

Measurement Affecting Errors in Digital Image Correlation

V V Titkov^{1,a}, S V Panin^{1,2,b}

¹Institute of Strength Physics and Material Science SB RAS, Tomsk, Russia, ispms.ru

²National research Tomsk polytechnic university, Tomsk, Russia, tpu.ru

^atitkov.vladimir@gmail.com, ^bsvp@ispms.ru

Abstract. Optical full-field measurement methods such as Digital Image Correlation (DIC) are increasingly used in the area of experimental mechanics. The reliability for each measurement technique depends on the knowledge of its uncertainty and the sources of errors of the results. The aim of this work is to systemize the sources of errors related to digital image correlation (DIC) technique applied to strain measurements. The paper is concluded by some suggestions proposed in order to minimize the errors.

1. Introduction

Nowadays Digital Image Correlation (DIC) is widely spread optical technique for strain measurement. The technique was proposed by Peters et al. in the 1980s [1, 2]. It allows to carry our investigation of deformation and fracture processes of heterogeneous materials (metals, alloys, ceramics, polymers etc.) as well as makes it possible estimating mechanical state of loaded machine parts and structure components. Application of this method benefits on high resolution and sensitivity, and provides reducing manufacturing and operational costs of the instrumentation. The strain measurement in the DIC technique consists of two principal stages: determination of optical flow and subsequent computation of deformation components.

As a measurement method, the accuracy of DIC at strain calculation is of crucial importance. There are many error sources involved in the DIC measurement procedure, either originating from the experimental set-up or from the employed correlation algorithm, which bring in difficulties for the uncertainty quantification [3].

2. Errors affecting DIC measurements

It is of importance to distinguish between systematic error (displacement of the average, resulting in lack of accuracy) and random error (large standard deviation, resulting in lack of correctness/robustness) [4]. In fact, accuracy and robustness of the DIC measurements cannot be taken for granted if the measuring system and the numerical processing have not been optimized and validated [4]. The displacement and strain affecting errors are originally induced by the overall quality of the raw experimentally gained images. A DIC-computed displacement field is less sensitive to variation of calculation parameters (specified by the user), while their effect is larger computation the strain [5, 6]. Palanca M. showed [6] the importance of a careful optimization of the DIC software and hardware settings to minimize random and systematic errors. The settings that allowed minimizing the random errors were also associated with averaging over a larger area, and were therefore associated with poorer spatial resolution. Accuracy and robustness of the DIC-system in computing the displacements are in the order of 0.01 pixel [5, 7, 8]; however with some optimizations errors can be further reduced [9]. The



discrepancies between DIC evaluated displacements and specified ones have been statistically analyzed [8] in terms of random errors and systematic ones; in doing so they were correlated with the fractional part of the displacement component expressed in pixels. Main results are as follows: calculated displacement amplitude is almost insensitive to subset size, standard deviation of random error increases with enlarging noise level and decreases with enhancing subset size. However, the DIC formulations can be split up into two main families regarding displacement sensitivity to noise. For the first one, the amplitude of the latter increases with noising while it remains nearly constant against the subset size. In addition, for the first family, a strong dependence of random error with τ is observed for noisy images. DIC-computed strain values are generally quite accurate (systematic errors is of the order of few microstrains). Conversely, large noise usually largely affects DIC-computed strains: an accuracy of some hundreds of unit can be achieved only under optimal conditions [4].

The DIC analysis relies on the presence of a suitable pattern on the specimen surface [4]. In order to evaluate the errors related to its morphology, digital images of the speckle patterns were varied [10], numerically deformed [11], correlated in a zero-strain condition [12]. Inappropriately chosen speckle pattern is likely to make the correlation impossible at some patches (square-shape image regions), reducing the number of measurements points [10]. It is shown that the size of the speckles combined with the size of the used pixel subset clearly influences the accuracy of the measured displacements [11]. An optimal ratio exists between the patch size and the mean speckle size to reduce errors affecting DIC-computed displacements [11, 13]. They also showed that a limited scatter of speckle sizes yields more accurate displacement measurements, and that larger size dots ensures larger random errors in the constructed displacement field. The differences between black-on-white and white-on-black speckle patterns are negligible in terms of measurement quality [9]. A clear relationship exists between the measurement error and the uniqueness of the pattern, which depends on the speckle size and shape, and on the patch size [14]. Errors reduced with increasing number of speckles in the pattern, with enlarging speckle size providing a greater variation of shape, resulting in a lower error than patterns with smaller speckles. The airbrush airgun method provides a better detectability of the dots dimension as compared to the use of powder speckle [15]. Even if at a limited extent an airbrush airgun can be adjusted to produce the desired speckle dots [14], the performance of DIC stands quite robust and stable [16].

Images acquired by the digital camera are subjected to random errors affect, being induced by thermal noise (or dark noise), excess noise due to the CCD-sensor and electromagnetic noise of the relative measurement channel [17]. Moreover, a source of systematic error in 2D-DIC derives from out-of-plane displacements of the specimen during loading. That is why 2D-DIC is often chosen in investigations at the microscopic level [18, 19]. In practical applications, various unavoidable disadvantageous factors, such as small out-of plane displacement of the test object surface occurred during loading, small out-of-plane motion of the sensor target due to the self-heating or temperature variation of a camera, and geometric distortion of the imaging lens, may seriously impair or slightly change the originally assumed linear correspondence. In certain cases, these disadvantages may lead to significant errors in displacements and strains measured by 2D-DIC [19]. Suboptimal choice of the calculation parameters (specified by the user) can result in higher noise, or, conversely, could hide existing strain gradients [20]. The optimal parameters can be identified through virtually imposed displacement [10]. Numerically “deformed” images were prepared to evaluate the accuracy and robustness at constructing the displacement field, and identify the optimal parameters [16, 21, 22, 23].

3. Conclusions and recommendations to minimize measurement errors

It is required to validate DIC measurements by their comparison against independent measurements; in [7, 24, 25] the DIC-computed strains were compared against single strain gauges. A more extensive validation may include the use of specimens with known material properties, subjected to well-defined loading conditions [7, 24, 25]. Moreover, preliminary tests to identify the spatial displacements could help in avoiding out-of-plane artifacts in 2D-DIC measurements.

The quality of the applied random speckle pattern is of crucial importance. It exerts some influence on the correlation results [10]. A low quality speckle pattern results in no correlation at some mesh nodes

of the virtual grid. It also exerts certain influence on the accuracy at calculating correlation function. Using an optimized speckle pattern that can be printed directly on the surface of the sample is an efficient solution. Thus, the obtained speckle pattern will be independent of the operator and; hence the results would be more reproducible. To optimize the speckle pattern a factorial design to adjust the airbrush settings is proposed to form a pattern having the required average speckle element size with minimal scatter [7, 26, 27]. Paper [26] shows that it is possible to obtain a pattern with a highly controllable average and a limited scatter of speckle sizes, so as to match the ideal distribution of speckle sizes for DIC. Although the settings identified here apply only to the specific equipment being used; however this method can be adapted to any airbrush to produce a desired speckle pattern.

The lens distortion is responsible for a systematic error, which can be partially compensated through dedicated algorithms [28], or an appropriate calibration [29, 30]. A method of lens distortion correction was proposed [28] in order to improve the measurement accuracy of digital image correlation for 2D displacement measurement. The amounts of lens distortion are evaluated from displacement distributions obtained in a rigid body in-plane translation or rotation test. After detecting the lens distortion, its coefficient is determined using the method of the least squares. Then, the corrected displacement distributions are obtained. Such artefacts can be completely eliminated with telecentric lenses [19], or by exploiting the central portion of the lens angle [7]. An in-house smart solution consists in performing 3D deformation measurements with a single camera using a biprism to avoid distortion of the images [31, 32].

As shown by the test, the errors related to the variation of the lighting source may be of importance [10]. The illumination must be stable and uniform to reduce the noise and register better quality raw experimental images. Noise and its influence can be somehow reduced, but not completely eliminated, even with high-performance hardware (i.e. lenses, cameras, frame grabber, etc.) [4].

The main destination of the subset is to characterize the similarity between two patches while it depends on the speckle pattern [10]. When a subset size is too small it is likely to find wrong correlation due to the increase in the number of local minima of the correlation coefficient distribution. The increase of the subset size enhances the correlation. The increase of the subset size over a given dimension does not present a tangible enhancement of measurements quality. One should keep in mind that the increase of the subset size is synonymous to the increase of computation time. So the subset size should cover a given range and one may try several sizes for the subset to find its appropriate value that presents a good compromise between accuracy and computational time. It should be noticed that the subset size is closely linked to the dimension of the speckle pattern [10].

Filtering can also help reducing the noise in the DIC-computed strains. However, filtering should be used with extreme caution to avoid loss of information in high-gradient regions [33, 34]. A careful optimization of the entire measurement chain can reduce the errors and provide more accurate and precise outputs [7]. DIC is aimed to measuring displacements with very high accuracy and robustness. However, to obtain accurate and precise strain measurement data, it is required to take care of surface preparation, as well as finding appropriate hardware and software settings [4].

Acknowledgments

This work was supported by Russian Science Foundation under grant № 18-71-00087.

References

- [1] Peters W H and Ranson W F 1982 Digital imaging techniques in experimental stress analysis *Opt. Eng.* **21** 213427
- [2] Sutton M A, Wolters W J, Peters W H, Ranson W F and McNeill S R 1983 Determination of displacements using an improved digital correlation metho. *Image Vis. Comp.* **1** 133–39
- [3] Wang Y, Lava P, Reu P and Debruyne D 2015 Theoretical Analysis on the Measurement Errors of Local 2D DIC: Part I Temporal and Spatial Uncertainty Quantification of Displacement Measurements *Strain* **52(2)** 110–28
- [4] Palanca M, Tozzi G and Cristofolini L 2015 The use of digital image correlation in the

- biomechanical area: a review. *Int. Biom.* **3(1)** 1–21
- [5] Nicoletta D P, Nicholls A E, Lankford J and Davy D T 2001 Machine vision photogrammetry: a technique for measurement of microstructural strain in cortical bone *J. of Biom.* **34(1)** 135–39
- [6] Palanca M, Brugo T M and Cristofolini L 2015 Use of digital image correlation to investigate the biomechanics of the vertebra. *J. of mech. in med. and biol.* **15(02)** 1540004
- [7] Zhang D and Arola D D 2004 Applications of digital image correlation to biological tissues *J. of Biom. Optics.* **9(4)** 691
- [8] Amiot F, Bornert M, Doumalin P, Dupré J-C, Fazzini M, Orteu J-J, Poilâne C, Robert L, Rotinat R, Toussaint E, Wattrisse B and Wienin J S 2013 Assessment of Digital Image Correlation Measurement Accuracy in the Ultimate Error Regime: Main Results of a Collaborative Benchmark *Strain* **49(6)** 483–496
- [9] Barranger Y, Doumalin P, Dupré J C and Germaneau A 2010 Digital Image Correlation accuracy: influence of kind of speckle and recording setup *EPJ Web of Conf.* **6** 31002
- [10] Haddadi H and Belhabib S 2008 Use of rigid-body motion for the investigation and estimation of the measurement errors related to digital image correlation technique. *Opt. and Las. in Eng.* **46(2)** 185–96
- [11] Lecompte D, Smits A, Bossuyt S, Sol H, Vantomme J, Van Hemelrijck D and Habraken A M 2006 Quality assessment of speckle patterns for digital image correlation *Opt. and Las. in Eng.* **44(11)** 1132–45
- [12] Carriero A, Abela L, Pitsillides A A and Shefelbine S J 2014 Ex vivo determination of bone tissue strains for an in vivo mouse tibial loading model *J. of Biom.* **47(10)** 2490–97
- [13] Lecompte D, Bossuyt S, Cooreman S, Sol H and Vantomme J 2007 Study and generation of optimal speckle patterns for DIC *Pr. of the Ann. Conf. and Exp. on Exp. and Appl. Mech.* **3** 1643–49
- [14] Crammond G, Boyd S W and Dulieu-Barton J M 2013 Speckle pattern quality assessment for digital image correlation *Opt. and Las. in Eng.* **51(12)** 1368–78
- [15] Myers K M, Coudrillier B, Boyce B L and Nguyen T D 2010 The inflation response of the posterior bovine sclera *Acta Biom.* **6(11)** 4327–35.
- [16] Wang Y, Lava P, Coppieters S, De Strycker M, Van Houtte P and Debruyne D 2012 Investigation of the uncertainty of DIC under heterogeneous strain states with numerical tests *Strain* **48(6)** 453–62
- [17] Freddi A, Olmi G and Cristofolini L 2015 Experimental stress analysis for materials and structures: stress analysis models for developing design methodologies Springer International Publishing Switzerland p 498
- [18] Sutton M A, Yan J H, Tiwari V, Schreier H W and Orteu J-J 2008 The effect of out-of-plane motion on 2D and 3D digital image correlation measurements *Opt. and Las. in Eng.* **46(10)** 746–57
- [19] Pan B, Yu L and Wu D 2013 High-Accuracy 2D Digital Image Correlation Measurements with Bilateral Telecentric Lenses: Error Analysis and Experimental Verification *Exp. Mech.* **53(9)** 1719–33
- [20] Baldoni J, Lionello G, Zama F and Cristofolini L 2015 Comparison of different strategies to reduce noise in strain measurements with digital image correlation *J. of Strain Anal. for Eng. Design* **51(6)** 416–30
- [21] Lava P, Cooreman S, Coppieters S, De Strycker M and Debruyne D 2009 Assessment of measuring errors in DIC using deformation fields generated by plastic FEA *Opt. and Las. in Eng.* **47(7-8)** 747–53
- [22] Lava P, Cooreman S and Debruyne D 2010 Study of systematic errors in strain fields obtained via DIC using heterogeneous deformation generated by plastic FEA *Opt. and Las. in Eng.* **48(4)** 457–68
- [23] Lava P, Coppieters S, Wang Y, Van Houtte P and Debruyne D 2011 Error estimation in measuring strain fields with DIC on planar sheet metal specimens with a non-perpendicular camera

- alignment *Opt. and Las. in Eng.* **49(1)** 57–65
- [24] Sutton M A, Ke X, Lessner S M, Goldbach M, Yost M, Zhao F and Schreier H W 2008 Strain field measurements on mouse carotid arteries using microscopic three-dimensional digital image correlation *J. of Biom. Mat. Res. Part A* **86A(2)** 569–569
- [25] Gilchrist S, Guy P and Crompton P A 2013 Development of an Inertia-Driven Model of Sideways Fall for Detailed Study of Femur Fracture Mechanics *J of Biom. Eng.* **135(12)** 121001
- [26] Lionello G and Cristofolini L 2014 A practical approach to optimizing the preparation of speckle patterns for digital-image correlation *Meas. Science and Techn.* **25(10)** 107001
- [27] Lionello G, Sirieix C and Baleani M 2014 An effective procedure to create a speckle pattern on biological soft tissue for digital image correlation measurements *J. of the Mech. Beh. of Biom. Mat.* **39** 1–8
- [28] Yoneyama S 2006 Lens distortion correction for digital image correlation by measuring rigid body displacement *Opt. Eng.* **45(2)** 023602
- [29] Patterson E A, Hack E, Brailly P, Burguete R L, Saleem Q, Siebert T, Tomlinson R A, Whelan M P 2007 Calibration and evaluation of optical systems for full-field strain measurement *Opt. and Las. in Eng.* **45(5)** 550–564
- [30] Sebastian C and Patterson E A 2012 Calibration of a Digital Image Correlation System *Exp. Techn.* **39(1)** 21–29
- [31] Genovese K, Casaletto L, Rayas J A, Flores V and Martinez A 2013 Stereo-Digital Image Correlation (DIC) measurements with a single camera using a biprism *Opt. and Las. in Eng.* **51(3)** 278–285
- [32] Genovese K, Lee Y-U, Lee A Y and Humphrey J D 2013 An improved panoramic digital image correlation method for vascular strain analysis and material characterization *J of the Mech. Beh. of Biom.Mat.* **27** 132–142
- [33] Panin S V, Titkov V V, Lyubutin P S 2013 Efficiency of vector field filtration algorithms in estimating material strain by the method of digital image correlation *Opt., Instr. and Data Proc.* **49(2)** 155–63
- [34] Panin S V, Lyubutin P S, Eremin A V, Titkov V V, Chemezov V O 2017 Application of lucas-kanade algorithm with weight coefficient bilateral filtration for the digital image correlation method *IOP Conf. Series: Mat. Scien. and Eng.* 012039