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## Design of a mill for the concentration of an Arkansas zinc ore

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FOR THE

Bachelor



IN



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### SUBJECT.

"Design of a Mill for the Concentration of an Arkansas Zinc Ore."

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R. A. CONRADS.

M. V. QUINN.

# Design of a Mill for the Concentration of an Arkansas Zine Ore.

The material to be treated is a zine ore from Boone County, Arkansas, a district as yet but little developed but from present indications of the ore deposits found in the vicinity, it promises in time to become one of the most important zine producing district ofnthe United States.

An abundant water and timber supply makes the cost of erection and operation of the mill comparatively cheap.

One of the greatest drawbacks to the development of the district in the past has been the lack of railroad facilities but the White River branch of the Missouri Pacific Railroad, which is nearing completion, overcomes this difficulty, m aking the district easily accessible and putting it on a direct line to the market.

The water supply is of especial importance as it does away with the necessity of saving the water from the mill.

### Analysis of Ore.

The ore, as carefully sampled in prospect working consists of an average of nine percent zinc blende in a gangue of gray limestone with a small amount of dolomite and a trace of iron pyrite.

### Occurance of Ore.

The ore occurs in a fairly course state of crystallization and as brought to the mill will average about twenty five percent fines (material passing a 24 m.m. ring)

### Capacity of Mill.

The frame work of the mill will be of yellow pine. Sides and roof of corrugated iron.

Laboratory Tests on the Ore and Conclusions drawn from them.

In the Missouri district the present practice allows from twenty to twenty five percent of the zinc in the ore to go to waste in the tailings. We propose to reduce this loss by a more careful and better treatment of the slimes which under the prevailing Missouri practice is almost totally neglected.

Experiments were carried on to ascertain the best methods of of crushing and concentrating the ore. From these experiments the most economical size to which the ore should be crushed was determined to be twelve m.m. Finer crushing than this tended to make too large a percentage of slimes. Crushing to this size gives about ten percent of middlings but also gives a large enough coneentrate for the first stage of crushing. The middlings were crushed through rolls set close and screened through two and onehalf m.m. sieve and together with the same sized material from the first crushing were treated in a classifier. The spigot discharge from this classifier(consisting of 2 1/2 m.m. to 1 m.m. material) was treated in a fine jig.

The system of classifiers used in our experiments and which will be installed in the mill is the Sherman System. Although this system is new and has not been used in Missouri to our knowledge, it has been used in mills in the west and has poven, it's superiority in the following respects:

- (a) Simplicity and consequently few repairs, etc.
- (b) Easy regulation
- (e) Delivering the classified material to the tables without an excess of water, thus effecting a higher saving from the fine material.

By the use of this system in connection with the Wilfley Tables, a greater percentage of the value in the fines and slimes will be saved and also a higher grade concentrate obtained with poorer tailings wasted

Flow of the Ore through the Mill

(subject to change in detail)

The ore is brought to the mill in cars and is dumped onto a grizzley with bars set twenty four m.m. apart. A powerful magnet is placed at the upper end of the grizzley to remove any pieces of iron, pieces of frick, drills, hammers, etc. which may be brought from the mine and would be injurious to the crusher and rolls.

The material passing over the grizzley goes into a bin and is fed through a shute to Two Blake Crushers set to twenty four m.m. From the crusher it drops directly into a bin together with the material which passes through the grizzley. From the bin it is fed by a roll feeder to one set of Rolls set to ten m.m. From the rolls through a chute to an elevator delivering the ore to a trummel with twelve m.m. round holes. The oversize is returned to the bin and is recrushed, undersize goes to second trummel having six m.m. round holes. Oversize goes to two coarse Harz jigs, undersize to third trammel with two and one half m.m. square holes. Oversize to three Harz Jigs. Middlings from first five jigs totgether with second, third and fourth hutch product of same jig and hutches of jigs number six, seven and eight are recrushed the on middling rolls and pumped by centrifugal pump to third tranmely. Undersize from this trommel to first elassifier, Spigot discorging to three fine jigs, overflow to second classifier with spigot discharging to one Wilfley Table. Overflow from second classifier goes to third elassifier with spigot discharging to One Wilfley table.

Overflow from third goes to fourth classifier with spigot discharge to one Wilfley Table. Overflow from fourth classifier to waste.

Specifications of Machinery Employed in the Mill.

- 1 Grizzley 6' X 10' bars 24 M/M. apart. Slope 45.
- 2 No.5 Blake Crushers, 15" X 9", feed set to 24 m.m.
- 1 Set Middling Rolls, set close
- 1 Set No.1 Rolls 14" X 36" set to 12 M/M.
- 1 Roll Reeder
- Trommel 4' X 7 1/2', 12 m.m. round holes. Incl. 5 degrees. 17 revolutions per minute
- 1 Trommel 2 1/2' X 5', 6 m.m. round holes, incl. 5 degrees, 17 revolutions per minute
- 1 Trommel 3 1/2' X 5', 2 1/2 m.m. square holes I ncl. 5 deg. 17 revolutions per minute.
- 1 Eldvator
- 2 4 Com. Harz Jigs 7 sq. ft. area wach screen

3 4Com. Harz Jigs, 3.5 sq.ft. area each screen

- 3 4 Harz Com. Jigs 3.5 sq. ft. area aach sereen.
- 3 Wilfley Tables.
- 1 Sherman Classifier 4'3" X 12'
- 1 Sherman Classifier 6'0" X 12'
- 1 Sherman Classifier 8'6" X 12'
- 1 Sherman Classifier 12'0" X 12'

5

Capacity and Horse Power Required by Machinery.

						•
2	Blake Crushers	Capa	eity 80	tons/10	hours	20HP
1	Set Rolls		120	••		10"
1	Set Rolls(middling)		2 <b>5</b>	*	**	5 "
1	Trommel	Ħ	120		Ħ	י ב
1	n	=	75	••	77	1 <b>"</b>
1	n	Ħ	50	Ħ		l"
2	-4 Com. Harz Jigs	Ħ	66	11	<b>11</b>	6 "
3	••• <b>4</b> •• •• •	Ħ	25.2	**	<b>11</b>	3"
3	••• <b>4</b> •• ••	Ħ	9	**		1.5HI
1	Wilfley Table (coars	se)	7 1/2"	<b>H</b>		י ב
	(medium	n)	<u>6</u>	**	<b>N</b>	י ב
	(fir	ne)	3	**	Ħ	י ב
1	Elevator					1.5"
		_	-			

Centrifugal Pumps, One #2, One #6, One

Total

HP

This gives an actual needed HP of but it would be well to allow 100 HP which would amply cover losses in friction, transmission, etc.

One one hundred horse power Copliss Engine, One one hundred horse power Heine Water Tube Boiler. Heine boilers are to be employed because of their efficiency, greater safety and longer life.

A feed pump and pump (#6 Centrifugal Pump) for mill supply. The diameter of shafting to be used was determined by formula given in Kent(s Mechanical Engineers Pocket-Book.

D

D Diam of shaft in inches

H HP to be transmitted

R number of revolutions per minute.

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The width of belting necessary was determined by formula from Kent's

W width of belt in inches R revolutions per minute L length of are of contact in feet d diam of pulley a angle of are of contact. Corliss Engine 90 revolutions per minute Diameter of fly wheel 10 feet " of shaft 4 1/2" To run main shaft at 120 revolutions per minute 120 : 90 120 : X 90" 7 1/2 feet diameter pulley on shaft.

Shaft Making 120 revolutions per minute.

W

Machine	Spe	ed I	Requ:	ired	Pulley Mach.	Pulley on Shaft
Blake Crusher	250	rev.	.per	m.	24" diam	50 *
Rolla	120	n	**	H	78 "	78"
Rolle onlower					Ratio of be-	vels
end, bevel gear or lowar and	17	TT -	Ħ	<b>99</b>	3:20	· · · · · ·
Jigs # 1 & 2	144	W	11	W	18"	21.6
" 3.4 &5	190			W	18"	28.5
" 6/7 &8	200	2	49	Ħ	18"	30 *
Tables by bevel gwar from main shaft.	240	rev	. p.e	r min	Ratio of be 2:1	evel
No. 2 Cent.Pump	850			Ħ	6 *	42.5"
No.6 Cent. Pump	745	11	Ħ	Ħ	16"	99.3