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# Adjustment of Bracket Position Away From the Andrew's Plane to Achieve a Flat Occlusal Plane

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# Adjustment of Bracket Position Away From the Andrew's Plane to Achieve a Flat Occlusal Plane

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Thesis submitted to School of Dentistry, Department of Orthodontics at West Virginia University

in partial fulfillment of the requirments for the degree of

Master of Science in Orthodontics

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# ABSTRACT

# "Adjustment of Bracket Position Away From the Andrew's Plane to Achieve a Flat Occlusal Plane."

#### Dr. Jason Lawrence

**Background**: "The Six Keys to Normal (Optimal) Occlusion" published by Andrews in 1972 identified six common features characteristic of an optimal occlusion. Among these characteristics are flat maxillary and mandibular occlusal planes. Andrews further developed the Straight-Wire Appliance<sup>™</sup> to facilitate attaining an optimal occlusion in an efficient manner with few if any arch wire bends. In addition to the Six Keys, Andrews proposed that attaining a flat occlusal plane with a straight arch wire is predicated on siting the bracket slots on the FA Points of the tooth crowns (Andrews Plane). Observation of the maxillary and mandibular Andrews plane will reveal that these two planes diverge when both occlusal planes are levelled. This may be attributed to a proportional height discrepancy between the tooth crowns; which requires an adjustment to the sited vertical position of the slots on certain tooth crowns.

**Objective**: The purpose of this study was to investigate if there is a need to adjusted the FA Points on certain maxillary and mandibular tooth crowns to permit a flat parabolic shaped arch wire to produce level slot alignment and a flat occlusal plane. Correlations between the tooth crown heights and FA Point discrepancies were also analyzed.

**Materials and Methods**: Casts of twenty patients were scanned and virtually treated using software (ORTHO INSIGHT 3D version 6.0.7036, Motionview Software, LLC). Crown heights of all maxillary and mandibular teeth were digitally measured and recorded. Each sample case was treated virtually to precise level slot alignment with the brackets sited on the FA Points as defined by Andrews. A second treatment was virtually completed on these cases where a flat occlusal plane was not attained with the initial virtual treatment. Bracket positions were adjusted vertically as needed on certain tooth crowns to permit level slot alignment and a flat occlusal plane. The required height adjustment required to attain level slot alignment were recorded as a + or - vertical height discrepancy between Andrews FA Point and the "adjusted FA Point". Normative statistics was generated for all tooth heights, FA Points, and FA Point discrepancies. Correlations analyses were performed between tooth crown heights, FA Points, and FA Point discrepancies.

**Results and conclusions:** Mx centrals will likely require an adjustment to the incisal edge of at least 0.5mm (avg.=1.23 p=<0.0001) Mx laterals will show a positive correlation with crown height and incisal adjustment though not likely to require a change greater than 0.5 mm(avg=0.43mm p=. Md incisors will require an adjustment greater than 0.5mm (laterals avg =0.77mm p=0.0001 centrals avg=0.87mm p=<0.0001) Proclination of lower incisors do not yield a significant change from previously discovered adjustment (lateral avg= 1.34mm p=<0.0001 central avg=1.04mm p=<0.0001) retroclining lower incisors requires no significant adjustment from FA (lateral avg=-0.23mm p=<0.0001 central avg=-0.27mm p=<0.0001 all other teeth found no significant need for occlusal or gingival adjustment.

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# Chapter 1: Introduction Background:

Dr. Angle was one of the first dentists to develop appliances that applied forces to the dentition in an attempt to correct for crowding and mal occlusions; he developed a number of different mechanisms until he finally landed on the Edgewise appliance. After Dr. Angle began the process of developing treatment techniques two main philosophies dominated the orthodontic world, Begg light wire and Tweed edgewise. These two philosophies were developed for an almost exclusively non extraction technique that followed in the same line of thought as Angle's.<sup>20</sup>

With the traditional edgewise appliance brackets were placed at a determined position from occlusal or incisal edges of the dentition. Any discrepancy in height, prominence, angulation, or inclination was corrected with first, second, and third order bends. This made for a highly effective yet subjective, tedious, and inefficient application of the art and science of orthodontics. The edgewise appliance remained unchanged for several decades until the work of Dr. Andrews approached the concept of using a twin bracket from a new perspective and built on the idea of the partially programmed appliance.<sup>20</sup>

Larry Andrew's straight wire appliance (SWA) is often compared to Angle's edgewise appliance, or considered a variation of the edgewise appliance. This comparison is a bit flawed because the edgewise appliance relied on the practitioner to impose the proper tip, torque, angulation, rotation, and prominence. The brackets of the Edgewise appliance are universal; meaning no regard for specific teeth is given to the selection of a bracket. By contrast the SWA contains customized brackets for each tooth type, pre angulation slots that impose proper

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angulation to the tooth if the bracket is sited squarely on the facial surface, bases of these brackets are contoured occlusogingivally and mesiodistally to allow for proper fit to the facial axis point on the labial surface of each tooth, bases of the brackets are angulated so as to communicate proper tip/torque to each tooth, and bracket bases are designed uniquely to impart proper prominence. Outside of the twin bracket design, use of an edgewise wire, and the rectangular slot very little similarities with traditional edgewise appliances exist.<sup>3</sup> The SWA has become so prominent that nearly every orthodontist in the world now uses some variation of the appliance.

The fully programmed nature of the SWA requires that the prescription be expressed from the same location on every tooth known as the Facial Axis (FA) point.<sup>3</sup> the FA point lies on a plane that is similar to, but not exactly parallel to the occlusal plane of each arch *(fig. 1)*. This results in two Andrews planes, one for each arch. These planes diverge from each other as they travel anteriorly.



Fig.1 Illustration of properly positioned brackets on Facial Axis points. Notice that the occlusal planes converge anteriorly allowing for the Andrews planes to assume a parallel orientation. Ideally, if one places a preprogrammed bracket on the Facial Axis (FA) of any tooth such that the bracket is properly assigned to its predetermined tooth, no need for extractions exist, the transverse dimension is correct, and all crowding can be resolved with expression of the prescription, then an occlusion will result that satisfies the Six Keys to an optimal occlusion and all brackets will eventually lie on the Andrews plane of their respective arch.

### The Problem

As with all aspects of anatomy, human dental anatomy is highly variable and often deviates from prescribed normal forms. While Andrews' appliance is built with room within the bracket slot to account for anatomical changes, sometimes the changes are greater than for which may be accounted. Andrews himself postulates that the idea of the preprogrammed appliance adheres to the theory of centrality<sup>3</sup>. The theory of centrality states that the majority of individuals will occupy the greatest area under a bell curve. It is reasonable to assume that the majority of all patients will fall within the so called central tendency of anatomy and not require any deviation from bracket position espoused by Andrews. To the patient or parent who does not fall within the central portion of the bell curve, incidence or rarity of their morphology is irrelevant. Proper treatment and acceptable smile aesthetics must remain a treatment goal. Deviations from normal may include peg laterals, labial prominences being located far more incisally or gingivally in the instance of incisors, excessive labial curvature particularly of mandibular first premolars, maxillary incisors that are significantly longer than the posterior dentition with either the incisors deviating from normal or the molars and premolars having insufficient crown height, or any other not yet considered variation. These conditions should not be considered abnormal but rather a variation on normal owing to the presence of these variations in McLaughlin's bracketing study.<sup>18</sup> Placement of brackets solely on the Facial Axis point may not result in a

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leveled Curve of Spee. When such a discrepancy is present, especially since the maxillary and mandibular Andrews planes can be observed to diverge when the occlusal planes of the respective arches are level, or there remains a Curve of Spee maintained on the lower arch and an reverse curve on the upper arch, An adjustment to the bracket location must be employed to account for this naturally occurring discrepancy. This exploration chooses to focus on innate height discrepancy between posterior and anterior dentition. To date, no study has examined whether a deviation from the ideal FA point on the clinical crown is acceptable or even desirable.

#### Glossary

- Curve of Spee: the curvature of the mandibular occlusal plane beginning at the tip of the lower incisors and following the buccal cusps of the posterior teeth, continuing to the terminal molar.
- Facial Axis of the Clinical Crown(FACC): the long axis of any tooth that is centered mesio-distal on the facial surface of the clinical crown. Exeptions are the molars where the FACC is defined as the line running down the buccal groove of the clinical crown.
- Facial Axis Point(FA): the midpoint of the FACC that is meant as the optimal location for bracket placement.
- Occlusal plane: a plane passing through the occlusal or biting surfaces of the teeth. It represents the mean of the curvature of the occlusal surface. Also called biteplane.
- Andrews Plane: a plane created by the FA points of a level arch. One plane exists for the mandible and one for the maxilla. These planes may or may not be level with the occlusal plane

### Goals

- Determine average heights of clinical crowns that exhibit a height discrepancy from posterior to anterior
- Determine if vertical proportion of dentition should affect bracket positioning.
- Evaluate proper bracket position in the presence of an increase vertical dimension of the anterior dentition in relation to the posterior dentition.
- Determine a predictable technique for determining proper bracket position outside of clinical judgment.

## Limitations

- Human error in construction of ideal occlusal planes
- Computer distortion of scanned casts
- Lack of consensus on ideals for perfect dentition concerning angulation and inclination
- Prescription will be expressed regardless of periodontal limitations.
- Current technological capabilities are limited in accuracy and execution of occlusion from

scanned models

- Statistical occurrence of height discrepancy not explored.

### Delimitations

- All virtual treatments will be designed by the same operator using the same software.
- Only one prescription will be referenced when initially aligning the dentition

#### Assumptions

-Flat occlusal plane is optimal

-Computer modeling accurately predicts bracket expression

- Flat occlusal plane with no rotations, crowding, spacing, extremes in angulation or inclination will yield an ideal occlusion.

# Chapter 2: Review of the Literature.

### Notable Variations in Dental anatomy.

The human dentition is prone to significant anatomical variation, and while normal forms do exist many teeth fall within the realm of a variation from normal. Even if all dentition is studied from a single ethnic group considerable variability in dental morphology is present. <sup>35</sup> Variants may occur in facial curvature, crown width, crown height, or number of developmental lobes. Sometimes these variations occur all at once or individually. A brief discussion of some of the more notable morphological variations of the dentition follows. This examination is limited to serve the purposes of this investigation only and does not represent an exhaustive recollection of all morphological variables.

The maxillary central incisor is wedge shaped when viewed from the facial aspect. Crown length of the central can but does not always correspond with root length. The tooth is always formed by four developmental lobes, three that make up the facial aspect and one that forms the cingulum. Sometimes the middle lobe becomes obliterated if the two lateral lobes are oversized and absorb the middle one.<sup>35</sup> An examination of the height of contour of the labial aspect finds that the most facially prominent point is located in the middle third of the crown and corresponds to the facial axis point roughly 80% of the time.<sup>31</sup> This means that in 20% of cases the most prominent point will not coincide with the FA point and will result in a different expression of the appliance prescription.

Variability of Maxillary lateral incisors is well documented. <sup>29</sup> These teeth are typically more rounded at the point angles than are their central counterparts. Sometimes they are malformed enough to constitute as pegged laterals where developmental lobes have either never formed or all fused into a single lobe.<sup>29</sup> Often these teeth present clinically with a mesially tipped crown forming an almost boot shape with the mesio-incisal point angle being significantly more incisal than the disto-incisal. The disto-incisal point angle is often so rounded as to be nearly obliterated. The variability of the lateral incisor disposes it to a study solely concerned with siting brackets on this tooth; however it will be included in this study on a purely inciso-gingival basis.

Mandibular first premolars present with their own unique variations particularly of the labial surface. These members of the dentition exhibit the greatest amount of labial curvature in the dentition hence making the more prone to torsional forces when bracket slot heights are varied. A study by Sardarian et al found that torque forces in a more incisal position produce decrease as one positions a slot more gingival until the slot is roughly 4.5 mm from the incisal edge. Once past this point forces increase rapidly.<sup>29</sup>

Mandibular first Molars all form from five lobes and typically fall within two morphological categories as evidences by Doo Eun Park et al in their study concerning first molar morphology. This study showed that the two morphological types both fall within the tolerances of designated prescriptions. This means that only in extreme cases do variations in bracket position need to be employed concerning Mandibular first molars.<sup>29</sup>

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#### Straight wire appliance theory and back ground

In an attempt to eliminate the need for finishing bends Dr. Larry Andrews studied 120 untreated optimal cases. Through records of these cases Dr. Andrews was able to arrive at normal values for inclination, angulation, prominence, and relationship of the arches concerning intercupsation and curve of Spee for every tooth within a dentition<sup>2</sup>

From these normal values Dr. Andrews was able to record and articulate the six keys to a normal occlusion. The straight wire appliance was developed with the six keys programmed into the bracket in an attempt to simplify the orthodontic treatment process. Simplification of orthodontic process was only one motivation, Dr. Andrews also noticed great variation in treatment goals and results amongst the American Board of Orthodontics approved cases.<sup>5</sup> Any significant variation is troubling when trying to establish ideals thus a need for clear treatment goals was needed.

The concept of a straight wire appliance relies upon the prescription contained within the bracket being properly expressed from the FA point. The FA is defined as the center Facial axis of the clinical crown (FACC). Andrews defined the FACC as the central line of the anatomical crown often comprising the remnants of the central developmental lobe. Ideally the FA point will also coincide with the most prominent aspect of the facial surface (the height of contour) of the tooth so that the prescription is expressed optimally.<sup>4</sup> In order for the bracket prescription to be expressed properly three points must all align: the FA point, the base of the bracket and the base of the slot. (*Fig. 2) To* accomplish this coordination any required torque needed to be expressed in the base of the bracket as opposed to the slot.<sup>4</sup>



If all brackets are expressed properly, then at the conclusion of treatment all brackets will fall on a plane created by a line drawn between all FA points. This line indicates the Andrews plane as previously discussed.<sup>5</sup>

Dr. Andrews conducted further analysis on other cases that exemplified orthodontic ideals. From this later analysis the six elements of orofacial harmony were derived. For purposes of brevity and relevance only the sixth element dealing with occlusion will be reviewed.

### **Optimal Occlusion**

Optimal occlusion involves: the Six Keys to Optimal Occlusion (fig. 3), Element I teeth and arches, and the Element II, III, and IV jaw positions. Collectively, these are the characteristics of an esthetic, functional, and healthy occlusion. This particular study focuses on the impacts of the Sixth Element and in particular the Sixth key of the Sixth element.

#### Six Keys to optimal occlusion

The SWA was not the only result of Andrews labors. In fact several years prior to the development of the SWA Andrews used the initial 120 untreated patients along with 1105 treated patients to identify all of the aspects that made these occlusions so desirable. He Devised six aspects of occlusion that were all shared by these natural and optimally treated occlusion that later became known as the six keys to normal occlusion. A brief summary of the six keys to optimal occlusion is necessary to properly describe the treatment objectives pursued by this study.

#### Key I. Molar relationship.

The first of the six keys is molar relationship. The natural occlusion models consistently demonstrated that the distal surface of the distobuccal cusp of the upper first permanent molar occluded with the mesial surface of the mesiobuccal cusp of the lower second molar. Simply judging occlusion by the Mesiobuccal cusp of the Maxillary first molar in occlusion with the buccal grove of the mandibular first molar is insufficient since a malocclusion may still exist even with this relationship intact. A mesial angulation of the maxillary first molar is required for proper key I relationship to be achieved.<sup>2</sup>

#### Key II. Crown angulation (tip).

When the casts were studied it was determined that the gingival portion of the long axes of all crowns was more distal than the incisal portion. Crown tip is expressed in degrees, positive or negative. The degree of crown tip is the angle between the long axis of the crown and a line bearing 90 degrees from the occlusal plane. A positive angulation is determined when the gingival portion of the long axis of the crown is distal to the incisal portion. A negative angulation is assigned when the gingival portion of the long axis of the crown is mesial to the incisal portion. Each natural optimal model consistently had a distal inclination of the gingival portion of each crown. It varied with each tooth type, but within each type the angulation pattern was consistent from individual to individual.<sup>2</sup>

#### Key III. Crown inclination (labiolingual of buccolingual inclination).

Crown inclination is expressed in positive or negative degrees, representing the angle formed by a line which bears 90 degrees to the occlusal plane and a line that is tangent to the bracket site or Facial Axis point. A positive inclination is given if the gingival portion of the tangent line is lingual to the incisal portion. A negative inclination is recorded when just the opposite of the previous circumstance is present. Upper and lower anterior crown inclinations are intricately complementary and significantly affect overbite and posterior occlusion. Properly inclined anterior crowns contribute to normal overbite and posterior occlusion, when occlusal stops are eliminated by too negative of an inclination function is disrupted and over eruption is results. When anterior crowns are properly inclined the posterior teeth are encouraged into their normal positions. Even when the upper posterior teeth are in proper occlusion with the lower posterior teeth, spaces will result somewhere between the anterior and posterior teeth if the inclination of the anterior crowns is too positive. Crowding will result if inclination is too negative.

The pattern of upper posterior crown inclination was consistent in the naturally optimal models. A negative crown inclination existed in each crown from the upper canine through the upper second premolar. The lower posterior crown inclination pattern also was consistent among

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### all the untreated normal models.<sup>2</sup>

#### Key IV. Rotations.

The fourth key to optimal occlusion is that the teeth should be free of rotations.<sup>2</sup>

#### Key V. Tight contacts.

The fifth key is that the contact points should be tight (no spaces). Tooth size discrepancies pose special challenges to this key however in the absence of such a discrepancy all contacts should be tight. Without exception, the contact points on the untreated models were tight. <sup>2</sup>

#### Key VI. Occlusal plane.

The planes of occlusion found on the untreated models ranged from flat to slight curves of Spee. Even though not all of the untreated models had flat planes of occlusion, a flat plane should be a treatment goal as a form of overtreatment. There is a natural tendency for the curve of Spee to deepen with time, as the mandible continues its growth forcing the lower anterior dentition into a narrower aspect of the upper dentition resulting un up righting and deepening of the curve of Spee. Intercuspation of teeth is best when the plane of occlusion is relatively flat. A deep curve of Spee results in a more contained area for the upper teeth, making normal occlusion impossible. <sup>2</sup>



The ABO uses these keys to grade cases and while no specific requirement for a flat occlusal plane is present, there are standards for inclination, overjet, over bite, angulation, interproximal contact, and occlusion. These criteria combined are very difficult if not impossible to achieve with an occlusal plane that deviates from the slight to flat ideal set forth by Andrews.

### Straight wire appliance practice and application

Precise placement of an orthodontic bracket by hand is a difficult task. Though Dr. Andrews asserts the capability of the human eye to precisely dissect the anatomy of a tooth and locate the FA point, errors still occur. These errors may be attributed to operator error, variance in anatomy, or both. Proffit has espoused the benefits of the straight wire appliance while also noting the necessity for finishing bends.<sup>29</sup> All pre-programmed appliances have built in "slop" between the bracket and wire interface to allow for anomalous anatomy. The space allowed between the bracket and the wire also allow for a less than precise placement of brackets. Owing to the difficulty of consistently and precisely placing brackets many devices, gauges, and stents have been developed to aid Orthodontists when bonding a case with a straight wire appliance.<sup>1,10,11,12,17,32</sup> Many of these devices tend to lead the practitioner astray as exposed by Suarez et al.<sup>33</sup> Even with a programmed appliance, many orthodontists rely on first, second, and third order bends for finishing cases, defeating the purpose of a straight wire appliance.

Some of the final discrepancies present in the dentition may in fact be due to a greater height difference anteroposteriorly within the dentition than is allowed for in a prescription. This is to say that expression from the FA points, even if perfectly positioned does not yield satisfactory occlusal results. The final result is a non-ideal occlusal plane that is the result of improper expression and not owing to improper placement. If a large enough height discrepancy exist anteroposteriorly; then the Andrews plane must be adjusted incisally in order for a proper expression of the prescription.

### Bracket siting as a clinical execution

Sighting brackets has been part of clinical execution of the straight wire appliance since the development of the SWA. Andrews asserts that the human eye can adequately identify the midpoint of the clinical crown with no real need for measurements from any fixed location.<sup>4</sup> This has been proven in a study by Taylor et al found that bracket positioning in both the vertical and horizontal dimensions was accurate and consistent. Bracketing positioning in the angular regards however, is neither accurate nor reproducible.<sup>31</sup> As mentioned previously determining bracket position was traditionally done from a fixed location, but this has proven to result in unsatisfactory results with the SWA. Andrews postulates that a visual dissection of the clinical crown is required to identify the midpoint vertically and horizontally; the FA point. This approach to sighting brackets used anatomical land marks and appearances to illuminate proper positioning for a bracket to express its prescription. Some prominent clinicians still advocate for a fixed point reference for siting brackets. Many still hold to the incisal edge as the ideal point to reference including McLaughlin<sup>18</sup> and Damon<sup>9</sup> who both have published charts to reference proper bracket heights from incisal edges. A study out of China recently confirmed that these bracketing charts do yield satisfactory results when used for extraction cases.<sup>16</sup>

A study by McLaughlin et al determined average heights of FA points within a dentition as well as the most common bracket sighting errors. This study found that it is uncommon for clinicians to misidentify the FA of any dentition.<sup>18</sup> The inclusion criteria did not allow for significant anatomical variance that must occur within a clinical setting, for which an adjustment must be made. Even within the sample size of Mclaughlin's et al study the maximum half clinical crown measurement of a Maxillary central (6.94mm) varied significantly from the minimum clinical crown height of a Maxillary First molar (1.98mm)<sup>18</sup> The result of this study was the fabrication of a bracket sighting chart that uses a fixed value measured form the incisal edge to the midpoint of the bracket to determine proper bracket height. A clinician may use this chart coupled with clinical measurements of crown heights to adjust bracket position.

Unfortunately the previously mentioned recent study by Suarez et al explored marginal ridge leveling when a fixed point method is used to site brackets. This study found that when a fixed height was employed almost certainly marginal ridge discrepancies became worse. They

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concluded that using a bracket siting chart would likely not result in any improvement in final occlusion in fact it would likely only become worse.<sup>31</sup> Thus the human eye remains the best likely gauge for measuring proper bracket location.

Sound techniques for siting brackets must employ several strategies to ensure accuracy. A clinician must be able to locate the FACC of a clinical crown; this will determine the mesiodistal location. As mentioned previously the FACC runs the length of the clinical crown along the remnants of the midfacial developmental lobe.<sup>4</sup> The exception to this initial identification technique is applied to the maxillary and mandibular molars where the buccal grove serves as the FACC.<sup>4</sup> A Line running the length of the buccal grove from the occlusal terminus to the free gingival margin is identified. Once this mesiodistal determinant is identified the occlusoginigval midpoint can be determined fairly accurately by simple observation. In order to aid the clinician in identifying these land marks accurately the eye should be aligned squarely with the facial surface of any tooth being sited.<sup>19</sup> Viewing the facial surface from a view perpendicular to the FACC helps to eliminate any parallax of the clinical crown. A direct view should help the clinician determine the proper height and mesiodistal placement of a bracket, if one employs a mouth mirror to view the occlusal aspect of the dentition any rotations of the tooth of interest can be identified. The mouth mirror should be positioned the view the incisal or occlusal aspect squarely just as the facial aspect was viewed. This view should help indicate the long axis of the tooth, eliminate any distortion caused by rotations and thus increase the accuracy of siting a bracket for angulation.<sup>35</sup> As mentioned previously, angulation is the aspect that is subject to the most error when siting brackets.

One must ask if any deleterious side effects may result from an adjustment in vertical height with regards to final inclination, periodontal health, occlusion or smile aesthetics. As

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mentioned previously the SWA allows for variation in anatomy that was demonstrated in the study by R.N. Smith et al. when they identified that the most prominent point of the central incisors coincides with FA only 80% of the time and only 50% when assessing maxillary lateral incisors and Maxillary cuspids.<sup>31</sup> The range of this tolerance must be explored to determine effective bracket citing. Recently Rainer et al conducted a study and found that significant first and third order changes occur based on the labial anatomy and bracket location particularly of maxillary incisors. This study also showed that an adjustment either in the wire or bracket location should be expected for satisfactory completion of treatment with a pre-adjusted appliance(SWA)<sup>23</sup> these findings are additionally reinforced by Van Loenen at al who

# Significance

The significance of this research lies in determining the proper bracket height to achieve a level occlusal plane. Should a consistent correction be discovered or a consistent rate of correction it can help to finish cases with a higher compliance to the six keys of optimal occlusion.

# Null Hypothesis

No significant vertical adjustment in clinical crown height away from the FA point is required to yield a flat occlusal plane.

# Materials and Methods:

# Materials

- One PC with sufficient processing and graphics generating power
- Two 24" monitors to facilitate data entry and measurement observation
- One motion view model scanner
- One licensed copy of Motion View proprietary software
- 20 dental case models
- Copy of Microsoft Excel to record data.

## Methods

20 cases consisting of Maxillary and Mandibular. dental casts that were lacking any significant anatomical variation (such as peg laterals or amelogenesis imperfect), having a representation of a full adult dentition, free of restorations, free of cavitated carious lesions, and of Caucasian individuals were scanned into a Personal computer using a Motion View scanner with its proprietary software. All cases were deindivdualized by assigning them a case number. N=40 considering each case contains two of each tooth.



- Scanned cases (fig. 4) had every tooth identified and separated virtually (fig 5)
- All teeth were measured along the central developmental lobe (FACC) (fig. 8) from cusp tip/incisal edge to the free gingival margin. This constituted the heights of clinical crowns. Exceptions to this measurement were the maxillary and mandibular molars. The molars were measured along their buccal grove from the occlusal terminus to the free gingival margin.



- All necessary anatomical land marks were identified automatically by the software and any corrections were applied by the operator. Particular attention was paid to marginal ridge indicators. These dots will be located at the most concave point of its respective marginal ridge. (fig. 6)
- Marginal ridges served as a key landmark for later adjustments. Marginal ridges were chosen based on their inclusion in grading of ABO cases.



• Following all of these identifying steps the computer was then capable of digitally separating the clinical crowns from the model and manipulating the crown locations in space. (fig. 7)



- After the teeth were digitized 6 color coded points are generated by the software.
- Measurements were automatically generated by the software providing

- Distance of the mesial yellow dot to the red FA dot
- Distance of the distal yellow dot to the red dot
- Distance of the orange dot from the red dot
- The Red dot was dragged to the gingival limit of the clinical crowns along the FACC
- The Orange dot was placed at the inciso-facial line angle/mesio Buccal cusp tip/ occlusal terminus of the buccal groove. This location was automatically decided by the computer but confirmation was required by the operator.
- This provided the measurement of the FACC by taking advantage of the auto measurement of the distance from the orange dot to the red dot – FACC Measurement
- All FACC values were recorded
- Excel division function was utilized to provide an FA point measurement we will call anatomical FA. The FACC values were divided by 2. This measurement is accurate to 0.01 mm.



- the Andrews prescription was chosen as the reference prescription for auto alignment of the crowns.
- The FA heights were designated for bracket placement on an individual case by case basis. Heights were drawn from the excel spread sheet.



• An arch wire is generated and adjusted to form a straight line. The archwire is straightened using the overlay grid feature of the software. (fig. 9)



align the clinical crowns.

• Auto alignment tool was engaged.

- Any malposition concerning rotations or angulations present from the initial alignment were corrected. Any dental overlap by location bugs were corrected.
- The alignment process began by aligning the mesial marginal ridge of the second molar to the distal marginal ridge of the first molar. Mesiobuccal cusp tips were placed on the same latitude for second molars as the first molars mesio buccal cusp. Then marginal ridges of the premolars were coordinated to the first molar. This established the occlusal plane. Most mesial premolar with aligned marginal ridges were referenced for its buccal cusp height. This reference is only relevant if the cusp tips are of a different height.(fig.10)
- The overlay mesh feature was activated. This provided a latitude to align the incisors with the buccal cusp of the most mesial, aligned premolar.
- All incisors will be aligned with the reference cusp using the overlay mesh as a fixed reference.
- Distal bulge of the cuspids aligned with mesial contact points of first premolars.
- The brackets were then be reapplied to the crowns in the corrected positions.
   Reapplication of the bracket to the aligned teeth is a feature of motion view software.
   This will move the FA point to the base of the bracket automatically allowing for the scribe lines to indicate new vertical measurements. The bracket position is a reference to the arch wire which has remained fixed in space during all adjustments to the clinical crowns.
- After the brackets have been automatically re applied a new measurement from red dot to the orange dot will be available. This measurement will be recorded and excel will

calculate the difference between red dot – orange dot measurement one (anatomical FA) and red dot- orange dot measurement two (adjusted FA)



- After initial alignment, correction of digital errors, and simple measurements of newly
  aligned crowns the mandibular incisors are selected and proclined en masse a total of 37
  mouse clicks. This will result in a proclination of approximately 1mm. These same teeth
  will then be tipped lingually 65 clicks to both compensate for initial proclination and
  retrocline the dentition another 1mm.
- Retroclining adjustment will always be done from the proclined positions hence the need to double the clicks for equal amount of adjustment.
- At the end of each proclination or retroclination step the teeth will be adjusted to the occlusal plane as indicated by the same reference cusp. Brackets will again be reapplied to aligned teeth and new FA measurments will be recorded.

## Statistical analysis

- A pilot study of 7 patients was completed and submitted to a statistician for power analysis. The analysis revealed that for an alpha value greater than 0.90 9 samples must be tested. This study consisted of 32 samples of each tooth giving an alpha of 0.99
- Averages and standard deviation of crown heights were obtained.
- Average and standard deviation of adjustment from anatomical FA were calculated.
- Simple hypothesis testing was engaged for all teeth to measure probability that an adjustment greater than 0.5 mm is required in either direction.
- Correlation between crown height and bracket adjustment was explored to determine if a specific height adjustment can be universally applied or if a rate of adjustment associated with clinical crown height may be employed.
- Correlation between necessary proclination or retroclination and bracket adjustment were also be analyzed in the same manner as

# Results

Results were recorded with positive values indicating an adjustment toward the incisal or occlusal surface and negative values representing an adjustment in the gingival direction. For teeth numbers 2-7, 10-15, 18-22, and 27-31, no significant adjustment in vertical position away

from the FA point was found (p = 1.0000).



Table 1 shows the average adjustments for each tooth.

- For the maxillary centrals average adjustment incisally from FA point of 1.21 mm and a probability of the adjustment being greater than 0.5 mm of nearly 100% (p = 1.000)
- For maxillary Laterals p= 0.8747 though the mean adjustment was 0.43 mm incisally from FA
- For mandibular laterals average adjustment was 0.77 mm incisally with a p = < 0.0001.
- For mandibular centrals an average adjustment of 0.87 mm incisally and a p = < 0.0001.
- Correlations for initial crown height to required adjustment were weak for many of the teeth. However, for all incisors the correlation between necessary adjustment and initial crown height was strong: 0.62 for lower laterals, 0.70 for lower centrals, 0.63 for upper laterals and 0.50 for upper centrals.

- Adjustments for lower incisors during proclination did not vary significantly from those needed for a level occlusal plane. (avg adjustment 1.1 mm p=<0.0001 for centrals and 1.3 mm for laterals p=<0.0001)</li>
- Adjustments for retroclined lower incisors did not vary significantly from original FA.
   Averaging -0.28mm for centrals p=1.000 and -0.24mm for laterals (p=1.000)

# Discussion

For the majority of the teeth the adjustments required to achieve a level occlusal plain are extremely small and not clinically relevant. For example, the maxillary second premolar required a very small adjustment (-0.2mm) in the gingival direction; this could be attributed to initial placement error or a very slight lack of eruption by the tooth. It is important to note that the threshold for clinical relevance was set to 0.5 mm not just because of human ability to correct such minor discrepancies, but also due to the ability of the appliance to express such small adjustments. For these reasons the majority of adjustments are not considered relevant and the null hypothesis is accepted.

Adjustments begin to be more significant as one travels anteriorly in the dental arch. The maxillary laterals need an adjustment of greater than 0.5mm only 44% of the time though the mean adjustment was 0.52 mm. This is likely due to a few cases of extremely long laterals requiring large adjustments. The maxillary central is the most outstanding adjustment needed with a mean of 1.28 mm. The probability of needing to adjust the bracket at least 0.5 mm was

close enough that one can say 100% of the time the bracket needs to be more incisal than FA. It is important to note that among all of the maxillary teeth only the centrals required an adjustment the majority of the time that was clinically significant and that adjustment was only in the incisal direction.

The only maxillary tooth that consistently adjusted more gingival was the second molar. It is probable that this adjustment was due to the tooth being slightly under erupted similar to the second premolar; a theory that is further supported by the negative correlation present in the clinical crown to bracket adjustment comparison seen in the results. A similar adjustment to the maxillary central is required for all of the lower incisors where a mean incisal adjustment is around 0.8mm and 0.76mm for centrals and lateral respectively. The probability of an adjustment being required for a level occlusal plane was also significant for mandibular centrals and laterals with p-values of 99.99% and 99.95% respectively.

These adjustments are required almost certainly because of the crown length exhibited by these teeth. The correlation between crown height and necessary adjustment was strong for Maxillary centrals, mandibular laterals, and mandibular centrals. (0.50,0.62, 0.70 respectively.) Correlation for crown height and Maxillary laterals was also strong (0.63), but due to their anatomical variability the probability of an adjustment being needed was very low only about 44% occurrence. The strong correlation is likely the result of average adjustment falling around .5 mm. One would initially think that an average being clinically significant would make the necessary sighting change significant, but again these teeth are highly variable. In the end clinical judgment must prevail for Maxillary laterals.

For many patients ideal lower incisor inclination (-1° to true vertical for the facial surface and 15° to true vertical along the long axis.) is not attainable for proper anterior guidance and coupling. The treatment may require proclination or retroclination depending on a class II or class III skeletal relationship respectively. In such cases one should site brackets appropriately depending on the desired final result. The brief exploration into any necessary adjustments contained within this study reveals that in the cases of proclination the brackets should be adjusted more incisal only slightly more than the height required for a flat occlusal plane. So slight is the difference that clinical relevance is absent.

However the incisors required little to no adjustment when a retroclined mandibular anterior was a desired treatment goal. When Lower incisors needed to be retroclined the bracket sighting was very close to FA and in fact was approximately .2 mm more gingival than FA. This change is not clinically significant however the placement is worth noting. The relationship of brackets depends on the final inclination of the teeth and the brackets relationship to the center of resistance. If a tooth needs to be more proclined and we imagine a fixed flat occlusal plane represented by the wire (a more gingival translation but a parallel plane.) as the tooth rotates anteriorly the fixed nature of the bracket height (fixed by the brackets of all other teeth) will extrude the tooth. The opposite can be said for any incisor that needs to be retroclined. The fixed nature of the occlusal plane and the movable nature of a center of resistance would tend to intrude an incisor as it rotated more lingual.

It is important to understand that this study is not meant to result in a bracketing chart where all patients are treated to a prescribed bracketing scheme. The purpose is to exhibit that variation in bracket height is almost always necessary. When starting a case proper diagnosis will

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absolutely inform the practitioner of proper bracket height. It is also important to note that this study did not exam occlusal relationships in any way thus no bracket was ever significantly adjusted more gingival from the FA. A clinician may find that open bites manifest as an expression of an inharmonious skeletal relationship and may require bracketing on the FA, in the instances of the maxillary and mandibular incisors, or gingival to the FA...

An astute clinician may voice concerns that differential bracketing will result in improper inclinations or torque expression for incisors. Regarding this concern, it is important to remember that a great deal of space exists between the wire and bracket interface. Often a clinician must employ 45° or more of torque in order to affect a small desired clinical change. This allows for significant height changes without a significant affect in torque. In the end clinical judgment must be employed when bracketing a case.

# Conclusions

- Maxillary centrals should be adjusted at least 1mm incisally form FA in the majority of cases
- Maxillary Laterals are highly variable but may only require adjustments in less than half of the cases
- All Mandibular incisors require at least 0.5 mm adjustment incisaly for a flat occlusal plane
- If mandibular incisors need proclined then the standard adjustment from FA (0.75mm) will be sufficient.
- If mandibular incisors need retroclined then brackets should be placed on the FA.

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Appendicies

# Appendix A: Variable Definitions

U : indicated upper arch toothL: indicates lower arch tooth
D: indicates that the measurement is the difference between measured FA and adjusted FA
1: indicates that the tooth is the first of a type of tooth such as molar or premolar
2: indicates that the tooth is the second of a type of tooth
M: molar
PM: Premolar
I: cuspid
L: lateral
C: central

Example: LD2PM is the lower second premolar difference between measured Facial Axis point and Adjusted Facial axis point ExceptionsData set labeled UC or LC are crown measurements along the FACC Data set labeled UFA are calculated FA measurements Data set labeled UA are adjusted FA measurements Appendix B Data

Patient Nu	mber UC	1.00	UC.	UCare	UCton	UC.	UC. L		Com LC	ten LC	-	LCtom	LC.	LC.	LC.
172	26929	5.32	4.73	5.54	1 6	8.55	6.96	9.46	4.97	5.64	5.58	6.67	8.1	3 7.65	6.84
16	70124	4.66	4.43	5.4	6.73	8.85	7.57	8.58	4.11	4.54	5.89	6.94	8.5	1 8.66	8.68
168	81268	4.73	4.58	5.36	5.49	7.59	6.41	8.78	3.79	5.09	5.89	6.95	8.7	4 7.6	5 7.32
163	35488	4.14	4.41	4.96	5.85	7.63	6.01	7.98	4.17	5.28	5.73	6.14	6.7	3 5.94	6.36
168	86264	5.62	5.81	6.13	7.51	8.7	7.4	8.61	5.44	5.53	5.92	6.83	8.2	9 8.71	8.78
169	98630	5.68	6.04	6.63	7.97	8.73	8.18	10.21	4.98	6.69	6.58	7.94	8.9	5 7.63	8.35
162	28985	4.57	5.13	4.55	5.41	7.62	6.39	8.95	3.15	5.19	5.74	6.02	8.1	.7 6.71	6.6
170	09329	4.52	3.92	4.81	6.41	7.7	6.81	8.2	4.34	5.22	5.82	6	7.1	4 6.67	7 7.05
	14	5.11	5.1	5.65	7.55	10.08	7.86	8.06	4.47	5.43	6.32	7.71	7.4	2 6.95	7.19
	60	5.49	4.69	6.08	7.84	9.05	8.52	9.66	4.07	5.38	6.7	8	9.6	2 7.96	8.08
	18	4.65	6.06	7.33	8.31	9.23	7.91	9.69	5.22	6.15	7.23	8.71	. 8.7	6 8.01	l 8.8
	66	6.37	5.18	6.16	6.39	9.42	7.2	9.07	4.38	5.14	5.5	7.48	9.5	4 8.27	8.29
	46	3.95	4.61	5.62	6.31	8.97	6.78	9.12	3.86	6.11	6.75	7.78	9.4	6 7.06	6.94
	151	4.37	4.67	5.95	5 7	10.14	7.85	8.92	4.74	6.09	7.69	7.38	9.	5 8.09	8.24
	50	4.26	4.39	6.33	3 7.2	7.81	7.12	8.48	4.64	6.08	5.78	7.28	7.5	3 6.66	i 7.18
	23	6.19	6.47	5.83	7.63	10.11	9.09	10.2	6.04	6.44	7.43	8.46	10.3	5 6.69	8.65
172	26929	4.97	4.71	4.5	5.47	8.9	7.22	9.06	5.25	5.39	5.53	6.46	7.8	5 6.47	7.1
16.	/0124	4.11	3.81	5.87	/ /.02	9.41	7.59	8.58	4.81	5.35	5.79	7.37	8.3	6 8.64	8.66
100	81268	3.79	4.31	4.08	5 5.0	8.55	6.28	9.07	3.89	5.27	5.5	6.91	. /.	b /.11	. 7.97
10:	35488	4.1/	4.29	4.33	5.94	8.05	5.77	8.62	4.20	5.21	5.72	0.04	0.0	5 6.23	4.94
100	80204	5.44	5.79	0.43	7.58	10.04	0.55	8.07	5.29	5.48	0.41	7.45	8.0	3 8.01	. 7.9
16	20030	2 15	3.42	0.41	5.02	7.51	5.00	0.54	2.05	5.45	7.55	5.0	9.0	o o.2	. 7.52
10.	20303	3.15	4.55	4.72	5.55	7.51	6.66	7.55	3.45	5.45	5.04	5.5		5 7.52	6 71
1/0	14	4.34	4.40	4.76	6.87	9.54	8.05	8.78	4.47	5.58	6.24	7 33	77	4 6 90	712
-	60	4.47	4.00	5.81	6.78	9.43	8.3	9.37	3.99	5.41	5.97	8.12	91	6 7.83	7.12
	18	5 22	5.87	6.84	8 37	9.82	8.56	9.94	5.96	5.87	7	8.32	95	3 8.04	1 8 69
	66	4.38	5.15	6.41	5.61	9.03	7.02	9.38	4.8	5.26	6.23	7.03	9.6	8 8.8	7.8
	46	3.86	4.66	5.48	6.18	8.27	7.32	7.84	3.88	5.26	6.5	7.08	8.0	2 6.41	6.56
-	151	4.74	5.01	5.83	7.46	8.36	7.97	9.46	4.59	6.47	6.58	8.1	10.1	8 8.41	7.87
	50	4.64	4.5	5.54	7.6	8.69	7.28	8.52	4.21	6.02	7.1	7.66	8.4	9 6.63	6.72
	23	6.04	6.08	5.81	8.29	10	9.05	10.54	6.73	6.9	8.25	8.82	10.4	7 8.33	7.52
Average		4.75	4.955938	5.640625	6.82375	8.830938	7.495625	9.019063	4.630938	5.66625 6	5.307188	7.307813	8.52312	5 7.475625	7.556563
Standard D	ev 0	74406	0.670901	0.766664	0.915796	0.847335	0.92278	0.753882	0.77934 0	.565713 0	0.734501	0.836458	1.07883	3 0.833852	0.880123
Standard D			0.070501				U.J.L.I.U						107000		0.000 ILU
UFA <sub>2m</sub>	UFAim	UFA	zom UF	Aipm U	JFA	UFAL	UFAc	LFA <sub>2m</sub>	LFA <sub>1m</sub>	LFA <sub>2pm</sub>	LFA <sub>1</sub>	pm LF/	A, L	FAL I	LFAc
UFA <sub>2m</sub> 2.66	UFA <sub>1m</sub> 2.3	UFA	2.77	FA <sub>1pm</sub> l 3	JFA <sub>1</sub> 4.275	UFA <sub>L</sub> 3.48	UFA <sub>c</sub> 4.73	LFA <sub>2m</sub> 2.485	LFA <sub>1m</sub> 5 2.8	LFA <sub>2pm</sub> 2 2.	LFA <sub>1</sub>	<sub>pm</sub> LF/ 3.335	4.065	.FA <sub>L</sub> 1 3.825	LFA <sub>c</sub> 3.42
UFA <sub>2m</sub> 2.66 2.33	UFA <sub>1m</sub> 2.3 2.2	UFA 55 15	2.77 2.7	FA <sub>1pm</sub> U 3 3.365	JFA <sub>1</sub> 4.275 4.425	UFA <sub>L</sub> 3.48 3.785	UFA <sub>c</sub> 4.73 4.29	LFA <sub>2m</sub> 2.485 2.055	LFA <sub>im</sub> 5 2.8 5 2.2	LFA <sub>2pm</sub> 2 2. 7 2.9	LFA <sub>1</sub> 79	pm LF/ 3.335 3.47	4.065 4.255	.FA <sub>L</sub> 3.825 4.33	LFA <sub>c</sub> 3.42 4.34
UFA <sub>2m</sub> 2.66 2.33 2.365	UFA <sub>im</sub> 2.30 2.21 2.11	UFA 55 15 29	2.77 2.7 2.68	FA <sub>1pm</sub> U 3 3.365 2.745	JFA <sub>1</sub> 4.275 4.425 3.795	UFA <sub>L</sub> 3.48 3.785 3.205	UFA <sub>c</sub> 4.73 4.29 4.39	LFA <sub>2m</sub> 2.485 2.055 1.895	LFA <sub>im</sub> 5 2.8 5 2.2 5 2.54	LFA <sub>2pm</sub> 2 2. 7 2.9 5 2.9	LFA <sub>1</sub> 79 45	pm LF/ 3.335 3.47 3.475	4.065 4.255 4.37	.FA <sub>L</sub> 3.825 4.33 3.8	LFA <sub>c</sub> 3.42 4.34 3.66
UFA <sub>2m</sub> 2.66 2.33 2.365 2.07	UFA <sub>1m</sub> 2.30 2.22 2.2 2.2	UFA 55 15 29 05	2.77 2.77 2.68 2.48	FA <sub>1pm</sub> U 3 3.365 2.745 2.925	JFA <sub>1</sub> 4.275 4.425 3.795 3.815	UFAL 3.48 3.785 3.205 3.005	UFA <sub>c</sub> 4.73 4.29 4.39 3.99	LFA <sub>2m</sub> 2.485 2.055 1.895 2.085	LFA <sub>1m</sub> 5 2.8 5 2.2 5 2.54 5 2.6	LFA <sub>2pm</sub> 2 2. 7 2.9 5 2.9 4 2.8	LFA <sub>1</sub> 79 45 45	pm LF/ 3.335 3.47 3.475 3.07	4.065 4.255 4.37 3.365	FAL 3.825 4.33 3.8 2.97	LFA <sub>c</sub> 3.42 4.34 3.66 3.18
UFA <sub>2m</sub> 2.66 2.33 2.365 2.07 2.81	UFA <sub>1m</sub> 2.30 2.21 2.11 2.20 2.90	UFA 55 15 29 05 05	2.77 2.77 2.68 2.48 3.065	FA <sub>1pm</sub> U 3 3.365 2.745 2.925 3.755	JFA <sub>1</sub> 4.275 4.425 3.795 3.815 4.35	UFAL 3.48 3.785 3.205 3.005 3.7	UFA <sub>c</sub> 4.73 4.29 4.39 3.99 4.305	LFA <sub>2m</sub> 2.485 2.055 1.895 2.085 2.085	LFA <sub>1m</sub> 5 2.8 5 2.2 5 2.54 5 2.6 2 2.76	LFA <sub>2pm</sub> 2 2. 7 2.9 5 2.9 4 2.8 5 2.	LFA <sub>1</sub> 79 45 45 65 96	pm LF/ 3.335 3.47 3.475 3.07 3.415	4.065 4.255 4.37 3.365 4.145	LFAL 3.825 4.33 3.8 2.97 4.355	LFA <sub>c</sub> 3.42 4.34 3.66 3.18 4.39
UFA <sub>2m</sub> 2.66 2.33 2.365 2.07 2.81 2.84	UFA <sub>1m</sub> 2.30 2.2 2.1 2.2 2.90 3.0	UFA 55 15 29 05 05 02	2.77 2.77 2.68 2.48 3.065 3.315	FA <sub>1pm</sub> 3 3.365 2.745 2.925 3.755 3.985	JFA <sub>1</sub> 4.275 4.425 3.795 3.815 4.35 4.365	UFAL 3.48 3.785 3.205 3.005 3.7 4.09	UFA <sub>c</sub> 4.73 4.29 4.39 3.99 4.305 5.105	LFA <sub>2m</sub> 2.485 2.055 1.895 2.085 2.77 2.45	LFA <sub>1m</sub> 5 2.8 5 2.2 5 2.54 5 2.6 2 2.76 9 3.34	LFA <sub>2pm</sub> 2 2. 7 2.9 5 2.9 4 2.8 5 2. 5 3.	LFA <sub>1</sub> 79 45 45 65 96 29	pm LF/ 3.335 3.47 3.475 3.07 3.415 3.97	4.065 4.255 4.37 3.365 4.145 4.475	FAL 3.825 4.33 3.8 2.97 4.355 3.815	LFA <sub>c</sub> 3.42 4.34 3.66 3.18 4.39 4.175
UFA <sub>2m</sub> 2.66 2.33 2.365 2.07 2.81 2.84 2.285	UFA <sub>1m</sub> 2.3 2.2 2.2 2.2 2.9 3.0 2.5	UFA 55 15 29 05 05 02 55	2.77 2.7 2.68 2.48 3.065 3.315 2.275	A <sub>1pm</sub> 4 3 3.365 2.745 2.925 3.755 3.985 2.705	JFA <sub>1</sub> 4.275 4.425 3.795 3.815 4.35 4.35 4.365 3.81	UFA <sub>L</sub> 3.48 3.785 3.205 3.005 3.7 4.09 3.195	UFA <sub>c</sub> 4.73 4.29 4.39 3.99 4.305 5.105 4.475	LFA <sub>2m</sub> 2.485 2.055 1.895 2.085 2.77 2.49 1.575	LFA <sub>1m</sub> 5 2.8 5 2.2 5 2.54 5 2.6 2 2.76 9 3.34 5 2.59	LFA <sub>2pm</sub> 2 2. 7 2.9 5 2.9 4 2.8 5 2. 5 3. 5 3.	LFA1 79 45 45 65 96 29 87	pm LF/ 3.335 3.475 3.475 3.07 3.415 3.97 3.01	4.065 4.255 4.37 3.365 4.145 4.475 4.085	FAL 3.825 4.33 3.8 2.97 4.355 3.815 3.355	LFA <sub>c</sub> 3.42 4.34 3.66 3.18 4.39 4.175 3.3
UFA2m 2.66 2.33 2.365 2.07 2.81 2.84 2.285 2.26	UFA1m 2.30 2.22 2.30 2.20 2.90 3.0 2.50 1.5	UFA 55 15 29 05 05 02 55 96	2.77 2.77 2.77 2.68 2.48 3.065 3.315 2.275 2.405	FA <sub>1pm</sub> 4 3 3.365 2.745 2.925 3.755 3.985 2.705 3.205	JFA <sub>1</sub> 4.275 4.425 3.795 3.815 4.35 4.365 3.81 3.81 3.85	UFAL 3.48 3.785 3.205 3.005 3.7 4.09 3.195 3.405	UFA <sub>c</sub> 4.73 4.29 4.39 3.99 4.305 5.105 4.475 4.1	LFA <sub>2m</sub> 2.485 2.055 1.895 2.085 2.77 2.45 1.575 2.17	LFA <sub>1m</sub> 5 2.8 5 2.2 5 2.54 5 2.6 2 2.76 9 3.34 5 2.59 7 2.6	LFA <sub>2pm</sub> 2 2. 7 2.9 5 2.9 4 2.8 5 2. 5 3. 5 2. 1 2.	LFA1 79 45 45 65 96 29 87 91	pm LFA 3.335 3.47 3.475 3.07 3.415 3.97 3.01 3	A,         L           4.065         4.255           4.37         3.365           4.145         4.475           4.085         3.57	FAL 3.825 4.33 3.8 2.97 4.355 3.815 3.355 3.335	LFA <sub>c</sub> 3.42 4.34 3.66 3.18 4.39 4.175 3.3 3.525
UFA2m 2.66 2.33 2.365 2.07 2.81 2.84 2.285 2.26 2.555	UFA1m 2.30 2.21 2.20 2.90 3.0 2.50 1.1 2.50	UFA 55 15 29 05 05 05 05 55 66 55	2.77 2.77 2.68 2.48 3.065 3.315 2.275 2.405 2.825	FA <sub>1pm</sub> 4 3 3.365 2.745 2.925 3.755 3.985 2.705 3.205 3.205 3.775	JFA, 4.275 4.425 3.795 3.815 4.35 4.365 3.81 3.85 5.04	UFAL 3.48 3.785 3.205 3.005 3.7 4.09 3.195 3.405 3.93	UFA <sub>c</sub> 4.73 4.29 4.39 3.99 4.305 5.105 4.475 4.1 4.03	LFA2m 2.483 2.055 1.895 2.083 2.77 2.49 1.575 2.17 2.235	LFA <sub>1m</sub> 5 2.8 5 2.2 5 2.54 5 2.6 2 2.76 9 3.34 5 2.59 7 2.6 5 2.71	LFA <sub>2pm</sub> 2 2. 7 2.9 5 2.9 4 2.8 5 2.9 5 3. 5 2. 1 2. 5 3.	LFA1 79 45 45 65 96 29 87 91 16	pm LFA 3.335 3.47 3.475 3.07 3.415 3.97 3.01 3.01 3.855	4.065 4.255 4.37 3.365 4.145 4.475 4.085 3.57 3.71	FAL 3.825 4.33 3.8 2.97 4.355 3.815 3.355 3.335 3.335 3.475	LFA <sub>c</sub> 3.42 4.34 3.66 3.18 4.39 4.175 3.3 3.525 3.595
UFA2m 2.66 2.33 2.365 2.07 2.81 2.84 2.285 2.26 2.555 2.745	UFA <sub>1m</sub> 2.30 2.22 2.1 2.90 3.0 2.50 1.1 2.3	UFA 55 15 29 05 05 05 02 55 66 55 15	2.77 2.77 2.68 2.48 3.065 3.315 2.275 2.405 2.825 3.04	EA <sub>1pm</sub> 3 3.365 2.745 2.925 3.755 3.985 2.705 3.205 3.775 3.92	JFA, 4.275 4.425 3.795 3.815 4.365 3.815 4.365 3.81 3.85 5.04 4.525	UFA 3.48 3.785 3.205 3.005 3.77 4.09 3.195 3.405 3.93 4.26	UFA <sub>c</sub> 4.73 4.29 4.39 3.99 4.305 5.105 4.475 4.1 4.03 4.83	LFA2m 2.483 2.055 1.895 2.083 2.77 2.49 1.575 2.17 2.235 2.035	LFA <sub>1m</sub> 5 2.8 5 2.2 5 2.54 5 2.6 2 2.76 9 3.34 5 2.59 7 2.6 5 2.71 5 2.6	LFA <sub>2pm</sub> 2 2. 7 2.9 5 2.9 4 2.8 5 2.9 4 2.8 5 2. 5 3. 5 2. 1 2. 5 3. 9 3.	LFA1 79 45 45 96 29 87 91 16 35	pm LFA 3.335 3.475 3.07 3.415 3.97 3.01 3.855 4	4.065 4.255 4.37 3.365 4.145 4.475 4.085 3.57 3.71 4.81	FAL 3.825 4.33 3.8 2.97 4.355 3.815 3.355 3.355 3.335 3.475 3.98	LFA <sub>c</sub> 3.42 4.34 3.66 3.18 4.39 4.175 3.3 3.525 3.595 4.04
UFA2m 2.66 2.33 2.365 2.07 2.81 2.84 2.285 2.26 2.555 2.745 2.325	UFA <sub>1m</sub> 2.3 2.2 2.1 2.2 2.9 3.4 2.5 1.5 2.5 2.3 3.4 2.3 3.4	UFA 55 15 29 05 05 05 55 66 55 55 15 53	2,77 2,77 2,68 2,48 3,065 3,315 2,275 2,405 2,825 3,04 3,665	A <sub>1pm</sub> 4 3 3.365 2.745 2.925 3.755 3.985 2.705 3.205 3.205 3.775 3.92 4.155	JFA, 4.275 4.425 3.795 3.815 4.35 4.365 3.81 3.85 5.04 4.525 4.615	UFA 3.48 3.785 3.205 3.005 3.77 4.09 3.195 3.405 3.93 4.26 3.955	UFAc 4.73 4.29 4.39 3.99 4.305 5.105 4.475 4.11 4.03 4.83 4.845	LFA2m 2.485 2.055 2.055 2.055 2.055 2.055 2.17 2.245 1.575 2.17 2.235 2.035 2.035 2.035	LFA <sub>1m</sub> 5 2.8 5 2.2 5 2.54 5 2.6 2 2.76 9 3.34 5 2.59 7 2.6 5 2.71 5 2.6 1 3.07	LFA <sub>2pm</sub> 2 2. 7 2.9 5 2.9 4 2.8 5 2. 5 3. 5 2. 1 2. 5 3. 9 3. 5 3.6	LFA <sub>11</sub> 79 45 45 96 29 87 91 16 35 15	pm LFA 3.335 3.47 3.475 3.07 3.415 3.97 3.01 3.855 4 4.355	4.065 4.255 4.37 3.365 4.145 4.475 4.085 3.57 3.71 4.81 4.81 4.38	FAL 3.825 4.33 3.8 2.97 4.355 3.815 3.355 3.355 3.355 3.3475 3.98 4.005	LFA <sub>c</sub> 3.42 4.34 3.66 3.18 4.39 4.175 3.3 3.525 3.595 4.04 4.4
UFA2m 2.66 2.33 2.365 2.07 2.81 2.84 2.285 2.26 2.555 2.745 2.325 3.185 3.185	UFA <sub>1m</sub> 2.3 2.2 2.1 2.2 2.9 3.6 2.5 1.5 2.5 2.3 3.6 2.3 3.6 2.3	UFA 55 15 29 05 05 05 55 66 55 55 66 55 59 60 55 59 60 55 59 60 55	2.77 2.77 2.68 2.48 3.065 3.315 2.275 2.405 2.825 3.04 3.665 3.04	A <sub>1pm</sub> ( 3 3.365 2.745 3.755 3.755 3.985 2.705 3.205 3.205 3.775 3.92 4.155 3.195	JFA <sub>1</sub> 4.275 4.425 3.795 3.815 4.35 4.365 3.81 3.85 5.04 4.525 4.615 4.71	UFAL 3.48 3.785 3.005 3.005 3.77 4.09 3.195 3.405 3.93 4.26 3.955 3.6	UFA <sub>c</sub> 4.73 4.29 4.39 3.99 4.305 5.105 4.475 4.11 4.03 4.83 4.83 4.845 4.535	LFA <sub>2m</sub> 2.483 2.055 1.895 2.057 2.49 1.575 2.17 2.49 1.575 2.11 2.235 2.035 2.65	LFA <sub>1m</sub> 5 2.8 5 2.25 5 2.54 5 2.66 2 2.76 9 3.34 5 2.59 7 2.6 5 2.71 5 2.6 1 3.07 9 2.5	LFA <sub>2pm</sub> 2 2. 5 2.9 4 2.8 5 2.9 4 2.8 5 2. 5 3. 5 2. 1 2. 5 3. 9 3. 5 3.6 7 2.	LFA1 79 45 45 65 96 29 87 91 16 35 35 15 47	pm LF/ 3.335 3.47 3.475 3.07 3.415 3.97 3.01 3.855 4 4.355 3.74	4.065 4.255 4.37 3.365 4.145 4.475 4.085 3.57 3.71 4.81 4.38 4.77	FAL 3.825 4.33 3.8 2.97 4.355 3.815 3.355 3.355 3.475 3.98 4.005 4.135	LFA <sub>c</sub> 3.42 4.34 3.66 3.18 4.39 4.175 3.3 3.525 3.595 4.04 4.4 4.44 4.145
UFA2m 2.66 2.33 2.365 2.07 2.81 2.84 2.285 2.26 2.555 2.745 2.325 3.185 1.975	UFA <sub>1m</sub> 2.34 2.22 2.34 2.94 3.6 2.55 1.1 2.55 1.1 2.34 3.6 2.34 3.6 2.34	UFA 55 15 29 05 05 02 55 02 55 55 145 03 59 05	2.77 2.77 2.68 2.48 3.065 3.315 2.275 2.405 2.825 3.04 3.665 3.08 2.81 3.08 2.81	A <sub>1pm</sub> ( 3 3.365 2.745 3.755 3.985 2.705 3.985 2.705 3.925 3.775 3.92 4.155 3.195 3.195	JFA, 4.275 4.425 3.795 3.815 4.365 3.81 3.85 5.04 4.525 4.615 4.71 4.485	UFAL 3.48 3.785 3.205 3.005 3.77 4.09 3.195 3.405 3.93 4.26 3.955 3.6 3.39	UFAc 4.73 4.29 4.39 3.99 4.305 5.105 4.475 4.11 4.03 4.83 4.835 4.835 4.535 4.56	LFA <sub>2m</sub> 2.483 2.055 1.895 2.085 2.77 2.44 1.577 2.17 2.23 2.033 2.033 2.61 2.19	LFA <sub>1m</sub> 5 2.88 5 2.22 5 2.54 5 2.66 2 2.76 9 3.34 5 2.59 7 2.6 5 2.71 5 2.6 1 3.07 9 2.5 3 3.05 7 2.5	LFA <sub>2pm</sub> 2 2. 7 2.9 5 2.9 4 2.8 5 2. 5 3. 5 2. 1 2. 5 3. 9 3. 5 3.6 7 2. 5 3.3	LFA1 79 45 45 65 96 97 91 16 35 15 75 75	pm LF/ 3.335 3.47 3.475 3.07 3.415 3.97 3.01 3.855 4 4.355 3.74 3.89	4.065 4.255 4.37 3.365 4.145 4.475 4.085 3.57 3.71 4.81 4.38 4.77 4.73	FAL 3.825 4.33 3.8 2.97 4.355 3.815 3.355 3.355 3.3475 3.98 4.005 4.135 3.53	LFA <sub>c</sub> 3.42 4.34 3.66 3.18 4.39 4.175 3.3 3.525 3.595 4.04 4.4 4.145 3.47
UFA2m 2.66 2.33 2.365 2.07 2.81 2.84 2.285 2.265 2.265 2.255 2.745 2.3255 3.185 1.975 2.185	UFA <sub>1m</sub> 2.31 2.22 2.32 2.99 3.6 2.55 1.1 2.55 1.1 2.55 1.1 2.5 2.34 3.6 2.5 2.34 3.6 2.5 2.34 2.34 2.34 2.34 2.34 2.34 2.34 2.34	UFA 55 15 29 05 05 05 55 45 03 55 55 35 55 35 55 55 35 55	2.77 2.77 2.68 2.48 3.065 3.315 2.275 2.405 3.04 3.665 3.08 2.81 2.975	A <sub>1pm</sub> ( 3 3.365 2.745 2.925 3.755 3.985 2.705 3.205 3.775 3.922 4.155 3.195 3.155 3.5	JFA, 4.275 4.425 3.795 3.815 4.365 3.81 3.85 5.04 4.525 4.615 4.71 4.485 5.07	UFAL 3.48 3.785 3.205 3.005 3.77 4.09 3.195 3.405 3.93 4.26 3.955 3.6 3.39 3.925	UFAc 4.73 4.29 4.39 3.99 4.305 5.105 4.475 4.11 4.03 4.83 4.845 4.535 4.535 4.566 4.466	LFA <sub>2m</sub> 2.483 2.055 1.895 2.085 2.77 2.44 1.577 2.13 2.235 2.033 2.033 2.033 2.033 2.033 2.235 2.3355 2.335 2.3355 2.3355 2.3355 2.3355 2.3355 2.3355 2.3355 2.3355 2.3355 2.3355 2.3355 2.33555 2.3355 2.3355 2.33555 2.335555 2.335555 2.335555555555	LFA1m 5 2.8 5 2.2 5 2.54 5 2.6 2 2.76 9 3.344 5 2.59 7 2.6 5 2.71 5 2.6 7 2.6 5 2.71 5 2.6 9 3.9 4 7 2.6 5 2.71 5 2.6 9 3.9 7 2.6 5 2.71 5 2.6 9 3.9 7 2.6 5 3.9 7 2.6 5 3.9 7 2.6 5 3.9 7 2.6 5 3.9 7 2.6 5 3.9 7 2.6 7 3.9 7 5.9 7	LFA <sub>2pm</sub> 2 2. 7 2.9 5 2.9 4 2.8 5 2.9 4 2.8 5 3.6 5 2. 1 2. 5 3. 9 3. 5 3.6 7 2. 5 3.3 5 3.3	LFA1 79 45 665 99 87 91 16 35 115 75 75 75	pm LF/ 3.335 3.47 3.475 3.475 3.07 3.415 3.97 3.01 3.855 4 4.355 3.74 3.89 3.69 3.69	4.065 4.255 4.357 3.365 4.145 4.475 4.085 3.57 3.71 4.81 4.38 4.77 4.73 4.75	FAL 3.825 4.33 3.8 2.97 4.355 3.815 3.355 3.355 3.475 3.98 4.005 4.135 3.53 4.045	LFA <sub>C</sub> 3.42 4.34 3.66 3.18 4.39 4.175 3.33 3.525 3.595 4.04 4.14 5.3.47 4.12
UFA <sub>2m</sub> 2.666 2.33 2.365 2.07 2.81 2.84 2.285 2.265 2.2745 2.255 2.745 2.3185 2.1375 2.185	UFA <sub>1m</sub> 2.34 2.22 2.5 3.6 2.5 1.1 2.3 3.6 2.5 1.2 2.3 3.6 2.3 3.6 2.3 2.3 3.6 2.3 3.6 2.3 3.6 2.3 3.6 2.3 3.6 2.3 3.6 2.3 3.6 2.3 3.6 2.5 3.5 3.6 2.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3	UFA 55 15 29 05 05 05 05 05 05 05 05 05 05 05 05 05	2.77 2.77 2.68 2.48 3.065 3.315 2.275 2.405 2.825 3.04 3.665 3.08 2.81 2.975 3.165 3.08	A <sub>1pm</sub> ( 3 3.365 2.745 2.925 3.755 3.985 2.705 3.925 3.775 3.922 4.155 3.195 3.155 3.5 3.6 3.5 3.5 3.5	JFA, 4.275 4.425 3.795 3.815 4.365 3.811 3.85 5.04 4.615 4.711 4.485 5.07 3.905	UFAL 3.48 3.785 3.205 3.005 3.77 4.09 3.195 3.405 3.93 4.26 3.955 3.66 3.39 3.925 3.56	UFAc 4.73 4.29 4.39 3.99 4.305 5.105 4.475 4.11 4.03 4.83 4.83 4.845 4.56 4.456 4.466 4.466 4.24	LFA2m 2.488 2.055 1.895 2.088 2.77 2.44 1.577 2.11 2.23 2.033 2.63 2.11 1.93 2.33 2.33	LFA <sub>1m</sub> 5 2.8 5 2.2 5 2.54 5 2.6 2 2.76 9 3.344 5 2.59 7 2.6 5 2.71 5 2.6 7 2.6 5 2.71 5 2.6 1 3.07 9 2.5 3 3.05 7 3.04 2 3.0	LFA2pm 2 2. 7 2.9 5 2.9 4 2.8 5 2.9 4 2.8 5 3. 5 3. 5 3.6 7 2. 5 3.3 5 3.8 4 2. 2 2 2	LFA1 79 45 66 69 29 87 91 16 35 115 75 75 75 89	pm LF/ 3.335 3.47 3.475 3.07 3.415 3.97 3.01 3.855 4 4.355 3.74 3.89 3.69 3.69 3.69	4.065 4.255 4.37 3.365 4.145 4.475 4.085 3.57 3.71 4.81 4.81 4.38 4.77 4.73 4.75 3.765 3.765	FAL 3.825 4.33 3.8 2.97 4.355 3.815 3.355 3.355 3.475 3.98 4.005 3.53 4.045 3.33	LFA <sub>C</sub> 3.42 4.34 3.66 3.18 4.39 4.175 3.3 3.525 3.595 4.04 4.4 4.145 3.47 4.12 3.59
UFA <sub>2m</sub> 2.666 2.33 2.365 2.07 2.81 2.84 2.285 2.265 2.2745 2.285 2.2745 2.325 3.185 1.975 2.135 2.133 3.095 2.405	UFA <sub>1m</sub> 2.34 2.22 2.21 2.20 2.90 3.6 2.55 1.1 2.34 3.6 2.34 2.34 2.34 2.34 2.34 2.34 2.34 2.34	UFA 555 125 229 55 55 56 55 56 55 56 55 56 55 56 55 56 55 55	2.77 2.68 2.48 3.065 3.315 2.275 2.405 2.825 3.04 3.665 3.04 3.665 3.08 2.81 2.975 3.165 2.915 3.165 2.915	A <sub>1pm</sub> ( 3 3.365 2.745 2.925 3.755 3.925 3.205 3.205 3.775 3.92 4.155 3.155 3.155 3.155 3.5 3.6 3.85 3.6	JFA, 4.275 4.425 3.795 3.815 4.355 4.365 3.81 3.85 5.04 4.525 4.615 4.71 4.485 5.07 3.905 5.055	UFAL 3.48 3.785 3.205 3.005 3.77 4.09 3.195 3.405 3.93 4.26 3.955 3.66 3.39 3.925 3.56 4.545	UFAc 4.73 4.29 4.39 3.99 4.305 5.105 4.475 4.1 4.03 4.83 4.835 4.835 4.845 4.56 4.46 4.24 5.1	LFA2m 2.488 2.055 1.899 2.088 2.77 2.49 1.577 2.11 2.235 2.03 2.61 2.19 1.939 2.31 2.33 2.33 3.00 2.511	LFA1m           5         2.8           5         2.25           5         2.64           6         2.67           3         3.34           5         2.76           6         2.6           7         2.66           1         3.07           9         2.53           3         3.05           7         3.04           2         3.02           3.2         3.02	LFA2pm 2 2.7 5 2.9 4 2.8 5 2.9 4 2.8 5 2.9 4 2.8 5 3.6 7 2. 5 3.6 7 2. 5 3.3 5 3.6 7 2. 5 3.3 5 3.8 4 2. 2 3.7 5 2.7	LFA <sub>1</sub> 79 45 45 45 96 29 87 91 16 35 115 75 75 45 89 115 65	pm LF/ 3.335 3.47 3.475 3.07 3.415 3.07 3.01 3.01 3.01 3.855 4 4.355 3.74 3.89 3.89 3.89 3.89 3.64 4.23 3.64	4.065 4.255 4.37 3.365 4.145 4.475 4.085 3.57 3.71 4.81 4.38 4.77 4.73 4.73 4.75 3.765 5.175 3.95	FAL           3.825           4.33           3.8           2.97           4.355           3.815           3.355           3.355           3.475           3.98           4.005           4.135           3.53           4.045           3.33           3.345	LFA <sub>c</sub> 3.42 4.34 3.66 3.18 4.39 4.175 3.3 3.525 4.04 4.44 4.145 3.47 4.12 3.59 4.359 4.325
UFA <sub>2m</sub> 2.66 2.33 2.365 2.07 2.81 2.84 2.285 2.265 2.2745 2.285 2.265 2.2745 2.2355 2.2745 2.2355 2.2745 2.2325 3.185 2.2	UFA <sub>1m</sub> 2.33 2.22 2.3 2.5 1.5 2.5 1.5 2.5 2.3 3.6 2.5 2.3 3.6 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3	UFA 55 15 229 55 55 55 55 55 55 55 55 55 55 55 55 55	2.77 2.77 2.68 2.48 3.065 3.045 2.825 3.04 3.665 3.08 2.81 2.975 2.975 2.915 2.925	A <sub>1pm</sub> 4 3 3.365 2.745 2.925 3.755 3.985 2.705 3.205 3.705 3.205 3.705 3.922 4.155 3.992 4.155 3.992 4.155 3.95 3.56 3.615 3.815 2.735 2.51	JFA, 4.275 4.425 3.795 3.815 4.365 3.81 3.85 4.365 4.365 4.615 4.525 4.615 4.71 4.485 5.07 3.905 5.055 4.45	UFAL 3.48 3.785 3.205 3.005 3.77 4.09 3.195 3.405 3.93 4.26 3.93 4.26 3.955 3.66 3.39 3.925 3.56 4.545 3.61 2.705	UFAc 4.73 4.29 4.39 3.99 4.305 5.105 4.475 4.11 4.03 4.835 4.555 4.555 4.555 4.455 4.565 4.466 4.464 5.11 4.535 4.535 4.515 4.535 4.515 4.535 4.515 4.5	LFA2m 2.488 2.055 1.899 2.088 2.77 2.45 2.03 2.03 2.03 2.03 2.03 2.03 2.33 2.33	LFA1m           5         2.8           5         2.2           5         2.54           6         2.54           6         2.59           7         2.66           5         2.71           5         2.71           5         2.71           5         2.71           5         2.71           5         2.71           7         3.04           2         3.02           3         3.02           2         3.2           5         2.67	LFA2pm 2 2. 7 2.9 5 2.9 4 2.8 5 2.9 4 2.8 5 2.9 1 2. 5 3.3 5 3.6 7 2. 5 3.3 5 3.8 4 2. 2 3.7 5 2.9 4 2.8 5 2.9 4 2.8 5 2.9 4 2.8 5 2.9 5 3.3 5 3.6 7 2.9 5 3.6 7 2.9 7 3.3 7 2.9 7 3.3 7 3.8 8 4 2.8 7 2.9 7 2.9 7 3.3 7 3.8 8 4 2.8 7 2.9 7 3.3 7 3.8 8 4 2.8 7 2.9 7 3.8 7 3.8 7 3.8 7 2.9 7 3.8 7 3.8 7 3.8 7 2.9 7 3.8 7 3.8 7 3.9 7 5 7 7 7 7 7	LFA <sub>1</sub> 79 45 45 65 96 29 91 16 35 15 75 75 45 89 15 65 595	pm         LF/           3.335         3.475           3.475         3.07           3.415         3.07           3.415         3.97           3.01         3           3.855         4           4.3555         3.74           3.89         3.69           3.64         4.23           3.23         2.685	4.065 4.255 4.37 3.365 4.145 4.475 4.085 3.57 3.71 4.81 4.38 4.77 4.73 4.73 3.765 5.175 3.925 5.175 3.925 4.18	FAL           3.825           4.33           3.8           2.97           4.355           3.815           3.355           3.335           3.435           3.98           4.005           4.135           3.53           4.045           3.33           3.345           3.325	LFA <sub>c</sub> 3.42 4.34 3.66 3.18 4.39 4.175 3.3 3.525 3.595 4.04 4.4 4.145 3.47 4.12 3.59 4.325 3.55
UFA2m UFA2m 2.666 2.33 2.365 2.07 2.81 2.84 2.285 2.265 2.745 2.255 2.745 2.255 2.745 2.235 2.245 2.235 2.185 2.255 2.21	UFA <sub>10</sub> 2.33 2.22 2.2 2.29 3.6 2.56 1.5 2.56 1.5 2.33 3.6 2.33 2.11 3.22 2.33 2.11 3.22 2.33 2.11 3.22 2.33 2.11 3.22 2.33 2.11 3.22 2.33 2.11 3.22 2.33 2.11 3.22 2.34 2.34 2.34 3.55 3.55 3.55 3.55 3.55 3.55 3.55 3	UFA 55 55 55 55 55 55 55 55 55 55 55 55 55	2.77 2.77 2.68 2.48 3.065 3.315 2.275 2.405 2.825 3.04 3.665 3.08 2.81 2.915 2.25 2.915 2.25 2.935 2.264	A <sub>1pm</sub> 4 3 3.365 2.745 2.925 3.755 3.205 3.205 3.205 3.205 3.752 3.155 3.195 3.155 3.155 3.55 3.51 2.735 3.51 2.835	JFA, 4.275 4.425 3.795 3.815 4.365 3.815 4.365 3.81 4.365 4.615 4.71 4.485 5.07 3.905 5.055 4.45 4.705 4.275	UFAL 3.48 3.785 3.205 3.005 3.785 3.405 3.405 3.93 4.26 3.955 3.60 3.393 3.925 3.566 4.545 3.61 3.795 3.104	UFAc 4.73 4.29 4.39 4.305 5.105 4.475 4.11 4.03 4.83 4.835 4.56 4.535 4.56 4.424 5.11 4.53 4.51 4.53 4.51 4.53 4.51 4.53 4.51 4.53 5.10 5.10 5.10 5.10 5.10 5.10 5.10 5.10	LFA2m 2.488 2.055 1.899 2.088 2.77 2.11 2.233 2.033 2.051 2.15 2.13 2.033 2.051 2.13 3.00 2.625 2.400 1.992 1.992 2.400 1.992 1	LFA1m           5         2.8           5         2.2           5         2.54           5         2.6           2         2.76           3         3.44           5         2.59           7         2.6           5         2.71           5         2.67           3         3.05           7         3.04           2         3.02           2         2.69           5         2.675           5         2.675	LFA2pm 2 2. 7 2.9 5 2.9 4 2.8 5 2. 5 3. 5 3. 5 3. 5 3. 5 3. 5 3. 5 3. 5 3. 5 3. 8 3. 5 3.8 4 2. 2 3.7 5 2.8 5 2.8 5 2.9 1 2. 5 3.8 4 2.8 5 3.8 4 2.8 5 3.8 4 2.8 5 3.8 5 3.8 4 2.8 5 3.8 5 3.8 7 5 2.8 7 5 7 5 2.8 7 5 7 5 2.8 7 5 7 5 7 5 7 5 7 5 7 5 7 5 7 5 7 5	LFA <sub>1</sub> 79 45 45 29 87 91 16 35 15 45 45 89 15 65 95 55	pm         LFJ           3.335         3.47           3.475         3.475           3.475         3.415           3.97         3.01           3.855         3.45           4.355         3.74           3.89         3.64           3.64         4.23           3.685         3.685	4.065 4.255 4.37 3.365 4.145 4.475 4.085 3.57 3.711 4.81 4.83 4.77 4.73 4.75 3.765 5.175 3.925 4.18 3.8	FAL           3.825           4.33           3.8           2.97           4.355           3.815           3.355           3.435           3.455           3.53           4.005           4.135           3.53           4.005           3.33           3.345           3.235           4.225	LFA <sub>C</sub> 3.42 4.34 3.66 3.18 4.39 4.175 3.3 3.525 3.595 4.04 4.4 4.145 3.47 4.12 3.59 4.325 3.55 4.33 3.985
UFA2m UFA2m 2.666 2.33 2.365 2.07 2.81 2.84 2.285 2.265 2.745 2.265 2.745 2.225 3.185 2.13 3.095 2.185 2.13 3.095 2.485 2.055	UFA100 2.33 2.32 2.22 2.22 2.29 3.6 2.50 1.5 2.50 1.5 2.50 2.33 3.6 2.33 2.33 2.33 2.33 2.33 2.33	UFA 55 52 52 53 55 55 55 55 55 55 55 55 55 55 55 55	2,2pm UF 2,77 2,77 2,68 2,48 3,065 2,825 3,045 2,825 3,04 2,811 2,975 3,165 2,935 2,935 2,045	A <sub>1pm</sub> 4 3 3.365 2.745 2.925 3.755 3.985 2.705 3.985 3.775 3.92 4.155 3.155 3.155 3.155 3.155 3.155 3.155 3.51 2.735 3.51 2.82 2.97	JFA, 4.275 4.425 3.795 3.815 4.365 3.81 3.85 4.365 3.81 3.85 4.365 4.525 4.615 4.715 4.715 5.055 5.055 5.055 4.45 4.705 4.275 4.025	UFAL 3.48 3.785 3.005 3.005 3.005 3.409 3.195 3.409 3.93 4.26 3.93 4.26 3.93 3.93 3.93 3.925 3.56 4.545 3.56 4.541 3.795 3.14 2.885	UFAc 4.73 4.29 4.39 3.99 4.305 5.105 4.475 4.1 4.03 4.83 4.83 4.83 4.845 4.535 4.56 4.46 4.24 5.11 4.53 4.29 4.29 4.29 4.23 4.21 4.21 4.21 4.21 4.21 4.21 4.21 4.21	LFA2m 2.483 2.055 1.895 2.065 2.07 2.45 2.17 2.23 2.03 2.61 2.11 1.93 2.33 3.00 2.62 2.40 1.943 3.01 2.40 1.943 2.41 2.41 4.411 4.4111 4.4111 4.4111 4.4111 4.4111 4.4111 4.4111 4.41111111111	LFA1m           5         2.8           5         2.25           5         2.54           6         2.66           2         2.76           3         3.34           5         2.59           7         2.66           2         3.71           5         2.67           3         3.02           5         2.675           5         2.675           5         2.63	LFA <sub>2pm</sub> 2 2. 7 2.9 5 2.9 4 2.8 5 2. 5 2. 5 3. 5 5. 5 5.	LFA1 79 45 45 45 96 97 91 16 35 15 45 89 15 45 89 15 56 59 57 58 86	LFJ           3.335           3.47           3.475           3.07           3.415           3.97           3.01           3.97           3.05           4           3.55           4           3.74           3.89           3.69           3.69           3.69           3.69           3.69           3.69           3.69           3.69           3.68           3.23           3.685           3.423	4.065 4.255 4.37 3.365 4.145 4.475 4.085 3.57 3.71 4.81 4.38 4.77 4.73 4.73 4.75 3.765 5.175 3.925 4.18 3.325	FA,         3.825           3.825         4.33           3.8         2.97           4.355         3.815           3.815         3.355           3.335         3.475           3.98         4.005           4.135         3.53           4.045         3.53           3.345         3.255           3.345         3.235           4.32         3.555           3.115         555	LFA <sub>C</sub> 3.42 4.34 3.66 3.18 4.39 4.175 3.3 3.525 3.595 4.04 4.14 4.145 3.47 4.12 3.59 4.325 3.55 4.33 3.985 2.47
UFA2m UFA2m 2.666 2.33 2.365 2.07 2.81 2.285 2.265 2.275 2.285 2.275 2.285 2.275 2.215 2.215 2.215 2.2455 2.2555 2.2555 2.2555 2.2555 2.2555 2.2555 2.2555 2.2555 2.2555 2.2555 2.2555 2.2555 2.25555 2.25555 2.25555 2.255555 2.255555555	UFA <sub>1m</sub> 2.3 2.2 2.2 2.2 2.9 3.0 2.5 1.1 2.5 2.3 3.0 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.1 1.9 2.3 3.1 9 2.3 2.3 2.3 2.1 2.3 3.1 2.3 2.3 3.1 2.3 3.1 2.3 3.1 2.3 3.1 2.5 5 5 5 5 5 5 7 5 7 5 7 7 7 7 7 7 7 7 7	UFA 55 55 55 55 55 55 55 55 55 55 55 55 55	2.277 2.77 2.77 2.68 2.48 3.065 3.315 2.275 2.405 3.065 3.04 3.665 3.04 3.665 3.08 2.81 2.825 3.04 3.665 3.08 2.81 2.975 3.165 2.2935 2.204 2.165	A <sub>1pm</sub> 4 3 3.365 2.745 2.925 3.755 3.985 2.705 3.985 3.775 3.92 4.155 3.155 3.155 3.155 3.155 3.155 3.51 2.735 3.51 2.8 2.97 3.79	JFA, 4.275 4.425 3.795 3.815 4.355 4.365 3.81 3.85 5.04 4.525 4.615 4.71 4.485 5.07 3.905 5.055 4.45 4.705 4.275 4.025 5.002	UFAL 3.48 3.785 3.205 3.005 3.77 4.09 3.195 3.405 3.93 4.26 3.955 3.66 3.39 3.925 3.56 4.545 3.56 4.545 3.61 3.795 3.14 2.885	UFAc 4.73 4.29 4.39 3.99 4.305 5.105 4.475 4.14 4.03 4.83 4.845 4.535 4.56 4.466 4.24 5.1 4.535 4.535 4.535 4.535 4.535 4.535 4.535	LFA2m 2.485 2.055 1.899 2.085 2.77 2.49 1.577 2.17 2.23 2.035 2.65 2.19 2.33 3.00 2.652 2.405 1.945 2.12 2.405 2.405 1.945 2.157 2.652 2.405 2.157 2.15	LFA1m           5         2.8           5         2.25           5         2.60           2         2.76           3         3.44           5         2.67           7         2.66           1         3.07           2         2.53           7         2.66           1         3.07           2         3.20           2         2.69           5         2.61           3         3.05           7         3.04           2         3.02           2         2.69           5         2.61           5         2.63           3         3.05           2         2.69           5         2.63           3         2.60           5         2.73	LFA <sub>2pm</sub> 2 2. 7 2.9 5 2.9 4 2.8 5 2. 5 3. 5 2. 1 2. 5 3. 9 3. 5 3. 9 3. 5 3. 8 3. 5 3.8 4 2. 2 3.7 5 2.7 5 2.8 5 2.2 3.8 4 2. 3.7 5 2.8 5 3.8 4 2.8 5 2.9 4 2.8 5 2.9 4 2.8 5 2.9 5 2.9 4 2.8 5 2.9 5 2.9 5 3.8 5 2.7 5 2.8 5 3.8 5	LFA1 79 45 45 96 97 91 16 35 91 16 35 75 45 89 15 65 89 55 55 88 95	LFJ           3.335           3.475           3.07           3.07           3.07           3.07           3.07           3.07           3.07           3.07           3.07           3.07           3.07           3.07           3.07           3.07           3.07           3.089           3.69           3.64           4.23           3.64           3.23           3.685           3.23           3.685           3.23           3.685           3.23           3.69	4.065 4.255 4.37 3.365 4.145 4.475 4.085 3.57 3.71 4.81 4.38 4.77 4.73 3.765 5.175 3.925 4.18 3.8 3.325 4.265	FAL           3.825           4.33           3.8           2.97           4.355           3.815           3.355           3.355           3.475           3.98           4.005           4.135           3.53           4.045           3.33           3.405           3.33           3.405           3.235           4.045           3.235           4.32           3.555           3.115	LFA <sub>c</sub> 3.42 4.34 3.66 3.18 4.39 4.175 3.3 3.525 4.04 4.44 4.145 3.59 4.325 4.32 3.595 4.33 3.985 2.47 3.95
UFA <sub>2m</sub> 2.666 2.33 2.365 2.07 2.81 2.84 2.285 2.245 2.265 2.745 2.325 3.185 2.245 2.325 3.185 2.133 3.095 2.485 2.055 2.1895 2.085 2.085 2.085	UFA <sub>1m</sub> 2.34 2.22 2.5 3.4 2.5 1.5 2.5 2.34 3.4 2.34 2.34 2.33 2.33 2.33 2.11 3.22 2.33 2.31 1.99 2.33 2.33 2.31 2.34 2.34 2.34 2.34 2.34 2.34 2.34 2.34	UFA 55 55 55 55 55 55 55 55 55 55 55 55 55	2.77 2.77 2.77 2.68 2.48 3.065 3.315 2.275 2.405 2.825 3.04 3.665 3.08 2.81 3.065 3.08 2.81 3.04 3.665 3.08 2.975 3.165 2.915 2.935 2.935 2.94 2.165 3.215	A <sub>1pm</sub> 4 3 3.365 2.745 2.925 3.755 3.985 2.705 3.985 3.755 3.922 4.155 3.195 3.195 3.195 3.195 3.195 3.55 3.6 3.815 2.735 3.51 2.8 2.97 3.79 3.775	JFA, 4.275 4.425 3.795 3.815 4.355 4.365 3.81 3.85 5.04 4.525 4.615 4.71 4.485 5.07 3.905 5.055 4.45 4.275 4.275 4.025 5.02 4.635	UFAL 3.48 3.785 3.205 3.005 3.77 4.09 3.195 3.405 3.93 4.26 3.955 3.61 3.795 3.61 3.795 3.14 2.885 3.14 4.825	UFAc 4.73 4.29 4.39 3.99 4.305 5.105 4.475 4.475 4.475 4.433 4.833 4.835 4.565 4.466 4.464 4.24 5.11 4.535 4.455 4.355 4.	LFA2m 2.483 2.055 1.899 2.083 2.77 2.44 1.577 2.13 2.23 2.033 2.63 2.15 2.15 2.33 2.33 3.00 2.632 2.400 1.945 2.400 1.945 2.400	LFA1m           5         2.8           5         2.25           5         2.69           6         2.69           7         2.66           5         2.76           8         3.07           9         2.53           3         3.05           7         3.04           2         3.00           5         2.67           5         2.76           5         2.67           5         2.63           8         3.05           7         3.04           2         3.00           5         2.67           5         2.63           8         2.60           5         2.75           5         3.44	LFA2pm 2 2. 7 2.9 5 2.9 4 2.8 5 2.9 4 2.8 5 2.9 1 2.8 5 2.1 1 2.8 5 3.3 5 3.6 7 2. 5 3.3 5 3.8 4 2.8 5 3.6 7 2. 5 3.3 5 3.8 5 5 3.8 5 5 3.8 5 5 3.8 5 5 5	LFA1 79 45 665 99 87 91 16 35 45 45 89 16 35 45 89 15 45 89 15 75 45 89 5 5 75 88 65 95 5 75 88 65 95 65 75 65 75 65 75 88 65 75 88 75 75 88 75 75 75 75 75 75 75 75 75 75 75 75 75	LFJ           3.335           3.475           3.475           3.07           3.07           3.01           3.855           4.355           3.69           3.69           3.69           3.645           3.635           3.645           3.625           3.625           3.625           3.625           3.625           3.625           3.625           3.625           3.625           3.625	4.065 4.255 4.37 3.365 4.145 4.475 4.085 3.57 3.71 4.81 4.38 4.77 4.73 3.765 5.175 3.765 5.175 3.925 4.18 3.8 3.325 4.269	FAL           3.825           4.33           3.8           2.97           4.355           3.815           3.355           3.355           3.475           3.98           4.005           4.135           3.353           3.475           3.33           3.345           3.334           3.345           3.235           4.045           3.33           3.405           3.235           4.045           3.315           4.045	LFA <sub>c</sub> 3.42 4.34 3.66 3.18 4.39 4.175 3.39 4.175 3.59 4.04 4.145 3.47 4.12 3.59 4.325 3.55 4.325 3.55 4.33 3.985 2.47 3.95
UFA2m UFA2m 2.66 2.33 2.365 2.07 2.81 2.84 2.285 2.265 2.2745 2.2755 2.185 2.13 3.095 2.185 2.13 3.095 2.485 2.055 2.185 2.055 2.055 2.055 2.085 2.205	UFA <sub>100</sub> 2.34 2.34 2.22 2.2 2.5 1.5 2.5 3.4 2.5 3.4 2.5 3.4 2.3 3.4 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3	UFA 55 55 55 55 55 55 55 55 55 55 55 55 55	2.77 2.77 2.77 2.68 2.48 3.065 3.065 3.04 3.665 3.08 2.81 2.975 2.405 3.04 3.665 3.08 2.81 2.975 2.915 2.25 2.935 2.04 2.165 3.205 3.205 3.205	A <sub>1pm</sub> 4 3 3.365 2.745 2.925 3.755 3.985 2.705 3.205 3.705 3.205 3.705 3.922 4.155 3.195 3.195 3.195 3.195 3.195 3.55 3.6 3.815 2.735 3.6 3.815 2.735 3.51 2.735 3.75 2.96	JFA, 4.275 4.425 3.795 3.815 4.355 4.365 3.81 3.85 5.04 4.525 4.615 4.71 4.485 5.07 3.905 5.055 4.45 4.705 4.275 4.025 5.02 4.635 3.755	UFAL 3.48 3.785 3.205 3.005 3.195 3.405 3.93 4.26 3.93 4.26 3.955 3.66 3.393 3.925 3.56 4.545 3.61 3.795 3.61 3.795 3.14 2.885 4.1 4.285 4.1 4.285 3.41	UFAc 4.73 4.29 4.39 3.99 4.305 5.105 4.475 4.11 4.03 4.835 4.565 4.455 4.555 4.455 4.555 4.455 4.555 4.429 4.535 4.29 4.535 4.29 4.315 5.105 5.27 4.335 5.27 4.305 5.27 4.305 5.27 4.305 5.27 4.305 5.27 4.305 5.27 4.305 5.27 4.305 5.27 4.305 5.27 4.305 5.27 4.305 5.27 4.305 5.27 4.305 5.27 4.305 5.27 4.305 5.27 5.27 4.305 5.27	LFA2m 2.483 2.055 1.899 2.083 2.77 2.11 2.233 2.033 2.63 2.15 1.93 2.33 2.33 2.33 2.33 2.33 2.405 1.944 2.13 2.405 1.944 2.13 2.644 2.15 2.644 2.15 2.644 2.15 2.644 2.15 2.644 2.15 2.644 2.15 2.644 2.15 2.644 2.15 2.644 2.15 2.644 2.15 2.644 2.15 2.644 2.15 2.644 2.15 2.644 2.15 2.644 2.15 2.644 2.15 2.644 2.15 2.15 2.15 2.15 2.15 2.15 2.15 2.15	LFA1           5         2.8           5         2.2           5         2.54           5         2.54           5         2.59           7         2.6           5         2.71           5         2.71           5         2.71           5         2.71           5         2.61           3         3.05           7         3.04           2         3.25           5         2.675           5         2.675           5         2.63           6         2.675           7         3.04           5         2.71           5         3.444           5         2.72           5         3.44	LFA2pm 2 2. 7 2.9 5 2.9 4 2.8 5 2.9 4 2.8 5 2.9 1 2. 5 3.3 5 3.6 7 2. 5 3.3 5 3.8 4 2. 2 3.7 5 2.8 5 2.8 5 2.5 4 3.2 5 2.9 4 3.2 5 3.3 5 3.8 4 2. 2 3.7 5 2.8 5 2.8 5 2.9 4 2.8 5 3.6 5 3.3 5 3.8 4 2.8 5 3.6 5 3.3 5 3.8 4 2.8 5 3.6 5 3.3 5 3.8 4 2.8 5 3.8 4 2.8 5 3.8 5 3.8	LFA1 79 45 45 45 29 87 91 16 35 115 45 88 95 75 88 80 55 86 65 95	LFJ           3.335           3.47           3.475           3.475           3.07           3.01           3           3.415           3.97           3.01           3           3.855           3.74           3.855           3.74           3.685           3.645           3.645           3.425           3.425           3.645           3.645           3.425           3.425           3.425           3.425           3.425           3.425           3.425           3.425           3.425           3.425           3.425           3.425           3.425           3.425	4.065 4.255 4.37 3.365 4.145 4.475 4.085 3.57 3.71 4.81 4.38 4.77 4.73 4.75 3.765 5.175 3.765 5.175 3.765 5.175 3.925 4.18 3.8 3.325 4.265 4.265 4.79 3.65	FAL           3.825           4.33           3.8           2.97           4.355           3.815           3.335           3.435           3.335           3.475           3.98           4.005           4.135           3.33           3.345           3.235           4.045           3.33           3.345           3.235           4.025           3.115           4.005           4.11           3.655	LFA <sub>c</sub> 3.42 4.34 3.66 3.18 4.39 4.175 3.3 3.525 3.595 4.04 4.4 4.145 3.47 4.12 3.59 4.325 3.985 2.47 3.985 2.47 3.985 2.47 3.985 2.47
UFA2m UFA2m 2.666 2.33 2.365 2.07 2.81 2.84 2.285 2.265 2.2745 2.2745 2.2755 2.2745 2.2745 2.2755 2.18	UFA <sub>1</sub> , 2.3 2.3 2.2 2.2 2.2 2.5 1.5 2.5 2.3 3.6 2.5 2.3 3.6 2.3 2.3 2.3 2.1 3.2 2.3 2.1 2.3 2.1 2.3 2.1 2.3 2.1 2.3 2.1 2.3 2.1 2.3 2.1 2.3 2.1 2.3 2.3 2.1 2.3 3.6 2.3 2.3 2.3 3.6 2.3 2.3 3.6 2.3 2.3 3.6 2.3 2.3 3.6 2.3 2.3 3.6 2.3 2.3 3.6 2.3 2.3 2.3 3.6 2.3 3.6 2.3 3.6 2.3 2.3 3.6 2.3 3.6 2.3 3.6 2.3 3.6 2.3 3.6 2.3 3.6 2.3 3.6 2.3 2.3 3.6 2.3 3.6 2.3 3.6 2.3 3.6 2.3 2.3 3.6 2.3 3.6 2.3 3.6 2.3 3.6 2.3 3.6 2.3 3.6 2.3 3.6 2.3 3.6 2.3 3.6 2.3 3.6 2.3 3.6 2.3 3.6 2.3 3.6 2.3 3.6 2.3 3.6 2.3 3.6 2.3 3.2 3.2 2.3 3.2 2.3 3.2 2.3 3.2 2.3 3.2 2.3 3.2 2.3 3.2 2.3 3.2 2.3 3.2 2.3 3.2 2.3 3.2 2.3 3.2 2.3 3.2 2.3 3.2 2.3 2.3	UFA 55 55 55 55 55 55 55 55 55 55 55 55 55	2.77 2.77 2.77 2.68 2.48 3.065 3.315 2.275 2.405 2.825 3.04 3.665 3.08 2.81 2.975 2.915 2.915 2.2915 2.2915 2.2915 2.2915 2.204 2.165 3.215 3.205 2.366	A <sub>1pm</sub> 4 3 3.365 2.745 2.745 3.755 3.985 2.705 3.205 3.725 3.205 3.725 3.195 3.195 3.155 3.195 3.155 3.55 3.55 3.51 2.735 3.51 2.88 2.97 3.775 2.965 3.255	JFA, 4.275 4.425 3.795 3.815 4.365 3.81 3.88 5.04 4.525 4.615 4.71 4.485 5.07 3.905 5.055 4.45 4.705 4.275 4.025 5.02 4.635 3.755 3.775	UFAL 3.48 3.785 3.205 3.005 3.77 4.09 3.195 3.405 3.93 4.26 3.93 3.93 3.925 3.56 4.545 3.61 3.795 3.14 2.885 4.1 4.825 3.44 3.34	UFAc 4.73 4.29 4.39 4.305 5.105 4.475 4.11 4.03 4.835 4.565 4.455 4.565 4.464 5.11 4.535 4.29 4.535 4.24 5.11 4.335 5.27 4.36 3.775 4.36 4.375 4.36 4.355 4.	LFA2m 2.488 2.055 1.899 2.088 2.77 2.44 1.575 2.17 2.233 2.033 2.033 2.033 2.031 2.455 1.93 2.33 3.007 2.625 2.405 1.944 2.13 2.645 2.765 1.725 2.238 2.238 2.765 1.725 2.238 2.238 2.765 1.725 2.238 2.238 2.765 1.725 2.238 2.765 1.725 2.238 2.765 1.725 2.238 2.7555 2.755 2.755 2.755 2.755 2.755 2.755 2.7555 2.7555	LFA1           5         2.8           5         2.2           5         2.54           5         2.54           5         2.59           7         2.66           5         2.71           5         2.67           5         2.71           5         2.67           5         2.73           3         3.057           7         3.044           2         3.29           5         2.675           5         2.633           2         3.02           5         2.633           5         2.633           5         2.633           5         2.633	LFA2pm 2 2. 7 2.9 5 2.9 4 2.8 5 2. 5 3. 5 2. 1 2. 5 3. 5 3. 5 3. 6 3. 5 3. 6 3. 5 3. 6 3. 6 3. 7 2. 5 3.3 5 3.8 4 2. 2 3.7 5 2.8 5 2. 4 3.2 5 2. 5 2. 4 3.2 5 2. 5 3.8 4 2. 5 3.8 5 5 2. 5 5 2. 5 5 2. 5 5 2. 5 5 5 2. 5 5 5 5 2. 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	LFA1 79 45 45 45 29 87 91 16 35 15 45 89 15 45 89 595 75 86 80 595 97	LFA           3.335           3.47           3.475           3.475           3.475           3.475           3.475           3.415           3.97           3.01           3           3.855           3.74           3.859           3.645           3.642           4.233           3.685           3.625           3.625           3.02           3.4255           3.02           3.725           2.955           3.235	4.065 4.255 4.37 3.365 4.145 4.475 4.085 3.57 3.71 4.81 4.81 4.88 4.77 4.73 4.75 3.765 5.175 3.925 4.18 3.88 3.325 4.265 4.79 3.65 3.38	FAL           3.825           4.33           3.8           2.97           4.355           3.815           3.355           3.335           3.475           3.98           4.005           4.135           3.53           4.045           3.33           3.345           3.235           3.115           4.005           4.11           3.666           3.295	LFA <sub>c</sub> 3.42 4.34 3.66 3.18 4.39 4.175 3.3 3.525 3.595 4.04 4.4 4.145 3.47 4.12 3.59 4.325 3.55 4.33 3.985 2.47 3.95 3.96 3.685 3.355
UFA2m UFA2m 2.666 2.33 2.365 2.07 2.81 2.84 2.285 2.265 2.745 2.255 2.745 2.255 2.745 2.255 2.745 2.255 2.133 2.215 2.215 2.20	UFA <sub>1m</sub> 2.34 2.22 2.5 2.5 3.6 2.5 1.5 2.3 3.6 2.3 2.3 3.6 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3 2.3	UFA 515 529 55 55 55 55 55 55 55 55 55 55 55 55 55	2.77 2.77 2.77 2.68 2.48 3.065 3.315 2.275 2.405 3.04 3.665 3.04 3.665 3.04 3.665 3.04 3.665 3.04 2.825 3.04 2.825 3.04 2.825 2.915 3.205 2.235 2.24 2.935 2.24 2.825 2.24 2.825 2.825 2.935 2.25 2.24 2.825 2.25 2.25 2.25 2.25 2.25 2.25 2.2	A <sub>1pm</sub> 4 3 3.365 2.745 2.925 3.755 3.985 2.705 3.985 3.775 3.92 4.155 3.155 3.155 3.155 3.155 3.155 3.155 3.55 3.	JFA, 4.275 4.425 3.795 3.815 4.365 3.815 4.365 3.81 3.85 5.04 4.525 4.615 4.71 4.425 5.07 3.905 5.055 4.45 5.055 4.275 4.025 5.055 4.275 4.025 5.055 4.275 4.275 4.025 5.027 4.635 3.775	UFAL 3.48 3.785 3.205 3.005 3.005 3.409 3.195 3.403 3.93 4.26 3.955 3.66 3.955 3.66 4.545 3.56 4.545 3.56 4.545 3.14 2.885 3.14 2.885 3.14 2.885 3.14 3.333 4.025	UFAc 4.73 4.29 4.39 3.99 4.305 5.105 4.475 4.475 4.475 4.475 4.475 4.475 4.475 4.475 4.475 4.475 4.535 4.535 4.24 5.11 5.125 4.426 4.24 5.11 5.125 4.29 4.535 5.27 4.36 3.775 4.39	LFA2m 2.483 2.055 1.899 2.077 2.49 1.577 2.17 2.233 2.035 2.61 2.19 2.33 3.07 2.62 2.405 1.945 2.11 2.644 2.11 2.644 2.11 2.644 2.11 2.644 2.11 2.645 1.945 2.11 2.645 1.945 2.11 2.645 1.945 2.11 2.645 1.945 2.11 2.645 1.945 2.11 2.645 1.945 2.11 2.11 2.11 2.11 2.11 2.11 2.11 2.1	LFA1m           5         2.8           5         2.25           5         2.60           2         2.76           3         3.44           5         2.61           5         2.61           5         2.61           5         2.61           5         2.61           5         2.61           5         2.61           3         3.05           7         3.04           2         3.25           5         2.675           5         2.603           5         2.675           5         2.61           5         2.725           5         2.74	LFA <sub>2pm</sub> 2 2. 7 2.9 5 2.9 4 2.8 5 2. 5 2. 5 3. 5 3. 6 3. 9 3. 5 3. 6 3. 7 2. 5 3. 6 3. 7 2. 5 3. 6 3. 8 4 2. 2 3. 7 2. 5 3. 6 3. 8 4 2. 2 5 3. 8 5 2. 9 3. 5 3. 6 3. 7 2. 9 3. 8 5 3. 6 3. 7 2. 9 3. 8 5 3. 9 3. 8 5 3. 9 3. 8 5 3. 9 3. 8 5 3. 9 3.	LFA1 79 45 665 99 87 91 16 35 15 75 75 45 89 91 15 65 95 75 88 65 95 97 12	LFJ           3.335           3.475           3.475           3.07           3.07           3.07           3.07           3.07           3.07           3.07           3.07           3.07           3.085           4           3.55           3.665           3.423           3.685           3.423           3.685           3.425           3.02           3.725           4.23           3.685           3.423           3.665           3.225           3.235	4.065 4.255 4.37 3.365 4.145 4.085 3.57 3.71 4.81 4.38 4.77 4.73 4.75 3.765 5.175 3.925 4.18 3.825 4.265 3.325 4.265 3.38 3.87	FAL         3.825           3.825         4.333           3.8         2.97           4.355         3.815           3.815         3.355           3.355         3.375           3.475         3.98           4.005         4.135           3.345         3.345           3.355         3.155           3.345         3.235           4.32         3.555           3.155         3.165           4.105         4.105           3.666         3.295           3.245         3.245	LFA <sub>c</sub> 3.42 4.34 3.66 3.18 4.175 3.3 3.525 3.595 4.04 4.145 3.59 4.04 4.12 3.59 4.325 4.33 3.985 2.47 3.95 3.96 3.685 3.356
UFA2m UFA2m 2.666 2.33 2.365 2.07 2.81 2.285 2.265 2.275 2.285 2.275 2.235 2.275 2.185 2.2455 2.2455 2.2455 2.2455 2.2455 2.2455 2.2055 2.2455 2.2055 2.2455 2.2055 2.2455 2.2055 2.2455 2.2055 2.2455 2.2055 2.2455 2.2055 2.2455 2.2055 2.2455 2.2055 2.2455 2.2055 2.2455 2.2055 2.2455 2.2055 2.2475 2.2475 2.24555 2.24555 2.2455555 2.245555555555	UFA <sub>1m</sub> 2.34 2.22 2.5 2.24 2.99 3.6 2.5 2.34 3.6 2.5 2.34 3.6 2.33 2.33 2.33 2.33 2.33 2.33 2.33	UFA 55 15 29 55 55 55 55 55 55 55 55 55 55 55 55 55	2.277 2.77 2.77 2.68 2.48 3.065 3.315 2.275 2.405 3.04 3.665 3.04 3.665 3.08 2.81 3.08 2.81 3.08 2.81 3.08 2.81 3.08 2.81 3.08 2.81 2.975 3.165 3.205 2.04 2.165 3.215 2.235 2.04 2.165 3.205 2.366	A <sub>1pm</sub> ( 3 3.365 2.745 2.925 3.755 3.985 2.705 3.985 3.775 3.92 4.155 3.775 3.155 3.155 3.155 3.155 3.155 3.155 3.51 2.735 3.51 2.8 2.73 3.51 2.8 2.97 3.775 2.965 3.255 3.339	JFA, 4.275 4.425 3.795 3.815 4.355 4.365 3.81 3.80 4.355 4.615 4.71 4.485 5.07 3.905 5.055 4.45 4.705 4.275 4.025 5.025 3.775 3.777 4.715	UFAL 3.48 3.785 3.205 3.005 3.77 4.09 3.195 3.405 3.935 3.405 3.955 3.66 4.545 3.39 3.925 3.56 4.545 3.61 3.795 3.14 2.885 4.11 4.825 3.44 3.33 4.025	UFAc 4.73 4.29 4.39 3.99 4.305 5.105 4.475 4.14 4.03 4.83 4.835 4.535 4.555 4.466 4.466 4.24 5.11 4.335 4.535 4.355 4.315 4.335 5.277 4.366 3.775 4.39 4.685 5.275 4.39 4.395 5.275 4.395 5.277 4.395 5.277 4.395 5.277 4.395 5.277 4.395 5.277 4.395 5.277 4.395 5.277 4.395 5.277 4.395 5.277 4.395 5.277 4.395 5.277 4.395 5.277 4.395 5.277 4.395 5.277 4.395 5.277 5.275 5.277 5.275 5.277 5.275 5.277 5.275	LFA2m 2.483 2.055 1.899 2.085 2.77 2.43 1.577 2.13 2.23 2.65 2.13 3.07 2.62 2.405 1.945 2.765 1.945 2.405 1.945 2.15 2.405 1.945 2.15 2.405 1.945 2.15 2.25 2.25 2.15 2.15 2.25 2.15 2.25 2.15 2.25 2.15 2.15 2.25 2.15 2.15 2.25 2.15 2.	LFA1m           5         2.8           5         2.25           5         2.60           2         2.76           3         3.44           5         2.61           7         2.66           2         2.76           7         2.61           3         3.05           7         3.04           2         3.20           2         2.69           5         2.77           5         2.77           5         2.77           5         2.75           5         2.75           5         2.75           5         2.75           5         2.75           5         2.75	LFA2pm 2 2. 7 2.9 5 2.9 4 2.8 5 2.9 5 2.5 3.6 5 2. 1 2. 5 3. 9 3. 5 3.6 7 2. 5 3.3 5 3.6 7 2. 5 3.8 4 2. 5 3.8 4 2. 5 3.8 5 2. 9 3.8 5 3.8 5 2. 9 3.8 5 2.8 5 3.8 5 2.8 5 3.8 5 2.8 5 3.8 5 2.8 5 2.8 5 3.8 5 3.8 5 2.8 5 3.8 5 3.8 5 2.8 5 3.8 5 3	LFA1 79 45 665 99 29 87 91 16 35 75 45 89 15 45 89 95 95 95 95 97 12 85	LFJ           3.335           3.475           3.475           3.07           3.07           3.07           3.07           3.07           3.07           3.07           3.07           3.07           3.07           3.07           3.07           3.07           3.07           3.07           3.07           3.07           3.09           3.64           4.23           3.685           3.23           3.685           3.23           3.645           3.23           3.645           3.23           3.645           3.23           3.625           3.725           3.235           3.235           3.235           3.235           3.235           3.235           3.235           3.665           3.665	4.065 4.255 4.37 3.365 4.145 4.475 4.085 3.57 3.71 4.81 4.38 4.77 4.73 3.765 5.175 3.925 5.175 3.925 4.18 3.825 4.265 3.325 4.279 3.655 3.38 3.87	FAL           3.825           4.33           3.8           2.97           4.355           3.815           3.355           3.355           3.355           3.357           3.475           3.53           4.005           4.135           3.235           4.32           3.555           3.155           4.025           4.32           3.555           3.115           4.025           4.11           3.66           3.295           3.46	LFA <sub>c</sub> 3.42 4.34 3.66 3.18 4.39 4.175 3.3 3.525 3.595 4.04 4.44 4.145 3.595 4.04 4.47 3.59 4.33 3.985 4.33 3.985 2.477 3.95 3.966 3.685 3.355 3.565 3.565 3.566 3.805
UFA2m UFA2m 2.66 2.33 2.365 2.07 2.81 2.285 2.265 2.245 2.255 2.245 2.325 3.185 2.245 2.325 3.185 2.245 2.213 2.265 2.245 2.213 2.205 2.249 2.205 2.249 2.205 2.249 2.205 2.217 2.235 2.20	UFA <sub>100</sub> 2.34 2.34 2.52 2.5 3.4 2.55 1.4 2.55 1.5 2.54 2.54 2.34 2.34 2.34 2.34 2.33 2.34 2.33 2.34 2.34	UFA 55 15 15 15 15 15 15 15 15 15 15 15 15	2.277 2.77 2.77 2.68 2.48 3.065 3.315 2.275 2.405 2.825 3.04 3.665 3.08 2.81 3.04 3.665 3.08 2.81 3.04 3.665 3.08 2.975 3.165 2.975 3.165 2.935 2.935 2.935 2.04 2.165 3.215 3.205 2.236 2.675 2.38 2.236 2.675 3.205 3.	A <sub>1pm</sub> ( 3 3.365 2.745 2.925 3.755 3.985 2.705 3.985 3.755 3.922 4.155 3.755 3.755 3.795 3.155 3.195 3.155 3.55 3.6 3.815 2.735 3.51 2.8 2.97 3.79 3.775 2.965 3.255 3.435 3.435 3.435	JFA, 4.275 4.425 3.795 3.815 4.355 4.365 3.811 3.85 5.04 4.525 4.615 4.711 4.485 5.07 3.905 5.055 4.45 4.705 4.275 4.025 5.02 4.635 3.775 3.775 3.775 4.715	UFAL 3.48 3.785 3.205 3.005 3.77 4.09 3.195 3.405 3.93 4.26 3.955 3.61 3.92 3.56 4.545 3.61 3.795 3.14 2.885 4.14 4.825 3.344 3.33 4.025 4.15	UFAc 4.73 4.29 4.39 3.99 4.305 5.105 4.475 4.41 4.03 4.83 4.835 4.535 4.545 4.545 4.545 4.535 4.545 4.535 4.535 4.31 4.535 4.355 4.35	LFA2m 2.488 2.055 1.899 2.083 2.77 2.44 1.577 2.13 2.23 2.033 2.63 2.15 2.33 3.00 2.642 2.440 1.945 2.400 1.945 2.400 1.945 2.400 1.945 2.405 1.725 2.235 2.355 1.995 2.956 1.995 2.956 1.995 2.956 1.995 2.956 1.995 2.956 1.995 2.956 1.995 2.956 1.995 1.9	LFA1m           5         2.8           5         2.25           5         2.64           6         2.67           7         2.66           7         2.67           6         2.76           7         2.64           7         2.67           8         3.07           9         2.53           3         3.05           7         3.04           2         3.00           5         2.67           5         2.63           8         2.69           5         2.77           5         3.44           5         2.75           5         2.75           5         2.70           8         2.03	LFA2pm 2 2. 7 2.9 5 2.9 4 2.8 5 2.9 5 2.5 3.6 5 2.1 1 2. 5 3.3 5 3.6 7 2. 5 3.6 7 2. 5 3.6 7 2. 5 3.3 5 3.8 4 2. 7 2. 5 3.3 5 3.8 5 3	LFA1 79 45 665 99 87 91 16 35 45 45 89 15 45 89 15 445 89 15 65 95 75 86 95 95 95 97 12 85 85 85 85	LFJ           3.335           3.475           3.475           3.07           3.07           3.01           3.875           4.355           3.74           3.69           3.69           3.69           3.685           3.685           3.625           3.725           3.625     <	4.065 4.255 4.37 3.365 4.145 4.475 4.085 3.57 3.71 4.81 4.38 4.77 4.73 3.765 5.175 3.925 4.18 3.325 4.265 4.265 4.265 3.38 3.38 3.38 3.387 4.55	FAL           3.825           4.33           3.8           2.97           4.355           3.815           3.355           3.355           3.355           3.355           3.355           3.355           3.475           3.475           3.345           3.345           3.345           3.345           3.555           3.115           4.005           4.11           3.66           3.295           3.46           3.91	LFA <sub>c</sub> 3.42 4.34 3.66 3.18 4.39 4.175 3.3 3.525 4.04 4.145 3.59 4.04 4.145 3.59 4.325 3.55 4.325 3.56 3.665 3.855 3.56 3.855 4.345 3.565 3.5555 3.555 3.555
UFA2m UFA2m 2.666 2.33 2.365 2.07 2.81 2.84 2.285 2.265 2.2745 2.275 2.185 2.2745 2.133 3.095 2.185 2.133 3.095 2.485 2.055 2.185 2.205 2.185 2.205 2.	UFA <sub>100</sub> 2.34 2.34 2.54 2.59 3.6 2.55 1.5 2.34 3.6 2.34 2.34 2.34 2.34 2.34 2.34 2.34 2.34	UFA 55 15 15 15 15 15 15 15 15 15 15 15 15	2.277 2.77 2.77 2.68 2.48 3.065 3.065 3.045 2.275 2.405 2.825 3.04 3.665 3.08 2.81 3.065 3.08 2.81 3.065 3.08 2.975 3.165 2.975 2.915 2.915 2.944 2.165 3.205 2.38 2.36 2.38 2.36 2.38 2.36 2.38 2.36 2.38 2.36 3.422 3.425	A <sub>1pm</sub> ( 3 3.365 2.745 2.925 3.755 3.985 2.705 3.205 3.205 3.205 3.205 3.922 4.155 3.195 3.195 3.195 3.195 3.195 3.55 3.6 3.815 2.735 3.6 3.815 2.735 3.6 3.815 2.735 3.55 3.6 3.815 2.975 3.75 2.965 3.255 3.435 3.39 4.185 2.805	JFA, 4.275 4.425 3.795 3.815 4.355 4.365 3.81 3.85 4.365 4.615 4.71 4.485 5.07 3.905 5.055 4.475 4.275 4.025 5.02 4.635 3.775 4.715 3.775 4.715 4.511	UFAL 3.48 3.785 3.205 3.005 3.77 4.09 3.195 3.405 3.93 4.26 3.93 3.925 3.66 3.393 3.925 3.66 3.393 3.925 3.61 3.795 3.14 2.885 4.14 4.825 3.34 4.285 4.15 4.28 3.51	UFAc 4.73 4.29 4.39 4.39 4.305 5.105 4.475 4.475 4.43 4.835 4.565 4.466 4.466 4.464 4.51 4.535 4.315 5.27 4.39 4.535 5.27 4.39 4.685 5.27 4.39 4.685 5.27 4.39 4.685 5.27 4.39 5.27 4.39 5.27 5.2	LFA2m 2.488 2.055 1.899 2.083 2.77 2.49 1.577 2.13 2.033 2.033 2.033 2.033 2.033 2.033 2.033 2.15 1.992 2.235 1.995 2.962 2.95 1.995 2.962	LFA1m           5         2.8           5         2.25           5         2.54           5         2.54           5         2.54           5         2.54           5         2.54           5         2.59           7         2.65           5         2.71           5         2.67           3         3.05           7         3.04           2         3.63           2         3.63           5         2.675           5         2.75           5         3.44           2         2.75           5         2.77           5         2.77           5         2.70           5         2.77           5         2.70           5         2.70           5         2.70           5         2.70           5         2.70           5         2.70           5         2.70           5         2.70           5         2.70           5         2.70      5	LFA2pm 2 2. 7 2.9 5 2.9 4 2.8 5 2.9 4 2.8 5 2.9 4 2.8 5 2.9 3 .3 5 2.1 5 3.8 7 2. 5 3.8 7 2. 5 3.8 7 2. 5 3.8 7 2. 5 3.8 5 3.8	LFA1 79 45 65 29 87 91 16 35 115 75 45 89 75 45 89 95 95 95 95 97 22 86 59 5 95 95 97 12 83 5 15	LFJ           3.335           3.47           3.475           3.475           3.475           3.475           3.475           3.475           3.475           3.475           3.415           3.97           3.01           3           3.855           3.74           3.69           3.64           4.23           3.69           3.64           4.23           3.69           3.64           3.63           3.645           3.62 </td <td>4.065 4.255 4.37 3.365 4.145 4.475 4.085 3.57 3.71 4.81 4.38 4.77 4.73 4.73 3.765 5.175 3.765 5.175 3.925 4.18 3.8 3.325 4.265</td> <td>FAL           3.825           4.33           3.8           2.97           4.355           3.815           3.355           3.355           3.355           3.355           3.355           3.355           3.355           3.3475           3.333           3.345           3.235           4.045           3.333           3.345           3.235           3.115           4.005           4.11           3.66           3.295           3.46           3.91           4.02</td> <td>LFA<sub>c</sub> 3.42 4.34 3.66 3.18 4.39 4.175 3.3 3.525 3.595 4.04 4.4 4.145 3.47 4.12 3.595 4.04 4.415 3.47 4.125 3.555 3.555 3.555 3.985 2.47 3.985 3.395 3.395 3.355 3.355 3.566 3.805 3.355 3.56 3.805 3.421 3.95 3.955 3.565 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.805 3.556 3.355 3.566 3.5666 3.566 3.566 3.5666 3.5666 3.5666</td>	4.065 4.255 4.37 3.365 4.145 4.475 4.085 3.57 3.71 4.81 4.38 4.77 4.73 4.73 3.765 5.175 3.765 5.175 3.925 4.18 3.8 3.325 4.265	FAL           3.825           4.33           3.8           2.97           4.355           3.815           3.355           3.355           3.355           3.355           3.355           3.355           3.355           3.3475           3.333           3.345           3.235           4.045           3.333           3.345           3.235           3.115           4.005           4.11           3.66           3.295           3.46           3.91           4.02	LFA <sub>c</sub> 3.42 4.34 3.66 3.18 4.39 4.175 3.3 3.525 3.595 4.04 4.4 4.145 3.47 4.12 3.595 4.04 4.415 3.47 4.125 3.555 3.555 3.555 3.985 2.47 3.985 3.395 3.395 3.355 3.355 3.566 3.805 3.355 3.56 3.805 3.421 3.95 3.955 3.565 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.805 3.355 3.566 3.805 3.556 3.355 3.566 3.5666 3.566 3.566 3.5666 3.5666 3.5666
UFA2m UFA2m 2.666 2.33 2.365 2.07 2.81 2.84 2.285 2.265 2.745 2.275 2.2745 2.275 2.185 2.285 2.185 2.185 2.285 2.185 2.285 2.185 2.285 2.285 2.185 2.285 2.185 2.285 2.285 2.185 2.285 2.285 2.185 2.285 2.185 2.275 2.277 2.295 2.217 2.217 2.217 2.217 2.217 2.217 2.217 2.217 2.215 2.217 2.217 2.215 2.215 2.2	UFA <sub>1m</sub> 2.34 2.22 2.24 2.99 3.4 2.55 1.5 2.34 2.34 2.34 2.34 2.34 2.34 2.34 2.34	UFA 55 15 15 15 15 15 15 15 15 15 15 15 15	2.277 2.77 2.77 2.68 2.48 3.065 3.315 2.275 2.405 3.315 2.275 2.825 3.04 3.665 3.08 2.81 2.975 3.165 2.915 2.25 2.935 2.04 2.165 3.215 3.215 3.225 2.38 2.236 2.38 2.325 2.38 2.325 3.215 3.225 2.38 2.325 3.225 2.38 2.325 2.38 2.325 2.38 2.325 2.38 2.325 2.38 2.325 2.38 2.325 2.38 2.25 3.215 2.38 2.25 3.215 2.25 2.38 2.25 3.215 2.25 2.36 2.25 2.36 2.25 2.36 2.25 2.36 2.25 2.36 2.25 2.25 2.25 2.25 2.25 2.25 2.25 2.2	A <sub>1pm</sub> 4 3 3.365 2.745 2.925 3.985 2.705 3.985 2.705 3.985 3.775 3.92 4.155 3.155 3.155 3.155 3.155 3.51 2.735 3.51 2.735 3.51 2.8 2.977 3.775 2.965 3.255 3.435 3.455 3.455 3.455 3.455 3.455 3.455 3.455 3.455 3.455 3.455 3.455 3.55 3.	JFA, 4.275 4.425 3.795 3.815 4.365 3.811 3.85 4.365 5.04 4.525 4.615 4.615 4.615 4.615 4.615 4.615 4.625 5.05 5.055 4.45 4.275 4.025 5.02 4.635 3.755 3.755 3.775 4.777 4.775 4.715 4.715 4.515	UFAL 3.48 3.785 3.005 3.005 3.005 3.409 3.195 3.405 3.403 3.93 4.26 3.93 4.26 3.93 3.93 4.26 3.93 3.93 3.925 3.56 4.543 3.795 3.14 2.885 3.14 4.825 3.44 3.333 4.025 4.15 4.28 3.51 3.51	UFAc 4.73 4.29 4.39 3.99 4.305 5.105 4.475 4.475 4.475 4.475 4.475 4.475 4.475 4.475 4.475 4.535 4.535 4.466 4.426 4.24 4.535 5.27 4.33 4.355 5.27 4.39 4.365 5.27 4.39 4.365 5.27 4.39 4.365 5.27 4.39 4.365 5.27 4.39 3.92 4.365 5.27 4.39 3.99 4.685 4.97 4.97 4.99 4	LFA2m 2.483 2.055 1.895 2.065 2.07 2.13 2.033 2.65 2.15 2.25 2.25 2.25 2.45 2.25 2.55	LFA1m           5         2.8           5         2.8           5         2.254           5         2.54           6         2.59           7         2.66           5         2.711           5         2.67           6         2.711           5         2.67           7         3.04           2         3.22           5         2.675           5         2.675           5         2.633           5         2.725           5         2.775           5         2.703           4         2.66	LFA <sub>2pm</sub> 2 2. 7 2.9 5 2.9 4 2.8 5 2. 5 2. 5 3. 5 3. 8 4 2. 2 3. 5 2. 5 2. 5 2. 5 3. 8 5 3. 8 4 2. 2 3. 5 2. 5 3. 8 5 3. 8 7 5 7 5 7 5 7 7 7 7 7 7 7 7 7 7 7 7 7	LFA1 79 45 66 59 99 87 91 16 35 15 75 75 75 45 88 95 95 75 86 55 95 97 12 88 83 5 15 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	LFJ           3.335           3.475           3.477           3.07           3.415           3.97           3.01           3.97           3.07           3.415           3.97           3.01           3.89           3.665           3.423           3.665           4.25           2.95           3.665           4.066           4.106           3.515	4.065 4.255 4.37 3.365 4.145 4.475 4.085 3.57 3.71 4.81 4.38 4.73 4.73 4.73 3.765 5.175 3.765 5.175 3.765 5.175 3.925 4.18 3.82 3.325 4.265 4.265 4.265 4.58 4.58 4.58 4.765 4.401	FA,         3.825           3.825         4.33           3.8         2.97           4.355         3.815           3.355         3.355           3.353         3.475           3.98         4.005           4.135         3.533           4.045         3.345           3.345         3.245           3.155         3.155           3.155         3.155           3.155         3.155           3.155         3.155           3.105         4.12           3.666         3.295           3.405         3.405           3.246         3.91           4.02         4.02           4.02         3.205	LFA <sub>c</sub> 3.42 4.34 3.66 3.18 4.175 3.3 3.525 3.595 4.04 4.4 4.145 3.59 4.04 4.12 3.59 4.325 3.595 4.32 3.985 2.475 3.985 3.355 3.55 3.
UFA2m UFA2m 2.666 2.33 2.365 2.07 2.81 2.285 2.265 2.2745 2.285 2.2745 2.285 2.2745 2.285 2.2745 2.285 2.2745 2.215 2.215 2.2185 2.215 2.2055 2.245 2.2055 2.245 2.2055 2.2055 2.215 2.2055 2.217 2.215 2.217 2.21	UFA <sub>100</sub> 2.34 2.34 2.22 2.34 2.99 3.6 2.55 1.15 2.34 3.6 2.34 2.34 2.34 2.34 2.34 2.34 2.34 2.34	UFA 55 15 15 15 15 15 15 15 15 15 15 15 15	2.277 2.77 2.77 2.68 2.48 3.065 3.315 2.275 2.405 3.04 3.665 3.04 3.665 3.04 3.665 3.04 2.825 3.04 3.665 3.08 2.81 2.975 3.165 2.25 2.935 2.04 2.165 2.25 2.935 2.24 2.05 2.25 2.235 2.24 2.62 2.75 2.25 2.25 2.25 2.25 2.25 2.25 2.2	A <sub>1pm</sub> ( 3 3.365 2.745 2.925 3.985 2.705 3.985 3.775 3.92 4.155 3.155 3.155 3.155 3.155 3.155 3.55 3.55 3.6 3.815 2.735 3.51 2.8 2.977 3.775 3.927 3.51 2.8 2.977 3.75 3.51 2.965 3.255 3.435 3.455 3.595 3.455 3.595 3.	JFA, 4.275 4.425 3.795 3.815 4.355 4.365 3.81 3.85 5.04 4.525 4.615 4.71 4.425 5.07 3.905 5.055 4.45 5.055 4.45 5.055 4.275 4.025 5.055 3.775 4.275 4.025 5.055 3.777 4.715 4.515 4.135 4.135	UFAL 3.48 3.785 3.205 3.005 3.005 3.005 3.409 3.195 3.409 3.933 4.26 3.955 3.66 3.955 3.66 4.545 3.39 3.925 3.56 4.545 3.39 3.795 3.14 2.885 4.11 4.825 3.44 3.33 4.025 4.15 4.28	UFAc 4.73 4.29 4.39 3.99 4.305 5.105 4.475 4.475 4.475 4.475 4.475 4.475 4.535 4.56 4.466 4.24 5.11 4.535 4.29 4.535 5.27 4.36 3.775 4.39 4.365 5.27 4.36 3.775 4.39 4.685 4.97 4.685 4.97 4.685 4.97 4.685 4.97 4.685 4.97 4.685 4.97 4.685 4.97 4.685 4.97 4.98 4.685 4.97 4.98 4.99 4.98 4.99 4.98 4.98 4.98 4.98 4.98 4.98 4.98 4.98 4.98 4.98 4.98 4.98 4.99 4.685 4.99 4.685 4.99	LFA2m 2.485 2.055 1.899 2.085 2.77 2.49 1.577 2.13 2.233 2.65 2.15 2.15 2.15 2.15 2.233 2.65 2.15 2.405 1.945 2.25 2.405 1.945 2.15 2.64 2.15 2.55 2.15 2.5 2.25 2.55 2	LFA1m           5         2.8           5         2.22           5         2.54           5         2.62           2         2.76           3         3.44           5         2.61           5         2.61           5         2.61           5         2.61           3         3.05           7         3.04           2         3.22           5         2.67           5         2.63           3         2.63           5         2.77           5         2.77           5         2.70           3         2.93           4         2.64           4         2.65           5         2.775           5         2.70           3         2.93           4         2.66           4         2.66           5         3.23	LFA <sub>2pm</sub> 2 2. 7 2.9 5 2.9 4 2.8 5 2. 5 2. 5 3. 5 3. 5 3. 6 3. 5 3. 6 3. 5 3. 6 3. 5 3. 6 3. 5 3. 6 3. 5 3. 6 3. 6 3. 7 2. 5 3. 6 3. 6 3. 7 2. 5 3. 6 3. 6 3. 7 2. 5 3. 8 3. 6 3. 7 2. 5 3. 8 3. 6 3. 7 2. 5 3. 8 3. 7 2. 5 3. 8 3. 6 3. 7 2. 5 3. 8 3. 7 2. 5 3. 8 3. 7 2. 5 3. 8 3. 7 2. 5 3. 8 3. 6 2. 7 2. 5 3. 8 3. 8 4 2. 2 3. 7 5 2. 8 3. 8 5 2. 7 2. 5 3. 8 3. 8 5 2. 7 2. 5 3. 8 3. 8 5 3. 8 5 3. 8 5 3. 8 5 3. 8 5 3. 8 5 2. 9 3. 8 5 5 3. 8 5 5 5 5 5 5 5 3. 8 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	LFA1 79 45 665 99 87 91 16 35 15 75 45 88 95 75 45 88 65 95 97 75 65 97 75 88 65 99 75 12 88 83 5 97 12 25 22 92	LFJ           3.335           3.475           3.475           3.07           3.07           3.07           3.07           3.07           3.07           3.07           3.07           3.07           3.07           3.07           3.07           3.085           4.355           3.64           4.23           3.685           3.02           3.725           4.25           3.02           3.725           4.25           3.02           3.725           4.25           3.665           4.06           4.16           3.54           4.05	4.065 4.255 4.37 3.365 4.145 4.475 4.085 3.57 3.71 4.81 4.38 4.77 3.765 5.175 3.925 4.18 3.325 4.18 3.325 4.18 3.325 4.18 3.325 4.265 3.387 4.265 3.387 4.58 4.58 4.765 4.84 4.001 5.09	FA,         3.825           3.825         4.333           3.8         2.97           4.355         3.815           3.355         3.355           3.355         3.475           3.475         3.98           4.005         4.135           3.345         3.235           3.235         4.32           3.555         3.115           4.025         4.11           3.666         3.295           3.402         4.12           3.405         3.415           4.025         4.12           3.666         3.91           4.02         4.415           3.205         3.425	LFA <sub>c</sub> 3.42 4.34 3.66 3.18 4.175 3.3 3.525 3.595 4.04 4.145 3.595 4.04 4.145 3.595 4.04 4.125 3.595 4.325 3.985 2.477 3.985 3.985 3.356 3.355 3.356 3.355 3.356 3.355 3.3
UFA2m UFA2m 2.66 2.33 2.365 2.07 2.81 2.285 2.265 2.275 2.285 2.275 2.255 2.135 2.135 2.135 2.485 2.485 2.485 2.485 2.485 2.495 2.485 2.499 1.575 2.175 2.175 2.265 2.499 1.575 2.175 2.272 2.499 1.575 2.177 2.235 2.065 2.491 2.235 2.065 2.491 2.235 2.245 2.235 2.245 2.235 2.245 2.255 2.245 2.245 2.255 2.24	UFA <sub>100</sub> 2.34 2.34 2.52 2.24 2.99 3.4 2.55 2.34 3.6 2.34 3.6 2.33 2.33 2.33 2.33 2.33 2.33 2.33	UFA 55 15 15 15 15 15 15 15 15 15 15 15 15	2.277 2.77 2.77 2.68 2.48 3.065 3.315 2.275 2.405 3.04 3.665 3.04 3.665 3.08 2.82 3.04 3.665 3.08 2.81 2.975 3.165 2.915 2.29 2.935 2.04 2.165 3.205 2.36 2.675 2.38 2.905 3.42 3.205 2.77 2.38 3.205 2.36 2.905 3.42 2.905 3.42 2.905 3.42 2.905 3.42 2.905 3.42 2.905 3.42 2.905 3.42 2.905 3.42 3.205 2.77 2.78 3.205 2.77 2.78 3.205 2.905 3.205 2.905 3.205 2.905 3.205 2.905 3.205 2.905 3.205 2.905 3.205 2.905 3.205 2.905 3.205 2.905 3.205 2.905 3.205 2.905 3.205 2.905 3.205 2.905 3.205 2.905 3.205 2.905 3.205 2.905 3.205 2.905 3.205 2.905	A <sub>1pm</sub> ( 3 3.365 2.745 2.925 3.755 3.985 2.705 3.925 3.775 3.922 4.155 3.775 3.155 3.155 3.155 3.155 3.155 3.51 2.763 3.51 2.88 2.979 3.775 2.965 3.255 3.435 3.295 3.435 3.39 4.185 2.805 3.09 3.73 3.8	JFA, 4.275 4.425 3.795 3.815 4.355 4.365 3.81 3.82 4.365 4.355 4.455 4.615 4.71 4.485 5.07 3.905 5.055 4.45 4.505 4.45 4.705 4.275 4.275 4.275 3.777 4.715 4.375 3.777 4.715 4.91 4.515 4.315 4.315	UFAL 3.48 3.785 3.205 3.005 3.77 4.09 3.195 3.405 3.405 3.935 3.66 3.939 3.925 3.66 4.545 3.61 3.795 3.14 2.885 4.11 4.825 3.44 3.33 4.025 4.12 4.25 3.44 3.33	UFAc 4.73 4.29 4.39 3.99 4.305 5.105 4.475 4.14 4.03 4.83 4.835 4.535 4.466 4.466 4.24 5.11 4.033 4.29 4.535 4.335 5.277 4.36 3.775 4.39 4.355 5.277 4.36 3.775 4.39 4.355 5.27 4.36 3.775 4.39 4.355 5.27 4.36 3.775 4.39 4.355 4.375 4.39 4.355 4.375 4.39 4.355 4.375 4.39 4.355 5.277 4.36 3.775 4.39 4.395 4.397 4.699 3.992 4.265 4.265 4.275 4.395 4.295 4.395 4.397 4.699 3.992 4.265 4.265 4.275 4.265 4.275 4.265 4.397 4.699 3.992 4.265 4.265 4.265 4.265 4.275 4.265 4.275 4.265 4.275 4.265 4.275 4.265 4.275 4.265 4.275 4.265 4.275 4.265 4.275 4.265 4.275 4.265 4.275 4.265 4.275 4.265 4.275 4.265 4.275 4.265 4.275 4.265 4.275 4.265 4.275 4.265 4.275	LFA2m 2.483 2.055 1.899 2.083 2.77 2.43 1.577 2.13 2.23 2.033 2.65 2.13 3.07 2.652 2.403 1.945 2.765 1.945 2.765 1.945 2.755 1.999 2.235 2.455 1.999 2.235 2.995 2.99 2.455 1.995 2.9	LFA1m           5         2.8           5         2.25           5         2.61           6         2.67           7         2.66           7         2.67           7         2.67           7         2.61           3         3.05           7         3.04           2         3.25           2         2.63           3         3.05           2         3.62           2         2.63           3         2.05           5         2.67           5         2.76           5         2.75           5         2.75           5         2.75           5         2.70           8         2.60           6         2.73           5         2.70           5         2.70           6         2.73           7         2.03           4         2.60           4         2.61           4         2.62           5         3.23           5         3.23	LFA2pm 2 2. 7 2.9 5 2.9 4 2.8 5 2.9 5 2.5 3.5 5 2. 1 2. 5 3. 9 3. 5 3.6 7 2. 5 3.3 5 3.6 7 2. 5 3.3 5 3.6 7 2. 5 3.3 5 3.8 4 2. 5 3.3 5 3.8 4 2. 5 3.8 4 2. 5 3.8 5 3.8 1 3 3.5 5 3.8 1 3.8 5 3.8 1 3.8	LFA1 79 45 665 99 77 75 45 45 45 45 45 45 45 45 45 95 75 45 95 95 95 97 12 88 95 97 12 25 29 55	LFJ           3.335           3.475           3.477           3.08           3.64           4.23           3.645           3.23           3.645           3.23           3.645           3.23           3.645           3.23           3.645           3.23           3.645           3.23           3.642           4.25           3.643           4.25           3.644           4.25           3.655           3.645           3	4.065 4.255 4.37 3.365 4.425 4.437 4.75 4.085 3.57 3.71 4.81 4.38 4.77 4.73 3.765 5.175 3.925 5.175 3.925 4.18 3.825 4.265 4.265 3.38 3.87 4.58 4.765 4.84 4.701 5.09 9 4.245	FAL           3.825           3.83           4.335           3.81           3.855           3.815           3.355           3.355           3.355           3.355           3.355           3.475           3.53           4.005           4.135           3.555           3.155           4.015           3.235           4.025           4.11           3.666           3.295           3.401           4.021           4.415           3.205           3.215	LFA <sub>c</sub> 3.42 3.42 4.34 3.66 3.18 4.175 3.3 3.525 3.595 4.04 4.44 4.45 3.595 4.04 4.44 4.45 3.595 4.04 4.45 3.595 4.325 3.366 3.685 3.355 3.366 3.805 3.355 3.366 3.805 3.355 3.805 3.
UFA2m UFA2m 2.666 2.33 2.365 2.07 2.81 2.285 2.265 2.2745 2.285 2.2745 2.325 3.185 2.2745 2.325 2.133 3.095 2.485 2.055 2.145 2.055 2.085 2.085 2.085 2.085 2.085 2.085 2.095 2.035 2.035 2.61 2.19 3.031 2.37 2.32 2.302 2.302 2.302 2.302 2.302 2.302 2.302 2.302 2.302 2.302 2.302 2.302 2.302 2.302 2.302 2.305 2.30	UFA <sub>100</sub> 2.34 2.34 2.54 2.59 3.4 2.55 1.5 2.34 3.4 2.34 3.4 2.34 2.34 2.34 2.34 2	UFA 55 15 15 15 15 15 15 15 15 15 15 15 15	2.277 2.77 2.77 2.68 2.48 2.48 3.065 3.315 2.275 2.405 2.825 3.04 3.665 3.08 2.821 3.04 3.665 3.08 2.821 3.04 3.665 3.08 2.975 3.165 2.975 3.165 2.935 2.935 2.935 2.04 2.165 3.215 3.205 2.36 2.675 2.38 2.905 2.36 2.905 2.74 2.905	A <sub>1pm</sub> ( 3 3.365 2.745 2.925 3.755 3.985 2.705 3.925 3.755 3.922 4.155 3.755 3.755 3.755 3.755 3.755 3.755 3.755 3.755 3.66 3.815 2.735 3.55 3.61 3.815 2.735 3.55 3.55 3.55 3.255 3.255 3.255 3.4355 3.295 3.295 3.295 3.733 4.185 2.805 3.09 3.73 3.88 4.145	JFA, 4.275 4.425 3.795 3.815 4.365 3.813 3.815 4.365 4.365 4.365 4.504 4.525 4.615 4.705 5.055 4.425 5.005 4.275 4.275 4.275 3.775 3.375 3.377 4.715 3.375 3.377 4.715 4.911 4.515 4.135 4.135 4.135 4.345 5.5	UFAL 3.48 3.785 3.205 3.005 3.77 4.09 3.195 3.405 3.93 4.26 3.955 3.61 3.92 3.52 3.56 4.545 3.61 3.795 3.14 2.885 4.14 4.825 3.344 3.33 4.025 4.15 4.22 3.51 3.66 3.985 3.64 4.525	UFAc 4.73 4.29 4.30 3.99 4.305 5.105 4.475 4.41 4.03 4.83 4.835 4.535 4.56 4.46 4.46 4.24 5.11 4.535 4.535 4.46 3.775 4.33 4.29 4.535 4.31 4.335 5.437 4.36 3.775 4.39 4.69 3.92 4.73 4.69 3.92 4.73 4.73 4.75 4.77 4.75 4.77 4.75 4.77 4.75 4.77 4	LFA2m 2.488 2.055 1.899 2.083 2.77 2.44 1.577 2.13 2.23 2.033 2.63 2.15 2.15 2.40 2.33 2.33 3.00 2.642 2.40 1.945 2.400 1.945 2.400 1.945 2.405 1.955 1.955 2.955 1.955 2.955	LFA1m           5         2.8           5         2.25           5         2.64           6         2.59           7         2.66           5         2.76           6         2.77           5         2.71           5         2.73           6         2.79           7         2.66           3         3.05           7         3.04           2         3.00           5         2.77           5         2.763           5         2.75           5         2.75           5         2.75           5         2.70           8         2.69           5         2.75           5         2.70           3         2.61           6         2.73           7         3.44           2.63         3.23           4         2.64           5         3.23           5         3.23           5         3.4	LFA2pm 2 2. 7 2.9 5 2.9 4 2.8 5 2.9 5 2.5 3.3 5 2. 1 2. 5 3. 9 3. 5 3.6 7 2. 5 3.3 5 3.6 7 2. 5 3.3 5 3.6 7 2. 5 3.3 5 3.8 4 2. 7 2. 5 3.3 5 3.8 5 3.8	LFA1 79 45 66 99 90 37 91 16 35 45 45 45 89 15 45 45 89 15 45 65 95 95 95 97 12 88 95 97 12 83 5 55 22 25 25	LFJ           3.335           3.475           3.475           3.07           3.07           3.01           3.875           4.355           3.741           3.897           3.685           3.685           3.685           3.685           3.625	4.065 4.255 4.37 3.365 4.425 4.445 4.475 4.085 3.57 3.71 4.81 4.38 4.75 3.765 5.175 3.925 4.18 3.325 4.265 4.265 4.38 3.38 3.325 4.265 3.38 3.387 4.565 4.38 3.387 4.565 4.245 5.235	FAL           3.825           4.33           3.8           2.97           4.355           3.815           3.355           3.355           3.355           3.355           3.355           3.475           3.475           3.345           3.333           3.345           3.235           4.123           3.533           4.045           3.3345           3.255           3.115           4.005           4.11           3.66           3.295           3.46           3.295           3.46           3.205           4.415           3.205           4.205           3.315	LFA <sub>c</sub> 3.42 4.34 3.66 3.18 4.39 4.175 3.3 3.525 4.04 4.44 4.145 3.59 4.325 3.55 4.325 3.56 3.665 3.355 3.366 3.805 3.355 3.56 3.805 3.55 3.56 3.805 3.55 3.56 3.805 3.56 3.805 3.56 3.805 3.55 3.56 3.805 3.56 3.805 3.55 3.56 3.805 3.55 3.56 3.805 3.55 3.55 3.56 3.805 3.56 3.805 3.95 3.56 3.805 3.56 3.805 3.56 3.805 3.56 3.55 3.56 3.56 3.55 3.56 3.355 3.36 3.355 3.36 3.36 3.355 3.36 3.36 3.36 3.36 3.36 3.365 3.36 3.365
UFA2m UFA2m 2.666 2.33 2.365 2.07 2.81 2.84 2.285 2.265 2.2745 2.285 2.2745 2.285 2.2745 2.285 2.2745 2.285 2.2745 2.285 2.2745 2.285 2.275 2.185 2.285 2.392 2.375	UFA <sub>100</sub> 2.34 2.34 2.54 2.59 3.6 2.55 2.34 3.6 2.34 3.6 2.34 2.34 3.6 2.34 2.34 3.6 2.34 2.34 2.34 2.34 2.34 2.34 2.34 2.34	UFA 55 15 15 15 15 15 15 15 15 15 15 15 15	2.277 2.77 2.77 2.68 2.48 3.065 3.065 3.04 3.665 3.04 3.665 3.08 2.815 2.275 3.165 2.915 2.915 2.915 2.915 2.944 2.165 3.205 2.38 2.04 2.165 3.205 2.38 2.305 2.38 2.305 2.38 2.305 2.38 2.305 2.38 2.305 2.38 2.305 2.38 2.305 2.38 2.305 2.38 2.305 2.38 2.305 2.38 2.305 2.39 2.305 2.3	A <sub>1pm</sub> ( 3 3.365 2.745 2.925 3.755 3.985 2.705 3.205 3.205 3.205 3.922 4.155 3.195 3.195 3.195 3.195 3.195 3.195 3.55 3.6 3.815 2.735 3.6 3.815 2.735 3.6 3.815 2.735 3.6 3.815 2.735 3.55 3.255 3.255 3.435 3.295 3.435 3.295 3.435 3.99 3.775 2.965 3.255 3.435 3.99 3.775 2.965 3.255 3.435 3.99 3.775 2.965 3.255 3.435 3.99 3.755 3.435 3.99 3.755 3.435 3.99 3.755 3.435 3.99 3.755 3.435 3.99 3.755 3.435 3.99 3.755 3.435 3.99 3.755 3.435 3.99 3.755 3.435 3.99 3.755 3.435 3.99 3.755 3.435 3.99 3.755 3.435 3.99 3.755 3.435 3.99 3.755 3.435 3.99 3.755 3.435 3.99 3.755 3.435 3.435 3.435 3.435 3.435 3.435 3.435 3.435 3.455 3.4355 3.4355 3.4355 3.4355 3.4355	JFA, 4.275 4.425 3.795 3.815 4.365 3.815 4.365 3.81 3.85 4.455 4.615 4.71 4.485 5.07 3.905 5.055 4.47 4.705 4.275 4.025 5.02 4.635 3.775 4.715 4.215 4.911 4.515 4.135 4	UFAL 3.48 3.785 3.205 3.005 3.195 3.405 3.93 4.26 3.933 4.26 3.955 3.66 3.393 3.925 3.62 3.56 4.545 3.61 3.795 3.14 2.885 4.11 4.825 3.144 3.333 4.025 4.15 4.28 3.511 3.66 3.985 3.64 4.525 3.747813	UFAc 4.73 4.29 4.39 4.305 5.105 4.475 4.11 4.03 4.835 4.475 4.13 4.03 4.835 4.565 4.466 4.466 4.464 4.24 5.11 4.535 5.27 4.39 4.335 5.27 4.39 4.685 4.31 4.335 5.27 4.39 4.685 4.475 4.39 4.685 4.475 4.39 4.685 4.475 4.39 4.685 4.475 4.39 4.685 4.475 4.39 4.685 4.475 4.39 4.685 4.475 4.39 4.685 4.475 4.39 4.685 4.475 4.39 4.685 4.475 4.39 4.685 4.475 4.39 4.685 4.475 4.39 4.685 4.475 4.39 4.685 4.39 4.685 4.475 4.39 4.685 4.475 4.39 4.685 4.475 4.39 4.685 4.475 4.39 4.685 4.475 4.39 4.685 4.475 4.39 4.685 4.475 4.39 4.685 4.475 4.39 4.685 4.475 4.39 4.685 4.475 4.39 4.685 4.475 4.475 4.39 4.685 4.475 4.39 4.685 4.475 4.39 4.685 4.426 4.475 4.39 4.685 4.475 4.39 4.685 4.475 4.39 4.685 4.426 4.475 4.39 4.685 4.475 4.39 4.685 4.475 4.29 4.59 4.29 4.59 5.27 5.27 5.	LFA2m 2.488 2.055 1.899 2.083 2.77 2.13 2.033 2.033 2.033 2.033 2.033 2.033 2.033 2.033 2.033 2.033 2.033 2.033 2.035 1.999 2.40 2.999 2.42 2.999 2.42 2.199 2.999 2.42 2.199 2.999 2.45 1.999 2.995 1.999	LFA1m           5         2.8           5         2.22           5         2.54           5         2.54           5         2.54           5         2.54           5         2.54           5         2.59           7         2.66           5         2.71           5         2.67           3         3.05           7         3.04           2         3.00           7         3.04           2         3.00           5         2.675           5         2.675           5         2.675           5         3.44           5         3.44           5         2.70           3         2.03           4         2.6           5         3.44           5         3.23           4         2.6           5         3.01           5         3.02           5         3.03           6         3.23           6         3.23           7         3.4           5<	LFA2pm 2 2. 7 2.9 5 2.9 4 2.8 5 2.9 4 2.8 5 2.9 4 2.8 5 2.9 3 .3. 5 3.8 7 2. 5 3.8 7 2. 5 3.8 7 2. 5 3.8 7 2. 5 3.8 5 3.8 4 2. 7 2. 5 3.8 5 3.8 5 2.5 5 2.5 5 2. 5 2.8 5 2.8 5 2.8 5 2.8 5 2.8 5 3.8 5 2.8 5 2.8 5 2.8 5 2.8 5 2.8 5 2.9 5 3.8 5 2.9 5 3.8 5 2.9 5 3.8 5 2.9 5 3.8 5 4.1 5 5 5.1 5 5 5.1	LFA1           79           45           45           45           45           45           29           87           91           15           75           45           65           97           65           97           65           97           88           95           97           12           83           3.5           15           55           29           94	LFJ           3.335           3.475           3.475           3.475           3.475           3.475           3.475           3.475           3.475           3.475           3.475           3.475           3.475           3.475           3.475           3.475           3.47           3.855           3.685           3.642           3.623           3.625           3.635           4.05           3.83	4.065 4.255 4.37 3.365 4.145 4.475 4.085 3.57 3.71 4.81 4.38 4.77 4.73 4.73 3.765 5.175 3.925 4.18 3.8 3.325 4.265 4.265 4.79 3.65 3.38 3.325 4.265 3.38 3.87 4.58 4.765 3.38 3.87 4.58 4.765 3.38 3.87 4.58 4.765 3.38 3.87 4.58 4.765 3.38 3.87 4.58 4.765 3.38 3.87 4.58 4.765 3.38 3.87 4.58 4.765 3.38 3.87 4.58 4.765 3.57 3.515 3.38 3.87 3.57 3.515 3.525 4.255 3.38 3.87 3.525 4.255 3.38 3.87 3.57 3.515 3.38 3.87 3.57 3.515 3.38 3.87 3.57 3.515 3.525 4.255 3.38 3.87 3.57 3.515 3.38 3.87 3.525 4.255 3.38 3.87 3.55 3.55 3.38 3.87 4.58 4.755 3.58 4.755 3.595 3.575 3.755 3.575 3.755 3.38 3.87 4.755 3.575 3.255 3.255 3.38 3.87 4.755 3.2557 3.2	FA           3.825           4.33           3.8           2.97           4.355           3.815           3.355           3.355           3.345           3.475           3.405           4.045           4.033           3.405           3.331           3.405           3.333           3.345           3.235           3.135           4.005           4.11           3.66           3.295           3.46           3.91           4.025           4.405           4.205           3.215           4.205           3.215           4.205           3.315           4.165           3.737813	LFA <sub>c</sub> 3.42 4.34 3.66 3.18 4.39 4.175 3.3 3.525 3.595 4.04 4.4 4.145 3.595 4.04 4.414 4.145 3.595 4.04 4.325 3.595 4.325 3.595 3.585 3.585 3.395 3.366 3.805 4.345 3.935 3.56 3.365 3.366 3.778281

12         12<	UA	UA	UA		JA.	UA.	U	۵.	UA.	14		I A	LA.		A	LA.	IA.	1	A
b         b<         b<<         b<< <td>2 44</td> <td>1 98</td> <td>C 2pm</td> <td>2 65</td> <td>2 86</td> <td></td> <td>1 25</td> <td>2 55</td> <td>2</td> <td>85</td> <td>2 47</td> <td>2 1m</td> <td>63</td> <td>2 9 3</td> <td>2 5</td> <td>5 3</td> <td>3 24</td> <td>24</td> <td>2 45</td>	2 44	1 98	C 2pm	2 65	2 86		1 25	2 55	2	85	2 47	2 1m	63	2 9 3	2 5	5 3	3 24	24	2 45
1         2         2         3         3         3         5         2         3	2.6	2.47		2.74	3.53	. 4	1.06	3.39	3	3.39	2.47	2.	21	3.31	3.3	5 4	4.17	3.05	2.88
B         B	2.29	2.21		2.83	3.16		3.68	2.93	з	8.08	1.77	2.	46	2.7	2.7	3 3	3.59	2.49	2.5
3.3.3         3.7.7         5.7.7         5.0.8         3.7.7         3.0.8         3.7.7         3.0.8         3.7.7         3.0.7 <th< td=""><td>2.39</td><td>2.13</td><td></td><td>2.66</td><td>3.1</td><td></td><td>3.72</td><td>3.06</td><td>з</td><td>3.04</td><td>1.79</td><td>2.</td><td>55</td><td>2.64</td><td>2.9</td><td>5 3</td><td>3.32</td><td>2.69</td><td>2.9</td></th<>	2.39	2.13		2.66	3.1		3.72	3.06	з	3.04	1.79	2.	55	2.64	2.9	5 3	3.32	2.69	2.9
13.3         2.95         3.08         3.54         4.11         3.27         4.24         3.25         4.41         3.47         4.24         3.2         2.44         3.25         2.44         3.24         2.25         2.24         3.35         3.24         1.21         2.24         1.25         2.44         3.45         2.45         3.45         4.25         3.35         4.47         3.40         2.47         2.55         2.55         3.57         4.25         3.35         4.40         3.40	3.39	3.78		3.1	3.77	· 4	1.08	3.5	3	3.47	3.06	2.	53	2.81	3.2	7 3	3.89	3.03	3.1
2         2         2         2         3	3.13	2.95		3.08	3.54	. 4	4.11	3.27	з	.23	2.96	3.	34	3.13	3.5	2 4	4.41	3.17	3.1
1         2         1         3	2.02	2.02		3.19	3.3		3.87	3.13	з	3.24	1.81	2.	51	2.61	3.1	6	3.8	2.94	2.
1         2         2         1         3         3         4         3         4         3         6         3         2         2         2         3         3         4         3         6         3	2.92	1.83		2.46	3.2		3.48	2.97	2	2.84	1.95	2.	51	2.37	2.4	9 3	3.47	2.67	2.5
12.29         2.54         3.53         4.37         4.48         3.66         3.95         2.65         2.60         3.74         4.64         3.61         3.51           2.57         2.52         3.57         4.43         3.51         3.52         2.50         3.74         4.64         3.81         3.22         2.50         3.64         4.63         3.34         4.32         3.51         3.34         4.32         3.50         3.34         4.43         3.34         4.32         3.50         3.34         4.33         3.22         2.50         3.64         4.33         3.32         2.50         3.34         4.32         3.22         2.55         2.66         3.34         5.32         3.34         5.32         3.35         4.41         3.32         2.57         2.37         2.37         2.35         2.44         3.34         2.32         3.35         3.41         3.22         2.57         2.33         2.37         2.32         3.35         4.41         3.40         3.32         2.57         2.33         2.57         3.41         3.41         3.22         2.57         3.13         3.41         3.22         2.57         3.41         3.41         3.41         3.22         2	2.34	2.51		3.43	3.75	4	4.31	3.06	2	2.84	2.49	2.	66	2.92	3.3	3 3	3.65	2.72	2.8
b         b	2.29	2.54		3.53	4.37	4	1.84	3.86	3	8.95	2.85	1	2.6	3.24	3.8	6 4	4.72	3.52	3.5
L         L <thl< th="">         L         L         L</thl<>	3.57	2.92		3.67	4.43		4.5	3.88		4	3.43	2.	96	3.76	4.0	8 4	4.35	3.61	3.
1         1	2.69	2.84		2.85	3.35		1.17	3.13	2	2.97	2.47	2.	51	2.15	3.3	1 4	1.23	2.8	2.8
1.9.0         1.9.0         2.0.0 <th< td=""><td>2.45</td><td>2.30</td><td></td><td>3.84</td><td>3.75</td><td></td><td>1.42</td><td>3.3</td><td>3</td><td>0.29</td><td>2.52</td><td>2.</td><td>99</td><td>2.84</td><td>3.4</td><td></td><td>1.09</td><td>3.39</td><td>3.2</td></th<>	2.45	2.30		3.84	3.75		1.42	3.3	3	0.29	2.52	2.	99	2.84	3.4		1.09	3.39	3.2
10.7         13.6         29.3         13.8         4.96         15.9         14.4         23.3         20.60         13.7         13.6         13.2         13.2         13.2         13.2         13.2         13.2         13.2         13.2         13.2         13.2         13.2         13.7         23.2         12.55         2.53         2.57         2.63         3.14         3.25         13.2         13.7         2.37         2.27         2.55         2.68         3.31         2.55         2.53         2.7         3.42         2.55         2.53         3.1         2.55         2.52         3.1	1.97	1 09		2.00	2 10		+.20 A	2.75	2	0.00	2.03	2.	90	3.00	2.2	4 ·	+.30	2.01	2.0
12.99         12.47         2.57         2.75         2.76         2.37         2.52         2.55         2.63         3.48         2.29         2.29           1.96         2.13         3.16         3.72         2.99         3.2         2.17         2.53         2.56         3.18         2.55         3.13         2.55         2.55         2.55         2.53         2.57         3.22         2.57         2.54         2.58         2.55         2.53           2.10         2.47         3.18         2.25         3.30         2.27         2.55         2.58         3.13         2.55         2.55         2.53           2.90         2.47         3.18         3.66         4.40         3.34         3.47         3.24         2.25         2.29         3.16         2.47         3.38         2.47         2.48         3.06         2.55         2.53         3.33         2.27         2.44         3.04         2.55         2.53         3.33         2.27         2.48         3.34         2.27         2.48         3.34         2.27         2.48         3.34         2.27         2.48         3.34         2.27         2.48         3.34         2.27         2.48         3.44 <td>3.7</td> <td>3.16</td> <td></td> <td>2 93</td> <td>3.5</td> <td></td> <td>1 96</td> <td>3.59</td> <td>3</td> <td>44</td> <td>3.53</td> <td>3</td> <td>08</td> <td>3.87</td> <td>3.9</td> <td>4</td> <td>5.12</td> <td>3.22</td> <td>3.2</td>	3.7	3.16		2 93	3.5		1 96	3.59	3	44	3.53	3	08	3.87	3.9	4	5.12	3.22	3.2
2.16         2.14         2.97         3.62         4.33         2.46         3.21         2.35         4.1         3.42         2.28         2.25         2.35         2.35         4.1         3.42         2.28         2.25         2.37         2.35         2.47         2.36         3.22         2.37         2.46         3.38         2.45         3.48         3.46         3.45         3.48         3.45         3.48         3.45         3.48         3.45         3.48         3.46         2.35         3.41         4.47         3.46         2.35         2.37         3.48         3.48         3.48         3.48         3.48         3.48         3.48         3.48         3.48         3.48         3.48         3.44         3.43         3.41         2.47         3.48         3.48         3.44         3.41         2.47         3.48         3.44         3.43         3.44         3	2.69	2.47		2.65	2.95		1.37	2.75	2	2.73	2.37	2.	52	2.55	2.6	3	3.48	2.32	2.7
1.19         2.13         2.13         3.14         2.72         2.97         2.57         2.67         3.42         2.79         3.52         2.57         3.11         2.55         3.51         2.55         3.51         3.55         5.5         5.5           3.18         2.26         3.18         3.22         3.70         4.53         3.48         3.49         3.05         2.55         3.42         3.61         3.65         3.52         5.25         3.24         3.64         2.64         3.64         3.64         2.26         3.64         3.64         3.64         2.26         3.64         3.64         3.64         2.26         3.64         3.64         3.64         3.64         3.64         3.64         3.64         3.64         3.64         3.64         3.64         3.64         3.64         3.64         3.64         3.64         3.64         3.64         3.64	2.36	2.14		2.97	3.62		1.33	3.46	3	3.32	2.5	2.	66	3.31	3.5	5	4.1	3	2.9
1         2         1         3         2         3         2         2         7         2         6         3         3         2         2         2         2         3	1.96	2.13		2.31	3.16		3.72	2.99		3.2	1.78	2.	37	2.53	2.	7 :	3.42	2.39	2.5
1         1         3         3         3         3         3         3         5         3         3         5         3         3         5         3         3         5         3         3         5         3         3         5         3         3         5         3         3         5         3         3         5         3         3         5         3         3         5         3         3         5         3         3         5         3	2.27	1.98		2.14	2.95		3.93	2.9		3.3	2.27	2.	57	2.6	2.8	9 :	3.31	2.55	2.5
2.67         3.18         3.63         4.06         3.3         3.18         2.99         2.59         3.50         4.74         3.16         3.17           1.68         2.45         3.01         3.19         3.37         2.88         7.28         7.25         7.22         3.11         3.13         3.16         3.27         3.48         3.38         3.7         3.44         3.38         3.54         4.7         3.38         3.54         4.7         3.38         3.56         3.27         3.28         3.38         3.54         4.7         3.38         3.56         3.27         3.38         3.56         3.27         3.38         3.56         3.27         3.38         3.56         3.27         3.38         3.56         3.27         3.38         3.36         3.38 <td>3.18</td> <td>2.81</td> <td></td> <td>3.22</td> <td>3.79</td> <td>. 4</td> <td>1.53</td> <td>3.48</td> <td>3</td> <td>3.49</td> <td>3.05</td> <td>2.</td> <td>56</td> <td>3.42</td> <td>3.6</td> <td>1 3</td> <td>3.85</td> <td>3.12</td> <td>3.2</td>	3.18	2.81		3.22	3.79	. 4	1.53	3.48	3	3.49	3.05	2.	56	3.42	3.6	1 3	3.85	3.12	3.2
1.68         2.48         3.0         3.83         3.47         3.28         2.28         2.29         2.29         3.29	2.91	2.67		3.18	3.63	4	1.08	3.3	з	3.18	2.95	2.	59	3.1	3.6	1 4	4.74	3.16	3.1
2.18         3.01         3.19         3.37         2.88         3.06         2.59         3.22         3.28         3.22         2.65         2.47           3.42         2.51         3.72         4.28         5.04         3.93         2.05         2.25         2.72         3.11         3.13         3.81         3.83         3.73         3.88         4.7         3.78         3.88         4.7         3.78         3.88         4.7         3.78         3.88         4.7         3.78         3.88         4.7         3.78         3.88         4.7         3.78         3.88         4.7         3.83         3.50         3.22         2.48         3.83         3.55         3.92         3.14         4.05         3.91         3.50         3.92         3.56         3.92         3.56         3.92         3.55         3.92         3.56         3.92         3.56         3.92         3.56         3.92         3.56         3.92         3.56         3.92         3.56         3.92         3.56         3.92         3.56         3.92         3.56         3.92         3.55         3.92         3.56         3.92         3.56         3.92         3.55         3.92         3.56         3.56	1.68	2.45		2.6	3.06	6 3	3.83	3.47	з	3.24	2.18	2.	66	2.58	2.9	3 3	3.68	2.95	2.9
3.42         2.41         3         3.43         4.39         3.15         2.91         2.72         3.14         3.1         3.16         2.67         2.88           3.35         2.71         3.44         4.19         4.6         4.02         4.07         3.94         2.67         2.73         3.88         4.77         3.56         3.6           2.64         3.04         3.06         3.44         4.03         3.44         4.02         2.94         2.66         2.93         2.66         3.1         4.32         2.74         2.66           2.16         2.445         3.04         3.44         4.02         2.94         2.96         2.95         2.12         2.43         3.55         4.72         3.35         3.32         3.35         3.25	2.69	2.18		3.01	3.19	) 3	3.37	2.88		2.8	3.06	2.	59	3.22	3.2	8 3	3.32	2.65	2.4
1.2.51         3.7.2         4.7.4         4.7.9         4.6.4         4.02         4.07         3.7.4         3.7.5         3.7.5         3.7.6         3.7.7         3.7.4         4.7.8         4.7.7         3.7.6	3.42	2.41		3	3.43	4	1.39	3.15	2	2.91	2.25	2.	72	3.11	3.	1 8	3.81	2.67	2.8
3.53         2.7.1         3.44         4.19         4.00         4.07         3.34         2.147         3.38         4.7.7         3.38         4.7.7         3.38         4.7.7         3.38         4.7.7         3.35         4.7.7         3.35         4.7.7         3.35         4.7.7         3.35         3.7.7         4.16         4.00         3.54         4.02         2.98         2.98         2.93         2.6         3.34         4.05         3.04         3.00           3.54         3.39         3.54         3.36         4.36         4.20         2.98         2.98         2.83         3.35         3.25         3.27         3.35         3.55         4.7.7         3.35         3.36         0.354         0.344         0.354         0.354         0.354         0.354         0.354         0.354         0.354         0.354         0.355         4.7.7         5.16         3.46         3.8         0.354         0.354         0.354         0.35         3.25         3.27         4.16         0.35         0.321         0.321         0.321         0.321         0.321         0.321         0.321         0.321         0.321         0.321         0.321         0.321         0.321         0.321 <td>2.83</td> <td>2.51</td> <td></td> <td>3.72</td> <td>4.28</td> <td></td> <td>0.04</td> <td>3.93</td> <td>4</td> <td>.08</td> <td>2.5</td> <td>2.</td> <td>06</td> <td>2.49</td> <td>3.2</td> <td>5 4</td> <td>4.49</td> <td>3.48</td> <td>3.3</td>	2.83	2.51		3.72	4.28		0.04	3.93	4	.08	2.5	2.	06	2.49	3.2	5 4	4.49	3.48	3.3
Losa         L/A         S.2.6         A.4.7         L/S         S.0.6         L/S         L/S         L/S         S.2.6         S.4.1         A.4.2         L/S         L/S         S.2.6         S.4.1         A.4.2         L/S         L/S         S.2.6         S.4.1         A.5.5         A.7.7         A.3.5         S.3.6         A.3.6         S.2.2         L/S         L/S <thl s<="" th=""> <thl s<="" th="">         L/S</thl></thl>	3.35	2.71		3.44	4.19		4.6	4.02	4	1.07	3.94	2.	87	3.73	3.8	8	4.7	3.56	3.6
2.16         2.46         3.06         3.46         4.12         2.96         2.96         2.92         2.13         2.12         2.43         3.05         3.77         3.07         3.01         3.07         3.07         3.01         3.00         3.01         3.00         3.01         3.00         3.01         3.00         3.00         3.00         3.00         3.00         3.00         4.10         3.00         4.00         3.00         4.00         3.00         4.00         3.00         4.00         3.00         4.00         3.00         4.00         3.00         4.00         4.00         3.00         4.00 <th< td=""><td>2.64</td><td>2.7</td><td></td><td>3.23</td><td>3.20</td><td></td><td>1.47</td><td>2.98</td><td>3</td><td>5.06</td><td>2.51</td><td>2.</td><td>59</td><td>2.86</td><td>3.</td><td>1 4</td><td>1.32</td><td>2.74</td><td>2.0</td></th<>	2.64	2.7		3.23	3.20		1.47	2.98	3	5.06	2.51	2.	59	2.86	3.	1 4	1.32	2.74	2.0
2.10         1.51         2.59         3.56         4.03         2.24         3.24         3.25         3.22         2.21         2.28         3.35         3.25         3.22         2.21         2.28         3.35         3.25         3.22         2.21         2.28         3.25         3.25         3.26         3.44         3.44         3.44         3.44         3.44         3.44         3.44         3.44         3.44         3.44         3.44         3.44         3.44         3.44         3.44         3.44         3.44         3.45         3.45         3.462         3.44         3.44         3.44         3.44         3.44         3.44         3.44         3.44         3.44         4.44         4.45 <t< td=""><td>2.10</td><td>2.48</td><td></td><td>3.08</td><td>3.48</td><td></td><td>1.12</td><td>3.40</td><td>2</td><td>.92</td><td>2.19</td><td>2.</td><td>12</td><td>3.02</td><td>3.4</td><td>1 4 5</td><td>4.05</td><td>3.04</td><td>3.0</td></t<>	2.10	2.48		3.08	3.48		1.12	3.40	2	.92	2.19	2.	12	3.02	3.4	1 4 5	4.05	3.04	3.0
3.5.4         3.33         3.5.4         3.5.4         3.5.9         4.5.7         4.16         4.5.7         5.16         7.4.6         4.5.7         5.16         7.4.6         4.5.7         5.16         7.4.6         4.5.7         5.16         7.4.6         4.5.7         5.16         7.4.6         4.5.7         5.16         7.4.6         4.5.7         5.16         7.4.6         4.5.7         5.16         7.4.6         4.5.7         5.16         7.4.6         7.4.7         7.4.16         4.5.7         5.16         7.4.6         7.4.7         7.4.16         4.5.7         5.16         7.4.6         7.4.7         7.4.16         4.5.7         7.5.16         7.4.7         7.5.16         7.4.7         7.5.7         7.4.16         4.5.7         7.5.16         7.4.7         7.5.16         7.4.7         7.5.7         7.5.16         7.4.7         7.5.16         7.5.7         7.5.16         7.5.7         7.5.16         7.5.7         7.5.16         7.5.7         7.5.16         7.5.7         7.5.16         7.5.7         7.5.16         7.5.7         7.5.16         7.5.7         7.5.16         7.5.7         7.5.16         7.5.7         7.5.16         7.5.7         7.5.16         7.5.7         7.5.16         7.5.7         7.5.16	2.30	1 91		2 59	3.56		1.03	2.50	2	99	2.5	2	88	3 33	3.5	5 6 *	3 92	2.91	2.8
1         1	3.54	3.39		3.54	3.98		1.92	3.61	-	3.6	3.99	3.	37	4.16	4.5	7 5	5.16	3.46	3.
0.33391         0.442227         0.413566         0.419883         0.41098         0.37306         0.595429         0.266183         0.467198         0.462552         0.55911         0.362278         0.32144           Patert Number         00m         00	2.652188	2.480313	3.010	0625	3.522188	4.202	813 3	.237188	3.228	438 2	2.597813	2.7071	88 2.	993125	3.32531	3 4.05	625 2.9	71875	2.98562
Pettert Number         UD <sub>m</sub>	0.533913	0.442227	0.41	1566	0.419883	0.410	069 0	.373019	0.379	466 0	.596429	0.2661	83 0.	467198	0.46255	2 0.549	115 0.3	363278	0.32144
Partin Control         Doga         Doga <thdoga< th="">         Doga         Doga</thdoga<>	Patient Number	- lup - u	0	UD.	LUD.		UD	LID.	10	ID	10	10		10	in T				
Introl 12         -0.25         -0.4         -0.15         0.35         0.9         1.46         1.20         0.055         0.05         0.07         1.13         1.13         1.13         1.07         0.75         0.25         0.15         0.17         0.15         0.035         0.015         0.14         0.103         0.015	172692	9 0.22	0.385	0.1	00 <sub>1pm</sub>	0.025	0.93	1.88	0.94	1.42	15 0.825	0.785	-0.14	4 0.19	0.015	PRODI	PRODZ	REIDI	REIDZ
Issesse         0.032         0.03         0.013 <t< td=""><td>167012</td><td>4 -0.27</td><td>-0.255</td><td>-0.0</td><td>-0.165</td><td>0.365</td><td>0.395</td><td>0.9</td><td>1.46</td><td>1.2</td><td>8 0.085</td><td>0.12</td><td>-0.36</td><td>5 0.06</td><td>-0.415</td><td>0.07</td><td>0.795</td><td>-1.26</td><td>-0.555</td></t<>	167012	4 -0.27	-0.255	-0.0	-0.165	0.365	0.395	0.9	1.46	1.2	8 0.085	0.12	-0.36	5 0.06	-0.415	0.07	0.795	-1.26	-0.555
1613488         -0.32         0.075         -0.18         -0.015         0.075         0.025         0.12         0.22         0.005         0.025 <t< td=""><td>168126</td><td>8 0.075</td><td>0.08</td><td>-0.1</td><td>L5 -0.415</td><td>0.115</td><td>0.275</td><td>1.31</td><td>1.11</td><td>1.3</td><td>0.78</td><td>0.745</td><td>0.24</td><td>5 0.085</td><td>0.125</td><td>1.47</td><td>1.185</td><td>-0.03</td><td>-0.195</td></t<>	168126	8 0.075	0.08	-0.1	L5 -0.415	0.115	0.275	1.31	1.11	1.3	0.78	0.745	0.24	5 0.085	0.125	1.47	1.185	-0.03	-0.195
Index264         -0.38         -0.87         -0.08         -0.27         0.22         0.28         1.12         0.28         0.48         0.13         0.23         0.49         1.17         1.02         0.755         0.68           1068268         0.48         0.45         0.25         0.48         0.45         0.25         0.41         0.025         0.47         0.175         1.53         0.46         0.055         0.47         0.175         0.48         0.125         0.44         0.055         0.05         0.075         0.66         0.05         0.025         0.41         0.05         0.025         0.48         0.41         0.025         0.41         0.05         0.025         0.41         0.025         0.425         0.415         0.015         0.46         0.435         0.415	163548	8 -0.32	0.075	-0.1	L8 -0.175	0.095	-0.055	0.95	0.22	0.2	.8 0.045	0.12	0.22	5 0.09	0.295	1.12	1.04	-0.03	0.12
1028850         0.25         0.03         0.23         0.03         0.23         0.043         0.03         0.043         0.03         0.043         0.03         0.043         0.03         0.043         0.03         0.043         0.03         0.043         0.03         0.043         0.03         0.043         0.03         0.043         0.03         0.043         0.024         0.03         0.024         0.03         0.024         0.03         0.024         0.03         0.024         0.03         0.025         0.03         0.045         0.03         0.043         0.044         0.041         0.04         0.045         0.025         0.03         0.027         0.015         0.046         0.04         0.044         0.03         0.025         0.03         0.025         0.015         0.046         0.015         0.045         0.025         0.015         0.015         0.015         0.015         0.015         0.015         0.015         0.015         0.015         0.015         0.015         0.016         0.011         0.015         0.015         0.015         0.015         0.015         0.015         0.015         0.015         0.015         0.015         0.015         0.015         0.015         0.015         0	168626	4 -0.58	-0.875	-0.03	35 -0.015	0.27	0.2	0.835	1.21	1.32	0.255	0.145	0.1	5 0.235	-0.34	1.175	1.02	0.755	0.68
1979222         -0.6         -0.13         -0.05         0.00         0.37         0.43         -1.1         0.51         0.54         -0.1         0.21         1.13         1.17         -0.56         -0.33           14         0.215         0.04         -0.05         0.13         0.075         0.735         0.66         0.525         0.24         0.055         -0.255         1.115         0.09         0.6625         -0.33           66         0.455         -0.15         0.45         0.135         0.47         0.88         0.5         0.44         0.01         0.025         0.13         0.46         0.4         0.11         0.08         0.35         0.05         0.44         0.41         0.13         0.08         0.14         0.41         0.055         0.05         0.03         0.74         0.45         0.25         0.03         0.74         0.35         0.055 <td>162898</td> <td>5 0.265</td> <td>0.545</td> <td>-0.91</td> <td>-0.595</td> <td>-0.06</td> <td>0.065</td> <td>1.235</td> <td>0.4</td> <td>0.04</td> <td>5 0.285</td> <td>-0.15</td> <td>0.2</td> <td>6 0.085</td> <td>-0.235</td> <td>1.705</td> <td>1.535</td> <td>0.255</td> <td>0.035</td>	162898	5 0.265	0.545	-0.91	-0.595	-0.06	0.065	1.235	0.4	0.04	5 0.285	-0.15	0.2	6 0.085	-0.235	1.705	1.535	0.255	0.035
14       0.253       0.04       0.663       0.025       0.73       0.87       1.19       0.735       0.755       0.04       0.055       -0.255       1.15       0.88       0.625       0.24       0.055       -0.255       1.15       0.40       0.88       0.55       0.03       0.275       -0.445       0.115       -0.45       0.125       0.15       0.40       0.88       0.55       0.03       0.275       -0.445       0.115       -0.45       0.165       0.43       0.074       0.535       0.717       0.915       0.44       0.417       0.055       0.13       0.075       0.041       0.44       0.355       0.015 <td< td=""><td>170932</td><td>9 -0.66</td><td>0.13</td><td>-0.05</td><td>55 0.005</td><td>0.37</td><td>0.435</td><td>1.26</td><td>0.975</td><td>0.66</td><td>5 0.1</td><td>0.51</td><td>0.54</td><td>4 0.1</td><td>0.22</td><td>1.3</td><td>1.17</td><td>-0.56</td><td>-0.5</td></td<>	170932	9 -0.66	0.13	-0.05	55 0.005	0.37	0.435	1.26	0.975	0.66	5 0.1	0.51	0.54	4 0.1	0.22	1.3	1.17	-0.56	-0.5
66       0.435       -0.439       -0.439       -0.43       0.41       0.88       0.5       0.46       0.09       0.14       0.11       0.015       1.275       1.05       0.015       -0.46         66       0.485       -0.25       0.23       0.135       0.045       0.047       1.565       1.305       1.335       0.045       0.047       0.53       0.045       0.047       0.045       0.047       0.045       0.047       0.045       0.047       0.045       0.047       0.045       0.047       0.045       0.045       0.045       0.047       0.045	1	4 0.215	0.04	-0.60	0.025	0.73	0.87	1.19	0.735	0.75	i5 0.06	0.525	0.24	4 0.055	-0.255	1.115	0.89	-0.625	-0.33
18       -1.245       0.11       -0.005       -0.275       0.113       0.075       0.848       0.88       0.38       0.275       -0.145       0.115       -0.28       0.124       0.025       0.024       0.024       0.025       0.015       0	6	0 0.455	-0.195	-0.4	49 -0.45	-0.315	0.4	0.88	0.5	0.4	6 0.09	0.14	0.13	1 0.09	-0.815	1.275	1.05	0.015	-0.46
66         0.43         0.43         0.43         1.343         1.343         1.343         0.34         0.35 <th0.35< th="">         0.35         0.35         <th< td=""><td>1</td><td>8 -1.245</td><td>0.11</td><td>-0.00</td><td>0.275</td><td>0.115</td><td>0.075</td><td>0.845</td><td>0.8</td><td>0.39</td><td>0.03</td><td>0.275</td><td>-0.14</td><td>5 0.115</td><td>-0.82</td><td>1.6</td><td>2.045</td><td>-0.28</td><td>0.385</td></th<></th0.35<>	1	8 -1.245	0.11	-0.00	0.275	0.115	0.075	0.845	0.8	0.39	0.03	0.275	-0.14	5 0.115	-0.82	1.6	2.045	-0.28	0.385
1       0.445       0.035       0.315       0.23       0.79       0.915       1.6       0.85       0.905       0.73       0.25       0.785       0.085       -0.16       1.435       1.675       -0.255       0.015         0       0.26       0.215       0.025       0.025	4	6 -0.475	-0.25	-1.0	0.195	0.065	0.47	1.505	0.25	0.1	4 0.04	0.37	0.53	5 0.065	0.13	0.74	0.535	-0.75	-0.915
50         0.26         0.215         0.415         0.42         0.042         0.042         0.042         0.013         0.11         0.19         -0.71         0.79         0.735         0.035         0.035           23         -0.065         0.075         -0.015         0.015         0.095         0.025         0.025         0.013         0.11         0.055         1.13         1.1725         -0.025         0.025         0.027         0.014         0.015         1.13         0.075         0.025         0.027         0.035         0.035         0.035         0.035         0.037         0.035         0.047         0.014         0.055         0.025         0.025         0.025         0.015         0.017         0.035         0.055         0.025	15	1 -0.445	0.035	0.31	15 0.23	0.79	0.915	1.6	0.85	0.90	0.37	0.35	0.78	5 0.085	-0.16	1.495	1.675	-0.555	-0.215
12         0.005         0.005         0.015         0.015         0.015         0.015         0.115         0.115         0.015         0.111         0.015         0.135         0.115         0.015         0.111         0.015         0.135         0.115         0.015         0.111         0.015         0.135         0.115         0.015         0.	5	0 <mark>0.26</mark>	0.215	0.16	55 0.42	-0.095	0.81	1.29	0.53	0.4	0.045	0.25	-0.1	1 0.19	-0.71	0.79	0.535	-0.78	-0.345
25       -0.82       -0.837       -0.335       -0.335       -0.335       -0.335       -0.335       -0.335       -0.335       -0.335       -0.335       -0.137       -0.11       -0.06       -0.335       -0.137       -0.25       -0.137       -0.25       -0.13       -0.15       -0.17       -0.14       -0.15       -0.07       -1.335       -1.07       -0.125       -0.15 </td <td>2</td> <td>3 -0.605</td> <td>0.075</td> <td>-0.01</td> <td>L5 0.015</td> <td>0.095</td> <td>0.955</td> <td>1.66</td> <td>1.045</td> <td>0.12</td> <td>5 0.055</td> <td>0.29</td> <td>-0.15</td> <td>5 0.14</td> <td>-0.51</td> <td>1.41</td> <td>1.725</td> <td>-0.29</td> <td>0.135</td>	2	3 -0.605	0.075	-0.01	L5 0.015	0.095	0.955	1.66	1.045	0.12	5 0.055	0.29	-0.15	5 0.14	-0.51	1.41	1.725	-0.29	0.135
1/10       0.01       0.02       0.03       0.015       0.05       0.03 <th0.03< th="">       0.03       0.03</th0.03<>	2	-0.82	-0.565	-0.37	-0.355	-0.095	0.285	0.73	1.42	0.5	0.01	0.135	0.17	5 0.11	0.065	1.335	1.075	-0.285	-0.075
74       -0.345       0.07       -0.01       -0.025       -0.285       0.125       0.87       1.56       1.325       0.415       0.445       0.455       0.045       0.055       0.055       0.055       0.055       0.165       1.22       0.025       -0.43         1670124       0.01       -0.235       -0.035       -0.11       0.375       0.335       0.97       1.36       1.32       0.08       0.415       0.015       0.025       0.027       -0.64       0.055       0.015       0.115       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.15       0.115       0.115       0.015	2	6 -0.95	0.035	-0.5	59 -0.55	-0.18	0.01	1.235	0.05	0.5	1 0.47	0.14	0.10	5 0.07	-1.39	1.11	0.555	-1.89	-1.235
1726929       0.105       -0.115       -0.4       -0.215       0.08       0.18       0.84       0.915       0.45       0.175       0.255       1.31       0.71       -0.64       -0.82         1670124       0.01       -0.235       -0.035       -0.11       0.375       0.335       0.97       1.35       1.45       1.15       0.025       0.22       0.265       0.165       1.17       1.675       0.25       0.015       1.16       0.085       0.22       0.265       0.165       0.15       0.155	7	4 -0.345	0.07	-0.0	-0.025	-0.285	0.125	0.87	1.56	1.32	0.425	0.415	0.49	5 0.055	0.055	1.655	1.22	0.025	-0.43
16/0124         0.012         0.013         0.013         0.013         0.015         <	172692	9 0.105	-0.115	-0	.4 -0.215	0.08	0.86	1.8	0.84	0.91	.5 0.445	0.6	0.21	5 0.175	0.255	1.31	0.71	-0.64	-0.82
100100         04100         04100         040000         04000         04000         <	167012	4 0.01	-0.235	-0.03	-0.11	0.375	0.335	0.97	1.36	1.3	0.08	0.135	-0.41	0.015	-0.095	1.7	1.675	0.25	0.495
1666224       -0.61       0.085       -0.05       0       0.49       0.62       0.845       0.66       0.885       0.115       -0.215       0.18       -0.405       0.666       0.885       0.135       -0.215       0.18       -0.405       0.666       0.885       0.155       0.115       0.18       -0.405       0.615       0.815       0.115       0.015       0.065       0.485       0.015       0.015       0.055       0.185       0.015       0.015       0.065       0.485       0.015       0.	163548	8 -0.155	0.025	-0.2	25 0.02	0.095	-0.015	1.335	-0.05	0.56	0.38 5 0.015	0.755	0.2	6 0.035	-0.14	1.315	0.675	0.105	0.005
1698630       -0.47       0.04       0.025       0.145       0.555       1.525       2.09       0.81       0.94       0.05       0.64       0.565       0.855       -0.185       1.115       1.485       0.305       -0.045         1628985       0.355       -0.175       -0.02       -0.05       -0.075       -0.03       1.12       0.065       -0.045       0.055       -0.455 <td< td=""><td>168626</td><td>4 -0.61</td><td>0.085</td><td>-0.00</td><td>05 0</td><td>0.49</td><td>0.62</td><td>0.845</td><td>0.66</td><td>0.88</td><td>5 0.415</td><td>0.115</td><td>-0.21</td><td>5 0.18</td><td>-0.405</td><td>0.66</td><td>0.885</td><td>0.28</td><td>0.385</td></td<>	168626	4 -0.61	0.085	-0.00	05 0	0.49	0.62	0.845	0.66	0.88	5 0.415	0.115	-0.21	5 0.18	-0.405	0.66	0.885	0.28	0.385
1622985       0.355       -0.175       -0.075       -0.075       -0.03       1.12       0.695       0.71       -0.03       0.02       0.015       0.665       -0.455       1.245       1.025       -0.415       -0.185         1709329       -0.78       0.02       -0.62       0.065       0.016       -0.025       0.015       -0.25       0.165       -0.25       1.31       0.79       -0.09       -0.04         14       -0.745       0.02       -0.62       0.005       0.38       0.875       1.48       0.72       0.79       0.06       0.65       0.01       0.07       0.109       1.31       0.79       -0.09       -0.04         60       -0.475       0.025       -0.025       0.035       0.25       0.425       0.045       -0.25       0.145       -0.25       0.045	169863	0 -0.47	0.04	0.02	0.145	0.555	1.525	2.09	0.81	0.9	4 0.05	0.64	0.56	5 0.855	-0.185	1.915	1.485	0.305	-0.055
1/0522       -0.78       -0.78       -0.79       -0.78       -0.79       -0.74       -0.745       -0.76       -0.76       -0.79       -0.79       -0.79       -0.745       -0.79       -0.76       -0.75       -0.79	162898	5 0.355	-0.175	-0.2	-0.095	-0.075	-0.03	1.12	0.695	0.7	1 -0.03	0.02	0.01	5 0.065	-0.455	1.245	1.025	-0.415	-0.185
6       0.472       0.005       0.0	170932	-0.78 4 -0.745	0.05	-0.33	0.065 52 0.005	0.4	0.45	0.975	0.865	0.64	0.06	-0.045	-0.2	0.165	-0.825	1.31	0.79	-0.09	-0.04
18       -1.215       0.225       -0.02       -0.005       0.31       0.26       0.9       0.735       0.46       0.065       0.28       -0.23       0.065       -0.96       1.945       1.765       0.025       0.475         66       0.145       -0.125       -0.025       -0.455       0.045       0.53       1.63       1.24       1.675       0.52       0.415       0.25       0.04       -0.01       0.91       0.59       -0.05       -0.47         46       -0.165       -0.15       -0.34       -0.39       0.15       0.105       1.75       0.485       0.85       0.06       0.015       -0.05       1.63       1.295       -0.3       -0.665         50       0.145       0.34       0.18       0.24       0.315       0.79       1.27       0.5       0.405       0.325       0.27       0.22       0.13       -0.16       0.38       0.665       1.63       1.295       -0.38       -0.215       0.015       0.015       0.015       0.015       0.015       0.015       0.015       0.015       0.015       0.016       0.015       0.016       0.015       0.012       1.015       0.125       0.12       0.125       0.125	6	0 -0.475	-0.06	-0.81	L5 -0.89	-0.325	0.22	0.605	0.465	0.4	3 0.09	0.81	0.49	5 0.045	-0.505	1.39	1.015	-0.02	-0.535
66       0.145       -0.125       -0.025       -0.455       0.045       0.05       1.63       1.24       1.67       0.52       0.415       0.255       0.04       -0.11       0.91       0.59       -0.47         46       -0.165       -0.15       -0.34       -0.39       0.05       0.2       1       0.23       0.15       -0.41       0.25       0.04       -0.11       0.05       1.63       1.295       -0.3       -0.665         151       0.115       0.055       -0.42       0.105       1.75       0.845       0.325       0.27       0.22       0.13       -0.055       1.63       1.295       -0.38       -0.21         0       0.145       0.34       0.18       0.24       0.315       0.79       1.27       0.5       0.455       0.455       0.45       0.42       0.31       0.17       0.38       0.21       -0.55       0.655       0.655       0.655       0.655       0.65	1	8 -1.215	0.225	-0.0	-0.005	0.31	0.26	0.9	0.735	0.4	0.065	0.28	-0.2	3 0.065	-0.96	1.945	1.765	0.085	0.325
46       -0.165       -0.15       -0.34       -0.39       0.005       0.2       1       0.23       0.165       -0.40       0.13       0.03       0.08       -0.25       1.63       1.29       -0.3       -0.665         151       0.115       0.045       0.125       -0.01       0.005       1.005       1.75       0.845       0.39       0.5       0.86       0.115       -0.665       1.26       0.79       -0.38       -0.21         0       0.145       0.34       0.18       0.18       0.19       0.15       0.065       0.15       -0.05       0.06       0.115       -0.605       1.26       0.79       -0.38       -0.21         2       0.07       -0.35       0.65       0.08       0.915       1.67       0.66       0.705       0.015       -0.25       0.08       -0.25       0.76       0.16       0.035       0.08       -0.625       1.045       0.48       0.25       0.075       0.08       0.025       0.08       0.025       0.07       -0.28       0.15       0.025       0.08       0.126       0.49       0.21       0.45       0.25       0.45       0.25       0.45       0.25       0.47       -0.21       0.42	6	6 0.145	-0.125	-0.02	-0.455	0.045	0.53	1.63	1.24	1.67	0.52	0.415	0.25	5 0.04	-0.11	0.91	0.59	-0.56	-0.47
131       0.115       0.125       0.014       0.00       1.00       1.05       0.453       0.453       0.45       0.22       0.22       0.23       -0.13       -0.17       0.45	4	6 -0.165	-0.15	-0.3	-0.39	0.105	0.2	1	0.23	0.16	5 -0.04	0.13	0.2	3 0.08	-0.25	1.63	1.295	-0.3	-0.665
23       -0.75       -0.85       -0.65       0.165       0.08       0.915       1.67       0.66       0.705       0.017       0.116       0.08       -0.685       0.165       0.66       0.705       0.075       -0.015       -0.085       0.08       -0.625       0.68       -0.625       0.08       -0.625       0.08       -0.625       0.08       -0.625       0.08       0.025       -0.185       0.12       0.08       -0.625       0.08       0.025       -0.77       -0.125         72       0.06       0.19       0.315       0.025       0.07       0.04       0.82       0.89       0.335       -0.045       0.22       0.045       0.03       1.26       0.4       -0.77       -1.12         26       0.155       0.085       0.035       0.11       1.2       1.055       0.69       0.45       0.455       0.22       0.045       0.03       1.26       0.77       -1.12         26       0.155       0.085       0.035       0.11       1.2       1.055       0.69       0.45       0.455       0.22       0.045       0.03       1.46       1.11       0.05       -0.17       -1.12         26       0.15       0.085	15	0.115	0.055	-0.12	-0.01	0.06	0.79	1.75	0.845	0.85	0.39	0.5	0.8	2 0.115	-0.605	1.26	0.79	-0.38	-0.21
25       0.05       0.04       0.025       -0.625       0.08       0.045       0.725       1.025       1.055       0.015       -0.185       0.12       0.08       0.265       1.89       0.058       0.12       -0.82         72       0.06       0.19       0.315       0.025       0.07       0.04       0.82       0.89       0.335       -0.04       0.045       0.22       0.045       0.03       1.16       0.07       -1.11         26       0.155       0.08       0.035       -0.15       0.017       1.12       1.055       0.69       0.435       0.455       0.095       0       1.46       1.11       0.05       -0.21         74       -0.3       -0.005       -0.005       0.03       -0.25       0.396       0.38356       0.49461       0.24277       0.4166       1.14       0.05       -0.211         standard eviatic       0.44722       0.265047       0.33426       0.33262       0.238562       0.383568       0.49461       0.242477       0.42157       0.421678       0.532527       0.471707         standard eviatic       0.44722       0.265047       0.338426       0.3022       0.273539       0.128578       0.17875       0.11825	2	3 -0.76	-0.35	-0.63	35 0.165	0.08	0.915	1.67	0.66	0.70	0.075	-0.16	-0.03	5 0.08	-0.625	2.315	0.765	0.625	-1.045
72       0.06       0.19       0.315       0.025       0.07       0.04       0.82       0.89       0.335       -0.04       0.045       0.22       0.045       0.03       1.26       0.07       -1.11         26       0.155       0.08       0.035       -0.55       0.035       0.11       1.2       1.055       0.69       0.435       0.455       0.095       0       1.46       1.11       0.05       -0.21         74       -0.3       -0.005       -0.005       0.03       -0.25       0.07       0.82       1.47       1.09       0.785       0.175       -0.416       1.46       1.11       0.05       -0.21         standard deviati       0.47720       0.265047       0.33426       0.3302       0.273539       0.38582       0.40861       0.244277       0.2623       0.29357       0.1325       0.421727       0.421678       0.532527       0.471707         standard deviati       0.4772       0.265047       0.338426       0.330562       0.383580       0.424277       0.424277       0.1215       0.32875       0.17875       0.11825       0.425784       1.44       1.050156       0.23875       0.424277       0.11825       0.1825       0.1825       0.1825	2	5 0.05	0.04	0.02	-0.625	0.08	0.045	0.725	1.025	1.05	5 0.015	-0.185	0.1	2 0.08	0.265	1.89	0.58	0.12	-0.82
26         0.155         0.08         0.035         0.035         0.013         1.22         1.055         0.69         0.435         0.145         0.855         0.095         0         1.46         1.11         0.05         -0.21           74         -0.3         -0.005         -0.005         -0.03         -0.225         0.07         0.82         1.47         1.29         0.785         0.185         0.205         0.175         -0.145         0.427227         0.421678         0.532527         0.471107           standard deviati         0.4772         0.2650477         0.338426         0.3022         0.335682         0.383568         0.404861         0.244277         0.1228         0.33242         0.421678         0.532527         0.471107           -0.27938         0.0105         0.1608         -0.139         0.155625         0.42875         1.206125         0.82657         0.18875         0.11825         -0.125288         1.14         1.050156         -0.23875         -0.27644	7	2 0.06	0.19	0.31	15 0.025	0.07	0.04	0.82	0.89	0.33	-0.04	0.045	0.2	2 0.045	0.03	1.26	0.4	-0.77	-1.1
standard deviatic 0.44722 0.255047 0.338426 0.3002 0.273539 0.385682 0.385682 0.38865 0.44861 0.244277 0.26238 0.299357 0.132928 0.383424 0.427227 0.421678 0.532527 0.477107	2	6 0.155	0.08	0.03	-0.55	0.035	0.11	1.2	1.055	0.6	0.435	0.145	0.58	5 0.095	0	1.46	1.11	0.05	-0.21
-0.25938 0.0105 0.16063 -0.139 0.155625 0.422875 1.206125 0.865875 0.770375 0.216125 0.28575 0.178875 0.11825 -0.25288 1.34 1.050156 -0.23875 -0.27641	standard deviat	ic 0.44722	0.265047	0.33842	26 0.3022	0.273539	0.385682	0.38067	0.383858	0.40486	0.785	0.26238	0.29935	7 0.132928	0.383424	0.427227	0.421678	0.532527	0.477107
		-0.25938	0.0105	-0.1606	-0.139	0.155625	0.428875	1.206125	0.865875	0.77037	5 0.216125	0.28575	0.17887	5 0.11825	-0.25288	1.34	1.050156	-0.23875	-0.27641

Appendix C Statistical analyses

D2m	UD1m
-1.5 -1 -0.5 0 0.5	-1 -0.5 0
Ouantiles	Ouantiles
100.0% maximum 0.495	100.0% maximum 0.65
99.5% 0.495	99.5% 0.65
97.5% 0.494	97.5% 0.64738
90.0% 0.2645	90.0% 0.3285
75.0% quartile 0.1375	75.0% quartile 0.10375
50.0% median -0.295	50.0% median 0.04
25.0% quartile -0.5988	25.0% quartile -0.1225
10.0% -0.816	10.0% -0.2545
2.5% -1.2443	2.5% -0.8673
0.5% -1.245	0.5% $-0.875$
Summary Statistics	Summary Statistics
Mean _0 250375	Mean 0.0105
Std Dev 0.4472196	Std Dev 0 2650467
Std Err Mean 0.0707116	Std Err Mean 0.0419076
Upper 95% Mean -0.116347	Upper 95% Mean 0.095266
Lower 95% Mean -0.402403	Lower 95% Mean -0.074266
N 40	N 40
Test Mean	Test Mean
Hypothesized Value 0.5	Hypothesized Value 0.5
Actual Estimate -0.2594	Actual Estimate 0.0105
DF 39	DF 39
Std Dev 0.44722	Std Dev 0.26505
t Test	t Test
lest Statistic -10.739	lest Statistic -11.680
Prob > [t] <.0001*	$Prob >  t  < 0001^{-1}$
Prob < t < 00014	Prob < t < 8061°
and the second	<del>ا من مراسم معراسية مسارسية مسارسة م</del>

D2pm		UD1pm
-1 -0.5	0 0.5	-1 -0.75 -0.5 -0.25
		Quantilas
100.0% maximum 0.315		100.0% maximum 0.44
99.3% 0.313 07.5% 0.215		99.3% 0.444
90.0% 0.2345		90.0% 0.223
75.0% guartile 0.025		75.0% quartile 0.025
50.0% median -0.035		50.0% median -0.02
25.0% quartile -0.3663		25.0% quartile -0.382!
10.0% -0.6335		10.0% -0.590
2.5% -1.0271		2.5% -0.8836
0.5% -1.03		0.5% -0.89
0.0% minimum –1.03		0.0% minimum -0.89
Summary Statistics		Summary Statistics
Mean -0.160625		Mean -0.13
Std Dev 0.3384262		Std Dev 0.302199
Std Err Mean 0.0535099		Std Err Mean 0.04778
Upper 95% Mean -0.052391		Upper 95% Mean -0.04235
Lower 95% Mean -0.268859		Lower 95% Mean -0.23564
lest Mean		
Hypothesized Value 0.5		Hypothesized Value 0
Actual Estimate -0.1606		Actual Estimate -0.1
Std Dev 0.33843		Std Dev 0.30
t Test		t Test
Test Statistic -12.346		Test Statistic -13,373
Prob >  t  <.0001*		$Prob >  t  < .0001^*$
Prob > t 1.0000		Prob > t 1.0000
Prob < t <.0001*		Prob < t <.0001*

0.25

N	UDI
-0.4 -0.2 0 0.2 0.4 0.6 0.8	0 0.5 1
Quantiles	Quantiles
100.0% maximum 0.79	100.0% maximum 1.525
99.5% 0.79	99.5% 1.525
97.5% 0.7885	97.5% 1.512
90.0% 0.5535	90.0% 0.9285
75.0% quartile 0.36875	75.0% quartile 0.8175
50.0% median 0.095	50.0% median 0.31
25.0% quartile 0.0275	25.0% quartile 0.095
10.0% -0.2745	10.0% 0.013
	2.5% -0.0544
U.5% -U.325	U.5% -U.055
0.0% minimum -0.325	0.0% minimum -0.055
Summary Statistics	Summary Statistics
Mean 0.155625	Mean 0.428875
Std Dev 0.2735385	Sta Dev 0.385682
Stu Eff Mean 0.0432502	Sta Err Mean 0.000981/
Opper 95% Mean 0.2451009	Lower 95% Mean 0.3055279
N 40	N 40
Test Mean	Test Mean
Hypothesized Value 0.5	Hypothesized Value 0.5
Actual Estimate 0.15563	Actual Estimate 0.42888
DF 39	DF 39
Std Dev 0.27354	Std Dev 0.38568
t Test	t Test
Test Statistic -7.9624	Test Statistic ~1.1663
Prob >  t  <.0001*	Prob >  t  0.2506
Prob > t 1.0000	Prob > t 0.8747
Prob < t <.0001*	Prob < t 0.1253
$\wedge$	$\bigwedge$

0.5 1 1.5 2	-1.5 -1 -0.5 0
Quantiles	Quantiles
100.0% maximum 2.09	100.0% maximum 0.295
99.5% 2.09	99.5% 0.295
97.5% 2.08475	97.5% 0.29425
90.0% 1.795	90.0% 0.2145
75.0% quartile 1.54375	75.0% quartile 0.05125
50.0% median 1.195	50.0% median -0.18
25.0% quartile 0.8725	25.0% quartile -0.4963
10.0% 0.82	10.0% -0.8195
2.5% 0.608	2.5% -1.3792
0.5% 0.605	0.5% -1.39
0.0% minimum 0.605	Cummany Ctastictics
Summary Statistics	Summary Statistics
Mean 1.206125	Mean -0.252875
Std Dev 0.3800099	Std Err Moon 0.0606247
Unner 95% Mean 1 3278602	Upper 95% Maan0 13025
lower 95% Mean 1 0843808	Lower 95% Mean -0.3755
N 40	N 40
Test Mean	Test Mean
Hypothesized Value 0.5	Hypothesized Value 0.5
Actual Estimate 1.20613	Actual Estimate -0.2529
DF 39	DF 39
Std Dev 0.38067	Std Dev 0.38342
t Test	t Test
Test Statistic 11.7318	Test Statistic -12.419
Prob >  t  <.0001*	$Prob >  t  < .0001^{*}$
Prob > t <.0001*	Prob > t 1.0000
Prob < t 1.0000	<b>Prob &lt; t</b> <.0001×
$\bigwedge$	
	······································

D1m	LD2pm
	-0.5 -0.25 0 0.25 0.5 0
Quantiles	Quantiles
100.0% maximum 0.855	100.0% maximum 0.86
99.5% 0.855	99.370 0.80 07.5% 0.85.812
97,5% 0.04025	90.0% 0.583
75.0% quartile 0.1375	75.0% guartile 0.26
50.0% median 0.085	50.0% median 0.21
25.0% guartile 0.06125	25.0% quartile -0.0238
10.0% 0.0405	10.0% -0.2285
2.5% 0.00525	2.5% -0.4138
0.5% 0.005	0.5% -0.415
0.0% minimum 0.005	0.0% minimum -0.415
Summary Statistics	Summary Statistics
Mean 0.11825	Mean 0.178875
Std Dev 0.1329283	Std Dev 0.2993572
Std Err Mean 0.0210178	Std Err Mean 0.0473325
Upper 95% Mean 0.1607625	Upper 95% Mean 0.2746141
Lower 95% Mean 0.0757375	N 40
I est mean	
Hypothesized Value 0.5	Hypothesized Value 0.5
Actual Estimate 0.11825	DE 20
UF 37 Std Day 0 13293	Std Dev 0.29936
	t Test
Liest Test Statistic _18 163	Test Statistic -6.7844
Prob > $ t  < 0001^{\circ}$	$Prob >  t  < .0001^{\circ}$
Prob > t 1.0000	Prob > t 1.0000
Prob < t <.0001*	Prob < t <.0001*
00 02 04 06 08 10	0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9

D1pm	
-0.2 0 0.2 0.4 0.6 0.8 1	0 0.2 0.4 0.6
Quantiles	Quantiles
100.0% maximum 0.81	100.0% maximum 0.825
99.5% 0.81	99.5% 0.825
97.5% 0.80938	97.5% 0.824
90.0% 0.7345	90.0% 0.538
75.0% quartile 0.4875	75.0% quartile 0.40875
50.0% median 0.26	50.0% median 0.0825
25.0% quartile 0.1225	25.0% quartile 0.045
10.0% -0.0385	10.0% -0.0215
2.5% -0.1844	2.5% -0.04
0.5% -0.185 0.0% minimum -0.185	0.0% minimum -0.04
Summary Statistics	Summary Statistics
Mean 0.28575	Mean 0.216125
Std Dev 0.2623795	Std Dev 0.2442768
Std Err Mean 0.0414858	Std Err Mean 0.0386235
Upper 95% Mean 0.369663	Upper 95% Mean 0.2942485
Lower 95% Mean 0.201837	Lower 95% Mean 0.1380015
N 40	N 40
Test Mean	Test Mean
Hypothesized Value 0.5	Hypothesized Value 0.5
Actual Estimate 0.20375	DE 20
Std Dev 0.26238	Std Dev 0 24428
+ Tast	510 Dev 0.24420
LIESL Test Statistic -5 1644	Test Statistic7 3/08
$\frac{1}{2} \frac{1}{2} \frac{1}$	$\frac{1}{2} = \frac{1}{2} = \frac{1}$
$\frac{100}{100} = 10000$	Prob > t = 1.0000
Prob < t <.0001*	Prob < t <.0001*

	LDC
0 0.5 1 1.5	0 0.5 1
Quantiles	Quantiles
100.0% maximum 1.675	100.0% maximum 1.56
99.5% 1.675	99.5% 1.56
97.5% 1.66875	97.5% 1.55775
90.0% 1.325	90.0% 1.4425
75.0% quartile 1.1375	75.0% quartile 1.09625
50.0% median 0.7075	50.0% median 0.85
25.0% quartile 0.4225	25.0% quartile 0.66
10.0% 0.2855	10.0% 0.265
2.5% 0.12538	2.5% -0.053
0.5% 0.125	0.5% –0.06
Summary Statistics	Summary Statistics
Moon 0 770375	Mean 0 865875
Std Dev 0.4048605	Std Dev 0.3838584
Std Err Mean 0.0640141	Std Err Mean 0.0606933
Upper 95% Mean 0.8998557	Upper 95% Mean 0.9886389
Lower 95% Mean 0.6408943	Lower 95% Mean 0.7431111
N 40	N 40
Test Mean	Test Mean
Hypothesized Value 0.5	Hypothesized Value 0.5
Actual Estimate 0.77038	Actual Estimate 0.86587
DF 39	DF 39
Std Dev 0.40486	Stu Dev 0.56566
Test Statistic 4 2237	Test Statistic 6 0283
Proh >  t  0.0001*	$Prob >  t  < 0.0001^{\circ}$
Prob > t <.0001*	$Prob > t < .0001^{+}$
Prob < t 0.9999	Prob < t 1.0000
······································	

ROD1	PROD2
0 0.5 i 1.5 2 2.5	0.5 1 1.5
Quantiles	Quantiles
100.0% maximum 2.315	100.0% maximum 2.045
99.5% 2.315	99.5% 2.045
97.5% 2.315	97.5% 2.045
90.0% 1.9075	90.0% 1.71
75.0% quartile 1.6225	75.0% quartile 1.27625
50.0% median 1.3125	50.0% median 1.0225
25.0% quartile 1.13375	25.0% quartile 0.72375
10.0% 0.755	10.0% 0.541
2.370 0.07 0.5% 0.07	2.5% U.4
0.0% minimum 0.07	0.0% minimum 0.4
Summary Statistics	Summary Statistics
Mean 1.34	Mean 1.0501563
Std Dev 0.4272266	Std Dev 0.4216777
Std Err Mean 0.0755237	Std Err Mean 0.0745428
Upper 95% Mean 1.4940316	Upper 95% Mean 1.2021873
Lower 95% Mean 1.1859684	Lower 95% Mean 0.8981252
N 32	N 32
Test Mean	Test Mean
Hypothesized Value 0.5	Hypothesized Value 0.5
Actual Estimate 1.34	Actual Estimate 1.05016
Std Dev 0.42723	Std Dev. 0.42169
t Tart	JU DEV 0.42108
LICSL Test Statistic 11 1223	L Test Test Statistic 7 3804
Prob > $ t  < 0.001^\circ$	$Prob >  t  \ll 0.001^{\circ}$
$Prob > t < .0001^\circ$	$Prob > t < .0001^{\circ}$
Prob < t 1.0000	Prob < t 1.0000
$\bigwedge$	

-2 -1.5 -1 -0.5 0 0.5 1	-1 -0.5 0
Ouantiles	Quantiles
100.0% maximum 0.755	100.0% maximum 0.68
99.5% 0.755	99.5% 0.68
97.5% 0.755	97.5% 0.68
90.0% 0.2975	90.0% 0.385
75.0% quartile 0.1	75.0% quartile 0.0275
50.0% median -0.185	50.0% median -0.2125
25.0% quartile -0.56	25.0% quartile -0.55
10.0% -0.777	10.0% -1.006
2.5% -1.89	2.5% -1.235
0.5% -1.89	0.5% -1.235
0.0% minimum –1.89	0.0% minimum -1.235
Summary Statistics	Summary Statistics
Mean -0.23875	Mean -0.276406
Std Dev 0.5325274	Std Dev 0.4771069
Std Err Mean 0.0941384	Std Err Mean 0.0843414
Upper 95% Mean -0.046753	Upper 95% Mean -0.104391
Lower 95% Mean -0.430747	Lower 95% Mean -0.448422
N 32	N 32
Test Mean	Test Mean
Hypothesized Value 0.5	Hypothesized Value 0.5
Actual Estimate -0.2388	Actual Estimate -0.2764
DF 31	DF 31
Std Dev 0.53253	Sta Dev 0.47/11
t Test	t Test
Test Statistic -7.8475	lest Statistic -9.2055
Prob > [t] <.0001*	$Prob >  t  < .0001^{\circ}$
Prob > t 1.0000	$Prob < t \qquad < 0.001 *$
**************************************	
-0.5 0.0 0.5 1.0 1.5	-0.5 0.0 0.5 1.0 1.5

Appendix D Research ethics



#### Acknowledgement Letter Exempt Initial Protocol Review

09/11/2015
Peter Ngan
WVU Office of Research Integrity and Compliance
09/11/2015
09/10/2018
Acknowledgement Letter Exempt Initial Protocol Review
1506733970
Adjustment of Bracket Position Away From the Andrew's Plane to Accommodate for Height Discrepancy.

The above-referenced study was reviewed by the West Virginia University Institutional Review Board IRB and was granted exemption in accordance with 45 CFR 46.101.

" This research study was granted an exemption in accordance with Research on existing data, documents, records, pathological specimens, or diagnostic specimens [45 CFR 46.101(4)]. In accordance with the Health Insurance Portability and Accountability Act, a waiver of research authorization has been granted. Please fulfill the subject accounting requirements associated with the granting of this waiver. All exemptions are only good for three years. If this research extends more than three years beyond the approved date, then the researcher will have to request another exemption. The following documents have been acknowledged for use in this study and are available in the WVU+kc system:

Documents reviewed and/or approved as part of this submission:

Data Points.docx: 2015-09-09-04:00

Documents for use in this study have been acknowledged and are available in the WVUkc system in the Notes and Attachments section of your protocol.

The Office of Research Integrity and Compliance is here to provide assistance to you from the initial submission of an IRB protocol and all subsequent activity. Please feel free to contact us by phone at 304.293.7073 with any question you may have. Thank you.

WVU Office of Research Integrity and Compliance

Date:09/11/2015

Signed:

fton Wagner A R

Afton Wagner IRB Administrator