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Article Sub-Title		
Article CopyRight	Springer Science+Business Media Dordrecht (This will be the copyright line in the final PDF)	
Journal Name	Artificial Intelligence Review	
Corresponding Author	Family Name	Zhang
	Particle	
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Abstract

An artificial compound eye system is the bionic system of natural compound eyes with much wider field-of-view, better capacity to detect moving objects and higher sensitivity to light intensity than ordinary single-aperture eyes. In recent years, renewed attention has been paid to the artificial compound eyes, due to their better characteristics inheriting from insect compound eyes than ordinary optical imaging systems. This paper provides a comprehensive survey of the state-of-the-art work on artificial compound eyes. This review starts from natural compound eyes to artificial compound eyes including their system design, theoretical development and applications. The survey of artificial compound eyes is developed in terms of two main types: planar and curved artificial compound eyes. Finally, the most promising future research developments are highlighted.

Keywords (separated by '-')

Artificial compound eye - Image reconstruction - Depth estimation - Motion detection - Extended depth of field - Large field-of-view imaging

Footnote Information

Artificial compound eye: a survey of the state-of-the-art

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1 Introduction

Based on the principle of survival of the fittest, introduced by Darwin (2003), living beings on the earth have evolved a lot of features that adapt to their living environments. Different creatures always have different unique features because of their different living environments. Inspired by this, researchers always envisage to imitate the unique features of creatures so as to manufacture various bionic systems. Up to date, bionic systems have been widely researched and applied, for instance, airplane is inspired by birds (Wright and Kelly 1953); a sonar system is inspired by a bat's distance measure system (Barshan and Kuc 1992); helicopter is inspired by dragonfly (Johnson 2012); and so on.

Creatures see the outside world through their eyes, while in imaging devices such as cameras, the images with environment information can also be captured. In the traditional imaging device, the single-aperture principle imitating the mammal eye is utilized to design the optic imaging system. But the factors like image-forming principle and diffraction limit result in the large size of traditional imaging devices and the difficulty to further reduce the size and weight. In some application areas such as intelligent robot vision systems, micro imaging devices and portable devices, the whole imaging system with small size and wide field-of-view (FOV) is always expected. To reach this goal, researchers started to focus on the animals with compound eye system. In comparison with single-aperture eye (also called camera eye), compound eyes have many unique features, such as normally much smaller size, wider FOV, better capability to detecting moving objects and normally much lower spatial resolution. Therefore, the natural compound eye system is imitated to obtain the multi-aperture system so as to break the limitation of the ordinary imaging principle. From the 1970s to 1980s in the twentieth century, not only the biological perspective of compound eyes, but also the optical imaging principles were taken into account, based on the thorough research of natural compound eyes (Snyder 1977; Land 1976; Horridge 1978, 1987; Snyder et al. 1977). Since then, the artificial compound eye system with the merits of natural compound eyes becomes an active and hot research field.

Until now, numerous variants of artificial compound eyes have been proposed and much attention has also been paid to the theoretical investigation and various applications. It is very necessary to summarize systematically, to compare and analyze the work on artificial compound eyes reported in the literature. In this paper, a comprehensive survey of the state-of-the-art work on artificial compound eyes is presented. The survey starts from natural compound eyes to artificial compound eyes, which are reviewed from several aspects such as the system design, theoretical development and applications. The most promising future research developments are also highlighted.

The rest of this paper is arranged as follows. Section 2 introduces natural compound eyes. Section 3 presents the design and analysis of artificial compound eyes. In Sect. 4, the theoretical developments of artificial compound eyes are discussed. Various applications of artificial compound eyes are summarized in Sect. 5. Finally, conclusions and possible further developments are given in Sect. 6.

2 Natural compound eyes

Compound eyes (Fig. 1a–d) are the most common visual principle in the animal realm, simply because they are typical for arthropods, which comprise the highest number of species, and individuals. Normally associated with insects, eyes which consist of numerous identical visual units are represented likewise in crustaceans, myriapods, chelicerates (such as the horseshoe crab *Limulus*), in some mollusks (ark clams) and annelids (e.g. *Sabellaria*) (Cronin et al. 2014).

There exist two principles after which these individual units can be constructed. The first is represented for example in most myriapoda, and many chelicerates such as scorpions. Their visual units consist of small cups, floored by a retina which is covered by a tiny lens—a system which is called ocellus (Fig. 1c). The lens of these ocelli focuses the light, but often deeper than the level of the retina, they underfocus, and thus the image built appears as blurred. These lenses, however, may have a gradient of centrally increasing density, acting as so-called ‘gradient index lenses’ shortening the focal length. Each of these ocelli is able to perceive the direction of the incident light, to detect movements, and even the formation of images is possible, while the acuity depends among other factors on the number of receptors in the retina, and of course on the focal length of the lens. An example given may be the predatory myriapod *Lithobius*. It has up to 40 separated ocelli, and these have up to 110 receptors each Bähr (1974). Compound eyes, which consist of ocelli, sometimes are called ‘aggregate eyes’ to distinguish them from the compound eyes of insects and crustaceans. The compound eyes of insects and crustaceans are also composed of identical visual units, here called ‘ommatidia’. Ommatidia are different from the visual units composing the eyes of the systematic groups mentioned before. The dioptric apparatus of each ommatidium consists of a translucent cuticular ‘corneal lens’ (Fig. 1b2-1) and an adjacent ‘crystalline cone’ (Fig. 1b2-2).

In terrestrial systems the lens focuses the light through the crystalline cone onto a central light guiding structure, the so-called ‘rhabdom’ (Fig. 1b2-3). The latter is part of the sensory cells (Fig. 1b2-4), and contains the visual pigments. The sterical structure of the pigments is changed by the energy of the incident light, producing an electric signal, which is processed by the nervous system of the arthropod. In aquatic systems the refractive power of the organic lens is not high enough to focus the light sufficiently, because of the low difference of refractive indexes between water and lens. Here the crystalline cone, as a gradient index lens or with other mechanisms, overtakes the function of focusing light. Because all contrasts inside the angle of view of each ommatidium are concentrated on the rhabdom, and thus become melted to one average, there is *no image formation* inside of each ommatidium—the field of view that belongs to one facet is represented by one mean contrast and colour (Fig. 1b4: orange dot). Because the ommatidia are optically isolated against each other by pigment cells acting comparable to a curtain (Fig. 1b2-5), the image seen by the bearer of this compound eye is that of a mosaic, while each ommatidium contributes one tile. The fineness of vision thus depends among other factors on the number of ommatidia, as the number pixels contribute to the acuity of a computer graphic (Fig. 1e). Although each lens of course is capable to perform images by its physical structure, this power is not used—the lens “just” concentrates the light onto the rhabdom. Other parameters contribute also to the acuity of vision in a compound eye. There is the so-called ‘interommatidial angle’ ($\Delta\varphi$), the angle between the optical axes of adjacent facets’ lenses, which, as the width of the angle of acceptance of each ommatidium (-> rhabdom) should be as small as possible to achieve a high resolution (Fig. 1f, g). ($\Delta\varphi$) represents the fineness of scanning inside the field of view. In flat eyes an

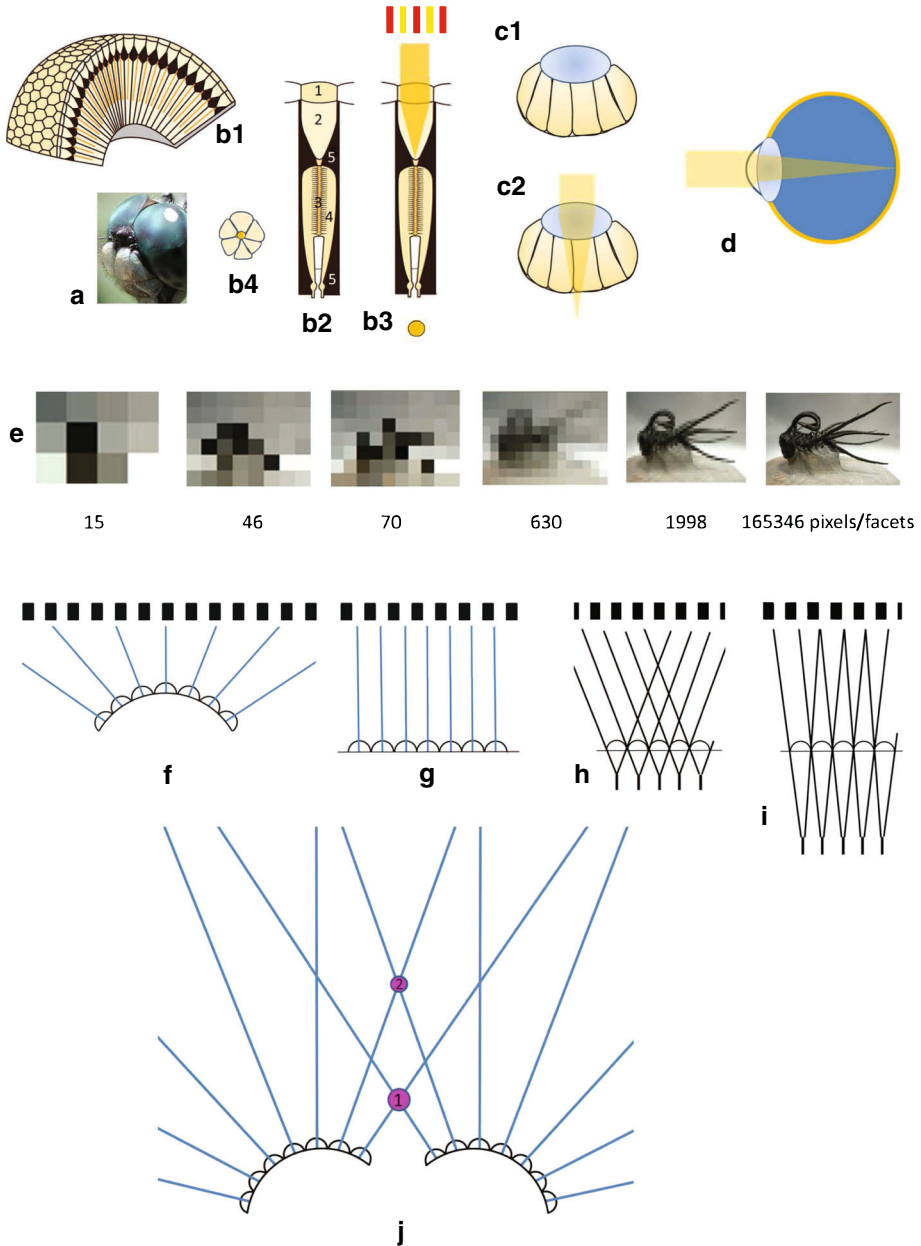


Fig. 1 Structures of focal apposition compound eyes. **a** Compound eye of the dragonfly *Aeschna sp* (Source: de.wikipedia.org, David L. Green.) **b1** schematic drawing of a focal apposition compound eye (bee). **b2** Visual cross-section through a visual unit (ommatidium): 1 lens, 2 crystalline cone, 3 rhabdom, 4 receptor cell, sensory cell, 5 screening pigment cells. **b3** Light path and optical signal processing in the ommatidium of a focal apposition eye. **b4** Cross-section of **b2**. **c1** ocellus. **c2** Light path through an ocellus, underfocusing. **d** Vertebrate eye. **e** Acuity of the mosaic-like image formation of an apposition compound eye, depending on the number of ommatidia. **f** resolution with a curved visual surface. **g** Resolution with a flat visual surface. **h** Resolution with a short crystalline cone. **i** Resolution with a long crystalline cone. **j** Distance estimation in a focal apposition compound eye

99 optimal, high acute scanning is easier to realise than in eyes with curved surfaces (Fig. 1f,
100 g). Another feature is the overlapping of the angles of acceptance the units cover. The latter
101 depends, among others, on the position of the rhabdom below the crystalline cones (lengths
102 of the crystalline cones). Eyes with long crystalline cones usually supply a less ambiguous
103 information than those with short crystalline cones (Fig. 1h, i).

104 The mosaic-like vision has consequences for distance estimation, which is possible just
105 in visual systems with overlapping fields of view, represented in many predatory arthropods.
106 Figure 1j shows, that where the optical axes of ommatidia intersect, an estimation of relative
107 positions is possible. For example, beyond intersection 2 in Fig. 1j, no more points of inter-
108 section exist, and thus no unambiguous information about relative distances is possible any
109 more beyond this point. From here for the arthropod everything seen is just as “far away”
110 (compare Horridge (1977)).

111 The number of ommatidia usually varies from some few, as in terrestrial isopods, up
112 to several 10,000 per eye in *Aeschna* (Fig. 1a) or *Anax junius* 28,672 ommatidia in each
113 eye, Sherk (1978), both dragonflies. The number depends on living environments of the
114 respective species, as of its life-style. The effectiveness of a predatory life-style for example,
115 as the success of chasing sexual partners depends on an acute vision. A huge number of facets
116 is installed mainly in daylight adapted arthropods, because dim light conditions demand for
117 a wide aperture, and thus large lenses in a limited space of a compound eye’s surface. So the
118 design of any compound eye is a trade-off between optimal acuity (high number of facets)
119 and the necessity to capture photons enough to work sufficiently demanding for a minimum
120 aperture. By optical reasons (diffraction) the lower limit of lens diameters lies at $10\ \mu\text{m}$
121 (Snyder 1977, 1979), and is nearly realised in certain mites and diurnal mosquitoes (Collett
122 and Land 1975; Land et al. 1999; Kawada et al. 2006). Arthropods of dark environments often
123 show lens diameters of $200\ \mu\text{m}$ and more. The interommatidial angle ($\Delta\varphi$), describing the
124 fineness of scanning of the environment, can vary inside of the visual surface, but especially
125 among species. $\Delta\varphi$ varies from several tens of degrees in *Collembola* or 7° in *Chlorophanus*,
126 a beetle (Land 1997, 1981) to 0.24° in the acute zone of the visual surface of a dragonfly such
127 as *Anax junus*. For many flying insects, such as bees, flies and butterflies $\Delta\varphi$ lies typically
128 in the range of 1° – 3° , less than 1° is valid for many predators such as dragonflies, mantids
129 and spicid wasps (Land 1997).

130 2.1 Classification

131 The compound eye system explained before is the most common, especially among diurnal
132 insects and crustaceans, and probably the oldest one. Just recently it was described for a
133 160 million year old crustacean (Vannier et al. 2016). Because the light is focused on the
134 central rhabdom, it is called ‘focal apposition eye’ Nilsson (1989a). As mentioned, each
135 ommatidium is an independent visual unit, forming one “pixel” to the total mosaic-like
136 image. In arthropods living under dimmer light conditions, adaptive forms of compound
137 eyes evolved, equipped with a higher sensitivity. These are the super-position eyes (optical
138 superposition eyes: refractive superposition eye—e.g. moths; reflecting superposition eyes,
139 working with mirror boxes—e.g. decapod shrimps and crayfish; parabolic superposition
140 eyes—certain amphipod crustaceans; neural superposition eyes—many dipteran flies) (Land
141 and Nilsson 2012). The imaging principles of five different types of compound eyes are shown
142 in Fig. 2 (Nilsson 1989). In superposition eyes the visual units do not work independently. Up
143 to hundreds of adjacent facets support each other in capturing light, enhancing the aperture,
144 but possibly pay with a loss of acuity. Refracting superposition eyes by moving pigment

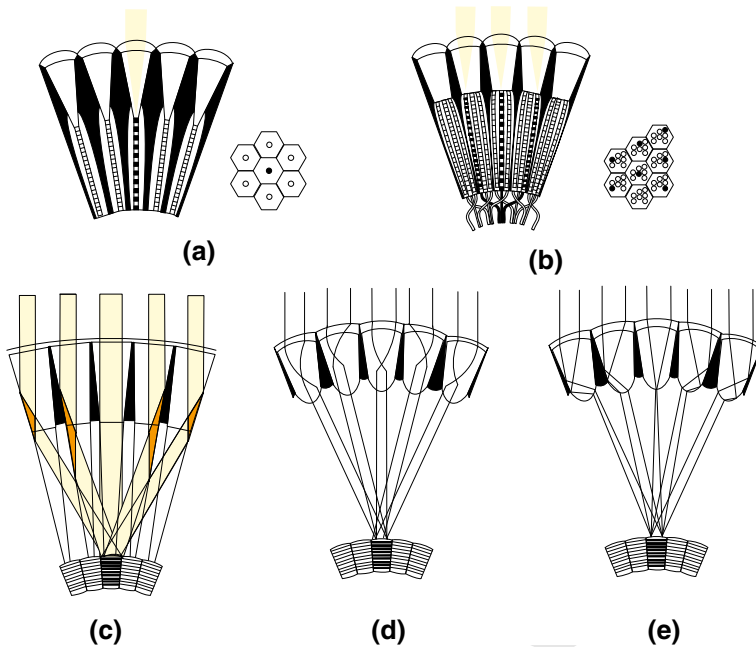


Fig. 2 The imaging principles of different types of compound eyes. **a** The apposition compound eye. **b** The neural superposition compound eye. **c** The reflective superposition compound eye. **d** The refractive superposition compound eye. **e** The parabolic superposition compound eye (Nilsson 1989)

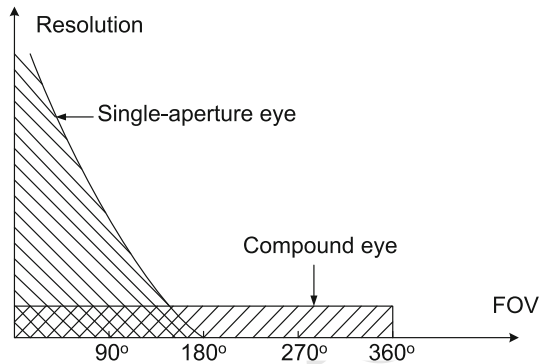
Fig. 3 Trilobite: *Geesops schlotheimi* (BRONN, 1825). Age and location: Middle Devonian Ahrdorf Formation, Flesten Member, Salmerweg bei Gees/Gerolstein, Eifel, Germany



145 cells can be changed to apposition eyes, and many other intermediate forms between these
 146 types of eyes are realised. If the apposition compound eye can be regarded as a *one-to-one*
 147 relationship, then the superposition compound eye can be considered as a *many-to-many*
 148 relationship.

149 Some fossil trilobites, extinct arthropods which dominated the faunas of the Palaeozoic,
 150 were assumed to possess an ocellar compound eye system. One type of trilobite (*Geesops*
 151 *schlotheimi*) is shown in Fig. 3 (Schoenemann and Clarkson 2013). They possess a sophisti-
 152 cated optic, probably correcting spherical aberrations typical, for thick lenses allowing clear
 153 image formation (Clarkson and Levi-Setti 1975). According to these results Schoenemann in
 154 2007 developed a model, where by the processing of information of the individual receptor

Fig. 4 Comparisons of the compound eye and the single-aperture eye with respect to resolution and FOV (Sanders and Halford 1995)



155 cells, among the ocelli by means of a neuronal matrix in common, one total image could be
 156 produced—optimised in sharpness, acuity and contrasts (Schoenemann 2007).

157 2.2 Comparative analysis

158 It becomes obvious that the imaging principle of an ommatidium in an arthropod's apposition
 159 compound eye is very different from that of a one lens camera eye, as in vertebrates. In the
 160 camera eye through one lens an image is formed onto a retina, which consists in a human
 161 being of several millions of receptors that form one image (~6 million cones, ~120 million
 162 rods)—while in a compound eye of the apposition type the total image is established by
 163 numerous individual units, forming pixels of a mosaic-like image. So, while in a human eye
 164 the image is formed by millions of receptors, in arthropods the highest number of receptor
 165 units lies at about 30,000 in dragonflies. Thus, in general, a compound eye has a much smaller
 166 spatial resolution than a human eye with a single aperture. While a compound eye normally
 167 has hardly any modes of accommodation (it is not needed because of their short focal length,
 168 some can change their acceptance angle, however that is for capturing more light), a variable
 169 or movable lens in a camera eye system brings great advantages in focusing objects at different
 170 distances, for those lenses are normally much larger than those of compound eyes. In contrast,
 171 due to a curved visual surface in arthropod compound eyes the field of view often is much
 172 wider than that of the one lens systems. Figure 4 compares the resolution and FOV between
 173 the compound eye and the single-aperture eye. Finally, the temporal resolution of compound
 174 eyes (the number of signals distinguished per time unit [signals (ss)/second (s)]) in insects
 175 often is higher than in vertebrate eyes. Here the frequencies as most commonly quoted:
 176 Because in neural superposition eye the signals are not forwarded but processed directly,
 177 this system reaches ~300[ss/s], the apposition eye of a honey bee about ~100[ss/s], a
 178 human's camera eye 20–25 [ss/s]. This temporal resolution depends on the velocity of the
 179 nervous structures, furthermore among others on the morphological design of the compound
 180 eye (e.g. the width of the acceptance angle of the rhabdom) and the velocity of movement
 181 of the arthropod. A comparison of different eyes and their related parameters are shown in
 182 Table 1, where human, bee and moth represent a single-aperture eye, apposition compound
 183 eye and superposition compound eye, respectively.

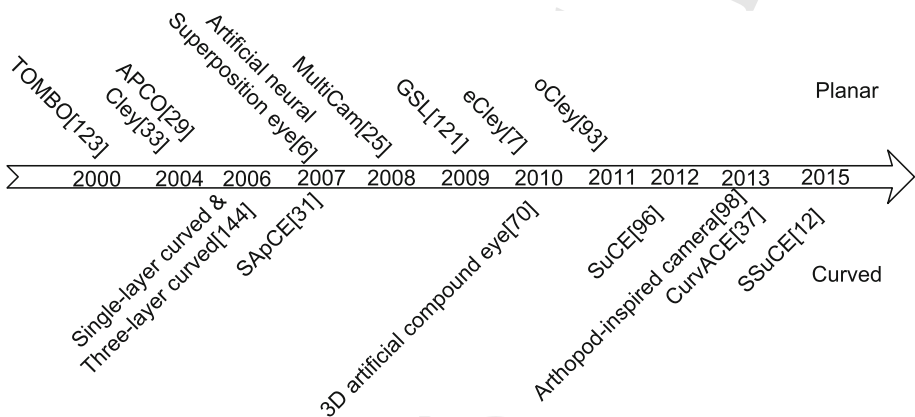
184 3 Design and analysis of artificial compound eye

185 The study of artificial compound eye was initiated in 1990s. Due to the limitations of process-
 186 ing and manufacturing technologies, most artificial compound eyes are made with a planar

Table 1 Parameter comparisons of different eyes (Sarkar 2011)

Parameter	Human	Bee (<i>worker bee</i>)	Moth (<i>Ephestia</i>)
Eye type	Single-aperture eye	Apposition	Superposition
Light habitat	Diurnal	Diurnal	Nocturnal
Lens diameter (mm)	7	0.025	0.4
Focal length (mm)	23	0.06	0.17
Receptor diameter (μm)	2	1.5	8
F-number ($F/\#$)	3.3	2.4	0.4
Sensitivity (μm^2)	0.23	0.24	218
Acceptance angle ($^\circ$)	0.007	1.9	<13
Interreceptor angle ($^\circ$)	0.005	–	3
Interommatidial angle ($^\circ$)	–	0.95	–
Resolution ($LP/^\circ$)	100	0.52	>0.08

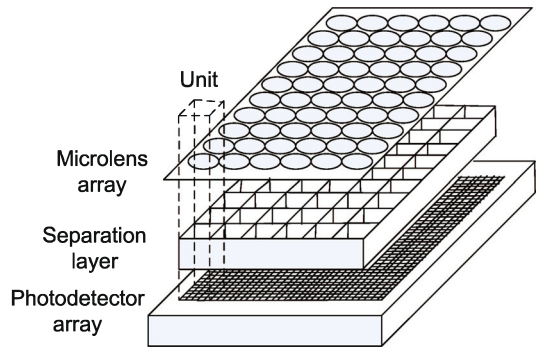
($LP/^\circ$ means line pair per degree)

**Fig. 5** Start time of different kinds of artificial compound eyes

187 surface. This structure leads to a large aberration distortion in a large incident angle. It is
 188 shown by the research results that curved artificial compound eye has the best structure imi-
 189 tating the functions and features of insect compound eye (Sanders and Halford 1995). With
 190 the improvement of micro fabrication technology, curved artificial compound eyes were
 191 widely researched in 2000s. Figure 5 shows the advance of several typical planar and curved
 192 artificial compound eyes in the twenty-first century. This figure indicates that many curved
 193 compound eyes were proposed after the year of 2006 and the research of planar compound
 194 eye is still in progress. The main reason is that large overlapped screen information in the
 195 ommatidia of planar compound eye can be utilized to enhance resolution and to obtain super-
 196 resolution images while keeping the compact structure. Thus, this section reviews the design
 197 and analysis of the two kinds of artificial compound eyes, planar and curved, respectively.

198 3.1 Planar artificial compound eye

199 In the early research of artificial compound eyes, most researchers focused on planar artificial
 200 compound eyes because of the limitation of micro fabrication technology. The prototype of

Fig. 6 TOMBO system (Tanida et al. 2000)

201 planar artificial compound eyes is either apposition compound eye or superposition compound
 202 eye. To date, a lot of planar artificial compound eyes have been proposed (Tanida et al. 2000;
 203 Duparré et al. 2004b, a; Duparré and Wippermann 2006; Duparré and Völkel 2006; Duparré
 204 et al. 2005d, a, 2004c, 2005b, c; Wippermann et al. 2005; Brückner et al. 2007, 2008; Druart
 205 et al. 2008; Brückner et al. 2010a, b; Bräuer et al. 2011; Brückner et al. 2011; Meyer et al.
 206 2011; Stollberg et al. 2009; Duparré et al. 2008; Druart et al. 2009; Di et al. 2009; Leitel et al.
 207 2010; Ueno et al. 2013; Brückner et al. 2010c; Ogata et al. 1994; Carr et al. 2004; Hornsey
 208 et al. 2004; Kinoshita et al. 2005; Christensen et al. 2006; Wippermann et al. 2006; Yang
 209 et al. 2009; Sieler et al. 2010; Fallah and Karimzadeh 2010; Dunkel et al. 2014; Belay et al.
 210 2014). In what follows, several typical planar artificial compound eyes are selected to discuss
 211 the design principle.

212 Inspired by a dragonfly's apposition compound eye, a compact imaging system called
 213 TOMBO (Thin Observation Module by Bound Optics) was proposed by Tanida and his
 214 research team (Tanida et al. 2000). As shown in Fig. 6, TOMBO is composed of a microlens
 215 array, a separation layer and a photodetector array. Each microlens covers multiple photosen-
 216 sitive cells on the photodetector array to form a small imaging system called unit. Specially,
 217 adjacent units are separated by separation layers to prevent signal crosstalk. Obviously, this
 218 system is thinner than that of traditional cameras. It is noting that the structure can be further
 219 improved because each part of TOMBO is separable. However, this separability leads to
 220 much bias during the system integration and worsen its images.

221 A kind of artificial apposition compound eye called APCO (Apposition Compound eye
 222 Objective) was proposed by Duparré et al. (2004a, b), Duparré and Wippermann (2006),
 223 Duparré and Völkel (2006). In APCO, the overall thickness is only about 300 μm and the
 224 FOV about 21° on diagonal is achieved. Generally, the monolithic device is composed of
 225 a microlens array, a substrate, a pinhole array in the focal plane and a CMOS sensor array.
 226 Moreover, a pitch difference between lens array and pinhole array is designed to obtain
 227 wider FOV. In order to prevent crosstalk between adjacent channels, an opaque wall between
 228 adjacent channels is added (Duparré et al. 2005a, d). The schematic diagram of APCO is
 229 shown in Fig. 7. Subsequently, an imaging system that imitates the superposition compound
 230 eye was proposed by this team. As the implementation of each channel is optically isolated,
 231 this system is not called superposition compound eye, but cluster eye (Cley) (Duparré and
 232 Wippermann 2006; Duparré and Völkel 2006; Duparré et al. 2004c, 2005b, d). Cley is com-
 233 posed of three microlens arrays (MLAs) with different pitches. The working principle of
 234 Cley is shown in Fig. 8. Comparing with APCO, the image resolution and distortion in mar-
 235 ginal channels of Cley have been greatly improved. However, due to the structure with three
 236 MLAs, it is quite complicated in fabrication and the thickness is nearly ten times as much as

Fig. 7 Schematic diagram of APCO (Duparré et al. 2004b). **a** Without opaque wall. **b** With opaque wall

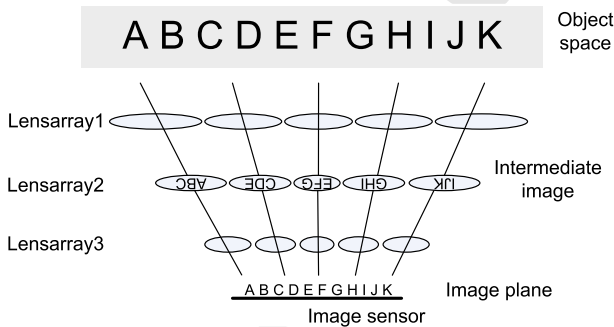
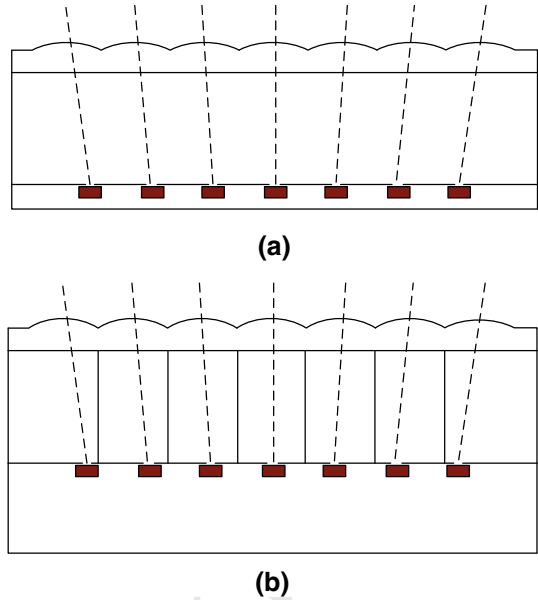


Fig. 8 Working principle of Cley (Duparré et al. 2004c)

237 that of APCO. The different pitches between MLAs can obtain large FOV, but this structure
 238 also suffers obviously by astigmatism in a large incident angle. Since the Cley can be seen as
 239 multiple isolated imaging systems, each ommatidium can be designed specifically to correct
 240 astigmatism. Inspired by this, Duparré et al. presented chirped arrays, in which ellipsoidal
 241 microlenses are used (Duparré et al. 2005c; Wippermann et al. 2005). Each microlens is
 242 designed carefully to correct the astigmatism. The related spot diagrams of the circular and
 243 ellipsoidal lenses under perpendicular and oblique incidence are shown in Fig. 9, which indicates
 244 that it is feasible to use the ellipsoidal lens to correct astigmatism. Thus, the Cley can
 245 be further improved by using the ellipsoidal lens. Figure 10 shows the schematic diagram of
 246 Cley and two kinds of microlens arrays.

247 A well-known problem in the area of artificial apposition compound eyes is that the
 248 inverse relationship between resolution and sensitivity (Duparré et al. 2005a). The reflective
 249 and refractive superposition compound eyes are too complicated to fabricated. Brückner et
 250 al. proposed an artificial neural superposition eye Brückner et al. (2007, 2008), just like the

Fig. 9 Circular and ellipsoidal lenses under perpendicular and oblique incidence and related spot diagrams (Duparré et al. 2005c)

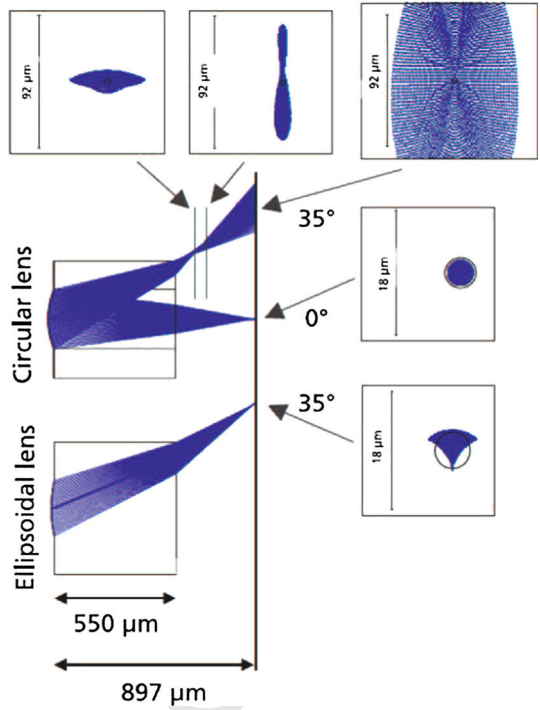
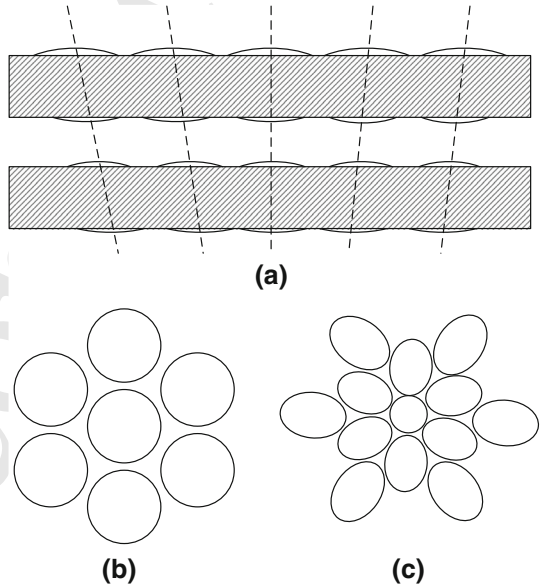


Fig. 10 Cley systems Duparré et al. (2004c). **a** Schematic diagram of Cley. **b** Regular microlens array. **c** Chirped microlens array



251 neural archetype. In the artificial neural superposition eye, each channel has multiple pixels
 252 and each object point is imaged by multiple channels separately; the outputs of the pixels that
 253 have parallel optical axes are summed up to increase the sensitivity of the eye under reserving
 254 the resolution. The working principles of neural superposition compound eyes in nature and

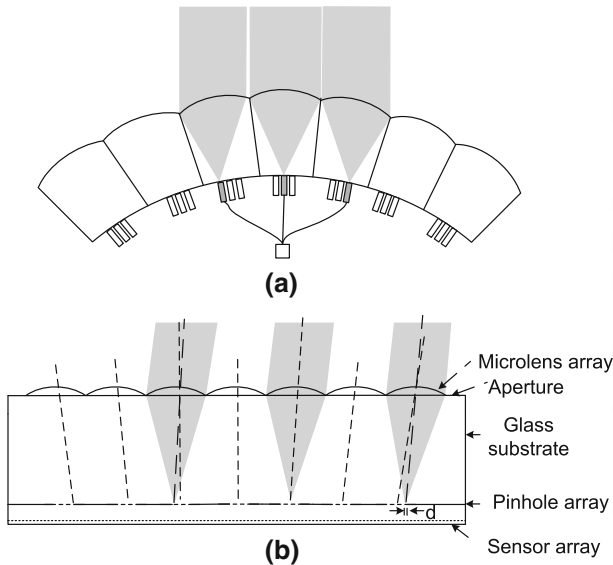


Fig. 11 Working principles of neural superposition compound eye. **a** Neural superposition compound eye in nature. **b** Artificial neural superposition compound eye (Brückner et al. 2007)

255 the artificial counterparts are shown in Fig. 11, where the working principles of the artificial
 256 neural superposition compound eye is just like the prototype found in nature. The artificial
 257 neural superposition eye exhibits a set of 3×3 pixels underneath each microlens, but the
 258 arrangement does not overcome the main disadvantages of the apposition principle. Later,
 259 inspired by the compound eye of a parasite of wasps called *Xenos Peckii*, Druart et al. came
 260 up with the idea to read out the completely partial image within each imaging channel, and
 261 then an imaging pre-processing method is used to form a full high resolution image (Druart
 262 et al. 2008). Brückner et al. followed this idea and presented an artificial compound eye
 263 system called eCley (Electronic Cluster Eye) (Brückner et al. 2010a, b; Bräuer et al. 2011;
 264 Brückner et al. 2011). eCley has an overall thickness only 1.4 mm, but it achieves a VGA
 265 resolution with 700×550 pixels. Generally, the partial images of the eCley are electronically
 266 stitched together to form a final image with high resolution. In contrast to other super-
 267 resolution algorithms, the relationship between the viewing directions of adjacent channels
 268 is well defined by thoroughly setting up the pitch difference between the optics and each
 269 channel, then the partial images are braided together. The principle of braided sampling
 270 is shown in Fig. 12. Inevitably, the eCley has a drawback that a customized image sensor
 271 in a large active area is needed. In order to overcome the major drawback of eCley, an
 272 artificial compound eye with optical stitching of segments called oCley (Optical Cluster
 273 Eye) is introduced by Meyer et al. (2011). The oCley is composed of four MLA layers. A
 274 special feature is that the second layer acts as field aperture and defines the shape and size of
 275 each partial image. The principle of oCley and the aperture shape of each layer are presented
 276 in Fig. 13.

277 The parameters of several typical planar artificial compound eyes are summarized in
 278 Table 2. Although the overall size of artificial compound eyes can not be as small as the natural
 279 compound eye, the overall thickness can reach 0.2 mm. Even when the VGA resolution is
 280 achieved, the overall thickness is only about 1.4 mm.

Fig. 12 The principle of braided sampling (Brückner et al. 2011). Colors are used for visualization only

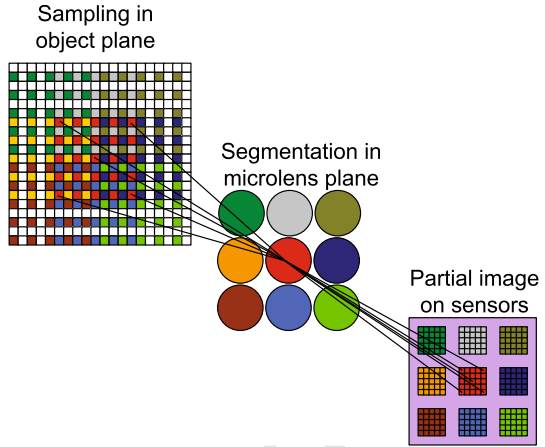
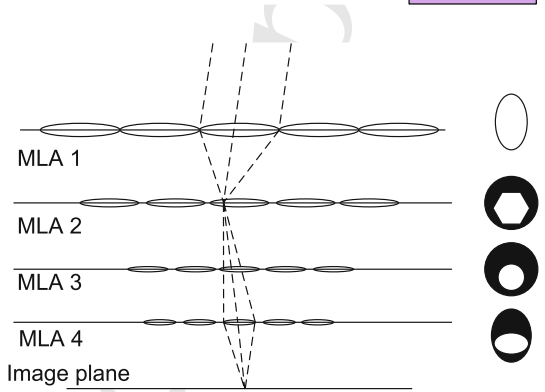


Fig. 13 The principle of oCley (Meyer et al. 2011). The first and the fourth microlens array include toroidal lenses. The second aperture is the hexagonal field aperture, which defines the partial image size



281 3.2 Curved artificial compound eye

282 The curved artificial compound eye was first introduced in 2006. Inspired by bees, Jeong
 283 et al. (2006) proposed a hemispherical compound eye with 8370 ommatidia. As shown in
 284 Fig. 14, each ommatidium is composed of a microlens, a polymer cone, a waveguide core
 285 and a photodetector to imitate the natural ommatidium. A comparison between the proposed
 286 artificial compound eye and natural compound eye is shown in Table 3. This table indicates
 287 that the physical dimensions and the optical characteristics of the proposed artificial compound
 288 eye are very comparable to the natural compound eye. Zhang et al. (2006) presented
 289 two kinds of curved compound eye: a single-layer and three-layer curved compound eye,
 290 in which the curved field lens array was introduced into the compound eye. The FOV of
 291 these two kinds of compound eyes are 60° and 88° , respectively. Due to the manufacturing
 292 complexity of the curved compound eye, a simplification of the complex natural archetype,
 293 called spherical artificial compound eye, was proposed by Radtke et al. (2007), Duparré et al.
 294 (2007). This compound eye system is composed of a lens array on a concave bulk lens and
 295 a pinhole array on a convex bulk lens. The design principle is shown in Fig. 15, where the
 296 designed channels are 112×112 and the FOV is $31^\circ \times 31^\circ$. However, due to the lack of
 297 opaque walls, the distortion leads to the usable channels only about 40×40 and the FOV
 298 only $10.3^\circ \times 10.3^\circ$. Actually, this is a spherical apposition compound eye (SApCE). Two
 299 kinds of spherical superposition compound eyes were proposed by Nakamura et al. (2012)

Table 2 The parameters of planar compound eye (“-” means unknown)

Type	Spatial resolution LP/mm	Angular resolution $LP/^\circ$	FOV	Size (mm) ²	Thickness (mm)	$F/\#$	Pixels	Channels
TOMBO (Tanida et al. 2000)	-	-	-	6×5	-	-	320×240	4×4 to 32×32
APCO (Duparré et al. 2004b)	3.6	1.5	$20^\circ \times 20^\circ$	9×9	$0.216 \sim 0.345$	2.2	-	130×130
Chirped APCO (Duparré et al. 2005e)	24	-	64.3°	9×9	0.9	2.6	130×130	130×130
Cley (Duparré et al. 2004c)	71	3.3	$70^\circ \times 10^\circ$	4.5×0.5	2	1.8	700×550	21×3
Neural superposition eye (Brückner et al. 2007)	-	-	$115^\circ \times 86^\circ$	-	0.65	2.5	60	40×30
Zoom compound eye (Duparré et al. 2008)	-	-	$49^\circ \times 37^\circ$	-	6.9	5.6	-	80×60
MULTICAM (Druart et al. 2008)	-	8	30°	-	24.8	8	320×256	5×5
Spherical isolated-islands array (Di et al. 2009)	-	-	-	9×9	0.7	-	-	9×9
GSL (Stollberg et al. 2009)	49	2	29°	2.8×2.8	2	2.8 ± 0.2	156×156	15×15
eCley (Brückner et al. 2010a)	156	-	$58^\circ \times 46^\circ$	6.8×5.2	1.4	3.7	700×500	17×13
Ultra-thin Array Microscope (Ueno et al. 2013)	115	-	-	36.1×24	4	-	4872×3248	150×90
oCley (Meyer et al. 2011)	155	4.2	$53.2^\circ \times 39.9^\circ$	2.2×2.9	1.86	6.7	640×480	14×13
Close-up imaging system (Brückner et al. 2010c)	150	-	$52^\circ \times 63^\circ$	8.5×8.5	6	2.8	3280×2464	26,000

Fig. 14 Structure of artificial ommatidium (Jeong et al. 2006)

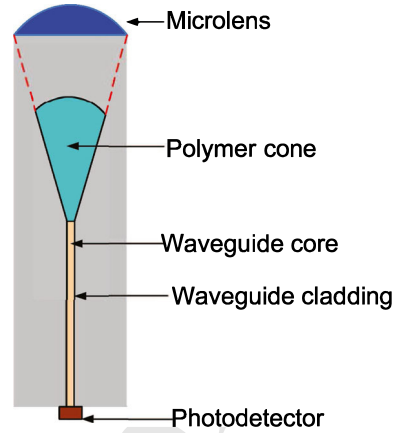


Table 3 Comparisons of an artificial compound eye and a natural compound eye (Jeong et al. 2006)

	Artificial compound eye	Natural compound eye
Shape of lens aperture	Hexagon	Hexagon
Maximal lens diameter	25 μm	20–36 μm
F number	1.8–2.9	2.7–3.3
Number of lenses	8370	Few~30,000
Refractive index of lens	1.584	1.363
Index difference	0.029	0.023
Waveguide shape	Cylindrical	Cylindrical
Waveguide core	5.1–6.3 μm	2–8 μm
Waveguide length	150–300 μm	Appr. 100 μm
Angular sensitivity function	1.1°–4.4°	1.6°–4.7°

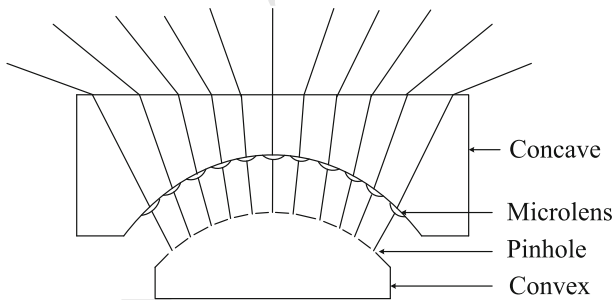


Fig. 15 Design principle of spherical compound eye (Radtke et al. 2007)

300 and Cao et al. (2015). The superposition compound eye (SuCE) was presented by Nakamura
 301 et al. using a spherical array of erect imaging optics to extend the FOV, and the deconvolution
 302 processing was introduced to reconstruct a sharp image. Subsequently, a spherical superpo-
 303 sition compound eye (SSuCE) with three layers of lens arrays was proposed by Cao et al..
 304 The two kinds of spherical superposition compound eyes have much higher energy efficiency
 305 and better resolution than conventional spherical apposition compound eyes. Li and Yi pro-

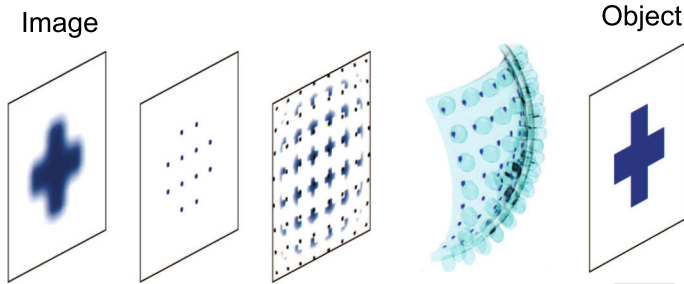
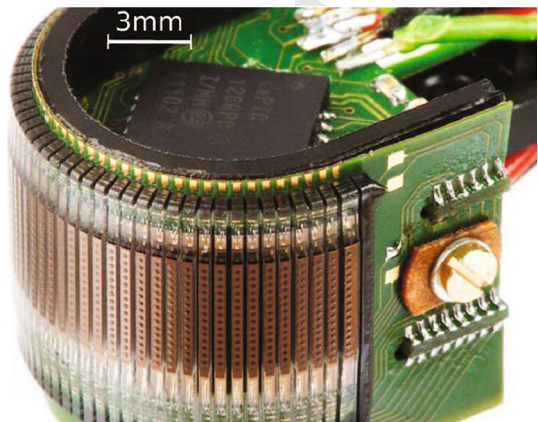


Fig. 16 The imaging principle of arthropod-inspired camera (Song et al. 2013)

Fig. 17 The CurvACE prototype (Viollet et al. 2014)



306 posed a microfabrication system created on a steep curved substrate. In fact, the fabricated
 307 three-dimensional microlens array has very high dimensional accuracy and the profile error
 308 is less than $6\ \mu\text{m}$ over the entire surface (Li and Yi 2009, 2010). Based on this structure, the
 309 maximum light deviation angle reaches 18.43° and the maximal FOV, in theory, can be as
 310 large as 180° , if the entire hemispherical surface is used.

311 In recent years, various curved artificial compound eyes were proposed (Song et al. 2013;
 312 Xiao et al. 2014a, b; Floreano et al. 2013; Viollet et al. 2014; Zhang et al. 2010; Hiura
 313 et al. 2011; Moens et al. 2010; Shen and Su 2013; Li et al. 2013; Liu et al. 2012). Their
 314 representatives are the arthropod-inspired camera introduced by Song et al. (2013), Xiao
 315 et al. (2014b), Xiao et al. (2014a) and the CurvACE (Curved Artificial Compound Eye)
 316 presented by Floreano et al. (2013), Viollet et al. (2014). The arthropod-inspired camera is
 317 composed of elastomeric compound optical elements with deformable array of thin silicon
 318 photodetectors, the total FOV up to 160° can be achieved. The imaging principle of the
 319 arthropod-inspired camera is shown in Fig. 16. Subsequently, a totally different imaging
 320 system, called computational compound eye (COMPU-EYE) (Lee et al. 2016) was proposed
 321 for improving the resolution. The CurvACE is inspired by *Drosophila* and composed of a
 322 microlens array, a neuromorphic photodetector array and a flexible PCB. Figure 17 shows the
 323 CurvACE prototype, which contains 630 ommatidia. The FOV of CurvACE is $180^\circ \times 60^\circ$.
 324 A comparison between CurvACE and its natural archetype is provided in Table 4.

325 The parameters of these curved artificial compound eyes are summarized in Table 5.

Table 4 Comparison of CurvACE and Drosophila eye (Floreato et al. 2013)

	CurvACE	Drosophila eyes
Number of ommatidia	630	600 ~ 700
Facet diameter (μm)	172	16
Eye diameter (mm)	12.8	0.36
Interommatidial angel	$\approx 4.2^\circ$	$\approx 4.7^\circ - 5.5^\circ$
Acceptance angle	4.2°	$\sim 4.5^\circ$
FOV	$180^\circ \times 60^\circ$	$160^\circ \times 180^\circ$
Signal acquisition bandwidth	300 Hz	<100 Hz
Adaptability to illuminance	Yes	Yes
Crosstalk prevention	Yes	Yes

326 4 Theoretical development of artificial compound eye

327 This section will discuss the theoretical development of artificial compound eyes including
 328 planar and curved compound eyes. The curved compound eye is the best imaging model
 329 that imitates insect compound eyes. While the planar compound eye can also imitate natural
 330 compound eyes to some extent. Furthermore, some drawbacks of natural compound eyes
 331 can also be overcome by using planar compound eyes. For instance, the post-processing
 332 technology can be utilized to process large overlapped information in adjacent channels in a
 333 planar compound eye, and the final image with high resolution is reconstructed to overcome
 334 the low resolution of natural compound eyes.

335 4.1 Planar compound eye

336 The theoretical development of planar compound eyes mainly focuses on the image recon-
 337 struction, depth estimation and depth of field extension. In what follows, the three aspects
 338 will be discussed step by step.

339 4.1.1 Image reconstruction

340 In the artificial compound eye, each visual unit can be seen as an independent imaging
 341 channel, but in general the imaging channel has only up to several hundred pixels, comparing
 342 with traditional camera, which leads to the lower resolution. Due to the small interommatidial
 343 angle and large overlapped information between adjacent channels, the reconstruction of the
 344 final image with high resolution while keeping the compact structure is very important and
 345 also an challenging research topic in the planar artificial compound eye.

346 In 2001, in order to test the effectiveness of the TOMBO in image retrieval, Tanida et al.
 347 used the image sampling and back projection method to fuse and retrieve the final image with
 348 high resolution from multiple images with low resolution (Tanida et al. 2001a). In Tanida
 349 et al. (2001b), Kitamura et al. (2004), Tanida et al. presented a pixel rearrange method to
 350 further overcome the drawbacks that the sampling method can not increase the resolution
 351 in principle and the back projection method is difficult to suppress undesired noises. The
 352 principle of the pixel rearrange method is that the geometrical parameters of each unit image
 353 are first estimated to determine the position of the pixels, and then the pixels in all unit images
 354 are rearranged onto a virtual image plane with high resolution, and finally the interpolation is
 355 applied to compensate the pixels which are not assigned values. In 2003, the pixel rearrange

Table 5 Parameters of curved artificial compound eye

Type	Angular resolution $L/P/^\circ$	FOV	Size (mm)	Thickness (mm)	$F/\#$	Pixels	Channels
Hemispherical compound eye (Jeong et al. 2006)	–	–	–	–	1.8–2.9	–	8370
Convex solid substrate based compound eye (Zhang et al. 2010)	–	60°	1.435	–	–	–	11 × 11
Krill-eye (Hiura et al. 2011)	–	≈180°	D = 1.8	–	–	–	10 × 10
Single-layer (Zhang et al. 2006)	–	60°	0.9 × 0.9	0.5	–	–	–
Three-layer (Zhang et al. 2006)	–	88°	0.9 × 0.9	0.5	–	–	–
Spherical compound eye (Radtke et al. 2007)	–	10.3° × 10.3°	D = 40	–	–	40 × 40	40 × 40
3D compound eye (Li and Yi 2009)	–	18.43°	D = 20	2.03	–	–	601
Two-layer lenses compound eye (Moens et al. 2010)	0.3	124°	–	–	–	–	25
Parabolic cluster eye (Shen and Su 2013)	–	102° × 90°	6.12 × 4.62	2.74	2.26	2053 × 1540	59
Arthropod-inspired camera (Song et al. 2013)	–	160°	R = 6.96	–	–	–	16 × 16
CurvACE (Floreano et al. 2013)	–	180° × 60°	R = 12.8	–	–	–	630

The symbols –, D and R means unknown, diameter and radius

method was extended to color imaging; and two configurations, color separation by pixels and color separation by units, were discussed (Tanida et al. 2003). The result shows that the first configuration has a better performance than the second and is more complicated than the second in integration. As the pixel rearrange method used the interpolation method to compensate the invalid pixels, it cannot solve the problem caused by undersampling. In Nitta et al. (2006), to further improvement of the method, Nitta et al. introduced an iterative back projection method (IBP), where the pixel rearrange method was first applied to obtain the initial image and the back projection method was iteratively applied to refine the image.

Except for the pixel rearrange method, lots of image reconstruct methods were also discussed in planar artificial compound eye (Kanaev et al. 2007; El-Sallam and Boussaid 2008, 2009; Horisaki et al. 2009; Oberdörster et al. 2011; Mendelowitz et al. 2013; Wood et al. 2004, 2005, 2006; Li et al. 2007, 2009; Chan et al. 2006b; Choi and Schulz 2008; Tudela et al. 2008b, a). Kanaev et al. (2007) presented a scene-independent method, in which the final image with high resolution could be reconstructed only based on the accurate relative pixel shifts. In El-Sallam and Boussaid (2008), El-Sallam et al. introduced a spectral-based blind image restoration method, which neither requires the prior information about the imaging system nor the original scene. This method was extended to color imaging later El-Sallam and Boussaid (2009). Horisaki et al. (2009) proposed to divide the compound-eye imaging into the low and high frequency components to suppress the effect of the color shift. The low-frequency component was utilized to generate the final smooth image and the high-frequency component was used in the depth estimation. Based on eCley system, a braiding algorithm to restore the final image was discussed in Oberdörster et al. (2011). Various image reconstruct methods for planar artificial compound eye are summarized in Table 6, where the advantages and limitations of different methods are compared.

4.1.2 Depth estimation

In stereo vision, in order to obtain depth information of the environment, in generally, two cameras or multiple cameras are required to capture the same object in different directions. Thus, the stereo matching algorithms for obtaining the accurate depth information are very important and a hot area of research in computer vision. A survey on the stereo correspondence algorithms was made in Scharstein and Szeliski (2002). An artificial compound eye is a multi-aperture camera, where each ommatidium lies in the different view direction. In generally, an object can be seen by multiple ommatidia. So the structure of artificial compound eyes has a potential function for 3D information extraction.

Based on the multi-aperture structure, the multiple base-lines method was first used in TOMBO system to retrieve the 3D image, and the outlines of objects were obtained in the early research of the depth estimation in artificial compound eyes (Yamada et al. 2006). As the high-resolution image was reconstructed by the pixel rearrange method, which assumes that the object is located at specific distance, different object distances between the actual and the assumed positions will result in the poor reconstruction performance. Inspired by this, several candidate object distances were used to estimate the depth information and the final depth was obtained by evaluating the SSD (Sum of Squared Difference) between the reconstructed image and the back-projected image (Horisaki et al. 2007). In Miyazaki et al. (2008), the pixel rearrange method was further improved by using the parallax images and directly mapping the pixel value onto a 3D surface, and then a high-resolution 3D image was retrieved by using the ray tracing. In Kagawa et al. (2010), a high-speed multispectral 3D imaging system was discussed by introducing time delay and multiple wavelength decomposition. The depth map was obtained by comparing the images for different wavelengths in the same time. Gao et al.

Table 6 Comparisons of different image reconstruct methods for planar artificial compound eye

Methods	Systems	Advantages	Limitations
Image sampling (Tanida et al. 2001a)	TOMBO	Simple principle and easy implementation	Cannot increase resolution
Backprojection (Tanida et al. 2001a)	TOMBO	Simple principle and easy implementation	Difficult to suppress undesired noise
Pixel rearrange based on correlation method (Tanida et al. 2001b)	TOMBO	Simple principle, easy implementation, need not to know the shift between units	Geometry parameter is not accurate enough; inaccuracy of measurement
Pixel rearrange based on ML method (Kitamura et al. 2004)	TOMBO	More accurate than in Tanida et al. (2001b)	High spatial resolution information cannot efficiently restore
IBP (Nitta et al. 2006)	TOMBO	Useful to restore high spatial resolution information	Time consuming
Scene-independent method (Kanaev et al. 2007)	TOMBO	Scene-independent; robust; stable and efficient	Have to first know relative subimage shift
Spectral-based blind method (El-Sallam and Boussaid 2008)	TOMBO	Do not require prior information; robust to additive noise	PSF of subimages needs to be known
IBP+depth estimated method (Horisaki et al. 2009)	TOMBO	Depth information is introduced to sharpen image	Computational error due to correlation method
Braiding algorithm (Oberdörster et al. 2011)	eCley	Near real-time	Imaging accuracy effected by estimated depth
MVE algorithm using lens diversity (Wood et al. 2005)	-	Multiple lenses provide more information	High cost due to multiple lenses
Shift & add algorithm (Li et al. 2007)	-	Have clearer edges	System PSF needs to be known
Signal-processing based method (Choi and Schulz 2008)	TOMBO	Very accurate if no noise exists	Margin oscillation effects; sensitive to noise
Wiener filter method (Tudela et al. 2008a, b)	APCO	Simple principle and easy implementation	PSF needs to be known; sensitive to noise

403 (2012a) proposed a method, which combines segmentation-based adaptive support-weight
 404 approach with scale invariant feature transform, to estimate depth for TOMBO. In Gao et al.
 405 (2012b), the investigation indicates that the compound images could be treated as 4-D light
 406 field data and a Fourier slice algorithm was introduced for digital refocusing. In Jiang et al.
 407 (2014), a new method for eCley, which is based on the property of the intensity transitional
 408 area, was presented by Jiang et al. to measure the depth information.

409 4.1.3 Depth of field extension

410 Generally, the compact structure of artificial compound eyes leads to short focal length. To
 411 improve the performance of artificial compound images, the extension of the depth of field
 412 is also an important research topic in planar compound eye.

413 To extend the depth of field, Chan et al. proposed to incorporate TOMBO with a phase mask
 414 and they introduced a conjugate gradient method to obtain the final image (Chan et al. 2006a,
 415 2007). The final images obtained from two kinds of system structures, without phase mask
 416 and with phase mask, are shown in Fig. 18. On the other hand, in a conventional TOMBO
 417 system, lenses are placed on a flat surface, so this structure will result in the degradation
 418 of rays for far objects. This problem is solved by the irregular lens-array arrangement and
 419 the depth of field is extended in Horisaki et al. (2008, 2010). Figure 19 shows the irregular
 420 lens-array of TOMBO.

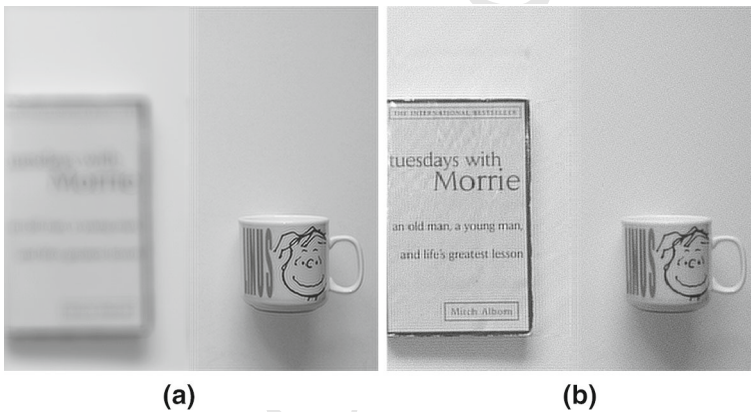
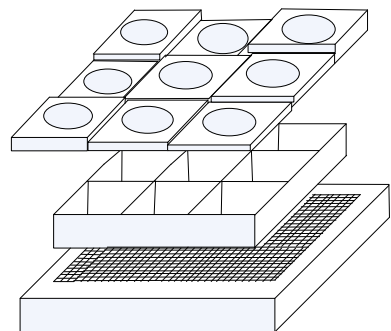


Fig. 18 The reconstructed images in Chan et al. (2006a)

Fig. 19 Irregular lens-array
 arrangement of TOMBO
 (Horisaki et al. 2008)



421 4.2 Curved compound eye

422 4.2.1 Large FOV imaging

423 The theoretical research of curved compound eyes mainly focuses on the large FOV imaging
 424 because curved compound eyes have the intrinsic features such as large FOV and less distort-
 425 tion in large incident angle. In [Huang and Xu \(2006\)](#), a seven-camera model was proposed to
 426 imitate curved compound eyes. In this model, the position of each camera is pre-determined;
 427 adjacent images have small overlapped areas; the final large FOV image is obtained by
 428 directly splicing the adjacent images; the connecting mark is eliminated by combining the
 429 pixel values of adjacent images in the transition area. But this is just a multi-camera model
 430 imitating the principle of the compound eye. A direct method splicing the ommatidia images
 431 of artificial compound eyes was proposed by [Cao et al. \(2012\)](#). The excellent image quality
 432 is achieved when the FOV is over 166° .

433 4.2.2 Performance analysis

434 In order to further improve the performance of the curved compound eye, some researchers
 435 also devote to the performance analysis of the curved compound eyes. In [Cheng and Lin](#)
 436 [\(2007\)](#), [Lin and Cheng \(2007, 2008\)](#), a novel spherical compound-like eye of a superposition
 437 type was presented, based on two different configurations; and how the number of eyelets
 438 impacts on the performance of the compound-like eye was tested and analyzed. In [Liu et al.](#)
 439 [\(2009a, b\)](#), a generalized compound eye detector array was proposed to detect and localize
 440 the particle emitting sources, in addition, the statistical analysis about the performance of the
 441 compound eye array was analytically and numerically derived by computing Cramér-Rao
 442 bounds on the errors in estimating the direction of the incident particles. Many impact factor,
 443 such as Signal-to-Noise Ratio, the number of eyelets in the array, the number of detectors in
 444 each eyelet, were analyzed to illustrate the properties and performance of the array.

445 5 Applications of artificial compound eyes

446 Due to the fast advance of the fabrication and imaging techniques of artificial compound eyes,
 447 much attention has been increasingly paid to their various applications. In what follows, we
 448 review the applications from planar artificial compound eye to curved compound eye, like in
 449 Sect. 4.

450 5.1 Applications of planar artificial compound eyes

451 The compact structure and the good capacity of depth estimation are very useful in tiny
 452 equipments, so the planar artificial compound eye have been successfully applied to various
 453 fields, such as security systems, medical instruments, tiny scanners and projectors.

- 454 1. Security systems: [Shogenji et al. \(2004\)](#) presented a fingerprint capturing system, which
 455 combines TOMBO system with a light-guide plate. Each unit of TOMBO captures a
 456 partial fingerprint and the final fingerprint image is obtained by combining all the unit
 457 images. The resolution 1727 dpi of the fingerprint image can be obtained.
- 458 2. Medical instruments: In medical devices, endoscopes-based surgical techniques are
 459 widely used. Conventional endoscopes have great difficulty in the estimation of the exact

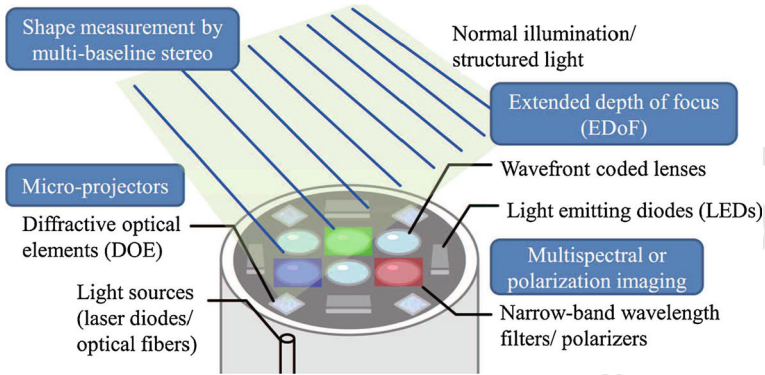


Fig. 20 Architecture and functions of TOMBO endoscope [Kagawa et al. \(2012c\)](#)

size of a lesion due to the lack of depth information. Applying the capacity of TOMBO in depth estimation, Yamada and Kagawa et al. invented a 3D endoscope system with the functions of extended depth of focus (EDoF), depth estimation, multispectral or polarization imaging ([Yamada et al. 2005](#); [Kagawa et al. 2012a, b, c](#)). The architecture and functions of the TOMBO endoscope are shown in Fig. 20. As the intraoral diagnosis is very important to keep one's teeth healthy, Kagawa et al. created an active 3D shape measurement system with TOMBO ([Kagawa et al. 2009a, b](#)), which can be put into a narrow intraoral space. A horizontal stripe was introduced into the 3D shape measurement system as a structure pattern because the large textureless intraoral regions will lead to incorrect depth estimation. In [Lai and Meng \(2013\)](#), a MRI compatible SPECT system called MRC-SPECT-II was introduced based on an artificial compound eye gamma camera. This SPECT system is very compact and could obtain peak geometry efficiency about 1.5 %, while modern pre-clinical SPECT systems can gain the typical level of 0.1–0.01 %. This SPECT system could potentially take simultaneous MRI/SPECT imaging.

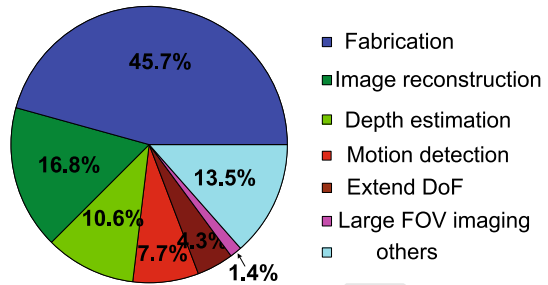
3. Tiny scanners and projectors: The conventional front-projection systems for free-form screens always require a trade-off between the system complexity and achievable performance, the compound eye structures could potentially use to handle this problem. A microoptical array projector was proposed by [Sieler et al. \(2012, 2013\)](#), and a novel slide pre-processing algorithm was presented to get the final projected image. A high-speed 3D array projector was proposed by [Heist et al. \(2013\)](#), and a combination of Gray code and phase-shifted sinusoidal fringes was used for depth estimation. A compact and large FOV image scanner was proposed by [Kawano et al. \(2013\)](#), which has the optical track length with 32 mm and the track width with 40 mm.

5.2 Applications of curved compound eyes

The large FOV of curved compound eyes is very useful for autonomous navigation and motion detection.

1. Autonomous navigation: In [Leitel et al. \(2014\)](#), [Pericet-Camara et al. \(2014\)](#), the CurvACE system was reported to directly applied in the autonomous navigation system. In this system, the optical flow method was used for navigation.
2. Motion detection: [Neumann et al. \(2003, 2004\)](#), a polydioptric camera, which is able to estimate its 3D motion by using an independently linear algorithm of scene, was invented. [Krishnasamy et al. \(2004a, b\)](#), a compound-eye image sensor, named “DragonflEYE”,

Fig. 21 Statistical pie chart of artificial compound eye researches from 1994 to 2014



492 was designed for target tracking, and an extension of the vanishing-point calibration
493 method was also presented and evaluated.

494 In addition, a comprehensive survey about insect-like robots that navigate and control their
495 motion using biologically inspired visual strategies can be referred in [Franceschini \(2014\)](#).

496 6 Conclusions and future research lines

497 This paper provides a comprehensive survey on the bionic system, the artificial compound
498 eyes and the natural compound eyes. We review and analyze the system design, theoretical
499 development and applications of artificial compound eye in terms of their two main types:
500 planar and curved artificial compound eyes.

501 Artificial compound eyes are regarded as *the promising next generation compact imaging*
502 *system*, due to their compact system structure, wide FOV and sensitivity to motion objects. A
503 pie chart shown in Fig. 21 indicates the statistical values (%) with respect to the numbers of
504 publications reported from 1994 to 2014. Among 210 papers, almost a half of researches are
505 concentrating on the fabrication of artificial compound eye; the percentage 16.8% implies
506 that the image reconstruction is the most concern in the theoretical development of artificial
507 compound eye. Given the current increasing research interest in artificial compound eye, we
508 think it is worth discussing some future research directions in this area that the researchers
509 envisage to further develop. In what follows, we list the future research lines from the design
510 and fabrication, theoretical development and applications of artificial compound eye, respec-
511 tively.

512 1. Design and fabrication of artificial compound eyes: Due to the compact structure, a very
513 small assembly error will result in huge quality deterioration in the manufacturing process
514 of artificial compound eye. So the fabrication technology and the design parameters need
515 to be further improved.

516 (a) How to treat the trade-off between field of view, resolution and sensitivity is
517 a challenging issue to enhance the imaging performance of artificial compound
518 eyes.

519 (b) Now the imaging performance of artificial compound eye is comparable to its natural
520 archetype, but compared with traditional cameras, the imaging performance of arti-
521 ficial compound eye needs to be greatly enhanced. A possible solution is to design a
522 new artificial compound eye with advanced imaging techniques.

523 (c) Now the image sensors are still placed in flat surface in the fabrication of a curved
524 compound eye, which results in much complexity of fabricating techniques for cor-

525 recting distortion. How to overcome this limitation is also an important research
526 issue.

527 2. Theoretical development: The theoretical study of artificial compound eye mainly focuses
528 on how to obtain the final high quality images by using various good and efficient methods
529 and algorithms so as to well mimic the natural compound eye.

530 (a) The quality of image, which is reconstructed by the artificial compound eye, mainly
531 depends on the accuracy of interommatidial angles and the shift estimation of adjacent
532 images. So it is very important to develop high-accuracy methods to estimate the
533 adjacent images shift.

534 (b) Interpolation methods are widely used in image reconstruction of artificial compound
535 eyes, but they always bring the edge blur effect. So the research of edge contour
536 enhancement methods needs to be further pushed. At the meantime, the PSFs of the
537 channels are available. This information could be used to regain some sharpness with
538 PSF deconvolution.

539 (c) The image reconstruction has to consider the parallax between the ommatidia of
540 artificial compound eye. This parallax depends on object depth. In fact, conventional
541 depth estimation methods in compound eye are quite time-consuming and also result
542 in estimation errors due to the short base line. The depth estimation could be deter-
543 mined either by correlating neighboring subimages, as the principle of light field
544 (Wanner and Goldluecke 2014), or by using the defocus measure (Tao et al. 2013).
545 So new and better depth estimation methods are required.

546 (d) Other features of natural compound eyes are also worth further researching. For
547 example, motion detection is one of the most important feature of natural compound
548 eyes, but only a very limited number of investigations related to motion detection
549 are reported in the community of artificial compound eyes. Therefore, any methods
550 or algorithms for better imitating insect compound eyes' functions are also worth
551 discussing.

552 3. Applications: The compact imaging structure and the wide field of view of artificial
553 compound eye are very attractive in downsizing the imaging devices, especially are very
554 necessary in the fields requiring tiny imaging instruments.

555 (a) Application in security systems: Nowadays, more and more attention is paid to prop-
556 erty security such as credit card safety. As usual, the thickness of the credit card is
557 less than 1 mm, how to well embed an artificial compound eye into ID cards or credit
558 cards to capture the users' fingerprints as an identification is a promising technique.

559 (b) Application in biomedicine area: Now internal examination is much straightforward
560 to check the symptom of a patient. The micro capsule robot is widely researched
561 to hope to be used in internal examination. Due to the compact structure and short
562 range imaging feature, artificial compound eye can be integrated into micro capsule
563 robots as the imaging system. This will greatly improve the diagnosis reliability of
564 the patients' symptoms.

565 **Acknowledgments** This work is supported by the National Natural Science Foundation of China (61373047),
566 the projects supported by the State Key Laboratory of Robotics No. 2014-O09, by Scientific Research Founda-
567 tion of CUIT under Grant No. J201508, by Scientific Research Fund of Sichuan Provincial Science &
568 Technology Department under Grant No. 2015GZ0304, and by Fund of Robot Technology Used for Special
569 Environment Key Laboratory of Sichuan Province No. 14zxtk04.

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