

1 **Assessment of the reflectivity and emissivity impact on light metal roofs thermal behaviour, in**
2 **warm and humid climate.**

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9 **Abstract**

10 The light metal roof is one of the roof typologies most used in low latitude regions with warm and humid
11 climates. The low installation cost is one of the benefits of this typology, however, they offer only low
12 resistance to the heat flux. In order to analyse strategies to reduce the indoor overheating in this
13 climates, this investigation addresses the impact of reflectivity and emissivity on the light metal roof
14 thermal behaviour. The study was carried out with dynamic simulations, considering the climate of a
15 city in the south coast of Ecuador (Santa Rosa, 3°27'S). This analysis has parameterized the interior
16 surface temperature in function of the reflectivity and emissivity, which has been validated with the
17 measurements of several samples with different radiative properties. The analysed samples show that
18 the effect of the aging and the use of different paints have a higher impact on the increase in emissivity
19 than on reflectivity. In conclusion, the results show that the radiative parameter with the highest
20 influence on interior surface temperature reduction is emissivity.

21 **Keywords:** metal roof, solar reflectivity, thermal emissivity, warm and humid climates.

22 **1. Introduction.**

23 The regions located near to the equator are characterized by high temperatures, humidity and especially
24 high global solar radiation [1] [2]. Due to the angle of sun rays in this zone, the roof is the part of the
25 envelope most exposed to solar flux throughout the year. Despite solar paths being nearly the same for
26 different regions within these latitudes, cities that are located near the sea have a high relative humidity,
27 while cities farther away from the sea have less cloudy conditions [3] [4].

28 The importance of roofs on interior conditions depends on the urban context and the building
29 morphology [5] [6]. The constant and hasty growth of the world urban population in the last decades
30 has brought as a consequence a sharp increase of residential demand [7], and with it, the increase of
31 energy consumption, especially in low latitudes countries [8] [9]. In the cities of these regions, which
32 have adopted an urban sprawl model [10], the most extended building typology is the low rising building.

33 Hence, the roof surface represents 32% of the whole building envelope. As a result, the roof, within this
34 climatic and urban context, is the main source of heat gains (54%) in buildings of these regions, even
35 higher than window solar gains [11].

36 One of most the important parameters for the user interior thermal conditions is the mean radiant
37 temperature (T_{mrt}) [12] [13]. This parameter has a similar importance as the indoor air temperature
38 (T_a) on the user thermal perception [14]. Due to the high proportion of the roof with respect to the interior
39 space, the interior surface temperature of this element can determine T_{mrt} [15] [16].

Nomenclature

T_{mrt}	Mean radiant temperature
T_a	Outdoor air temperature
T_s	Exterior surface temperature
T_{si}	Interior surface temperature
MR	Light metal roof
MR_new	Metal roof in new state
MR_old1	Metal roof with 1 year installed
MR_old2a	Metal roof with more than 5 years installed (sample a)
MR_old2b	Metal roof with more than 5 years installed (sample b)
MR_old2c	Metal roof with more than 5 years installed (sample c)
MR_cool	Metal roof painted with cool roof paint
MR_white	Metal roof painted with white paint
MR_green	Metal roof painted with green paint

40

41 In regions at these latitudes, the most commonly used roof is the light metal roof (MR), as in Malaysia
42 [17], Indonesia [18], and especially in countries from Central and South America: Costa Rica [19],
43 Dominican Republic [20], or Ecuador. In the warm humid Region of this last country, 65% of the entire
44 residential buildings use this typology of roof [21]. A major benefit of this typology is the low installation
45 cost. However, due to its low thickness and its thermal properties, this roof has a low resistance to the
46 heat flux.

47 In order to reduce the overheating conditions in buildings of these regions, an analysis of the strategies
48 applied to the light metal roof (MR) is necessary. Among the parameters that modify the thermal
49 behaviour of the roof are the solar reflectivity and thermal emissivity of the surface material, where
50 especially the reflectivity factor has high repercussions on indoor overheating reduction [22] [23] [24]
51 [25]. The solar reflectivity refers to shortwave reflected by the roof (wavelengths inferior to 4 μm , nearly
52 50% of which in the visible spectrum and 50% in the near infrared), and, the thermal emissivity refers
53 to the long wave radiation emitted by the roof (wavelengths superior to 4 μm or far infrared) [5]. So, the
54 interior surface temperature (T_{si}) largely depends on the balance of these two fluxes. Nevertheless, the
55 aging and the exposition to the outdoor environment modify these a [26], which significantly influences
56 the thermal performance of the roof.

57 Therefore, this work deals with the thermal behaviour of the light metal roof (MR) in warm humid climate
58 of low latitude regions. The specific objective of this research is to evaluate the repercussions of
59 modifying solar reflectivity and thermal emissivity on this roof interior surface temperature (T_{si}).

60 **2. Methodology**

61 The method of this investigation was carried out in a three-step process. The first part consists of *in situ*
62 measurements of climatic factors and thermal parameters of a light metal roof (MR). The second part
63 focuses on the simulation of the roof thermal behaviour, using as input data all the parameters
64 measured before in the first part. In the last part, measurements of several samples of this roof typology
65 have been used to validate the results obtained in the simulations. Once the simulations have been
66 validated, conclusions can be drawn from these results.

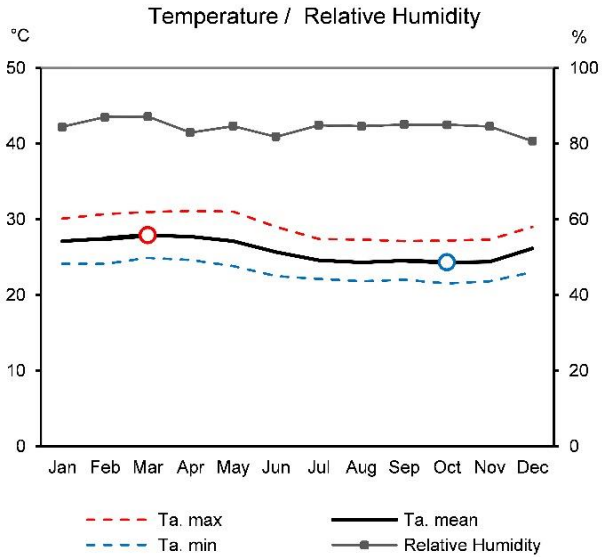
67 **2.1 Measurements of Input Data**

68 The measurement campaign was conducted in Santa Rosa, a city in the south coast of Ecuador, at
69 latitude 3°27'S and altitude 14masl. A total of 70% of residential buildings in this city are only one floor
70 high [21], and the most used roof material is the metal sheet as shown in Fig. 1.



72 Fig. 1 Aerial view (left) and street view (right) of Santa Rosa city in Ecuador. Images retrieved from
73 google maps.

74 This region is characterized by its warm-humid climate throughout the whole year. The mean
75 temperature is 26°C, with a daily and annual oscillation of 6°C and 4°C respectively; and the mean
76 relative humidity in the year is 85% as illustrated in Fig. 2.



77

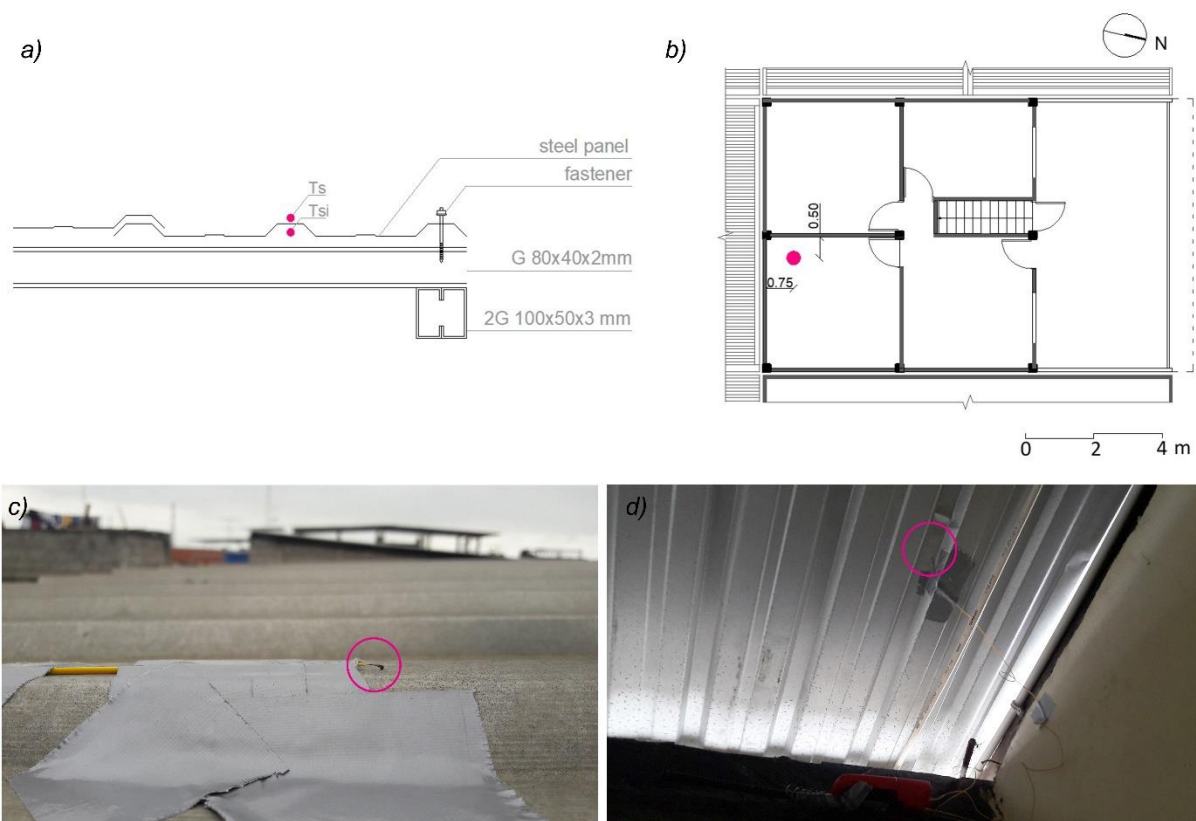
78 Fig. 2 Monthly average of: mean, maximum and minimum air temperature, and relative humidity of
79 Santa Rosa city-Ecuador. Data collected from meteorological station [27].

80 The climatic factors measured are: air temperature, humidity, air velocity, solar radiation, cloud cover
81 and sky temperature. Data measurements for all these factors, except sky conditions, were gathered
82 from a meteorological station (ID: IELOROEL2) located at 15 km from Santa Rosa (3°18'3''S,
83 79°53'53''O, 20 masl) [30]. The technical specification of the meteorological station corresponds to a
84 Davis Vantage Pro2 Plus (Wireless). These data were collected during the entire year 2016 in 15 min
85 intervals. With respect to sky conditions, the cloud cover factor, which is defined as the fraction of the
86 sky vault covered by clouds [28], was measured with the method of observation [29] [30]. In addition,
87 solar radiation with clear sky conditions has been simulated with the use of the software Heliodon [31].
88 The sky temperature measurements were carried out using an infrared thermometer TESTO 830 T4
89 with a range of -30°C to +400°C. Due to the fact that the sky is not uniform, the sky temperature was
90 measured in different points of the sky vault, from the skyline to the zenith. These measurements were
91 used to obtain an average of the sky temperature. The cloud cover and the sky temperature were
92 captured at 2 hours intervals during 7 days in October and December of 2016.

93 Based on statistical analysis of all the data collected in this year, climatic factors have been obtained of
94 a day that represents the mean extreme heat conditions in this region. Nevertheless, the whole data

95 obtained from these measurements are detailed in supplementary Table 1 and supplementary Table 2
96 in Ref [52].

97 The measured MR belongs to a residential building located in Santa Rosa city. The specific
98 characteristics of this roof correspond to a 0.3mm galvanized steel sheet and covered by an alloy of
99 aluminium and zinc (55%-45%) [32] [33]. According to the manufacturer and bibliography, this material,
100 in its original new state, has a solar reflectivity of around 0.75 and thermal emissivity of around 0.12
101 [34] [35] [36]. However this roof had been installed more than 5 years before the measurements, thus,
102 its current state is dusty and old but not rusted. Because of these circumstances, it is necessary to
103 measure the reflectivity and the emissivity of this roof in the current conditions, Fig. 3.



104
105 *Fig. 3 Light metal roof constructive detail (a), floor plan with the thermocouple position (b), outside (c)*
106 *and inside (d) surface temperature measurements.*

107 The measured roof parameters are the visible reflectivity, thermal infrared emissivity, as well as the
108 exterior (T_s) and interior surface temperature (T_{si}). The measurement methods of the reflectivity and
109 emissivity of this roof are based on previous works from [37] [38] [39] [40] and [41]. Due to the high
110 conductivity of the metal roof and its low thickness, the exterior and interior surface temperature are the
111 same. The same results were obtained in other studies [42] [43]

112 The process to measure the reflectivity consisted in comparing the MR surface with a reference surface
113 by capturing photographic images, which were taken at angles of less than 45° from the normal to the

114 surface to minimize the error of the measurements [38]. Each image was processed through a graphics
115 software (Adobe-Photoshop) [44] to obtain the optical histogram of the sample and the reference
116 surface. The reference surface used for this comparison was a sheet of 100% opaque white paper.
117 Assuming that the surface has a fully Lambertian reflection, the reflectance factor of this surface was
118 obtained through Eq. 1.

$$119 \quad r = \frac{\pi \cdot L}{E} \quad \text{Eq. 1}$$

120 Where r is the reflection factor, L is the luminance value (cd / m^2) and E the illuminance value (lux).
121 The values of L and E were obtained through measurements. The instruments used to measure the
122 parameters were a Light meter LX1010B lux meter, and a Konica Minolta LS 110 Luminance meter.
123 The solar reflectance obtained from the reference surface (white paper) was 0.85.

124 In order to measure emissivity, the process consisted of simultaneously measuring the exterior surface
125 temperature and exterior radiant temperature of the roof, using a multi-logger thermometer Amprobe
126 TMD 56 with a thermocouple type K, and an infrared camera (adjusted to an emissivity of 1.00),
127 respectively. Two infrared cameras were used for this process: a FLIR I7 and an InfRec H2640. In one
128 hand, the measurements were made *in situ* in Santa Rosa-Ecuador with the use of FLIR i7 infrared
129 camera. In order to validate the field results, additional measurements were carried out in the laboratory,
130 where the infRec H2640 has been used.

131 The taking of measurements with both cameras were made with angles lower than 45° with respect to
132 the normal to the surface. Then, using the software of these cameras (FLIR Tools, Infracore Analyzer
133 Lite), the radiant temperature (infrared camera) was equalized to the surface temperature
134 (thermometer) according to the change in the emissivity value. By achieving the equality of their
135 temperatures, the emissivity of this surface was obtained.

136 The emissivity measurement procedure was based on the standard Test Methods for Measuring and
137 Compensating for Emissivity Using Infrared Imaging Radiometers: contact thermometer method [41].
138 The apparent temperature was configured with an emissivity value of 1.00. The reflected temperature
139 was assumed as the sky temperature for measurements made *in situ*, as well as the air temperature
140 was set for laboratory measurements. Both measurements give quite similar emissivity values, with a
141 variation between them of less than 3%. The values used for the analysis of each sample were the
142 average of two measurements.

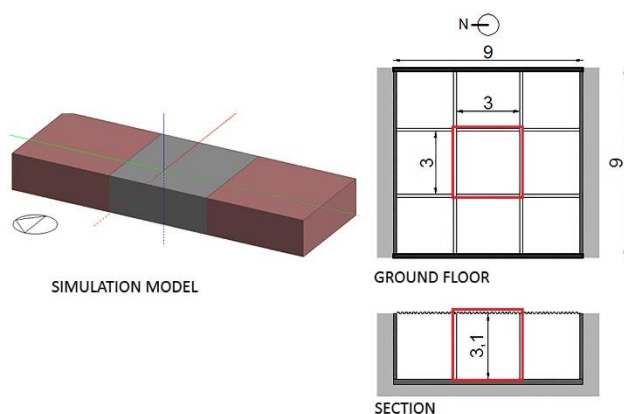
143 The interior and exterior surface temperatures were measured with the same multi-logger used to
144 measure the emissivity. The data was gathered in 10 min intervals during 10 days in October and 10

145 days in December of 2016. The purpose of these field measurements was the validation of the
146 simulated results.

147 **2.2 Simulations**

148 The second part of the methodology is based on dynamic simulations with the use of the Design Builder
149 interface [45], which uses Energy Plus as a calculation engine [46]. The EPW file (Energy Plus Weather)
150 used for these simulations were set by using the data collected in the measurements campaign carried
151 out in October and December (see supplementary Table 3 in ref [52]. From these simulations, one day
152 (October 10th) with the characteristics coincident with the day with mean extreme heat conditions from
153 the whole year was chosen to analyse. The purpose of choosing this day is to show the extreme effect
154 of the radiative properties of the light metal roof.

155 Furthermore, a simulation model has been established, where the roof thermal parameters were set
156 according to the values obtained in the measurements. Additionally, the geometry, materials, orientation
157 and urban typology of this model were configured based on the predominant characteristics in these
158 regions, where the low height floor is the predominant building typology, the use of light block is the
159 most used material for walls and the typical plot of land is 9m x 9m [47]. Following these characteristics,
160 the model is a one-floor residence of 9m x 9m x 3.1m height, attached to equal buildings by its North
161 and South sides. The model has been divided into 9 subzones (spaces), through a 3 x 3m grid. The
162 subdivision of this model resembles the buildings structural characteristics in these regions, where the
163 typical inter-columns distance is 3m. In order to avoid the influence of direct solar radiation, the model
164 does not include glass surfaces and only the central space has been evaluated, see Fig. 4. In regards
165 to the infiltrations and the occupation values were set according to the collected data in situ. Infiltrations
166 were approached by measuring CO₂ concentrations in a windowless room. The measurements were
167 taken by several hours, following the Tracer Gas process specified in [48]. The values obtained from
168 these measurements were confronted with the simulation software and were in agreement. All the
169 simulation parameters are shown in Table 1.



Roof	
Reflectivity	0.10 – 1.00
Emissivity	0.10 – 1.00
Thermal mass	0.65 kJ/m ² .K
Thermal transmittance	7.40 W/m ² .K
Walls-thermal transmittance	3.20 W/m ² .K
Floor-thermal transmittance	1.96 W/m ² .K
Occupancy	Constant 0.04 people/m ²
Infiltrations	Constant 0.7 ac/h
Ground Temperature	25.80°C

172

173 *Table 1 Simulation parameters*

174 Finally, with the use of the simulation model, the interior surface temperature of this roof has been
175 parameterized as a function of changes in the reflectivity and emissivity parameters.

176 **2.3 Validation**

177 The next part of this methodology is the validation of the simulation results. First of all, the radiative
178 properties from several samples of the light metal roof (MR) have been measured. After this, the surface
179 temperatures of these samples have been simulated. Finally, the surface temperatures of these
180 samples have been measured and compared with the simulated results.

181 The samples measured correspond, on the one hand, to roofs of this typology in their unpainted state
182 with different weathering, and on the other hand, to roofs with different paints coatings.

183 About the unpainted set, it has measured 3 different states of weathering: a sample in a new state
184 (MR_new), a sample with 1 year installed (MR_old1), and 3 samples with more than 5 years installed
185 (MR_old2a, MR_old2b and MR_old2c). Despite that the 3 oldest roofs have approximately the same
186 age, they belong to three different houses which were exposed to three different conditions of
187 weathering. These roofs were measured to have a larger number of samples to analyse the tendency
188 of radiative parameters influenced by the aging. MR_oldda corresponds to the metal roof of the measured
189 residential building.

190 While the painted set consists of: a sample with cool roof paint coating (MR_cool), a sample with white
191 paint coating (MR_white) and a sample with green paint coating (MR_green).

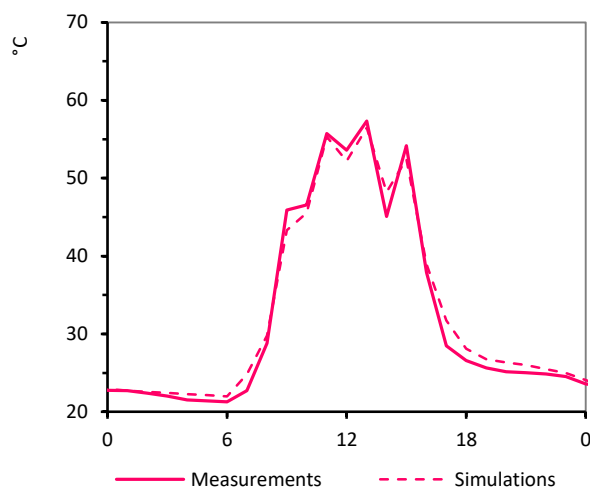
192 The reflectivity, the emissivity and the surface temperature of all these samples have been measured
 193 with the same methods and the same instrumentation as mentioned before. The specific characteristics
 194 of all measured samples are shown in Table 2.

Roof sample	Graphic code	Specifications	Real State
MR_new	○	Unpainted state	Clean
MR_old1	◉	Unpainted state	Dusty
MR_old2a	◐	Unpainted state	Dusty
MR_old2b	◑	Unpainted state	Dusty
MR_old2c	◒	Unpainted state	Dusty
MR_cool	◻	Cool Roof paint	Clean
MR_white	◻	White paint	Clean
MR_green	◻	Green paint	Clean

195

196 *Table 2 List of the all measured samples.*

197 The comparison between simulated data and the on-site measurements is shown in Fig. 5, which
 198 reveals that the maximum difference between them is 1.5°C out to $(T_{max} - T_{min}) = 36^{\circ}\text{C}$.



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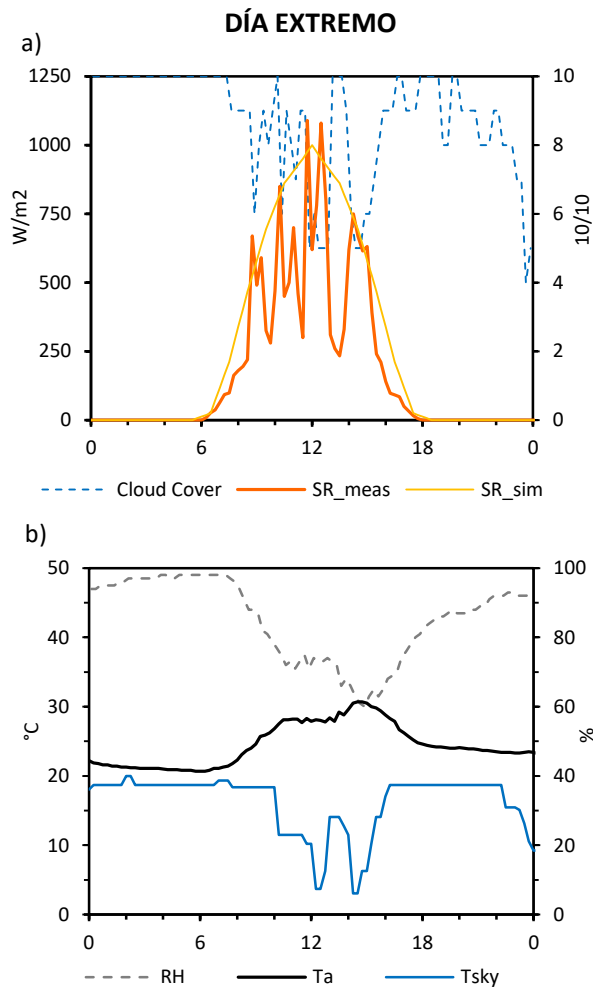
200 *Fig. 5 Interior surface temperature of the residential building metal roof obtained by measurements and*
 201 *simulations, during a day with extreme heat conditions in these regions.*

202 Finally, once the simulated results have been validated, the computation can be used to draw
 203 conclusions for this climate.

204 **3. Results and discussion**

205 **3.1 Measurements**

206 From the measured data, the climatic factors for a day with extreme heat conditions are shown in Fig.
207 6. According to all the data collected, this day represents 20% of the total number of days analysed in
208 this year. In addition, this figure shows the simulated solar radiation with clear sky condition, with the
209 purpose to evidence the high influence of the cloudiness on solar radiation.



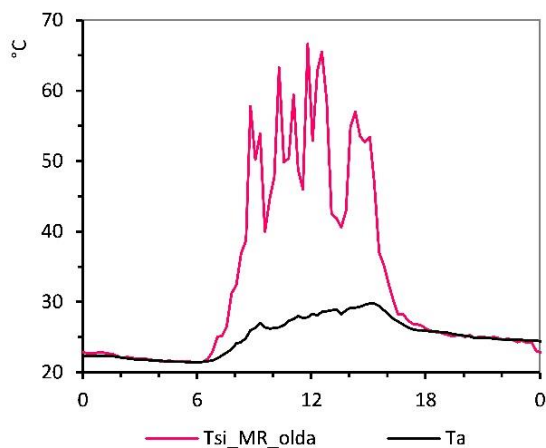
210

211 *Fig. 6 Climatic factors of a day which describe extreme heat conditions in this region, a) measured cloud*
212 *cover, measured global solar radiation and simulated solar radiation with clear sky conditions. b)*
213 *Relative humidity, outdoor air temperature and sky temperature.*

214 The results show a very inconstant and irregular measured solar radiation (SR_meas), which reflects
215 the cloudy sky conditions throughout the whole day. The peak solar radiation in this day is 1075 W/m²,
216 when the cloud cover is 5/10. However, when this sky condition increases to 10/10, at 13h30, the solar
217 radiation reduces to 230 W/m². Furthermore, according to these results, most of these measured values
218 are lower than simulated solar radiation values (SR_sim). This behaviour reveals the great influence of
219 cloud cover on the amount of solar radiation received.

220 Moreover, high levels of cloud cover are also shown during night-time. In the first night period (00h00 –
221 06h00), the sky is totally covered with 10/10. Although in the second night period (18h00 – 24h00) the
222 levels of sky cover are lower than in the first period, the average is still very high with 8/10. This climatic
223 condition directly affects the radiative cooling capacity of the sky, especially in this period. According to
224 Fig. 6b, the sky temperature, in both night periods, is around 18°C, among 3°C and 6°C below air
225 temperature. Meanwhile, in the day-time, the lowest sky temperature is 3°C, which coincides with the
226 lowest cloud cover in this period (5/10). According to these data, the difference between air temperature
227 and sky temperature is low, especially in the night period. Thus, the flux by long wave radiation emitted
228 to the sky is limited in this region.

229 Regarding the measurements of the roof parameters, the interior surface temperature of the residential
230 building roof (MR_oldda) is shown in Fig. 7. These results correspond to the chosen day with extreme
231 heat conditions. In order to put some reference parameter for the behaviour of the roof temperature,
232 this figure also shows the outdoor air temperature measured in this day (T_a). According to the radiative
233 properties measurements of this roof, its reflectivity is 0.52 and its emissivity is 0.30.



234
235 *Fig. 7 Measured interior surface temperature of the residential building metal roof ($T_{si_MR_oldda}$) and*
236 *measured outdoor air temperature (T_a) during a day with extreme heat conditions in these regions.*

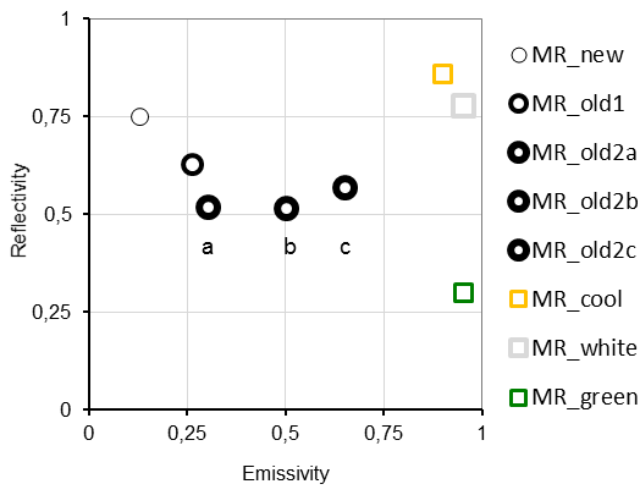
237 The interior surface temperature of the MR_oldda shows a behaviour very similar to the solar radiation
238 Fig. 6a, which reflects the high influence of this flux on the roof temperature. In the solar radiation peak,
239 MR_oldda reaches an interior surface temperature of 66°C, and when solar flux reduces to 230 W/m² (at
240 13h30), this temperature straightaway reduces to 40°C. Moreover, when the solar radiation disappears,
241 the temperature of MR_oldda is immediately reduced to the same temperature of the air (T_a), around
242 26°C. MR_oldda maintains the same temperature as air throughout the whole night-time. Due to the low
243 emissivity of this roof, in addition to the low cooling capacity of the sky, heat losses by long wave
244 radiation are minimal, and consequently, the interior surface temperature of the MR_oldda is not reduced

245 below T_a almost at any time, as it happens in other climates and other roofs with higher emissivity [49]
 246 [50] [51].
 247 Furthermore, the reflectivity and emissivity values of all measured samples are shown in Table 3, and
 248 Fig. 8.

Roof sample	Graphic code	Reflectivity	Emissivity
MR_new	○	0.75	0.13
MR_old1	◐	0.63	0.26
MR_old2a	◑	0.52	0.30
MR_old2b	◒	0.52	0.50
MR_old2c	◓	0.57	0.65
MR_cool	◻	0.86	0.90
MR_white	◻	0.77	0.95
MR_green	◻	0.25	0.95

249

250 *Table 3 Reflectivity and emissivity measured values of all samples*



251

252 *Fig. 8 Reflectivity and emissivity measured values of metal roof samples in its original state with different*
 253 *aging (circles), and metal roof samples with different paint coatings (squares).*

254 All the samples in their unpainted state with different weathering show a reduction in their reflectivity,
 255 with respect to the metal roof in its new state (MR_new). However, they also show an increase in their
 256 emissivity. The polished and smooth of the metal roof becomes a surface with higher roughness, due
 257 to the accumulation of dust and other chemical processes, thus, its emissivity is increased.

258 Samples with more than 5 years of installation (MR_old2a, MR_old2b, MR_old2c) present a reflectivity
259 reduction of 0.23, 0.23 and 0.18 respectively. However, the same samples show an emissivity increase
260 of 0.17, 0.37 and 0.52 respectively. In the case of MR_old1, the sample with only 1 year of installation,
261 have a similar behaviour: a reflectivity reduction of 0.12 and an increase in its thermal emissivity of 0.13.
262 According to these results, the general effect of aging on the light metal roof has a higher impact on the
263 increase of its emissivity than on the reduction of its reflectivity. The highest reflectivity reduction is 0.23,
264 from 0.75 to 0.52, while, the highest emissivity increase is 0.52, from 0.13 to 0.65. Based on the data
265 analysed, the average relation between the reflectivity decrement and the emissivity increment is 1:1.6.
266 In regard to the samples with paint coating, the results show that painting the metal roof changes
267 significantly its radiative properties with respect to all samples in their original state. In comparison to
268 the metal roof in its new state (MR_new), the reflectivity can change in both ways, while the emissivity
269 only increases.

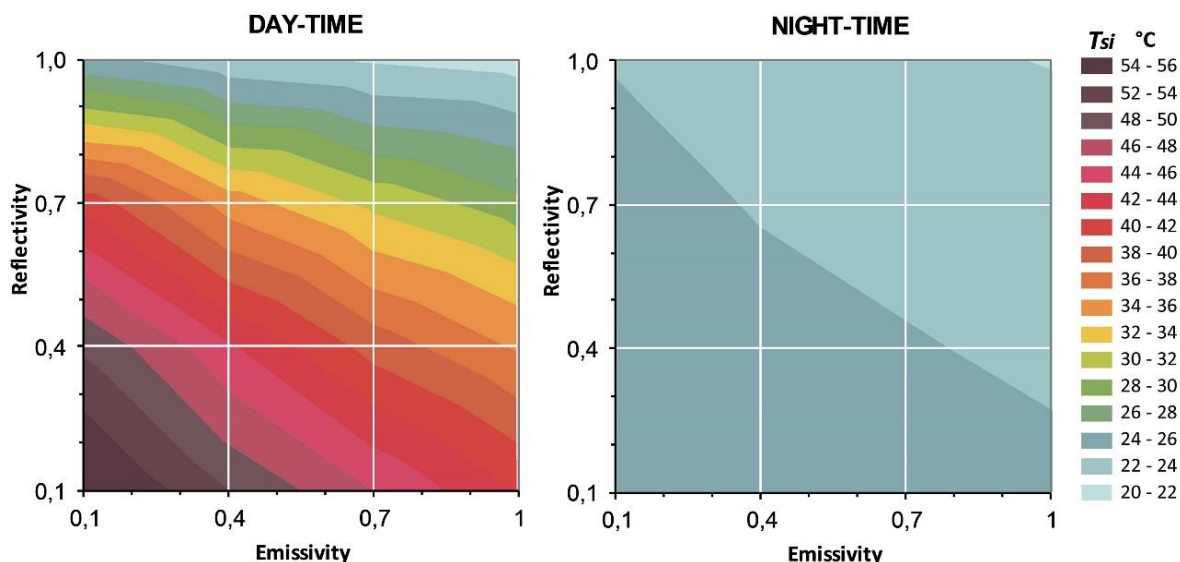
270 MR_cool and MR_white show an increase in both factors, in their reflectivity 0.11 and 0.03, and in their
271 emissivity 0.77 and 0.82 respectively. MR_green shows a reflectivity reduction of 0.50, and an
272 emissivity increase of 0.82. According to these results, the paint coating on the metal roof has a low
273 impact on the increase of its reflectivity, however, it shows a high repercussion on the increase of its
274 thermal emissivity.

275 The thermal response of the radiative parameters of these two samples set is discussed in a later
276 section.

277 **3.2 Simulations**

278 Once the EPW file was set according to climatic data of the chosen day, and the roof parameters were
279 configured agreeing to the measurements, the interior surface temperature of the metal roof (T_{si_MR})
280 has been parameterized in function of the reflectivity and the emissivity as presented in Fig. 9. This
281 figure uses a colour scale to represent the behaviour of the T_{si_MR} . Every colour band indicate a
282 common area of temperature "isotherms". Every isotherm represents an interval of 2°C. The Y-axis
283 shows the values of the reflectivity, and the X-axis shows the values of the emissivity. The range of
284 both parameters goes from 0.10 to 1.00. According to this representation, the lowest temperatures are
285 represented with cyan colours in a range of 20-22°C, and the highest temperatures are represented by
286 the purple colour in a range of 54-56°C. The results have been divided into two periods: day-time and
287 night-time, thus, the T_{si_MR} has been analysed with the average in every period. Due to the geographic
288 location of this city (near latitude 0°) both periods have the same number of hours throughout the year,

289 12h. Daytime lasts from 06h00 to 18h00 and night time comprises two semi-periods from 00h00 to
 290 06h00 and 18h00 to 24h00. The same colour scale is used for both periods.



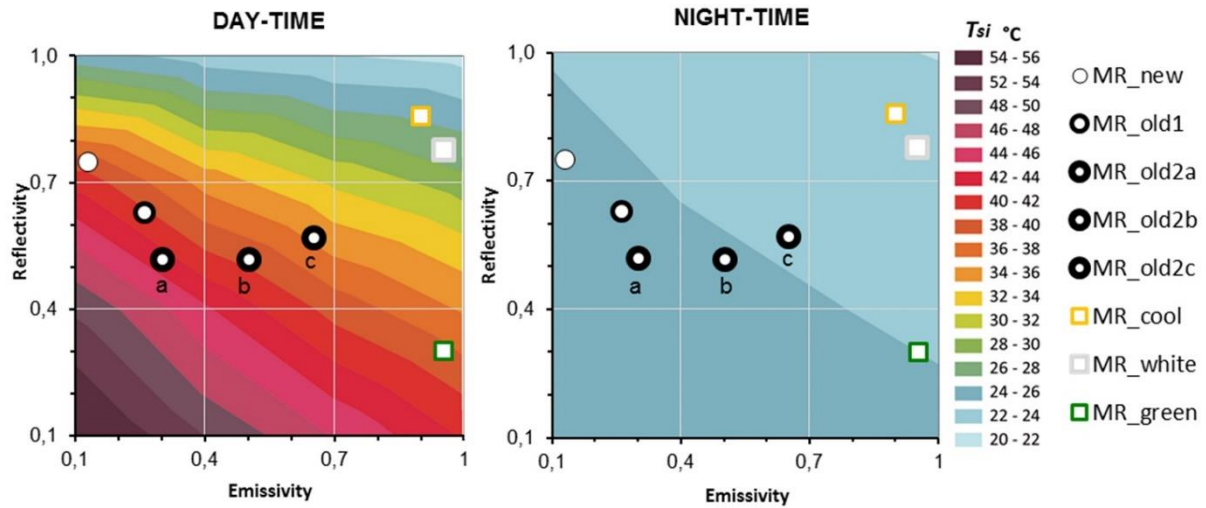
291
 292 *Fig. 9 Parameterization of T_{si_MR} in function of the reflectivity and emissivity, in day and night-time*
 293 *period.*

294 During day-time, both radiative parameters show a large influence on T_{si_MR} . The maximum variation
 295 is 36°C, between the lowest ($r=0.10$ $e=0.10$) and the highest ($r=1.00$ $e=1.00$) values of both parameters.
 296 Nevertheless, the reflectivity has a greater impact on this variation than emissivity. On the one hand,
 297 the increment of the reflectivity from 0.10 to 1.00, with the lowest emissivity 0.10, represents a
 298 temperature reduction of 32°C. The reflectivity impact on T_{si_MR} is less important according to
 299 emissivity increase. The increase of the reflectivity from 0.10 to 1.00, with the highest emissivity 1.00,
 300 shows a temperature reduction of 22°C. On the other hand, the increment of the emissivity from 0.10
 301 to 1.00 only represents a temperature reduction of 12°C and 6°C, with the lowest and highest reflectivity
 302 value (0.10 and 1.00) respectively.

303 On the contrary, in the night period, the influence of the reflectivity and emissivity on T_{si_MR} is minimal.
 304 This time, the maximum variation is only 4°C, between the lowest ($r=0.1$ $e=0.1$) and the highest ($r=1.00$
 305 $e=1.00$) values of both parameters. In spite of the absence of solar flux in this period, the reflectivity
 306 factor shows some impact on T_{si_MR} . This is because of the heat stored within the indoor space.
 307 Additionally, in this period, the emissivity is the only parameter that has a direct influence on the roof
 308 balance, however, due to the low cooling capacity of the sky, the impact of this factor on the reduction
 309 of T_{si_MR} is minimal, even with high values.

310 **3.3 Measured thermal response of roof radiative parameters**

311 The thermal response (T_{si}) of the radiative parameters of all the samples analysed before (see Fig. 8)
 312 has been visualized with the isotherms graph, as seen in Fig. 10. These results were validated with the
 313 temperature of every sample obtained by measurements. All samples are going to be analysed in
 314 comparison to the sample in its new state.



315
 316 *Fig. 10 The thermal response (T_{si}) of the radiative parameters of all analysed samples: metal roof*
 317 *samples in its original state with different weathering (circles), and metal roof samples with a coating of*
 318 *paint (squares).*

319 With respect to the samples in their unpainted state with different weathering, during day-time, the T_{si}
 320 of the sample in its new state (MR_new) is 39°C, while for the sample with one year of installation
 321 (MR_old1) the T_{si} is 40°C, and for the samples with more years of use (MR_old2a, MR_old2b,
 322 MR_old2c) the T_{si} is 43°C, 39°C and 35°C respectively. While for night-time, all samples have a
 323 temperature slightly higher than 24°C, with the exception of MR_old2c which is below 24°C.

324 According to these results, the metal roof with the lowest temperature in both periods is the sample with
 325 the highest value of emissivity, (MR_old2c), which is one of the samples with more years of installation.
 326 The temperature of this sample is even lower than the metal roof sample in its new state (MR_new),
 327 which has a higher reflectivity but a lower emissivity. Even MR_old2b, one of the sample with the lowest
 328 reflectivity but with an emissivity of 0.52 has the same temperature as MR_new. In the case of MR_old1
 329 and MR_old2a, due to they have the lowest emissivity increase, their temperatures show an increase
 330 compared to MR_new. Nevertheless, these temperatures are only 1°C and 3°C higher than MR_new
 331 respectively.

332 In consequence, since the effect of the aging has a greater impact on the emissivity increase than on
 333 the reflectivity reduction, the metal roofs with several years of use tend to have similar temperatures

334 than these roofs in their new state, and eventually, in function on the increase of their emissivity, they
335 show a lower temperature.

336 Regarding the samples with different paint coatings, during day-time, the white painted sample
337 (MR_white) has an interior surface temperature of 27°C, while the cool roof painted sample has a
338 temperature of 26 °C, and the green painted sample of 36.5°C.

339 According to these results, the roofs with the lowest temperatures of all the analysed samples in both
340 periods are MR_cool and MR_white. Due to their increased of reflectivity and especially emissivity, in
341 comparison to the metal roof in its new state, these samples have a temperature of 16°C and 14°C
342 lower than MR_new respectively. Even, with a lower reflectivity, MR_green has the same temperature
343 as MR_new during day-time and a lower temperature during night-time, due to the high increase of its
344 emissivity.

345 In consequence, since the use of paint coating on light metal roofs has a large impact on the emissivity
346 increment, these samples tend to have a lower temperature in comparison to the roofs in their new
347 state, even when using paints with lower values of reflectivity.

348 Based on the analysed samples, the greatest impact on the reflectivity reduction due to the aging is by
349 0.23, from 0.75 down to 0.52, which represents a temperature increment of 4°C, while, the greatest
350 impact on the emissivity increasing is by 0.52, from 0.13 up to 0.65, which results in a temperature
351 reduction of 12°C. Furthermore, the changes caused by the use of paint show a maximum reflectivity
352 increase of 0.11, from 0.75 up to 0.86, which represents a temperature reduction of 8°C. While, the
353 maximum emissivity increase is 0.82, from 0.13 up to 0.95, which results in a temperature reduction of
354 14°C.

355 Although the general parametric analysis shows that the reflectivity has greater repercussions on the
356 roof thermal behaviour than emissivity, the results of both samples set show that the emissivity stands
357 out as the radiative parameter with the highest impact on the T_{si} reduction of the MR.

358 **4. Conclusions**

359 The central scope of this research has been the thermal behaviour of light metal roofs in latitudes near
360 to Equator with warm and humid climates. This roof typology has been widely disseminated in these
361 regions despite of the general opinion is that it provides a high indoor overheating. This investigation
362 has been developed from the radiative perspective, considering both the short wave radiation and the
363 long wave radiation. In order to accomplish the aim of this investigation, a set of results have been
364 obtained through simulations based on measurements carried out in a city on the coast of Ecuador.

365 The simulations have been validated with further measurements of several samples of this roof
366 typology. From these results some conclusions can be mentioned:

367 The reflectivity and emissivity have large repercussions on the light metal roof interior surface
368 temperature during day-time, while, during night-time, the influence of these radiative parameters is
369 minimal. Due to the low cooling capacity of the sky in this region, even the maximum increase in
370 emissivity has a minimal impact on the interior surface temperature reduction during the night period.

371 Finally, contrary to what is generally believed, a light metal roof with low reflectivity and high emissivity
372 tends to have a lower temperature than a roof in its new state. Even, an old roof with high emissivity
373 may have a lower surface temperature than a new roof, apparently more reflective to sunlight.
374 Therefore, since the capacity of the light metal roof to increase its emissivity with the use of simple
375 methods such as common commercial paints or its own aging, make this type of roof a viable option in
376 construction in climates similar to the studied in this research.

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