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# The climate of the Northeast : heating degree-days

W.H. Dickerson

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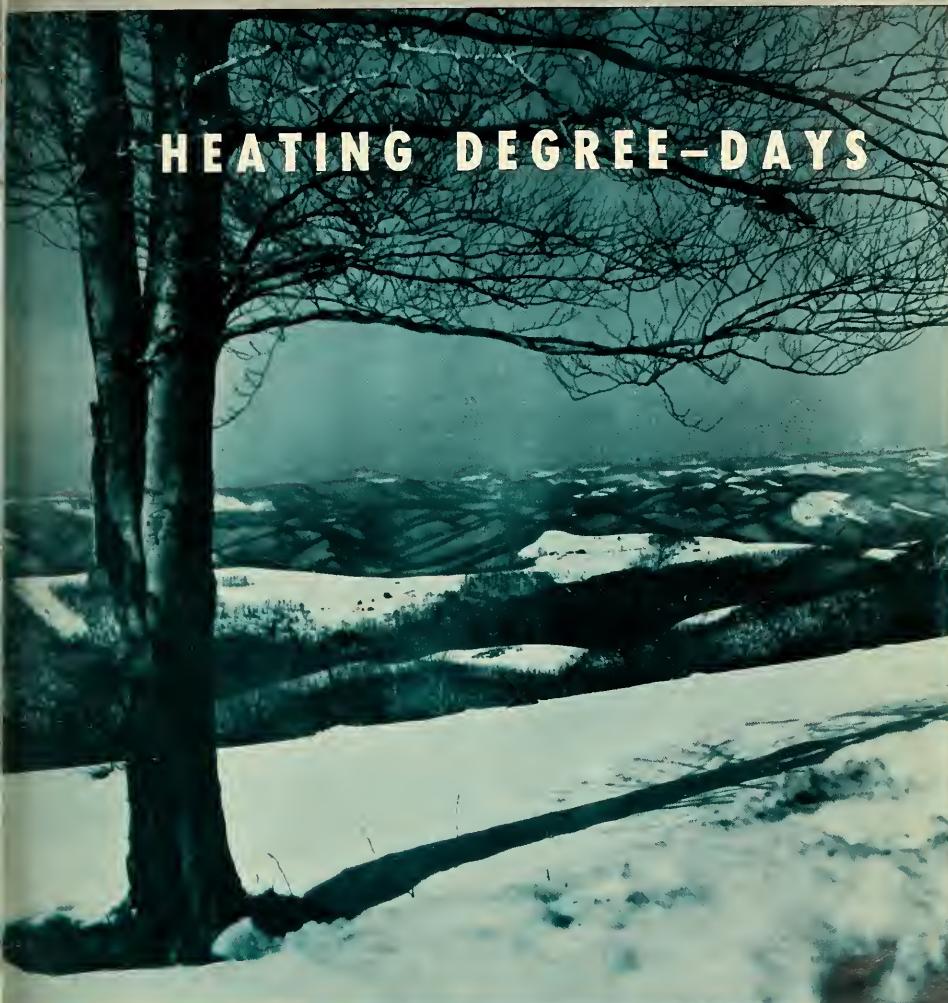
NORTHEAST REGIONAL RESEARCH PUBLICATION



3

## THE CLIMATE OF THE NORTHEAST

### HEATING DEGREE-DAYS



BULLETIN 483T

JUNE 1963

WEST VIRGINIA UNIVERSITY AGRICULTURAL EXPERIMENT STATION

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# THE CLIMATE OF THE NORTHEAST

## HEATING DEGREE-DAYS

W. H. DICKERSON, Agricultural Engineer

**T**HE HDD, or heating degree-day, has been defined as "a unit based on the difference between 65° F and the daily mean temperature when the latter is below 65° F" (2). Thus, the number of degree days for a given day is equal to 65° F minus the average temperature for the day, with negative differences being counted as zero. The HDD for any period such as a month, season, or year is secured by accumulating the daily values over the period.

The concept of the HDD is credited to the American Gas Industry. The theory (verified by extensive statistics) is that an average outdoor temperature of 65° F is the lowest permissible without supplying heat to a building which is used for human occupancy and is to be maintained at approximately 70° F. When the daily mean temperature drops below 65° F, heat is required and the amount of energy or fuel required is proportional to the number of HDD. The method may be applied to the estimation of energy requirements for maintaining indoor temperatures other than 70° F. For instance, according to Strock and Hotchkiss (11), the industrial heating degree day is sometimes based on 55° or 45°, instead of 65°, depending upon the temperature requirements of the structure.

Heating degree-day data may be used as a basis for planning the insulation and heating plants of buildings, and also for estimating the fuel requirements where heat losses can be calculated. Other uses include: checking the efficiency of heating plant operation for commercial buildings, in sales promotional work of insulating materials, or in special types of energy-use (such as electric heating), and for the estimation of fuel consumption to regulate the delivery of fuel by the distributor to the consumer. Current data on HDD may also provide a valuable public relations tool for fuel suppliers. Variations in the weather not readily discernible or remembered by the customer

which may cause complaints can be explained where these were due to temperature aberrations.

An example of the application of the HDD concept in agricultural production is found in the work reported by McCune (8). In experiments with the use of electric heat in the production of nursery stock, it was determined that energy consumption for soil heating was related to HDD during the heating period. A basis was provided for estimating energy requirements for various weather conditions.

The purpose of the work reported herein has been to compile, analyze, and prepare for publication basic climatological data on heating degree-days for the Northeastern United States. It is expected that the data will be most useful to engineers and others concerned with practical problems relating to heating, insulation, and construction. The information may also be of value for the development of new applications, methods, or theories, which will extend the usefulness of climatological data. As an example, data made available by the NE-35 program have provided a basis for calculating a multiple regression equation to be used in estimating normal annual HDD. The derivation, uses, and possible advantages of the equation are discussed in a later section of this bulletin.

## OUTLINE OF WORK ON HDD

### The NE-35 Committee and its Work

This bulletin is one of a series on The Climate of the Northeast which is being sponsored by the Northeast Regional Technical Committee on Climatology, commonly referred to as the NE-35 Committee. The committee is composed of representatives of agricultural experiment stations of the region who cooperate with the Weather Bureau

in the application of climatology to agriculture. The participating experiment stations and federal agencies are listed elsewhere, as are the titles of bulletins published to date. In addition, Gosslee and Brumbach (4) and Kolega and Palmer (6) have reported the results of work with HDD, supported in part by NE-35.

### **Source of Data for the Analysis**

Data on HDD were compiled as a part of the basic plan for the regional research. Each cooperating experiment station provided, in accordance with the decision of the technical committee, punched cards containing the weather data for selected weather stations. The original data were secured by the Weather Bureau through its network of cooperative observers. Checking and verification of the data prior to its use in the NE-35 program were accomplished through the cooperation of Weather Bureau personnel in the various states, and the Northeast Area Climatologist.

### **Computer Programs**

Information presented in the following sections of this report was secured almost entirely by the execution of electronic computer programs, which tabulated, summarized, and analyzed the raw data supplied by cooperating states. The computer programs were designed to:

- A. Re-calculate the four-week period averages and standard deviations, as shown in Table 3.
- B. Calculate the average annual HDD, including the estimated 14th period (which was not available for most stations), and the standard deviation.
- C. Estimate the return period of the coldest four-week periods by the extreme value frequency distribution.
- D. Test the homogeneity of variance between stations for the respective four-week periods and also for the annual means.
- E. Calculate a multiple regression equation for estimating the mean annual HDD for a station from its latitude, elevation, and mean annual temperature.

## **EXPLANATION AND DISCUSSION OF RESULTS AND DATA**

### **Station-Locator Map**

The station numbers assigned by the Weather Bureau are shown on Map 1, (Page 25) adjacent to the circle representing the geographical location. These numbers are related to the alphabetical order of the station name within each state. Accordingly, low numbers refer to stations the initial letters of which are in the first portions of the alphabet.

### **Annual Mean And Standard Deviation**

Table 2 is to be used in conjunction with the locator map. The state, station number, and county as well as elevation, latitude, and longitude of each station are shown in the first part of the table. Further information on these stations can be found in the Substation History publications of the U. S. Weather Bureau (17). Also given is the mean annual HDD and its standard deviation. The mean has been adjusted to account for Period 14. The estimate for this period was added to each year prior to calculation of the variance and standard deviation. The leap year date of February 29 was ignored. Table 1, a calendar of the climatological year, will clarify the period system used.

The annual mean and standard deviation is considered to be the most useful and important single statistic derived from the study. It is believed that the map of isolines of HDD, Map 2, is the most detailed and accurate representation that has been developed to date. The basis for this assertion is the station network density, which exceeds by far that previously available. It is advisable to insert a word of caution in using the data. The map is based on 156 stations, and should provide a good regional picture. It is true, however, that some individual stations, or small areas, may deviate significantly from the general picture. This is likely to be most pronounced in mountainous terrain, where differences in elevation and other orographic influences produce anomalies.

The usefulness of the standard deviation is based on the fact that the annual HDD totals follow the normal, or Gaussian, distribution,

according to Thom (15). Most applications of HDD have been based on use of the mean. For some purposes, a probability estimate is useful. The mean and standard deviation establish probability relationships for data which are normally distributed. After plotting standard deviations of the annual means on a map of the Northeast, it became evident that regional differences, which had been anticipated, were not large and followed no readily discernible pattern. A statistical test, Bartlett's Test for Homogeneity (10), indicated a common variance for the region. Variances were then pooled, and the standard deviation thereby derived was 443 HDD. This provided the basis for construction of Figure 1. With the annual mean, the annual HDD for any frequency can be determined.

### **Four-Week Period Means and Standard Deviations**

HDD were originally summarized in the NE-35 program by four-week periods of the climatological year. These data are shown in Table 3. Periods covering the summer months show zero or very low values for most stations, with only the coldest localities having any appreciable accumulation of HDD.

A test for homogeneity was made on the variances of the individual periods. No evidence of heterogeneity of variance was found among locations within periods covering the coldest portion of the year. Heterogeneity appeared in the warm periods, notably Periods 4, 5, 6, and 7. Over the region, the mean variance for a particular period was found to be related to mean HDD for that period. A standard deviation was calculated from the pooled variances for each period. These were then plotted against the corresponding average HDD and a smooth curve drawn through the points. Values of the standard deviation scaled from this curve were then used as a basis for constructing Figure 2. By selecting the mean HDD for any period and entering the graph at this value on the ordinate, the four-week period HDD for any frequency is readily determined.

The simplifying assumptions necessary for the construction of Figures 1 and 2 are probably not valid for every individual station and climatological period reported in Tables 2 and 3. Where this is suspected, the procedure outlined in Example 4, Page 6, should be followed to work out frequencies.

### **Extreme Value Analysis of HDD**

Four-week period values were analyzed by the extreme value frequency method (Lieblein procedure) to estimate the probability of occurrence of cold periods (5), (7). Because of the length of the four-week sample in relation to the annual period, the extreme value method has little to recommend it over other frequency distributions, such as for example, the log normal, which could have been used. Frequencies were expressed as a "return period." Used in this manner, return period signifies the number of years within which a given number of HDD will be equaled or exceeded once on the average. These frequencies differ from those determined by the normal distribution, as explained in the previous section, although the differences are not large. The reason for this is that the coldest period (highest HDD) did not occur in the same climatological period each year. In the extreme value analysis, the highest four-week HDD for each year was selected and used in the frequency determination. Results of this phase of the study are shown in Table 4. HDD for selected return periods are indicated, as is the distribution by periods of the annual highest four-week HDD. For example, in Rumford, Maine, it can be expected to have a four-week HDD equaling or exceeding 1,547 one year out of ten. Sixty per cent of the time, the greatest accumulation of HDD occurred during Period 12 at this station.

### **HDD by Calendar Months**

Tabulation and summarization of HDD data by climatological four-week periods was necessary because of machine routines for processing the data. Because the Weather Bureau has reported HDD by calendar months, it was believed to be desirable to work out a method of converting the NE-35 data. The procedure employed involved the construction of a family of curves, secured by plotting accumulated values of HDD against a time scale measured in units of the four-week climatological period. Smooth curves were drawn through the plotted points. These assumed an "S" shape when the beginning and ending time periods were four-week Periods 6 and 5, respectively. Calendar months were fitted to the four-week period scale. The percentage of the total degree days accumulated to the end of each month could be estimated from the "S" curves. Percentage distribution by months derived from

these relationships is depicted in Table 5. While no great precision can be claimed for this method, it is presented as a practical means of converting periods of the climatological year to calendar months.

It is interesting, in connection with this procedure, to see if stations having approximately the same annual mean HDD have about the same monthly distribution. More specifically, does Dover, Del., (annual mean of 4,369 HDD), located near the coast, have the same time distribution of HDD as does Point Pleasant, W. Va., (annual mean of 4,356 HDD) located on the Ohio River some 400 miles inland? A cursory examination of a number of stations in this category indicated the time distributions to be similar. This is a question which might well be given a more careful examination.

### Equation for Estimating HDD

Map 2 shows that the network of 156 weather stations used in the present study leaves many areas where the isolines are drawn by interpolating between widely spaced stations. These interpolations were modified in some cases by the known features of the terrain. This illustrates the need for a more accurate estimate of the mean annual HDD for a locality that is far removed from a network station. Consideration of this problem led to an attempt to develop a method of estimating mean annual HDD for any station on the basis of parameters which have been determined, and data for which are readily available. A procedure for estimating monthly degree-day totals from monthly mean temperatures has been developed by Thom and adopted by the Weather Bureau (16). While this method gives satisfactory results, it is somewhat time consuming and requires, in addition to monthly mean temperatures, the standard deviation of the monthly mean temperature for the location in question.

In search of a method for estimating HDD, the development of a multiple regression equation was explored. A computer program was available for the study. A variety of parameters, (including station elevation, latitude, longitude, January mean temperature, frost-free days, annual mean temperature, etc.) were tried, and the significance of the terms examined by an appropriate statistical test. This led to the following equation, which will estimate average annual HDD with an error no greater than 3 per cent in most cases.

$$X_1 = 6625 - 186.6 X_2 + .2X_3 + 209.9X_4$$

Where:

$X_1$  = mean annual HDD for the station

$X_2$  = mean annual temperature in ° F

$X_3$  = elevation above sea level in feet

$X_4$  = latitude in degrees, with fractions expressed as decimals.

Figure 3 is a nomogram from which an approximate solution to the equation can easily be determined. A more accurate solution can, of course, be obtained by substituting the appropriate values in the equation. The equation has not been tested for stations outside of the Northeastern region.

### APPLICATION OF HDD DATA

A more complete description and illustration of the uses of HDD in estimating energy requirements for space heating may be found in publications of ASHRAE, TVA, NEMA, and others (1), (12), (9), (3). A few brief examples are presented to give some idea of possible uses for the data.

The fuel required for heating a structure may be calculated from the following equation as given by ASHRAE (1).

$$F = \frac{XN}{eC} \quad [II]$$

Where  $F$  = quantity of fuel or energy (in same units as  $C$ , below)

$X$  = average heat requirements (Btu/hr) for the period under consideration

$N$  = number of heating hours in the estimate period

$e$  = efficiency of utilization of fuel over the period, expressed as a decimal

$C$  = heating value of one unit of fuel (or energy)

The value of  $X$  is usually computed by

$$X = \frac{H(t - t_o)}{t_i - t_d} \quad [II]$$

Where  $H$  = calculated heat loss, (Btu/hr), based on  $t_i$  and  $t_d$  and including infiltration loss

$t$  = average inside temperature maintained, ° F

$t_i$  = inside design temperature, usually 70° F

$t_o$  = average outside temperature for estimate period

$t_d$  = outdoor design temperature (consult references (1), (3), and (9) for design values)

These relationships can then be expressed as

$$F = \frac{H(t - t_0)N}{eC(t_i - t_d)} \quad [III]$$

or

$$E = \frac{H(t - t_0)N}{t_i - t_d} \quad [IV]$$

where  $E$  = energy requirement, (Btu)

This form IV of the equation will be used as it is more convenient for the present purposes and can easily be converted to fuel requirements by taking into account  $e$  and  $C$  as defined above.

Thom, (13) and (14), states that the inside temperature product  $(t - t_0) N$  is often assumed to be a function of the normal season HDD. This relationship may be expressed as

$$K\bar{d} = (t - t_0)N \quad [V]$$

where  $\bar{d}$  = normal heating degree days

Thom's derivation of the constant,  $K$ , produces a value of approximately 30 for mean HDD in the range of 4,000 to 10,000 annually, which includes the Northeastern states.

The ASHRAE Guide (1) notes that  $X$ , the average energy requirement, is often overestimated by the use of Equation II because  $H$  is the calculated maximum heat loss. There are usually sources of heat, not taken into account in calculating the maximum heat demand, which will tend to decrease the overall energy requirements. Again according to ASHRAE, the most important sources are solar radiation, people, lights, and equipment.

Some allowance for this may be made by using  $t$  as  $65^\circ$  rather than  $70^\circ$  F, as is often done. If  $t = 65^\circ$  F, then the expression  $\frac{(t - t_0)N}{24}$

is identical to degree-days for the period and

$$24\bar{d} = (t - t_0)N \quad [VI]$$

For electrically heated houses, the Tennessee Valley Authority (12) has developed the following formula for estimating seasonal energy requirements:

$$KWH = \frac{HL \times DD \times 20}{TD} \quad [VII]$$

Where  $KWH$  = the seasonal energy heat loss of building in kilowatt hours

$HL$  = heat loss of building in kilowatts per hour

$DD$  = normal annual degree-days for the locality

$TD$  = difference ( $^{\circ}$ F) between inside and outside design temperatures, or  $(t_i - t_d)$ , in symbolism employed above

This formula is primarily applicable to residential space heating, according to TVA, and is presumably based on data collected in the electric service area of this agency.

Considering Equations V, VI, and VII, it can be seen that Equation IV can be written in the form:

$$E = \frac{HK\bar{d}}{t_i - t_d} \quad [VIII]$$

It is evident from the above formulas, selected as representative of those in common use, that a fairly wide range of values has been assigned to the constant  $K$ . The suggestion has been made that the constant depends upon such variables as: geographical location, orientation and design of the particular house, living habits of the occupants, and type of heating equipment used. Obviously, the selection of  $K$  must necessarily be based on judgment and experience. Studies to develop a more precise and objective method for determining this term are needed.

The Federal Housing Administration (3) has developed a formula which affords a short-cut method of determining  $H$ , heat loss. The following form of FHA's Heat Loss Check Formula is limited to one, one-and-one-half-, and two-story detached dwellings that are substantially rectangular in plan, have an inside floor area (exclusive of basement and garage) not in excess of 1,500 square feet, and a total window and door area of between 20 and 28 per cent of the inside floor area.

$$H = A (G + U_c + U_w + U_f) (t_i - t_d) \quad [IX]$$

or

$$H = AU(t_i - t_d) \quad [X]$$

Where  $H$  = heat loss (Btu/hr), from one-story building

$G$  = glass and infiltration factor for doors and windows

$U_c$  = heat transmission coefficient for ceiling (Use .5  $U_c$  for 1 1/2 and 2-story dwellings)

$U_w$  = heat transmission for exterior walls (Use 1.2  $U_w$  for 1 1/2 and 2-story dwellings)

$U_f$  = heat transmission coefficient for floor (Use .5  $U_f$  for 1 1/2 and 2-story dwellings)

$A$  = inside floor area in square feet. Sum of floor areas measured to inside face of enclosing exterior walls on each principal floor level, and floor area measured to inside face of enclosing walls and partitions of all finished rooms and spaces in the attic. Basement and garage areas are not to be included.

$U$  = the combined transmission coefficient for the above condition.

Combining Equations VIII and X, we have

$$E = A U K \bar{d} \quad [XI]$$

Procedures for computing  $H$  or  $HL$  (conversion can be made on the basis that 1 KWH = 3,413 BTU) in addition to the short-cut method are explained in detail in references (1), (3), (9), and (12). These procedures will not be reviewed here.

## SAMPLE CALCULATIONS

Some examples of how HDD data may be applied to the solution of practical problems follow.

### Example 1

A dwelling at Frostburg, Md., is calculated to have a heat loss,  $H$ , of 45,000 BTU per hour. This includes losses by transmission and infiltration. The normal annual HDD at Frostburg is 5,685, the inside minus the outside design temperature is  $70^\circ$ , and the floor area is 1,200 square feet. What is the estimated normal annual energy requirement for heating?

Use Equation VIII and assume  $K = 24$

$$E = \frac{HK\bar{d}}{t_i - t_d}$$

$$E = \frac{45,000 \times 24 \times 5,685}{70}$$

$E = 87.7$  million BTU per year

### Example 2

A house has a floor area of 1,500 square feet. The  $U$  term for the FHA short-cut method has been calculated as .62. Estimate the average seasonal energy requirements, if the location has a normal annual HDD of 5,200.

Use Equation XI,

$$E = A U K \bar{d}$$

If  $K$  is 30, then

$$E = 1,500 \times .62 \times 30 \times 5,200$$

$$E = 145.1$$
 million BTU per year

### Example 3

With the conditions and location described in Example No. 1,

(a) What will be the energy requirements that will not be exceeded more than one-fourth of the years on the average?

On Figure 1, enter with the mean annual HDD of 5,685 on the ordinate. Projecting to the 25 per cent frequency line and then to the abscissa indicates a value of approximately 6,000 HDD. This means that, on the average, annual HDD at Frostburg will not exceed this figure 3 years out of 4, or conversely, the figure will be exceeded 1 year out of four. Then

$$E = 87.7 \times \frac{6000}{5685}$$

$E = 92.6$  million BTU per year

(b) What will be the energy requirements for the four-week period during which the HDD will be equaled or exceeded only once in 10 years?

The solution may be determined by referring to Table 4. The extreme value frequency gives about 1,200 HDD for Frostburg for a return period of 10 years. This is to say that once in 10 years a four-week period HDD equaling or exceeding this magnitude will be expected. The analysis does not show in what period this will occur. However, the coldest weather as measured by the highest HDD has been experienced in Period 11 in 40 per cent of the years of record. From this,

$$E = \frac{45,000 \times 24 \times 1,200}{70}$$

$E = 18.5$  million BTU for the period

It should be noted that the relationship of HDD to energy requirements is usually more reliable for longer periods than for shorter ones. The four-week period calculation may therefore provide estimates that are not as reliable as can be expected for several periods combined, or for an entire heating season.

### Example 4

The frequency charts, Figures 1 and 2, are based upon the premise that the data conform to the normal distribution. A further assumption involved is that the annual means have homogeneity of variance. This provided the basis for calculating the position of the frequency lines on Figure 1. Application of this reasoning to the construction of Figure 2 has been explained briefly in a previous section. Some individual stations do not fit, as well as one might hope, the idealized relationship. The following procedure may be employed to utilize the data for

any station and period in working out frequency relationships, as an alternate to use of the charts. (Application to the warmer four-week periods should be with caution, because the HDD may not be normally distributed, and large biases in probabilities result.)

$$\text{HDD} = \bar{d} \pm sf \quad [\text{XII}]$$

Using  $\text{HDD}$  = heating degree-days for any return period or frequency (Table 6)

$\bar{d}$  = average or mean HDD for the period

$s$  = sample standard deviation. This was derived from appropriate pooled variances for constructing Figures 1 and 2. The individual station values of standard deviation, reported in Tables 2 or 3, may be used to work out the frequency relationships.

$f$  = factor for area under the normal curve

Equation XII may be used in conjunction with Table 6 in the following manner:

What is the four-week HDD that will be equalled or exceeded one year in 25 years on the average for climatological Period 1 at Williamson, W. Va.?

From Table 3, the mean is 545 HDD, the standard deviation is 134 HDD, and from Table 6, the area factor for a return period of 25 years is 1.75. Then

$$\text{HDD} = 545 + 134 (1.75) = 780$$

On the average, the Period 1 HDD can be expected to equal or exceed this figure only once in 25 years.

Also,

$$\text{HDD} = 545 - 134 (1.75) = 310$$

In this case, 310 HDD is a figure for which the expectancy is that a lower value will occur only once in 25 years, or that HDD will equal or exceed this 96 per cent of the time.

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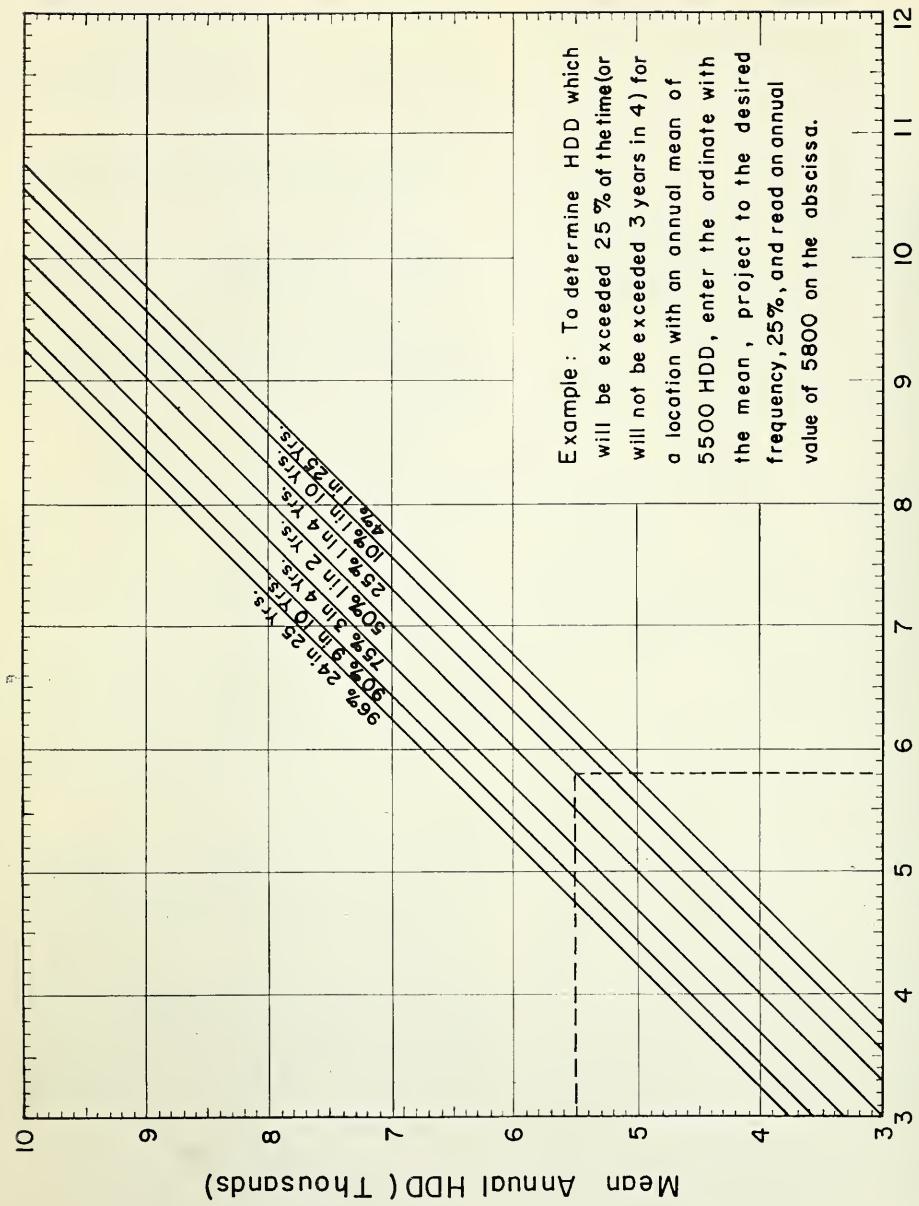
## Regional Publications

Three additional publications in *The Climate of the Northeast* series have been published by personnel of the NE-35 Committee. Their titles and authors are listed below.

*Spring and Fall Low-Temperature Probabilities*. New Jersey Agricultural Experiment Station Bulletin 801, June, 1961. The authors of this publication are A. V. Havens and J. K. McGuire.

*Probability of Selected Weekly Precipitation Amounts in the Northeast Region of the United States*. Cornell University Agricultural Experiment Station Agronomy Mimeo No. 614, November, 1961. The authors of this publication are B. E. Dethier and J. K. McGuire.

*Growing Degree-Days*. New York State Agricultural Experiment Station Bulletin 801, 1963. The authors of this publication are B. E. Dethier and M. T. Vittum.



**Example :** To determine HDD which will be exceeded 25 % of the time (or will not be exceeded 3 years in 4) for a location with an annual mean of 5500 HDD, enter the ordinate with the mean, project to the desired frequency, 25%, and read an annual value of 5800 on the abscissa.

FIGURE 1. Frequency Curves for Mean Annual HDD.

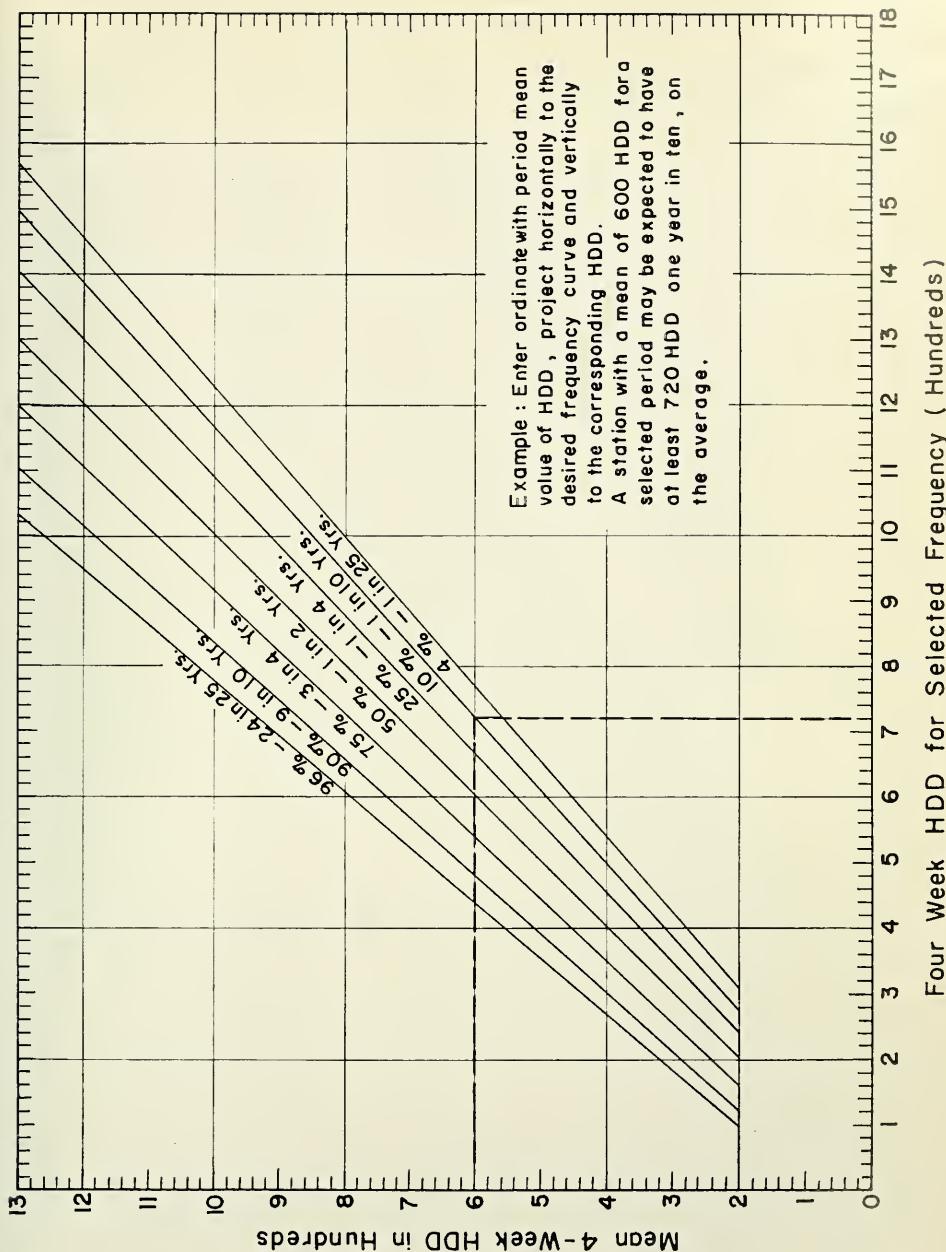
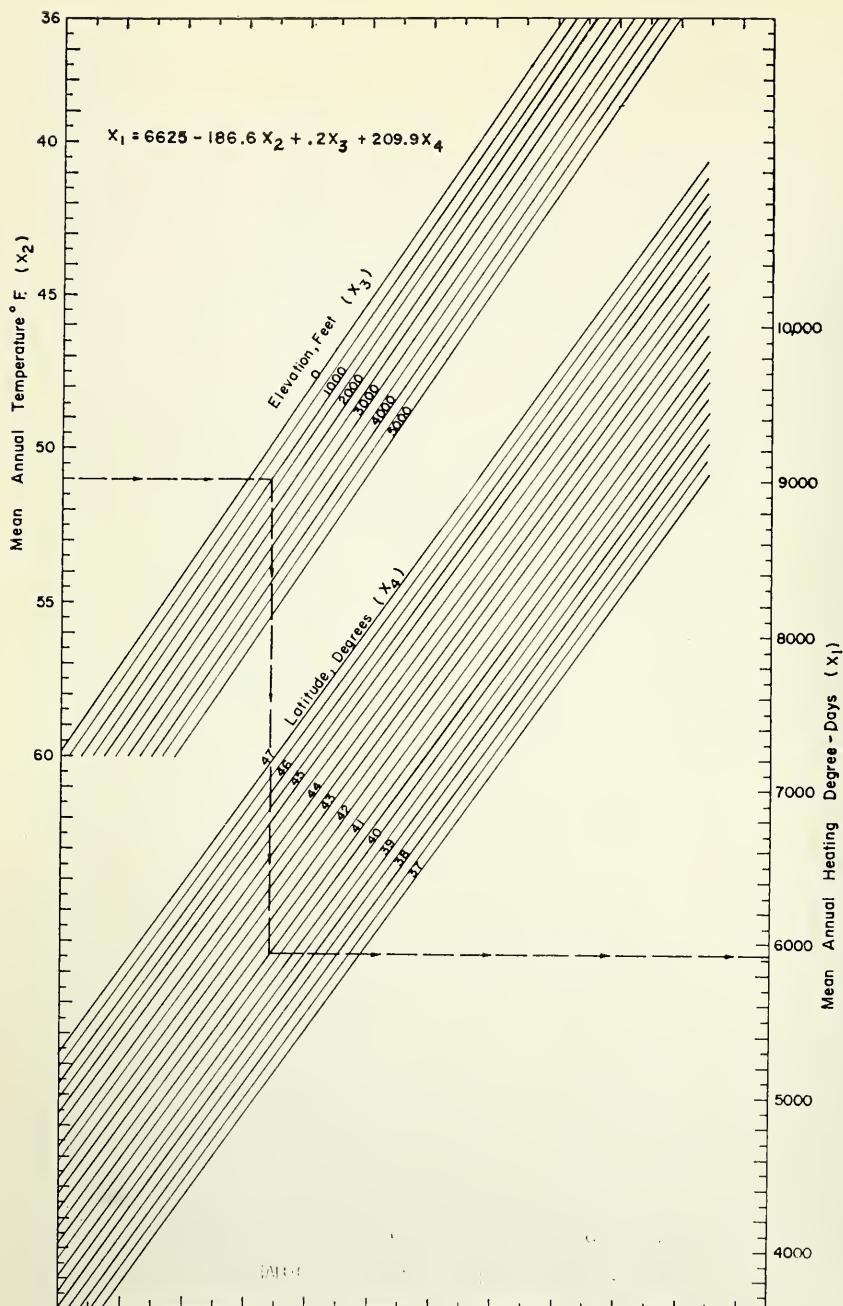


FIGURE 2. Frequency Curves for Four-Week Period Mean HDD.



**FIGURE 3.** Nomogram for Solving Multiple Regression Equation.

**Table 1. The Climatological Year.**

<b>Week Number</b>	<b>Beginning Date</b>	<b>Ending Date</b>	<b>4-Week Period Number</b>	<b>Beginning Date</b>	<b>Ending Date</b>
01	Mar 1	Mar 7	01	Mar 1	Mar 28
02	Mar 8	Mar 14			
03	Mar 15	Mar 21	02	Mar 29	Apr 25
04	Mar 22	Mar 28			
05	Mar 29	Apr 4	03	Apr 26	May 23
06	Apr 5	Apr 11			
07	Apr 12	Apr 18	04	May 24	Jun 20
08	Apr 19	Apr 25			
09	Apr 26	May 2	05	Jun 21	Jul 18
10	May 3	May 9			
11	May 10	May 16	06	Jul 19	Aug 15
12	May 17	May 23			
13	May 24	May 30	07	Aug 16	Sep 12
14	May 31	Jun 6			
15	Jun 7	Jun 13	08	Sep 13	Oct 10
16	Jun 14	Jun 20			
17	Jun 21	Jun 27	09	Oct 11	Nov 7
18	Jun 28	Jul 4			
19	Jul 5	Jul 11	10	Nov 8	Dec 5
20	Jul 12	Jul 18			
21	Jul 19	Jul 25	11	Dec 6	Jan 2
22	Jul 26	Aug 1			
23	Aug 2	Aug 8	12	Jan 3	Jan 30
24	Aug 9	Aug 15			
25	Aug 16	Aug 22	13	Jan 31	Feb 27
26	Aug 23	Aug 29			
27	Aug 30	Sep 5	14	Feb 28	Feb 29
28	Sep 6	Sep 12			
29	Sep 13	Sep 19	08	Sep 13	Oct 10
30	Sep 20	Sep 26			
31	Sep 27	Oct 3	09	Oct 11	Nov 7
32	Oct 4	Oct 10			
33	Oct 11	Oct 17	10	Nov 8	Dec 5
34	Oct 18	Oct 24			
35	Oct 25	Oct 31	11	Dec 6	Jan 2
36	Nov 1	Nov 7			
37	Nov 8	Nov 14	12	Jan 3	Jan 30
38	Nov 15	Nov 21			
39	Nov 22	Nov 28	13	Jan 31	Feb 27
40	Nov 29	Dec 5			
41	Dec 6	Dec 12	14	Feb 28	Feb 29
42	Dec 13	Dec 19			
43	Dec 20	Dec 26	12		
44	Dec 27	Jan 2			
45	Jan 3	Jan 9	13		
46	Jan 10	Jan 16			
47	Jan 17	Jan 23	14		
48	Jan 24	Jan 30			
49	Jan 31	Feb 6	14		
50	Feb 7	Feb 13			
51	Feb 14	Feb 20	14		
52	Feb 21	Feb 27			
53	Feb 28	Feb 29			

**Table 2**  
**Station list with geographical data, annual mean HDD, and standard deviation.**

Name	Station No.	County	Elev. (ft.)	Lat. °	Long. °	Annual No. Yrs. Analyzed	Mean, HDD	Standard Deviation HDD
<b>CONNECTICUT</b>								
Cream Hill	1715	Litchfield	1300	41	52	73	20	30
Hartford	3451	Hartford	15	41	72	39	30	5973
Norwalk	5892	Tolland	120	41	73	27	30	5936
Storrs	8138	New Haven	600	41	72	15	30	6661
Waterbury	8911		288	41	73	02	17	5648
<b>DELAWARE</b>								
Bridgeville	1330	Sussex	50	38	45	75	37	30
Dover	2730	Kent	34	39	10	75	32	4412
Milford	5915	Sussex	10	38	55	75	26	386
							4314	402
								377
<b>MAINE</b>								
Caribou	1175	Aroostook	624	46	52	68	01	17
Eastport	2426	Washington	100	44	54	66	59	9744
Farmington	2765	Franklin	390	44	40	70	09	371
Houlton	2878	Aroostook	530	47	15	68	36	8099
Houlton	3897	Aroostook	410	46	08	67	10	452
Lewiston	4566	Androscoggin	182	44	06	70	14	9159
Old Town	6420	Penobscot	108	44	56	68	39	338
Portland	6905	Cumberland	61	39	70	19	30	8757
Presque Isle	6931	Aroostook	606	46	39	68	00	347
Rockland	7250	Knox	40	44	06	69	07	7499
Rumford	7330	Oxford	505	44	33	70	33	422
							30	401
							7876	452
								763
<b>MARYLAND</b>								
Chesapeake	1790	Washington	560	39	38	77	41	5247
Crisfield	2205	Somerset	5	37	59	75	51	429
Easton	2695	Talbot	28	38	46	76	04	462
Elkton	2860	Cecil	28	39	36	75	04	404
Frederick	3348	Frederick	380	39	25	77	25	4329
Frostburg	3410	Allegany	2035	39	39	78	56	365
Keedysville	4780	Washington	420	39	29	77	56	4829
Oakland	6620	Garrett	2420	39	24	79	24	389
Owings Ferry Landing	6770	Calvert	120	38	42	76	41	5685
Princess Anne	7330	Somerset	17	38	12	75	26	382
Salisbury	8000	Wicomico	10	38	22	75	36	402
Westminster	9435	Carroll	770	39	35	77	00	4200
Woodstock	9750	Baltimore	415	39	20	76	53	385
								315
								431
								371
								389



**Table 2 (continued)**  
**Station list with geographical data, annual mean HDD, and standard deviation.**

Name	Station No.	County	Elev. (ft.)	Lat. °	Long. °	Annual No. Yrs. Analyzed	Mean, HDD	Standard Deviation HDD
<b>NEW YORK (Continued)</b>								
Lowville	4912	Lewis	860	43	48	75	29	30
Morrisville	5512	Madison	1325	42	54	75	39	30
New York Central Park	5801	New York	132	40	47	75	58	30
Norwich	6085	Chenango	1070	42	33	75	32	30
Ogdensburg	6164	St. Lawrence	258	44	44	75	27	30
Oswego	6314	Oswego	292	43	27	76	31	30
Port Jervis	6774	Dutchess	470	41	23	74	41	30
Poughkeepsie	6817	Monroe	103	41	41	73	56	28
Rochester	7167	Delaware	543	43	07	77	40	30
Roxbury	7317	Herkimer	1494	42	17	74	34	29
Salisbury	7413	Sullivan	1300	43	09	74	51	30
Seatauket	7633	Surfside	40	57	73	06	24	24
South Wales	8058	Erie	1073	42	43	78	36	24
Syracuse	8383	Onondaga	419	43	34	76	07	30
Walden	8902	Orange	400	41	34	74	10	30
Wanakena	8944	St. Lawrence	1510	44	09	74	54	30
Watertown	9000	Jefferson	497	43	58	75	52	30
Whitehall	9389	Washington	119	43	33	73	24	13
<b>PENNSYLVANIA</b>								
Altoona	0134	Blair	1500	40	30	78	29	28
Bethlehem	0634	Northampton	436	43	36	75	23	27
Brookville	1002	Jefferson	1417	41	09	79	06	25
Butler	1130	Butler	1100	40	52	79	54	26
Carlisle	1234	Cumberland	460	40	12	77	11	30
Claysville	1512	Washington	1150	40	07	80	25	30
Corry	2190	Erie	1427	41	55	79	38	25
Donora	2466	Washington	814	40	11	79	51	29
Ebensburg	2633	Cameron	2090	40	29	78	43	25
F Emporium	3028	Venango	1160	41	31	78	13	24
Franklin	3056	Luzerne	987	41	23	79	49	30
Freeland	3200	Bucks	1900	41	01	75	54	25
George School	3218	Adams	135	40	13	74	56	29
Gettysburg	3526	Mercer	540	39	50	77	14	30
Greenville	4159	Huntingdon	1026	41	24	80	23	26
Huntingdon	4385	Cambria	706	40	30	78	01	29
Johnstown	4758	Lancaster	1214	40	20	78	55	26
Lancaster	4873	Tioga	255	40	03	81	33	29
Lawrenceville			1000	41	59	77	07	28



**Table 3**  
**Four-week period means of HDD and standard deviations.\***

Station	Climatological Period Number											
	1				2				3			
	M	S	M	S	M	S	M	S	M	S	M	S
<b>CONNECTICUT</b>												
Cream Hill	888	187	607	100	309	75	120	52	23	23	11	10
Hartford	787	107	517	80	239	58	76	37	8	13	3	3
Newark	787	99	523	77	246	58	72	49	9	13	13	13
Storrs	868	108	539	82	318	72	121	49	23	18	14	13
Watervliet	752	115	473	89	212	59	58	31	8	14	2	3
<b>DELAWARE</b>												
Bridgeville	587	108	365	66	143	43	32	21	2	4	0	0
Dover	588	111	336	68	130	42	27	21	1	3	0	0
Milford	585	91	339	64	132	38	27	21	0	0	5	5
<b>MAINE</b>												
Caribou	1205	119	853	109	504	71	248	57	89	35	64	29
Eastport	977	87	737	68	519	39	320	41	157	39	98	27
Farmington	1004	105	682	90	362	69	130	50	31	23	19	15
Fort Kent	1133	100	783	107	476	65	204	69	50	25	47	24
Houlton	1085	117	758	89	432	66	178	54	50	30	21	12
Lewiston	969	101	672	82	376	65	134	46	25	18	11	11
Old Town	941	89	652	72	333	57	169	49	39	24	12	12
Portland	1154	115	804	93	469	72	210	67	43	36	50	23
Presque Isle	932	95	661	81	426	64	200	43	34	27	23	18
Rockland	1009	115	695	104	386	79	149	52	93	41	30	33
Rumford												
<b>MARYLAND</b>												
Chesapeake	676	123	430	84	182	58	50	33	5	8	2	3
Crisfield	504	141	217	74	76	37	111	13	0	0	0	0
Easton	576	106	345	74	127	44	26	21	1	3	0	0
Elkton	634	104	388	68	146	47	30	20	2	4	0	0
Frederick	613	110	388	69	131	47	27	19	1	3	0	0
Frostburg	740	128	666	89	213	66	75	41	13	12	7	8
Kedzysville	626	118	381	75	142	48	66	31	23	12	4	0
Oakland Ferry Landing	759	154	533	101	219	72	117	54	36	26	20	18
Princess Anne	565	113	338	68	121	43	26	21	42	34	2	4
Salisbury	572	93	338	68	132	42	34	23	1	1	1	1
Westminster	539	118	320	71	116	36	22	18	1	3	0	0
Woodstock	638	109	382	71	152	51	40	27	3	5	1	2

\* M = mean; S = standard deviation

MASSACHUSETTS															
Adams	626	938	130	121	41	29	24	19	15	79	37	273	54		
Amherst	626	938	130	43	15	18	9	8	46	21	201	45	214	45	
Blue Hill	626	938	130	65	120	38	24	22	9	30	19	161	45	420	79
East Wareham	626	822	844	76	332	49	119	36	22	18	5	8	30	19	
Hanover	626	803	803	46	122	21	18	5	8	30	19	161	45	365	73
Lawrence	626	847	104	563	92	34	13	15	4	5	24	16	149	44	
Springfield	626	804	110	476	89	203	53	55	10	2	42	22	192	44	
Weston	626	804	110	533	91	269	65	50	32	15	5	10	24	366	81
Worcester	626	863	110	587	90	306	67	115	48	21	19	13	11	59	27
NEW HAMPSHIRE															
Berlin	1025	121	751	100	441	72	196	55	73	35	55	27	143	45	
Durham	1025	101	601	83	340	68	126	45	25	19	14	11	63	31	
Hanover	1025	120	662	95	354	71	132	45	32	26	21	16	83	33	
Keene	909	116	612	94	326	69	122	43	32	30	19	15	79	39	
NEW JERSEY															
Belvidere	724	111	449	87	176	53	50	33	4	6	1	3	18	16	
Boonton	786	99	508	89	247	61	86	45	12	14	4	5	32	20	
Charlotteburg	793	119	525	82	250	64	97	44	19	16	11	49	29	153	
Flemington	692	108	79	176	52	48	31	4	6	1	3	13	122	43	
Indian Mills	674	111	431	71	181	50	55	33	5	6	1	3	20	133	
Layton	821	111	544	88	265	57	94	50	15	17	1	3	51	29	
Long Branch	707	99	444	80	229	60	64	32	3	5	7	1	13	11	
Moorestown	678	108	434	74	185	52	51	30	3	5	1	2	127	46	
New Brunswick	698	108	447	80	184	48	52	51	3	4	6	1	12	124	
Pleasantville	703	100	468	72	222	50	66	33	9	9	2	2	18	11	
NEW YORK															
Albany	835	121	532	91	234	60	62	36	7	11	2	3	28	17	
Alfred	923	133	664	102	357	85	160	47	51	32	29	25	102	45	
Angelica	917	131	626	91	329	71	111	50	15	18	6	7	38	20	
Auburn	858	131	570	96	277	68	97	48	17	19	10	11	20	122	
Bridgehampton	772	85	545	66	311	54	104	35	14	15	2	1	22	18	
Buffalo	916	130	645	110	358	81	127	54	21	21	7	8	45	28	
Canton	1037	147	677	107	354	78	127	55	30	23	20	15	89	36	
Carmel	846	109	557	93	271	59	96	42	14	14	6	40	20	189	
Cooperstown	960	153	642	112	346	77	144	62	42	35	29	26	96	43	
Dannemora	1060	144	719	118	373	86	142	62	40	33	24	18	29	59	
Delhi	937	137	644	98	342	72	144	61	40	28	21	89	39	268	
Elmira	847	122	555	97	263	67	88	41	100	49	9	9	47	29	
Genesee	866	134	580	110	300	78	100	49	14	14	5	6	34	19	
Hamilton	916	129	573	95	282	72	90	48	12	15	5	8	41	23	
Ithaca	896	127	605	91	315	74	104	48	16	16	9	58	30	220	
Jamesstown	855	149	567	108	278	73	103	49	25	19	11	14	66	25	
Little Falls	929	137	590	110	321	77	120	56	25	21	15	14	52	23	
Lockport	914	129	627	97	334	79	123	58	21	19	10	10	52	25	

**Table 3 (continued)**  
**Four-week period means of HDD and standard deviations.\***

Station	Climatological Period Number																																						
	1			2			3			4			5			6			7			8			9			10			11			12			13		
	M	S	M	M	S	M	M	S	M	M	S	M	M	S	M	M	S	M	M	S	M	M	S	M	M	S	M	M	S	M	M	S							
<b>NEW YORK (Continued)</b>																																							
Lowville	1036	142	687	108	356	76	136	46	34	29	22	17	90	38	293	61	559	94	902	118	121	121	1301	168	1286	122													
N. Y. Central Park	1005	130	688	97	387	77	174	66	56	34	37	32	109	43	312	68	568	89	874	101	1164	129	1220	161	1234	121													
Norwich	692	106	1437	81	173	52	41	25	3	5	0	0	22	93	40	286	59	539	90	842	108	1125	117	1191	151	1191	125												
Ogdensburg	954	135	656	99	350	70	113	59	19	18	10	11	62	33	244	61	509	75	856	108	1204	133	1305	171	1276	124													
Oswego	1015	130	651	106	337	78	113	59	19	18	10	11	62	33	244	61	509	75	856	108	1037	110	1110	137	1116	125													
Port Jervis	805	111	518	91	238	68	81	44	12	16	6	7	36	25	184	52	427	90	733	83	1001	99	1046	135	1025	114													
Poughkeepsie	781	112	490	99	212	64	54	28	4	8	1	2	23	17	163	47	393	78	712	92	984	117	1044	154	1029	121													
Rochester	895	132	705	102	304	75	102	56	13	13	8	8	48	206	55	452	87	758	106	1023	109	1090	146	1101	116														
Roxbury	995	133	550	103	350	85	153	66	45	31	28	21	94	40	281	55	594	88	835	92	1107	118	1148	155	1142	125													
Watertown	1056	139	733	112	399	94	189	68	57	36	40	30	10	10	110	37	311	69	583	79	833	95	927	105	1231	110	1256	148											
Staunton	730	94	484	76	229	94	66	9	35	27	20	16	81	38	259	61	501	95	753	104	1039	121	1107	121	1150	124													
South Wales	950	138	640	103	353	78	133	49	31	27	20	16	81	38	259	61	501	95	753	104	1039	121	1107	121	1150	124													
Syracuse	888	135	588	100	293	67	98	44	15	15	7	48	25	212	56	451	81	753	99	997	115	1052	155	1052	131	1342	165												
Walden	821	114	539	116	265	77	95	52	12	12	8	8	48	220	56	451	77	738	99	997	115	1052	155	1052	131	1342	165												
Wanaakena	1097	139	539	116	418	81	190	59	76	43	58	33	144	52	353	63	621	95	956	123	1275	130	1107	130	1013	135	1334	155											
Watertown	963	138	631	102	328	75	116	55	21	19	11	6	61	26	239	59	493	83	820	113	1150	132	1229	178	1222	127													
Whitehall	891	149	532	109	266	60	73	38	5	5	6	6	33	21	206	36	445	80	800	90	1133	130	1209	156	1180	169													
<b>PENNSYLVANIA</b>																																							
Altoona	796	137	516	90	241	70	92	45	18	16	10	11	49	28	198	52	436	86	756	96	991	111	1001	145	1000	131													
Bethlehem	700	118	443	78	174	51	46	33	4	6	1	2	14	12	119	43	346	78	641	85	894	98	895	125	925	112													
Brookville	895	122	608	106	326	85	135	68	67	51	26	22	91	56	276	58	533	95	822	93	1045	118	1078	163	1082	151													
Butler	616	133	471	101	218	68	68	58	37	27	2	1	17	15	133	49	366	84	671	76	916	94	951	165	952	132													
Carlisle	720	139	463	93	218	72	71	36	14	14	8	11	39	27	228	59	481	83	727	88	930	118	1051	165	952	132													
Corry	880	154	579	111	320	70	122	53	30	25	19	17	62	35	228	59	481	83	727	88	930	118	1051	165	952	132													
Donora	877	136	387	87	157	57	41	30	3	5	1	2	13	11	113	46	327	83	727	88	930	118	1051	165	952	132													
Emporium	863	111	571	102	285	74	115	51	24	22	12	11	51	35	229	53	498	104	803	106	1054	99	1117	153	1092	118													
Franklin	892	144	601	104	285	74	109	56	25	20	11	11	51	35	229	53	498	104	803	106	1054	99	1117	153	1092	118													
Freeland	707	99	450	65	181	55	50	39	24	2	1	15	123	43	343	75	349	80	644	92	920	143	909	125															
George School	659	119	405	73	154	50	39	24	2	1	15	123	43	343	75	349	80	644	92	637	137	879	108	1033	167														
Gettysburg	784	138	518	93	256	74	93	52	13	9	13	11	42	25	193	59	445	82	743	96	994	106	1033	168	1066	138													
Greenville	747	113	480	80	210	57	68	36	11	6	31	20	156	55	398	99	687	93	938	112	954	165	952	123															
Huntingdon	740	137	466	89	198	64	64	58	31	10	18	3	5	30	26	156	55	398	99	687	93	938	112	954	165	952	123												
Johnstown	688	115	435	84	276	69	102	55	22	17	56	22	14	18	155	55	398	99	687	93	938	112	954	165	952	123													
Lancaster	859	131	575	91	276	69	102	55	22	17	56	22	14	18	155	55	398	99	687	93	938	112	954	165	952	123													
Lawrenceville																																							

\*M = mean; S = standard deviation



**Table 4**  
**Extreme value frequency analysis of heating degree-days.**

Station	HDD for Return Periods					% Years with Highest HDD by Clim. Period				
	2-yr.	5-yr.	10-yr.	20-yr.	50-yr.	Period 10	Period 11	Period 12	Period 13	Period 1
<b>CONNECTICUT</b>										
Cream Hill	1171	1286	1361	1424	1528	3	20	47	30	
Hartford	1076	1189	1263	1334	1426		20	50	27	
Norwalk	1052	1152	1219	1282	1365		23	43	33	
Storrs	1130	1239	1311	1381	1471		24	53	18	
Waterbury	1042	1135	1196	1225	1330		29			
<b>DELAWARE</b>										
Bridgeville	850	961	1034	1105	1196		33	34	30	3
Dover	853	965	1040	1112	1204		34	30	30	3
Milford	833	926	987	1046	1122		35	31	30	4
<b>MAINE</b>										
Caribou	1567	1658	1719	1777	1852		12	59	29	
Eastport	1230	1325	1388	1448	1526		7	56	30	
Farmington	1337	1445	1517	1583	1675		17	60	23	
Fort Kent	1510	1620	1693	1762	1853		10	50	40	
Houlton	1454	1554	1620	1683	1765		10	70	20	
Lewiston	1272	1372	1455	1525	1615		7	63	30	
Old Town	1278	1378	1463	1533	1625		10	60	30	
Portland	1202	1321	1389	1459	1573		10	57	37	3
Presque Isle	1500	1581	1635	1686	1752		10	56	33	
Rockland	1202	1294	1335	1414	1490		11	56	33	
Rumford	1295	1447	1547	1644	1769		10	60	23	7
<b>MARYLAND</b>										
Chews Cove	967	1078	1152	1224	1314		40	37	23	
Crisfield	764	846	900	952	1020		31	38	31	
Easton	844	949	1018	1084	1170		33	40	24	3
Elkton	923	1030	1101	1169	1257		36	39	25	3
Frederick	914	1032	1110	1185	1282		37	37	23	
Frostburg	1014	1124	1197	1267	1338		40	40	27	7
Keedysville	924	1032	1104	1172	1261		37	40	23	
Oakland	1064	1182	1261	1336	1433		40	26	27	7
Owings Ferry Landing	839	945	1014	1081	1167		33	38	26	3
Princess Anne	813	917	986	1052	1138		32	32	28	8
Salisbury	794	897	955	1030	1114		32	32	32	4
Westminster	936	1047	1120	1190	1280		37	34	26	3
Woodstock	928	1036	1108	1177	1267		37	34	37	



Table 4 (continued)  
Extreme value frequency analysis of heating degree-days.

Station	HDD for Return Periods					% Years with Highest HDD by Clim. Period				
	2-yr.	5-yr.	10-yr.	20-yr.	50-yr.	Period 10	Period 11	Period 12	Period 13	Period 1
<b>NEW YORK (Continued)</b>										
Lowville	1351	1488	1579	1666	1778	10	57	33		
Morrisville	1287	1418	1505	1588	1695	17	38	45		
N. Y. Central Park	943	1047	1117	1183	1269	20	50	30		
Norwich	1250	1368	1446	1521	1618	18	46	36		
Ogdensburg	1340	1469	1555	1638	1744	3	14	45		
Oswego	1160	1280	1359	1435	1533					
Port Jervis	1104	1208	1276	1342	1427	7	50	40		
Poughkeepsie	1098	1211	1287	1359	1452	23	47	30		
Rochester	1144	1266	1346	1424	1524	21	54	35		
Roxbury	1219	1335	1413	1487	1583	4	21	50		
Salsbury	1352	1479	1563	1643	1747	13	43	32		
Setauket	944	1043	1109	1172	1254	17	50	37		
South Wales	1209	1338	1423	1505	1611	25	42	33		
Syracuse	1167	1303	1394	1480	1593	17	43	37		
Walden	1113	1225	1300	1371	1464	20	50	37		
Wanaqua	1396	1536	1628	1717	1822	3	17	50		
Watertown	1281	1429	1527	1621	1743	15	54	30		
Whiterall	1260	1355	1418	1478	1556	15	46	31		
<b>PENNSYLVANIA</b>										
Altoona	1075	1184	1256	1325	1414	36	25	35		
Bethlehem	977	1081	1150	1216	1301	30	44	26		
Brookville	1147	1291	1386	1456	1596	36	36	28		
Butler	1033	1142	1214	1283	1372	38	35	23		
Carlisle	988	1100	1174	1245	1337	30	43	27		
Claysville	1011	1143	1231	1315	1423	47	24	26		
Corry	1138	1289	1388	1483	1607	24	36	36		
Donora	916	1037	1118	1195	1294	31	31	34		
Ebensburg	1124	1240	1316	1390	1485	28	36	32		
Emporium	1128	1265	1356	1444	1557	29	38	33		
Franklin	1104	1239	1328	1414	1524	23	30	44		
Freeland	1159	1266	1337	1405	1493	16	56	28		
George School	977	1081	1150	1217	1303	35	41	24		
Gettysburg	954	1061	1131	1199	1287	37	37	26		
Grenville	1096	1211	1288	1361	1456	23	50	19		
Huntingdon	1028	1144	1220	1294	1389	31	34	35		
Johnstown	1018	1114	1178	1239	1318	42	31	23		
Lancaster	996	1105	1177	1247	1336	35	41	24		
Lawrenceville	1147	1247	1314	1377	1460	25	39	36		



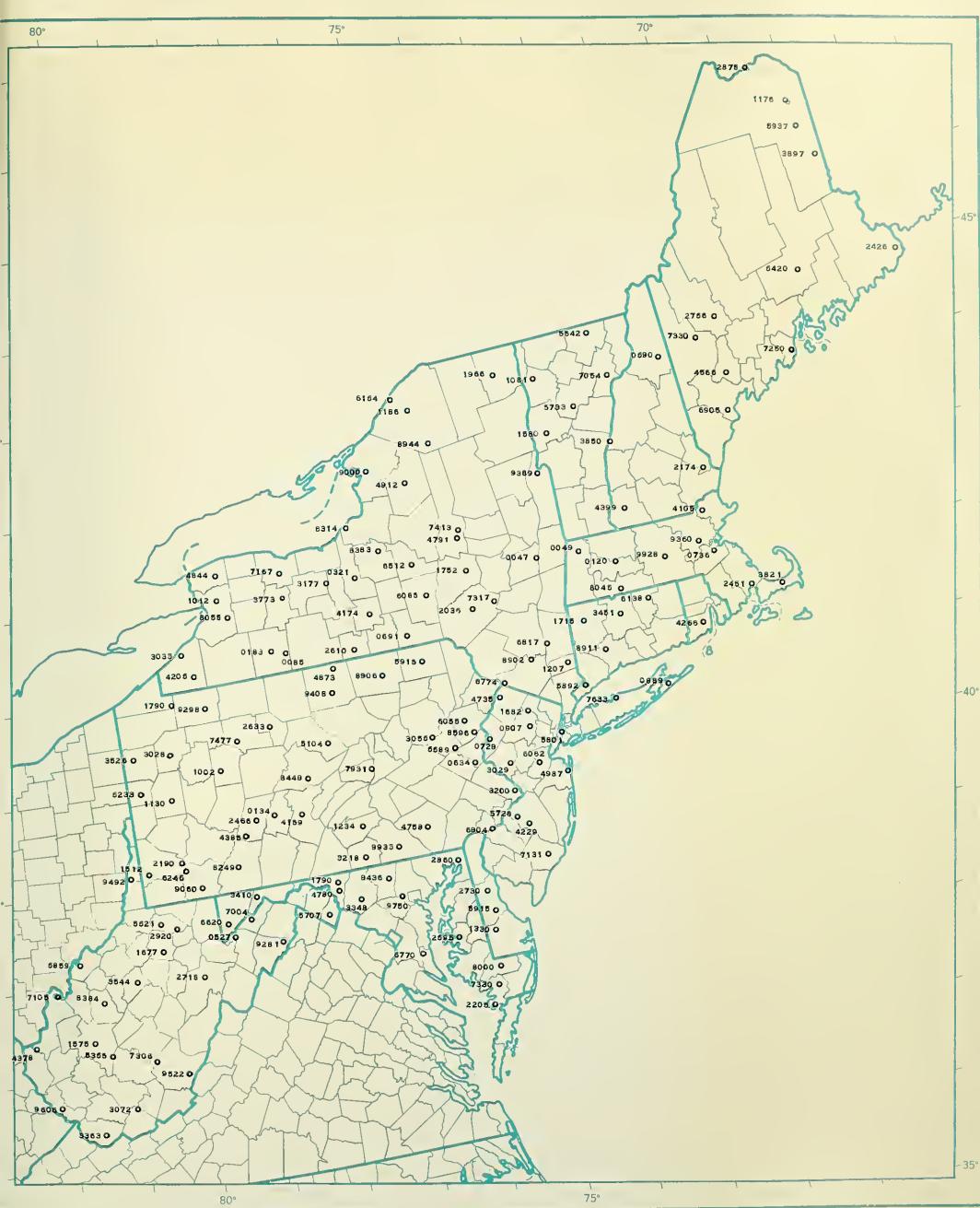
**Table 5. Per Cent of total HDD by months.**

Normal Annual Range of HDD	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
3000-3999	20.8	18.2	14.7	7.2	1.8	0.3	0.0	0.0	5.1	12.1	19.4	
4000-4999	20.1	17.5	14.4	8.0	2.4	0.3	0.0	0.0	1.0	5.9	12.0	18.4
5000-5999	19.3	17.0	14.2	8.6	3.2	0.4	0.0	0.0	1.6	6.3	11.7	17.7
6000-6999	18.6	16.6	14.1	9.0	4.0	0.6	0.0	0.0	2.2	6.5	11.4	17.0
7000-7999	18.0	16.2	13.8	9.3	4.6	1.0	0.3	0.4	2.5	6.6	11.1	16.2
8000-8999	17.7	15.6	13.4	9.5	5.2	1.6	0.4	0.7	2.8	6.7	10.9	15.5
9000-9999	17.6	15.3	12.9	9.6	5.6	2.0	0.4	0.9	3.0	6.8	10.6	15.3

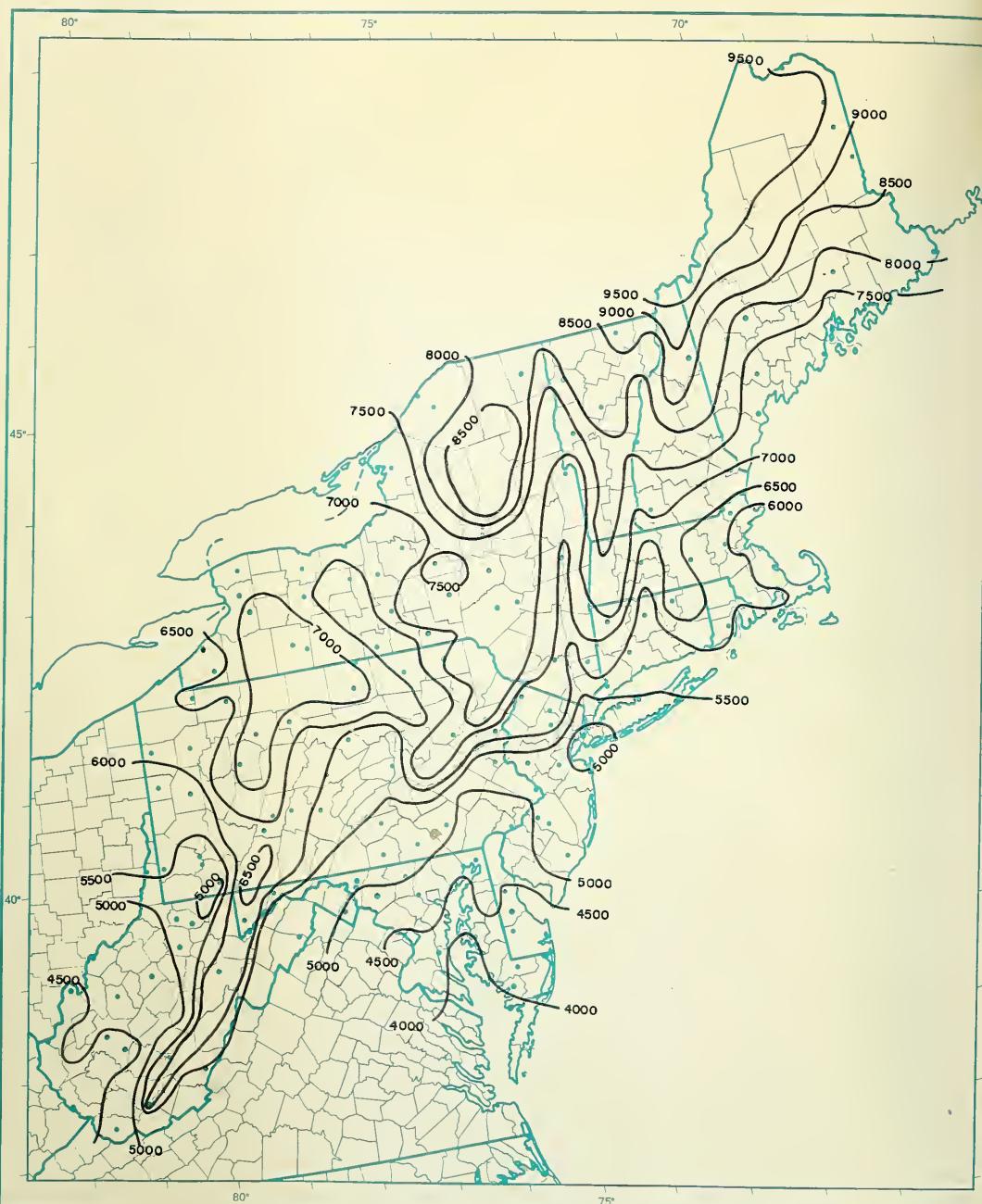
**Table 6. Frequency Relationships.**

Return Period Years	% Frequency	f*
2	50	0.00
4	75 or 25	0.67
5	80 or 20	0.84
10	90 or 10	1.28
20	95 or 5	1.64
25	96 or 4	1.75
50	98 or 2	2.05

\*Factor for area under normal curve.



**Map 1**  
**Station Locator Map**



Map 2  
Mean Annual Heating Degree-Days



