



Science Arts & Métiers (SAM)

is an open access repository that collects the work of Arts et Métiers Institute of Technology researchers and makes it freely available over the web where possible.

This is an author-deposited version published in: <https://sam.ensam.eu>
Handle ID: <http://hdl.handle.net/10985/16790>

To cite this version :

Benjamin JODAR, Gabriel SEISSON, David HÉBERT, Isabelle BERTRON, Michel BOUSTIE, Laurent BERTHE - Enhancement of a dynamic porous model considering compression-release hysteresis behavior: Application to graphite - Journal of Physics D: Applied Physics - Vol. Volume 49, Issue 32, p.Article number 325301 - 2016

Any correspondence concerning this service should be sent to the repository

Administrator : archiveouverte@ensam.eu



Enhancement of a dynamic porous model considering compression-release hysteresis behavior: application to graphite

B Jodar¹, G Seisson², D Hébert¹, I Bertron¹, M Boustie³ and L Berthe⁴

¹ CEA CESTA, 15 avenue des Sablières CS60001, 33116 Le Barp Cedex, France

² CEA DIF, Bruyères-le-Châtel, 91297 Arpajon Cedex, France

³ Institut P' UPR3346 CNRS-ENSMA-Université de Poitiers, 1 avenue Clément Ader, 86961 Futuroscope Cedex, France

⁴ Laboratoire PIMM UPR8006 CNRS-Arts et Métiers ParisTech, 151 boulevard de l'Hôpital, 75013 Paris, France

E-mail: gabriel.seisson@cea.fr (G. Seisson)

Abstract

Because of their shock wave attenuation properties, porous materials and foams are increasingly used for various applications such as graphite in the aerospace industry and polyurethane (PU) foams in biomedical engineering. For these two materials, the absence of residual compaction after compression and release cycles limits the efficiency of the usual numerical dynamic porous models such as P - α and POREQST. In this paper, we suggest a simple enhancement of the latter in order to take into account the compression-release hysteresis behavior experimentally observed for the considered materials. The new model, named H-POREQST, was implemented into a Lagrangian hydrocode and tested for simulating plate impact experiments at moderate pressure onto a commercial grade of porous graphite (EDM3). It proved to be in far better agreement with experimental data than the original model which encourages us to pursue numerical tests and developments.

Keywords: POREQST, P - α , carbon, foam, constitutive relation

(Some figures may appear in colour only in the online journal)

1. Introduction

The shock wave attenuation capability of foams and porous materials is one of the main research topics in preventing damage caused by the propagation of shock waves. The mechanisms responsible for the shock wave attenuation in such materials are not yet completely understood nor described. For instance, a porous graphite similar to those used in the aerospace industry as a constitutive element of C/C composite materials, revealed no residual compaction after static confined compression (see figure 1 and [1]). In biomedical engineering, polyurethane (PU) foams, used as a specimen to understand shock interaction with complex media, showed a similar behavior during uniaxial-strain experiments (see figure 1(b) and [2]). This particular behavior is also expected during shock wave propagation. The concern of this paper is to pave the way

for developing a numerical model able to correctly reproduce such complex mechanisms under shock-and-release loading.

To describe the dynamic behavior of porous materials, several numerical models have been developed during the last decades. Among them, the simplest one is the 1D model of Thouvenin [3]. It can be called a geometric model since it consists in describing a porous material as an assembly of parallel slabs of dense matter. The ratio between the slab thickness and the empty spaces between them is related to the macroscopic density of the material. It originally gave good results for sustained shocks onto porous metals but was also tested for laser-induced shocks onto aluminum [4] and porous graphite [5]. Nevertheless, its validity is limited to a range of pressures where compaction is complete and where materials do not undergo phase transition since it assumes the symmetry of the Hugoniot and the release isentrope.

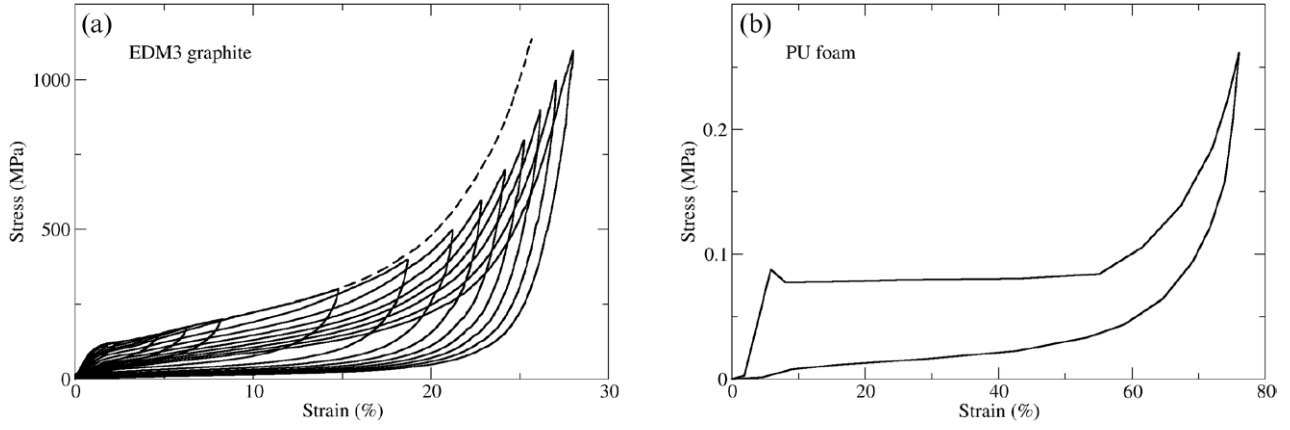


Figure 1. Highlighting of the compression-release hysteresis phenomenon for polycrystalline porous graphite and polyurethane foam. For both materials, no residual compaction exists after compression (at least up to 1.1 GPa for EDM3 and 0.26 MPa for PU foam). (a) Uniaxial strain tests in compression (dashed) and cycled compression and release (solid) onto an isotropic porous grade of graphite. Adapted from [1]. (b) Uniaxial strain test in compression and release onto a PU foam. Extracted with permission from [2]. Copyright 2006 Springer-Verlag.

Conversely, nongeometric models such as those expressed by Zel'dovich and Raizer [6], McQueen *et al* [7] and Charakhch'yan [8–10] allow 2D and 3D computations. They suppose an almost instantaneous density transition between the initial porous state and the solid state. Hence, they have the property to correctly deal with high-pressure phase transitions but cannot properly manage low-pressure ranges where compaction is uncomplete.

The P - α model, firstly introduced by Herrmann [11], is certainly the most known and used porous model in the literature. It is also able to deal with phase transition and palliates the lacuna of the models of Thouvenin, Zel'dovich, McQueen and Charakhch'yan when compaction is uncomplete. It uses a plastic compaction curve that manages the gap between the initial porous state to the dense one. The totally compacted material is modeled by the original dense equation of state (EOS). After a partial compaction, the return to a zero-pressure state is performed following elastic surfaces. Several developments of this model were then proposed, e.g. [12, 13], but none of them accounted for a potential hysteresis behavior.

The POREQST model expressed by Seaman *et al* [14] is based on fundamentals similar to P - α but the compaction curve is easier to fit on experimental data. Moreover, the elastic surfaces are defined by a Mie–Grüneisen EOS that allows computing time to be saved since the porosity is analytically calculated instead of with an algorithm like for P - α . It is also able to deal with negative pressures introducing a pore re-opening curve and all of its parameters have a physical meaning, most of them being obtainable at the first order by quasi-static tests. Extensive investigations have already been conducted by the present authors [1, 5, 15–17] on this model in order to shape a set of parameters adapted to the commercial grade of porous graphite evoked in figure 1. Therefore POREQST has been chosen for being enhanced in order to reproduce a compression-release hysteresis behavior.

The next section recalls the main features of the original POREQST model before proposing a substantial modification for the representation of the compression-release hysteresis behavior. The third section will adjust the new model, called

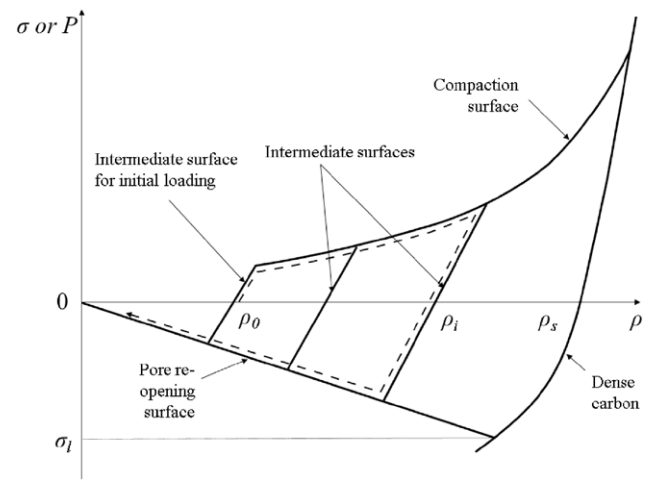


Figure 2. Schematic of the original POREQST model adapted from [14] in the zero internal energy plane. The dashed arrow depicts a typical compression-tension path (without damage model).

H-POREQST, for a commercial grade of graphite (EDM3) and discuss its limitations and benefits.

2. Enhancement of POREQST

2.1. Original model

The original POREQST model [14] is implemented into Hésione, a Lagrangian–Eulerian hydrocode developed at CEA. It supplies constitutive relations for porous materials submitted to dynamic loading. Figure 2 presents an overview of its features in the zero internal energy plane.

2.1.1. Dense material. Let ρ_s be the initial density of the dense (or solid) material at zero pressure P and internal energy e . The EOS of the solid can be any tabulated EOS such as a SESAME or a Mie–Grüneisen expressed as follows:

$$P_s(\rho, e) = K_s \left(\frac{\rho}{\rho_s} - 1 \right) \left(1 - \frac{\Gamma}{2} \left(\frac{\rho}{\rho_s} - 1 \right) \right) + \Gamma \rho e \quad (1)$$

with ρ the current density, K_s the dense compressibility modulus and Γ the Grüneisen coefficient of the solid which is assumed to be constant. The two parameters of the elastic-plastic behavior law are tabulated and depend on P and e :

- $Y_s(P, e) = Y_s(P)f_1(e)$: the elastic limit of the solid;
- $G_s(P, e) = G_s(P)f_2(e)$: its shear modulus.

f_1 and f_2 are tabulated softening functions varying between 0 for the melting internal energy and 1 for a zero energy.

2.1.2. Porous material. The porous material is represented as a succession of intermediate elastic surfaces that are delimited by two other surfaces, one accounting for its compaction and the other modeling the pore re-opening.

Intermediate surfaces. The first of the intermediate surfaces i is the elastic surface of the porous material. Their density at zero pressure and energy, called intermediate density, is denominated ρ_i . Along these intermediate surfaces, the pressure is also expressed thanks to a Mie-Grüneisen EOS:

$$P_i(\rho, e, \rho_i) = K_i \left(\frac{\rho}{\rho_i} T_f - 1 \right) \quad (2)$$

with

$$T_f = 1 + \frac{\Gamma \rho_s e}{K_s}, \quad K_i = \frac{K_s f_3(e)}{\alpha_i + L_1(\alpha_i - 1)}, \quad L_1 = \frac{K_s/K_0 - \alpha_0}{\alpha_0 - 1} \quad (3)$$

where T_f is a term of thermal dilatation which is constant whatever the intermediate surface. f_3 (as the following functions f_i of the model) is a tabulated softening function similar to f_1 and f_2 . Moreover, we define $\alpha_i = \rho_s/\rho_i$ as the material distension of the porous material at the intermediate density ρ_i . In the specific case of the first intermediate surface, i.e. the initial elastic surface of the porous material, we have $K_i = K_0$, $\rho_i = \rho_0$ and then $\alpha_i = \alpha_0 = \rho_s/\rho_0$. Note that the hidden hypothesis is that the dilatation coefficient at zero pressure is the same whatever the intermediate surface. It means that the volume V is written as:

$$V = V_i(1 + \alpha_i \Delta T) \quad \text{with} \quad \alpha_i = \frac{\Gamma \rho_s C_p}{K_s}. \quad (4)$$

As regards the deviatoric stress, the elastic limit and the shear modulus progress according to the intermediate density and the internal energy in the same way as the compressibility modulus:

$$Y_i = \frac{Y_s f_4(e)}{\alpha_i + L_2(\alpha_i - 1)} \quad \text{with} \quad L_2 = \frac{Y_s/Y_0 - \alpha_0}{\alpha_0 - 1} \quad (5)$$

$$G_i = \frac{G_s f_5(e)}{\alpha_i + L_3(\alpha_i - 1)} \quad \text{with} \quad L_3 = \frac{G_s/G_0 - \alpha_0}{\alpha_0 - 1}. \quad (6)$$

Thereby, when $\alpha_i = \alpha_0$ we obtain the initial values Y_0 and G_0 corresponding to the initial porous material; when $\alpha_i = 1$, we have the values of the solid material Y_s and G_s .

Delimitation of the intermediate surfaces. Assuming a positive stress in compression, it follows that:

$$\bar{\sigma} = P\bar{I} - \bar{S} \quad \text{with} \quad \text{tr}(\bar{S}) = 0. \quad (7)$$

In the principal system, let the extrem deviatoric stresses be:

$$S_{\max} = \max(S_i)_{i=1,3} \quad \text{and} \quad S_{\min} = \min(S_i)_{i=1,3}. \quad (8)$$

In compression, the limitation of the intermediate surfaces is fulfilled by a compaction surface described by:

$$\sigma_c(\rho, e) = \Sigma_c(\rho)f_6(e) \quad (9)$$

where $\Sigma_c(\rho)$ results from experimental data of a static uniaxial strain test in compression of the healthy porous material such as displayed in figure 2 (dashed line).

In traction, the limitation is undertaken by a pore re-opening curve whose intersect at zero energy with the dense material surface occurs at $(\rho_i; \sigma_i)$:

$$\sigma_o(\rho, e) = \Sigma_o(\rho)f_7(e)T_f \quad \text{with} \quad \Sigma_o(\rho) = \rho \frac{\sigma_i}{\rho_i} \quad (10)$$

σ_i being the main parameter of this surface. Note that in practice, $f_3(e) = f_6(e) = f_7(e)$.

2.1.3. General algorithm. Then, it is necessary to perform a series of tests (see algorithm 1) in order to establish what value of the pressure the code must use. For that purpose, we note ID the index characterizing the behavior pattern:

- $ID = 0$: no change of intermediate surface;
- $ID = 1$: pore re-opening;
- $ID = 2$: compaction;
- $ID = 3$: complete densification.

2.1.4. Damage criterion and treatment. The typical compression-tension path drawn in figure 2 (dashed arrow) indicates that, without failure model, tension may lead to very low and inconsistent local densities. Therefore, let a failure criterion be defined as follows:

$$\text{If } ID = 1, \quad \alpha_{\text{lim}} \leq \frac{\rho_s}{\rho_i} = \alpha_i. \quad (11)$$

It means that damage is activated when both of the following conditions are met: (1) the matter in a Lagrangian cell has a negative pressure located on the pore re-opening surface of the POREQST model (i.e. $ID = 1$); (2) the intermediary distension in this cell is higher than the critical value α_{lim} . In that case, pressure and deviatoric stress are relaxed to zero, and a damage variable D is set to 1. Then in each cell, σ_i is maintained to its original value if $D = 0$ or set to 0 if $D = 1$, which is equivalent to withdrawing the local tension strength of the damaged material.

2.2. New model: H-POREQST

The original POREQST (just as the P - α model and its derivatives) obviously predicts a residual compaction after compression. As written in the introduction, this is not realistic regarding the available data for such materials as graphite and polyurethane foams which present compression-release hysteresis cycles.

Algorithm 1. General algorithm of POREQST, where e_{melt} is the assumed-constant melting energy by volume unit.

```

begin
  ID ← 0;
  If  $e \geq e_{\text{melt}}$  then
    /* Use the dense EOS */
     $P \leftarrow P_s(\rho, e)$ 
    ID ← 3
  else
    /* Research of the correct pressure expression */
    If  $P_s(\rho, e) - S_{\text{max}} < \sigma_o(\rho, e)$  and  $P_s(\rho, e) - S_{\text{max}} < \sigma_o(\rho, e)$  then
       $P \leftarrow \sigma_o(\rho, e) + S_{\text{max}}$ ;
      ID ← 1;
    end
    If  $P_s(\rho, e) > P_i(\rho, e)$  and ID = 0 then
       $P \leftarrow P_s(\rho, e)$ ;
      ID ← 3;
    end
    If  $P_s(\rho, e) - S_{\text{min}} > \sigma_c(\rho, e)$  and ID = 0 then
       $P \leftarrow P_s(\rho, e)$ ;
      ID ← 3;
    end
    If  $P_i(\rho, e) - S_{\text{min}} > \sigma_c(\rho, e)$  and ID = 0 then
       $P \leftarrow \sigma_c(\rho, e) + S_{\text{min}}$ ;
      ID ← 2;
    end
    If  $P_i(\rho, e) - S_{\text{min}} < \sigma_c(\rho, e)$  and ID = 0 then
       $P \leftarrow P_i(\rho, e)$ ;
      ID ← 0;
    end
  end
  end
  If ID = 1 or ID = 2 then
    /* Deduce the new intermediate surface */
     $\rho_i \leftarrow (K_s f_1(e) \rho T_f - P \rho_s (1 + L_1)) / (K_s f_1(e) - P L_1)$ ;
  end
end

```

This work suggests an enhancement of the original POREQST model adapted to materials that experience compression-release hysteresis cycles and calls it H-POREQST (i.e. hysteresis-POREQST). For consistency with the phenomenological framework of the original model, we introduce a simple plane surface denominated hysteresis surface as shown in figure 3. It is only defined by the parameter σ_h which refers to its intersection with the dense EOS in the zero internal energy plane and its equation is given by:

$$\sigma_{\text{hys}}(\rho, e) = \Sigma_h(\rho) f_8(e) \quad \text{with} \quad \Sigma_h(\rho) = \sigma_h \left(\frac{\rho T_f - \rho_0}{\rho_h - \rho_0} \right) \quad (12)$$

where ρ_h is the density of the intersection point and T_f the same thermal dilatation coefficient defined by equation (3). A numerical adjustment of the parameter σ_h will be required to reproduce the experiments. Henceforth, pressure relaxation follows successively the intermediary and the hysteresis surfaces that involves two distinct ranges of release wave velocity.

Tension is only permitted when the current density is smaller than the initial one, i.e. as long as the distension is greater than $\alpha_0 = \rho_s / \rho_0$. In that case, the pressure evolution

will follow the negative part of the hysteresis surface. This behavior is not well-suited for a tensile initial loading but might be appropriate for tension after a compression-release cycle during which the microstructure of the material may have changed. Hence, H-POREQST must be considered relevant only for computations without initial tension. Algorithm 2 gives the series of tests necessary to implement the new model (the dissimilarities with the original POREQST are in blue) thanks to a new index of behavior pattern defined as:

- ID = 4: hysteresis.

Finally, just as POREQST, our new model will encounter density anomalies in tension. To avoid this phenomenon, the damage criterion and treatment enunciated in section 2.1.4 are also used with H-POREQST. Hence, α_{lim} is set to 1, meaning that pore re-opening is never authorized.

3. Application to graphite and discussion

The EDM3, a polycrystalline graphite produced by sintering, is manufactured by the compagny POCO [18, 19]. Its porosity

Algorithm 2. General algorithm of H-POREQST, where e_{melt} is the assumed-constant melting energy by volume unit. In blue are the dissimilarities with the original POREQST.

```

begin
  ID ← 0;
  If  $e \geq e_{\text{melt}}$  then
    /* Use the dense EOS */
     $P \leftarrow P_s(\rho, e)$ 
    ID ← 3
  else
    /* Research of the correct pressure expression */
    if  $P_i(\rho, e) - S_{\text{max}} < \sigma_o(\rho, e)$  and  $P_s(\rho, e) - S_{\text{max}} < \sigma_o(\rho, e)$  then
       $P \leftarrow \sigma_o(\rho, e) + S_{\text{max}}$ ;
      ID ← 1;
    end
    if  $P_i(\rho, e) - S_{\text{max}} < \sigma_{\text{hys}}(\rho, e)$  and  $\sigma_o(\rho, e) < \sigma_{\text{hys}}(\rho, e)$  then
       $P \leftarrow \sigma_{\text{hys}}(\rho, e) + S_{\text{max}}$ ;
      ID ← 4;
    end
    if  $P_s(\rho, e) > P_i(\rho, e)$  and ID = 0 then
       $P \leftarrow P_s(\rho, e)$ ;
      ID ← 3;
    end
    if  $P_s(\rho, e) - S_{\text{min}} > \sigma_c(\rho, e)$  and ID = 0 then
       $P \leftarrow P_s(\rho, e)$ ;
      ID ← 3;
    end
    if  $P_i(\rho, e) - S_{\text{min}} > \sigma_c(\rho, e)$  and ID = 0 then
       $P \leftarrow \sigma_c(\rho, e) + S_{\text{min}}$ ;
      ID ← 2;
    end
    if  $P_i(\rho, e) - S_{\text{min}} < \sigma_c(\rho, e)$  and ID = 0 then
       $P \leftarrow P_i(\rho, e)$ ;
      ID ← 0;
    end
  end
  If ID = 1 or ID = 2 or ID = 4 then
    /* Deduce the new intermediate surface */
     $\rho_i \leftarrow (K_s f_1(e) \rho T_f - P \rho_s (1 + L_1)) / (K_s f_1(e) - P L_1)$ ;
  end
end

```

(i.e. $1 - \rho_0/\rho_s$) is about 20% and it is macroscopically homogeneous and isotropic. Characterization tests were conducted by the present authors [1, 5, 16] in order to investigate its behavior under quasi-static and dynamic loading. Quasi-static confined compression-release cycles revealed a hysteresis behavior, as displayed in figure 1(a). In the case of dynamic loadings, the release waves are expected to be governed by this phenomenon inducing two distinct ranges of velocities. Furthermore, the experiment tends to show that the density of EDM3 returns to its initial value after compression, i.e. EDM3 does not experience residual compaction.

3.1. EDM3 modeling

The main parameters used for modeling EDM3 with POREQST and H-POREQST are given in table 1. The dense EOS is the tabulated SESAME 7832 of carbon, the compaction

curve is adapted from the dashed line of figure 1(a), and the intermediate surfaces are defined through the elastic moduli K and G . The deviatoric stress is constrained by the Von-Mises criterion and the elastic limit Y . Note that G_s and Y_s are tabulated piecewise-linear functions of the pressure. The value of the parameter σ_l is set to -95 MPa in order to make the intersect between the pore re-opening surface and the initial intermediate surface at zero energy to be equal to -70 MPa, which is the tension strength of healthy EDM3 [1]. The limit distension α_{lim} is set to 1, i.e. the condition of equation (11) is always fulfilled. Thus, the use of the pore re-opening surface is totally prohibited, thereby transcribing the brittleness of the material (fracture toughness of about $1 \text{ MPa} \cdot \text{m}^{1/2}$ [20–25]). Last, the unique parameter of the hysteresis surface σ_h is equal to 200 MPa (see section 3.2).

As shown in figure 4, this set of parameters allows a satisfying match between the test from figure 1(a) and its simulation

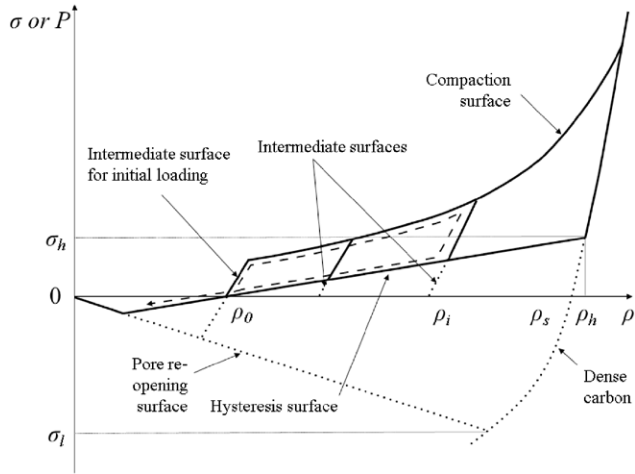


Figure 3. Schematic of the new H-POREQST model in the zero internal energy plane. The dashed arrow depicts a typical compression-tension path (without damage model). Dotted lines are unusable surface parts.

Table 1. Main parameters used for computations with POREQST and H-POREQST performed in section 3.2.

Dense graphite EOS	SESAME 7832	
Compaction curve	figure 1 ^a	
Pore re-opening parameter σ_l (MPa)	-95 ^a	
Hysteresis parameter σ_h (MPa)	200	
Softening function $f_l(e)$	Linear	
Initial densities (kg m^{-3})	Porous ρ_0	1754 ^a
	Dense ρ_s	2250 ^c
Compressibility modulus (GPa)	K_0	8.58 ^a
	K_s	34.05 ^c
Shear modulus (GPa)	G_0	5.01 ^a
	$G_s(P=0)$	20 ^a
	$G_s(P=18 \text{ GPa})$	50 ^a
	$G_s(P=27.5 \text{ GPa})$	280 ^a
Elastic limit (GPa)	Y_0	0.1 ^b
	$Y_s(P=0)$	0.1 ^b
	$Y_s(P=25 \text{ GPa})$	5 ^b
Limit distension α_{lim}	1	

^a Data extracted from [1].

^b Data from [26].

^c Values deduced from the SESAME 7832 table.

up to 1 GPa with H-POREQST and the hydrocode Hésione. It was a prerequisite prior to simulating dynamic experiments.

3.2. Plate impact test

In order to appraise H-POREQST, two experiments with EDM3 samples have been performed. Both consisted in a 2 mm-thickness copper plate launched at 330 m s^{-1} by a mono-stage light-gas gun onto a 3 mm-thickness plate of graphite. A PDV probe [27–29] recorded the rear free surface velocity of the latter. Since the experiments were perfectly repeatable only one velocity is displayed in figure 5(a) (circles).

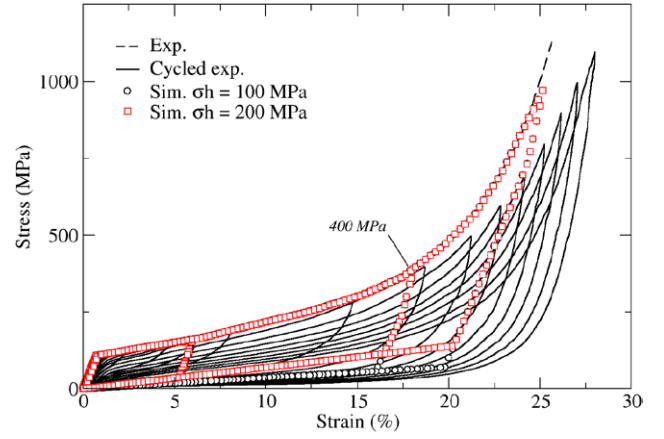


Figure 4. Comparison between the quasi-static cycled test from figure 1 and its simulation with H-POREQST and Hésione using the parameters of EDM3 from table 1. As an illustration of the discussion of section 3.3, both simulations with $\sigma_h = 100 \text{ MPa}$ (black rounds) and with $\sigma_h = 200 \text{ MPa}$ (red squares) are given. Discontinuities in the slope of the intermediate surfaces are logically due to the elastoplastic modeling.

Numerical simulations were performed with Hésione in a planar 1D Lagrangian configuration. The maximum generated stress onto the graphite target rear face was around 400 MPa. It allowed the model to be tested in the middle range of the static uniaxial compression data of figure 1.

Results are given in figure 5(a). The continuous line gives the rear surface velocity of EDM3 obtained with the original model of POREQST associated to the damage model presented in section 2.1.4, whilst the dotted lines display signals computed with the model H-POREQST with the same damage model. In both case, the curve foot is squared due to the successive rebounds of the shock elastic precursor on the rear surface of the target corresponding to the elastic initial surface of the models. Throughout an adjustment of the value of σ_h was set to 200 MPa, the new model clearly improves the first peak of the free-surface velocity. Furthermore, the pull-back phenomenon is well reproduced and the spall ejection velocity satisfactorily oscillates around the experimental signal.

3.3. Discussion

The increase of the maximum free surface velocity up to the experimental level induced by H-POREQST confirms that hysteresis behavior also occurs in the dynamic regime. It is well understood thanks to figure 5(b) which gives the numerical σ - u diagram of the target recorded close to the back face, u being the particle velocity and σ the longitudinal stress. The target undergoes a non-monotonic compression (because of the rebounds of the elastic precursor on the back face) (1) up to a maximum stress of about 400 MPa (2). The shock break-out on the rear surface involves a stress decrease (3) whose shape depends on the model. Original POREQST implies a straight-like pressure decay (plain) due to the intermediate surfaces generating a low free surface velocity around 360 m s^{-1} . Whereas H-POREQST implies an upper free surface velocity around 450 m s^{-1} coming from the two-straight-part pressure

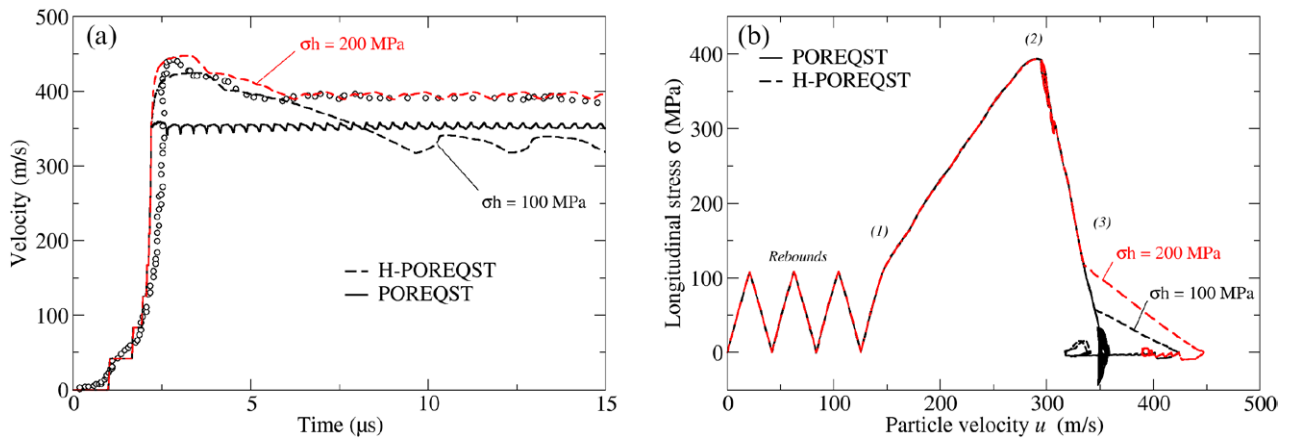


Figure 5. Comparison between the original model and the enhanced one in the case of a plate impact experiment on EDM3 with spallation. (a) Experimental free surface velocity of the EDM3 target compared to the simulations results with POREQST and H-POREQST. (b) σ - u diagram of the experiment extracted from numerical simulations (with artificial viscosity [30]). Comparison between POREQST and H-POREQST.

decrease (dashed) related to the intermediate and hysteresis surfaces.

According to the hysteresis cycle of figure 1 reaching 400 MPa (i.e. the maximum stress endured by the target back face during the plate impact experiment), the adjusted value of σ_h (200 MPa) should be more around 100–150 MPa, a value more or less confirmed by the simulation of the quasi-static test displayed in figure 4. Nonetheless, it does not give the best result for the dynamic experiment as shown in figure 5(a). There are three hypotheses that may explain this discrepancy: (1) the material has been softened by the first cycles of the static test; (2) a dynamic hardening of the target occurs during the plate impact experiment; (3) the linear modeling of the lower part of the hysteresis (intermediate and hysteresis surfaces) is not representative enough.

However, despite the simplicity of the modeling, the overall agreement between the experiment and the computation with H-POREQST is very satisfactory which paves the way for potential further improvements, when more various experimental results will be available.

4. Conclusion

The purpose of this paper was to enhance the POREQST model in order to be able to numerically reproduce the assumed density recovery after shock compression of certain porous materials and foams.

Hence, we introduced a new constitutive surface beside the original ones and called it the hysteresis surface that is defined through a single parameter. This simple modeling was tested for plate impact experiments on EDM3, a commercial porous graphite. It clearly improved the target free surface velocity first peak as well as the spall phenomenon and its flight average velocity, thereby confirming the existence of the hysteresis behavior under dynamic shock-and-release loading.

Finally, testing this model on more different loading cases (unsustained shock, compression up to higher pressures and release, etc) might be relevant for its improvement and validation. Then, the new H-POREQST model should be tested

for computing hypervelocity impacts of steel spheres into graphite [26, 31] where it may help to simulate the crater refill phenomenon observed experimentally.

Acknowledgments

The authors express their gratitude to the team of the Complexe 500 at CEA CESTA for having performed the plate impact experiments.

References

- [1] Seisson G 2014 Experimental and theoretical study of the damaging of graphite under dynamic loading—application to hypervelocity impacts *PhD Thesis* ISAE-ENSMA École Nationale Supérieure de Mécanique et d'Aérotechnique—Poitiers <https://tel.archives-ouvertes.fr/tel-01127342>
- [2] Kitagawa K, Yasuhara M and Takayama K 2006 Attenuation of shock waves propagating in polyurethane foams *Shock Waves* **15** 437–45
- [3] Thouvenin J 1966 Action d'une onde de choc sur un solide poreux *J. Phys.* **27** 183–9
- [4] Zagouri D, Romain J P, Dubrujeaud B and Jeandin M 1991 Laser shock compaction of porous materials *J. Phys. IV France* **01** 47–50
- [5] Hébert D, Seisson G, Bertron I, Chevalier J M, Thessieux C, Quessada J H and Tastet S 2014 Plate impact experiments and simulation on porous graphite *J. Phys.: Conf. Ser.* **500** 182016
- [6] Zel'dovich Y B and Raizer Y P 1967 *Physics of Shock Waves and High-Temperature Hydrodynamic Phenomena* vol 2 (New York: Academic)
- [7] McQueen R G, Marsh S P, Taylor J W, Fritz J N and Carter W J 1970 The equation of state of solids from shock wave studies *High Velocity Impact Phenom.* **293** 293–417
- [8] Khishchenko K V, Charakhch'yan A A, Fortov V E, Frolova A A, Milyavskiy V V, Shurshalov L V 2011 Hydrodynamic simulation of converging shock waves in porous conical samples enclosed within solid targets *J. Appl. Phys.* **110** 053501
- [9] Charakhch'yan A A, Khishchenko K V, Fortov V E, Frolova A A, Milyavskiy V V and Shurshalov L V 2011 Shock compression of some porous media in conical targets: numerical study *Shock Waves* **21** 35–42

- [10] Charakhch'yan A A *et al* 2011 Converging shock waves in porous media *Tech. Phys. Lett.* **30** 33–5
- [11] Herrmann W 1969 Constitutive equation for the dynamic compaction of ductile porous materials *J. Appl. Phys.* **40** 2490–9
- [12] Carroll M M and Holt A C 1972 Static and dynamic pore-collapse relations for ductile porous materials *J. Appl. Phys.* **43** 1626–36
- [13] Wünnemann K, Collins G S and Melosh H J 2006 A strain-based porosity model for use in hydrocode simulations of impacts and implications for transient crater growth in porous targets *Icarus* **180** 514–27
- [14] Seaman L, Tokheim R E and Curran D R 1974 Computational representation of constitutive relations for porous materials *Technical Report No. DNA-3412F* Stanford Research Institute
- [15] Seisson G *et al* 2013 Dynamic behavior of a porous brittle material: experiments and modeling *Procedia Eng.* **58** 715–23
- [16] Seisson G *et al* 2014 Modeling of laser-driven waterconfined shocks into porous graphite *J. Phys.: Conf. Ser.* **500** 112057
- [17] Seisson G *et al* 2014 Dynamic cratering of graphite: experimental results and simulations *Int. J. Impact Eng.* **63** 18–28
- [18] Poco 2016 www.poco.com
- [19] Sheppard R G, Morgan D, Mathes D M and Bray D J (ed) 2002 *Properties and Characteristics of Graphite for the EDM Industry* 5th edn (Decatur, TX: Poco Graphite)
- [20] Takahashi S, Aoki S and Oku T 1993 Impact fracture toughness of a nuclear graphite measured by the one-point-bending method *Carbon* **31** 315–23
- [21] Ayatollahi M R, Berto F and Lazzarin P 2011 Mixed mode brittle fracture of sharp and blunt v-notches in polycrystalline graphite *Carbon* **49** 2465–74
- [22] Burchell D 1996 A microstructurally based fracture model for polygranular graphites *Carbon* **34** 297–316
- [23] Salazar A, Pastor J Y and Llorca J 2002 *In situ* observation of damage nucleation in graphite and carbon/carbon composites *Carbon* **40** 609–16
- [24] Latella B A and Liu T 2006 The initiation and propagation of thermal shock cracks in graphite *Carbon* **44** 3043–8
- [25] Mirhabibi A R and Rand B 2007 Graphite flake-carbon composites. II: fracture behaviour, toughness, notch insensitivity and Weibull modulus *Carbon* **45** 991–7
- [26] Hébert D *et al* 2015 Simulations of hypervelocity impacts into graphite *Procedia Eng.* **103** 159–64
- [27] Strand O T and Whitworth T L 2007 Using the heterodyne method to measure velocities on shock physics experiments *AIP Conf. Proc.* **955** 1143–6
- [28] Mercier P *et al* 2009 PDV measurements of ns and fs laser driven shock experiments on solid targets *AIP Conf. Proc.* **1195** 581–4
- [29] Hébert D *et al* 2011 A KDP equation of state for laser-induced damage applications *J. Appl. Phys.* **109** 123527
- [30] Wilkins M L 1980 Use of artificial viscosity in multidimensional fluid dynamic calculations *J. Comput. Phys.* **36** 281–303
- [31] Seisson G *et al* 2014 Penetration and cratering experiments of graphite by 0.5 mm diameter steel spheres at various impact velocities *Int. J. Impact Eng.* **70** 14–20