

DEFLECTION OF REINFORCED CONCRETE BEAMS STRENGTHENED WITH CFRP**Tomas Skuturna¹, Mykolas Daugevičius², Juozas Valivonis³**^{1,2,3}*Department of Reinforced Concrete and Masonry Structures, Vilnius Gediminas Technical University, Saulėtekio ave 11, 10223 Vilnius, Lithuania**E-mail: ¹tomas.skuturna@vgtu.lt (corresponding author); ²mykolas.daugevicius@vgtu.lt; ³juozas.valivonis@vgtu.lt*

Abstract. This paper presents the results of an experimental study to investigate the deflection of reinforced concrete beams strengthened with external CFRP reinforcement. The influence of anchoring of external reinforcement was investigated. CFRP reinforcement was anchored in three different ways. Steel clamps, fibre wraps and steel pins were used for anchoring. Also different prepressing levels and different areas of steel clamps were used. The analysis of results of experimental research shows that anchoring of external reinforcement affects the performance and deflection of the strengthened reinforced concrete beams.

Keywords: reinforced concrete beams, strengthening, CFRP, deflection.

Introduction

Reinforced concrete structures can be strengthened with CFRP reinforcement. Such method is quite widely applied and is supposed to be efficient and convenient for the purpose of strengthening (Lamanna *et al.* 2004; Bank, Arora 2007; Li *et al.* 2008; Skuturna *et al.* 2008; Valivonis, Skuturna 2007; David *et al.* 2003; Bulavs *et al.* 2005; Duthinh, Starnes 2004; Chahrour, Soudki 2005; Ekenel *et al.* 2006; Ferrier, Hamelin 2002; Fayyadh, Razak 2012; Ceroni, Pecce 2007; Trapko, Trapko 2012; Buyukozturk *et al.* 2004; Yail *et al.* 2013; Smith, Teng 2002a; Smith, Teng 2002b; Hajsadeghi *et al.* 2011; Heffernan, Erki 2004; Xie, Hu 2013; Thomsen *et al.* 2004; Hsu *et al.* 2003; Harries *et al.* 2007). This strengthening technique, due to such excellent qualities of CFRP as high tensile strength, resistance to aggressive environment, and low weight, has a lot of advantages in comparison to other commonly applied techniques.

It is well known that the bond between concrete and CFRP is not stiff and due to shear strains external reinforcement may slip (Chen, Pan 2006; Pham, Al-Mahaidi 2007; Perera *et al.* 2004; Ueda, Jianguo 2005; Camli, Binici 2007; Lu *et al.* 2006; Casas, Pascual 2007; Schilde, Seim 2007; Iovinella *et al.* 2013; Ferracuti *et al.* 2007; Subramaniam *et al.* 2007; Mostofinejad, Shameli 2013; Wang *et al.* 2007; Freddi, Savoia 2008; Biolzi *et al.* 2013; Yuan *et al.* 2004; Ramos *et al.* 2004; Dai *et al.* 2005; Ramos *et al.* 2006; Pan, Leung 2007a; Saxena *et al.* 2008; Niu, Wu 2006; Pham *et al.* 2006; Pan, Leung 2007b; Ferrier *et al.* 2006; Mazzotti *et al.* 2008). So the deflection of the strengthened structure increases and the effect of strengthening decreases. The bond between concrete and CFRP is influenced by a few factors such as dimensions of concrete structure and CFRP, properties of the materials, and the way of anchoring external reinforcement. Only integrated performance of CFRP and strengthened structure can ensure effective strengthening. This can be reached by using additional anchoring of external reinforcement.

Experimental work

For experimental research 18 beams were produced. The beams were divided into two groups: B1 and B2. The focus of the first group was on investigation of the influence of different ways of anchoring. For the second group the focus was on investigation of the influence of different pre-pressing levels and different areas of steel clamps.

During the research all beams were tested in four-point bending (Fig. 1 and Fig. 2).

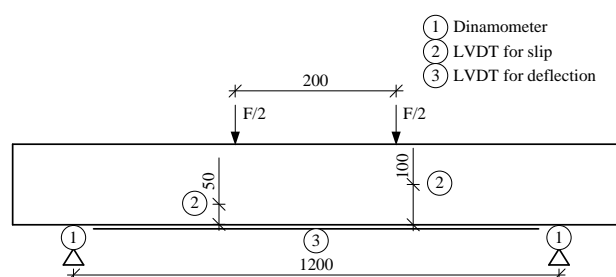


Fig. 1. Scheme of test setup and instrumentation.

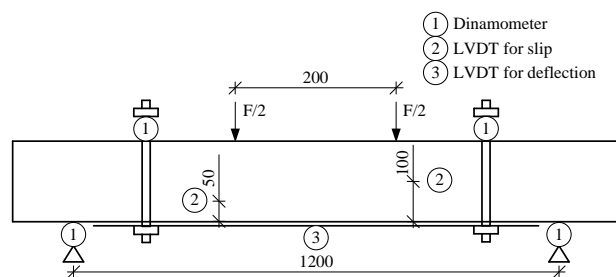


Fig. 2. Scheme of test setup and instrumentation (of beams whose external reinforcement is anchored with steel clamps).

The dimensions of the beams were 100 mm wide, 200 mm deep and 1,500 mm long. The span of the beams was 1,200 mm. The tension zone and the compression zone of beams were reinforced with 2Ø8 and 2Ø6 mm steel bars respectively (Fig. 3).

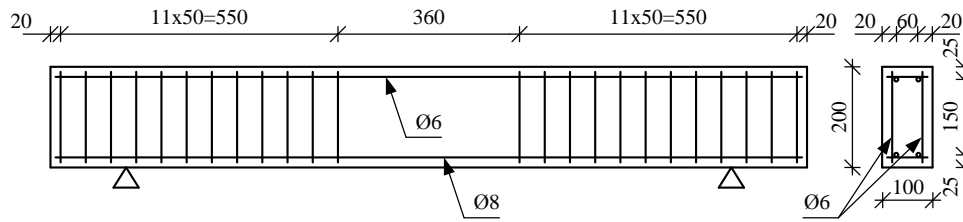


Fig. 3. Reinforcing details of B beams.

The shear spans of the beams were reinforced with 2Ø6 mm stirrups spaced at 50 mm along the beam. The width of the carbon fibre strip was 100 mm and its cross-sectional area was 16.8 mm².

The concrete strength class was C30/37. All internal reinforcement was standard steel reinforcing bars with nominal yield strength of 500 MPa. The strength in tension of carbon fibre was 3850 MPa.

Beams BN1-1 and BN2-1 were control specimens without external reinforcement (Fig. 4 (a)). Beams BR1-2, BR1-3 and BR2-2 (Fig. 4 (b)) were strengthened with CFRP but external reinforcement was not additionally anchored. For the rest of the beams external reinforcement was anchored in different ways. Steel pins were used in beams BA1-4 and BA1-5 (Fig. 4 (c)). For beams BS1-6 and BS1-7 external reinforcement was anchored with U wraps of carbon strips (Fig. 4 (d)).

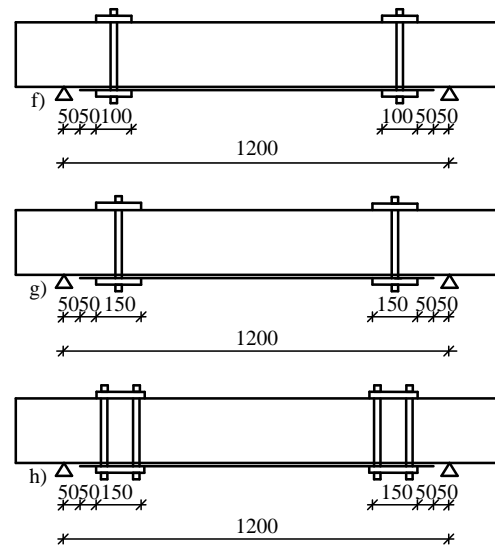
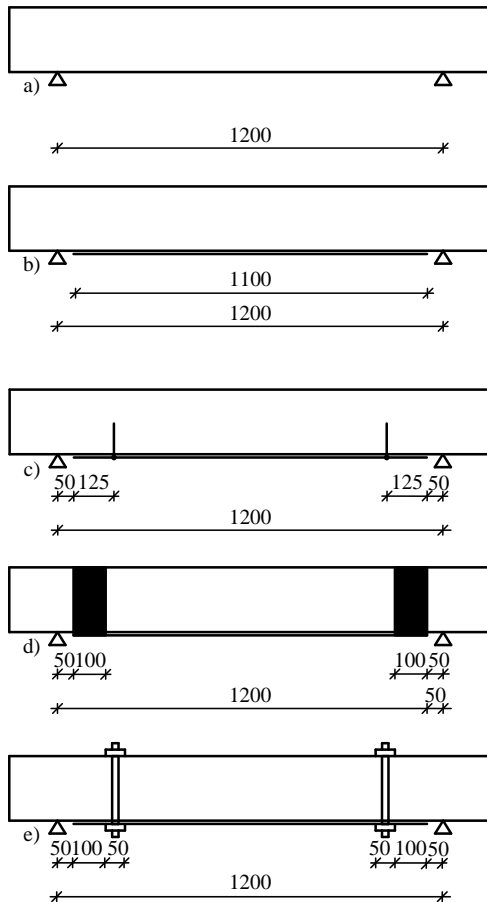


Fig. 4. Strengthening details of beams: a) control beams BN1-1, BN2-1; b) beams BR1-2, BR1-3, BR2-2; c) beams BA1-4, BA1-5; d) beams BS1-6, BS1-7; e) beams BC1-8, BC1-9, BC2-3, BC2-4, BC2-5, BC2-6; f) BC2-7; g) BC2-8; h) BC2-9.

Table 1. The way of anchoring external reinforcement

Beam	Anchoring	Note
BA1-4	Steel pin	-
BA1-5	Steel pin	-
BS1-6	U wrap	-
BS1-7	U wrap	-
BC1-8	Steel clamp	Clamp area 50 cm ²
BC1-9	Steel clamp	Clamp area 50 cm ²
BC2-3	Steel clamp	Clamp area 50 cm ² , 1MPa
BC2-4	Steel clamp	Clamp area 50 cm ² , 1MPa
BC2-5	Steel clamp	Clamp area 50 cm ² , 0,5MPa
BC2-6	Steel clamp	Clamp area 50 cm ² , 2MPa
BC2-7	Steel clamp	Clamp area 100 cm ²
BC2-8	Steel clamp	Clamp area 150 cm ² , 2 bolts
BC2-9	Steel clamp	Clamp area 150 cm ² , 4 bolts

The external reinforcement was anchored with steel clamps in beams BC1-8 and BC1-9 (Fig. 4 (e)). The areas of steel clamps were 50 cm². For B2 group of beams steel clamps areas were 50 cm² (BC2-3, BC2-4, BC2-5, BC2-6) (Fig. 4 (e)), 100 cm² (BC2-7) (Fig. 4 (f)), 150 cm² (BC2-8, BC2-9) (Fig. 4 (g, h)). Also for B2 group of beams different prepressing levels of steel clamps were applied – 0.5 MPa (BC2-5), 1 MPa (BC2-3, BC2-4) and 2 MPa (BC2-6).

Experimental results

It is expedient to distinguish three stages in the performance of reinforced concrete flexural structures strengthened with external CFRP reinforcement: performance of the member prior to the opening of first cracks; from the opening of cracks till the appearance of yield stresses in the steel bar reinforcement; when steel bar reinforcement yields until beam failure.

The graphs of the load-deflection relation for beam with the best anchorage (when steel clamps were used) beam without additional anchoring and control beam are presented in Fig. 5.

Analysis of graphs expressing load-deflection relationships (Fig. 5) indicates that in the first stage deflections of all beams were almost of the same value. After the appearance of normal cracks, deflections began to increase significantly, and the beams entered the second stage of performance. Stiffness of the beams is reduced due to cracks in the beams. At this stage of performance deflections grow with the load. Also the effect of strengthening can be seen in this stage, the deflection of the control beam is bigger than deflection of the strengthened beams. When the value of stress in the steel bar reinforcement reaches the value of the yield stress, the load-deflection curves demonstrate that beams enter the next stage. At this stage the effect of additional anchoring is seen. The beam external reinforcement of which is additionally anchored deflects less than the strengthened beam without anchors.

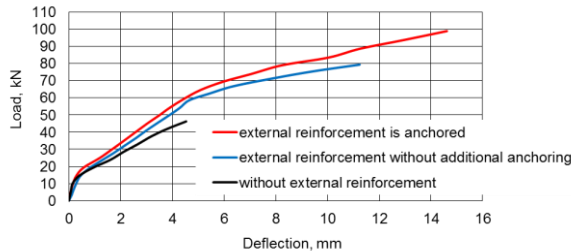


Fig. 5. Experimental deflection of beams.

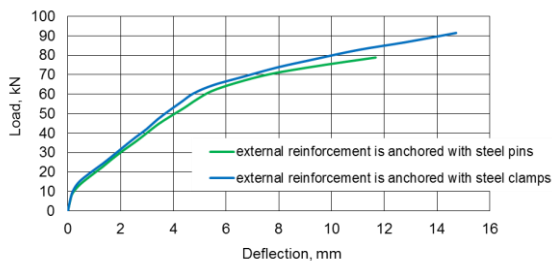


Fig. 6. Experimental deflection of beams BA1 (anchored with steel pins) and BC1 (anchored with steel clamps).

The performed analysis of experimental results shows that deflection of beams (which CFRP reinforcement anchored with steel pins) in all performance stages is by 10 percent bigger than that of the beams whose external reinforcement was anchored with steel clamps or U wrap (Fig. 6 and Fig. 7). In all stages of performance deflections of beams BC1 and BS1 (CFRP anchored with steel clamps and U wrap respectively) are similar.

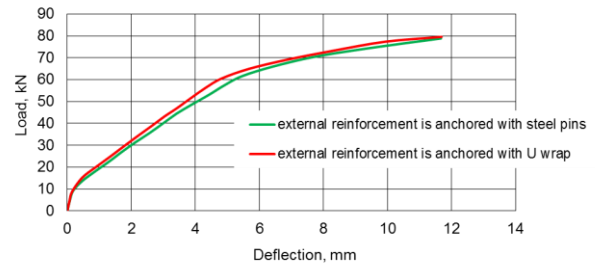


Fig. 7. Experimental deflection of beams BA1 (anchored with steel pins) and BS1 (anchored with U wrap).

Experimental research shows that different levels (0.5 MPa, 1 MPa, 2 MPa) of pre-pressing the anchorage area of external reinforcement with metal clamps do not have significant influence on the deflections of strengthened beams (Fig. 8).

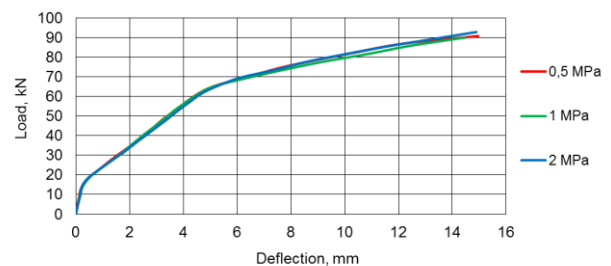


Fig. 8. Experimental deflection of beams BC2-4 (pre-pressing level 1 MPa), BC2-5 (pre-pressing level 0.5 MPa), BC2-6 (pre-pressing level 2 MPa).

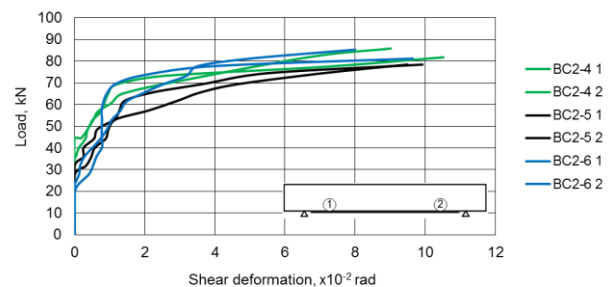


Fig. 9. Load-shear curves of beams BC2-4, BC2-5, BC2-6.

Analysis of the graph (Fig. 9) shows that when shear deformations of the bond grow, deflections of beams and pre-pressing levels of steel clamps also grow (Fig. 10). When the stress of steel bar reinforcement reaches and exceeds yield stress, the shear deformations increase significantly because the major part of the stress increment is resisted by CFRP reinforcement. Deflection of beams also increases significantly. The results of research show that pre-pressing level of steel clamps before failure increases by several times (Fig. 10). This can be explained by the fact that chocks have formed in the steel clamps due to shear deformations and deflection.

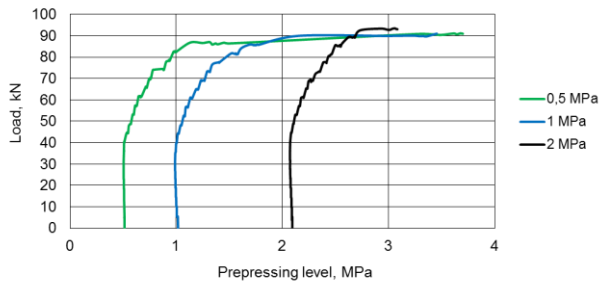


Fig. 10. Pre-pressing level in steel clamps.

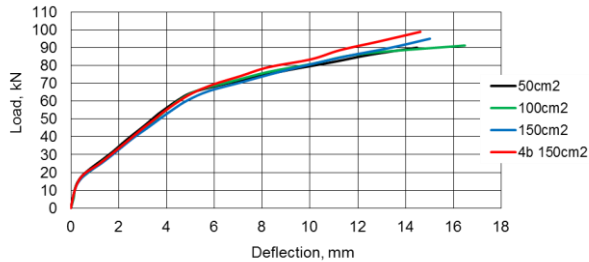


Fig. 11. Experimental deflection of beams BC2-4 (steel clamp area 50 cm²), BC2-7 (steel clamp area 100 cm²), BC2-8 (steel clamp area 150 cm²), BC2-9 (4 bolts, steel clamp area 150 cm²).

The research also shows that increasing of the area of pre-pressing with metal clamps does not have a significant influence on the load-carrying capacity of the beams strengthened with external CFRP reinforcement, however, it influences deflections of the strengthened beams (Fig. 11). The bigger the prepressing area, the smaller are the deflections.

Conclusions

Experimental research shows the influence of the type of additional anchorage of external reinforcement on the performance of the strengthened beams. The most effective way of anchorage is anchoring with steel clamps. When external reinforcement is anchored in this way, shear strains in the bond between external carbon fibre reinforcement and the strengthened member reduce as a result of which deflections decrease in comparison to the beams whose carbon fibre is not additionally anchored.

Research indicates that when external reinforcement is anchored with steel clamps, the level and area of pre-pressing of fibre do not have any influence on the load-carrying capacity of the strengthened beams. The recommended minimum area and level of pre-pressing of fibre in order to receive the maximum effectiveness of strengthening with respect to the deflection are 50 cm² and 1MPa. It has been established that the bigger the area of CFRP pre-pressing, the higher the stiffness of the bond between concrete and external reinforcement, the smaller are the deflections of the strengthened beams.

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