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# STUDIES AND RESEARCHES ON DESIGNING AND CONSTRUCTING A MECHANICAL MACHINE FOR MEAT TENDERIZATION WITH PNEUMATIC ACTION AND POSSIBILITIES FOR AUTOMATION

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#### ABSTRACT

Within meat processing technology the tenderization operation is important in the rapid maturation technique. Among tenderization methods, the least studied, yet with full ecological, biological and economical advantages is the mechanical tenderization. In this paper is presented an experimental model of machine of our own conception for the optimization of the tenderization process of the meat used for preparing traditionally products. Beside this the present paper presents the adequate system of pneumatic action and the automation elements of the working parameters which were made as our own conception for construction a machine for meat tenderization. Within the elaborated pneumatic scheme of driving there are identified the elements that can be electrically driven and the basis established scheme includes the programmable controller of the working process of machine and, finally, the cyclic scheme of function in order to establish the specific solutions for different meat types.

#### INTRODUCTION

The tenderization is a sensorial feature of the meat of high importance for establishing its final taste. The main feature is to facilitate the cutting, crushing and mixing the muscles fibers of the product with direct repercussions on the cumulative senses on tasting the final product. That's why the mechanical tenderization method can produce scraps after mastication that is smaller than biochemical methods and ensures against them superior eco-biologic qualities of the final product at low cost. [2,3]

Beating the meat method proposed by us to study will alow us to adjust different variations for working conditions of the machine in order to ensure optimum functional parameters for the main types of meat used. For this purpose the whole process is monitored in the framework of the pneumatic actuator of the designed machine by a microcontroller with programming posibilities after a previously established cyclogram. [9, 10]

#### MATHERIAL AND METHOD

#### 2.1. The mechanical structure of the machine. The cinematical scheme [9]

Mechanical construction of the machine requires knowledge of cinematic scheme, so that the conditions of functionality to be met. Based on the architecture and the principle of operation of the designed machine, cinematic scheme is shown in the figure below. Analele Universității din Craiova, seria Agricultură – Montanologie – Cadastru (Annals of the University of Craiova - Agriculture, Montanology, Cadastre Series) Vol. XLIII 2013



Fig. 2.1 The kinematical scheme of the machine

Legend:

- 1. Placement plate
- 2. Mobile pressing plate.
- 3. Guiding colons jointed with the placement plate.
- 4. Sliding bearings; they are jointed with the mobile plate for pressing and they glide on the guiding colons.
- 5. Upper securing cross part it is jointed with the guiding colons.
- 6. Coupling ball for correcting eventual coaxial deviations.
- 7. Driving pneumatic cylinder.

# **2.2.** The pneumatic installation for action. The operating scheme of the installation [5, 10]

The machine is driven by mean of a pneumatic cylinder. In order to adjust the working parameters in a wide range and to achieve the automation goal of machine there was adopted a pneumatic scheme of operating which is presented in the schetch bellow:



# Fig. 2.2 Pneumatic operating scheme

Legend:

- 1. Air pressuring unit compressor.
- Distributor with electrical command 5 HP/3 positions it determines the working status (direction).
- 3. Distributor with electrical command 5 HP/2 positions it determines the working way.
- 4. One-way switch of flow drosel.
- 5. Anti back flap.

Pneumatic cylinder

The functioning of the pneumatic installation is characterized by three states:

- Release state distributor (1) position R.
- Operating piston pushing distributor (1), position I
- Operating withdrawal of piston distributor (1), position T.
   In function of the distributor state (2) there are possible two working ways:

- With operation controlled piston pushing (adjusting the speed at pressing) distributor (2) not operating.
- No control at piston pushing (maximal speed) distributor (2) operating. With the controlled speed working way the functioning is as follows:
- Distributor (3) not in action
- Distributor (1) is brought in position I
- The air from the preparing unit follows the way branch B branch B1 flow flap branch B2 pneumatic cylinder. The air from cylinder will be evacuated on A way into the atmosphere. Due to flow flap (4), the speed of the piston will be determined by the flap adjustment. It is important that on the B3 way will not circulate air due to anti back flap (5).
- In order to withdraw the piston, the distributor (2) is brought to T position where the air circulation will be: preparing unit A branch head of the piston. The evacuation of the air will be made as follows: piston B2 branch flow flap B1 branch B branch atmosphere. In this case, the flow flap will have no effect because of the direction sense of the air circulation. As for the previous case, on the B3 branch there will not be air circulation due to anti back flap.
- For the working way with maximal speed, the functioning will be as follows:
- Distributor (3) in action
- Distributor (2) brought in I position
- The air from the preparing unit follows the following path: branch B3 flap (5) branch B2 pneumatic cylinder. The air from the cylinder will be evacuated on the A path into the atmosphere.
- For piston withdrawal, the distributor (2) is brought in position T, where the air circulation will be: preparing unit A branch head of the piston. The evacuation of the air will be made through the following path: piston branch B2 flow flap branch B1 branch B atmosphere. In this case the flow flap will have no effect due to the direction sense of the air circulation. On the B3 branch will be no air circulation due to anti back flap.

# 2.3. The electrical installation for operation and automation elements [6, 10]

The achievement of the operating and automation electrical scheme there are needed the operation conditions for each state of machine as described upward. In parallel, the operating must comply with the technological conditions of the process. Besides that the operating should follow the requirements imposed by the functioning parameters.

The operating conditions are determined by a series of factors as follows:

- Machine architecture
- Technological parameters
- Flexibility in changing the value of the functioning parameters
- Ensuring operation protection
- Ensuring the functioning within the limits of the working parameters.

# 2.3.1. The block operating scheme

From the pneumatic operation scheme results the elements that can be electrically driven:

- Distributor of machine states (sense of direction) this has two driving coils by which the distributor is brought to one of three states: R, I and T (see upward).
- Distributor of the working way by which there will be established the way the piston will be driven, the controlled speed or the maximal speed. The block scheme is presented below:



Fig. 3.1 The block operating scheme

# Legend:

- Power line electricity supply line
- Compressor drive on/off switch of the compressor
- Valve drive air valve operating block
- Position sensors position sensors and state; they are:
  - Superior course cut-off
  - UP position of mobile plate transmitter
  - DOWN position of mobile plate transmitter
- Cut off protection flap the machine is endowed with a flap that limits the working space of the machine in order to ensure operator protection
- Sensor of compressor state it signals the state of the compressor ON/OFF
- Programmable process controller, User interface.
- Signaling and local control through these features the operator can make functioning commands; they are:
  - Signaling of UP movement of the mobile plate
  - Signaling of DOWN movement of the mobile plate
  - Signaling the working way manual/automatic
  - Signaling the driving mode normal speed/maximal speed
  - Command of DOWN movement of the mobile plate
  - Command of UP movement of the mobile plate
  - Command START automatic cycle
  - Command STOP automatic cycle

# 2.3.2. Elements of automation and possibilities to use

The block scheme of electrical operation is endowed with the programmable controller of the process that is the main element of machine commands [6].

**Programmable process controller** is a real time programmable module with 8 digital entries and 8 digital exits. The implemented program into the controller has to comply with the functioning requirements of the machine. The controller is presented in the figure below.

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Fig. 3.2 The programmable controller

In the upper part there are 8 entries, from I1-I8. Also, here is mounted the power switch U+, U-. The exits O1-O8 are located in the bottom part. The connections to the controller are made by coupling the signal cables with the screw connectors according with the signal.

The interface with the user is made of an alphanumeric screen of LCD type which has 2 rows and 16 characters on each row. Also, there is a small bulb signaling that the processor is ON. The user can change the parameters by operating one of three buttons: M- menu; + plus – increase a value; - minus – decrease a value.

#### **Elements of controller software**

The implemented program in the controller implies the approaching of some aspects related to the state of the machine, the working way and the working parameters. The controller having as signals of entry the position sensors, the state of the compressor starting connector, the state of the protection flap and the state of the switchers of working way and driving mode can operate separately each state of machine.

The states of the machine are given by the working way and the position of the mobile plate.

With manual mode, the state of the machine is not limited by the program but for the lifting of the mobile plate so that the pneumatic cylinder of driving to not reach at the end of the course.



Fig. 3.3 The working graph of the automatic working way

The two active machine working ways, automatic and manual can be graphically represented. With the same aspect there can be represented each of the working states of machine: the working graph of the repose state, of the pressing state, of the release state, etc. For instance, for the automatic working way, the graph of the function is presented below:

In this working mode there are tested the states and for every one there is executed the specific function. The states noted in the figure with their correspondents are:

- mrest repose
- mdown Down movement
- mpress Pressing
- mrelase Release
- mup Up movement

If the system variable is not something that implies movement (mdown, mpress, mrelase or mup) there results that it is in mrest – repose.

#### The cyclograma of functioning

In the automatic working mode the variations of the mobile plate and of the pressure on the product are presented in the figure below:



Fig. 3.4 The cyclograma of functioning

Where:

Up- the upper position of the mobile plate

Down – the position of the mobile plate when pressing

Pn – nominal pressure on the product

Td – time of descending of the mobile plate

Tp – pressing time

Tr – releasing time

Tu - time of upper movement of the mobile plate

1,2...n – number of performed subcycles

# **RESULTS AND DISCUSSIONS**

The determination of the technological parameters of machine has had as main criterion the ensuring of quality of meat processing (tenderization) and means to optimize the working process by different working variants for specific meat types.

**The pressing force** – the product processing degree and the quality of tenderization are influenced by the pressing force. It is given by the features of the pneumatic cylinder and by the air pressure for its driving.

$$F_p = P_c \times S_p - Fr$$

Where: Fp – the pressing force (3.1)

Pc – the pressure from the cylinder

Sp – the surface of piston from pneumatic cylinder

Fr – the friction force to guidance parts.

#### The impact force

When the mobile plate touches the product, the driving force of cylinder increases very much and an impact force occurs upon the product. Taking account the fact that this machine is still in researching, the influence of this force on the product was considered.

The impact force is given by the pressure from the cylinder and by the weight of the aggregate formed of mobile plate and pressing element. The determination of the impact force was made by measuring the impact speed, the calculus of the transferred energy to the product and the distance the product is pressed.

$$Fi = \frac{Ep}{d} = \frac{\frac{m_p \times v_p^2}{2}}{Gi - Gp} = \frac{m_p \times v_p^2}{2 \times (Gi - Gp)}$$
(3.2)

where:

Fi - the impact force

Ep – the energy of the pressing plate

d – the distance of pressing

mp- the mass of the pressing plate plus the mass of the pressing element

vp – the speed of the pressing plate at impact moment

Gi – the initial thickness of the product

Gp – the thickness of the pressed product

#### Constructive parameters

There are several important issues that have to be accounted:

- > The loading capacity. It refers to the quantity of meat that can be processed in a cycle.
- The maximal course of the pressing plate.
- The maximal pressing force.

These elements determine the constructive parameters and, consequently, its dimensions. There was chosen a loading capacity of maximum 4 kg. On this basis there were calculated the dimensions of the pressing surface as 180 x 380 mm. By adding safety distances results an active surface of 200 x 400 mm. This parameter was used to calculate the minimal distance between the two guiding colons:

$$D_{\min} = W_{\max} + \Phi_c$$

(3.3)

Where:

Dmin – the minimal distance between colons

Wmax – the maximal length of the pressing surface

 $\Phi c$  – the diameter of the guiding colon; it will be calculated lately.

The chosen maximal course, of 200 mm is given by:

- The product height
- The additional distance where the operator can maneuver the product inside machine.

On the basis of this course, along with the features of the pneumatic piston there can be calculated the active height of the colons:

$$H_{ac} = C_{\max} + H_{cp} + H_{pm} \tag{3.4}$$

Where:

Hac- the active height of the colons

Cmax – the maximal course

Hcp - the height of the aggregate formed of pneumatic cylinder and its fixing system

Hpm – the thickness of the aggregate formed of mobile plate and pressing element

The maximal pressing force, as previously shown, is given by the formula (3.1.). Along with the maximal course there can be determined the characteristics of the pneumatic cylinder. This way there can be calculated the diameter of the piston:

$$D_{pcp} = 2 \times \sqrt{\frac{F_{\text{max}}}{\pi \times P_c}}$$
(3.5)

Where:

Dpcp – the diameter of the piston from the driving pneumatic piston

Pc – the pressure from the cylinder

Fmax – the maximal pressing force

For a maximal pressing force of 3,000 N and a working pressure of 6 bar there results:

$$F_{\text{max}} = 3000N = 305.9 \text{ Kgf}$$
  
 $P_c = 6bar = 6.12 \text{ Kgf/cm}^2$   
 $D = 2 \times \sqrt{\frac{305.9}{\pi \times 6.12}} = 7.98 \text{ cm} = 79.8 \text{ mm}$ 

There was chosen a pneumatic cylinder with the diameter of the piston of 85 mm and the course of the piston of 200 mm.

Along with the fixing system the pneumatic cylinder has a height Hcp=450mm. If the aggregate formed of mobile plate and the pressing element has the dimension of Hpm=80mm, from the formula (3.4.) there results the active height of the colons as follows:

 $H_{ac} = 200 + 450 + 80 = 730mm$ 

These dimensional parameters are used to final sizing of machine.

# CONCLUSIONS

The mechanical tenderization is a modern technological component of the process of meat manufacture. It allows the worker to modulate the working state of the machine on different optimal variants of applying the impact force, the pressing time and release of the product. It permits the worker to adjust the working parameters to the type of the meat; this issue makes this paper original;

The mechanical tenderization of meat by optimizing the economical, biological and economical conditions of the working process is the main objective of this paper which with the help of the experimental model of the machine presented in our own conception it can solve the problem of meat tenderization within the meat processing technology;

The authors have designed and constructed a pneumatic installation of operating the machine for mechanical tenderization where all working states of the process are automatic;

The programmable controller of the process has his own software program that ensures a programming variant after a cyclograma that was established by the operator;

The working graphs that are presented in the paper determine the recording of the functioning cyclograma that is needed for the performance of functioning.

This machine can be part of the technology used for making traditionally food products;

The present paper opens directions for researching in automation of different steps of technologies for meat processing.

#### BIBLIOGRAPHY

1. **Banu C., Alexe P., Vizireanu A.,** 2003- Procesarea industrială cărnii, Ediția a II a , Editura Tehnologică București, pag. 643.

2. Davis, K. A., D. L. Huffman, and J. C. Cordray, 1975 - Effect of mechanical tenderization, aging, and pressing on beef quality. Journal of Food Science. Volume 40, Pages: 1222-1224.

3. Jeremiah L. E., L. L. Gibson, and B. Cunningham, 1999 - The influence of mechanical tenderization on the palatability of certain bovine muscles. Food Research International. Volume 32, Pages: 585-591.

4. Loucks, L. J., et all., 1984 - Effect of mechanical tenderization and cooking treatments upon product attributes of pre-rigor and post-rigor beef roasts. Journal of Animal Science. Volume 58, Pages: 626-630.

5. **Măcuţa S.,** 2003 - Elemente de mecanică fină și servomecanisme. Editura Didactică și Pedagogică București.

6. **Oprean A. și al.,** 1983 - Acționări și automatizări hidraulice. Sisteme mecanopneumo-electrohidraulice. Editura Tehnică București.

7. Schilling M.W., N. G. Marriott, H. Wang, and M. B. Solomon, 2003 - Characteristics of USDA utility cow beef subjected to blade tenderization and hydrodynamic shock waves. Journal of Muscle Foods. Volume 14, Pages: 131-142.

8. **Seideman, S. C., et all., 1977** - Blade tenderization of beef psoas major and semitendinosus muscle. Journal of Food Science. Volume 42, Pages: 1510–1512.

9. **Simion A., Bădescu M.,** 2013 – Studii și cercetări privind proiectarea și realizarea unei mașini destinate tenderizării cărnii pentru obținerea produselor tradiționale. First International Conference, Danube – Black Sea, 3E-Energy, Environment&Efficiency, Universitatea Dunărea de Jos, Galați.

10. **Simion A., Bădescu M.,** 2013 – Studii și cercetări privind acționarea pneumatică a unei mașini destinate frăgezirii cărnii și posibilități de automatizare a acestei lucrări. First International Conference, Danube – Black Sea, 3E-Energy, Environment&Efficiency, Universitatea Dunărea de Jos, Galați.