# Extending the Real Remoteness of Long-Range Brillouin Optical Time-Domain Fiber Analyzers

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*Abstract*— The real remoteness of a distributed optical fiber sensor based on Brillouin optical time-domain analysis is considerably extended in this paper using seeded second-order Raman amplification and optical pulse coding. The presented analysis and the experimental results demonstrate that a proper optimization of both methods combined with a well-equalized two-sideband probe wave provide a suitable solution to enhance the signal-to-noise ratio of the measurements when an ultra-long sensing fiber is used. In particular, the implemented system is based on an extended optical fiber length, in which half of the fiber is used for sensing purposes, and the other half is used to carry the optical signals to the most distant sensing point, providing also a long fiber for distributed Raman amplification. Power levels of all signals launched into the fiber are properly optimized in order to avoid nonlinear effects, pump depletion, and especially any power imbalance between the two sidebands of the probe wave. This last issue turns out to be extremely important in ultra-long Brillouin sensing to provide strong robustness of the system against pump depletion. This way, by employing a 240 km-long optical fiber-loop, sensing from the interrogation unit up to a 120 km remote position (i.e. corresponding to the real sensing distance away from the sensor unit) is experimentally demonstrated with a spatial resolution of 5 m. Furthermore, this implementation requires no powered element in the whole 240 km fiber loop, providing considerable advantages in situations where the sensing cable crosses large unmanned areas.

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*Index Terms*— **Distributed optic fiber sensor, Brillouin scattering, distributed Raman amplification, optical pulse coding, strain and temperature measurements.**

## I. INTRODUCTION

T HE demand on distributed fiber optic sensors based on Brillouin optical time-domain analysis (BOTDA) [1-3] has been increasing over the past years in many application fields due to their unique capability to monitor distributed strain [1] and temperature [2] changes over many tens of km of optical fiber with metric spatial resolution. BOTDA sensors make use of two counter-propagating optical waves, a pulsed pump wave and a continuous-wave probe signal, which interact with an acoustic wave generated within the fiber through stimulated Brillouin scattering (SBS) [3]. Since pump and probe signals must propagate in counter-propagating directions along the optical fiber, the BOTDA interrogation unit requires access to both fiber ends. Therefore, BOTDA sensors can only exploit the entire sensing fiber whenever the fiber ends are at close distance, typically in bi-dimensional or three-dimensional configurations, e.g., for monitoring civil structures; however, for applications in which a linear fiber configuration is required, e.g., for long pipelines or offshore monitoring, the real remoteness of the sensor, and hence, the useful sensing distance, is restricted to half the fiber length.

In order to make an efficient use of the whole sensing length when long linear structures have to be monitored, the optical fiber length connected to the BOTDA sensing unit can be doubled, while only half of it is used for sensing purposes [4]. This way, the first half of the optical fiber can be used as a distributed sensing element, while the second half is only dedicated to transfer the probe signal up to the most distant point in the sensing fiber. In this paper this fiber arrangement will be hereafter called *'linear sensing fiber configuration'*. Although the sensing length is not increased in this fiber configuration, the real remoteness of the sensor can be doubled [4], allowing the BOTDA system to sense critical points located at much longer distances. Unfortunately, with such a scheme the probe power reaching the receiver is highly attenuated, and therefore, no sensing capabilities or eventually an extremely low sensing performance should be expected at long distances.

Some techniques have been recently proposed in the

literature to extend the sensing length of BOTDA sensors operating with the standard fiber configuration, challenging the well-known trade-off between spatial resolution and sensing range. In particular, optical pulse coding [5] and distributed first- and second-order Raman amplification [6-8] have made it possible to sense ranges beyond 100 km with spatial resolutions of a few meters. Although the use of those methods seems to be feasible and straightforwardly applicable for a very long linear fiber configuration, the high probe attenuation and the limited sensitivity of the optical detection stage make the design and power optimization much more challenging when compared to the use of the typical fiber-loop scheme [8]. In particular, the onset of amplified spontaneous Brillouin scattering imposes special constraints to the maximum probe power that is allowed in the fiber since this amplified Brillouin wave induces additional loss on the probe. It is interesting to notice that, although perfect power symmetry is required between the two probe sidebands to provide strong robustness against pump depletion in a long sensing fiber [9], the impact of any potential probe power imbalance in long-range sensing has been poorly addressed in the literature so far. One possibility to increase the optical power reaching the detector is to use bi-directional in-line Erbium-doped fiber amplifiers (EDFAs) along the whole optical fiber [4,10], partially compensating the fiber loss on both probe waves and Brillouin pump. However, in several applications for ultra-long remote sensing, such as long terrestrial pipelines or subsea flowlines, no electrical power is available for optical amplifiers. Actually, carrying the electrical power from one of the fiber ends would require several tens or even hundreds kilometer of electrical cables, resulting in an inefficient, costly, unreliable and unsafe alternative for long-range fiber sensing. Thus, it can be considered that methods based on powered optical repeaters at the middle of the fiber length do not provide a suitable and practical solution to extend the sensing range of BOTDA systems for many ultra-long applications.

In this paper an ultra-long BOTDA sensor in a linear configuration and without any powered elements in the sensing loop is implemented based on the optimized design of a seeded second-order distributed Raman amplifier [11,12] in combination with optical pulse coding techniques [13,14]. While Raman amplification is used to increase the probe power beyond the minimum detectable level, pulse coding enhances the probe power contrast resulting from the Brillouin gain, thus enhancing the signal-to-noise ratio (SNR) of the measurements [14]. The optimization procedure required for the system to operate along an ultra-long linear fiber configuration is fully described through this paper, paying special attention to the impact of the amplified spontaneous Brillouin scattering generated by the continuous-wave (CW) two-sideband probe signal. This way, the differences in the parameter optimization procedure with respect to previously published techniques [15,16], operating with the standard fiber configuration, are clarified. The power levels of the Brillouin pump, probe signal and Raman pumps are adjusted to optimize
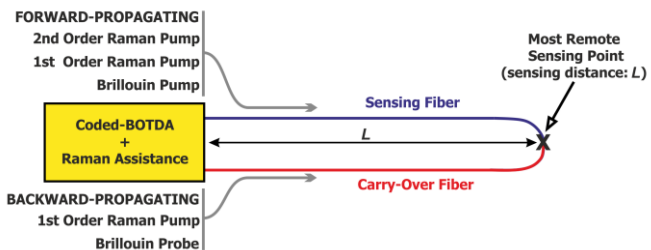


Fig. 1. Schematic diagram showing the principle of a long-range BOTDA sensor employing a linear sensing fiber configuration.

the Brillouin interaction within the sensing fiber and to simultaneously avoid probe power imbalance, pump depletion [9] and nonlinear effects [17]. In this way, to the best of our knowledge, the first distributed measurement with a real remoteness of 120 km, using a 240 km-long standard single-mode fiber, is experimentally demonstrated using a BOTDA sensor.

## II. EXTENDING THE REMOTENESS OF ULTRA-LONG RANGE BOTDA SENSORS

### A. BOTDA employing a linear sensing fiber configuration

In order to increase the real physical distance that a BOTDA sensor can reach, a *linear sensing fiber configuration*, as the one shown in Fig. 1, can be used. In comparison with the standard reported fiber configuration, where the whole optical fiber length is used for sensing [5-8], in this case only half of the optical fiber length is used for sensing purpose (this is the actual *sensing fiber*), while the other half (denominated as *carry-over fiber*) is only used to transfer the probe signal up to the most remote sensing location, corresponding to the farthest end of the sensing fiber. This feature actually makes a big difference when compared to the basic fiber configuration, since in this case the probe signal cumulates twice the effect of fiber attenuation; and therefore, it is more likely that the probe power does not reach the minimum detectable level at the optical receiver stage.

Using techniques such as distributed Raman amplification and/or optical pulse coding, sensing lengths up to 120 km have been reported using the standard fiber-loop configuration [5-8]. In all those cases the full sensing range has been determined by the fiber length, and hence only half of this length constitutes the real remoteness from the interrogation unit. Consequently, the longest sensing range reported with those techniques, which is 120 km [5,16], can only secure a remote sensing up to a distance of 60 km away from the interrogation unit. Extending the remoteness of the sensor up to 120 km requires a 240 km fiber-loop; however, under such a condition the probe signal is attenuated by about 48 dB while propagating along the entire optical fiber before reaching the receiver. This means that the CW probe power at the receiver is expected to be reduced by 24 dB when compared to the power measured in the basic configuration, in which a 120 km-long fiber-loop is only used.

In order to compensate for this additional attenuation of the probe signal, distributed Raman amplification provides a suitable solution. This would allow the probe signal to reach the minimum power levels required by the pre-amplifier at the receiver (typically used for long-range sensing [5]) to produce an acceptable optical SNR (OSNR) at the photo-detector. However, the power levels involved in a long sensing fiber configuration, such as the one shown in Fig. 1, are very different to the basic scheme [16], and therefore, a dedicated optimization of the Raman amplification is required. Actually, the optimization obtained from a system operating with the standard fiber-loop configuration cannot be straightforwardly applied (i.e. linearly extrapolated) to the case in which long sensing/carry-over fibers are used. This is because nonlinear effects occurring in the carry-over fiber have a significant impact on the power distribution of the signals propagating along the useful sensing fiber. Therefore, special design and optimization are required in this long linear fiber case.

### B. Use of seeded second-order Raman amplification combined with optical pulse coding

To overcome the problems associated to the sensitivity at the photo-detection stage when using very long sensing/carry-over fibers, in this paper optical pulse coding and seeded second-order Raman amplification are combined together in the BOTDA sensor.

The use of first-order distributed Raman amplification combined with optical pulse coding in BOTDA sensing has been proposed by X.-H. Jia *et al.* in [15]; however, the use of non-optimized Raman pump powers and the high-RIN of the Raman pumping scheme led in that case to a noisy system with a reduced sensing performance. Recently, much longer sensing distances have been achieved combining the above mentioned methods and optimizing the power levels launched into the usual standard fiber-loop configuration [16].

In the proposed scheme, the Brillouin pump is generated by intensity modulation of the laser light mapping the pulse sequence patterns defined by Simplex codes [13]. The pump power can be this way spread in the time domain, so that the intensity contrast of the Brillouin gain measurements is increased while the maximum peak pump power inside the fiber is kept below the onset of nonlinear effects, primarily modulation instability [14].

In order to improve the OSNR of the probe signal reaching the photo-detector, both the OSNR and gain resulting from the distributed Raman amplifier have to be optimized. On the one hand, in order to increase the maximum distance reached by the coded Brillouin pump, a "seeded" second-order Raman amplification scheme [11,12] is implemented to amplify the pulse sequences. In this scheme a low-power first-order Raman pump at 1455 nm acts as a seed that is amplified by a high-power second-order Raman pump at 1365 nm. Although this amplification scheme has been widely used in telecommunication systems [11,12], to the best of our knowledge, it has never been implemented for BOTDA

sensing. This way the maximum Brillouin pump power is shifted to a more distant location along the sensing fiber (up to about 30 km). The sensing range extension is reasonably estimated to be about 15 km with respect to direct first-order Raman amplification. Both first- and second-order Raman pump power levels have to be carefully adjusted in order to increase the power of the Brillouin pump at the end of the sensing fiber (or equivalently, to extend the distance reached by the coded pump), but at the same time, to avoid that the maximum Brillouin pump power in the fiber exceeds the threshold of nonlinear effects [17].

On the other hand, first-order low-RIN Raman amplification is also necessary on the probe side to secure a good performance of Raman-assisted BOTDA sensors [15]. Actually, although in counter-propagating Raman amplification the Raman pump RIN is averaged over the whole amplifier transit time, resulting in a negligible impact of the RIN on the sensor performance, a highly efficient pump-to-signal RIN transfer occurs in co-propagating Raman amplification [8,18]. Therefore, the co-propagating Raman assistance in the probe side has to be performed using low-RIN semiconductor laser diodes (LDs) to minimize the pump RIN transfer to the probe signal. Second-order Raman assistance co-propagating with the probe would result in a high and efficient pump RIN transfer, degrading significantly the SNR of the measurements. For this reason, as described in Fig. 1, only first-order Raman LD pumping is here proposed to co-propagate with the probe. As stated, the RIN characteristics of the Raman pumps used in the proposed second-order seeded Raman amplification scheme are not relevant. This can be easily justified by the fact that even though a high RIN transfer to the Brillouin pump is expected in this case (due to the co-propagating pumping scheme [18]), no penalties are expected in the SNR of the measurements due to the low cut-off frequency of the counter-propagating pump-to-signal RIN transfer function of the Brillouin scattering process [8].

Another important aspect of the proposed scheme is the use of pump pulses with return-to-zero (RZ) modulation format. It is well known that RZ pulses are required to apply optical pulse coding in BOTDA sensors, suppressing bit patterning effects resulting from pre-excited acoustic waves [19]. It turns out that, in the case of Raman assistance, RZ pulses also have the advantage to minimize the Raman cross-gain modulation occurring when the co-propagating Raman pump is depleted. Actually, a pulse separation of at least 50 ns is normally required to secure a complete decay of the acoustic wave amplitude between pulses of the code sequence. This time interval is much longer than the maximum walk-off between Raman pumps at 1450 nm and the Brillouin pump-probe signals at 1550 nm [18], which is of about 16 ns in standard single-mode fibers. Therefore, if the co-propagating Raman pump at 1450 nm is depleted by the amplification of a single Brillouin pump pulse, no impact on the amplification of the following pulses from the same sequence is expected.

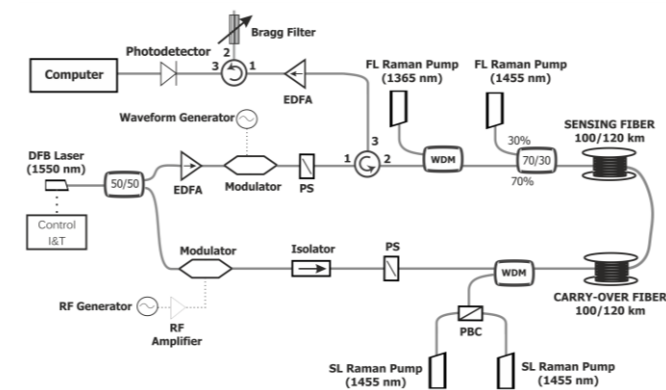As a difference to previously reported works [8,16], here a

Fig. 2. Experimental setup of the implemented BOTDA sensor based on seeded second-order Raman assistance and pulse coding. DFB: distributed feedback laser; EDFA: erbium-doped fiber amplifier; PS: polarization switch; WDM: wavelength division multiplexer; RF: radio-frequency; PBC: polarization beam combiner: SL: semiconductor laser; FL: fiber laser.

suitable power optimization has to be carried out for very long sensing/carry-over fibers. As it will be later described in Section II.D, the presented procedure mainly pays attention to the Raman amplification of the probe waves to avoid effects such as amplified spontaneous Brillouin scattering, which might unbalance the power of both probe sidebands along the carry-over fiber. In addition, the limited extinction ratio of the pump pulses provides a CW component that amplifies/deplete the probe waves, increasing the possibilities to unbalance the power of both probe waves. This turns out to be critical for systems aiming at an extremely long remote sensing, since an eventual power imbalance of the probe sidebands would induce pump depletion along the sensing fiber and distort the measured Brillouin gain spectrum.

### C. Experimental setup

Fig. 2 shows the experimental setup implemented to realize extremely long-range distributed measurements. Two different experiments have been carried out using the same setup: *i)* the first experiment corresponds to BOTDA measurements along 100 km sensing distance, using a 200 km fiber-loop and a spatial resolution of 3 m; and *ii)* the second one consists in the use of a 240 km fiber-loop for measurements along a 120 km range with 5 m spatial resolution.

A distributed feedback (DFB) laser operating at 1550 nm is the only optical source needed for the generation of Brillouin interacting signals in the system. Using a 50/50 coupler, the CW light from the laser is split into distinct branches to generate the coded pump signal and the probe signal.

A high-power pump signal is generated using an EDFA and an electro-optic modulator (EOM), which is used for on-off modulation of the CW laser light according to the Simplex code sequences. Note that the EDFA is placed before the EOM in order to avoid distortions in the pulse sequences resulting from the Erbium-doped fiber gain depletion [14]. To induce Raman amplification along the optical fiber, the coded pulse sequences are coupled with two depolarized fiber Raman lasers: a low-power seed first-order Raman pump at 1455 nm

and a high-power second-order Raman pump at 1365 nm.

As far as the probe signal is concerned, this is obtained using the well-known double-sideband technique [20], in which two equally spaced sidebands are generated by intensity modulation of the CW laser light. Thus, by adjusting the RF modulation frequency on the EOM, the Brillouin gain spectrum can be easily scanned. To minimize the polarization-dependent gain (PDG) of the distributed Raman amplification along the fiber, two orthogonally-multiplexed low-RIN semiconductor lasers at 1455 nm have been coupled with the probe signal inside a Raman pump unit that provides a PDG lower than 0.5 dB.

The optical fiber consists of several drums of standard single-mode fiber, with a total length of 200 km or 240 km (depending on the experiment). Polarization diversity schemes, based on polarization switches (PS), have been used in both pump and probe branches to reduce the polarization dependence of the Brillouin gain spectrum (BGS) measurements.

Before the receiver, an EDFA operating in linear-gain regime is inserted to increase the power level of the coded probe signal reaching the photo-detector. A narrow-band fiber Bragg grating is used to select one of the probe sidebands and to filter out other unwanted frequency components, such as the amplified spontaneous emission (ASE) noise from the EDFA, the Rayleigh signal generated by the coded Brillouin pump, the residual carrier of the probe and the second probe sideband. The data acquisition is carried through an acquisition card connected to a computer.

### D. Optimization of power levels in long-range BOTDA sensors using a linear sensing fiber configuration

In order to avoid Brillouin pump depletion and nonlinear effects in the fiber, the power of the Raman pumps, Brillouin pump and probe signals have been carefully adjusted.

Although the use of seeded Raman amplification has been widely studied in the context of optical networks and wavelength division multiplexed (WDM) systems [11,12], this is the first use of this kind of amplification in BOTDA sensors. In the context of distributed Brillouin sensing, the design and power optimization of a Raman amplifier has to deal with completely different conditions when compared with WDM transmissions systems. In particular, while in transmission systems the power of the signal is maintained at a very low level to avoid problems related to double Rayleigh scattering and cross-gain modulation resulting from Raman pump depletion [11,12], in distributed Brillouin sensors, the Brillouin pump power has to be amplified up to the highest possible level in order to maximize its output power, but maintaining the highest pump power level in the fiber below the onset of nonlinear effects. Actually, the use of coded RZ-pulse sequences or single pump pulses with very low repetition rate makes typical levels of Raman pump depletion to have only a negligible impact on the performance of BOTDA sensors.
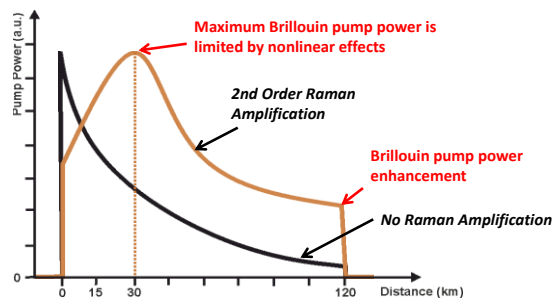
Fig. 3. Brillouin pump power evolution along the sensing fiber. The scheme shows the Brillouin pump power conditions needed for the Raman pump power optimization of the seeded second-order Raman amplification scheme.

In this work the optimization procedure for the forward propagating signals was carried out experimentally by knowing that, as a result of the second-order Raman amplification, the maximum Brillouin pump power occurs at about 30-40 km distance, as shown in Fig. 3. This way, by monitoring the power of the Simplex-coded Brillouin pump at the far fiber end, the maximum Brillouin pump power along the fiber can be estimated (after characterizing the fiber attenuation), so that the power of the Brillouin and forward-propagating Raman pumps can be adjusted to maximize the Brillouin pump power at the end of the sensing fiber, but at the same time to avoid that the maximum power exceeds the threshold of nonlinear effects while propagating inside the fiber. Since the sensing fiber in this case corresponds to a standard single-mode fiber, the maximum Brillouin pump power allowed in the system is limited by the threshold of modulation instability, which is about 100-200 mW [17]. Thus, following the above-described procedure, the optimal condition has been achieved using a peak Brillouin pump input power of 7.5 dBm and forward-propagating Raman pumps of 16.0 dBm and 29.8 dBm for the first- and second-order Raman pumps respectively. Note that power levels are referred at the input of the sensing fiber.

On the other hand, the backward-propagating Raman pump is adjusted to provide the highest possible probe power level at the end of the carry-over fiber (i.e. at the most distant sensing point, as shown in Fig. 4), but at the same time to make pump depletion negligible along the sensing section [19]. Although this procedure seems to be similar to the one required in standard Raman-assisted BOTDA sensors [16], in this case the maximum probe power has to be reached within the carry-over fiber and not in the sensing fiber as in the usual fiber-loop case. Under such a condition, and in order to compensate the high attenuation of a long optical fiber, very high probe power levels are required within the carry-over fiber. Contrarily to the standard fiber configuration [16], the pump depletion that could occur in the carry-over fiber is not a problem for this long linear fiber arrangement, since potential variations of the probe power in this fiber section are not measured in the time-domain Brillouin traces. However, with high CW probe power levels another problem could arise in the long linear fiber configuration: this is related to the CW interaction of the two probe sidebands and their respective spontaneous Brillouin
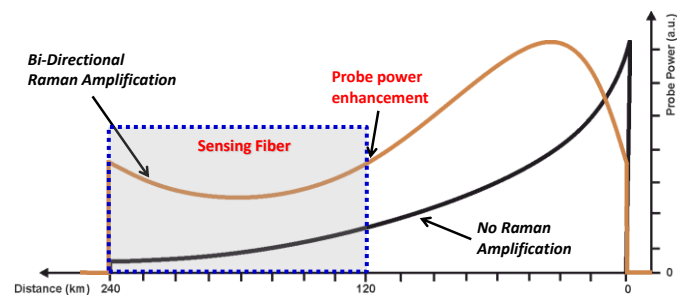


Fig. 4. Probe power evolution along the entire optical fiber loop. The scheme shows the probe power conditions needed for Raman pump power optimization in the backward first-order Raman amplification scheme.
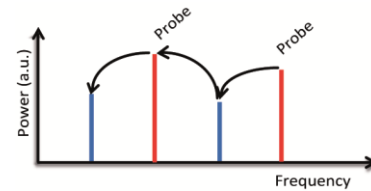


Fig. 5. Power imbalance resulting from the stimulated Brillouin scattering process occurring in a very long carry-over fiber when a high-power two-sideband probe signal is used. Power is transferred from higher to lower frequency components. Red lines represent the two probe waves propagating in a given direction (backwardly with respect to the Brillouin pump), and the blue lines correspond to the counter-propagating Brillouin components (in forward direction), initially generated by spontaneous Brillouin process.

scattering components. In particular, when the CW probe power increases beyond the threshold of amplified spontaneous Brillouin scattering, the energy transferred from the probe waves to their respective Stokes components could strongly unbalance the power among the two sidebands, as illustrated in Fig 5. The figure points out that under nonlinear Brillouin interaction, the energy transferred from the high-frequency probe sideband to its Stokes component is expected to be transferred to the lower-frequency probe sideband, which in turn transfer energy to the lowest Stokes component. In very long remote sensing, it is expected that this process would take place only along the carry-over fiber (within the nonlinear effective length), inducing depletion of the probe sideband at the higher frequency, while the lower-frequency sideband would not be significantly affected due to Brillouin gain/loss compensation. This cascaded energy transfer might quickly unbalance the power of the two probe waves, and thus compromise the robustness of the two-sideband probe technique against pump depletion within the useful sensing fiber section. Therefore, maintaining the same power for both probe waves is actually the main requirement that has to be satisfied when the power levels of the backward propagating Raman pump and probe wave are optimized. Thus, the proper optimization of these two backward-propagating signals requires *i)* to increase the probe power as much as possible within the sensing fiber, but keeping it below the level that induces pump depletion, and *ii)* to avoid power imbalance among the two probe waves within the carry-over fiber by maintaining the probe power below the critical power for the onset of amplified spontaneous Brillouin scattering. In this way the probe power at the receiver can be maximized, while

pump depletion is avoided along the sensing fiber. This condition has been achieved in our implementation using an input probe signal of -12.9 dBm per sideband and a backward-propagation Raman pump of 28.1 dBm. Note that these values correspond to the optimum power launched at the far end of the carry-over fiber for a 100 km sensing range (200 km fiber loop). However, for a 240 km fiber-loop, slightly higher power levels might be required to optimize the probe SNR at the receiver. Unfortunately, the low-RIN Raman pump module used in this experiment limits the maximum power launched into the carry-over fiber, so that only the optimal condition for a 100 km distance can be fully satisfied. As a result, the same power levels have been used for both experiments (i.e. for 200 and 240 km fiber loops).

### E. Mathematical model

In order to provide a better understanding of the Brillouin and Raman processes occurring in the proposed system, numerical simulations have been carried out and compared with experimental data shown in Sections III and IV.

From a numerical point of view, the Raman-amplification characteristics of the system can be defined through its steady-state equations [7,16]. The variations of the three Raman pumps and Brillouin pump along the optical fiber can be obtained by solving the following coupled equations [7], in which Rayleigh and spontaneous Raman scattering have been neglected, as well as the Brillouin-Raman pump depletion resulting from the low-power Brillouin probe:

$$\frac{dP_1^+(z)}{dz} = -\alpha_1 P_1^+(z) - g_{R12}\frac{v_1}{v_2}P_1^+(z)\left[P_2^-(z)+P_2^+(z)\right] \quad (1)$$

$$\frac{dP_2^+(z)}{dz} = -\alpha_2 P_2^+(z) - g_{R2B}\frac{v_2}{v_B}P_2^+(z)P_B^+(z)$$
$$+ g_{R12}P_1^+(z)P_2^+(z) \quad (2)$$

$$\frac{dP_2^-(z)}{dz} = \alpha_2 P_2^-(z) + g_{R2B}\frac{v_2}{v_B}P_2^-(z)P_B^+(z)$$
$$- g_{R12}P_1^+(z)P_2^-(z) \quad (3)$$

$$\frac{dP_B^+(z)}{dz} = -\alpha_B P_B^+(z) + g_{R2B}P_B^+(z)\left[P_2^-(z)+P_2^+(z)\right] \quad (4)$$

where the subscripts *1* and *2* represent Raman pumps at 1365 nm and 1455 nm respectively, the subscript *B* denotes the wavelength of the Brillouin pump/probe (which can be considered identical from the point of view of Raman interaction), the superscripts + and – represent forward or backward propagation respectively, $\alpha_i$ is the fiber attenuation at the wavelength *i*, and $g_{Rij}$ is the Raman gain coefficient between the wavelengths *i* and *j*.

On the other hand, the evolution of the Brillouin probe power $P_B^-(z)$ in the absence of the Brillouin pump in the Raman-amplified link can be obtained as:

$$\frac{dP_B^-(z)}{dz} = \alpha_B P_B^-(z) + g_{R2B}P_B^-(z)\left[P_2^-(z)+P_2^+(z)\right] \quad (5)$$

Solving numerically the system of equations (1)-(4), the Brillouin pump power evolution along the fiber $P_B^+(z)$ can be obtained. With this information, the pump spectral broadening resulting from self-phase modulation (SPM) can be evaluated along the fiber [21]. Since the impact of SPM in BOTDA sensing depends on the pulse shape [21], a proper pulse shaping has to be employed for the simulations. In this case, a 4th order super-Gaussian pulse has been used. Thus, in order to provide an estimation of the effective Brillouin gain bandwidth evolution along the fiber, the resulting pump spectrum has to be convolved with the natural Brillouin gain profile. This gain bandwidth can then be used to correct the Brillouin gain coefficient obtained for a non-broadened signal, resulting in a distance-dependent $g_B(z)$.

Then, the Brillouin gain trace can be calculated as:

$$Gain(z) = \frac{g_B(z)}{A_{eff}}\frac{cT}{2n}P_B^+(z) \quad (6)$$

where *c* is the speed of light, *T* is the pulse duration, *n* is the refractive index, and $A_{eff}$ is the fiber effective area.

### III. FIRST EXPERIMENT: BOTDA SENSING USING A 200 KM FIBER LOOP AND A SPATIAL RESOLUTION OF 3 M

#### A. Measurement conditions

The first experiment makes use of a 200 km-long optical fiber-loop, making distributed measurements possible up to a remote point located 100 km away from the interrogating unit. In particular, the 100 km sensing section (first fiber half) is composed of two 50 km fiber drums (named as Fiber A and B in the figures hereafter) with similar Brillouin frequency shifts (BFS = 10.66 GHz at room temperature and zero strain). In order to clearly visualize the end of the sensing fiber at 100 km distance, a carry-over fiber (corresponding to the second 100 km fiber section) has been used showing a completely different BFS (~10.85 GHz). The uniformity of the BFS along the entire sensing fiber actually leads to a continuous SBS interaction between the coded Brillouin pump and the probe signal over 100 km, resulting in the most critical situation to evaluate the impact of pump depletion on the system performance [9].

RZ Simplex coding with 127 bit has been implemented in this case, offering an SNR enhancement (so-called *coding gain*) of 7.5 dB with respect to the single pulse case [13]. The whole bit duration was set to 100 ns, while the single pulse duration was set to 30 ns (corresponding to a duty cycle of 30%), resulting in a 3 m spatial resolution. Each coded BOTDA trace has been averaged 16 times, resulting in 2032 equivalent time-averaged traces for each scanned frequency.
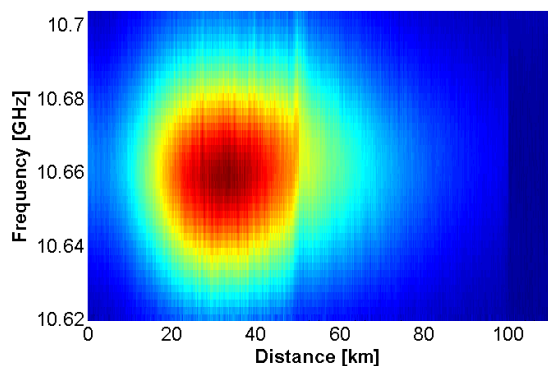
Fig. 6. Decoded BGS as a function of distance along 100 km sensing fiber, using a spatial resolution of 3 m and a 200 km-long fiber loop.
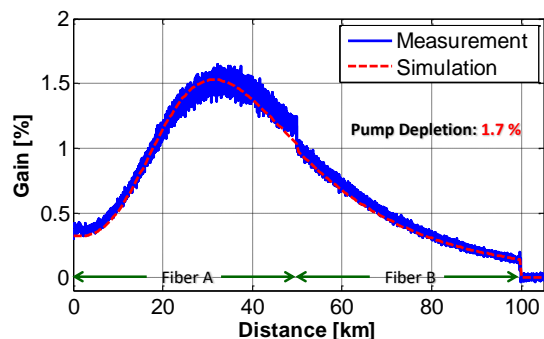


Fig. 7. Brillouin gain profile at 10.66 GHz vs distance when a 200 km-long fiber loop is used with 3 m spatial resolution. Measurements (blue straight line) are also compared with simulated results (red dashed line).

### B. Distributed measurements along 100 km

After measuring the BOTDA coded traces, a linear decoding process was used to retrieve the single-pulse fiber response at the different scanned frequencies. Fig. 6 shows a top view of the decoded BGS as a function of the distance along a sensing range of 100 km when a spatial resolution of 3 m is used. By carefully inspecting the trace at the maximum Brillouin gain (i.e. at 10.66 GHz), shown in Fig. 7, the sensing fiber end at 100 km distance can clearly be seen, showing a Brillouin net gain of ~0.17 %. In this figure, the experimental trace (blue continuous line) is compared with the BOTDA trace resulting from simulations at the peak Brillouin gain (red dashed line) using Eqs. (1)-(6). A good agreement between theoretical and experimental results is observed.

By fitting the decoded gain spectra at every fiber position, the BFS along the entire sensing range is obtained, as shown in Fig. 8. The uncertainty in the measurement (related to the temperature and strain resolution) has been evaluated by calculating the standard deviation of the BFS over the last meters of fiber. In this case the calculated standard deviation is 1.5 MHz close to a 100 km distant position, which is equivalent to either a temperature resolution of 1.5 K or a strain resolution of 30 με.

Pump depletion was finally evaluated measuring the residual coded Brillouin pump power with and without SBS interaction after propagation over 100 km. Measurements indicate that the pump depletion is kept as low as 1.7%, having a negligible impact on the BFS measurements [9].
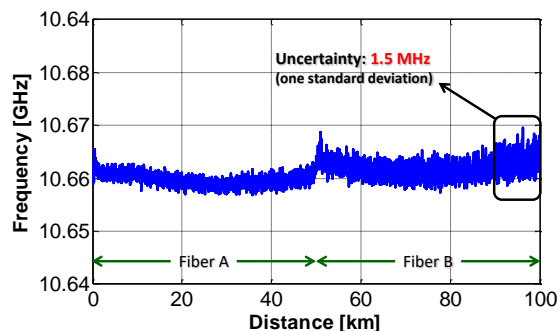


Fig. 8. BFS profile along 100 km distance, exhibiting a frequency uncertainty of 1.5 MHz at the end of the sensing fiber.
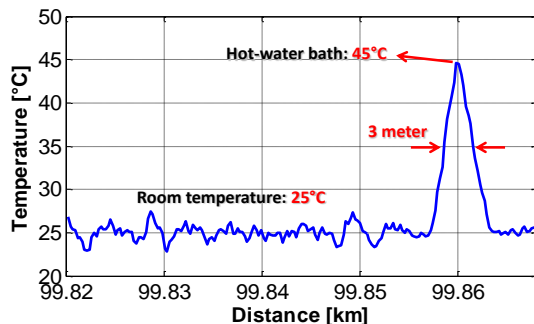


Fig. 9. Detection of a 3 m hot-spot at a 100 km sensing distance.

### C. Detection of a 3 m hot-spot at 100 km distance

In order to verify the sensing capabilities of the implemented BOTDA sensor in such an extreme condition, 3 meters of fiber from the region showing the lowest SNR (i.e. near 100 km distance) were introduced into a hot-water bath at 45ºC, while the rest of the fiber was kept in a controlled room temperature at 25ºC.

Fig. 9 shows the temperature profile measured in the last meters of fiber, where we can observe that the measured temperature profile perfectly matches the expected result. It is worth mentioning that this corresponds to the temperature measurement of a hot-spot located at a real 100 km distance away from the interrogation unit, in contrast with previously reported works [15,16] where the far end of the fiber is typically located in the close vicinity of the sensor unit.

### IV. SECOND EXPERIMENT: BOTDA SENSING USING A 240 KM FIBER LOOP AND A SPATIAL RESOLUTION OF 5 M

### A. Measurement conditions

In the second experiment a 240 km-long fiber-loop has been implemented, making measurements possible up to a distance 120 km away from the interrogation unit. In addition to the fiber drums of the previous experiment, two 20 km fiber drums have been appended to the fiber link; one segment with a BFS equal to 10.68 GHz (named as Fiber C) has been used at the beginning of the sensing fiber, while another drum with a BFS close to 10.9 GHz has been used to extend the carry-over fiber. Considering that the difference of the BFS along the whole sensing fiber is lower than the Brillouin gain linewidth, a
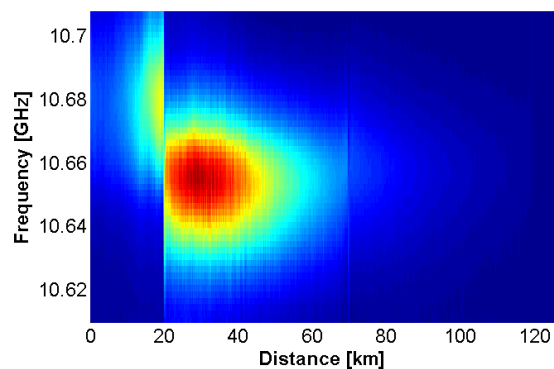
Fig. 10. Decoded BGS as a function of distance along 120 km sensing fiber, using a spatial resolution of 5 m and a 240 km-long fiber loop.
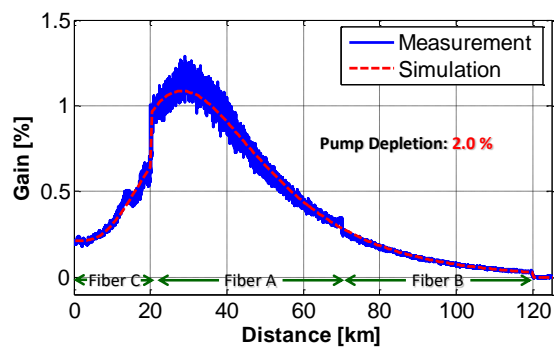


Fig. 11. Brillouin gain profile at 10.66 GHz vs distance when a 240 km-long fiber loop is used with 5 m spatial resolution. Measurements (blue straight line) are also compared with simulated results (red dashed line).
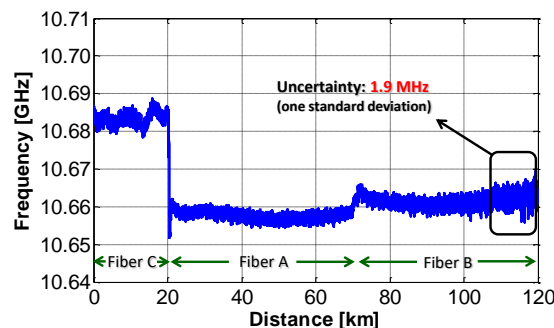


Fig. 12. BFS profile along 120 km distance, exhibiting a frequency uncertainty of 1.9 MHz at the end of the sensing fiber.

continuous Brillouin process takes place along the entire sensing fiber length (120 km), resulting in the worst-case condition for pump depletion.

Note that only 20 km have been added to the sensing range; however, this fiber extension induces a reduction of 12 dB in the SNR of the measurements with respect to the previous experiment. This comes from the fact that the pump power propagates along an extra 20 km of fiber length, i.e. being attenuated by an additional 4 dB at the end of the sensing fiber; while the probe signal propagates along an additional 40 km fiber length, i.e. being attenuated by another 8 dB before reaching the receiver. In order to recover part of this SNR reduction, the code length has been increased up to 255 bits and the spatial resolution has been downgraded to 5 m. Note that, even though longer code length could in principle be used, some effects on polarization noise restricted the code length to 255 bits, as described below in the experimental results.

In order to enhance the SNR while maintaining a number of acquisitions similar to the previous experiment, each coded BOTDA trace in this case has been averaged 8 times, resulting in a total equivalent averaging number of 2040 traces per scanned frequency. Under this condition (i.e. with similar measurement time), the SNR is expected to be enhanced by 1.5 dB with respect to the previous experiment using 127 bit; this represents a net coding gain of 9 dB when compared to the conventional single pulse method [9].

### B. Distributed measurements along 120 km

After decoding the BOTDA traces, the BGS has been obtained as a function of distance along 120 km. Fig. 10 shows a top view of the measured BGS when using a spatial resolution of 5 m. It is important to point out that despite the extremely long optical fiber used in this case, it is still possible to distinguish the end of the sensing fiber at 120 km, as clearly observed by inspecting Fig. 11. This figure also shows a comparison between the experimental BOTDA trace (blue continuous line) at 10.66 GHz and the trace obtained by numerical simulations (red dashed line) using Eqs. (1)-(6). A good match between both curves is clearly observed again. The discontinuity at about 20 km distance is simply a result from the BFS difference between the fiber segments. The SNR

at 120 km has been measured to be ~6.5 dB, corresponding to a Brillouin gain of 0.03%. Thus, the obtained SNR at 120 km distance is high enough to provide reliable measurements of temperature- and strain-dependent variations of the BGS.

Although two polarization switches (one at pump and another at the probe sides) are used to minimize the impact of Brillouin PDG, measurements indicate that BOTDA traces turn out to be slightly affected by polarization noise when extremely long sensing fibers are used. Actually, we have found that the used polarization diversity scheme, very common in standard BOTDA sensors, does not perform as expected with such a long optical fiber link (i.e. with 240-km fiber loop). It is believed that this issue results from residual polarization noise coming from the finite extinction ratio of the two polarization switches. This may lead to non-orthogonal states of polarization after propagation over several tens of km, inducing a residual Brillouin PDG in the measured BOTDA traces. In particular, it is observed that the residual polarization noise rises when the Brillouin gain increases (i.e. when longer code sequences are used), and has a larger impact at 30 km distance where the Brillouin pump reaches its maximum power, as shown in Fig. 11. This issue limits the maximum amplitude that the Brillouin gain can reach along the fiber, resulting in a real limitation to the maximum number of bits that can be used in the coded sequences.

The BFS along the fiber has been obtained by fitting the BGS at every fiber location, as shown in Fig. 12. It can be observed that using a pulse sequence of 255 bits, the polarization noise has a negligible impact on the BFS
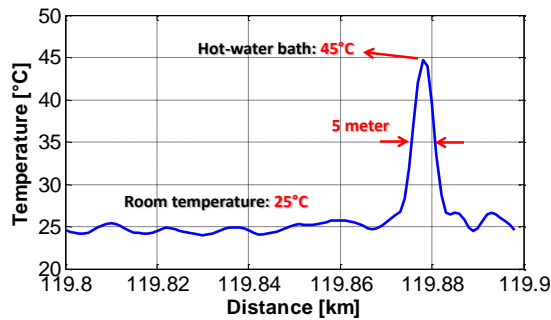
Fig. 13. Detection of a 5 m hot-spot at a 120 km sensing distance.

estimation. The standard deviation over the last meters of fiber (i.e. at the lowest SNR region) has been calculated to be 1.9 MHz, corresponding to a temperature/strain resolution of 1.9 K/38 με at 120 km distance.

As in the previous experiment, the pump depletion was estimated by measuring the power difference of the residual coded Brillouin pump with and without Brillouin interaction. The pump depletion in this case is 2.0%, which is low enough to induce no biasing on the BFS measurements [15].

### C. Detection of a 5 m hot-spot at 120 km distance

Finally, measurements under extreme SNR conditions have been carried out; in this case a section of 5 m of fiber was heated up to 45°C at a 120 km distance, while the rest of the fiber was maintained at a controlled room temperature of 25°C. Fig. 13 shows the measured temperature profile for the last 100 m of fiber, where we can clearly observe the 5 m hot-spot at 45°C. It is important to mention that this result constitutes the first demonstration of distributed measurements at a real 120 km distance away from the interrogating unit using a BOTDA sensor with no repeaters along the entire optical fiber.

## V. CONCLUSION

In this work we have presented a method to considerably extend the sensing range of BOTDA sensors. Using RZ optical pulse coding and seeded second-order Raman amplification, with a proper Raman pump power adjustment, we report extreme long-range BOTDA sensing capabilities along a real physical remote distance of 100/120 km from the sensor unit, using a 200/240 km-long entirely passive fiber-loop and 3/5 m spatial resolution. Such distances can be found while monitoring for instance long terrestrial pipeline or subsea flowlines for which no electrical power is available for repeater based sensing schemes. To the best of our knowledge this is the first time that such a distant remote sensing is reached using a BOTDA sensor, which we consider as a significant breakthrough in the field of distributed optical fiber sensors.

The presented analysis as well as the obtained experimental results point out that the power budget of both Brillouin pump and probe waves must be carefully controlled when using a ultra-long linear fiber configuration to avoid exceeding the critical powers for modulation instability and amplified spontaneous Brillouin scattering. Thus, the optimization of the Raman pumps is critical to maximize the sensor performance, avoiding simultaneously nonlinear effects in the fiber.

Finally, we believe that further extension of the sensing range needs a novel conceptual step since the implemented system shows very little margin to increase power levels (including the Raman pump power) and to extend the code length.

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