

Huygens Principle based UWB Microwave Imaging Method for Skin Cancer Detection

Navid Ghavami
School of Engineering
London South Bank University
London, SE1 0AA, UK
Email: ghavamin@lsbu.ac.uk

Gianluigi Tiberi
Fondazione IMAGO 7
IRCCS Stella Maris
Viale del Tirreno
I-56128 Pisa, Italy

Mohammad Ghavami
and Sandra Dudley
School of Engineering
London South Bank University
London, SE1 0AA, UK

Majella Lane
School of Pharmacy
University College London
London, WC1N 1AX, UK

Abstract—In recent years, Ultra Wideband (UWB) technology has emerged as a promising alternative for use in a wide range of applications. One of the potential applications of UWB is in healthcare and imaging, motivated by its non-ionizing signals, low cost, low complexity, and its ability to penetrate through mediums. Moreover, the large bandwidth covered by UWB signals permits the very high resolution required in imaging experiments. In this paper, a recently introduced UWB microwave imaging technique based on the Huygens principle (HP), has been applied to multilayered skin model with an inclusion representing a tumor. The methodology of HP permits the capture of contrast such that different material properties within the region of interest can be discriminated in the final image, and its simplicity removes the need to solve inverse problems when forward propagating the waves. Therefore the procedure can identify and localize significant scatterers inside a multilayered volume. Validation of the technique through simulations on multilayered cylindrical model of the skin with inclusion representing the tumor has been performed.

I. INTRODUCTION

The extremely low power of UWB technology and its large bandwidth makes it a good candidate to solve many problems in various areas including short range high data rate communications and radar applications. In addition to these application schemes, other fields of appropriateness of the UWB technology are under investigation. In particular, interest has grown in the utilization of UWB technology in medicine and healthcare. Recent advances in UWB hardware technology has enabled the possibility of achieving the large bandwidth which is required for higher resolution imaging and detection [1]. In addition, several unique properties of UWB, including its non-ionizing signals, low cost and the ability to penetrate through media (air, skin, bones and tissues) have transformed it into an ideal candidate for a number of health-oriented applications [2].

A number of well established medical imaging techniques are being used in clinics and hospitals today. These methods utilize different technologies and are able to produce well-defined tomographic reconstructions of living tissues using a range of media. Most common are X-ray-based computed tomography (CT), ultrasound scanners, and nuclear magnetic resonance imaging (known as MRI). Beside their advantages, each of these techniques suffer from their own drawbacks, including contrast problems in Ultrasound [3], ionizing radi-

ation in CT [4], and the long scan time in the case of MRI [5]. In response to these limitations, microwave imaging has been recognized as a promising non-ionizing and non-invasive alternative screening technology for these application areas.

In general, there are three known types of skin cancer: Squamous Cell Carcinoma (SCC), Basal Cell Carcinoma (BCC), and melanoma. In the majority of cases (especially BCC and SCC), the skin cancers are curable if they are diagnosed at an early stage. For this purpose, the dielectric properties of human tissues can be used as an effective and accurate indicator for diagnostic purposes. [6]. Microwave imaging makes use of the difference in dielectric properties between normal and malignant skin tissues for detection purposes. Human skin comprises of three layers; epidermis, dermis and hyperdermis. With a thickness varying between tissue for 0.1 to 0.5 mm, the epidermis is the outermost layer of the skin. The most external part of the epidermis is a very thin body of dead cells called Stratum Corneum (SC). The thickness of SC varies depending on the location of the skin and it normally ranges between 15 and 150 μm [7].

In the past few years, a number of uniform multilayer models have been proposed to simulate the skin layers, with each layer being distinguished by a set boundary and specific electrical properties (permittivity and conductivity) [6], determined by those of free water content [8]. There is an increase in the amount of water content in all types of skin cancer, most notably in the epidermis layer. For malignant tumors and lesions, the water content of the epidermis can reach up to 81% [9]. These changes in the water content result in a change in the permittivity value of the tissue.

Currently, the most common and accurate approach for skin cancer diagnosis is via the biopsy technique, in which the skin lesion is removed and examined in a laboratory [10]. The diagnostic results usually take around a week to become available and are not guaranteed to be accurate. Meanwhile, reflectometer techniques [10] use millimeter wave guides to discriminate malignant and normal lesions. On the other hand, the approach presented in this paper is a complete imaging technique which allows us to image the tissues and to localize the inclusions. To the best of our knowledge this method has not yet been applied for the application of skin cancer detection.

For this purpose, the aim of this paper is to apply a novel, fast, and accurate UWB microwave imaging method based on the Huygens Principle (HP) [11] for treating multilayered model with inclusions. Using HP removes the need to solve inverse problems and, consequently, no matrix generation/inversion is required.

Furthermore, UWB allows the utilization of all the information in the frequency domain by combining the information from the individual frequencies, resulting in the construction of a consistent image. It follows that the methodology can identify the presence and location of significant scatterers inside a multilayered volume without having apriori knowledge of the dielectric properties of the target object. Validation of the technique through simulations has been performed, and results are presented, illustrating the effectiveness of the proposed method. Potential applications of the method are skin cancer detection, internal organ and whole body imaging.

In the next section of this paper, the HP-based procedure is reviewed and summarized. The method is validated through realistic skin simulations in Section III, while Section IV concludes the paper.

II. THE HUYGENS PRINCIPLE-BASED PROCEDURE

The procedure employed in this section was first introduced and presented in [11], and was subsequently tested successfully through a number of simulations and measurements for the purpose of breast cancer detection, published in the following papers [12], [13], [14]. To assist reader understanding, some fundamental works presented in [11] is reused here.

As a simple example, consider a cylinder in free space illuminated by a transmitting line source tx_m , and operating at a frequency f . At this point, it is assumed that the dielectric properties of the bulk of the cylinder are known. The problem consists of identifying the presence and location of discontinuities by using only the fields measured at the receivers outside the cylinder (fig. 1).

Assume that the field at the surface points $rx_{np} = (a_0, \phi_{np})$ is known, such that:

$$E|_{rx_{np}} = E_{np} \quad \text{with} \quad np = 1, \dots, N_{PT} \quad (1)$$

where N_{PT} indicates the number of measured points across the outside cylinder. Recalling the HP, we note that: each locus of a wave excites the local matter which reradiates a secondary wavelets, and all wavelets superpose to a new, resulting wave (the envelope of those wavelets), and so on [15]. Making use of this theory, we calculate the field inside the cylinder as the superposition of the fields re-radiated by the N_{PT} receiving antennas of (1):

$$E_{HP}^{rcstr}(\rho, \phi; tx; f) = \sum_{np=1}^{N_{PT}} E_{np} G(k_1 | \vec{\rho}_{np} - \vec{\rho} |) \quad (2)$$

$(\rho, \phi) \equiv \vec{\rho}$ is the observation point and k_1 represents the wave number for the media constituting the cylinder. In (2), the string ‘‘rcstr’’ indicates the reconstructed internal field, while

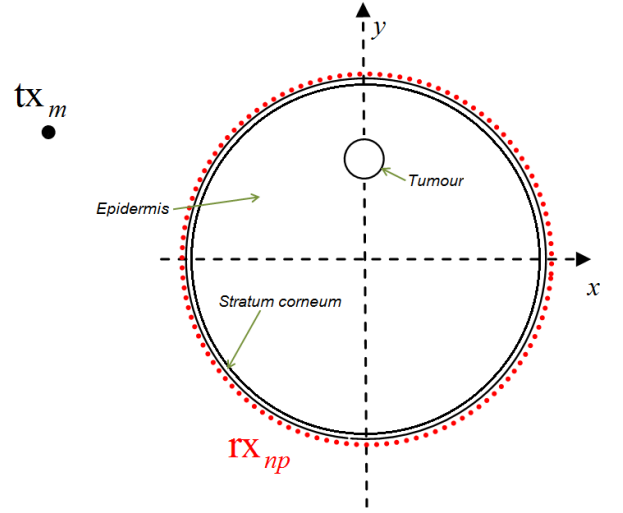


Fig. 1: Pictorial view of the skin cancer detection problem.

the subscript HP refers to the Huygens principle method, and $\text{avg}_M\{E_{np}\}$ represents the average of signals obtained illuminating the object using M different transmitter positions.

Moreover, $G(k_1 | \vec{\rho}_{np} - \vec{\rho} |)$ is the Green’s function defined as [11]:

$$G(k_1 | \vec{\rho}_{np} - \vec{\rho} |) = \frac{1}{4\pi | \vec{\rho}_{np} - \vec{\rho} |} e^{-jk_1 | \vec{\rho}_{np} - \vec{\rho} |} \quad (3)$$

During the initial simulations, it was observed that an image of the transmitter appeared in the result, which sometimes masked the area of interest. However, this transmitter image can be successfully removed by modifying (2) such that:

$$E_{HP}^{rcstr}(\rho, \phi; tx; f) = \sum_{np=1}^{N_{PT}} (E_{np} - \text{avg}_M\{E_{np}\}) G(k_1 | \vec{\rho}_{np} - \vec{\rho} |) \quad (4)$$

where $\text{avg}_M\{E_{np}\}$ represents the average of signals obtained illuminating the object using M different transmitter positions. This in effect ‘‘smears’’ out the transmitter image.

Thus, assuming M transmitting sources tx_m , $m = 1, 2, \dots, M$, and N_F frequencies f_i , the intensity of the resulting image I using the Green’s functions can be obtained through the incoherent summation:

$$I_{HP}(\rho, \phi) = \frac{1}{B} \sum_{m=1}^M \sum_{i=1}^{N_F} \Delta_f |E_{HP}^{rcstr}(\rho, \phi; tx; f_i)|^2 \quad (5)$$

In (5), Δ_f and B represent the frequency and the bandwidth, respectively. The resolution is expected to reach the optical resolution limit of $\lambda_{f_{\max}}/4$, where $\lambda_{f_{\max}}$ represents the wavelength in the cylinder calculated at the highest frequency; this gives the rule of thumb for determining the highest frequency to be used.

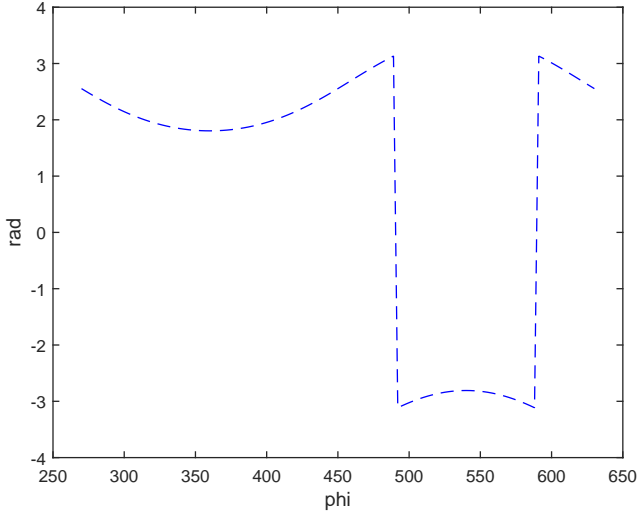


Fig. 2: Phase of the field on the external surface.

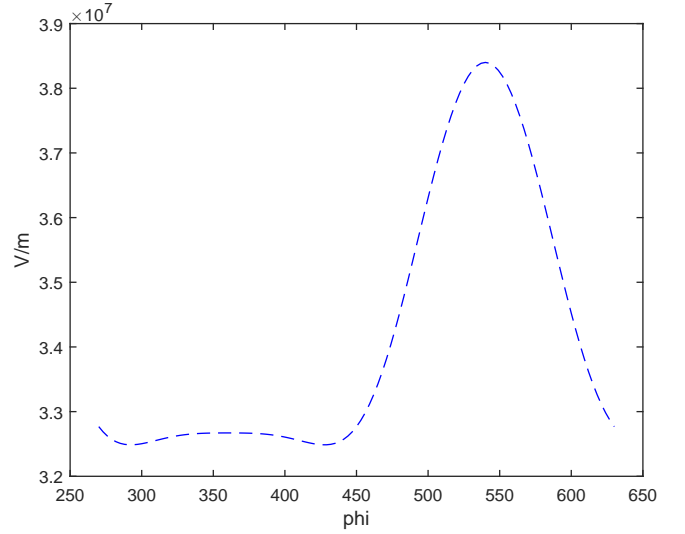


Fig. 3: Magnitude of the field on the external surface.

III. VALIDATION THROUGH SIMULATIONS:

MULTILAYERED MODEL WITH AN ECCENTRIC INCLUSION

The applicability of the analytical formulation presented in [13] is tested by simulating a 3-layer cylindrical model with an eccentric inclusion. The model, which is 2.5 mm in radius has realistic human skin tissue properties assigned to its three layers. The external cylinder is assumed to be a 0.1 mm thick Stratum Corneum, with $\epsilon_{r1} = 10$ and $\sigma_1 = 0.0001$ S/m [16]. The internal concentric cylinder and the eccentric inclusion are then assigned the electrical properties of Epidermis ($\epsilon_{r1} = 33$ and $\sigma_1 = 1$ S/m) [17] and malignant tumor ($\epsilon_{r1} = 50$ and $\sigma_1 = 3$ S/m) [18] respectively. Furthermore, the eccentric inclusion is 0.5 mm in radius and its center is placed at 2 mm deep from the external layer of the skin, 90° degrees relative to the x-axis.

Four transmitter sources placed 1 cm from the axis of the cylinder illuminate the external cylinder, while a frequency band of 1-10 GHz with frequency spacing of 10 MHz is used in the computer simulation. For each illuminating source and for each frequency, the field (E_{np}) at $N_{PT} = 120$ points lying on the external surface is calculated. Finally, the average of the 4 data sets ($\text{avg}_M\{E_{np}\}$) is calculated and HP is applied to the difference between the measured field and the average field as stated in (4).

Figures 2 and 3 show the variation in phase and magnitude of the measured field on the external surface of the cylinder, respectively, while fig 4 depicts the normalized intensity adjustment obtained through (5) and using an appropriate image adjusting. The image is adjusted by forcing the intensity values below 0.7 up to zero and expanding from 0 to 1 values above 0.7. A bright peak representing the tumor can be clearly observed and detected in the region of the inclusion with a resolution of 0.6 mm.

It can be observed that the method successfully detects and locates the skin tumor in this simulation. A malignant tumor has electrical properties higher than most human tissues [19],

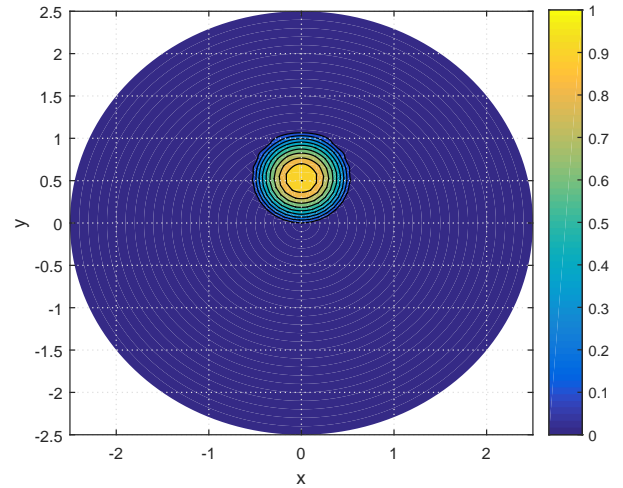


Fig. 4: Cylinder with an inclusion: normalized intensity obtained through (5). All scales are in millimeters.

hence this result would suggest its detection would be achieved in almost all cases in various parts of the body.

The effect of the change in the permittivity of the epidermis and that of the malignant tissue was then investigated. This was done to consider the change in the permittivity of the epidermis and the tumor caused by the amount of water content [18], and to take into account the alternative permittivity values of these tissues presented by other researchers [16]. More in detail, we were interested to see if these changes in permittivity values would affect the resolution and localization of the detected tumor. The results are tabulated in Table 1.

It can be seen that the change in the permittivity value of the malignant tumor does not have any affect on the resolution and positioning of the imaging results, while a similar change in the permittivity value of the epidermis results in a very negligible offset and resolution.

	Resolution (mm)	Offset (mm)
$\epsilon_{\text{epidermis}} = 33, \epsilon_{\text{malig}} = 40$	0.6	0
$\epsilon_{\text{epidermis}} = 33, \epsilon_{\text{malig}} = 60$	0.6	0
$\epsilon_{\text{epidermis}} = 20, \epsilon_{\text{malig}} = 50$	0.7	0.1
$\epsilon_{\text{epidermis}} = 40, \epsilon_{\text{malig}} = 50$	0.65	0.05

TABLE I: Comparison of the imaging results obtained through various permittivity value combinations.

IV. CONCLUSION

The application of a recently developed UWB microwave imaging algorithm based on the Huygens principle on realistic skin simulations has been analyzed. The multilayered simulated model assumes realistic skin dimensions and electrical properties for individual layers and the tumor. Forward-propagation of the waves using the HP procedure removes the need to solve inverse problems and matrix generation/inversion. This simple methodology benefits from the capability of capturing the contrast (dielectric variation). The method allows all the information in the frequency domain to be utilized by combining the information from the individual frequencies to construct a consistent image. HP method is able to provide a resolution of approximately one quarter of the shortest wavelength in the dielectric medium, while having bandwidths and power levels satisfying UWB rule and power safety limits, respectively. It has been shown that the HP can detect and locate an inclusion in a multilayered cylindrical skin model. Measurements on realistic skin models for further validation of the methodology are currently under investigation.

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