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Effect Of Various Process Parameters On Punch And Die Design In Deep Drawing Process

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Abstract: The model is designed in CREO software. Analysis is done in ANSYS software for different materials. In this work static analysis is done for cup and punch to determine the deformation, stress and strain at different load conditions and for different materials by changing the geometry thickness. In this work the stress have been calculated theoretically and as well as using ansys and both results are compared. Modal analysis is done for cup to determine the deformation and frequency for different materials by changing the geometry thicknesses. Random vibration analysis is done for cup to determine the directional deformation, shear stress and shear strain for different materials by changing the geometry thickness. In this work the shear stress have been calculated theoretically and as well as using ansys and both results are geometry thickness. In this work the shear stress have been calculated theoretically and as well as using ansys and both results are compared. Transient analysis is done for cup to determine the deformation, stress and strain for different materials by changing the geometry thickness with respect to time.

Keywords: Cup; Punch; Static Analysis; Random Analysis; CREO Parametric; ANSYS;

I. INTRODUCTION

Deep drawing is a sheet metal forming process in which a sheet metal blank is radially drawn into a forming die by the mechanical action of a punch. It is thus a shape transformation process with material retention. The process is considered "deep" drawing when the depth of the drawn part exceeds its diameter. This is achieved by redrawing the part through a series of dies. The flange region (sheet metal in the die shoulder area) experiences a radial drawing stress and a tangential compressive stress due to the material retention property. These compressive stresses (hoop stresses) result in flange wrinkles (wrinkles of the first order). Wrinkles can be prevented by using a blank holder, the function of which is to facilitate controlled material flow into the die radius as shown in Fig 1.1.



Fig 1.1 A Typical Deep Drawing Operation

1.2 Process of Deep Drawing

Commercial applications of this metal shaping process often involve complex geometries with straight sides and radii. In such a case, the term stamping is used in order to distinguish between the deep drawing (radial tension-tangential compression) and stretch-and-bend (along the straight sides) components. Deep drawing is always accompanied by other forming techniques within the press. These other forming methods include: **a. Beading:** Material is displaced to create a larger, or smaller, diameter ring of material beyond theoriginal body diameter of a part, often used to create O-ring seats.

b. Bottom Piercing: A round or shaped portion of metal is cut from the drawn part.

c. Bulging: In the bulging process a portion of the part's diameter is forced to protrude from the surrounding geometry.

d. Coining: Material is displaced to form specific shapes in the part. Typically coining should not exceed a depth of 30% of the material thickness.

e. Curling: Metal is rolled under a curling die to create a rolled edge.

f. Extruding: After a pilot hole is pierced, a larger diameter punch is pushed through, causing the metal to expand and grow in length.

g. Ironing / Wall Thinning: Ironing is a process to reduce the wall thickness of parts. Typically ironing should not exceed a depth of 30% of the material thickness.

h.Necking: A portion of the part is reduced in diameter to less than the major diameter.

i.Notching: A notch is cut into the open end of the part. This notch can be round, square, or shaped.

j. Rib Forming: Rib forming involves creating an inward or outward protruding rib during the drawing process.

k. Side Piercing: Holes are pierced in the side wall of the drawn part. The holes may be round or shaped according to specifications.



l.Stamping / Marking: This process is typically used to put identification on a part, such as a part number or supplier identification.

m.Threading: Using a wheel and arbor, threads are formed into a part. In this way threaded parts can be produced within the stamping press.

n. Trimming: In the Trimming process, excess metal that is necessary to draw the part is cut away from the finished part.

II. LITERATURE REVEIW

Some journal papers were selectively studied which have direct relevance with my work. A brief discussion is presented belowJay N.Mistri, K.D.Kothari,Gaurav, Kumar Sharma all[1], are discussed about Deep drawing is part of forming process in which sheet metal drawn into die cavity by action of a punch. So, due to action of punch desired shape can be achieved. For reduce various defects in deep drawing process it is essential to control or vary physical and geometric parameters of deep drawing process. Sheet-metal drawing is a more complex operation than cutting or bending, and more things can go wrong. Nowadays composite material is extensively used in manufacturing industries due to its better strength.

INTRODUCTION TO CAD

Computer-aided design (CAD) is using laptop structures (or workstations) to aid within the advent, change, analysis, or optimization of a layout. CAD software is used to increase the productiveness of the clothier, improve the great of layout, improve communications via documentation, and to create a database for production. CAD output is frequently within the form of digital documents for print, machining, or other manufacturing operations. The term CADD (for Computer Aided Design and Drafting) is also used.

INTRODUCTION TO CREO

Pro/ENGINEER Wildfire is the equal old in 3-d product layout, presenting employer-main productiveness equipment that sell outstanding practices in design on the identical time as making sure compliance together with your agency and business enterprise requirements. Integrated Pro/ENGINEER CAD/CAM/CAE answers can help you format quicker than ever, even as maximizing innovation and extraordinary to in the end create great merchandise.

Customer necessities might also additionally alternate and time pressures may additionally continue to mount, but your product layout desires remain the same - irrespective of your challenge's scope, you need the powerful, smooth-to-use, much less costly answer that Pro/ENGINEER provides.



Fig 3.1 2D Sketch of Cup



Fig 3.2 2D Sketch of Punch

By using PTC CREO Software, 3D Model of Cup and punch is developed. It is shown in Fig 3.3



Fig 3.3 3D Model of Cup



Fig 3.4 3D Model of Punch

INTRODUCTION TO FEA

Finite element evaluation is a technique of solving, normally approximately, certain problems in engineering and science. It is used specially for troubles for which no precise solution, expressible in a few mathematical shape, is available. As such, it is a numerical in preference to an analytical technique. Methods of this type are wanted due to the fact analytical strategies cannot cope with the real, complicated troubles which can be met with in engineering. For instance, engineering electricity of substances or the mathematical principle of elasticity may be used to calculate analytically the stresses and lines in a bent beam, but neither will be very successful in locating out what's going on in a part of a car suspension device for the duration of cornering.



3.2 THEORETICAL CALCULATIONS TO FIND THE STRESS OF CUP

$$F = \left(\frac{2}{\sqrt{3}}\right) \times \pi \times UTS \times D \times t$$
..... (Eq 3.1)

Where,

 $t_0 = thickness (mm)$

UTS =ultimate tensile strength (MPa)

Do = die diameter (mm)

Blank diameter =26

Punch diameter =25

Blank thickness =0.5,0.7,0.9

Radial clearance between punch and die radius =1.1

Punch nose radius =0.52

Parameters obtained from Sandeeppatil[29]

σ=F/A

-----(Eq 3.2)

A=333.923 mm²

Where,

 $\sigma = \text{stress} (\text{N/mm}^2)$

P = maximum load (N)

A = area (mm^2)

CASE 1-MATERIAL- STAINLESS STEEL

At t=0.5 mm, D_o=26 mm

$$=\left(\frac{2}{\sqrt{3}}\right) \times \pi \times 513.61 \times 26 \times 0.5/333.923$$

=62.5 MPa

At t=0.7 mm, D_o=26 mm

$$=\left(\frac{2}{\sqrt{3}}\right) \times \pi \times 513.61 \times 26 \times 0.7/333.923$$

=54.4 MPa

At t=0.9 mm, D_0 =26 mm

$$=\left(\frac{2}{\sqrt{3}}\right) \times \pi \times 513.61 \times 26 \times 0.9/333.923$$

=40.5 MPa

CASE 2-MATERIAL- AL 5083

At t=0.5 mm, D_o=26 mm

$$= \left(\frac{2}{\sqrt{3}}\right) \times \pi \times 228 \times 26 \times 0.5/333.923$$

=46 MPa

At t=0.7 mm, D_o=26 mm

$$= \left(\frac{2}{\sqrt{3}}\right) \times \pi \times 228 \times 26 \times 0.7/333.923$$

=45.07 MPa

At t=0.9 mm, Do=26 mm

$$= \left(\frac{2}{\sqrt{3}}\right) \times \pi \times 228 \times 26 \times 0.9/333.923$$

=32.199 MPa

CASE 3-MATERIAL- AL 7475

$$= \left(\frac{2}{\sqrt{3}}\right) \times \pi \times 345 \times 26 \times 0.5/333.923$$
$$= 63.2 \text{ MPa}$$

At t=0.7 mm, D_o=26 mm

$$=\left(\frac{2}{\sqrt{3}}\right) \times \pi \times 228 \times 26 \times 0.7/333.923$$

=62 MPa

At t=0.9 mm, Do=26 mm

$$=\left(\frac{2}{\sqrt{3}}\right) \times \pi \times 228 \times 26 \times 0.9/333.923$$

=48.7MPa

III. INTRODUCTION

ANSYS is wellknown-reason finite detail evaluation (FEA) software bundle. Finite Element Analysis is a numerical method of deconstructing a complicated system into very small pieces (of person-exact length) called factors. The software implements equations that govern the behaviour of these factors and solves all of them; creating a comprehensive clarification of ways the machine acts as a whole. These outcomes then can be offered in tabulated, or graphical forms. This kind of analysis is typically used for the layout and optimization of a machine some distance too complex to analyze by hand. Systems that may match into this category are too complicated due to their geometry, scale, or governing equations.

STATIC ANALYSIS OF CUP

Static structural analysis for deformation and stress are shown in Figure 3.5 and 3.6 respectively.



Fig 3.5 Deformation Contours of Cup



Fig 3.6 Stress Contours of Cup



From the Table 3.2 it can be seen that the stress value increases with increasing the load and decreases with increasing the thickness. The stress value occurred minimum for the material AL 5083 at 0.9 mm thickness for 1000N load.

Table 3.2 The Static Analysis Results Of Cup

Occurately (thickness)(rum)	Mainetal	CO	(mm)	(Norman2)	Strain
	Stanlass	1000	0.0022637	34.102	0.0010733
	steat	1300	0.0020420	34.542	0.00023831
		1600	0.003622	34.774	0.00031371
	AL 7475	1000	0.0061743	33.122	0.0005335
0.5		1300	0.0080266	34.009	0.00081354
		1800	6.6668780	34.176	0.00013339
	AL 1083	1000	0.0087666	31.717	0.0057929
		1300	0.0007063	31.832	0.00075638
		1600	0.010838	31.047	0.00002688
	Stainlass	1000	0.0016206	33.012	0.00015217
	steal	1300	0.0021164	33.992	0.00019782
		1600	0.0026073	34.001	0.00024343
	AL 7475	1000	0.004403	33.512	0.00041038
0.7		1300	0.0052400	33.613	0.00034543
		1600	0.0071585	33.812	0.000-07130
	AL 3083	1000	0.0045633	30.752	0.0004457
		1300	0.0063240	30.554	0.000320
		1600	0.0077845	30.042	0.00071312
	Stainless.	1000	0.0012615	33.717	0.00013207
	steal	1300	0.00164	33.815	0.00017180
		1600	0.0020185	33.905	0.00021131
	AL 7475	1000	0.0034362	33.532	8.66633294
0.9	1.200 2.002	1300	0.0044671	33.603	0.0004653
	and the second second	1600	0.003498	33.981	0.00053221
	AL 3010	1000	0.0037633	29.633	0.00038875
	Contraction of the	1300	0.0048923	29.635	0.00050538
	1	1600	0.0060213	29.639	0.000822

Below Table shows that static analysis fairly matches with the theoretical results

 Table 3.3 Comparison of Theoretical Stress And

 ANSYS Stress

Materials	Thickness (mm)	ANSYS stress (MPa)	Theoretical stress (MPa)
Stainlage	0.5	55.938	62.53
steel	0.7	46.736	54.4
	0.9	36.789	40.56
	0.5	57.736	63.2
AL 7475	0.7	56.206	62.02
	0.9	42.852	48.7
	0.5	39.994	46
AL 5083	0.7	38.925	45.07
	0.9	29.633	32.199

Summary:

According to the contours plot, the maximum stress at inside of the cup because of force acting on the area due to punch applied and the minimum stress at upside,down side and around the cup because of fixed the cup.

The stress value occurred minimum for the material AL 5083 at 0.9 mm thickness for 1000N load.

3.5 THEORETICAL CALCULATIONS TO FIND THE STRESS OF PUNCH

$$F = \left(\frac{2}{\sqrt{3}}\right) \times \pi \times UTS \times D \times t$$

σ=F/A, A=333.923 mm2

Stainless Steel

At t=0.5 mm, Dp=25 mm

$$=\left(\frac{2}{\sqrt{3}}\right) \times \pi \times 513.61 \times 25 \times 0.5/333.923$$

=59.74 MPa

At t=0.7 mm, Dp=25 mm

$$=\left(\frac{2}{\sqrt{3}}\right) \times \pi \times 513.61 \times 25 \times 0.7/333.923$$

=48.6 MPa

At t=0.9 mm, Dp=25 mm

$$= \left(\frac{2}{\sqrt{3}}\right) \times \pi \times 513.61 \times 25 \times 0.9/333.923$$

=42.54 MPa

AL 5083

At t=0.5 mm, Dp=25 mm

$$=\left(\frac{2}{\sqrt{3}}\right) \times \pi \times 228 \times 25 \times 0.5/333.923$$

=45.23 MPa

At t=0.7 mm, Dp=25 mm

$$=\left(\frac{2}{\sqrt{3}}\right) \times \pi \times 228 \times 25 \times 0.7/333.923$$

=42.4 MPa

At t=0.9 mm, Dp=25 mm

$$=\left(\frac{2}{\sqrt{3}}\right) \times \pi \times 228 \times 25 \times 0.9/333.923$$

=41.11 MPa

AL 7475

At t=0.5 mm, Dp=25 mm

$$= \left(\frac{2}{\sqrt{3}}\right) \times \pi \times 345 \times 25 \times 0.5/333.923$$
$$= 55.23 \text{ MPa}$$

At t=0.7 mm, Dp=25 mm

$$=\left(\frac{2}{\sqrt{3}}\right) \times \pi \times 228 \times 25 \times 0.7/333.923$$

=52.5 MPa

At t=0.9 mm, D_p=25 mm

$$=\left(\frac{2}{\sqrt{3}}\right) \times \pi \times 228 \times 25 \times 0.9/333.923$$

=46.84 MPa

3.6 STATIC ANALYSIS OF PUNCH

Static structural analysis of punch for deformation and stress are shown in Figure 3.7 and 3.8 respectively.



Fig 3.7 Deformation contours of Punch





Fig 3.8 Stress contours of Punch

From the Table 3.4 it can be seen that the stress value increases with increasing the load and decreases with increasing the thickness.

Geometry(thickness)	Material	Load	Deformation	Stress	Strain
Mm	104 NO20 0	(N)	(mm)	(N/mm2)	
	Stainless	1000	0.0019964	38.501	6.2184e-5
	steel	1300	0.0025953	38.601	8.0839e-5
	1	1600	0.0031942	38.942	9.941e-5
	AL 7475	1000	0.0054175	38.682	0.000166
		1300	0.00021627	38.755	0.0070428
0.5	31	1600	0.008668	38.950	0.00026618
	AL 5083	1000	0.0059065	38.155	0.00017879
		1300	0.0076285	38.185	0.00023242
		1600	0.0094504	38.289	0.00028260
	Stainless	1000	0.0020692	38.440	7.0734e-5
	steel	1300	0.00269	38.580	9.1955e-5
	25	1600	0.0033107	38.700	0.00011317
	AL 7475	1000	0.0056157	37.123	0.00018725
0.7	88	1300	0.0073004	37.550	0.00024408
		1600	0.0089852	37.990	0.0003004
	AL 5083	1000	0.0061234	37.601	0.0019974
	1	1300	0.0079604	37.500	0.00075966
	85	1600	0.0097974	37.405	0.0003458
	Stainless	1000	0.0020928	37.950	6.4738e-5
	steel	1300	0.0027206	37.828	8.416e-5
		1600	0.0033484	37.550	0.00010358
0.9	AL 7475	1000	0.00568	38.113	0.00016956
		1300	0.007384	37.520	0.0002043
		1600	0.009088	37.500	0.00027129
	AL 5083	1000	0.0061938	38.001	0.00017744
	8	1300	0.0080519	37.120	0.00023067
	25	1600	0.0099101	37.101	0.00028391

Material	Thickness (mm)	Theoretical Stress MPa	ANSYS Stress
	(11111)		MPa
Stainless Steel	0.5	59.74	45.125
Steel	0.7	48.6	40.123
	0.9	42.54	38.001
AL 5083	0.5	45.23	38.177
5005	0.7	42.4	38.152
	0.9	41.11	37.489
AL 7475	0.5	55.23	49.433
1713	0.7	52.5	46.233
	0.9	46.84	37.880

Summary:

According to the counters plot, the maximum stress at down side of the cup because of force acting on the area due to punch applied and the minimum stress at upside.

The stress value occurred minimum for the material AL 5083 at 0.9 mm thickness for 1000N load

IV. MODAL ANALYSIS OF CUP

The goal of modal analysis in structural mechanics is to determine the natural mode shapes and frequencies of an object or structure during free vibration. It is common to use the finite element method (FEM) to perform this analysis because, like other calculations using the FEM, the object being analyzed can have arbitrary shape and the results of the calculations are acceptable. The types of equations which arise from modal analysis are those seen in eigen systems. The physical interpretation of the eigen values and eigen vectorswhich come from solving the system are they represent the frequencies that and corresponding mode shapes. Sometimes, the only desired modes are the lowest frequencies because they can be the most prominent modes at which the object will vibrate, dominating all the higher frequency modes.

According to the counters plot, the maximum total deformation at around the cup because of force acting on the area due to punch applied and the minimum directional deformation at up and down side of the cup because of fixed the cup.

Modal analysis of cup for total deformation it is shown in Figure 4.1



4.1 Total Deformation contours

Here,Table4.1showndeformationofAL5083,AL7475andstainlesssteel,itcanbeseenthatthemaximumdeflection1692.4mmforAL7475andcorrespondingdeflectioninAL5083andStainlesssteelare1101mm,1019.4mm.

Material Mode shapes Deformation(mm) requenc (Hz) 084 27046 Stainless 959.2 2716 1019.4 AL 7475 1649.1 27522 0.5 1609 29463 1692.4 1077.5 1050.1 29113 AL 5083 16893 1101.1 17767 792.16 Stainless 845.6 36340 803.61 30512 AL 7475 1366.4 0.7 30812 1315 31061 AL 5083 838.2 18778 881.18 18800 18985 Stainless 732.96 38113 763.52 38341 681.83 39293 AL 7475 1243.5 39798 1282. 39201 0.9 AL 5083 818.6 2371 841.18 23853 756 53 24531

Table 4.1 Modal analysis results of cup

V. RANDOM VIBRATIONAL ANALYSIS OF CUP

The Random Vibration analysis uses the results from a modal analysis, specify which design



scenario in the current model has the modal results with the Use modal results from Design Scenario field.The Model Units of the random vibration analysis must be identical to the Model Units of the modal results.According to the counters plot, the maximum shear stress at inside of the cup because of force acting on the area due to punch applied and the minimum shear stress at upside ,down side and around the cup because of fixed the cup.

Random Vibration analysis of cup for Shear stress it is shown in Figure 5.1



Fig 5.1 Shear Stress contour

Here, Table 5.1 shown Shear stress of

AL5083,AL7475 and stainless steel, it can be seen that the minimum shear stress $1.5e^5N/mm2$ for AL5083 and corresponding shear stress in AL7475 and Stainless steel are $2.94e^5N/mm2$, $5.405e^5N/mm2$

The Shear stress value occurred minimum for the material AL 5083 at 0.9mm thickness

Geometry (thickness) (mm)	Material	Directional Deformation (mm)	Shear Stress (N/mm2)	Shear Strain
	Stainless steel	128.1	5.405e5	7.3382
0.5	AL 7475	191.79	2.945e5	11.046
1	AL 5083	116.86	2.642e5	6.7842
	Stainless steel	129.69	6.04e5	8.2066
0.7	AL 7475	249.98	4.28e5	15.899
-	AL 5083	113.21	1.651e5	7.1378
2.8	Stainless steel	2111.8	9.77e5	132.73
0.9	AL 7475	2831.2	4.72e5	177.8

Table 5.1 Random Vibration Analysis Results

5.1 THEORETICAL CALCULATIONS FOR SHEAR STRESS

1819

Shear stress (N/m²)

 $\tau = 4\mu u/(h-t),$ ----- (Eq 5.1)

u=Negligible

Stainless Steel--- $\mu = 0.3$

At t=0.5 mm, h=25.0484 mm

AL 5083

 $\tau{=}4\times0.3/(25.0484-0.5)$

 $=49.8 \ N/m^2$

At t=0.7 mm, h=25.0484 mm $\tau = 4 \times 0.3 / (25.0484 - 0.7)$ $=49.6 \text{ N/m}^2$ At t=0.9 mm, h=25.0484 mm $\tau = 4 \times 0.3 / (25.0484 - 0.9)$ =48.8 N/m² AL 5083--- $\mu = 0.129$ At t=0.5 mm, h=25.0484 mm $\tau = 4 \times 0.129 / (25.0484 - 0.5)$ =21.3 N/m² At t=0.7 mm, h=25.0484 mm $\tau = 4 \times 0.129 / (25.0484 - 0.7)$ =21.1 N/m² At t=0.9 mm, h=25.0484 mm $\tau = 4 \times 0.129 / (25.0484 - 0.9)$ $=21 \text{ N/m}^2$ AL 7475--- $\mu = 0.257$ At t=0.5 mm, h=25.0484 mm $\tau = 4 \times 0.257 / (25.0484 - 0.5)$ $=42.2 \text{ N/m}^2$ At t=0.7 mm, h=25.0484 mm $\tau = 4 \times 0.257 / (25.0484 - 0.7)$ $=42 \text{ N/m}^2$

At t=0.9 mm, h=25.0484 mm

 $\tau = 4 \times 0.257 / (25.0484 - 0.9)$

=41.8 N/m²

Below Table shows that theoretical results fairly matches with the ANSYS results

 Table 5.2 Comparison of Theoretical and ANSYS Shear Stress Values

Material	Thickness(mm	Ansys	Theoretical
s)	shear	shear
		stress(MPa	stress(MPa
))
Stainless	0.5	5.405×e ⁵	4.9800×e ⁵
steel	0.7	2.945×e ⁵	4.9600×e ⁵
	0.9	1.5×e ⁵	4.8800×e ⁵
AL 5083	0.5	6.04×e ⁵	2.1300×e ⁵
	0.7	4.28×e ⁵	2.1100×e ⁵
	0.9	1.651×e ⁵	2.1000×e ⁵
AL 7475	0.5	9.77×e ⁵	4.2340×e ⁵
	0.7	4.72×e ⁵	4.2200×e ⁵
	0.9	2.642×e ⁵	4.1800×e ⁵

Summary:

113.45

1.5e5



The Shear stress value occurred minimum for the material AL 5083 at 0.9mm thickness

VI. TRANSIENT ANALYSIS OF CUP

A transient dynamic analysis is used to determine the response of a structure subjected to a timedependent loading considering inertia and damping effects. It is often referred to as a time-history analysis. The full method in ANSYS uses the full system matrices to calculate the transient response at each solution point. The model-superposition method scales the mode shapes and sums them to capture the dynamic response.

Below Figures 6.1 to 6.3 shows the deformation of the cup at 10, 20 and 30 sec respectively for the given load.



Fig 6.1 Deformation of cup at 10 seconds.



Fig 6.2 Deformation of cup at 20seconds



Fig 6.3 deformation of cup at 30sec

Below Figure from 6.4 to 6.6 shows the maximum stress evaluated in cup at 10,20 and 30 sec for a given load.



Fig.6.4 Maximum stress of cup at 10 seconds.



Fig 6.5 Maximum stress of cup at 20 seconds.



Fig 6.6 Maximum stress of cup at 30 seconds.

Below Tables 6.1 to 6.3 shows the transient analysis results of cup. From the results table it can be seen that the deformation increases with respect to time and the difference in deformation value reduces with respect to time. Also the stress value increases with respect to the time and the difference in stress value decreases with respect to the time.

The stress value occurred minimum for the material AL 5083 at 0.9 mm, at 10sec.

Table 6.1 Transient Analysis of Stainless Steel

Geometry (thickness) mm	Time (sec)	Deformation (mm)	Stress (Nomm2)	Strain
	10	0.00310	25.2051	3.902e-04
0.5	20	0.0051328	31.5041	4.5056e-04
	30	0.004521	39.0025	5.562e-04
0.7	10	1.63e-03	21.2023	2.8700e-04
	20	2.216e-03	27.403	3.5332e-04
	30	2.82e-03	31,011	3.9053e-04
0.9	10	2.0107e-03	17.236	2.830e-04
	20	1.904e-03	19.330	3.0310e-04
	30	2.130e-03	22.3014	3.0338e-04

6.2 Transient Analysis of AL 7475

Geometry (thickness) mm	Time (sec)	Deformation (mm)	Stress (N/mm2)	Strain
	10	0.0024670	21.302	3.53e-04
0.5	20	0.0030458	27.9653	4.1072e-04
	30	0.003760	35.064	5.0015e-04
0.7	10	1.48e-03	18.1672	2.6710e-04
	20	1.906e-03	22.673	3.03512e-04
	30	2.64e-03	27.601	3.7532e-04
0.9	10	1.1205e-03	14.310	2.552e-04
	20	1.420e-03	16.521	2.7348e-04
	30	1.\$21e-03	19.6520	2.9238e-04

6.3 Transient Analysis of AL 5083

Geometry (thickness) mm	Time (sec)	Deformation (mm)	Stress (N/mm2)	Strain
	10	0.0021597	19.973	2.94e-004
0.5	20	0.0028076	25.965	3.8274e-04
	30	0.003454	31.957	4.7115e-04
0.7	10	1.44e-03	15.287	2.1808e-04
	20	1.876e-03	19.874	2.8352e-04
	30	2.30e-03	24.461	3.48966-04
0.9	10	1.0734±-03	11.239	1.649+04
	20	1.39e-03	14.611	2.1439e-04
	30	1.7174e-03	17.983	2.6357e-04

According to plot the maximum Shear stress of material at 0.9mm,Material Stainless Steel, minimum at 0.9 mm Material AL-5083, Here Material Thickness Increasing To Shear Stress Will Be Increasing it shown in Fig 6.7







VII. CONCLUSIONS AND FUTURE SCOPE OF WORK

Conclusions

- From the static analysis results of Cup, Punch it is seen that the stress values are increases by increasing the load and decreases with increasing the thickness and deformation values are increases by decreasing the loads at geometry thickness 0.9mm for AL 5083 material when we compare stainless steel and AL7475
- From the static analysis results of cup AL5083 material having minimum stress value 29.633N/mm² compared to AL7475 is 42.852N/mm²and stainless steel is 36.789N/mm²
- The static analysis of punch the stress values are increases by increasing and deformation values are increases by decreasing the loads at geometry thickness 0.9mm for AL 5083 material when we compare stainless steel and AL7475.
- From the static analysis results of punch AL5083 material having minimum stress value 37.489N/mm² compared to AL7475 is 37.880N/mm²and stainless steel is 38.001N/mm²
- The stress values are calculated using ansys as well as using theoretically for cup and punch.
- The modal analysis the deformation values are increases by decreasing the loads. The deformation increases by increasing the mode shapes of the die. The maximum deformation at geometry thickness 0.5mm for AL 7475.
- The random vibration analysis the shear strain value are increases by increasing the geometry thickness at 0.9 AL5083.
- The shearstress values are calculated using ansys as well as theoretically forcup.
- The transient analysis of cup the stress values are increases by increasing and deformation values are increases by decreasing the time at geometry thickness 0.9mm for AL 5083

material when we compare stainless steel and AL 7475.

• So it can be concluded the geometry thickness is 0.9mm and material is AL 5083 is best and punch material AL 5083 is the better material.

FUTURE SCOPE OF WORK

- Finite element analysis based simulation has been done using ANSYS for the single stage drawing process.
- The effect of parameters on the wrinkles, thinning and formability quality characteristics of single stage drawing process has been done.
- Further research is needed to study and develop predictive models for the other responses, such as bend allowance and residual stress for AL sheets.

VIII. REFERENCES

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