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1 **Enhanced performance and hindered membrane fouling for the treatment of coal**
2 **chemical industry wastewater using a novel membrane electro-bioreactor with**
3 **intermittent direct current**

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11 **Abstract:** A membrane electro-bioreactor (MEBR) embracing biological treatment,
12 electrokinetic phenomena and membrane filtration was established by applying intermittent
13 direct current (DC) to MBR. MEBR exhibited significant improvement of treatment
14 performance and reduction of membrane fouling. COD and total phenols removal efficiencies
15 increased to 83.53% and 93.28% at an exposure mode of 24'-OFF/6'-ON, compared to
16 71.24% and 82.43% in MBR. Trans-membrane pressure increment rate declined dramatically
17 in MEBR, which was mainly attributed to the increase of sludge floc size and decrease of zeta
18 potential, soluble microbial products and specific resistance to filtration, resulted from
19 electrokinetic effects such as electrocoagulation, electrophoresis, electroosmosis and
20 electromigration of ions. It was notable that DC exposure exerted distinct evolution on
21 microbial community, with the improvement of microbial community richness and diversity.
22 The relative abundances of functional genera were promoted noticeably in MEBR. An
23 interactive relevance existed among microbial community structure, mixed liquor properties

24 and operational parameters.

25 **Keywords:** membrane electro-bioreactor; membrane fouling; electrokinetics; mixed liquor
26 properties; microbial community; relationship analysis

27 **1. Introduction**

28 New coal chemical industry has been rapidly booming in China due to the stresses of
29 environmental pollution and energy shortage according to the national energy development
30 strategy, which is a comprehensive utilization of coal resource in a cleaner way. However, the
31 coal gasification process, an indispensable procedure in coal chemical industry, discharges
32 enormous amount of high-strength wastewater containing various of toxic compounds and a
33 great number of refractory organic and inorganic pollutants such as phenolic compounds
34 (main organic pollutants), nitrogen-containing heterocyclic compounds (NHCs), polycyclic
35 aromatic hydrocarbons (PAHs), long chain hydrocarbons, ammonia, cyanide and thiocyanate
36 et al (Xu et al., 2016). The high-strength wastewater has posed great pollution risk to
37 ecological environment due to its toxicity and refractory, especially without appropriate
38 treatment (Hou et al., 2015; Xu et al., 2018). Membrane bioreactor (MBR) integrates
39 activated sludge process with membrane filtration and has been applied to the treatment of
40 domestic wastewater and various kinds of industrial wastewater as well as wastewater reuse
41 with the advantages of higher mixed liquor suspended solids (MLSS) and organic pollutant
42 loading, superior effluent quality, independent control of hydraulic retention time (HRT) and
43 solids/sludge retention time (SRT) et al (Barreto et al., 2017; Chen et al., 2017). The
44 conventional MBR refers to aerobic MBR. With the development of MBR technology,
45 anaerobic MBR (AnMBR) emerged for the complement of membrane biological system.
46 AnMBR allows energy recovery by conversion of organic matter into methane-rich biogas

47 during the anaerobic digestion(Martin Garcia et al., 2013; Ruigómez et al., 2017). Both types
48 of MBR have been considered as the preferential available technology with potential
49 application in water and wastewater treatment(Huang and Lee, 2015; Xie et al., 2016; Liu et
50 al., 2018). However, membrane fouling remains the major issue to be solved to ensure the
51 sustainability of this promising technology(Ahmed et al., 2018; Fan et al., 2018). The
52 reduction of flux and rise of trans-membrane pressure (TMP) caused by membrane fouling
53 resulted in the increase of operational costs and deterioration of effluent quality(Jia et al.,
54 2014; Meng et al., 2017). Generally, membrane fouling was classified as reversible
55 (recoverable by physical methods) and irreversible (including irreversible can be removed
56 through maintenance cleaning, irreversible that can be removed through chemical cleaning
57 and irrecoverable fouling) (Ibeid et al., 2013). Factors affecting membrane fouling include
58 membrane properties, influent and sludge characteristics (soluble microbial products (SMP),
59 floc size, colloids et al.) as well as operational conditions (MLSS, SRT, HRT et al.) (Tian et
60 al., 2011). Several approaches had been attempted to hinder membrane fouling (Iorhemen et
61 al., 2017). However, it can be concluded from the attempts that searching for an effective and
62 powerful method to reduce membrane fouling at an acceptable range remains a formidable
63 challenge. Recently DC was introduced to MBR for the enhancement of pollutant removal
64 and fouling reduction (Bani-Melhem and Elektorowicz, 2011; Jiang et al., 2017). Synergic
65 effects worked on the treatment processes in the integrated system. Electrodes were placed in
66 MBR to form electric field as well as involve electrochemical reactions. The activity of most
67 microbes could be promoted by adequate electric field stimulation, leading to the
68 enhancement of treatment performance. Small-size soluble and colloid components were
69 reduced by electrochemical effects to migrate membrane fouling. Some researchers inserted a

70 cathode inside the membrane to form electric field with an anode outside the membrane
71 module, in which the negatively charged extracellular polymeric substance (EPS) were forced
72 to move away from the membrane surface and then effectively attenuated the precipitation of
73 EPS on membrane surface and membrane fouling(Liu et al., 2012). However, this membrane
74 module with built-in cathode was complex and constrained by the module form and adversely
75 affected the integrity of membrane module. In addition, few studies focused on the treatment
76 of industrial wastewater and microbial community dynamics induced by DC in the system
77 were rarely conducted. The relationships among intermittent DC mode, properties of mixed
78 liquor and microbial community dynamics were not clear.

79 In the current study, membrane electro-bioreactor (MEBR) coupling of MBR and
80 intermittent DC with iron anode was constructed to treat coal chemical industry wastewater.
81 The primary objective of this research was to evaluate the performance of efficiency
82 enhancement and fouling reduction. The variations of sludge mixture properties (such as zeta
83 potential, floc size, SMP, specific resistance to filtration (SRF) et al.) were inspected to
84 analyze the possible mechanism in MEBR. The microbial community in MEBR was
85 investigated preliminary by the high-throughput sequencing technology. Moreover, the
86 relationships among intermittent DC mode, current density, properties of mixed liquor,
87 membrane fouling and microbial community dynamics were analyzed, which was conducive
88 to a deeper understanding of the mechanism and optimization control.

89 **2. Materials and methods**

90 **2.1 Materials**

91 Real coal chemical industry wastewater was obtained from the full-scale wastewater
92 treatment facility of a coal chemical industry plant in China, and the wastewater samples used

93 in this study were the effluent of anaerobic treatment process. The wastewater characteristics
94 were as follows: COD 1486.4 ± 102.4 mg/L, BOD₅ 253.3 ± 18.2 mg/L, total phenols 233.8 ± 21.2
95 mg/L, TOC 335.6 ± 22.3 mg/L, NH₄-N 127.2 ± 8.5 mg/L. The inoculum sludge was collected
96 from the A/O tank, with SVI of 88.

97 **2.2 Experimental procedure**

98 A cylindrical Plexiglas bioreactor with the volume of 3.0 L was used as the reaction
99 medium. A hollow fiber membrane module (normal pore size 0.4 μ m, effective surface area
100 0.02 m^2) was positioned at the center of reactor to construct MBR. In MEBR, stainless steel
101 plate and graphite plate were installed inside the bioreactor as anode and cathode. Both
102 electrodes with the same dimension of 3.0×3.0 cm were fixed on two plastic brackets with
103 the distance of 10 cm. The electrodes were connected with a DC power supply which was
104 controlled by a timer to achieve intermittent DC. Current density was maintained at 1.33
105 mA/cm^2 . Air was bubbled from diffuser at the bottom of the reactor to supply oxygen and
106 shear stresses on the membrane surface. The effluent from the membrane module was
107 withdrawn via a peristaltic pump at the mode of suction 9.0 min followed by a 1.0 min rest.
108 HRT was maintained at 18 hours. The bioreactors were operated at complete SRT, which was
109 to say, no sludge was discharged from the bioreactors during the whole process except the
110 samplings for the properties measurements of mixed liquor. A MEBR and a MBR (controlled
111 trials) were operated simultaneously. Electrical exposure mode was defined as the ratio of
112 time without current to time with current in a cycle of 30 min. In the trials for relationship
113 analysis, current density varied in the range of 0.5 - 1.33 mA/cm^2 , and exposure mode ranged
114 in 2-5.

115 **2.3 Analytical methods**

116 Floc particle size was measured as the mean particle size diameter (PSD) using the laser
117 diffraction particle size analyzer. Zeta potential was measured with the Zeta Sizer 3000
118 analyzer. The specific oxygen uptake rate (SOUR) was calculated from the linear regression
119 slope of the DO drop vs. time divided by the VSS concentration in the test chamber (Hou et
120 al., 2014). SRF was calculated with the Carman equation (Formula S1) based on the data of
121 filtrate volume versus time in vacuum filtration test. Proteins and polysaccharides contents in
122 SMP were measured calorimetrically following Dubois et al. (Dubois et al., 1956) and Lowry
123 et al. (Lowry et al., 1951) methods. Microbial community was analyzed via high-throughput
124 sequencing technology using Miseq Illumina followed by DNA extraction and PCR according
125 to the methods in the literatures (Ma et al., 2015; Jia et al., 2016). Membrane fouling rate was
126 evaluated by measuring the TMP increment over time. When TMP increased to >10 kPa,
127 membrane module was disassembled from the reactor and cleaned thoroughly with tap water
128 and then returned back to the reactor. The number of physical cleanings represented the
129 severity of the reversible fouling and was also used to evaluate membrane fouling.

130 **3. Results and discussion**

131 **3.1 Treatment performance and organics removal**

132 Treatment performances of MBR and MEBR at various electrical exposure modes were
133 illustrated in Fig. 1. Average COD and total phenols removal efficiencies in MBR were
134 71.24% and 82.43% respectively during 10 days stable operation. It can be seen that
135 performances in MEBR at all modes were higher than MBR except mode 2, demonstrating
136 that intermittent DC with iron anode enhanced the treatment performance of MBR. Average
137 COD and total phenols removal efficiencies in MEBR at mode 4 increased to 83.53% and
138 93.28% respectively. At mode 2, COD and total phenols removal efficiencies decreased to

139 62.61% and 73.19%. Enhancement of DC declined with lower electrical exposure (mode 5,
140 77.16% for COD, 89.58% for total phenols). Appropriate electrical exposure promoted
141 treatment performance, while excess electrical exposure (mode 2) constrained the
142 effectiveness. Large amounts of iron ion were generated when MEBR run at high electrical
143 exposure, and high concentration and precipitation of iron ion inhibited the activity of
144 microbes in the sludge, thus exerting adverse effect on the treatment performance. Moreover,
145 it was found that pollutant removal efficiency in MEBR exceeded the sum of removal
146 efficiency by MBR and that by single electrochemical effect (only electric field worked). For
147 example, the sum of COD and total phenols removal efficiencies by MBR and single
148 electrochemical effect were 73.62% (71.24%+2.38%) and 86.21% (82.43%+3.78%), lower
149 than that in MEBR at mode 4. The comparison implied that a synergic effect existed between
150 biodegradation and electrochemical effect in MEBR. Performance improvement at appreciate
151 electrical exposure mainly resulted from the changes of the mixed liquor and microbial
152 community in activated sludge. Therefore, changes in the properties of the mixed liquor and
153 microbial community were discussed in the subsequent section. Mode 4 was selected to
154 conduct the following tests as comprehensive consideration of performance, energy
155 consumption as well as electrode dissolution. In addition, less foam was observed in MEBR,
156 which prevented the biomass from reducing due to dehydration of sludge caused by foam,
157 guaranteeing the high treatment performance.

158 Organic compositions in the wastewater were detected via GC-MS (Table 1). The
159 contents of various organic compounds decreased in the effluents of MBR and MEBR.
160 Phenolic compounds were nearly completely removed, which was consistent with the high
161 removal efficiencies both in MBR and MEBR. Long-chain hydrocarbons and part of

162 nitrogenous heterocyclic compounds were residual in the effluent. Moreover, the contents and
163 number of main organic compounds in the effluent of MEBR were less than that in the
164 effluent of MBR, which was probably attributed to the synergic effect of MBR and
165 electrochemical effects and the variation of microbial community in MEBR. This also verified
166 the enhancement efficiency of MEBR.

167 **3.2 Membrane fouling**

168 TMP variation with operation duration in MBR and MEBR with MLSS of 4500 mg/L
169 was depicted in Fig. 2a. The increase of TMP in MBR and MEBR was similar at the first 25
170 days. However, the first washing time in MBR was the 33rd day, and that in MEBR delayed
171 to the 47th day. The membrane in the MBR was cleaned 3 times compared to only 1 time for
172 MEBR. Membrane fouling rates (expressed by TMP increment over time) in MBR during
173 each membrane washing were 0.23 kPa/d and 0.55 kPa/d, and that in MEBR was 0.20 kPa/d,
174 exhibiting significant fouling reduction with the addition of intermittent DC. The comparison
175 of TMP variation demonstrated that membrane fouling can be recovered better via physical
176 cleaning in MEBR than MBR. This is mainly attributed to the effect of intermittent DC on
177 microbes and properties of the mixed liquor, which lowered the contents of fouling
178 compounds (SMP, colloidal materials, VSS et al.) contributing to irreversible membrane
179 fouling. Moreover, TMP variation in MBR and MEBR with MLSS of 3000 mg/L was also
180 investigated (Fig. 2b). Membrane washing in MBR was 2 times compared 1 time for MEBR.
181 The comparison of different MLSS suggested that membrane fouling reduction by MEBR
182 with high MLSS (high fouling potential) was more significant than that with low MLSS (low
183 fouling potential). The superiority of MEBR was less pronounced when the sludge had a low
184 fouling potential, though noticeable.

185 **3.3 Changes in the properties of the mixed liquor**

186 Performance improvement and membrane fouling reduction in MEBR were associated
187 with significant changes in the properties of the mixed liquor. It was reported that SMP,
188 sludge floc size, SRF were the key components determining the sludge fouling potential(Ibeid,
189 Elektorowicz et al., 2013). The changes in the properties of the mixed liquor were analyzed,
190 which provide a quantifiable basis for estimating membrane fouling.

191 Zeta potential determines the capability of microbial flocs to aggregate. The zeta
192 potential of flocs in MBR increased slightly during the operation (average value from -17.6
193 mV to -24.7 mV), while a significant zeta potential reduction was observed in MEBR (Fig.
194 3a). The average value decreased to -12.1 mV in MEBR, which was attributed to the Fe ions
195 released from the anode via electrolysis. Fe ions neutralized the negative charge on the solid
196 surfaces and microbial flocs and thereby reduced the repulsive forces between the flocs. Fe
197 ions led to the coagulation of colloidal particles and sludge flocs. This change of zeta
198 potential reflected the possibility of bio-flocculation and the formation of larger floc size, as
199 discussed subsequently.

200 Floc PSD changed in a way that reflected the impact of DC field on floc morphology and
201 structure. Fig. 3b illustrated the PSD variations in MBR and MEBR. Floc PSD in MBR
202 maintained at 123.6 μm . In contrast, floc PSD increased from 96.6 μm to nearly 157.1 μm ,
203 and then decreased and stabilized at 134.1 μm . The initial increase was caused by the
204 electrocoagulation due to the suppression of diffuse double layer as the reduction in zeta
205 potential, during which organic particles formed larger flocs and colloidal solids were reduced.
206 The increase of floc PSD was also corroborated by enhanced movement of the charged solid
207 particles as a result of applying an electrical field. Subsequently floc size recession was

208 associated with the electroosmotic extraction of the tightly bound water from the flocs.
209 Furthermore, the sludge in MEBR with a higher percentage of inorganic solids was likely to
210 have less electrostatic attraction forces with bound water. Moreover, ferric hydroxides flocs or
211 flocs combined with other solids with smaller size shifted the floc size distribution toward
212 lower values. The floc size was likely to stabilize at a certain value based on the average size
213 of the hydroxide complexes and electrical density. The increase in floc size was widely
214 known to hinder membrane fouling (Tafti et al., 2015). Small particles depositing on the
215 membrane surface or inside the voids of the cake layer caused an increased membrane
216 resistance. The bound water within the sludge flocs was one main sludge property affecting
217 its fouling potential. The change in floc size increased floc PSD and declined bound water,
218 thus reduced membrane fouling significantly. In addition, sludge with large floc size, high
219 density was kept from being taken away with foam, guaranteeing the high biomass and
220 treatment performance.

221 It was evident that a significant reduction of SMP was observed in MEBR compared to
222 MBR (Fig. 3c). SMP in MEBR and MBR at 50th day were 29.24 and 51.37 mg/L respectively.
223 SMP was removed as a result of electrokinetic effects through which the ferric cations
224 neutralized the negatively charged particles. Proteins with high density of negative charge
225 reacted electrostatically with the ferric cations to form stable flocs. SMP was considered as a
226 major component causing membrane fouling (Tian, Chen et al., 2011). Electrokinetic effects
227 in MEBR had considerable contribution to the removal of SMP, which made the sludge and
228 the cake layer on membrane less viscous and cohesive. Thus, the filterability of sludge was
229 improved and membrane fouling was reduced.

230 A substantial reduction of SRF in MEBR was observed compared to that in MBR (Fig.

231 3d). SRF of mixed liquor in MBR was around 3.52×10^{13} m/kg, while that in MEBR stabilized
232 at 1.96×10^{13} m/kg. The reduction of SRF was mainly related to the changes of floc size, SMP,
233 flocs bound water resulted from electrokinetic effects such as electrocoagulation,
234 electrophoretic, electroosmosis, ions electromigration et al. SRF was in inverse proportion to
235 the square of particle diameter according to Carman-Kozeny equation (Bani-Melhem and
236 Elektorowicz, 2010). The increase in floc size caused by electrocoagulation in MEBR
237 declined the SRF and minimized membrane fouling. In addition, the reduction of
238 MLVSS/MLSS (from 0.8 to around 0.68) in MEBR also exerted positive effect on attenuating
239 SRF. The reduction of SRF facilitated the following processes for excess sludge treatment.
240 The reduction of MLVSS/MLSS was mainly related to electrocoagulation by the electrolysis
241 on the iron anode. Iron content of the sludge in MEBR was around 5%, compared to that of
242 0.35% in MBR. The iron flocs changed the water distribution in the sludge, thus improved the
243 dewaterability. The component of easily dewatered iron floc also facilitated the decline of
244 SRF and promotion of dewaterability.

245 SOUR was a major indicator of microbial activity. Microbial activity expressed by
246 SOUR of activated sludge in MEBR gone up to $12.53 \text{ mgO}_2/(\text{g MLVSS} \cdot \text{h})$ compared to that
247 of $10.68 \text{ mgO}_2/(\text{g MLVSS} \cdot \text{h})$ (Fig. S1), showing an appreciable increase after applying
248 intermittent DC. Though the sludge was a rather complex composition, SOUR could be
249 considered as an indication of maintaining high microbial activity in MEBR. At an appreciate
250 current density and exposure, the improved microbial activity in MEBR translated into
251 amenability to application as a bioelectrical reactor where DC stimulated microbial
252 metabolism and/or pure cultures (Thrash and Coates, 2008).

253 **3.4 Microbial community**

254 Appropriate electric field exerted positive effect on treatment performance by improving
255 microbial activity and promoting microbial community. High throughput sequencing was
256 introduced to investigate the microbial community richness, diversity and structure shift in
257 MBR and MEBR. Some differences of microbial community were observed between MBR
258 and MEBR. Microbial community richness and microbial diversity were both promoted in
259 MEBR as indicate by Chao 1 index and Shannon index (Fig. S2). It was assumed that the
260 differences in microbial community richness and diversity were related closely to the addition
261 of intermittent DC. The larger size and compact sludge floc in MEBR provided a new growth
262 environment, which supplied a core carrier for the growth and propagation of microbes(Xin et
263 al., 2016; Zhang et al., 2017). Thus, the microbial community richness and diversity increased,
264 which enhanced community stability for maintaining high containments removal efficiency
265 and resisting perturbations. A similar finding was observed in a previous study, which showed
266 that the richness and diversity of anaerobic microbial communities were promoted by
267 appropriate electric field stimulation(Zhang et al., 2012). The analysis on genus level was
268 conducted to further identify the function succession of community. Abundance differences
269 were observed, though most core bacterial genera were shared by the two sludge samples (Fig.
270 4). *Thiobacillus* had been detected as the primary and universal genus in coking wastewater
271 treatment plants (Ma, Qu et al., 2015), and its relative abundance rose from 5.22% in MBR up
272 to 6.32% in MEBR. *Comamonas* was considered as a versatile aromatic degrader for PAHs
273 and NHCs as well as a promising denitrifier and nitrifier under various aeration conditions
274 (Ibarbalz et al., 2013; Jia et al., 2016). Abundance of *Comamonas* in MBR and MEBR were
275 5.02% and 6.28% respectively. *Thauera*, as a degrader for phenol, methylphenol and indole,
276 increase from 1.53% to 2.61%. *Truepera* was reported in close relation with the

277 biodegradation of indole, and its abundance increased from 2.24% to 3.38%, which was
278 consistent with the indole removal. The abundance increment of these microbes might be the
279 primary reason in terms of microbial community for the enhancement of pollutants removals in
280 MEBR. Moreover, the relative abundance of some genera for nitrification and denitrification
281 or participated in nitrogen removal (eg. *Nitrospira*, *Denitratisoma*, *Thermomonas*) rose in
282 varying degrees, which was mainly attributed to the anoxic/anaerobic microenvironment
283 created by the large and compact sludge flocs. This indicated that MEBR had enhanced
284 potential for nitrogen removal at controlled conditions.

285 **3.5 The relationships analyses**

286 The treatment performance enhancement, membrane fouling reduction, changes in the
287 properties of the mixed liquor and microbial community evolution were all resulted from the
288 addition of intermittent DC. The relationships analyses were conducted with ordination
289 method to discern the effects of operational parameters. The relationship between microbial
290 community structure and main operational parameters (electrical exposure mode, current
291 density and MLSS) was illustrated in Fig. 5a. It could be inferred that current density and
292 electrical exposure mode affected the microbial community significantly and MLSS
293 influenced some of the genera. An obtuse angle between current density and exposure mode
294 indicated that they had an adversely interactive impact in regulating microbial community
295 compositions, since current density and exposure mode affected electrical amount in opposite
296 direction. *Thiobacillus*, as the primary genus in coking wastewater treatment plants was
297 affected by electrical exposure mode dramatically. The dynamics of *Thauera* and *Comamonas*
298 were highly associated with current density and exposure mode. Variation of exposure mode
299 exhibited a positive impact on variations of *Thiobacillus*, *Nitrospira*, *Denitratisoma* and

300 *Thermomonas*. Negative correlations emerged between MLSS, current density and *Azoarcus*,
301 *GP4* and *Isosphaera*. The fact that microbial community was positively or negatively affected
302 by the operational parameters might be a primary reason for the community shifts. The
303 correspondence analysis between mixed liquor properties and operational parameters
304 suggested that the changes of properties in mixed liquor were highly related with current
305 density and electrical exposure mode (Fig. 5b). Current density and exposure mode exerted
306 different impact on the variations of mixed liquor properties. Zeta potential was associated
307 with electrical exposure mode significantly, since exposure mode determined the amount of
308 positive charge iron ion in the long period operation, thus exerting considerable effect on zeta
309 potential. SMP was influenced by current density with a high significance. PSD and SRF
310 were related with both current density and exposure mode. Membrane fouling depended on
311 the properties of the mixed liquor (Kurita et al., 2016; Abass et al., 2018). A regression model
312 was gained between membrane fouling rate expressed by TMP increment over time and
313 properties of mixed liquor with a high correlation coefficient (Formula S2, $R^2=0.95$),
314 suggesting that changes in properties of mixed liquor induced by operational parameters
315 (current density and exposure mode et. al) led to fouling reduction or aggravation.

316 Based on the above results, it can be obtained exactly that an interactive relevance
317 existed among microbial community structure, mixed liquor properties and operational
318 parameters. A thorough and comprehensive understanding of the relationships would
319 facilitate the optimizing control for fouling reduction as well as efficiency enhancement and
320 be conducive to the rapid development of MEBR in domestic and industrial wastewater
321 treatment.

322 **3.6 Long-term performance of MEBR**

323 According to the above results, microbial community evolution in a long period of
324 operation played a vital role in the performance enhancement of MEBR. It assumed that the
325 treatment efficiency of MEBR might be well even as the intermittent DC was cut off. The
326 treatment performance of MEBR with cutting off DC was investigated (Fig. 6). Average COD
327 and total phenols removal efficiencies of MEBR decreased from 83.38% to 78.33% and
328 93.97% to 87.97% respectively when intermittent DC was cut off. Treatment efficiency of
329 MEBR when DC was cut off was still higher than the sum efficiencies of MBR and the
330 electro-catalytic degradation ($71.3\%+2.38\%=73.68$ for COD, $82.47\%+3.78\%=86.25\%$ for
331 total phenols), which further confirmed the synergic effect between biodegradation and
332 electrochemical effect in MEBR. The results suggested that the functional bacteria enriched
333 by intermittent electric field still exerted dominating effect on pollutants removals, even
334 though the DC was cut off. When the intermittent DC was switched on after a period of
335 cutting off, COD and total phenols removal efficiencies recovered gradually in 4 days,
336 verifying the comprehensive effects of mixed liquor properties and microbial community
337 succession induced by intermittent DC with iron anode on the enhancement of treatment
338 performance. The variations of membrane fouling were also investigated by monitoring the
339 TMP. When intermittent DC was cut off, TMP increment rate of MEBR increased, indicating
340 the exacerbation of membrane fouling without the assistance of electrokinetic effects.
341 However, membrane fouling rate of MEBR (0.42 kPa/d) was still lower than MBR (0.56
342 kPa/d) when DC was cut off (Fig. S3), resulting from the residual electrokinetic effects. The
343 exacerbation of membrane fouling of MEBR as cutting off DC was mainly associated with
344 the changes in the mixed liquor. When the intermittent DC was switched on again, membrane
345 fouling was hindered accordingly. The long term operation of MEBR with high efficiency

346 also demonstrated the treatment stability and membrane fouling migration of MEBR with
347 intermittent DC.

348 The study demonstrated that MEBR enhanced the treatment performance and
349 substantially hindered membrane fouling with the employment of DC and electrodes. The
350 analyses of the mechanism and relationships were beneficial to the operation and optimization
351 of MEBR. The net cost increment of MEBR was mainly associated with the DC energy
352 demand and sacrificial anode, which were related to the raw wastewater properties, operating
353 conditions such as current density, exposure mode and HRT as well as the electrode price.
354 The DC energy demand and anode consumption of MEBR were calculated to be 0.036
355 kWh/m³ and 15 g/m³ in the laboratory scale experiments. The precise economic analysis
356 should be conducted in further pilot scale studies. Importantly, the improvement of treatment
357 performance and reduction of membrane fouling slashed the frequency of necessity
358 membrane cleaning and disassembling/assembling operations of membrane module as well as
359 the according costs meaningfully. Thus MEBR exhibited considerable advantages compared
360 to MBR and it could serve as a promising technology in wastewater treatment with potential
361 application. The reactor design should be the main problem to be resolved for the pilot scale
362 application of MEBR due to the complicated electro-biological system. The treatment and
363 disposal of the excess sludge discharged from MEBR should be paid more attention, though it
364 was reported that the dewaterability of the sludge electro-conditioned by membrane
365 electro-bioreactor was improved significantly(Ibeid et al., 2015). In addition, electrode
366 fouling due to the deposition of organic and inorganic sludge components was another aspect
367 needed to be considered.

368 **4. Conclusions**

369 MEBR with iron anode at appropriate exposure mode was found to be an efficient
370 method for hindering membrane fouling and promoting treatment performance, primarily
371 associating with the changes in properties of mixed liquor, such as the increase of floc size
372 and reduction of SMP and SRF, caused by electrokinetic effects. Microbial activity was
373 provoked to be enhanced by suitable current density and exposure. The microbial community
374 evolution promoted by DC exposure also accounted for performance enhancement in MEBR.
375 The understanding of relationships among microbial community structure, mixed liquor
376 properties and operational parameters was beneficial to applying efficient strategies to
377 MEBR.

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491 Table 1 Results of GC-MC analysis for the influent and effluents of MBR and MEBR

Compounds	Raw	MBR	MEBR
Phenols			
Phenol	10.9 ^a	0.8	0.5
Hydroquinone	0.5	0.7	0.9
Cathchol	1.3	0.9	0.9
P-Cresol	0.4	0.2	0.3
Phenol,3-ethylphenol	1.6	ND	ND ^b
Phenol,2,3-dimethyl	0.6	ND	ND
Phenol,4-tert-butyl	1.7	0.9	0.8
1,3-Benzenediol, 4,5-dimethyl-	1.6	ND	ND
Phenol,2,4-di-tert-butyl	0.6	ND	ND
2,6-Di-tert-butyl-4-methylphenol	1.5	0.9	0.6
1,3-Benzenediol, 4,5-dimethyl-	1.6	0.5	0.5
Phenol,4-methyl-2-nitro	1.2	0.6	0.5
Phenol,4-bis(1,1-dimethylethyl)-	0.7	0.2	ND
Phenol,2-[(trimethylsilyl)oxy]	ND	0.8	0.9
Phenol,2,6-dimethyl-4-nitro	ND	0.2	0.2
Nitrogenous heterocyclic compounds			
Quinoline	2.6	1.3	0.9
Isoquinoline	2.4	1.5	1.1

6-Amino-2-methyl quinoline	1.6	0.8	0.5
Pyridine	2.1	1.7	1.6
Pyridine,3-methyl-	1.9	1.3	1.1
2-Amino-4-methyl pyrimidine	1.2	0.8	0.7
Indole	1.4	0.2	ND
Indole, 2- methyl	1.1	ND	ND
2-Amino-3-picoline	1.6	0.7	0.6
2- methyl oxindole	1.4	0.3	ND
2,7-Diphenyl-1H-indole	1.2	ND	ND
2-Pyridine-carboxaldehyde	ND	0.6	0.6
3-Pyridine-carboxaldehyde	ND	0.8	0.5
1H-imidazole,1-methyl-2-nitro-	1.1	0.8	0.6
5-Methyl-2-nitro-1H-imidazole	1.2	0.3	ND
Long-chain hydrocarbons			
Undecane	2.0	1.3	0.9
Dodecane	1.2	ND	ND
Hexadecane	0.9	0.6	0.5
Heptadecane	1.2	0.8	0.6
Octadecane	1.1	0.3	ND
Eicosane	0.8	ND	ND
Heneicosanoic	0.6	ND	ND
Docosanoic	1.7	1.2	0.9

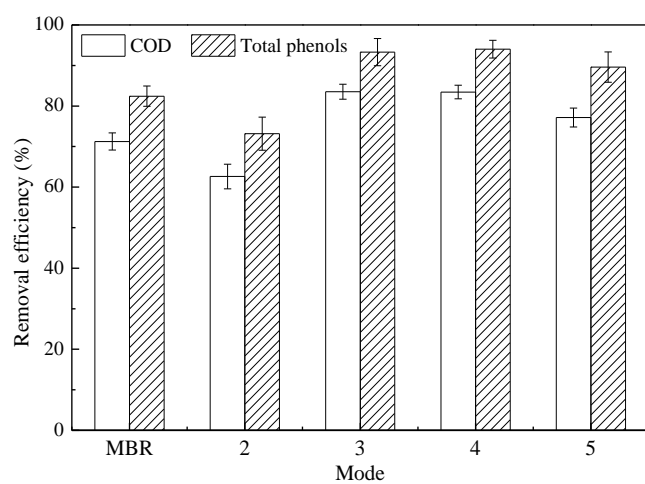
Pentacosane	0.8	0.5	0.3
Hexacosane	0.9	0.6	0.5
Octacosane	0.5	0.3	0.3
Nonacosane	ND	0.1	0.1
Polynuclear aromatic hydrocarbons			
Naphthalene	1.9	1.2	0.8
Naphthalene,1,3-dimethyl	1.5	1.1	0.9
Naphthalene, 2,6-Dimethyl	1.6	1.2	0.9
Naphthalene, 1,2,6-Trimethyl	0.2	ND	ND
Naphthalene, 1,2,6,7-Tetramethyl	0.2	0.2	0.3
Esters			
Dimethyl phthalate	1.2	0.7	0.6
Diisobutyl phthalate	0.8	0.6	0.4
Dibutyl phthalate	1.2	0.3	ND
Hexanedioic acid, bis(2-ethylhexyl) ester	0.5	ND	ND
Sum	65.9	28.8	22.3

492 a. Values represent the relative percentage of total peak area.

493 b. ND, not detected.

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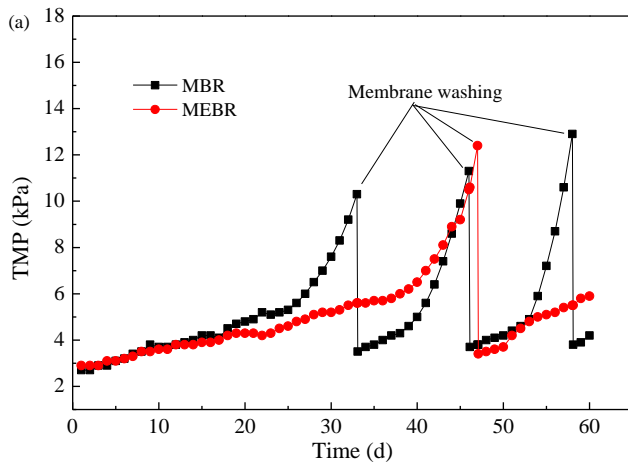
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498 Fig. 1 Performances of MBR and MEBR at various electrical exposure modes (mode 2:
499 20'-OFF/10'-ON, mode 3: 21.5'-OFF/7.5'-ON, mode 4: 24'-OFF/6'-ON, mode 5:
500 25'-OFF/5'-ON)

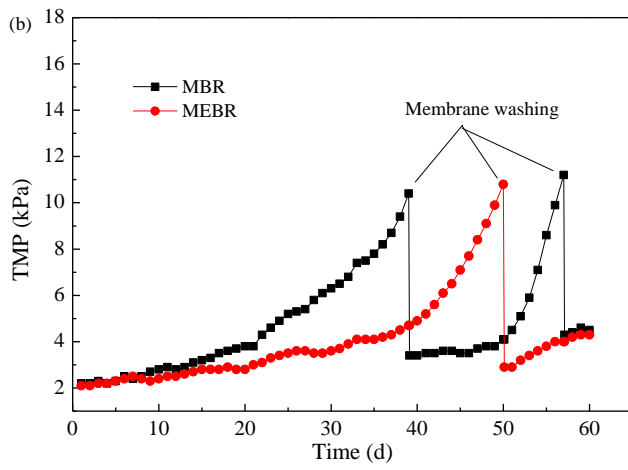
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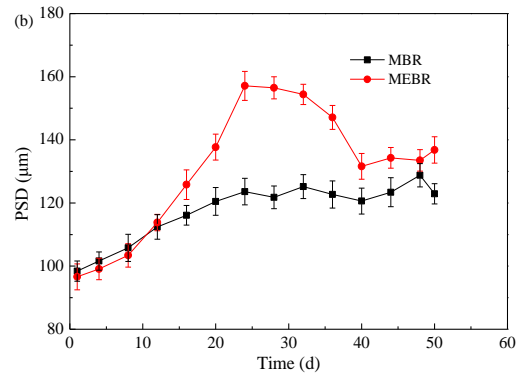
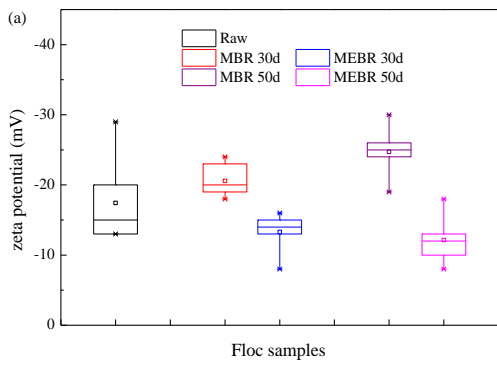
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506 Fig. 2 Variation of TMP in MBR and MEBR (a. MLSS 4500 mg/L, b. MLSS 3000 mg/L)

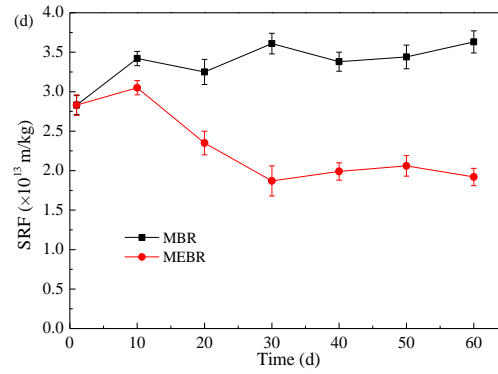
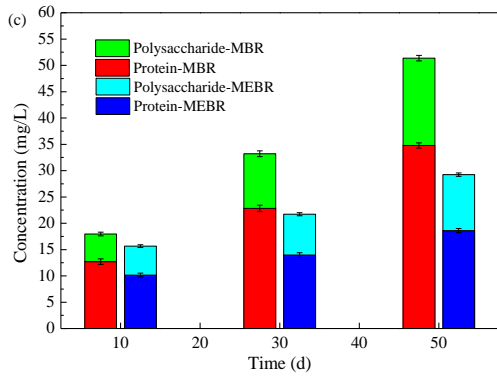
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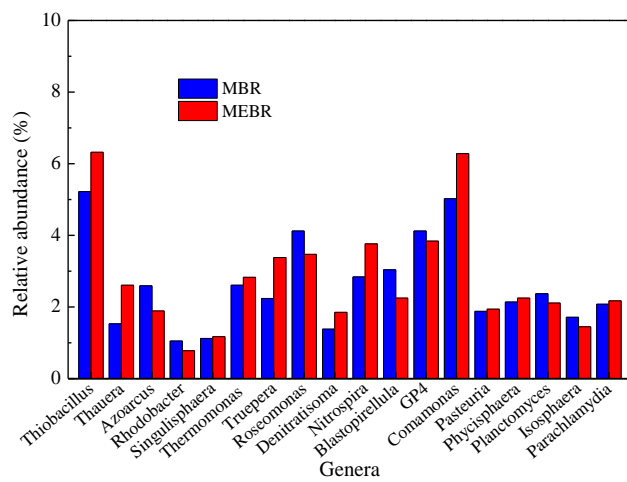
512 Fig. 3 Changes of mixed liquor properties in MBR and MEBR (a. zeta potential, b. floc PSD,
513 c. SMP, d. SRF)

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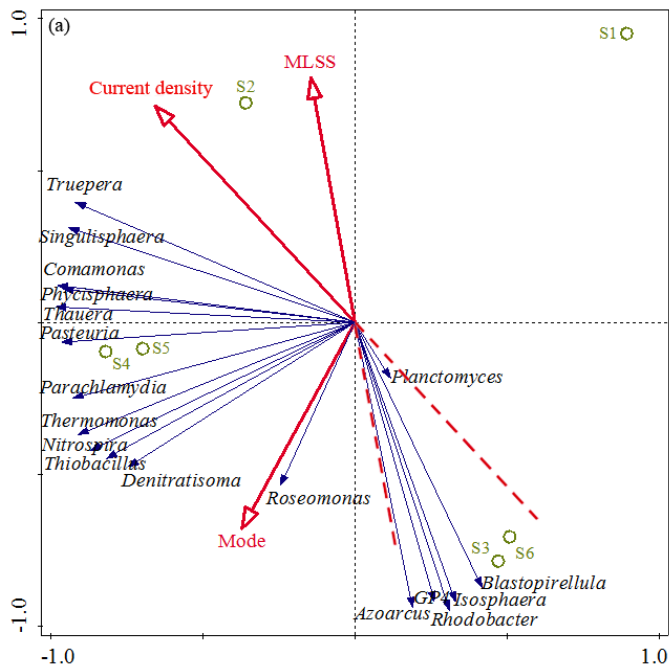


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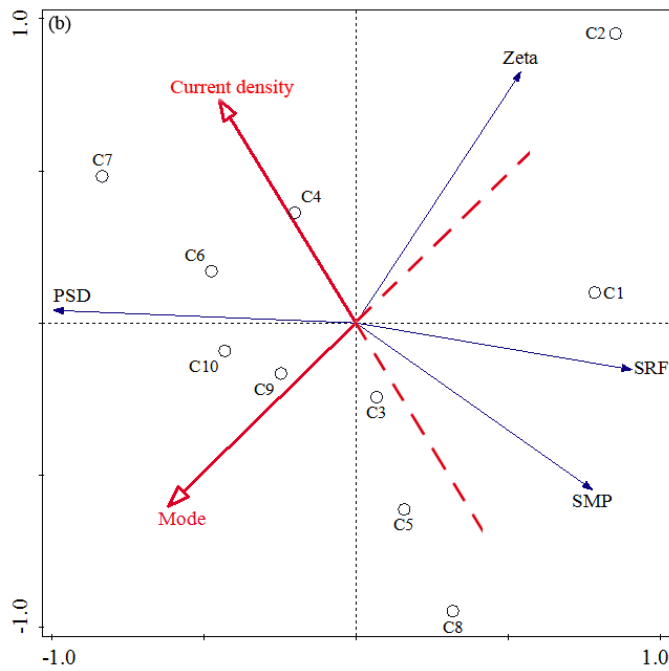
519 Fig. 4 Evolution of the primary genera in MBR and MEBR

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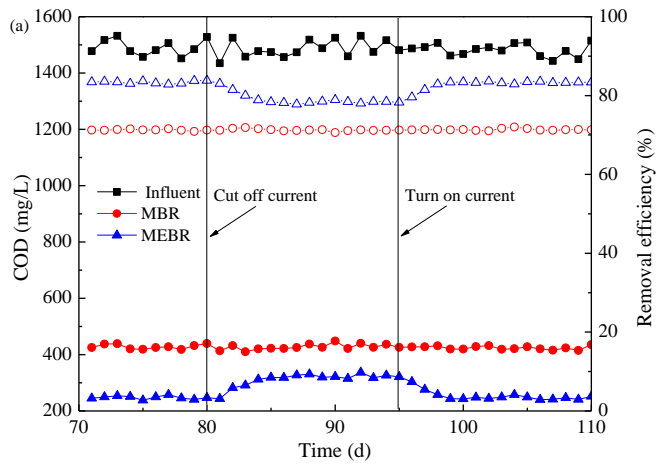
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525 Fig. 5 Principal component analysis (PCA) of the correlations (a. microbial community
526 composition vs operational parameters, b. mixed liquor properties vs operational parameters)

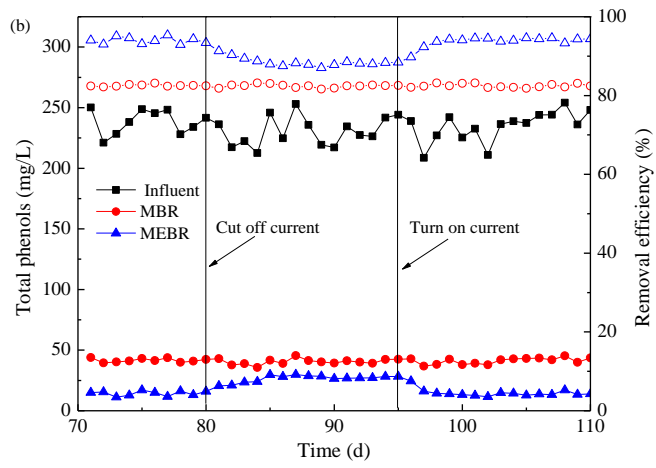
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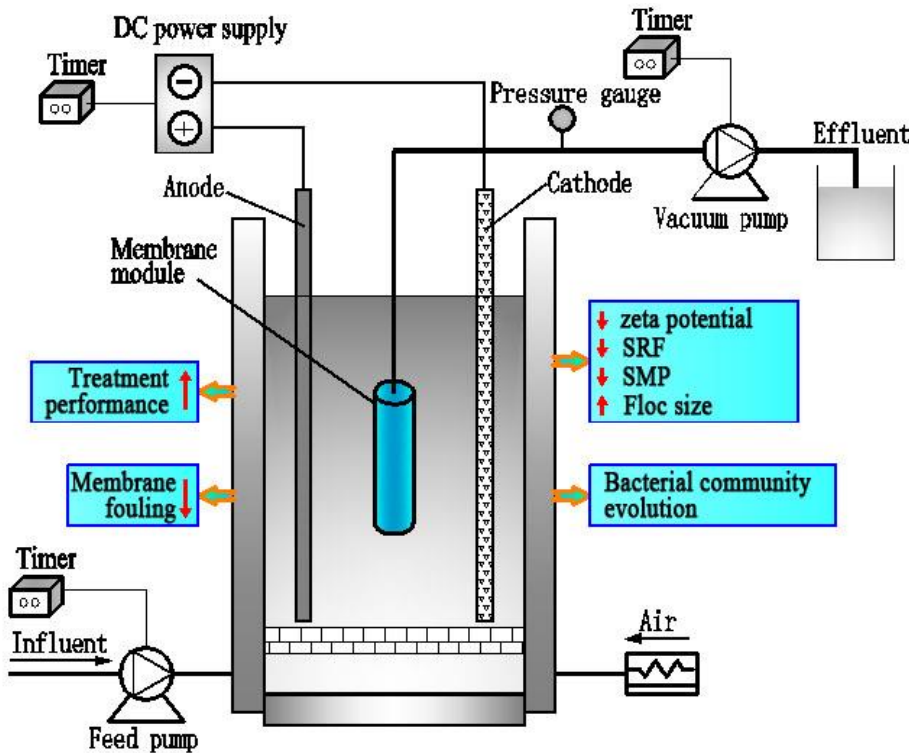
532 Fig. 6 Long-term treatment performance of MEBR (a. COD, b. total phenols)

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536 **Graphical abstract**



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539 **Highlights**

540 ◆ MEBR coupling intermittent DC and MBR was established to treat coal chemical industry
541 wastewater.

542 ◆ MEBR exhibited significant efficiency improvement and membrane fouling reduction.

543 ◆ Changes in properties of mixed liquor caused by electrokinetics accounted for fouling
544 migration.

545 ◆ MEBR with intermittent DC and iron anode promoted microbial community evolution.

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