

AFOSR-TN-57-786

ASTIA Document No. AD 148 017

CALIFORNIA INSTITUTE OF TECHNOLOGY

Antenna Laboratory

Technical Report No. 13

ELECTROMAGNETIC WAVES ON CORRUGATED LINES:  
PROPAGATION CONSTANT MEASUREMENTS

Georges G. Weill  
Hans Kuehl

This research was supported by the U.S. Air Force through the Air Force Office of Scientific Research of the Air Research and Development Command, under Contract No. AF18(600)-1113. Reproduction in whole or in part is permitted for any purpose of the United States Government.

Qualified requestors may obtain copies of this report from the ASTIA Document Service Center, Dayton 2, Ohio. Department of Defense contractors must be established for ASTIA services or have their "need-to-know" certified by the cognizant military agency of their project or contract.

ELECTROMAGNETIC WAVES ON CORRUGATED LINES:  
PROPAGATION CONSTANT MEASUREMENTS

Georges G. Weill  
Hans Kuehl

I. Introduction

In a previous report<sup>(1)</sup> an approximate formula for the constant of propagation has been derived from an exact integral equation. It is the purpose of this report to check experimentally the accuracy of our formula.

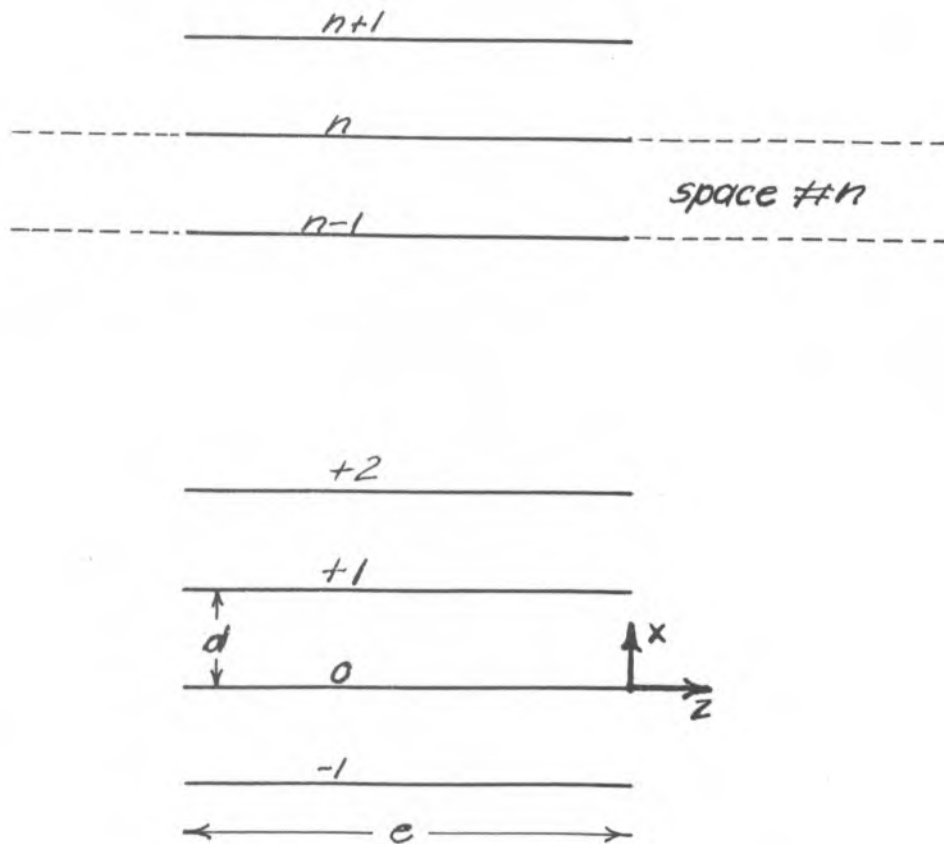


Figure 1.

<sup>(1)</sup>G. Weill, Propagation of Electromagnetic Waves along Corrugated Lines, (ASTIA Document AD115 049).

Let us recall first that the corrugated line under consideration is made of parallel "infinite" metallic strips. (Figure 1). The strips have length  $\ell$ , spacing  $d$ . They are supposed to be infinite in the direction of the axis  $y$ , and the line itself is infinite in the direction of the  $x$  axis. We are considering here the TM symmetric case  $(H_y, E_x, E_z)$ . With

$$H_y = u$$

$$E_z = \frac{1}{j\omega\epsilon} \frac{\partial u}{\partial x}$$

we defined the unilateral Fourier transforms:

$$\frac{1}{2\pi i} \int_{c-i\infty}^{c+i\infty} v(s) e^{sz} ds = \begin{cases} \frac{\partial u}{\partial x}(0, z) & z > 0 \\ 0 & z < 0 \end{cases}$$

$$\frac{1}{2\pi i} \int_{c-i\infty}^{c+i\infty} v(s) e^{-s(z+\ell)} ds = \begin{cases} 0 & z > -\ell \\ \frac{\partial u}{\partial x}(0, z) & z < -\ell \end{cases}$$

and we obtained the integral equation:

$$v(s) L_+^*(s) = \frac{1}{2\pi i} \int_{c-i\infty}^{c+i\infty} \frac{v(w) e^{-w\ell} dw}{(w+s) L_-^*(w)}$$

$L_+^*$  and  $L_-^*$  have been defined in (1).

A residue expansion gives us an infinite system of linear equations. Taking the first term of the first equation, the only significant one, we get:

$$e^{-\frac{ik_0 \ell}{2}} = \sqrt{\frac{d}{1 - \cos \gamma d}} \frac{L_+^*(ik_0)}{2i k_0}$$

Equating the arguments of both sides we get a relation

$$\ell = f(\gamma, d, k_0) .$$

Putting

$$\frac{k_0 d}{2\pi} = K \quad , \quad \frac{\gamma d}{2\pi} = \Gamma \quad , \quad \frac{2\pi \ell}{\lambda_0} = L$$

the relation becomes

$$L = F [K, \Gamma].$$

Curves have been drawn for

$$K = 1/10 \quad : \quad 10 \text{ strips per wavelength}$$

$$K = 1/3 \quad : \quad 3 \text{ strips per wavelength}$$

(See Figures 2 and 3.)

## II. Experimental Device.

For the sake of convenience, measurements have been made at microwave frequencies (S band). To measure the propagation constant of the surface wave we used a long "corrugated line". The length of the strips is great compared to their width. The launching of the surface wave is operated by means of a sectoral horn; the other end of the line radiates freely.

To avoid perturbation by the launching device or by end effects, measurements have taken place in the middle section of the line.

The experimental device is schematized on Figure 4 and represented in Figure 5.

### Equipment

UHF signal generator	HP model 616A
TWT amplifier	HP model 491A
Detector	HP model 415B
Slotted line	HP model 5810A
Variable attenuator	HP model S375 .

## III. Measurement Method.

We compare the phase of the wave propagated on the corrugated line with the phase of a reference wave propagated in a waveguide. The carriage of the slotted line is moved to get a zero on the detector. Then, any

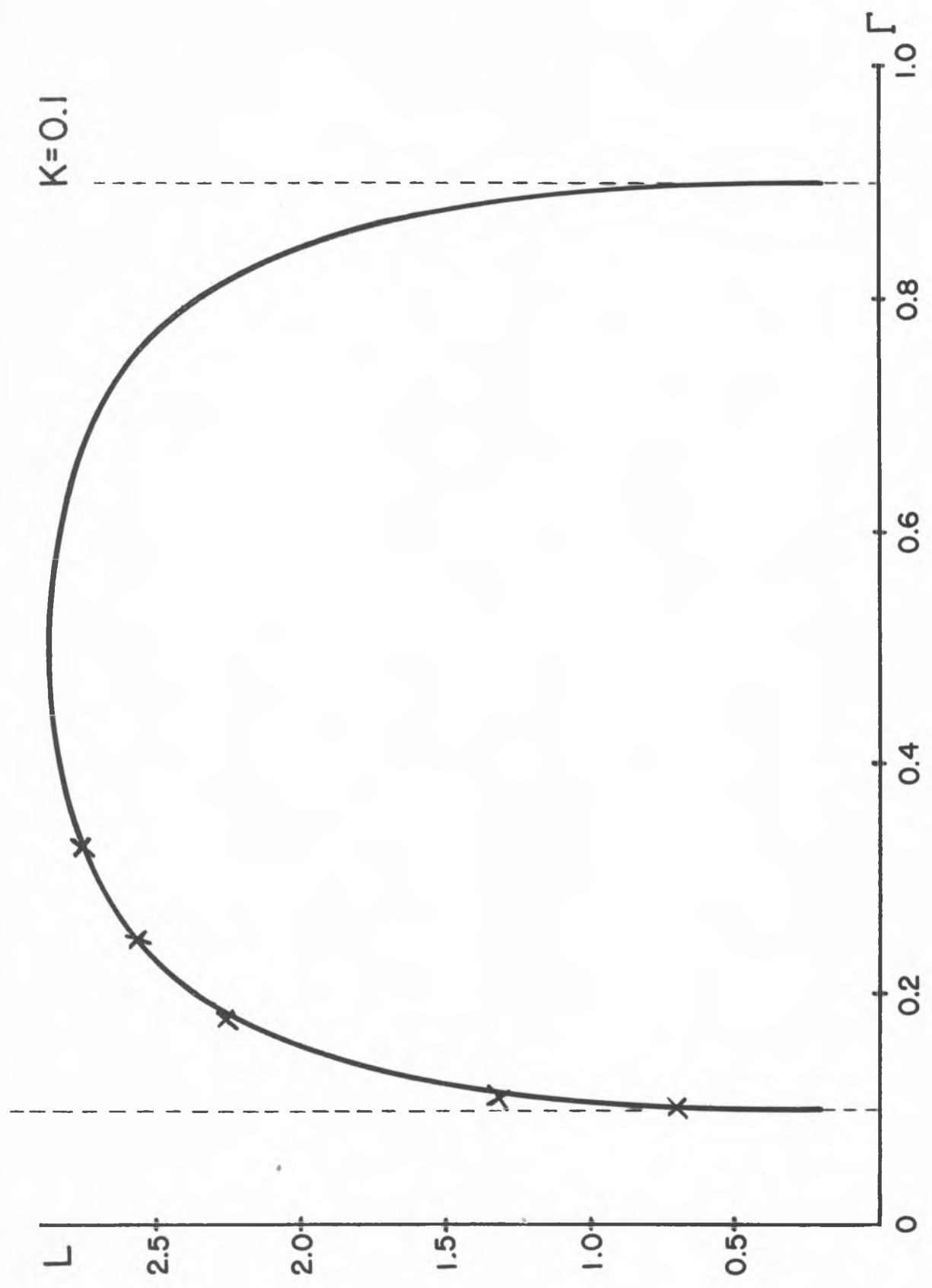


Figure 2.

SYMMETRIC CASE

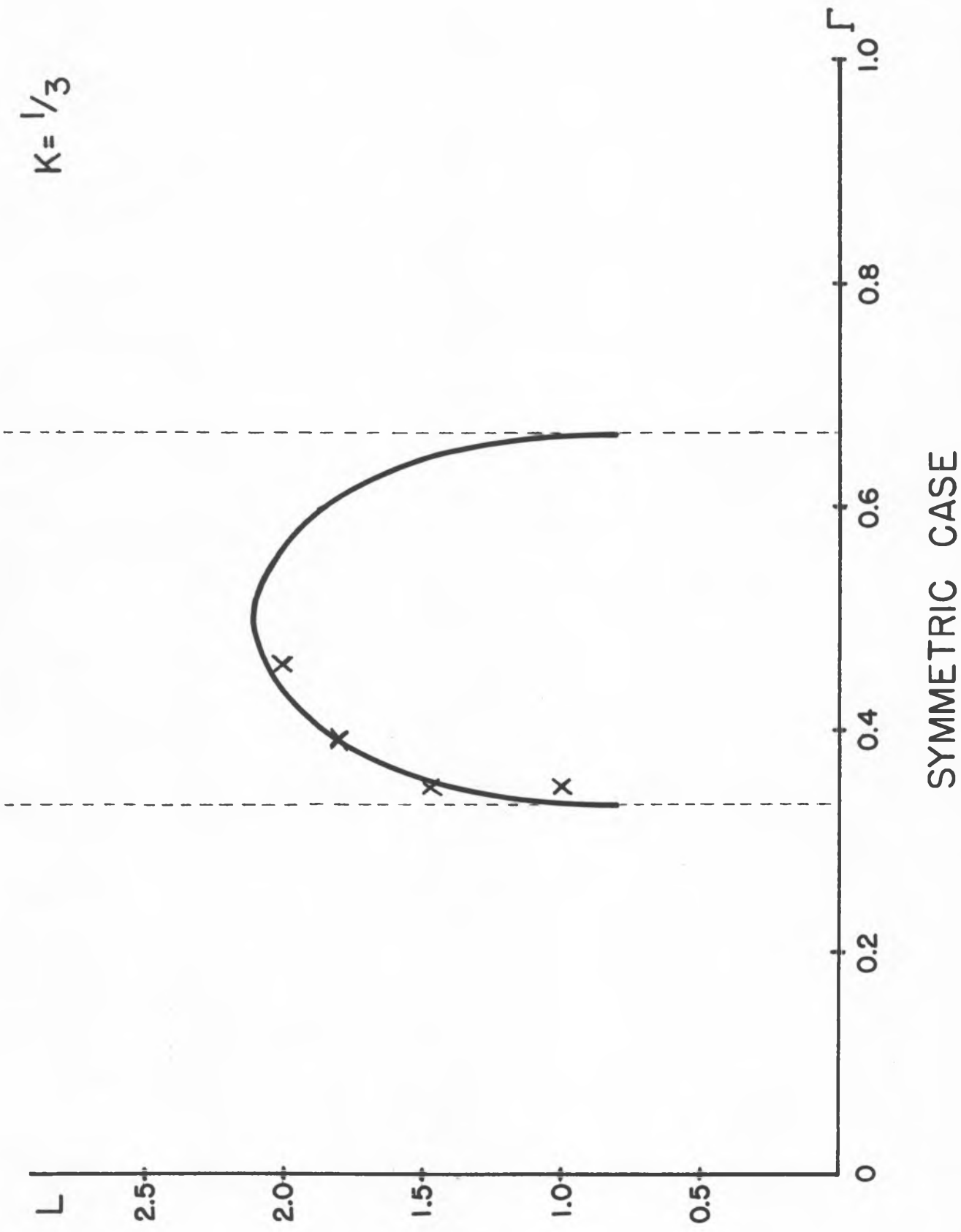


Figure 3.

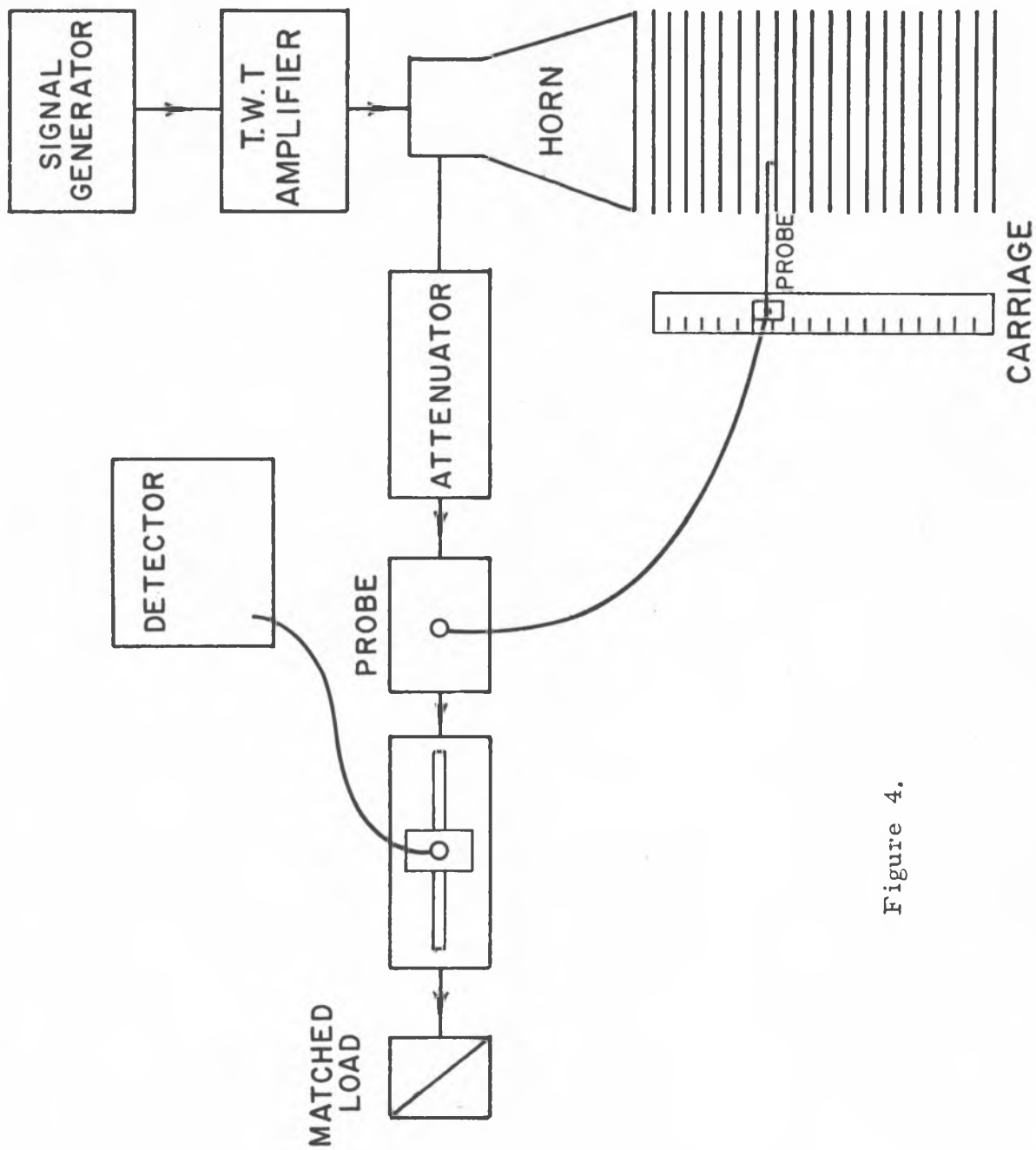


Figure 4.

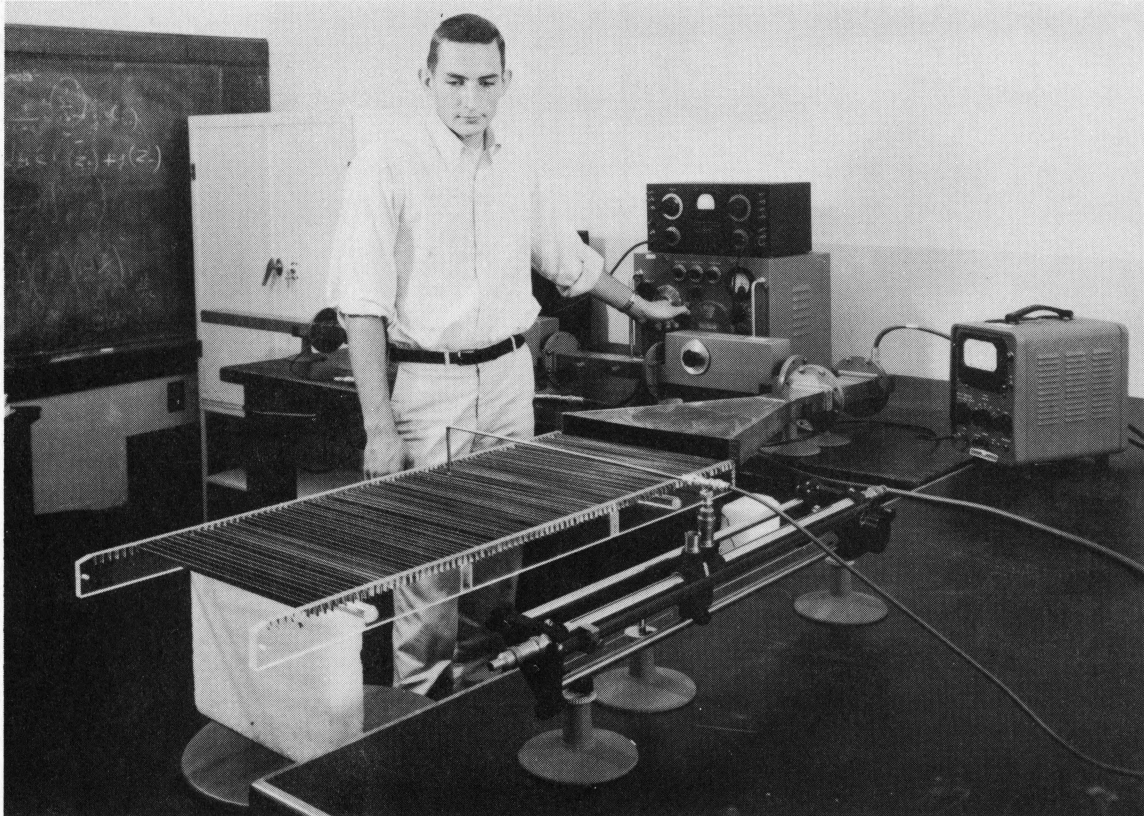


Figure 5



displacement of  $n \lambda_g$  ( $n$  integer;  $\lambda_g$  guided wavelength) of the probe gives us a zero on the detector meter.

The accuracy which can be expected from the method, taking  $n = 5$  is about 5% .

#### IV. Experimental Results.

To be able to use a smaller set of strips, measurements have been made at  $f_1 = 3000$  mc/s for  $K = 1/10$ , and  $f_2 = 3333$  mc/s for  $K = 1/3$ . The results, summarized in the following tables are represented on Figures 2 and 3, showing a very good agreement with the theoretical ones.

$$\underline{\underline{K = .1}} \quad d = 1 \text{ cm} \quad f = 3000 \text{ mc}$$

$\ell$ cm	L	$\lambda_g$ cm	$\Gamma_{\text{measured}}$	$\Gamma_{\text{theoretical}}$
1.10	.70	9.8	.10	.10
2.10	1.32	8.8	.11	.115
3.60	2.26	5.4	.18	.185
4.10	2.56	4.0	.25	.250
4.38	2.75	3.0	.33	.335
4.80	3.02	9.5		

$$\underline{\underline{K = 1/3}} \quad d = 3 \text{ cm} \quad f = 3333 \text{ mc}$$

$\ell$ cm	L	$\lambda_g$ cm	$\Gamma_{\text{measured}}$	$\Gamma_{\text{theoretical}}$
1.43	1.00	8.9	.35	.335
2.10	1.47	8.5	.35	.355
2.58	1.80	7.7	.39	.390
2.86	2.0	6.5	.46	.435
3.6	2.51	8.8		

We have checked points in the non-transmitting band of the structure. We get, as predicted, no guided wavelength but merely the primary excitation wave. (Points 4.80 and 3.6).

#### V. Conclusion.

The approximate formula for  $L = f[\Gamma, K]$  obtained from our integral equation shows a quite good agreement with experiment; now further approximation seems to be needed, at least for engineering purposes.

DISTRIBUTION LIST

<u>GOVERNMENTAL AGENCY</u>	<u>Copies</u>		
Commander Air Force Office of Scientific Res. Air Research and Development Comm. ATTN: SRY Washington 25, D. C.	5	Director, Research and Devel. Div. General Staff Department of the Army Washington 25, D. C.	1
Commander Wright Air Development Center ATTN: WCOSI-3 Wright-Patterson Air Force Base Ohio	4	Chief, Physics Branch, Div. of Res. U. S. Atomic Energy Commission 1901 Constitution Avenue, NW Washington 25, D. C.	1
Commander Air Force Cambridge Res. Center ATTN: Technical Library L. G. Hanscom Field Bedford, Massachusetts	1	U. S. Atomic Energy Commission Technical Information Service P. O. Box 62 Oak Ridge, Tennessee	1
Commander Rome Air Development Center ATTN: RCSST-4 Griffiss Air Force Base Rome, New York	1	National Bureau of Stds. Library Room 203, Northwest Building Washington 25, D. C.	1
Director, Office for Advanced Studies Air Force Office of Scientific Research Air Research and Development Command P. O. Box 2035 Pasadena 2, California	1	National Science Foundation 2144 California Street Washington 25, D. C.	1
Director, Office for Advanced Studies Air Force Office of Scientific Research Air Research and Development Command P. O. Box 2035 Pasadena 2, California	1	Director, Office of Ordnance Res. Box CM, Duke Station Durham, North Carolina	1
Commander, European Office Air Research and Development Comm. 47 rue Cantersteen Brussels, Belgium (Air Mail)	2	Office of Technical Services Department of Commerce Washington 25, D. C.	1
Chief, Document Service Center Knott Building Dayton 2, Ohio	10	Commander Arnold Engineering Development Center ATTN: Technical Library Tullahoma, Tennessee	1
Director of Research and Devel. Headquarters, USAF ATTN: AFDRD Washington 25, D. C.	1	Commander, Air Force Armament Center ATTN: Technical Library Eglin Air Force Base, Florida	1
Chief of Naval Research Department of the Navy ATTN: Code 420 Washington 25, D. C.	1	Commander, Air Force Flight Test Cen. ATTN: Technical Library Edwards Air Force Base, California	1
Director, Naval Research Laboratory ATTN: Technical Information Off. Washington 25, D. C.	1	Commander, Air Force Missile Test Cen. ATTN: Technical Library Patrick Air Force Base Cocoa, Florida	1
		Commander, Air Force Spec. Weapons Cen. ATTN: Technical Library Kirtland Air Force Base, New Mexico	1

GOVERNMENTAL AGENCY

11

Commander  
Holloman Air Development Center  
ATTN: Technical Library  
Holloman Air Force Base, New Mex.

1

Professor P. Kusch  
Radiation Laboratory  
Columbia University  
New York, New York

1

Office of Naval Research  
Branch Office London  
Navy 100, Box 39  
F.P.O. New York, New York

25

Dr. Donald E. Kerr  
John Hopkins University  
Department of Physics  
Baltimore 18, Maryland

1

PROFESSIONAL

Director  
Research Lab. for Electronics  
Massachusetts Inst. of Technology  
Cambridge 39, Massachusetts

1

Dr. D. W. Healy  
Electrical Engineering Dept.  
Syracuse U. Research Institute  
Syracuse 10, New York

1

Dean F. E. Terman  
Electronics Research Laboratory  
Stanford University  
Stanford, California

1

Dr. R. W. P. King  
Harvard University  
Cambridge, Massachusetts

1

Exchange and Gift Division  
Library of Congress  
Washington 25, D. C.

1

Professor E. Weber  
Microwave Research Laboratory  
Polytechnic Inst. of Brooklyn  
Brooklyn, New York

1

Professor E. M. Boone  
Dept. of Electrical Engineering  
Ohio State University  
Columbus 10, Ohio

1

Professor John Hoffman  
Dept. of Electrical Engineering  
University of Illinois  
Champaign, Illinois

1

Professor W. G. Shepherd  
Dept. of Electrical Engineering  
University of Minnesota  
Minneapolis, Minnesota

1

Technical Library  
Research and Development Labs  
Hughes Aircraft Company  
Culver City, California

1

Dr. R. G. E. Hutter  
Sylvania Electric Products, Inc.  
Sylvania Center,  
Bayside, L.I., New York

1

1/3/58