

Reconfigurable Multi-Beam Dual-Band Antenna based on Vee Dipoles

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Abstract

This paper presents a novel antenna configuration to support reconfigurable multi-beam feature with dual-band capability. The proposed design uses four double Vee dipoles with their arms printed on either sides of a substrate and fed through a single coaxial input probe. A single directional beam that can be configured in four directions at quadrature angle in the azimuth (xy-plane) and corresponding dual, triple and quad beams have been obtained by controlling the state of four PIN diodes. A prototype of the proposed antenna has been designed and fabricated. Measured antenna parameters are in good agreement with that of simulated parameters. This highly planar antenna shows similar radiation patterns at both design frequencies enabling concurrent dual-band communication for all fifteen possible beam configurations.

1. Introduction

Reconfigurability has become a highly desirable feature in modern wireless communication systems. Antennas with reconfigurable capability in terms of frequency, radiation pattern and polarization have been studied extensively in the past fifteen years for various applications. Advantages of having reconfigurable antennas are numerous: increase in channel capacity, reduction in co-channel interference and multipath fading, enhanced spectral efficiency, better wireless security and reduced power consumption [1]. Conventionally, pattern reconfigurability is achieved by using phased antenna arrays, which are large, complex and costly assemblies. Many applications do not require such complexity and a simpler/cheaper system is necessary to adapt. An antenna array with multi-port controlled beam switching is reported in [2] for multiple-input-multiple-output (MIMO) applications. A multi-beam antenna composed of nine vertical monopole antennas embedded in a dielectric cylinder mounted on a ground plane is presented in [3]. In [4], director-reflector pairs are used to achieve beam switching via PIN diodes. Such antennas with vertical standing features on the substrate lead to packaging concerns. Planar antenna having low profile, low cost and ease of integration is an attractive alternative.

One of the techniques employed in the design of planar reconfigurable antenna is the usage of parasitic

elements. Planar parasitic antennas with reconfigurable pattern are realized using PIN diodes in [5-7]. Dual-band capability along with pattern reconfigurability is necessary to support modern multi-band and multi-functional communication systems. Eventhough many papers are available on dual-band frequency reconfigurable antennas, only a few papers can be found on dual-band pattern reconfigurable antennas that support planar integration. A dual-band reconfigurable frequency-selective reflector based antenna is designed in [8]. Another design reported in [9] is based on parasitic arrays for MIMO applications. However, the non-planar arrangement of antenna elements makes these unsuitable for planar implementation. A dual-port diversity dual-band antenna is studied in [10]. A dual-band Yagi-Uda antenna is reported in [11] using complementary split ring resonators. However, the radiation patterns are not aligned in the same direction for the two design frequencies making it unsuitable for concurrent communication with the same receiver. To overcome these issues, a dual-band antenna based on printed Vee dipoles is proposed in this paper. Many proposals on antenna based on dipoles are available in the literature. A dual-band antenna based on printed dipoles is presented in [12]. Antennas based on dipoles with beam switching feature are reported in [13-15], but for single band applications. In addition to reconfigurable and dual-band capability, multi-beam feature is also necessary to enable concurrent communication with multiple users or to improve the link quality of wireless communication systems. The design of an antenna that has a planar structure supporting reconfigurable radiation pattern with simultaneous multi-beam configuration at more than one frequency is a task yet to accomplish. Such antennas are anticipated to be important for future concurrent communication systems. The antenna proposed in this paper uses four PIN diodes to connect any of the four double Vee dipoles to realize similar radiation beams at two frequency bands simultaneously. The truth table for different azimuth pattern configurations supported by the antenna is given in Table 1. The radiation patterns for all these states are confirmed by a series of pattern measurements at both frequencies. The proposed planar antenna thus provides an option to choose any one of the four single beam, six dual beam, four triple beam or one quad beam patterns in the azimuth plane. Moreover, similar

radiation patterns are obtained at two frequencies simultaneously making the antenna a good choice for use in concurrent diversity applications.

Table 1: Beam switching configurations.

Case	sw1	sw2	sw3	sw4	Beam Direction (ϕ)
1	1	0	0	0	90°
2	0	1	0	0	0°
3	0	0	1	0	270°
4	0	0	0	1	180°
5	1	1	0	0	90°,0°
6	1	0	0	1	90°,180°
7	1	0	1	0	90°,270°
8	0	1	1	0	0°,270°
9	0	1	0	1	0°,180°
10	0	0	1	1	270°,180°
11	1	1	1	0	90°,0°,270°
12	1	1	0	1	90°,0°,180°
13	1	0	1	1	90°,180°,270°
14	0	1	1	1	0°,180°,270°
15	1	1	1	1	0°,90°,180°,270°

2. Antenna Design

Vee dipoles are characterized by increase in directivity and reduced sidelobes as compared to their linear counterparts. Symmetrical Vee antenna having a specified arm length can have maximum directivity for an optimum Vee angle [16]. The proposed multi-beam antenna is composed of four identical elements arranged symmetrically around the centre input probe as shown in Fig. 1. Each element consists of a pair of Vee dipoles of which the inner Vee dipole decides the lower frequency whereas the outer dipole determines the

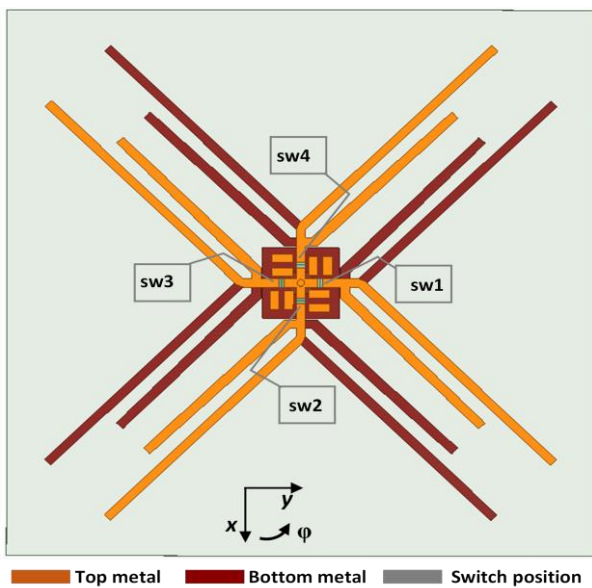


Figure 1: Geometry of the antenna.

higher frequency band. The symmetrical Vee dipoles are chosen to have unidirectional radiation pattern in the direction of the Vee opening. Each dipole has two identical double arms that are printed on either sides of the substrate. A single 50 Ω SMA connector fed from the other side of the substrate is connected to four parallel-strip feedlines. Each of these feedlines is connected to the antenna element through a switch (sw1-sw4) realized using PIN diode, BAP64-02. By controlling the combination of PIN diodes that are turned ON at any instant, single, dual, triple or quad beams are generated.

The bias circuit for the PIN diode is shown in Fig. 2. The DC supply is applied to the PIN diode through an inductor of 43nH to isolate the power supply. A capacitor of 2.2 pF is used to bypass any AC signals at the supply side.

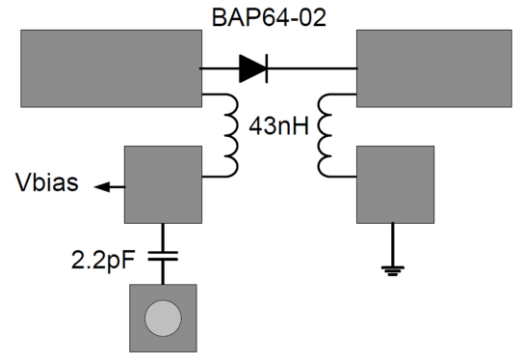


Figure 2: Biasing circuit for PIN diode.

For the design of dual-band antenna, the length of the Vee dipole arms is first determined. One full wavelength is chosen as a compromise between the size and directivity. Once the length (L_1) of the inner dipole arm is fixed as 49 mm corresponding to a frequency of 3.3 GHz (f_1), the length of parallel strip feed is designed for impedance matching [17]. The input impedance of the Vee dipole varies according to the included Vee angle (2θ). An angle of 90° has been chosen which provides an impedance value close to 50 Ω , thus simplifying the feed network. The length of outer dipole (L_2) is chosen as 39 mm for the second band's centre frequency of 4.2 GHz (f_2). The length of the parallel feedlines is further characterized to achieve good impedance matching for both frequency bands.

The design of the antenna has been simulated in ANSYS HFSS 17.1. The substrate having a relative permittivity of 4.4 and thickness of 0.8 mm is used in the design. The length of inner dipole, L_1 and the length of outer dipole, L_2 have been optimized to 46 mm and 36 mm owing to the coupling between the double Vee arms as well as the adjacent antenna elements. Switches have been simulated by modeling PIN diodes as two lumped RLC components in series. The ON state of PIN diode is modeled as two parallel RLC lumped components, L_s and R_s connected in series. The OFF state of PIN diode is modeled as the series combination of two parallel RLC lumped components L_s and C_p parallel R_p . The values of lumped components used for simulation are $L_s = 0.6$ nH, $R_s = 2$ Ω , and $C_p = 0.2$ pF. The length of the parallel strips has

been readjusted to compensate for the additional reactance introduced by the PIN diode.

3. Results and Discussion

The prototype of the antenna fabricated is shown in Fig. 3. The overall size of the antenna is 10 x 10 cm². The return losses for different switching cases listed in Table 1 are plotted in Fig. 4. The centre frequency is observed to be higher in the case where multiple PIN diodes are ON simultaneously. This is attributed to the change in effective length of the antenna when multiple dipole pairs are connected. The measured return loss is better than 10 dB for all cases. The slight deviations observed in the measured return losses as against the simulated results are due to manufacturing and soldering tolerances. The simulated current density of the antenna when a single switch sw1 is turned ON is shown in Fig. 5. The figure shows two distinct current paths for the two design frequencies. Similar current densities have been observed for multiple switches ON

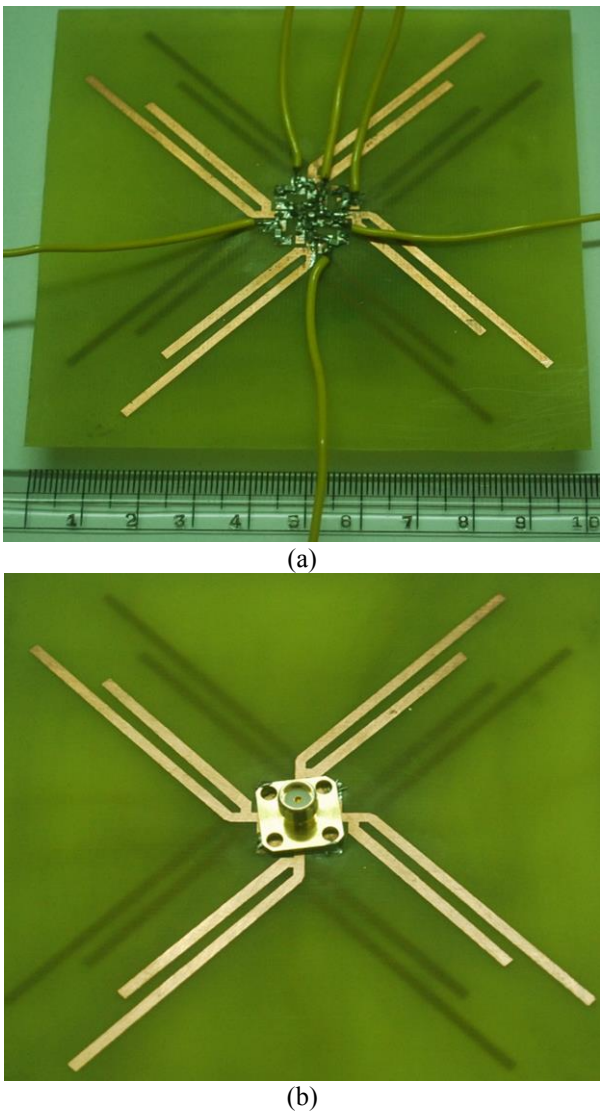
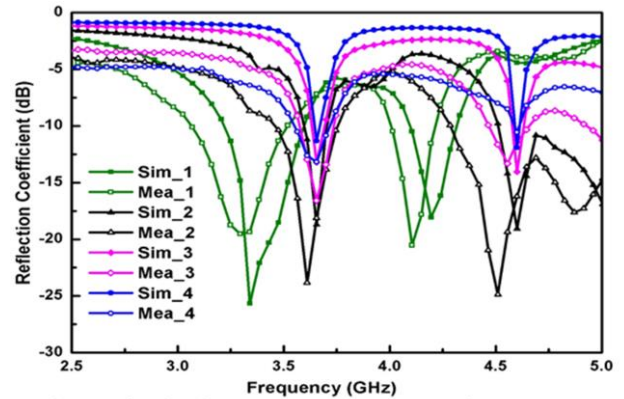


Figure 3: Photograph of the fabricated antenna (a) front view, (b) rear view.

cases too.

The desired radiation patterns according to Table 1 have been obtained according to the four switch combinations.



Sim_1: Simulated case 1-4, Mea_1: Measured case 1-4,
 Sim_2: Simulated case 5-10, Mea_2: Measured case 5-10,
 Sim_3: Simulated case 11-14, Mea_3: Measured case 11-14,
 Sim_4: Simulated case 15, Mea_4: Measured case 15

Figure 4: Return loss of the antenna.

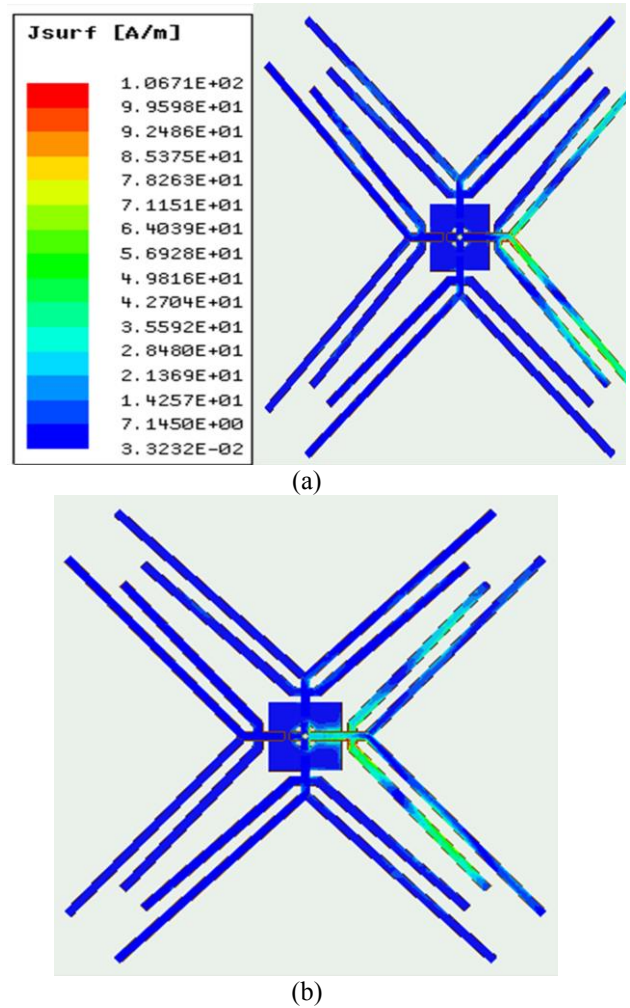


Figure 5: Simulated current distribution for case 1 (a) f_1 (b) f_2 .

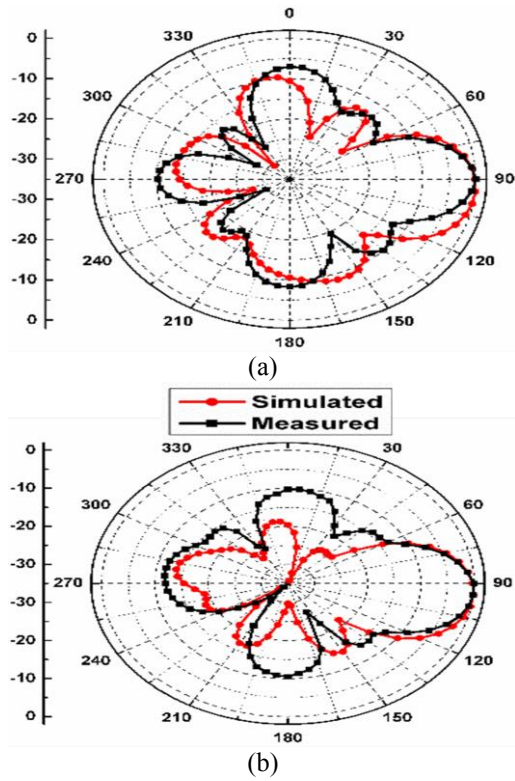


Figure 6: Radiation pattern in azimuth plane for case 1
(a) f_1 (b) f_2 .

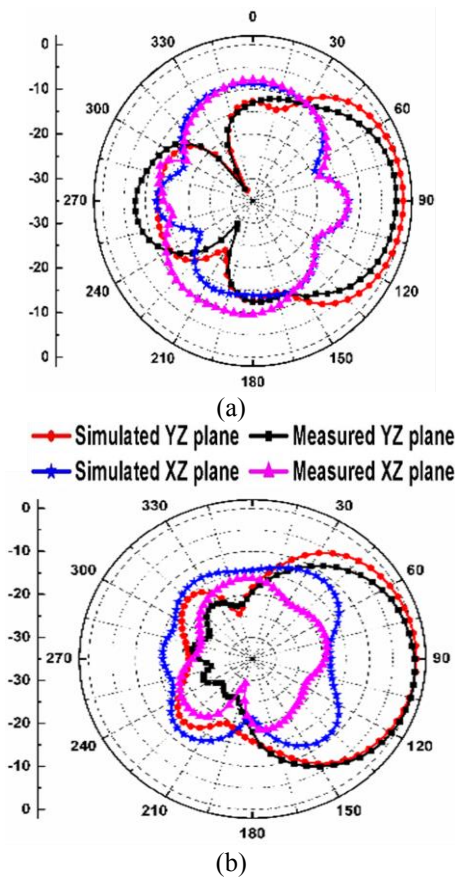
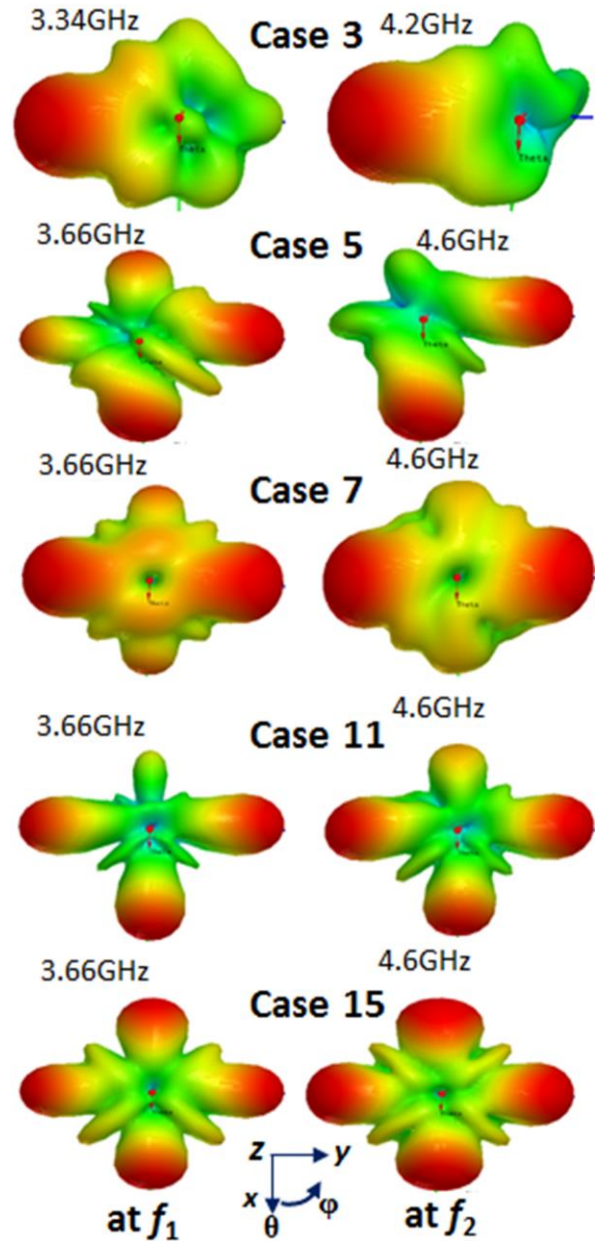


Figure 7: Radiation pattern in elevation plane for case 1
(a) f_1 (b) f_2 .



Note: Different scales are used to highlight the direction of max. radiation. Peak values are given in Table 2.

Figure 8: Simulated 3D radiation patterns.

When a single Vee dipole pair is activated, a directional pattern with an average half-power beam-width of 30° in azimuth is measured as shown in Fig. 6 at 3.3 GHz (f_1) and 4.11 GHz (f_2). Corresponding patterns in elevation plane are given in Fig. 7. When two switches are turned ON simultaneously, two sets of possible radiation patterns occur: one with peak radiation in opposite directions and another with peak radiation at perpendicular direction in the azimuth plane. The possible categories representative of single and multi-beam cases are illustrated by the 3D radiation patterns in Fig. 8 at f_1 and f_2 .

For all the switching configurations, the measured radiation patterns showed good correlation to the simulated

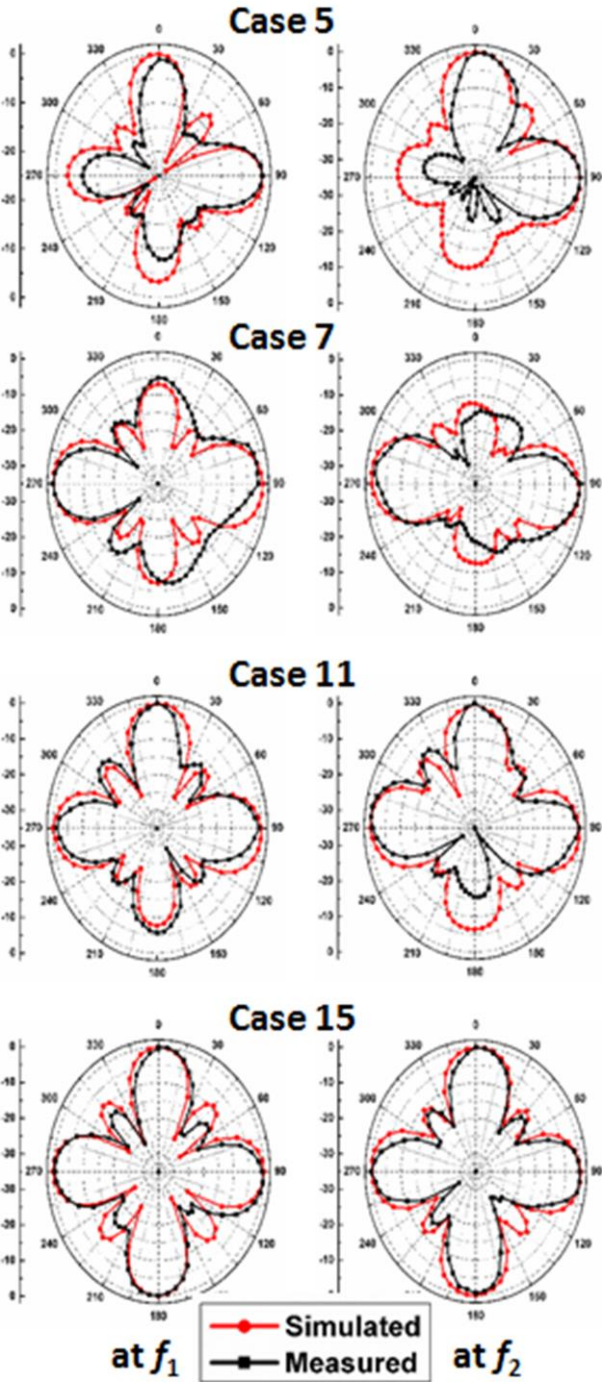


Figure 9: Measured and simulated radiation patterns in azimuth plane.

results as shown in Fig. 9 (azimuth: xy plane) and Fig. 10 (elevation plane). The centre frequencies for various configurations obtained during simulation and measurement are listed in Table 2. The antenna gain, directivity, efficiency and beam-width for the four categories of switch combinations are also consolidated in Table 2. Comparison of the proposed antenna to dual-band pattern diversity antennas already reported is given in Table 3.

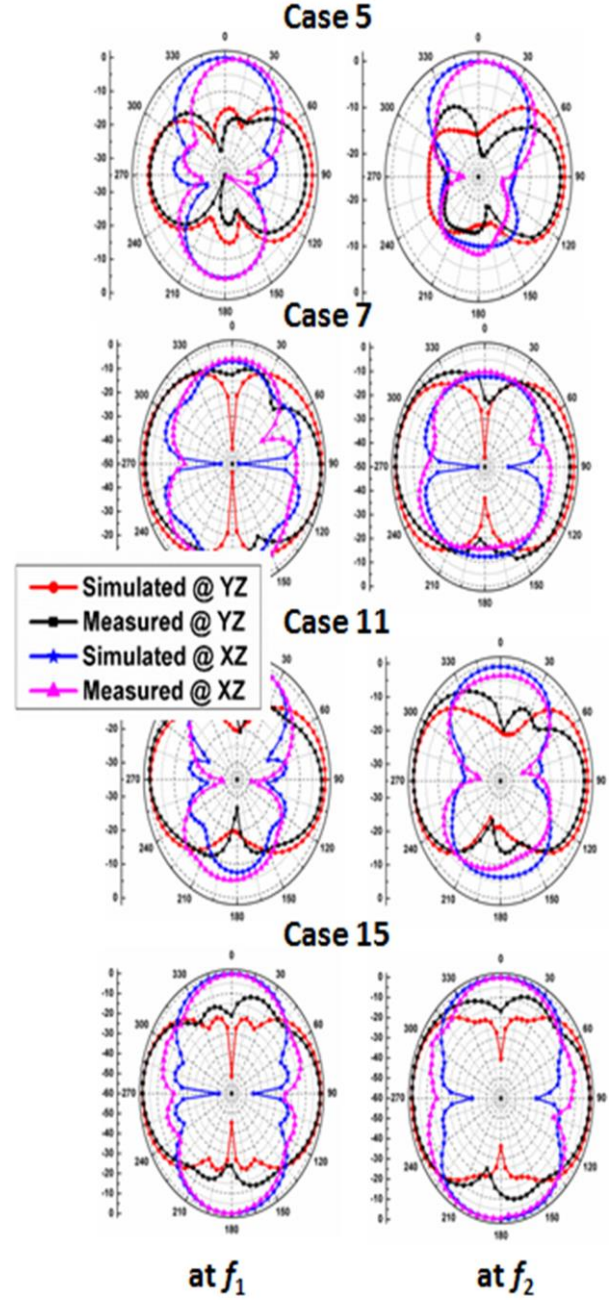


Figure 10: Measured and simulated radiation patterns in elevation plane.

Table 3: Comparison of the proposed antenna with the reported dual-band pattern diversity antennas.

Ref	Freq (GHz)	Switch	Size (λ_0)	No. of patterns
[8]	2.55/5.25	DPDT	1249	2
[9]	2.4/5.8	RF Switch	465	9
This work	3.6/4.6	PIN diode	88	15

Table 2 : Antenna parameters for different configurations

No. of switches ON	Centre Freq (GHz)	Centre Freq (GHz)		Peak gain (dBi)		Simulated directivity (dB)	Simulated Efficiency (%)	Beam-width ($^{\circ}$)	
		Simulated	Measured	Simulated	Measured			Simulated	Measured
1	f_1	3.34	3.30	7.82	7.23	8.61	83.79	35	30
	f_2	4.2	4.11	7.84	7.94	9.52	76.3	30	30
2	f_1	3.66	3.61	6.35	6.4	7.82	73.53	30-35	25-30
	f_2	4.6	4.51	4.57	3.91	7.69	67.16	35	30
3	f_1	3.66	3.66	3.41	3.78	7.97	73.2	30-35	20-30
	f_2	4.6	4.56	2.83	2.14	7.15	63.1	35	35
4	f_1	3.66	3.66	5.2	5.38	7.48	68.5	30	30
	f_2	4.6	4.6	2.22	2.06	6.24	61.6	30	25-30

4. Conclusions

A dual-band antenna based on printed Vee dipoles with multi-beam pattern reconfigurability feature is presented in this paper. The antenna is designed to have centre frequencies at 3.3 GHz and 4.2 GHz for single beam configurations and accordingly the multi-beam configuration showed resonance at 3.66 GHz and 4.6 GHz. Measured radiation patterns at both center frequencies validate the switching of patterns accomplished by electronically controlling the state of four PIN diodes. The antenna is shown to have peak radiation in the same directions for both frequencies, enabling concurrent dual-band communication between transmitter and receiver. A single substrate antenna without any complex feed circuitry makes this reconfigurable multi-beam antenna highly attractive to integrate into any concurrent dual-band communication system.

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