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4 **Associations between bipedal stance stability and locomotor stability**  
5 **following a trip in unilateral vestibulopathy**

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32 **Running Title:** Stance and Locomotor Stability in Vestibulopathy

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For Peer Review

34 **Abstract**

35 Posturography is used to assess balance in clinical settings, but its relationship to gait stability  
36 is unclear. We assessed if dynamic gait stability is associated with standing balance in 12  
37 patients with unilateral vestibulopathy. Participants were unexpectedly tripped during  
38 treadmill walking and the change in the margin of stability ( $MoS_{\text{change}}$ ) and base of support  
39 ( $BoS_{\text{change}}$ ) relative to non-perturbed walking was calculated for the perturbed and first  
40 recovery steps. The centre of pressure (COP) path during 30s stance with eyes open and  
41 closed, and the distance between the most anterior point of the COP and the anterior BoS  
42 boundary during forward leaning ( $A_{\text{Dist}}$ ) were assessed using a force plate. Pearson  
43 correlations were conducted between the static and dynamic variables. The perturbation  
44 caused a large decrease in the BoS, leading to a decrease in MoS. One of 12 correlations was  
45 significant ( $MoS_{\text{change}}$  at the perturbed step and  $A_{\text{Dist}}$ ;  $r = -.595$ ,  $P = .041$ ; non-significant  
46 correlations:  $.068 \leq P \leq .995$ ). The results suggest that different control mechanisms may be  
47 involved in stance and gait stability, as a consistent relationship was not found. Therefore,  
48 posturography may be of limited use in predicting stability in dynamic situations.

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50 **Keywords:** vestibular, dynamic gait stability, falls, balance, locomotion

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## Introduction

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Posturography assesses balance and postural sway through centre of pressure (COP) measurements during stance and has been used in groups at an increased falls risk, such as lower limb amputees,<sup>1</sup> elderly<sup>2,3</sup> and vestibulopathy patients.<sup>4,5</sup> Contributions of sensory systems to postural control can be estimated by disturbing vision,<sup>6</sup> changing the support surface<sup>7</sup> or via Achilles tendon vibration.<sup>7-9</sup> However, the majority of falls occur during ambulation,<sup>10-14</sup> not static stance, which may be one reason why posturography appears to be limited as a clinical test, rehabilitation tool and falls risk assessment method.<sup>15</sup>

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From a mechanical perspective, the vertical projection of the centre of mass (CoM) is within the base of support (BoS) during bipedal stance and is controlled through anticipatory adjustments of the sensory and neuromuscular systems. However, in dynamic settings, the extrapolated CoM is often situated outside of the BoS and the CoM has a velocity and specific direction, and effective reactive postural adjustments (e.g. by increasing BoS) are required to control stability.<sup>16-19</sup> These differences may explain why posturography could not separate fallers from non-fallers in a slip recovery test during gait.<sup>20</sup> Similarly, the maximum recoverable forward lean angle is not generally predicted by static posturography.<sup>21,22</sup> However, such comparisons between static and dynamic tasks have not, to our knowledge, been conducted in subject groups with balance disorders. Vestibulopathy is associated with imbalance, dizziness and falls<sup>23-26</sup> and decreased motor performance<sup>17,27,28</sup> and therefore, it is important to determine if posturography can provide some insight into gait stability issues seen in these patients.

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In a recent study of our group, we reported that patients with unilateral peripheral vestibular disorder have a diminished ability to control and adapt their dynamic gait stability following unexpected trip perturbations while walking compared to healthy participants.<sup>17</sup> Additionally, it has been well documented that various posturography methods can discriminate vestibular

79 patients from healthy subjects.<sup>29-32</sup> Given that both static and dynamic methods reveal  
80 differences between healthy and vestibulopathy groups, and that posturography can be easily  
81 and cheaply conducted, an assessment of the relationship between such tasks is needed to  
82 determine if posturography alone is sufficient to estimate dynamic gait stability. To address  
83 this, we collated previously collected data from the dynamic gait stability measurements<sup>17</sup>  
84 and from posturography measurements conducted with the same patients.<sup>33</sup> An explorative  
85 analysis was conducted to determine correlations between dynamic stability control following  
86 a trip and COP parameters during a forward leaning task and during quiet standing with the  
87 eyes open and closed. Based on previous results demonstrating a lack of relationship between  
88 static and dynamic stability tasks,<sup>20-22</sup> we did not expect to find a consistent relationship  
89 between the dynamic stability parameters and the COP parameters during quiet standing, but  
90 we suspected that the forward lean task may reveal some correlations with the dynamic task  
91 due to the fact that the anterior limit of stability is more challenged in this task than during  
92 quiet standing.

### 93 **Methods**

94 For this explorative analysis, we pooled previously collected data of patients with  
95 unilateral peripheral vestibular disorder from two previous studies, the first involving a  
96 tripping while walking task<sup>17</sup> and the second involving stance posturography tasks.<sup>33</sup> For each  
97 parameter of interest (see below) we included all patients with data from each variable. In  
98 total, 12 patients were included with age, height and weight of 50.5(5.4) years, 169.7(6.6) cm  
99 and 72.5(9.6) kg respectively (means and SD). All patients were assessed for inclusion by an  
100 otolaryngologist to confirm their diagnoses. Further inclusion criteria were that participants  
101 did not exercise more than once per week and had no other health issues. The studies were  
102 approved by the ethical board of the university, the procedures were explained to the

103 participants, and written informed consent was obtained in accordance with the Declaration  
104 of Helsinki.

105 Previous work has reported the effects of repeated trip perturbations on these  
106 subjects.<sup>17</sup> Here, we consider only the impact of the first unexpected trip, to exclude the  
107 possibility of adaptation influencing the results and to analyse a more ecologically valid  
108 response to the trip perturbation.<sup>34</sup> Full details on the trip perturbation device have been  
109 reported previously.<sup>17,35,36</sup> Briefly, the tripping task was conducted during treadmill walking  
110 at  $1.4 \text{ m}\cdot\text{s}^{-1}$  (pulsar 4.0, h/p/cosmos, Nussdorf-Traunstein, Germany) using a custom built  
111 electronically driven magnet system to provide a trip perturbation. The perturbation consisted  
112 of a single unilateral resistance of 2.1 kg, applied and removed unexpectedly to the right leg  
113 during the swing phase via a Teflon cable and ankle strap. Participants wore a safety harness  
114 connected to an overhead track during all trip recovery and posturography trials. Four to  
115 seven days before the measurement session, all participants took part in a treadmill walking  
116 familiarisation session lasting approximately 30 minutes, to become accustomed to the  
117 treadmill walking conditions. On the day of the measurement, the session began with five  
118 minutes of walking to ensure participants were comfortable on the treadmill. The ankle strap  
119 was then attached to the right leg and participants walked for another four minutes in order to  
120 establish a baseline (about 20 seconds was recorded towards the end of this period to be used  
121 as a non-perturbed walking baseline). Directly following the baseline period, the perturbation  
122 was applied for the entire duration of the swing phase and was subsequently removed.  
123 Participants were not given a warning about the upcoming perturbation. An example of a  
124 typical recovery response to the perturbation from one participant can be seen in Fig. 1.

125 **Insert Fig. 1**

126 In order to examine dynamic gait stability, we tracked a twelve-segment, full  
127 kinematic model using 26 reflective markers (radius 16 mm) recorded by an eight camera

128 (120 Hz) Vicon Nexus motion capture system. Segmental masses and locations were  
 129 calculated based on the data of Dempster et al.<sup>37</sup> The margin of stability (MoS) in the  
 130 anteroposterior direction was calculated, as defined by Hof et al.<sup>38</sup> (see Fig. 2), as the  
 131 difference between the BoS anterior boundary (anteroposterior position of the toe marker)  
 132 and the extrapolated CoM at the instant of foot touchdown (determined using tibia  
 133 accelerometer data (ADXL250; Analog Devices, Norwood, MA, USA)) during baseline non-  
 134 perturbed walking, and at touchdown of the perturbed step (PERT) and the first recovery step  
 135 following the perturbation (POST<sub>1</sub>). The extrapolated CoM was defined as follows:

$$\text{Extrapolated CoM} = P_{\text{CoM}} + \frac{(V_{\text{CoM}} + |V_{\text{BoS}}|)}{\sqrt{g \cdot L^{-1}}}$$

136 where  $P_{\text{CoM}}$  is the horizontal (anteroposterior) component of the projection of the CoM to the  
 137 ground,  $V_{\text{CoM}}$  is the horizontal velocity of the CoM,  $V_{\text{BoS}}$  is the average horizontal velocity of  
 138 the foot markers during stance (approximately the treadmill belt speed),  $g$  is gravitational  
 139 acceleration and  $L$  is the pendulum length (the distance between the CoM and the centre of  
 140 the ankle joint in the sagittal plane). We focussed here on these two steps as our previous  
 141 work demonstrated the importance of the perturbed and first recovery step when recovering  
 142 stability following such perturbations.<sup>17</sup> Baseline values for MoS and BoS (BoS defined as  
 143 the anteroposterior distance between the left and right toe markers) were calculated at foot  
 144 touchdown by averaging 12 consecutive steps of non-perturbed walking. In order to account  
 145 for individual differences in walking stability, the change in the MoS and BoS relative to  
 146 baseline non-perturbed walking at PERT and POST<sub>1</sub> was used for this study (MoS<sub>change</sub> and  
 147 BoS<sub>change</sub> respectively), where negative MoS<sub>change</sub> and BoS<sub>change</sub> values represent lower  
 148 stability and smaller BoS respectively relative to baseline non-perturbed walking.

149 **Insert Fig. 2**

150 Our previous study of stance stability assessed many variables from different sensory  
 151 conditions in these patents.<sup>33</sup> In the current study, we include three variables and two tasks



152 that are conducted in clinical settings and provide information on general stance stability with  
153 and without visual sensory information, and stability control near the anterior limit of  
154 stability. Participants stood on a custom made strain gauge force plate which was used to  
155 measure (at 1000 Hz) the position of the COP during forward leaning and upright standing  
156 tasks. Participants stood barefoot with their feet at pelvic width and with their heels on a  
157 marked line on the platform. The positions of both feet were marked with a line on the force  
158 plate in order to transform the coordinates of the anterior and posterior boundaries of the BoS  
159 into the coordinate system of the force plate. In this way, the position of the COP could be  
160 calculated in relation to the boundaries of the BoS. For the leaning task, participants were  
161 instructed to lean as far forward as possible without moving joints other than the ankles. The  
162 task was repeated three times, with the trial showing the least difference between the most  
163 anterior position of the COP under the feet and the anterior boundary of the BoS (the line  
164 connecting left and right metatarsal five) being used for each subject ( $A_{Dist}$ ). Participants were  
165 then asked to stand as still as possible on the platform for three trials, under both eyes open  
166 and eyes closed conditions each with a time frame of 30 seconds. For the eyes closed  
167 condition, participants wore blackout glasses (custom made) to ensure that there was no  
168 visual sensory input during this condition. A Hamming low-pass filter with a cut off  
169 frequency of 5 Hz was used to remove high frequency noise and eliminate sampling error.  
170 Postural stability was assessed by the total excursion distance of the COP ( $COP_{Path}$ ) over the  
171 30 seconds analysis window. The average values of the COP parameters from the three trials  
172 for each participant were used in the analysis.

173 Pearson correlations were used to analyse the relationships between the posturography  
174 measures ( $A_{Dist}$ , eyes open and eyes closed  $COP_{Path}$ ) and MoS and BoS values of the trip  
175 recovery task. 12 and eight participants' data were included for the  $A_{Dist}$  and  $COP_{Path}$   
176 correlation analyses respectively. The level of significance for all tests was set at  $\alpha = .05$ . The

177 distribution normality of the results was checked prior to applying statistical analysis using  
178 the Shapiro-Wilk test, which revealed normal distributions for all parameters ( $P > .05$ ).  
179 GraphPad Prism version 7.00 software (GraphPad Software Inc., La Jolla, California, USA)  
180 was used for the statistical analysis. All results are presented as mean and standard deviation.

## 181 **Results**

182 The perturbation resulted in large changes in both the BoS and MoS. Changes in BoS  
183 and MoS relative to baseline at touchdown of the perturbed step and first recovery step are  
184 presented in Fig. 3. The perturbation caused a large decrease in the BoS at touchdown of the  
185 perturbed step, leading to a decrease in MoS (Fig. 3). A larger step was then taken in an  
186 attempt to control stability (see BoS at POST<sub>1</sub> in Fig. 3) but due to the forward velocity  
187 induced by the trip, the MoS did not return to baseline level (Fig. 3).

188 Consistent correlations between the posturography and dynamic stability parameters  
189 were not found. The three posturography tasks yielded results of 5.96(1.6) cm, 21.17(5.87)  
190 cm and 30.98(9.54) cm for A<sub>Dist</sub>, eyes open and eyes closed COP<sub>Path</sub> respectively. The  
191 correlation analyses revealed a significant negative correlation between A<sub>Dist</sub> and  
192 MoS<sub>change</sub>PERT ( $r = -.595$ ,  $P = .041$ ; Fig. 4). The other 11 correlation coefficients were not  
193 significant (see all  $r$  and  $P$  values in Fig. 4).

194 **Insert Fig. 3 and Fig. 4**

## 195 **Discussion**

196 The current study aimed to determine if balance maintenance during quiet stance and  
197 dynamic gait stability recovery performance were related in patients with unilateral  
198 peripheral vestibular disorder. Only one significant correlation was found out of 12 (Fig. 4),  
199 suggesting that performance during static stability tasks is not closely related with stability in  
200 dynamic situations. This may be particularly relevant for clinical settings where assessment

201 of static stance, but not dynamic gait stability is conducted in patient groups at an increased  
202 falls risk.

203 The significant negative correlation between  $A_{Dist}$  and  $MoS_{changePERT}$  means that, in  
204 these participants, the ability to bring the COP closer to the anterior boundary of the BoS  
205 during forward leaning was associated with a less negative MoS at touchdown of the tripped  
206 step during walking. It could be speculated that a more anterior limit of stability was the  
207 underlying mechanism for this finding, as this could facilitate both a more anterior COP  
208 position during leaning, as well as the ability to apply force to the ground more anteriorly  
209 following the perturbation. Similarly, this could also be related to the ability to control CoM  
210 velocity in the anterior direction, although this is perhaps less likely, due to the large  
211 difference in movement speed of the tasks. In either case, this result suggests that such an  
212 anterior leaning task may have some value in assessing the ability to control stability in the  
213 anterior direction. However, given the lack of significant correlations in general, the use of  
214 posturography tasks for the purpose of estimating stability in dynamic settings is not well  
215 supported by our results. This agrees with previous studies in other populations using forward  
216 lean and release or slip perturbations.<sup>20-22</sup> That being said, one limitation of this study was  
217 that it was not powered to test a null hypothesis such as that no correlations between the tasks  
218 would be found and therefore, it may be that with a larger sample size, more significant  
219 correlations could have been detected. We do not think that this is likely, however, as when  
220 we included age, height and weight matched healthy subjects in the analysis (data not  
221 shown), thereby artificially increasing the variation of performance, this did not greatly  
222 change the results.

223 The lack of association between the posturography and trip recovery outcome  
224 measures may be due to differences in the governing control strategies and mechanisms of  
225 stability associated with the tasks. Posturography during quiet stance assesses the ability to

226 keep the vertical projection of the body's CoM within the BoS, principally by using  
227 anticipatory adjustments. In contrast, the ability to regain dynamic stability after tripping or  
228 slipping where the extrapolated CoM is located outside of the BoS is governed principally by  
229 reactive postural adjustments.<sup>18,19</sup> Here, a key factor in preventing a fall is the ability to take a  
230 large recovery step to lengthen the BoS and increase the MoS.<sup>16-18</sup>

231 It is important to note, that while the patients all had unilateral vestibulopathy, the  
232 degree of vestibular function remaining varied, and this information was not available for all  
233 patients. That being said, there were no significant outliers among the patients in our results,  
234 suggesting that while the vestibular function may have varied between patients, the overall  
235 impact on stability control was reasonably consistent. This was not a concern for our results,  
236 as we treated these subjects as a generalised group with balance disorders that should be  
237 distinct from healthy subjects in terms of stability and balance control.

238 In conclusion, no consistently significant relationship between posturography and the  
239 trip recovery task measures was found, indicating that different mechanisms of postural  
240 control appear to be involved in our static and dynamic stability tasks. Balance maintenance  
241 during quiet stance alone may be of limited use in predicting dynamic stability during  
242 perturbed walking. We therefore recommend that task specificity should be considered in  
243 clinical and research settings regarding stability and falls risk assessment. Future research  
244 should aim to relate laboratory-induced gait perturbation outcomes with real life falls.

245

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358

**Figure Captions**

359 **Figure 1** - Example of a typical recovery response to the trip perturbation in one participant.

360 The perturbation adds resistance to the swing phase of the right leg, leading to a reduction in  
361 the base of support at foot touchdown. This causes a more anterior position and higher  
362 velocity of the centre of mass at touchdown, relative to non-perturbed walking. In response,  
363 an increased base of support is required in the following recovery step to maintain gait  
364 stability.

365

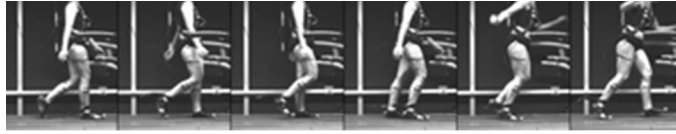
366 **Figure 2** - Schematic diagram of the inverted pendulum model during locomotion.<sup>38</sup>  $P_{CoM}$   
367 represents the horizontal (anterior-posterior) component of the projection of the center of  
368 mass (CoM) to the ground,  $V_{CoM}$  is the anterior-posterior velocity of the CoM,  $V_{BoS}$  is the  
369 average horizontal velocity of the foot markers during stance (approximately the treadmill  
370 belt speed),  $g$  is acceleration due to gravity and  $L$  is the pendulum length (i.e., distance  
371 between the CoM and the centre of the ankle joint in the sagittal plane). Margin of stability  
372 (MoS) in the anterior direction is calculated at foot touchdown as the difference between the  
373 anterior boundary of the base of support ( $BoS_{Umax}$ ) and the extrapolated centre of mass  
374 ( $X_{CoM}$ ). A stable body configuration is indicated by positive MoS values (A), whereas an  
375 unstable body configuration is indicated by negative margin of stability values (B), where  
376 additional motor actions, such as stepping, are required to preserve stability and to avoid a  
377 fall.

378

379 **Figure 3** - Change relative to baseline non-perturbed walking in base of support (BoS) and  
380 margin of stability (MoS) at touchdown of the perturbed step (PERT) and the first recovery  
381 step ( $POST_1$ ) for 12 patients with unilateral vestibulopathy (mean, SD and individual data  
382 points).

383

384 **Figure 4** - Pearson correlation coefficients ( $r$ ) between the static and dynamic stability tasks.  
385 12 patients with unilateral vestibulopathy were included for the  $A_{Dist}$  correlations and eight  
386 patients were included for the eyes open (EO) and eyes closed (EC)  $COP_{Path}$  correlations.  
387  $BoS_{change}^{PERT}$  and  $BoS_{change}^{POST_1}$ : Change in the base of support relative to baseline non-  
388 perturbed walking at touchdown of the perturbed and first recovery steps respectively.  
389  $MoS_{change}^{PERT}$  and  $MoS_{change}^{POST_1}$ : Change in the margin of stability relative to baseline  
390 non-perturbed walking at touchdown of the perturbed and first recovery steps respectively.  
391  $A_{Dist}$ : Distance between the most anterior point of the COP during the forward leaning task  
392 and the anterior boundary of the base of support (the line connecting left and right metatarsal  
393 five). EO and EC  $COP_{Path}$ : total path length of the centre of pressure trajectory during 30s of  
394 quiet stance with eyes open and closed respectively.

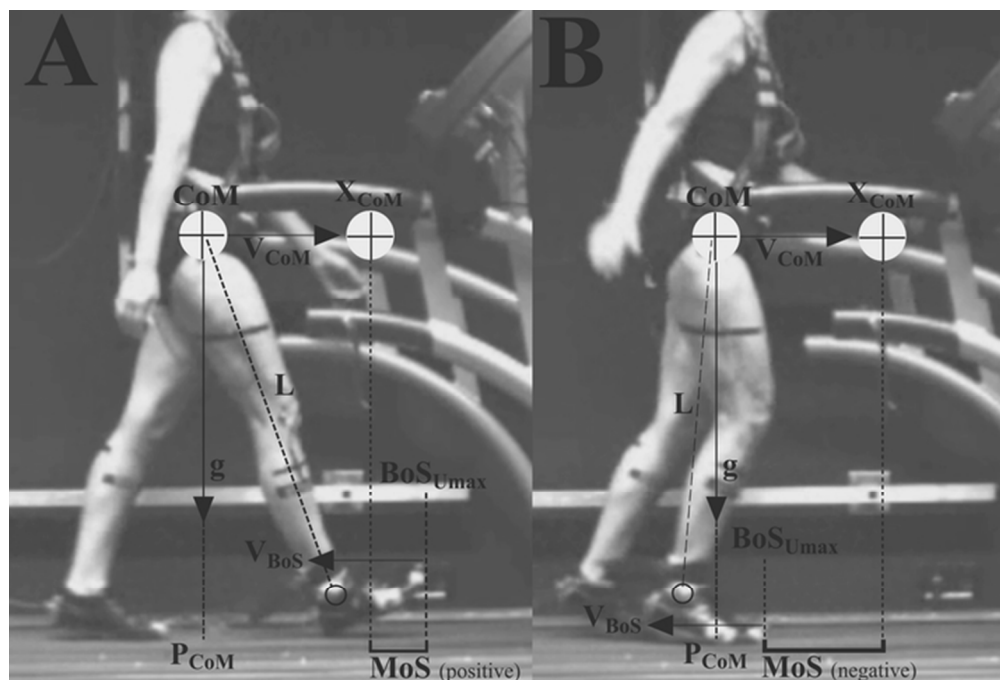


Example of a typical recovery response to the trip perturbation in one participant. The perturbation adds resistance to the swing phase of the right leg, leading to a reduction in the base of support at foot touchdown. This causes a more anterior position and higher velocity of the centre of mass at touchdown, relative to non-perturbed walking. In response, an increased base of support is required in the following recovery step to maintain gait stability.

Fig. 1

28x5mm (300 x 300 DPI)

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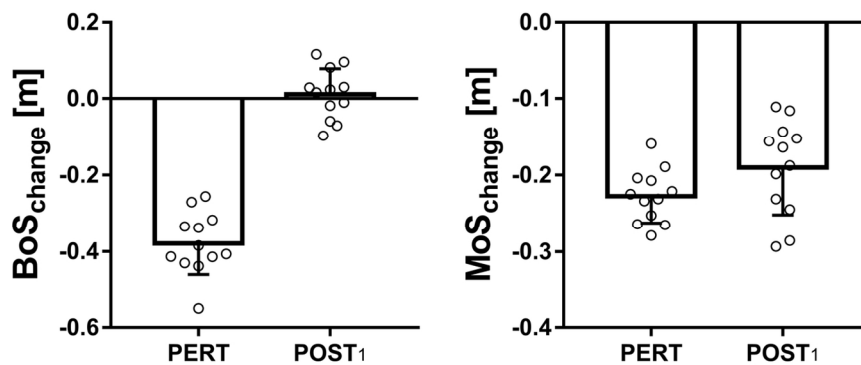


Schematic diagram of the inverted pendulum model during locomotion.<sup>38</sup> P<sub>CoM</sub> represents the horizontal (anterior-posterior) component of the projection of the center of mass (CoM) to the ground, V<sub>CoM</sub> is the anterior-posterior velocity of the CoM, V<sub>BoS</sub> is the average horizontal velocity of the foot markers during stance (approximately the treadmill belt speed), g is acceleration due to gravity and L is the pendulum length (i.e., distance between the CoM and the centre of the ankle joint in the sagittal plane). Margin of stability (MoS) in the anterior direction is calculated at foot touchdown as the difference between the anterior boundary of the base of support (BoS<sub>Umax</sub>) and the extrapolated centre of mass (XCoM). A stable body configuration is indicated by positive MoS values (A), whereas an unstable body configuration is indicated by negative margin of stability values (B), where additional motor actions, such as stepping, are required to preserve stability and to avoid a fall.

Fig. 2

60x40mm (300 x 300 DPI)

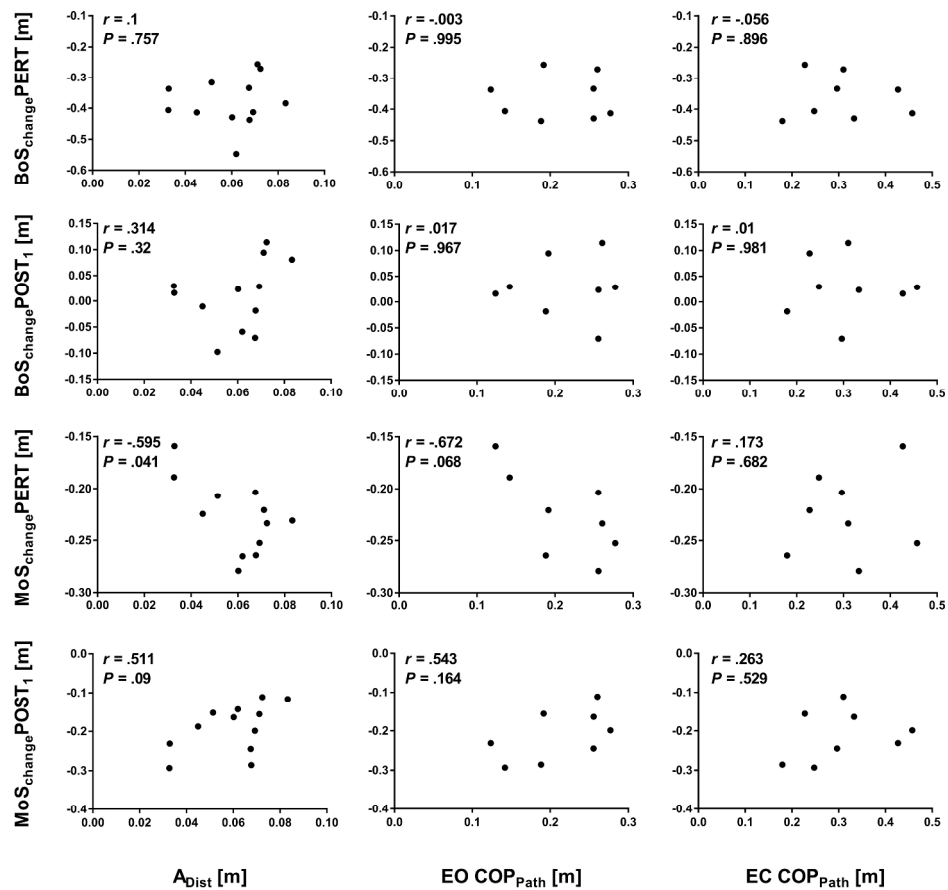




Change relative to baseline non-perturbed walking in base of support (BoS) and margin of stability (MoS) at touchdown of the perturbed step (PERT) and the first recovery step (POST1) for 12 patients with unilateral vestibulopathy (mean, SD and individual data points).

Fig. 3

68x30mm (600 x 600 DPI)



Pearson correlation coefficients ( $r$ ) between the static and dynamic stability tasks. 12 patients with unilateral vestibulopathy were included for the ADist correlations and eight patients were included for the EO and EC COPPath correlations. BoS<sub>change</sub>PERT and BoS<sub>change</sub>POST1: Change in the base of support relative to baseline non-perturbed walking at touchdown of the perturbed and first recovery steps respectively. MoS<sub>change</sub>PERT and MoS<sub>change</sub>POST1: Change in the margin of stability relative to baseline non-perturbed walking at touchdown of the perturbed and first recovery steps respectively. ADist: Distance between the most anterior point of the COP during the forward leaning task and the anterior boundary of the base of support (the line connecting left and right metatarsal five). EO and EC COPPath: total path length of the centre of pressure trajectory during 30s of quiet stance with eyes open and closed respectively.

Fig. 4

142x132mm (600 x 600 DPI)