LOW NOISE, HIGH GAIN RF FRONT END RECEIVER AT 5.8GHz FOR WIMAX APPLICATION

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Abstract

This paper presents the design of a high gain, low noise direct conversion Radio frequency(RF) front-end receiver system. The Front end receiver is designed to operate at 5.8 GHz in compliant with IEEE 802.16 WIiMAX standard. The system consists of a low noise amplifier (LNA), a radio frequency amplifier (RFA), a power divider and two band pass filters. The design process involved the use of software such as ADS 2000A, Ansoft Designer and MathCad. FET FHX76 LP is used in the design of the LNA due to its low noise figure and high impedance input. As for the RFA design, FET EPA018A was used. The LNA and the RFA used T lumped reactive element network and microstrip line matching network. Two 3 dBπ -attenuators were inserted at the input and output of the RFA to isolate the system from the reflected load power. A Wilkinson power divider is developed for two equal power structures using impedance microstrip line technique. Microstrip technology was used for designing the Chebyshev filter. The result of each module for the front end is presented.

Keywords: *communication protocol, Controller Area Front-end receiver, Low Noise Amplifier, Radio Frequency Amplifier, Filter, Power divider, WiMAX.*

I. INTRODUCTION

A radio frequency front-end is an important part of a receiver as it provides the necessary gain, while introducing minimal noise, to meet the required signal to noise ratio (SNR). A typical RF front-end receiver consists of low noise amplifier (LNA), filter and mixer. The number of circuits added in the front end receiver varies depending on the type of receiver. The design complexity involves a trade-off between noise, gain and size. A key step in arriving at a cost effective and timely solution is by choosing the proper technology for the RF front-end portion of the radio receiver. Factors considered into making decisions were for example: the amount of signal content to be integrated, the application performance requirements and the capabilities of the chosen device. Currently, CMOS and GaAs are both widely used devices for many RF front end receiver design. Questions remain over which technology is most appropriate and the performance trade-offs seen in migrating between technologies. Uncertainty remains due to differences between architectures, system specifications and circuit designer themselves .

With the rapid growth of wireless communication technology, integrating RF circuits into the front end receiver is regarded as the solution for high system performance while maintaining low cost for future wireless systems. Current wireless technology system consists of an antenna, an indoor unit (IDU) for baseband processing and an outdoor unit (ODU) for RF front-end. Wireless bridge allows communication in separated buildings to be connected over a distance ranging from several hundred meters to several kilometers [1]. For point - point or point -multipoint communication the ODU consists of an RF front-end circuit that has the ability to amplify the standard input signals of -80 dBm up to the required gain while minimizing the noise figure and maintaining the desired bandwidth of 20 MHz.

An RF front-end receiver for a WiMAX ODU unit would have to be designed for desired frequency, gain, bandwidth and noise figure. The system includes RF components such as a low noise amplifier (LNA), RF amplifier (RFA), power divider and filters. In an RF front-end design, the problem such as noise must be determined and reduced. Multiple parameters such as gain and noise in the RF components for the front-end receiver would have to be compensated. These trade-offs are the challenges that RF designers have to consider in getting a high performance communication system. The system developed should comply with the 802.16 WiMAX standards. A review of this standard is necessary in order to understand the requirements before designing an RF front-end receiver. The review below will focus on circuit parameters required in designing the RF front-end receiver.

II. IEEE 802.16 FIX STATION WIMAX STANDARD

WiMAX, also known as IEEE 802.16 standard, is a wireless digital communication system that is intended for wireless metropolitan-area network technology that provides interoperable broadband wireless connectivity to fixed, portable and nomadic users [2]. It provides up to 50-kilometers of service area for fixed station and 5-15km for mobile station. It allows users to get broadband connectivity without the need of direct line of sight to the base station, and provides total data rates of up to 70Mbps. It has enough bandwidth to simultaneously support hundreds of businesses and homes with a single base station. The term WiMAX has become synonymous with the IEEE 802.16 Wireless Metropolitan Area Network (MAN) air interface standard. A WiMAX compliant system would provide a cost effective broadband access to users at home, in the office, in areas served by wire-line Digital Subscriber Line (DSL), cable services and to users equipped with portable devices like laptops, Personal Digital Assistance (PDAs) and smart-phones [3].

Table 1 shows the comparison between WiMAX, and its predecessors, the WLAN and Bluetooth technologies. The table compares the three different standards in term of frequencies, communication distance, data transfer rates and number of users for each system. It also shows that WiMAX system is an evolution of WLAN and Bluetooth technologies. The frequency varies from 2.4 GHz for standard WLAN to 11 GHz for WiMAX standard. The communication distance for WiMAX can be extended to 50 km.

Table 1: Comparison between WiMAX, WLAN and Bluetooth

Parameters	802.16a (WiMAX)	802.11 (WLAN)	802.15 (Bluetooth)
Frequency Band	2-11 GHz	2.4 GHz	Varies
Range	~50 km (31 miles)	~100 meters	~10 meters
Data transfer sate	70 Mbps	11Mbps ~ 55Mbps	20 Kbps ~ 55Mbps
Number of users	Thousands	Dozens	Dozens

The minimum input sensitivity must be maintained to the standard of -80 dBm. This would accommodate amplification of signals from a distance of 50 km. A front-end amplifier of gain at least 30 dB is considered sufficient. The overall noise figure should also be maintained at less than -10 dB for the overall system.

Since the front end system is capable of providing higher gain and bandwidth, the tradeoffs such as insertion loss and isolation factor should also be considered to achieve the best overall performance for the system. Such performance can be achieved by adding suitable isolators or attenuators in the RFA module to provide isolation for the overall system.

III. RADIO FREQUENCY RECEIVER ARCHITECTURE

Recent advances in wireless networking technologies, including 1-1.8GHz cellular phone, 1.9-2.2 GHz W-CDMA, and 2.4-5.2GHz WLAN/HiperLAN have urged development of low-cost, low-power, and small-size multifunctional RF system [4]. In addition, to facilitate a global location free access and personal mobility, integration of these services is crucial and requires development of multimode front-end modules capable of switching from one service operating at a frequency to another service operating at another frequency. A currently available multimode approach makes use of different chips for different modes and therefore does not meet low cost low, low power and small size requirement [5]. Another available approach applies the same chip, but has an inter-mode multiple frequency relation constraint.

Figure 2 shows a typical heterodyne receiver. It consists of an antenna coupled directly to a pre-selection filter before passing through a low noise amplifier.

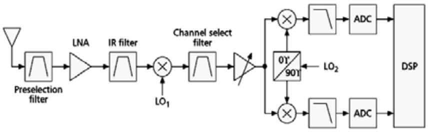

Figure 2: Typical Heterodyne Receiver

After passing through an image rejection filter(IR) the signal is mixed with a local oscillator (LO) and down converted to an intermediate frequency (IF). It is again filtered before being further amplified through a variable gain IF amplifier. The signal is then split and mixed with a second oscillator to produce a baseband signal for further processing. Figure 3 shows a direct conversion receiver.

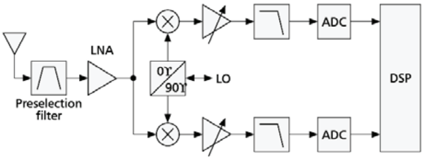

Figure 3: Typical Direct conversion Receiver

The difference between direct conversion receiver and the heterodyne receiver is that the direct conversion receiver does not require the IR filter, the RF mixer, an RF local oscillator and a channel select filter. The direct conversion receiver does not require a down conversion circuit.

IV. FRONT END RECEIVER DESIGN

Most of the front-end receivers developed were for licensed and unlicensed band of frequencies between 4.9 to 5.89 GHz. The maximum reported gain achieved was 32 dB with overall noise figure between 1.5 to 5.8 dB [6]. The channel bandwidth varied from 20 to 800 MHz with input sensitivity depending on the standard of WLAN and WiMAX. Therefore, it can be concluded, that for a better fixed front-end receiver to be developed the receiver should provide a better overall gain and noise figure with sufficient bandwidth to provide better performance yet compliant with the IEEE 802.16 WiMAX standard. A new proposed architecture specific link budget is introduced. Figure 4 shows the proposed architecture for the new direct conversion front-end.

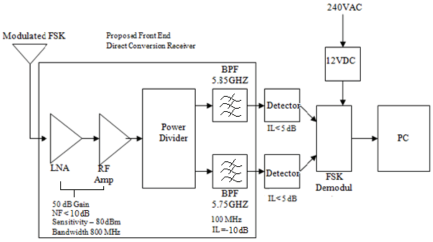

Figure 4: Proposed new front-end receiver.

The overall front-end receiver should introduce a higher gain of 50 dB compared to the 32 dB reported from the literature review, by taking into consideration the extension of communication distance of up to 50 km. To maintain a noise figure of less than 10 dB for the overall system as recommended by IEEE 806.12 WiMAX standard the noise figure for the front-end receiver should not exceeded -5 dB. Since the system should be capable of offering a higher capacity of subscribers of up to 200 channels, the bandwidth should be 800 MHz. This is double the standard 400 MHz for 20 sub-carrier of 20 MHz each. The input sensitivity of the system should cover the minimum sensitivity of -80 dBm.

V. LNA AND RFA

The Low Noise Amplifier (LNA) was introduced in the front-end receiver to separate the received signals with noise for a specific input sensitivity. Most of the LNA device in the review could only provide up to 20 dB gain. It was proposed that the low noise amplifier should have a gain of at least 35 dB. A budgeted high gain LNA will ensure a good signal to noise separation for further amplification. For this high gain of 35 dB, a cascaded amplifier is introduced for the LNA. At the same time the noise figure for the LNA should be less than 3 dB. A suitable device with super low noise parameter and required input sensitivity should therefore be selected for the LNA. An RF amplifier is introduced in the system to provide additional gain to meet the proposed overall gain of 50 dB. This addition of an RF amplifier is a new introduction to the architecture. Since the overall front-end gain targeted is 50 dB, the RF amplifier should provide an additional gain of 15 dB and noise figure less than 3dB.

The device chosen for the RF amplifier was selected based on the input sensitivity which is now at -55 dBm. Once the device was chosen the device parameter will have to be matched for maximum power transfer. At the same time added isolation can be provided by incorporating a matched 50 ohm Π network into the system. This also acts as a buffer for the next stage design. The approach taken in designing the amplifiers involves a series of chronological steps. No design is complete without some desired goals. The design specifications for the low noise amplifier and the targeted S parameter for the LNA and RFA are shown in Table 2 and Table 3.

Table 2: Design specifications for LNA and RFA

	LNA	RFA
Gain dB S_{21}	> 35	> 15
Frequency	5.8 GHz	5.8 GHz
NF dB	< 3	< 3
Matching Technique	Microstrip & Lump reactive element	Π Network & Microstrip + Lump reactive element
VSWR	1.5	1.5
Bandwidth MHz	> 1000 (5.8 GHz Centre)	>1000(5.8 GHz Centre)
Input sensitivity	- 80 dBm	- 55 dBm

Table 3: Targeted S Parameters for LNA and RFA

S Parameters	LNA	RFA
Input return loss S_{11} dB	-10	-10
Insertion Loss S_{12} dB	-10	-10
Forward Transfer S_{21} dB	35	15
Output Return loss S_{22} dB	-10	-10
Noise Figure NF dB *	< 3	< 3
Bandwidth MHz	>1000	>1000

VI. BANDPASS FILTER

Two bandpass filters with center frequencies 5.75 GHz and 5.85 GHz were required. Each of these filters should have a bandwidth of least 100 MHz. These filters are required to separate the signal into two main channels with four subchannels. Filter design methods include image parameter method and insertion loss method. Image parameter method is featured by master-slave configuration of simple 2-port filters to represent cut-off frequency and attenuation characteristic. Specific frequency response over the entire operating range is not taken into consideration. Therefore, design by image parameter method is comparatively simple but the same process must be repeated several times to get desired result. On the other hand, insertion loss method applies network synthesis technique to design a filter with desired frequency response. In other words, the insertion loss method synthesizes, band pass filter by converting prototype a low pass filter normalized with reference to impedance and frequency [7].

Chebyshev (equal-ripple) filter generates some degree of ripple at pass band but shows excellent cut-off characteristics at stop band. Since the critical design factor in this design is a fast cut-off characteristic at stop band, this filter was chosen. At this frequencies a microstrip line filter, which allow implementation of both compact size and integration was preferred. For this project, a coupled line Chebychev filter was selected.

VII. POWER DIVIDER

Power divider is a passive microwave device used to divide input power to more than two output ports with lower power level depending on the number of output ports as shown in Figure 4.

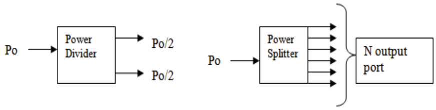

Figure 4: Power Divider

A power divider is ideally a lossless reciprocal device which can also perform vector summation of two or more signals and thus is sometimes called a power combiner or summer. For this project a Wilkinson power divider was adopted. A Wilkinson power divider has loss-free characteristics when output port was coupled. Moreover, two output ports are isolated and rarely interferes each other. Wilkinson power dividers are classified into several types depending on the number of output ports or power division ratio [7].

VIII. DESIGN AND SIMULATION

Low noise amplifier was design based on [7] and [8] listed in previous section. The FET chosen for the design is FHX76LP. The S parameter for the FET is shown in Table 4. These parameters were measured at $V_{DD} = 2$ V and $I_{DS} = 10$ mA which sets the biasing for the FET.

Table 4: S-parameter from Transistor FHX76LP datasheet

	S_{11}	S_{12}	S_{21}	S_{22}
Freq 5.8 GHz	0.712	0.065	8.994	0.237
Angle	-86.54	33.878	178.663	10.456

The overall performance of the low noise amplifier is determined by calculating the transducer gain G_T, noise figure F and the input and output standing wave ratios, $VSWR_{IN}$ and $VSWR_{OUT}$. The optimum, T_{opt} and T_L were obtained as $T_{opt} = 17.354 +j\ 50.131$ and $T_L = 79.913 - j7.304$. The calculated gain for the LNA was 19.3 dB, which correspond to a noise figure of 0.301 dB. The input matching load T_{opt} is required to provide high-loaded Q factor for better sensitivity. A T-network was used to match the input impedance [8]. The elements of T-network can be realized in the form of lump reactive elements and microstrip line impedance. The resultant matching component values are given in Table 5.

Table 5: LNA Amplifiers Parameters

Components	Values
L_1	3.60 nH
L_2	0.88 nH
L_3	0.67 nH
L_4	0.75 nH
C_1	0.5012 pF
C_B	7.5 pF

With these components, the schematic circuit for the single stage LNA is shown in Figure 5. This circuit was redrawn and simulated using Ansoft Designer to fine tune and further optimization for a better performance.

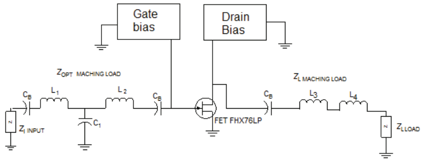

Figure 5: The schematic circuit for single stage amplifier

The RF amplifier was designed based on [6] and [7] listed in previous section. The design of the RF amplifier follows the same procedure used in designing the LNA [6]. Using theoretical design equations for the RFA, the equations are computed using MathCad. The FET chosen for the design is EPA018A. The S parameter given for the FET is shown in Table 6. These parameters were measured at V_{DD} = 2 V and I_{DS} = 10 mA which sets the biasing for the FET. This transistor biasing circuit is similar with the LNA amplifier.

Table 6: S Parameters of EPA018 A

	S_{11}	S_{12}	S_{21}	S_{22}
Freq. 5.8 GHz	0.728	0.049	6.327	0.237
Angle	-103.02	25.88	89.98	10.456

Gain, noise figure, input and output matching components were calculated and simulated using MathCad and ADS 2005A. Both calculated and simulated results were almost similar. Hence Table 7 lists both the calculated and simulated results for the RF amplifier. The stability factor as is 0.989. This showed a clear tendency for oscillation which confirmed the calculated stability factor. The calculated transducer power gain for matched condition was 16.28 dB. The input matching for optimum T_{opt} and T_L were obtained as T_{opt} = 12.662 +j 38.168 and T_L = 79.97- j7.286. The noise figure calculated is 2.475 dB.

Table 7: Calculated and Simulated Results for Designed RF Amplifier

S Parameters	Targeted RFA	Calculated and Simulated values
Input reflection S_{11} dB	-10	-8.03
Return Loss S_{12} dB	-10	-21.45
Forward Transfer S_{21} dB	15	15.31
Output Reflection loss S_{22} dB	-10	-7.85
Noise Figure NF dB *	<3	2.47
Bandwidth MHz	>1000	>1000

The RF amplifier can also act as an isolator for the overall front-end system and a suitable Π-network with 50 Ω load impedance was inserted at the input and output of the amplifier to provide a 3 dB attenuation each for the network. The RF amplifier component with the 3 dB attenuation is shown in Table 8.

Table 8: RF Amplifier parameters

Components	Values
L_1	7.21 nH
L_2	2.65 nH
C_1	0.30pF
L_3	0.67 nH
L_4	0.75 nH
R_1	8.17 Ω
R_2	8.17 Ω
R_3	616.27 Ω
R_4	8.17 Ω
R_5	616.27 Ω
R_6	616.27 Ω
C_B	7.50pF

Figure 6 shows the schematic circuit for RF amplifier with associated component and the 3 dB attenuator resistors.

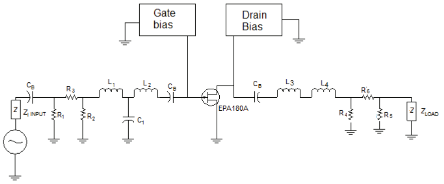

Figure 6: Schematic circuit for RF amplifier

The first step to design a bandpass filter is to determine the order of the filter that can work efficiently in the application system based on their design specification. In this project, the filter should be designed to fulfill the required specification for WiMAX application. The design specification for this bandpass filter is shown in Table 9 below

Table 9: Bandpass filter design specification

Filter Specification	Value
Center Frequency	5.75 GH
Filter Type	Chebyshev
Insertion Loss S_{21}	<-10 dB
Stopband Attenuation	25 dB @ 5.85 GHz
Bandwidth	100 MHz
Ripple	0.5 dB

For the filter design, the nth order of the filter was first decided based on the specification shown in Table 9. The order of the filter can be determine from plotting the normalized frequency versus attenuation. After determine the order of the filter, the design work of the filter begin with determination of normalized parameter values then converting the normalized parameter into lumped element equivalent circuit model and determination of even mode and odd mode of the impedances.

A simulation method was selected and simulation controller was added. When the simulation is finished, the data collected can be viewed in data display window. The data can be displayed in different format and manipulated for complex analyses. If the simulation result is not reaching the performance requirements, a new component or parameter is identified for optimization. The complete schematic circuit is shown in Figure 7. The circuit was optimized and the simulated S parameter output response for the filter was shown in Figure 8. Referring to simulated S-parameters, it was observed at 5.75 GHz frequency the insertion loss was -6.69 dB and the related reflection loss was -15.16 dB. These parameters values are acceptable since the required specification for insertion loss was less than -10 dB and reflection loss was more than -10 dB. The bandwidth was measured about 107 MHz.

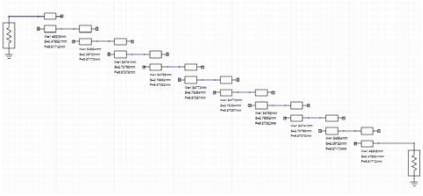

Figure 7: Complete bandpass filter circuit

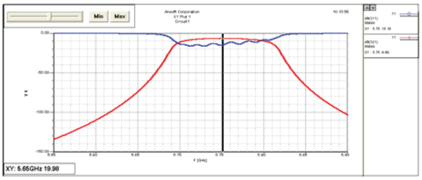

Figure 8: Simulation Filter Response

The comparison between targeted and simulated parameters result for band pass filter is shown Table 10.

Table 10: Comparison Parameters for Bandpass filter

Filter Specification	Targeted Value	Simulated Value
Center Frequency	5.75 GHz	5.75 GHz
Filter Type	Chebyshev	Chebyshev
Insertion Loss S_{21}	<10 dB	3.0 dB
Stopband Attenuation	25 dB @ 5.85 GHz	75 dB @ 5.85 GHz
Bandwidth	100 MHz	102 MHz
Ripple	0.5 dB	0.5 dB

Two forms of power dividers were generally constructed by cascading two-way dividers. These 2-way dividers were typically either terminated 180° hybrid (for RF frequency units) or Wilkinson or tapered line dividing structures (for microwave frequency devices). N-way dividers are devices which split signals in ways that are not 2N. M/A-COM offers a variety of 3-way and other N-way dividers that incorporate proprietary and patented circuit designs. Although power dividers could be composed of 90° hybrids, the term "power divider" normally refers to a device that splits an input signal into two or more in phase outputs [7].

In this paper, the entire receiver front-end system requires a 2-way equal power divider. The only parameter that needs to be calculated in power divider design is the value of characteristic impedance.

These characteristic impedances are then converted to line impedance using LineCalc Program provided in AnSoft Designer software. The power divider design specification is shown in Table 10.

Table 10: Power divider design specification

Power divider specification	Value
Frequency Range	5.3 to 6.3 GHz
Type	Wilkinson
Structure	2-way equal power
Insertion Loss	3.5 dB
Return Loss	<-10 dB
Input Return Loss	<-10 dB

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Table 10: Power divider design specification

Power divider specification	Targeted Value	SimulatedValue
Frequency Range	5.3 to 6.3 GHz	5.3 to 6.3 GHz
Type	Wilkinson	Wilkinson
Structure	2-way equal power	2-way equal power
Insertion Loss S_{21}	3.5 dB	3.14 dB
Return Loss S_{12}, S_{13},S_{31}	< -10 dB	-17.18 dB
Input Return Loss S_{11}	<-10 dB	-25.92 dB

The comparison between targeted and simulated parameters was shown in Table 11. As can be seen that the simulated parameter values were above and better than the targeted values. A final schematic circuit for power divider was simulated as shown in Figure 9.

Table 11: Comparison between Targeted and Simulated parameter value of Power divider.

Power divider specification	Targeted Value	SimulatedValue
Frequency Range	5.3 to 6.3 GHz	5.3 to 6.3 GHz
Type	Wilkinson	Wilkinson
Structure	2-way equal power	2-way equal power
Insertion Loss S_{21}	3.5 dB	3.14 dB
Return Loss S_{12}, S_{13},S_{31}	< -10 dB	-17.18 dB
Input Return Loss S_{11}	<-10 dB	-25.92 dB

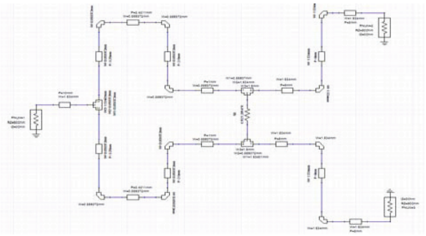

Figure 9: Complete power divider circuit

IX. MEASUREMENT AND ANALYSIS

The result for LNA RF front-end module was presented in Table 12.

Table 12: S Parameter result for LNA

S Parameters	Targeted	Measured
Input Reflection S_{11} dB	<-10 dB	-11.4
Return Loss S_{12} dB	<-10 dB	-39.1
Forward transfer S_{21} dB	>35 dB	36.8
Output ReflectionS_{22} dB	<-10 dB	-12.3
NF dB *	<3 dB	1.3
BW MHz	>1000	1240

From the tabulated values, the S_{11} parameter measured was 11.4 dB. This is -1.4 dB less than targeted which is better and acceptable. S_{22} measured was -12.3 dB which is less than targeted and acceptable. The return loss required

S_{12} obtained was less than -39 dB. The related measured gain S_{21} for the LNA amplifier was 36.8 dB. The noise figure values obtained was 1.37 dB which complied with the targeted value of less 3 dB. The use of T lump reactive element and microstrip line matching technique at the input of the LNA contributes the best performance for the amplifier.. This matching technique was used to provide high-loaded Q factor for better sensitivity and thus minimized the noise figure. The elements of T-network were realized in the form of lump reactive elements and microstrip line impedance. The 3 dB bandwidth for the amplifier is measured and the frequency response of LNA is shown in Figure 10. The 3dB bandwidth obtained was 1.24 GHz compliant with targeted result of more than 1 GHz.

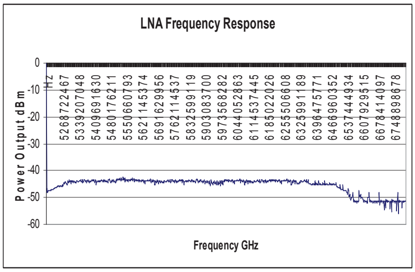

Figure 10: Power output Vs Frequency 5.8GHz fro LNA

The RF amplifier measurement setup was similar to the measurement set up for LNA. The results were shown in Table 13.

Table 13: S Parameter results for RFA

S Parameters	Targeted	Measured
Input Reflection S_{11} dB	<-10	-12.4
Return Loss S_{12} dB	<-10	-25.5
Forward transfer S_{21} dB	>15	15.6
Output ReflectionS_{22} dB	<-10	-12.3
NF dB *	<3	2.4
BW MHz	1000	1125

From the tabulated values, the S11 parameter measured was -12.4 dB. This is -2.4 dB less than targeted which is better and acceptable. S22 measured was -12.3 dB which is less than targeted and acceptable. The return loss required S12 obtained was less than -25 dB which is also acceptable and better. The use of Π-network with 50 Ώ load impedance at the input and output of the RFA shows a better return loss which was lower than -25 dB. The minimum return loss targeted for this amplifier was less than -10dB. The related measured gain S21 for the RFA amplifier was 15.6 dB measured.. The noise figure values obtained was 2.4 dB which complied with the targeted value of 3dB. Again shows that the use of T lump reactive element and microstrip matching network provide best performance for the RFA since the measure value nearly optimized. The 3dB bandwidth obtained was 1125 MHz which is more than the targeted result of 1000 MHz.

Both amplifiers were then cascaded and tested using measurement setup Figure 5.3a, and with 20dB attenuation set on the spectrum analyzer the output power versus frequency is shown in Figure 11. It was observed that the power output is -51 dBm and is expected if includes the total loss from cable and connector of 3.4 dB.

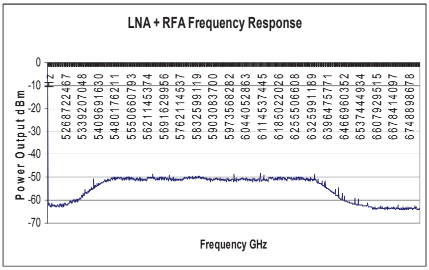

Figure 11: Power output vs Frequency GHz For LNA + RFA

The RF front end modular units were also tested for their frequency response. The front end module was completed with center frequency 5.75 GHz. The output from the filter is shown in Figure 12.

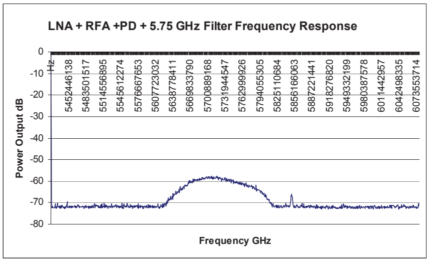

Figure 12: Power output vs Frequency GHz for LNA + RFAmp + Power Divider + Filter

The Front-end system designed consisted of a LNA, RFA, Power divider and filters were developed. The final result for overall amplifier gain was 52.40 dB gain with noise figure of 3.70 dB. The total insertion loss for the front-end was 5.80 dB which is contributed by passive network power divider and filters. With injecting a -80 dBm signal at the input of the front-end receiver, an output power of -59 dBm was achieved at the output. With considering the attenuation set at the spectrum analyzer, the actual signal output at the RF front-end receiver was -39.00 dBm. For a wireless communication system such as WiMAX system, this RF front-end receiver will capable to provide a better pipeline for the receiver with minimum noise figure and provide a high gain. This output is acceptable for further processing of the baseband system for IEEE 802.16 WiMAX standard.

X. CONCLUSION

A low noise, high gain front end receiver system consisting of Low noise amplifier (LNA), radio frequency amplifier (RFA), power divider and band pass filter has been developed. The overall noise figure targeted for the system was less than 6 dB and noise figure measured for the system was 3.733 dB. A cascaded LNA which was used in the system produced a high gain of 36.8 dB. The RFA contributes 15.6dB gain which is higher than the targeted of 15 dB. The implementation of T matching network for the LNA and the RFA that uses microstrip and lumped reactive element matching network gives a good overall performance of gain and noise figure for the system. Two 3 dB attenuators were inserted at the input and output of the RFA to isolate the system from the reflected load power also shows an improvement in return loss of the overall system. The radio frequency bandwidth recorded for the system was above 1000 MHz which complies with the targeted bandwidth. Using microstrip line technology for designing the filter, the channel bandwidth recorded was 107 MHz which can accommodate 4 sub channels. The front-end system developed can be implemented in IEEE 802.16 WiMAX standard with the standard input sensitivity of -80dB and channel bandwidth.

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