  |  |  |  |


| DANIEL BOONE PARKWAY - PAVEMENT TYPE |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Initially |  |  | Presently |  |  |
|  |  |  | ACIDGA | FDAC | PCC | ACIDGA | FDAC | PCC |
| County | Mloposts | Dates | km [mi] | km [mi] | km [mi] | km [mi] | km [mi] | km [mi] |
| Laurel | 0.00-0.93 | 70/87** |  |  | 1.50 [0.93] |  |  | 1.50 [0.93] |
| " | 0.93-8.80 | 71/87* |  |  | 12.67 [7.87] |  |  | 12.67 [7.87] |
| Laurel-Clay | 8.80-15.00 | 7179/93 | 9.98 [6.20] |  |  | 9.98 [6.20] |  |  |
| Clay | 15.00-20.33 | 71/79/93 | 8.58[5.33] |  |  | 8.58 [5.33] |  |  |
| " | 20.33-35.08 | 74 |  |  | 23.74 [14.75] |  |  | 23.74 [14.75] |
| Clay-Leslie | 35.08-41.46 | 74/79/86 |  | 10.27 [6.38] |  |  | 10.27 [6.38] |  |
| Losie | 41.46-44.04 | 74/79/86 |  | $4.15[2.58]$ EB |  |  | 4.15 [2.58] EB |  |
| " | 41.46-44.04 | 7479/82/86/917L |  | 4.15 [2.58] WB |  |  | 4.15 [2.58] WB |  |
| " | 44.04-44.35 | $74^{\text {t** }}$ |  |  | 0.50 [0.31] |  |  | 0.50 [0.31] |
| " | 44.35-45.37 | 74/86 |  | 1.64 [1.02] |  |  | 1.64 [1.02] |  |
| Leslie-Perry | 45.37-59.09 | 74/86 | 22.08 [13.72] |  |  | 22.08 [13.72] |  |  |
|  | Totals |  | $\begin{gathered} 40.64 \\ {[25.25]} \\ \hline \end{gathered}$ | $\begin{array}{r} 16.06 \\ {[9.98]} \\ \hline \end{array}$ | $\begin{gathered} 38.40 \\ {[23.86]} \\ \hline \end{gathered}$ | $\begin{gathered} 40.64 \\ {[25.25]} \\ \hline \end{gathered}$ | $\begin{array}{r} 16.06 \\ {[9.98]} \\ \hline \end{array}$ | $\begin{array}{r} 38.40 \\ {[23.86]} \\ \hline \end{array}$ |
| *Edge Drains <br> *Edge Drains and Joint Seals <br> "*Joint Seals |  |  |  |  |  |  |  |  |


| GREEN RIVER PARKWAY - PAVEMENT TYPE |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Initially |  |  | Presently |  |  |
|  |  |  | ACDGA | FDAC | PCC | ACIDGA | FDAC | PCC |
| County | Mileposts | Dates | km [mi] | $\mathrm{km}[\mathrm{mi}]$ | km [mi] | km [mi] | km [mi] | km [mi] |
| Warren | 0.00-7.10 | $72 / 91$ |  | 11.43 [7.10] |  |  | 11.43 [7.10] |  |
| " | 7.10.17.80 | 72/90 | 17.22 [10.70] |  |  | 17.22 [10.70] |  |  |
| Warren-Bulter | 17.80-26.42 | 72189 | 13.87 [8.62] |  |  | 13.87 [8.62] |  |  |
| Butier | 26.42-32.64 | 72/88 | 10.01 [6.22] |  |  | 10.01 [6.22] |  |  |
| Butler-Ohio | 32.64-42.27 | 72887* |  |  | 15.50 [9.63] |  |  | 15.50 [9.63] |
| Ohio | 42.27-52.60 | 72187** |  |  | 16.62 [10.33] |  |  | 16.62 [10.33] |
| Ohio-Daviess | 52.60-70.21 | 72/87** |  |  | 28.34 [17.61] |  |  | $28.34[17.61]$ |
|  | Totals |  | $\begin{array}{r} 41.10 \\ {[25.54]} \\ \hline \end{array}$ | $\begin{array}{r} 11.43 \\ {[7.10]} \\ \hline \end{array}$ | $\begin{gathered} 60.46 \\ {[37.57]} \\ \hline \end{gathered}$ | $\begin{gathered} 41.10 \\ {[25.54]} \\ \hline \end{gathered}$ | $\begin{aligned} & 11.43 \\ & {[7.10]} \\ & \hline \end{aligned}$ | $\begin{gathered} 60.46 \\ {[37.57]} \\ \hline \end{gathered}$ |
| **Edge Drains and Joint Seals |  |  |  |  |  |  | . |  |


| JACKSON PURCHASE PARKWAY - PAVEMENT TYPE |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Initially |  | Presently |  |  |
|  |  |  | AC/DGA | PCC | AC/DGA | AC/PCC | PCC |
| County | Mileposts | Dates | km [mi] | km [mi] | km [mi] | km [mi] | km [mi] |
| Fuiton | 0.00-2.48 | 68/85 | 3.99 [2.48] |  | 3.99 [2.48] |  |  |
| Fulton-Hickman | 2.48-8.35 | 68/86/91 | 9.45 [5.87] NB |  | 9.45 [5.87] NB |  |  |
| Fuilton | 2.48-3.41 | 68/83/88 | 1.50 [0.93] SB |  | 1.50 [0.93] SB |  |  |
| Hickman | 3.41-8.35 | 68/88 | 7.95 [4.94] SB |  | 7.95 [4.94] SB |  |  |
| Graves | 8.35-13.64 | 68/88 | 8.51 [5.29] |  | 8.51 [5.29] |  |  |
| n | 13.64-21.86 | 68/88 | 13.23 [8.22] |  | 13.23 [8.22] |  |  |
| " | 21.86-25.40 | 62/67/83/88 | 5.70 [3.54] |  | 5.70 [3.54] |  |  |
| Graves-Marshall | 25.40-39,92 | 68/92 | 23.37 [14.52] NB |  | 23.37 [14.52] NB |  |  |
| " | 25.40-39.92 | 68/89 | $23.37[14.52] \mathrm{SB}$ |  | 23.37[14.52] SB |  |  |
| Marshall | 39.92-52,33 | 68/91 | 19.97 [12.41] |  | 19.97 [12.41] |  |  |
|  | Totals |  | $\begin{gathered} 84.22 \\ {[52.33]} \\ \hline \end{gathered}$ | 0 | $\begin{gathered} 84.22 \\ {[52.33]} \end{gathered}$ | 0 | 0 |


| CUMBERLAND PARKWAY - PAVEMENT TYPE |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Initialy |  | Presently |  |
|  |  |  | ACIDGA | FDAC | ACIDGA | FDAC |
| County | Mileposts | Dates | km [mi] | km [mi] | km [mi] | km [mi] |
| Barren | 0.00-8. 17 | 72/93 |  | 13.15 [8.17] |  | 13.15[8.17] |
| " | 8.17-16.00 | 72 |  | 12.60 [7.83] |  | 12,60[7.83] |
| Barren-Metcaife | 16.00-24.10 | 72 |  | 13.04 [8.10] |  | 13.04 [8.10] |
| Metcalfe | 24.10-33.36 | 72 |  | 14.90 [9.26] |  | 14.90 [9.26] |
| " | 33.36-36.16 | $73 / 81$ |  | 4.51 [2,80] |  | 4.51 [2.80] |
| Adair | 36.16-43.02 | 73/79187* |  | 11.04 [6.86] |  | 11.04 [6.86] |
| " | 43.02-48.08 | 73/88 ${ }^{\text {²}}$ |  | 8.14 [5.06] |  | 8.14 [5.06] |
| " | 48.08-53.89 | 73/89* |  | 9.35 [5.81] |  | 9.35 [5.81] |
| Adair-Russell | 53.89-62.56 | 73 | 13.95 [8.67] |  | 13.95 [8.67] |  |
| Russell | 62.56-71.34 | 73 | 14.13 [8.78] WB |  | 14.13 [8.78] WB |  |
| Russell | 62.56-71.34 | 73193 | 14.13 [8.78] EB |  | 14.13 [8.78] EB |  |
| Russell.Pulaski | 71.34.76.55 | $74 / 92$ | $8.38[5.21] \mathrm{EB}$ |  | 8.38 [5.21]EB |  |
| " | 71.34-76.55 | 74 | 8.38[5.21] WB |  | 8.38 [5.21] WB |  |
| Pulaski | 76.55-84.31 | 74/91 | 12.49 [7.76] EB |  | 12.49 [7.76] EB |  |
| " | 76.55-84.31 | 74/92 | 12.49 [7.76] WB |  | 12.49 [7.76] WB |  |
| * | 84.31-88.55 | 74/91 | 6.83 [4.24] |  | 6.83 [4.24] |  |
|  | Totals |  | $\begin{gathered} 55.78 \\ {[34.66]} \end{gathered}$ | $\begin{gathered} 86.79 \\ {[53.89]} \\ \hline \end{gathered}$ | $\begin{gathered} 55.78 \\ {[34.66]} \end{gathered}$ | $\begin{gathered} 86.73 \\ {[59.89]} \end{gathered}$ |
| ${ }^{\text {* Polymer Seal }}$ |  |  |  |  |  |  |

## APPENDIX C

## SUMMARY DATA FOR <br> PAVEMENT SECTIONS EVALUATED

## PENNYRILE PARKWAY, HOPKINS COUNTY

- PORTLAND CEMENT CONCRETE

THICKNESS $=230 \mathrm{~mm}(229$ to 235 ) [9.04 in. ( 9.00 to 9.25 )]
COMPRESSIVE STRENGTH $=39.6 \mathrm{MPa}(32.4$ to 52.5$)$ [5,750 $\mathrm{psi}(4,710$ to 7,570$)]$
MODULUS OF ELASTICITY $=28.1 \mathrm{GPa}\left(26.9\right.$ to 29.6) [4.07 $\times 10^{6}(3.90$ to 4.30$\left.)\right]$

- DENSE GRADED AGGREGATE (DGA) BASE

THICKNESS $=104 \mathrm{~mm}(95$ to114) [4.08 in. ( 3.75 to 4.50 )]
MOISTURE CONTENT $=5.7 \%$ ( 3.5 to 7.1)
IN-SITU CBR = 12 (8 to 15)
MINUS $75-\mu \mathrm{m}(\mathrm{NO} .200)$ SIEVE $=12.3 \%$ ( 9.8 to 14.2)
NON-PLASTIC

- SUBGRADE SAMPLES

MOISTURE CONTENT BELOW DGA $=15.2 \%$ (10.9 to 20.8)
IN-SITU CBR = 6 (2 to 12)

- SUBGRADE TUBE SAMPLES

MOISTURE CONTENT @ 0-178 mm (0-7 in.) $=15.0 \%$ ( 11.4 to 20.7)
UNCONFINED COMPRESSIVE STRENGTH $=248 \mathrm{KPa}$ ( 123 to 419 ) [36.0 psi (17.9 to 60.8)]
WET DENSITY $=2,215 \mathrm{~kg} / \mathrm{m}^{3}(2,153$ to 2,278$)$ [ 138.0 pcf ( 134.1 to 141.9 )]
GENERAL SOIL CLASSIFICATION = CL

- GENERAL NOTES

CONSTRUCTED 1968
RATED TO BE IN NEAR EXCELLENT CONDITION
NO SUBSEQUENT MAINTENANCE ACTIVITIES PERFORMED THROUGH JANUARY 1994

## US 119, PIKE COUNTY

- PORTLAND CEMENT CONCRETE

THICKNESS $=234 \mathrm{~mm}(222$ to 254$)$ [ 9.21 in . ( 8.75 to 10.00 )] COMPRESSIVE STRENGTH $=42.3 \mathrm{MPa}$ ( 37.6 to 48.1 ) $[6,140 \mathrm{psi}(5,460$ to 6,980$)]$ MODULUS OF ELASTICITY $=27.9 \mathrm{GPa}(27.2$ to 29.0$)$ [ $4.05 \times 10^{6}(3.95$ to 4.20$\left.)\right]$

- DENSE GRADED AGGREGATE (DGA) BASE

THICKNESS $=99 \mathrm{~mm}(83$ tol14) [ $3.88 \mathrm{in} .(3.25$ to 4.50$)$ ]
MOISTURE CONTENT $=5.6 \%$ ( 3.4 to 8.2)
$\operatorname{IN}-$ SITU CBR $=24$ ( 13 to 48)
MINUS $75-\mu \mathrm{m}$ (NO. 200) SIEVE $=16.9 \%$ (14.2 to 20.5)
NON-PLASTIC

- SUBGRADE SAMPLES

MOISTURE CONTENT BELOW DGA $=8.1 \%$ ( 5.8 to 12.1 )
$\mathbb{N}$-SITU CBR = 13 ( 1 to 30 )

- SUBGRADE TUBE SAMPLES

MOISTURE CONTENT @ 0-178 mm ( $0-7 \mathrm{in}.)=9.8 \%$
GENERAL SOIL CLASSIFICATION = SM-SC

- GENERAL NOTES

CONSTRUCTED 1982
RATED TO BE IN EXCELLENT CONDITION
VARIABLE JOINT SPACING

## I-64, FAYETTE COUNTY

- PORTLAND CEMENT CONCRETE

THICKNESS $=254 \mathrm{~mm}(254$ to 254) [10.00 in. (10.00 to 10.00)]
COMPRESSIVE STRENGTH $=51.2 \mathrm{MPa}(47.7$ to 58.5$)[7,430 \mathrm{psi}(6,920$ to 8,490$)]$
MODULUS OF ELASTICITY $=35.0 \mathrm{GPa}(33.1$ to 37.6$)\left[5.08 \times 10^{6}(4.80\right.$ to 5.45$\left.)\right]$

- DENSE GRADED AGGREGATE (DGA) BASE

THICKNESS $=159 \mathrm{~mm}(152$ to165) [6.25 in. ( 6.00 to 6.50)]
MOISTURE CONTENT $=6.1 \%$ ( 5.7 to 6.4 )
$\mathbb{N}-$ SITU CBR $=20$ ( 13 to 27)
MINUS $75-\mu \mathrm{m}$ (NO. 200) SIEVE $=10.6 \%$ ( 9.3 to 11.5)
NON-PLASTIC

- SUBGRADE SAMPLES

MOISTURE CONTENT BELOW DGA $=24.8 \%$ (18.8 to 30.1 )
IN-SITU CBR $=2(1$ to 3 )

- SUBGRADE TUBE SAMPLES

MOISTURE CONTENT @ 0-178 mm (0-7 in.) $=23.2 \%$ ( 19.6 to 27.2)
UNCONFINED COMPRESSIVE STRENGTH = 241 KPa ( 108 to 432 ) [34.9 psi (15.6 to 62.7)]
WET DENSITY $=2,124 \mathrm{~kg} / \mathrm{m}^{3}(2,066$ to 2,175$)$ [ 138.0 pcf ( 134.1 to 141.9 )]
GENERAL SOIL CLASSIFICATION = CL

- GENERAL NOTES

CONSTRUCTED 1963
RATED TO BE IN EXCELLENT CONDITION
EDGE DRAINS INSTALLED IN 1987

## I-75, FAYETTE COUNTY

- PORTLAND CEMENT CONCRETE

THICKNESS $=254 \mathrm{~mm}$ (254 to 254 ) [ 10.00 in. ( 10.00 to 10.00)]
COMPRESSIVE STRENGTH $=40.0 \mathrm{MPa}(36.7$ to 43.0$)[5,800 \mathrm{psi}(5,330$ to 6,230$)]$
MODULUS OF ELASTICITY $=31.2 \mathrm{GPa}$ (27.2 to 34.8 ) [ $4.52 \times 10^{6}(3.95$ to 5.05$\left.)\right]$

- DENSE GRADED AGGREGATE (DGA) BASE

THICKNESS $=137 \mathrm{~mm}$ ( 127 to 40 ) [ 5.38 in. ( 5.00 to 5.50 )]
MOISTURE CONTENT $=6.1 \%$ ( 5.4 to 7.4 )
$\operatorname{IN}$-SITU CBR $=12(6$ to 16 )
MINUS $75-\mu \mathrm{m}(\mathrm{NO} .200)$ SIEVE $=9.2 \%$ (6.5 to 12.0)
NON-PLASTIC

- SUBGRADE SAMPLES

MOISTURE CONTENT BELOW DGA $=15.5 \%$ ( 8.7 to 21.6 )
$\mathbb{N}$-SITU CBR $=3$ ( 1 to 5 )

- SUBGRADE TUBE SAMPLES

MOISTURE CONTENT @ 0-178 mm ( $0-7 \mathrm{in}$. ) $=15.1 \%$ ( 12.8 to 20.6 )
UNCONFINED COMPRESSIVE STRENGTH $=157 \mathrm{KPa}(73$ to 241 ) [22.8 psi ( 10.6 to 34.9 )]
WET DENSITY $=2,228 \mathrm{~kg} / \mathrm{m}^{3}(2,122$ to 2,334$)$ [ $138.8 \mathrm{pcf}(132.2$ to 145.4$\left.)\right]$
GENERAL SOIL CLASSIFICATION = VARIABLE

- GENERAL NOTES

CONSTRUCTED 1969
RATED TO BE IN EXCELLENT CONDITION
EDGE DRAINS, PCC REPAIRS \& JOINT SEALS 1984

## I-64, SHELBY COUNTY

- PORTLAND CEMENT CONCRETE

THICKNESS $=254 \mathrm{~mm}(248$ to 260$)$ [ 10.00 in. ( 9.75 to 10.25)]
COMPRESSIVE STRENGTH $=47.0 \mathrm{MPa}(39.1$ to 55.4$)[6,810 \mathrm{psi}(5,670$ to 8,030$)]$
MODULUS OF ELASTICITY $=31.2 \mathrm{GPa}(27.9$ to 34.8$)$ [ $4.53 \times 10^{6}(4.05$ to 5.05$\left.)\right]$

- DENSE GRADED AGGREGATE (DGA) BASE

THICKNESS $=152 \mathrm{~mm}$ ( 140 to159) [ 6.00 in . ( 5.50 to 6.25 )]
MOISTURE CONTENT $=6.2 \%$ (5.1 to 7.0 )
$\mathbb{N}-$ SITU CBR $=16$ ( 6 to 27)
MINUS $75-\mu \mathrm{m}(\mathrm{NO} .200)$ SIEVE $=10.4 \%$ ( 9.0 to 11.9)
NON-PLASTIC

- SUBGRADE SAMPLES

MOISTURE CONTENT BELOW DGA $=22.8 \%$ (18.8 to 25.2)
IN-SITU CBR = 3 ( 2 to 3 )

- SUBGRADE TUBE SAMPLES

MOISTURE CONTENT @ 0-178 mm (0-7 in.) = 23.4\% (17.9 to 27.8)
UNCONFINED COMPRESSIVE STRENGTH $=156 \mathrm{KPa}(71$ to 321 ) [ 22.7 psi ( 10.3 to 46.5 )]
WET DENSITY $=2,106 \mathrm{~kg} / \mathrm{m}^{3}(2,050$ to 2,174 ) [131.2 pcf ( 127.7 to 135.4)]
GENERAL SOIL CLASSIFICATION = CL

- GENERAL NOTES

CONSTRUCTED 1961
RATED TO BE IN NEAR EXCELLENT CONDITION
EDGE DRAINS INSTALLED IN 1984

## US 27, PULASKI COUNTY

- PORTLAND CEMENT CONCRETE

THICKNESS $=192 \mathrm{~mm}(1 \mathrm{XX}$ to 2 XX ) [7.54 in. (7.XX to 8.XX)]
COMPRESSIVE STRENGTH $=51.3 \mathrm{MPa}(44.9$ to 57.4$)[7,440 \mathrm{psi}(6,510$ to 8,320$)]$
MODULUS OF ELASTICITY $=33.4 \mathrm{GPa}(31.7$ to 35.5$)\left[4.85 \times 10^{6}(4.60\right.$ to 5.15$\left.)\right]$

- DENSE GRADED AGGREGATE (DGA) BASE

THICKNESS $=93 \mathrm{~mm}(64$ to 102 ) [3.67 in. ( 2.50 to 4.00 )]
MOISTURE CONTENT $=8.1 \%$ ( 4.2 to 9.6 )
IN-SITU CBR $=9$ (2 to 16)
MINUS $75-\mu \mathrm{m}$ (NO. 200) SIEVE $=12.1 \%$ (9.3 to 16.7)
NON-PLASTIC

- SUBGRADE SAMPLES

MOISTURE CONTENT BELOW DGA $=26.3 \%$ (25.2 to 27.4)
IN-SITU CBR = $2(0$ to 4$)$

- SUBGRADE TUBE SAMPLES

MOISTURE CONTENT @ $0-178 \mathrm{~mm}(0-7 \mathrm{in})=.28.0 \%(20.6$ to 31.9$)$
UNCONFINED COMPRESSIVE STRENGTH $=129 \mathrm{KPa}(110$ to 176 ) [18.7 psi (15.9 to 25.6)]
WET DENSITY $=1,982 \mathrm{~kg} / \mathrm{m}^{3}$ ( 1,885 to 2,042 ) [123.5 pcf (117.4 to 127.2)]
GENERAL SOIL CLASSIFICATION $=\mathrm{CH}$

- GENERAL NOTES

CONSTRUCTED 1960
RATED TO BE PERFORMING VERY WELL
NO SUBSEQUENT MAINTENANCE ACTIVITIES PERFORMED THROUGH 1994

## US 127, OWEN COUNTY

- PORTLAND CEMENT CONCRETE

THICKNESS $=208 \mathrm{~mm}(197$ to 216) [8.17 in. (7.75 to 8.50)]
COMPRESSIVE STRENGTH $=41.3 \mathrm{MPa}(34.0$ to 50.5$)$ [ $5,990 \mathrm{psi}(4,930$ to 7,330$)]$
MODULUS OF ELASTICITY $=28.3 \mathrm{GPa}(27.9$ to 28.6$)\left[4.10 \times 10^{6}(4.05\right.$ to 4.15$\left.)\right]$

- DENSE GRADED AGGREGATE (DGA) BASE

THICKNESS $=90 \mathrm{~mm}(76$ to 121) [3.54 in. ( 3.00 to 4.75)]
MOISTURE CONTENT $=9.3 \%$ ( 6.8 to 13.2)
IN-SITU CBR = 8 (4 to 17)
MINUS $75-\mu \mathrm{m}$ (NO. 200) SIEVE $=11.3 \%(9.4$ to 12.9)
NON-PLASTIC

- SUBGRADE SAMPLES

MOISTURE CONTENT BELOW DGA $=24.6 \%$ (19.7 to 27.5)
IN-SITU CBR $=2$ ( 1 to 4 )

- SUBGRADE TUBE SAMPLES

MOISTURE CONTENT @ 0-178 mm (0-7 in.) = 22.6\% ( 18.5 to 24.2)
UNCONFINED COMPRESSIVE STRENGTH $=92 \mathrm{KPa}(59$ to 121 ) [13.4 psi ( 8.6 to 17.6)]
WET DENSITY $=2,143 \mathrm{~kg} / \mathrm{m}^{3}(2,052$ to 2,209 ) [ 133.5 pcf ( 127.8 to 137.6)]
GENERAL SOIL CLASSIFICATION = CL

- GENERAL NOTES

CONSTRUCTED 1973
RATED TO BE IN EXCELLENT CONDITION
NO SUBSEQUENT MAINTENANCE ACTIVITIES PERFORMED THROUGH JANUARY 1994

## BLUEGRASS PARKWAY, NELSON COUNTY

- PORTLAND CEMENT CONCRETE

THICKNESS $=229 \mathrm{~mm}(222$ to 235 ) [ 9.00 in . ( 8.75 to 9.25 )]
COMPRESSIVE STRENGTH $=57.2 \mathrm{MPa}$ ( 53.2 to 62.6 ) $[8,300 \mathrm{psi}(7,710$ to 9,080$)]$
MODULUS OF ELASTICITY $=35.0 \mathrm{GPa}(32.1$ to 37.6$)$ [ $5.08 \times 10^{6}$ ( 4.65 to 5.45 )]

- DENSE GRADED AGGREGATE (DGA) BASE

THICKNESS $=106 \mathrm{~mm}(89$ to 146$)$ [4.17 in. ( 3.50 to 5.75 )]
MOISTURE CONTENT $=5.9 \%$ ( 4.7 to 7.7 )
IN-SITU CBR = 14 (11 to 19)
MINUS $75-\mu \mathrm{m}$ (NO. 200) SIEVE $=11.2 \%$ ( 9.3 to 13.1)
NON-PLASTIC

- SUBGRADE SAMPLES

MOISTURE CONTENT BELOW DGA $=23.6 \%$ ( 19.5 to 27.4 )
IN-SITU CBR = 2 ( 1 to 2)

- SUBGRADE TUBE SAMPLES

MOISTURE CONTENT @ 0-178 mm (0-7 in.) $=22.2 \%$ ( 19.5 to 26.5)
UNCONFINED COMPRESSIVE STRENGTH $=161 \mathrm{KPa}(92$ to 231 ) [23.4 psi (13.3 to 33.5$)$ ]
WET DENSITY $=2,140 \mathrm{~kg} / \mathrm{m}^{3}(2,133$ to 2,164 [133.3 pcf (132.9 to 134.8)]
GENERAL SOIL CLASSIFICATION = CL

- GENERAL NOTES

CONSTRUCTED 1965
RATED TO BE IN EXCELLENT CONDITION
EDGE DRAINS, PCC REPAIRS \& JOINT SEALS 1984

## PENNYRILE PARKWAY, HOPKINS AND CHRISTIAN COUNTIES

- PORTLAND CEMENT CONCRETE

THICKNESS $=234 \mathrm{~mm}$ (229 to 241) [9.21 in. ( 9.00 to 9.50)] COMPRESSIVE STRENGTH $=48.7 \mathrm{MPa}(40.6$ to 52.8$)[7,060 \mathrm{psi}(5,890$ to 7,660$)]$
MODULUS OF ELASTICITY $=30.2 \mathrm{GPa}(28.6$ to 32.1$)$ [ $4.38 \times 10^{6}$ ( 4.15 to 4.65 )]

- DENSE GRADED AGGREGATE (DGA) BASE

THICKNESS $=90 \mathrm{~mm}(76$ to 102 ) [3.54 in. (3.00 to 4.00)]
MOISTURE CONTENT $=4.7 \%$ ( 3.2 to 5.5 )
$\operatorname{N}$-SITU CBR = 11 (7 to 14)
MINUS $75-\mu \mathrm{m}$ (NO. 200) SIEVE $=12.4 \%$ (10.6 to 14.7)
NON-PLASTIC

- SUBGRADE SAMPLES

MOISTURE CONTENT BELOW DGA $=14.8 \%$ ( 11.8 to 17.7)
IN-SITU CBR $=4$ ( 1 to 6 )

- SUBGRADE TUBE SAMPLES

MOISTURE CONTENT @ $0-178 \mathrm{~mm}(0-7 \mathrm{in})=.18.3 \%(12.3$ to 21.5$)$
UNCONFINED COMPRESSIVE STRENGTH = 233 KPa ( 69 to 515 ) [ $33.8 \mathrm{psi}(10.0$ to 74.7 )]
WET DENSITY $=2,196 \mathrm{~kg} / \mathrm{m}^{3}(2,143$ to 2,300 ) [136.8 pcf (133.5 to 143.3)]
GENERAL SOIL CLASSIFICATION = CL

- GENERAL NOTES

CONSTRUCTED 1968
RATED TO BE IN EXCELLENT CONDITION
EDGE DRAINS, PCC REPAIR \& JOINT SEALS 1993

## AUDUBON PARKWAY, DAVIESS COUNTY

- PORTLAND CEMENT CONCRETE

THICKNESS $=229 \mathrm{~mm}(229$ to 229) [9.00 in. ( 9.00 to 9.00)]
COMPRESSIVE STRENGTH $=39.6 \mathrm{MPa}$ ( 35.0 to 45.0 ) [ $5,740 \mathrm{psi}(5,080$ to 6,530$)]$
MODULUS OF ELASTICITY $=25.7 \mathrm{GPa}(24.8$ to 26.5$)$ [ $3.73 \times 10^{6}(3.60$ to 3.85$\left.)\right]$

- DENSE GRADED AGGREGATE (DGA) BASE

THICKNESS $=101 \mathrm{~mm}(95$ to 102) [ 3.96 in. ( 3.75 to 4.00 )]
MOISTURE CONTENT $=5.8 \%$ ( 4.9 to 6.8 )
IN-SITU CBR = 16 ( 9 to 34)
MINUS $75-\mu \mathrm{m}$ (NO. 200) SIEVE $=17.0 \%$ (14.8 to 18.9)
NON-PLASTIC

- SUBGRADE SAMPLES

MOISTURE CONTENT BELOW DGA $=14.5 \%$ ( 10.0 to 17.4)
IN-SITU CBR = 9 (5 to 15 )

- SUBGRADE TUBE SAMPLES

MOISTURE CONTENT @ 0-178 mm (0-7 in.) = 13.3\% (8.4 to 18.1)
UNCONFINED COMPRESSIVE STRENGTH $=280 \mathrm{KPa}$ ( 153 to 345 ) [40.6 psi (22.2 to 50.1)]
WET DENSITY $=2,186 \mathrm{~kg} / \mathrm{m}^{3}(2,088$ to 2,231$)$ [136.2 $\operatorname{pcf}$ ( 130.1 to 139.0 )]
GENERAL SOIL CLASSIFICATION = CL

- GENERAL NOTES

CONSTRUCTED 1970
RATED TO BE IN EXCELLENT CONDITION
EDGE DRAINS \& JOINT SEALS 1987

## GREEN RIVER PARKWAY, OHIO COUNTY

- PORTLAND CEMENT CONCRETE

THICKNESS $=230 \mathrm{~mm}(229$ to 235 ) [ 9.04 in . ( 9.00 to 9.25 )]
COMPRESSIVE STRENGTH $=45.4 \mathrm{MPa}$ ( 40.8 to 52.3 ) [ $6,580 \mathrm{psi}(5,920$ to 7,580$)$ ]
MODULUS OF ELASTICITY $=31.6 \mathrm{GPa}(30.3$ to 33.1$)\left[4.58 \times 10^{6}(4.40\right.$ to 4.80$\left.)\right]$

- DENSE GRADED AGGREGATE (DGA) BASE

THICKNESS $=103 \mathrm{~mm}(89$ to 114) [4.06 in. ( 3.50 to 4.50 )]
MOISTURE CONTENT $=5.4 \%$ ( 3.5 to 7.1 )
IN-SITU CBR = 17 ( 11 to 30 )
MINUS $75-\mu \mathrm{m}$ (NO. 200) SIEVE $=10.6 \%$ ( 8.9 to 16.0 )
NON-PLASTIC

- SUBGRADE SAMPLES

MOISTURE CONTENT BELOW DGA $=13.8 \%$ ( 11.2 to 16.0)
IN-SITU CBR = 7 ( 3 to 13 )

- SUBGRADE TUBE SAMPLES

MOISTURE CONTENT @ 0-178 mm (0-7 in.) = 11.4\% (10.3 to 13.2) .
UNCONFINED COMPRESSIVE STRENGTH = 201 KPa (158 to 243) [29.1 psi (22.9 to 35.2)]
WET DENSITY $=2,228 \mathrm{~kg} / \mathrm{m}^{3}(2,209$ to 2,246 ) [138.8 pcf (137.6 to 139.9)]
GENERAL SOIL CLASSIFICATION = VARIABLE

- GENERAL NOTES

CONSTRUCTED 1972
RATED TO BE IN EXCELLENT CONDITION
EDGE DRAINS \& JOINT SEALS 1987

## WESTERN KENTUCKY PARKWAY, HOPKINS COUNTY

- PORTLAND CEMENT CONCRETE

THICKNESS $=234 \mathrm{~mm}(229$ to 235$)$ [ 9.21 in . ( 9.00 to 9.25 )]
COMPRESSIVE STRENGTH $=48.7 \mathrm{MPa}(43.4$ to 51.8$)[7,060 \mathrm{psi}(6,290$ to 7,520$)]$
MODULUS OF ELASTICITY $=32.2 \mathrm{GPa}(31.0$ to 34.5$)$ [ $4.67 \times 10^{6}(4.50$ to 5.00$\left.)\right]$

- DENSE GRADED AGGREGATE (DGA) BASE

THICKNESS $=109 \mathrm{~mm}$ ( 95 to 121) [ 4.30 in . ( 3.75 to 4.75 )]
MOISTURE CONTENT $=7.9 \%$ ( 6.0 to 10.2)
IN-SITU CBR $=9$ ( 5 to 11)
MINUS $75-\mu \mathrm{m}$ (NO. 200) SIEVE $=12.7 \%$ ( 10.7 to 14.5)
NON-PLASTIC

- SUBGRADE SAMPLES

MOISTURE CONTENT BELOW DGA $=21.1 \%$ (15.7 to 27.5)
IN-SITU CBR $=4$ ( 2 to 5 )

- SUBGRADE TUBE SAMPLES

MOISTURE CONTENT @ 0-178 mm (0-7 in.) $=16.2 \%$ ( 12.1 to 20.7)
UNCONFINED COMPRESSIVE STRENGTH $=131 \mathrm{KPa}$ ( 36 to 197) [19.0 psi (5.3 to 28.6)]
WET DENSITY $=2,204 \mathrm{~kg} / \mathrm{m}^{3}(2,143$ to 2,284 ) [137.3 pcf ( 133.5 to 142.3)]
GENERAL SOIL CLASSIFICATION = VARIABLE (mostly CL)

- GENERAL NOTES

CONSTRUCTED 1963
RATED TO BE IN EXCELLENT CONDITION
NO SUBSEQUENT MAINTENANCE ACTIVITIES PERFORMED THROUGH JANUARY 1994

## APPENDIX D

## DETAILED TEST RESULTS FOR THE PAVEMENT SECTIONS EVALUATED

US 127, OWEN COUNTY
PORTLAND CEMENT CONCRETECOBES


DENSE GBADED AGGREGATE BASE


SUBGRADE TUBE SAMEIES

| SUBGBADE TURE SAMELES |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SAMPLE | DEPTH | MOISTURE CONTENT | UNCONFINED COMPRESSIVE STRENGTH | WET DENSITY |  | TE | JRG |  |
| ID | mm fin. ${ }^{\text {d }}$ | (\%) | kPa [psi] | $\mathrm{kg} / \mathrm{m}^{3}$ [pci] | LL | PL | PI | CLASS |
| 127-21-1 | 0-150 [0-6] | 24.0 | 121.3 [17.6] | 2,047 [127.8] | 40 | 20 | 20 | CL |
| 127-21-2 | 0-175 [0-7[ | 18.5 | 59.3 [8.6] | 2,204 [137.6] | 38 | 20 | 18 | CL |
| 127-21-3 | 0-175[0-7] | 24.2 | 68.9 [10.0] | 2,130 [133.0] | 37 | 20 | 17 | CL |
| 127-23-1 | 0-150 [0-6] | 24.0 | 98.6 [14.3] | 2,182 [136.2] | 45 | 19 | 26 | CL |
| 127-23-2 | 175-350 [7-14] | 30.2 | 133.1 [19.3] | 2,076 [129.6] | 37 | 20 | 17 | CL |
| 127-23-3 | $0-150$ [0-6] | 22.4 | 114.5 [16.6] | 2,132 [133.1] | 39 | 17 | 22 | Cl |
| AVERAGE |  | 23.9 | 99.3 [14.4] | 2.129 [132.9] | 39 | 19 | 19 |  |



| BLUEGRASS PARKWAY, NELSON COUNTY |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SAMPLE <br> ID | THICKNESS mm [in.] | COMPRESSIVE STRENGTH - MPa [psi] | MODULUS OF ELASTICITY GPa $\left[p s i \times 10^{6}\right]$ |  |  |  |  |  |
| BG-26-1 | 225 [9.00] | 59.4 [8,620] | 37.6 [5.45] |  |  |  |  |  |
| BG-26-2 | 225 [9.00] | 53.7 [7,790] | 32.1 [4.65] |  |  |  |  |  |
| BG-26-3 | 219 [8.75] |  |  |  |  |  |  |  |
| BG-25-1 | 225 [9.00] | 53.2 [7,710] |  |  |  |  |  |  |
| BG-25-2 | 231 [9.25] | $62.6[9,080]$ | 35.5 [5.15] |  |  |  |  |  |
| BG-25-3 | 225 [9.00] |  |  |  |  |  |  |  |
| - AVERAGE | -225[9.00] | - 57.2 [8,300] | 35.0 [5.08] |  |  |  |  |  |
| DENSEGBADED ASGREGATE RASE |  |  |  |  |  |  |  |  |
| SAMPLE $10$ | THICKNESS mm [in.] | MOISTURE CONTENT <br> (\%) | $\operatorname{IN}-\mathrm{SITU}$ CBR | MINUS $75 \mu \mathrm{~m}$ (No. 200) SIEVE $\qquad$ <br> (\%) |  | $\begin{aligned} & \text { ASTIO } \\ & \text { VDEX } \end{aligned}$ |  |  |
| BG-26-1 | 100 [4.00] | 6.1 | 12 | 13.1 |  |  |  |  |
| BG-26-2 | 144 [5.75] | 4.7 | 12 | 11.0 |  |  |  |  |
| BG-26-3 | 88 [3.50] | 5.0 | 19 | 11.3 |  |  |  |  |
| BG-25-1 | 88 [3.50] | 5.3 | 12 | 10.0 |  |  |  |  |
| BG-25-2 | 112 [4.50] | 7.7 | 17 | 9.3 |  |  |  |  |
| BG-25-3 | 94 [3.75] | 6.4 | 11 | 12.4 |  |  |  |  |
| AVERAGE | 104 [4.17] | 5.9 | 14 | 11.2 |  |  |  |  |
| IISTUBRED SUBGRADE SAMPIES |  |  |  |  |  |  |  |  |
| MOISTURE |  |  |  |  |  |  |  |  |
|  | CONTENT | IN-SITU |  |  |  |  |  |  |
| $\begin{gathered} \text { SAMPLE } \\ \text { ID } \\ \hline \end{gathered}$ | BELOW DGA $\qquad$ <br> (\%) | CBR |  |  |  |  |  |  |
| BG-26-1 | 23.1 | 1 |  |  |  |  |  |  |
| BG-26-2 | 19.5 | 2 |  |  |  |  |  |  |
| BG-26-3 | 20.9 | 2 |  |  |  |  |  |  |
| BG-25-1 | 23.4 | 1 |  |  |  |  |  |  |
| BG-25-2 | 27.4 | 2 |  |  |  |  |  |  |
| BG-25-3 | 27.1 | 2 |  |  |  |  |  |  |
| _ AVERAGE | 23.6 | 2 |  |  |  |  |  |  |
| SURGEADETUBE SAMPIES |  |  |  |  |  |  |  |  |
|  |  |  | UNCONFINED |  |  |  |  |  |
|  |  | MOISTURE | COMPRESSIVE | WET |  |  |  |  |
| SAMPLE | DEPTH | CONTENT | STRENGTH | DENSITY |  | TTER | IRG |  |
| ID | mm [in] | (\%) | kPa [psi] | $\mathrm{kg} / \mathrm{m}^{3}$ [pcf] | LL | PL | PI | CLASS |
| BG-26-1 | 0-175 [0-7] | 26.5 | 231.0 [33.5] | 2,129 [132.9] | 46 | 21 | 25 | Cl |
| BG-26-2 | 0-150 [0-6] | 21.3 | 130.3 [18.9] | 2,132 [133,1] | 39 | 18 | 21 | CL |
| BG-26-3 | 0-175 [0-7] | 22.3 | 91.7 [13.3] | 2,130 [133.0] | 41 | 20 | 21 | CL |
| BG-25-1 | 0-175 [0-7] | 21.6 | 228.9 [33.2] | 2,129 [132.9] | 44 | 20 | 24 | CL |
| BG-25-2 | 175-325 [7-13] | 19.1 | 293.0 [42.5] | 2,186 [136.5] | 42 | 20 | 22 | CL |
| BG-25-3 | 0-175 [0-7] | 19.5 | 126.2 [18.3] | 2,159 [134.8] | 41 | 21 | 20 | CL |
| BG-25-3 | 175-325 [7-13] | 32.9 | 84.8 [12.3] | 2,094 [130.7] |  |  |  |  |
| AVERAGE |  | 23.3 | 169.6 [24.6] | 2,137 [133.4] | 42 | 20 | 22 |  |









PENNYRILE PARKWAY, HOPKINS COUNTY

| SAMPLE ID | THICKNESS <br> mm [in.] | $\begin{gathered} \text { COMPRESSIVE } \\ \text { STRENGTH } \\ \text { MPa [psi] } \end{gathered}$ | MODULUS OF ELASTICITY <br> GPa $\left[\right.$ psi $\left.\times 10^{6}\right]$ |
| :---: | :---: | :---: | :---: |
| PRP-47-1 | 225 [9.00] | 32.5 [4,710] | 29.6 [4.30] |
| PRP-47-2 | 225 [9.00] | 38.3 [5,550] | 27.6 [4.00] |
| PRP-47-3 | 231 [9.25] |  |  |
| PAP-50-1 | 225 [9.00] |  |  |
| PRP-50-2 | 225 [9.00] | 52.2 [7,570] | 26.9 [3.90] |
| PRP-50-3 | 225 [9.00] | $35.7[5,180]$ |  |
| AVERAGE | 226 [9.04] | 39.6 [ 5.750$]$ | 28.1 [4.07] |


| SAMPLE ID | THICKNESS <br> (in.) | MOISTURE CONTENT $\qquad$ (\%) | IN-SITU CBR | MINUS 75 k. m (No. 200) SIEVE (\%) | $\begin{gathered} \text { PLASTICITY } \\ \text { INDEX } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| PRP-47-1 | 106 [4.25] | 6.8 | 15 | 11.2 | 4 |
| PRP-47-2 | 100 [4.00] | 3.5 | 11 | 12.5 | NP |
| PRP-47-3 | 94 [3.75] | 6.3 | 11 | 9.8 | NP |
| PRP-50-1 | 100 [4.00] | 4.3 | 14 | 12.6 | NP |
| PRP-50-2 | 100 [4.00] | 6.0 | 8 | 14.2 |  |
| PRP-50-3 | 113 [4.50] | 7.1 | 10 | 13.3 |  |
| AVERAGE | 102 [4.08] | 5.7 | 12 | 12.3 |  |

DISTUBRED SURGEANE SAMPIES
MOISTURE
CONTENT

|  | CONTENT <br> SAMPLE <br> ID | BELOW DGA <br> $(\%)$ |
| :---: | :---: | :---: | | IN-SITU |
| :---: |
| CBR |

## SUBGBANE TIIRE SAMPIES





[^0]:    * All base samples were non-plastic ** Excluding sandstone base project

