

Use of response surface methodology (RSM) to optimize pea starch-chitosan novel edible film formulation

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1 **Use of Response Surface Methodology (RSM) to Optimize Pea Starch-Chitosan Novel**
2 **Edible Film Formulation**

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22 **Abstract** The aim of this study was to develop an optimal formulation for preparation of an
23 edible film from chitosan, pea starch and glycerol using response surface methodology (RSM).
24 Three independent variables were assigned comprising chitosan (1-2%), pea starch (0.5-1.5%)
25 and glycerol (0.5-1%) to design an empirical model best fit in physical, mechanical and barrier
26 attributes. Impacts of independent variables on thickness, moisture content (MC), solubility,
27 tensile strength (TS), elastic modulus (EM), elongation at break (EB) and water vapor
28 permeability (WVP) of films were evaluated. All the parameters were found to have significant
29 effects ($p < 0.05$) on physical and mechanical properties of film. The optimal formulation for
30 preparation of edible film from chitosan, pea starch and glycerol was 1% chitosan, 1.5% pea
31 starch and 0.5% glycerol. An edible film with good physical and mechanical properties can be
32 prepared with this formulation and thus this formulation can be further applied for testing on
33 coating for fruit and vegetables.

34 **Keywords** Pea Starch. Chitosan. Plasticizer. Edible films. Box-Behnken Design

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44 **Introduction**

45 Many efforts have been made to develop and test edible films for further utilisation to extend
46 shelf life of fresh produce (Arnon et al. 2014; Dhall 2013; Gómez-Estaca 2009; Valencia-
47 Chamorro et al. 2010). Chitosan has been found to have a great potential for wide range of
48 application in formulation of edible films due to its biodegradability, biocompatibility,
49 antimicrobial activity and non-toxicity (Pelissari et al. 2009; Sánchez-González et al. 2010).
50 Pea starch has small granules size, 2-40 μ m (Ratnayake et al. 2002) and high amylose content
51 (60-70 %) (Hilbert and Macmasters 1945), thus it can provide a good transparent film with
52 good physical, and mechanical properties with composite materials. Glycerol has been widely
53 used as plasticizer for development of starch based films (Santacruz et al. 2015).

54 Previous studies indicated that physical and mechanical properties of the films could be
55 significantly affected by ingredients concentration of the formulation (van den Broek et al.
56 2015; Zhang et al. 2015). RSM was applied for optimisation because it has been useful in
57 finding the relationships between different independent and response variables while
58 minimizing the number of experiments and usage of resources (Dailey and Vuong 2016). The
59 findings of this study can be utilised for further application on coating fruit and vegetables.
60 Therefore the aim of this study was to develop an optimal formulation for preparation of edible
61 film from pea starch, chitosan and glycerol using RSM.

62 **Material and methods**

63 **Materials**

64 Chitosan (medium molecular weight Poly (D-glucosamine) deacetylated chitin, $\geq 75\%$
65 deacetylated) and acetic acid were purchased from Sigma-Aldrich USA. Pea starch was
66 supplied by Yantai Shuangta Food Co. Ltd China and was used as a film forming material.
67 Glycerol was purchased from Ajax Finechem Pty Ltd. Australia.

68 **Edible Film Preparation**

69 Films were prepared by the casting process and dehydrating the suspension solution in petri
70 plates. Suspension solution was prepared by dissolving 1 g chitosan (1-2 %) in 100 ml of 0.7
71 % (v/v) of aqueous acetic acid solution (Maciel et al. 2014). Pea starch powder (0.5-1.5 %) was
72 mixed to the above solution under control heating conditions (80°C) with continuous stirring
73 until the gelatinization temperature was reached. The ranges of chitosan (1-2 %), pea starch
74 (0.5-1.5%) and glycerol (0.5-1%) were selected based on previous studies (Chillo et al. 2008;
75 Maran et al. 2013b; Santacruz et al. 2015) and our preliminary studies (results not shown). The
76 film forming dispersion solution of starch-chitosan was cooled to room temperature before
77 glycerol (plasticizer; 0.5-1%) was added. The solution was stirred for further 20 minutes to
78 allow through mixing and removal of air bubbles. Film forming suspension solution (about 20
79 g) was casted in the petri dishes (10 cm in diameter) and dried at 30 °C for 24 hrs. Dried films
80 were peeled off and used for further analysis.

81 **Characteristics of pea starch-chitosan film**

82 **Physical properties**

83 **Thickness**

84 The thickness of film was measured according to previously reported method (Saber et al.
85 2015) using a digital micro-meter (Mitutoyo, Co., Model ID-F125, Japan). The sensitivity of
86 the instrument was 0.001 mm. Film sample was placed under the probe and thickness values in
87 mm was recorded. Random value from at least 10 different points was noted for individual film
88 sample and average was calculated. Results from thickness measurement were also used for
89 further calculation of water vapour permeability (WVP) of the samples.

90 **Moisture content (MC)**

91 Films were cut into 15 x 40 mm strips and placed into the aluminum dishes for drying at 110
92 °C for 24 hrs. Films were then cooled for 2 hrs after removal from the oven and the weight was
93 measured using a four decimal balance (HA-180 M, A & D company Ltd, Japan). MC was
94 calculated based on weight difference (Eq. 1). All the measurements were carried out in
95 triplicate and the values are expressed as means ± standard deviations.

$$96 \quad MC(\%) = \frac{M_i - M_f}{M_i} \times 100 \quad (1)$$

97 **Solubility**

98 Solubility of film was measured according to the method reported in a previous study (Ojagh
99 et al. 2010). Film specimens (40 × 15 mm) were dried to a constant weight at 110°C for 24 hrs.
100 Each sample was then placed into the glass-jar containing 50 ml of distilled water and
101 subsequently shaken at 25 rpm at room temperature for 24 hrs. Undissolved portion of the film
102 was collected and dried in the oven at 110°C for 24 hrs to reach a constant weight. Solubility
103 was calculated based on weight difference as shown in Eq. 2.

$$104 \quad S(\%) = \frac{S_{initial} - S_{final}}{S_{initial}} \times 100 \quad (2)$$

105 **Barrier properties**

106 **Water vapour permeability (WVP)**

107 Gravimetrically method, ASTM E96 procedure (ASTM 1996), with a 75 % RH gradient at
108 25°C was used to measure the WVP of the film. Permeation cells (0.7065 mm² film area)
109 containing anhydrous CaCl₂ (0 % RH) were sealed tightly by the sample film using parafilm.
110 Covered permeation cells were placed in a desiccator having saturated NaCl solution (75 %
111 RH). RH inside the permeation cell was always lower than outside, and water vapour transport
112 was determined using the weight gain of the cell at a steady state of transfer. Changes in the

113 weight of the cell were recorded and plotted as a function of time. The slope of each line was
114 evaluated by linear regression ($R^2 > 0.99$), and the water vapour transmission rate was
115 calculated through the slope of the straight line (g/s) divided by the test area (m^2). After the
116 permeation tests, the film thickness was measured and WVP ($g Pa^{-1}s^{-1}m^{-1}$) was calculated as:

$$117 \quad WVP = \frac{\Delta m}{A \Delta t} \frac{X}{\Delta P} \quad (3)$$

118 $\Delta m/\Delta t$ = weight of moisture gain per unit time (gs^{-1}) and can be calculated by the slope of the
119 graph. A= area of the exposed film surface (m^2), T = thickness of the film (mm), ΔP = represents
120 the water vapour pressure difference inside and outside of the film (Pa) (Saber et al. 2015).

121 **Mechanical properties**

122 The mechanical properties of the films were determined according to the method described by
123 (Saber et.al 2015) with modification using a Texture Analyzer (LLOYD Instrument LTD,
124 Fareham, UK). Film specimens (15× 40 mm) were used for all mechanical tests. The maximum
125 load (N) and extension (mm) curves were recorded to calculate tensile strength (TS), elongation
126 at break (E) and Elastic Modulus (EM) of the films using a tensile test at crosshead speed of 1
127 mm/s and initial grip distance 40 mm.

128 **Experimental design and statistical analysis**

129 **Response surface methodology (RSM)**

130 The statistical analysis and regression model study was performed with JMP software (Version
131 22, SAS, Cary, NC, USA). A Box-Behnken design at three levels for each independent
132 variables at three center points replicates was employed for study. Fifteen different edible
133 coating formulations comprising chitosan (1-2 %), pea starch (0.5-1.5%) and glycerol (0.5-1%)
134 were used to get the best optimal combination. Effect of polysaccharide biopolymers blended

135 with plasticizer (independent variables) on properties of casted film (response functions, Y)
 136 comprising thickness, WVP, solubility, moisture content, elongation at the break, elastic
 137 modulus, and tensile strength, was observed. In the process of optimization of coating
 138 formulation, response variables were related to independent variables by a second order
 139 polynomial equation (Eq. 4).

$$140 \quad Y = \beta_0 \sum_{i=1}^k \beta_i X_i + \sum_{i=1}^{k-1} \sum_{\substack{j=2 \\ i < j}}^k \beta_{ij} X_i X_j + \sum_{i=1}^k \beta_{ii} X_i^2 \quad (4)$$

141 X_i = independent variables

142 β_0 = intercept

143 $\beta_i, \beta_{ii}, \beta_{ij}$ = regression coefficients for intercept, linear, quadratic, and interaction terms

144 k = number of variables

145 The independent variables and their code variable levels are shown in Table 1. The JMP
 146 software was also employed to develop the model equations, to graph 3D plots, 2D contour
 147 plots of the responses, as well as predicting the optimum conditions of the independent
 148 variables. The three independent variables were assigned as: X1 (chitosan concentration %),
 149 X2 (pea starch, %) and X3 (glycerol, %). Thus, the function containing these three independent
 150 variables is expressed as follow

$$151 \quad Y = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_3 x_3 + \beta_{12} x_1 x_2 + \beta_{13} x_1 x_3 + \beta_{23} x_2 x_3 + \beta_{11} x_1^2 + \beta_{22} x_2^2 + \beta_{33} x_3^2$$

152 (5)

153

154 **Statistical analysis**

155 JMP (Version 11, SAS Cary, NC, USA) was used to predict the optimal conditions of
156 independent variables using 3D contour plots. Analysis of variance ANOVA, the coefficient
157 of determination (R^2) and adjusted the coefficient of determination ($Adj-R^2$) were used to
158 assess the validity of the model. Analysis of variance (one-way ANOVA) was used to compare
159 the mean differences of the samples. SPSS 16.0.0 statistical software for windows (SPSS IBM,
160 USA) was used for data treatment and statistical analysis. Comparison of the mean was
161 considered to be statistically significant at $P < 0.05$.

162 **Results and discussion**

163 **Fitting of the model**

164 Different analysis sources of variation, such as lack of fit, R^2 , Predicted Residual Sum of Square
165 (PRESS) for the models, F ratio and Prob > F were analyzed to identify the fitting of the RSM
166 mathematical models. The results (Table 2 and Fig. 1) showed that the value of the coefficient
167 of determination (R^2) was in the range of 0.79 to 0.97, reflecting that at least 79 % of the
168 predicted values could be matched with the actual values. Values of F ratio for physical
169 parameters (thickness, solubility and moisture content) (2.791, 3.26 and 2.84) and lack of fit
170 (0.5, 0.51 and 0.78) showed that the designed model was efficient in predicting the physical
171 properties of the film.

172 For barrier properties of the film, statistics showed that values of PRESS, F value and lack of
173 fit were 1377.8, 3.26 and 0.51, indicating that the mathematical model is a good predictor of
174 WVP of film (Table 2). The results also indicated that predicted model for mechanical
175 properties of the film had high PRESS values for EM, EB and TS (957664.1, 38.65 and 89595)

176 and the coefficient of determination (R^2) ranged from 0.79 to 0.94, indicating that the model is
 177 also reliable for predicting the mechanical properties of the chitosan-pea starch edible film.

178 **Empirical model for prediction of film properties**

179 Through applying multiple regression analysis on the experimentally attained data, the
 180 empirical model was developed by fitting the experimental data obtained from Box-Behnken
 181 design into second order polynomial mathematical equation (Eq. 4). The model could be fitted
 182 to the following second order polynomial equations (6) – (12). In order to investigate the
 183 relationship between process variables and response variables from the developed
 184 mathematical model equations 3D contour plots were constructed between two independent
 185 variables while keeping the 3rd variable constant.

$$186 \quad Y_{Thickness} = 0.11 + 0.01845x_1 + 0.00923x_2 + 0.017x_3 + 0.000725x_1x_2 +$$

$$187 \quad 0.00287x_1x_3 + 0.018x_2x_3 - 0.0074x_1^2 - -0.00143x_2^2 - 0.0038x_3^2 \quad (6)$$

$$188 \quad Y_{WVP} = 10.66 + 7.31x_1 + 4.52x_2 - 1.225x_3 + 4.315x_1x_2 - 1.0425x_1x_3 + 2.062x_2x_3 +$$

$$189 \quad 3.36x_1^2 + 0.9316x_2^2 - 0.6808x_3^2 \quad (7)$$

$$190 \quad Y_{Solubility} = 49.98 - 1.15x_1 + 0.392x_2 + 2.8x_3 + 3.185x_1x_2 - 1.64x_1x_3 - 4.175x_2x_3 -$$

$$191 \quad 2.28x_1^2 - 0.919x_2^2 + 0.660x_3^2 \quad (8)$$

$$192 \quad Y_{Moisture} = 29.47 - 6.31x_1 - 3.90x_2 + 6.67x_3 + 1.95x_1x_2 - 1.23x_1x_3 + 0.445x_2x_3 -$$

$$193 \quad 1.1929x_1^2 - 0.262x_2^2 - 2.395x_3^2 \quad (9)$$

$$194 \quad Y_{Elastic modulus} = 354.9 + 213.18x_1 + 591.28x_2 - 926x_3 + 90.39x_1x_2 - 381.9x_1x_3 -$$

$$195 \quad 1325x_2x_3 - 399.9x_1^2 + 595.7x_2^2 + 834.85x_3^2 \quad (10)$$

$$196 \quad Y_{Elongation at break} = 5.5 - 1.47x_1 - 1.325x_2 + 0.725x_3 + 0.65x_1x_2 - 0.4x_1x_3 +$$

$$197 \quad 0.35x_2x_3 + 0.275x_1^2 + 0.525x_2^2 + 0.27x_3^2 \quad (11)$$

198 $Y_{Tensile\ strength} = 57.61 + 37.20x_1 + 37.32x_2 - 42.05x_3 + 0.918x_1x_2 - 8.05x_1x_3 -$
199 $46.6x_2x_3 + 2.43x_1^2 + 20.42x_2^2 + 26.50x_3^2$ (12)

200 **Effect of operating parameters on properties of film**

201 **Thickness**

202 Thickness affects the structure of film in relations of drying kinetics, WVP and film opacity
203 (Maran et al. 2013a). Results showed that thickness varies from 0.06 mm to 0.16 mm with the
204 change in the amount of dry matter in film suspension solution (Table 1). Analysis results
205 showed that chitosan and glycerol had a significant impact on the thickness of the film (Table
206 2) whereas, starch did not show any significant impact on thickness of the film ($p > 0.05$). In
207 addition, the results in Fig. 2 (a) showed that higher the content of chitosan resulted in the
208 formation of film with greater thickness. Chitosan is a positively charged molecule and being
209 a positively charged moiety it have wide hydration layers with highly retained water molecules
210 which participates in the film structure thus inhibiting the chain approximation and giving rise
211 to thicker films. Similar explanation related to the chitosan concentration and thickness of the
212 films has been reported previously in the literature (Bonilla et al. 2013). The other possible
213 explanation could be the over loading of the suspension solution. Unoptimized formulations in
214 most of the previous studies is subject to increase in the unwanted film thickness as a result of
215 overloading of suspension solution which hinders the permeability control of film eventually
216 (Bof et al. 2015). Correlation between permeability properties and thickness can be explained
217 by fick's law of diffusion, which says that permeability is inversely proportional to the
218 thickness of the film. Hence higher the thickness lesser will be the mass transfer thorough the
219 film due to more resistance. Similar explanation has been provided in the literature on the water
220 vapour permeability and thicknes effect of hydrophilic films by McHugh et al. (1993).

221 **Water vapour permeability**

222 WVP is the main parameter used to explain the possible mass transfer mechanisms through the
223 film surface. For edible coatings it should be low to prevent moisture loss from the fresh
224 produce (Ma et al. 2008). The value of WVP varied significantly ($p < 0.05$) with the
225 concentration of polymer and plasticizer. Coating formulation comprising 1% chitosan; 0.5%
226 starch and 0.75% glycerol showed the minimum permeability values ($4.1 \times 10^{-10} \text{ gs}^{-1}\text{m}^{-1}\text{Pa}^{-1}$)
227 whereas increased concentration of starch and glycerol (1.5% pea starch and 0.75% glycerol)
228 resulted in to higher WVP response ($34.4 \times 10^{-10} \text{ gs}^{-1}\text{m}^{-1}\text{Pa}^{-1}$ (Table 1). Biopolymer-plasticizer
229 chemistry proposed a significant impact on WVP of the casted film. Binding between the NH_2
230 and OH functional groups forms a crosslinking network in the film structure and slow down
231 the rate of permeability. Fig. 2 (b) shows the behaviour of increasing starch concentration on
232 the film permeability attributes which could be due to the hydrophilic nature of starch that fails
233 to resist the migration of water through the film surface. These results are in line with the
234 previous study (Pelissari et al. 2009) where increased concentration of starch enhanced the
235 WVP rate. Another possible reason for these observations behaviour could be explained on the
236 basis of the oval granular structure of the pea starch, where the arrangement may leave some
237 inter-granular spaces which at lower concentration are filled by other partaking ingredients but
238 at higher concentration are available for free mass transfer. The WVP of the coated film
239 gradually decreased as the concentration of chitosan increased from 1 to 2% (Table 1). The
240 decreasing WVP value may be due to hydrophobic acetyl group of incompletely deacetylated
241 chitosan or due to intense hydrogen bond interactions between NH_2 and OH functional groups.
242 These interaction may be dominated over hydrophilic interactions thus reducing the availability
243 of free hydrophilic groups at lower starch concentration. Glycerol also increases the mobility
244 by reducing the rigidity and destabilisation of chain arrangements (by easily interacting with
245 the starch chain) by minimizing the starch intermolecular and intramolecular hydrogen bonds

246 with starch-glycerol hydrogen bonds which disrupted the crystalline pattern of starch and
247 facilitates the movement of water (Singh et al. 2009; Xu et al. 2005).

248 **Solubility**

249 Water solubility describes the water resistance and integrity of the edible film. Solubility of the
250 chitosan-starch film was significantly affected by glycerol and chitosan concentrations
251 ($p < 0.05$). Results showed that the solubility of casted film was in the range of 40.8 to 55.2%
252 and increases with the increase in glycerol concentration (Table 1; Fig. 2c) and decreases with
253 higher chitosan concentration. The possible reason may be due to glycerol which can disrupt
254 the crystalline structure of the starch and causes breakage of hydrogen bonds and formation of
255 new hydrogen bonds between exposed OH group of amylose and amylopectin and glycerol
256 (Ratnayake et al. 2002). These findings are also in agreement with the previous reported work
257 (Maran et al. 2013a; Mehyar and Han 2004). These results could be explained from the fact
258 that higher chitosan concentration induces the strong interactions between the two polymers
259 and lowers the resulting solubility. These observations supports the previous studies where
260 the solubility proportionally decreased as starch was blended with chitosan at higher
261 concentration (Bourtoom and Chinnan 2008; Kanmani and Lim 2013).

262 **Moisture content (MC)**

263 MC describes the available moisture present in the film. Variations in the moisture content are
264 shown in the Fig. 3 (a). Glycerol and starch were found to affect the moisture level in the film
265 significantly ($p < 0.05$) and MC was higher at higher concentration of glycerol, 1% (Table 1).
266 This may be due to the hydrophilic nature of the glycerol which assist in the formation of
267 hydrogen bonding with free OH groups (Cerqueira et al. 2012). Similar results were reported
268 in previous studies on the increasing effect of glycerol on MC (Saber et al. 2016; Sanyang et
269 al. 2015b). Starch also facilitates the retention of MC (due to its hydrophilic nature) in films as

270 compared to chitosan (Fig. 3a). Lower MC at higher chitosan concentration may be due to
271 higher interactions among the molecules leaving behind no free hydrophilic groups for
272 interaction with the water molecules.

273

274

275 **Mechanical properties: Tensile strength (TS), Elongation at break (EB) and Elastic**
276 **modulus (EM)**

277 TS is an important property of the films as it greatly affects the utility of the film for its
278 application in shelf life extension of fresh produce during storage. The stability of film was
279 measured on the basis of TS, EB, and EM. Fig. 3 (b-e) shows the effect of additives on the
280 mechanical properties of edible film. Pea starch and chitosan blend provided a film with good
281 mechanical properties which illustrate the compatibility of hydrocolloids. TS, EB and EM
282 values of chitosan– pea starch film are presented in Table 1. It was found that strength of the
283 film was significantly affected by varying polymeric concentration ($p < 0.05$). TS was maximum
284 with 1.5% chitosan and 1.5% of starch blended with lowest concentration of glycerol (0.5%)
285 and depicts the greatest integrity of film forming components. TS varied between 26.6 to 266.9
286 N/m (Table 1). This is due to the formation of dominating inter-molecular hydrogen bonding
287 between NH_2 and OH groups of chitosan-starch which increases with the increase in polymer
288 concentration. Interaction of polymers increases the stability because of the participating
289 functional groups in the bonding. Chitosan-starch hydrogen bonding is the intrinsic factor
290 which supports the mechanical and physical properties of the film. These results are in
291 agreement with previous research where tensile properties of starch films were improved
292 significantly when chitosan was incorporated in to the starch solution (Xu et al. 2005; Zhai et
293 al. 2004).

294 It is important to note that plasticizer also has a significant ($p < 0.05$) effect on the TS of the film
295 (Fig. 3c). TS increases with the decrease in the plasticizer concentration and was maximum
296 (266.9 N/m) at 0.5% glycerol. This phenomenon can be explained by the role of glycerol on
297 diminishing the strong intra-molecular hydrogen bonding between starch and chitosan
298 molecules as previously reported by Sanyang et al. (2015a). The effectiveness of glycerol for
299 TS reduction is due to hydrophilic nature of the compound which hold more H₂O molecules
300 and resulted in to more intense plasticizing effect. This arrangement increases the spatial
301 difference between the polymer chains and decrease the TS. Moreover, a more vigorous
302 relationship between tensile properties and moisture content was observed portraying the
303 negative effect of moisture which might have caused extra plasticizing effect hence lower the
304 tensile strength of starch film. The results are in line with the previous study reported by
305 Chinma et al. (2015) which showed that tensile properties of starch films decreased with
306 increase in film humidity.

307 The % E and EM varies between 3.4-10.5 mm and 191.4-5815.4 N/m² respectively (Table 1).
308 % E was greater when higher chitosan concentration was applied and lower with higher starch
309 concentrations. Both chitosan and starch were found to affect the elongation property of films
310 at a significant ($p < 0.05$) rate. Similarly EM value was higher for 1% chitosan, 1.5% starch and
311 0.5% glycerol (5815.4 N/m²) and minimum with higher concentration of glycerol. High starch
312 concentration results in a lower ability of edible film for stretching where plasticizer influences
313 the flexibility of film by occupying the free space between the polymers.

314 **Optimization and validation of coating formulation**

315 Optimal edible film formulation was achieved by optimizing chitosan, starch and glycerol for
316 physical, mechanical and barrier properties. RSM was used for the optimization of the coating
317 formulation. Based on the effect of independent variables (chitosan, starch and glycerol) on the

318 response values for physical and mechanical properties of film, the optimal conditions for
319 fomulation of this film were determined to be chitosan 1%, starch 1.5% and glycerol 0.5 %.
320 To validate these predicted conditions, this fomulation was tested in triplcate experiments and
321 the results showed that the actual values for physical and mechanical properties were found to
322 be similar to the predicted values (Table 3). These results shows that this fomulation can be
323 applied to prepare the pea starch film with good physical and mechanical properties for further
324 utilisation.

325 **Conclusion**

326 RSM has been sucessfully applied to optimize the best fomulation for preparation of pea starch
327 film for further utilisation in coating vegetable and fruits. All three tested ingridients (pea
328 starch, chitosan and glycerol) were found to have different effects on physical, and mechanical
329 properties of film. The results showed that optimal fomulation for preparation of pea starch
330 film were chitosan 1% pea starch 1.5% and glycerol 0.5%. which had satisfactory thickness,
331 good WVP, solubility, moisture content and mechanical properies. These findings can be
332 further applied for coating vegetables and fruit.

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438 **List of tables**439 **Table 1** Box- Behnken design employed for formulation of edible coating composition

Run	Independent variables					Dependent variables				
	Factors					Responses				
	X ₁ (%)	X ₂ (%)	X ₃ (%)	T (mm)	WVP × 10 ⁻¹⁰ (gs ⁻¹ m ⁻¹ Pa ⁻¹)	S (%)	M (%)	EM (N/m ²)	EB (mm)	TS (N/m)
1	1	1	0.5	0.0768	9.62	44.7	22.7	401.62	6.2	54.125
2	1	0.5	0.75	0.0736	4.16	52.7	42.1	681.93	10.5	26.64
3	1	1.5	0.75	0.0911	8.5	44.4	27.9	372.17	5.7	54.545
4	1	1	1	0.0841	5.09	53.1	40.4	372.79	8.2	30.46
5	1.5	0.5	0.5	0.0859	9.56	40.8	24.2	670.85	6.7	70.59
6	1.5	1.5	0.5	0.0677	10.56	52.6	18.0	5815.4	4.2	266.96
7	1.5	1	0.75	0.1246	16.25	54.0	31.0	191.50	5.6	65.64
8	1.5	1	0.75	0.1135	8.63	48.9	29.7	407.86	5.4	57.105
9	1.5	1	0.75	0.0919	7.12	47.1	28.0	465.56	5.5	50.105
10	1.5	0.5	1	0.1055	7.15	55.2	34.8	406.23	7.7	35.47
11	1.5	1.5	1	0.1596	16.4	50.3	30.3	249.92	6.6	45.165
12	2	1	0.5	0.1074	23.7	46.9	13.9	1970.9	4.7	149.015
13	2	0.5	0.75	0.1096	12.8	42.8	24.2	548.57	5.6	78.3
14	2	1.5	0.75	0.13	34.4	47.3	17.8	600.39	3.4	142.935
15	2	1	1	0.1262	15	48.8	26.6	414.15	5.1	93.145

440 Independent variables: X₁, = Chitosan (1-2%), X₂= Starch (0.5-1.5%), X₃= Glycerol (0.5-1%)441 Responses (Y): T= Thickness (mm); WVP= Water vapour permeability (gs⁻¹m⁻¹pa⁻¹); S= Solubility (%); M= Moisture (%); EM= Elastic modulus (N/m²); EB= Elongation at break (mm), TS= tensile strength (N/m).
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443 **Table 2** ANOVA study for the model fitting.

Parameters	T (mm)	WVP× 10 ⁻¹⁰ (gs ⁻¹ m ⁻¹ Pa ⁻¹)	S (%)	MC (%)	EM (N/m ²)	EB (mm)	TS (N/m)
Lack of fit	0.51	0.51	0.78	0.19	0.01	0.01	0.03
R ²	0.83	0.85	0.84	0.97	0.79	0.94	0.90
Adjusted R ²	0.54	0.59	0.54	0.91	0.40	0.84	0.71
F ratio of model	2.791	3.26	2.84	17.67	2.05	9.09	4.83
Prob>F	0.50	0.51	0.74	0.003	0.22	0.01	0.05
Press	0.0158	1377.8	338.5	376.0	957664.1	38.65	89595.6

444 WVP = Water vapour permeability (gs⁻¹m⁻¹pa⁻¹), S= Solubility (%), MC= Moisture content (%), EM= Elastic modulus (N/m²), EB= Elongation at
 445 break (mm), TS= Tensile strength (N/m).

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448 **Table 3** Validation of predicted values for physical, mechanical and barrier properties of pea starch: chitosan blended film.

Variables Response	Predicted value	Experimental value (n=3)
Thickness (mm)	0.055 ± 0.01	0.058 ± 0.03
WVP (gs ⁻¹ m ⁻¹ Pa ⁻¹)	5.29 ± 0.07	5.27 ± 0.03
Solubility (%)	45.53± 0.1	48.12±0.06
Moisture Content (%)	17.73±0.03	19.14±0.08
Elastic modulus (N/m ²)	3543.53 ±2.56	3559.25±5.69
Elongation at break (mm)	4.6±0.92	5.0 ±1.34
Tensile Strength (Nm ⁻²)	173.7±2.13	181.8± 1.78

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459 **Figure captions**

460 **Fig 1:** Correlation between predicted and experimental values for thickness (a), WVP (b), solubility (c), moisture content (d), tensile strength (e),
461 Elongation at break (f) and elastic modulus (g),

462 **Fig 2:** Response surface plots showing the interaction impact of independent variables on the thickness (a) WVP (b) and solubility (c) of the edible
463 film

464 **Fig 3:** 3 D Contour plots for moisture % (a), tensile strength (b-c), elongation at break (d) and Elastic modulus (e) showing the interaction impact
465 of independent variables on the pea starch: chitosan film

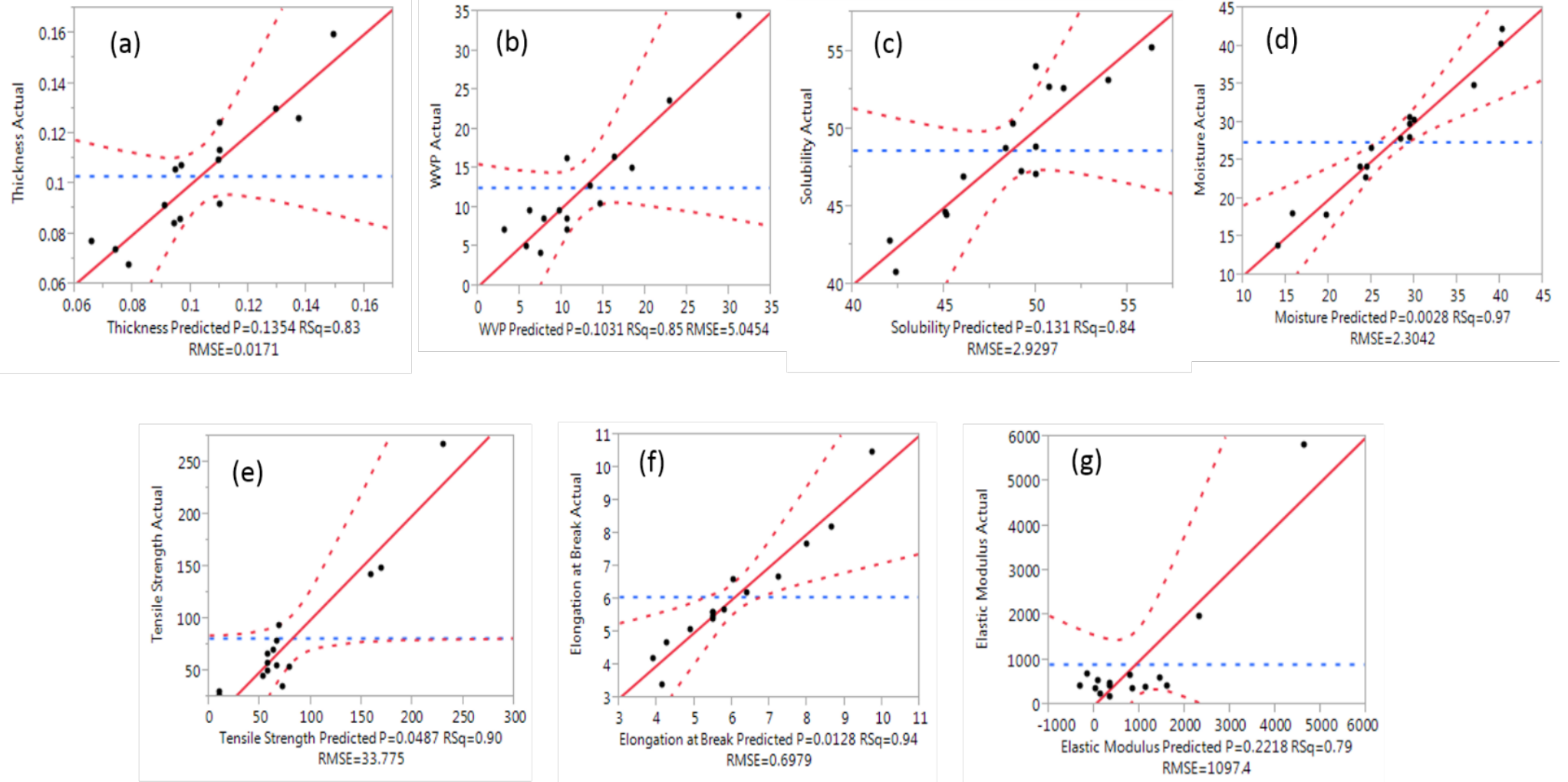


Fig 1

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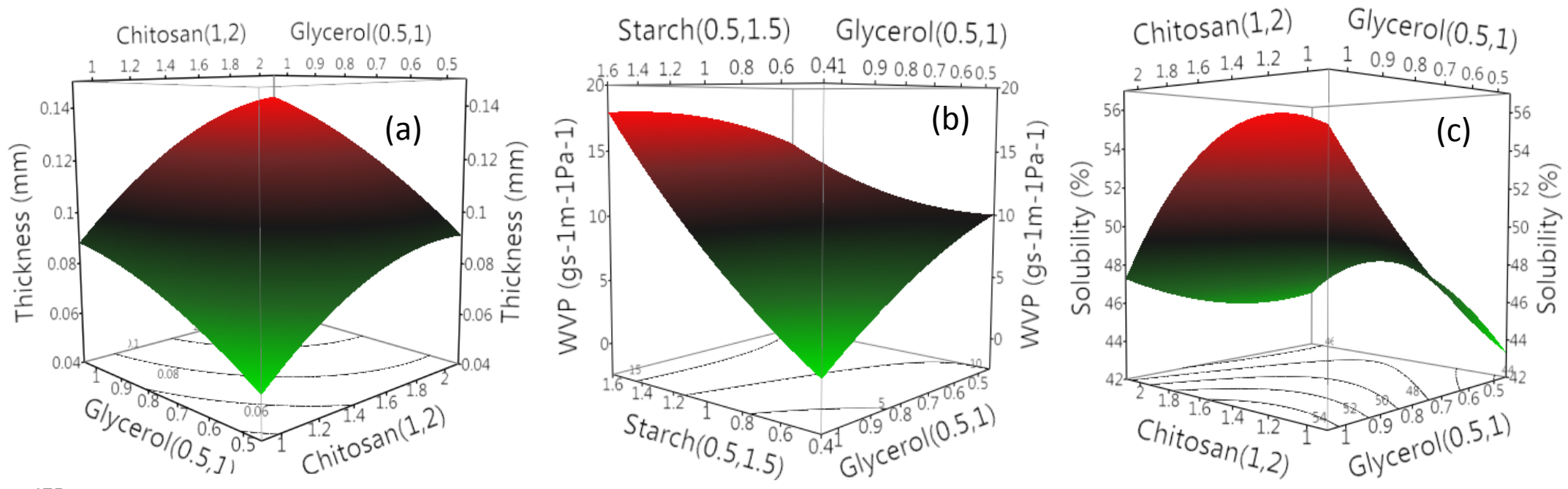
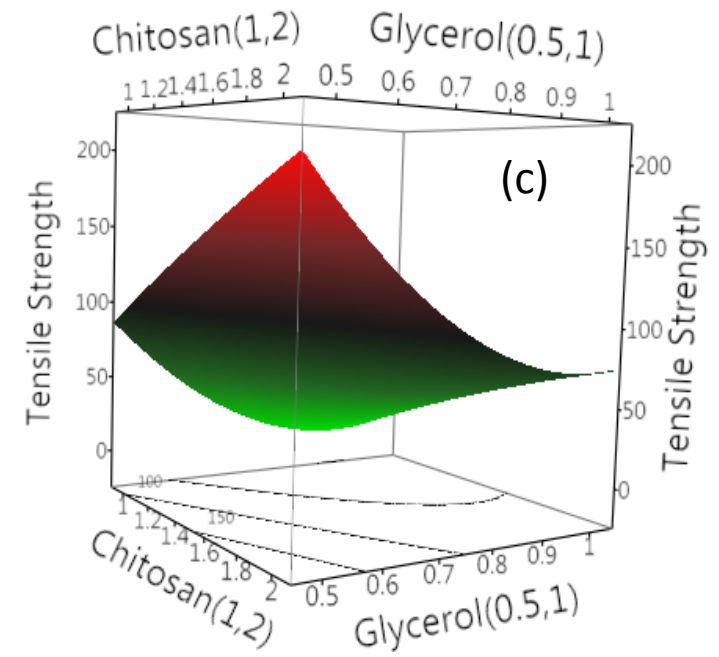
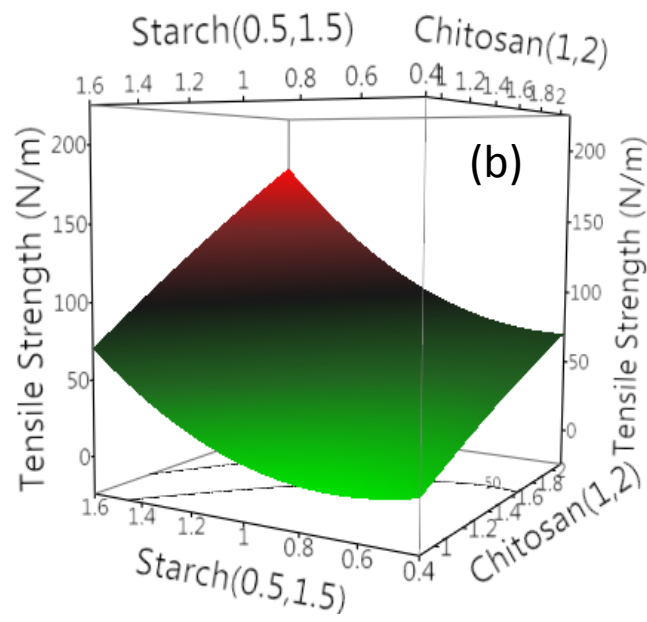
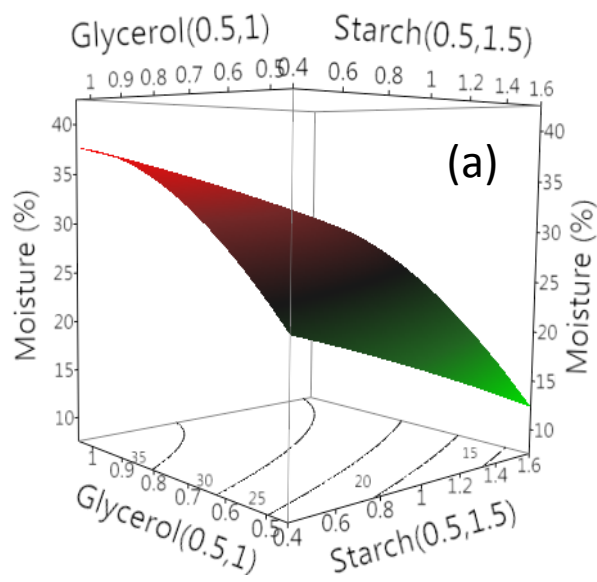


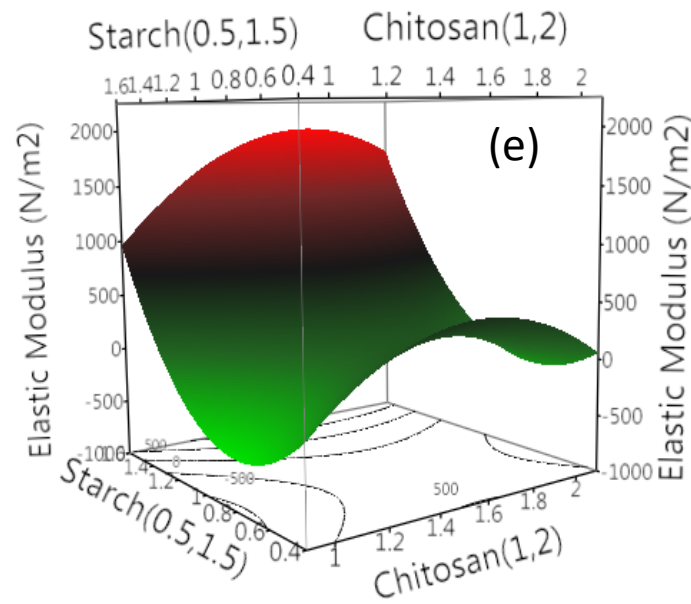
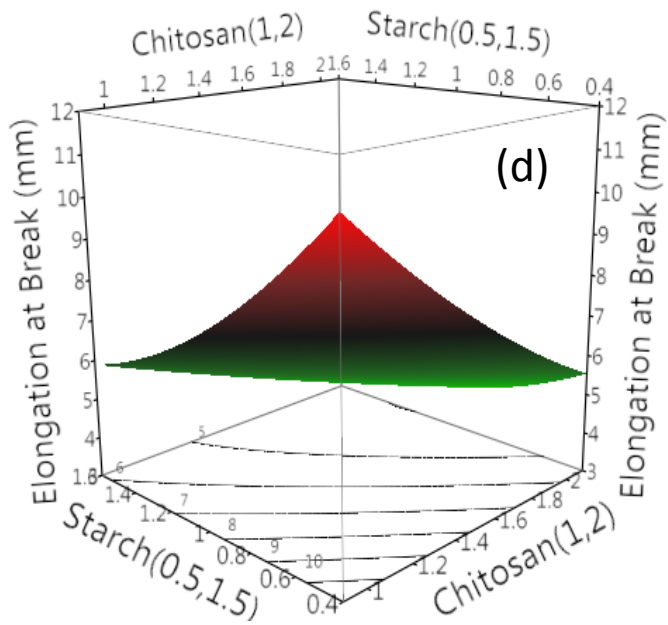
Fig 2

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Fig 3