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Local dissipation scales and energy dissipation-rate moments in channel flow

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Local dissipation-scale distributions and high-order statistics of the energy dissipation rate are examined in turbulent channel flow using very high-resolution direct numerical simulations at Reynolds numbers $Re_\tau = 180, 381$ and 590 . For sufficiently large Re_τ , the dissipation-scale distributions and energy dissipation moments in the channel bulk flow agree with those in homogeneous isotropic turbulence, including only a weak Reynolds-number dependence of both the finest and largest scales. Systematic, but Re_τ -independent, variations in the distributions and moments arise as the wall is approached for $y^+ \lesssim 100$. In the range $100 < y^+ < 200$, there are substantial differences in the moments between the lowest and the two larger values of Re_τ . This is most likely caused by coherent vortices from the near-wall region, which fill the whole channel for low Re_τ .

Key words: turbulent boundary layers, turbulence simulation, turbulence theory

1. Introduction

The dissipation of kinetic energy by viscosity in fully developed turbulence occurs primarily at the smallest scales of the flow, where viscous effects overwhelm inertial processes. All such dissipation is assumed to occur near the mean scale $\eta_K = (\nu^3 / \langle \varepsilon \rangle_{x,t})^{1/4}$ in the classical picture of turbulence developed by Kolmogorov (1941), where ν is the kinematic viscosity and $\varepsilon(\mathbf{x}, t) = (\nu/2) (\partial_i u_i' + \partial_i u_j')^2$ is the local energy dissipation rate. The variable u_i' is the fluctuating velocity and $\langle \cdot \rangle_{x,t}$ denotes an average over all space and time. Prior numerical and experimental studies (see e.g. Sreenivasan & Antonia 1997; Ishihara, Gotoh & Kaneda 2009; Wallace & Vukoslavcević 2010) have shown, however, that ε is highly intermittent, resulting in local values of ε that can be orders of magnitude larger than the mean, even for turbulent flows at moderate Reynolds numbers. Such high amplitudes are, by definition, the result of very large velocity gradients, or tiny shear layers across which the velocity varies significantly. The dissipation can thus be connected to a locally varying scale, $\eta(\mathbf{x}, t)$, associated with fluctuations in the velocity gradient field. This gives a range of fluctuating scales, η , over which dissipation occurs, as opposed to the single mean scale η_K . Certain aspects of the resulting distributions of η remain unclear, however, including the properties of the smallest scales (corresponding to the largest

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values of ε), as well as the universality of the distributions in flows with different large-scale turbulence generation mechanisms. The latter issue is of particular interest in wall-bounded shear flows, where turbulence is created mainly in the anisotropic near-wall region, while the bulk flow away from the walls is expected to be essentially isotropic.

In this work, we address both of these points by using very high-resolution direct numerical simulations (DNS) to study distributions of the local dissipation scale, η , and high-order statistics of ε in three-dimensional, fully-developed turbulent channel flow. The properties of η have been examined in the past from various perspectives, beginning with studies of turbulence multifractality (Paladin & Vulpiani 1987; Nelkin 1990; Biferale 2008). Later, Sreenivasan (2004) suggested that the local dissipation scale be written as $\tilde{\eta}(\mathbf{x}, t) = [\nu^3/\varepsilon(\mathbf{x}, t)]^{1/4}$, allowing fluctuations in the scale to be directly connected to variations in ε . The definition of η used in the present study is based on work by Yakhot (2006), which expresses η in terms of longitudinal velocity increments, $\delta_\eta u_i = |u_i(x_i + \eta) - u_i(x_i)|$ (summation over repeated indices is not implied), using the relation $\eta(\delta_\eta u_i) \approx \nu$. The connection between this relation for η and the Kolmogorov-type scale, $\tilde{\eta}$, is discussed in more detail in the [Appendix](#). The present definition from Yakhot (2006) identifies flow regions – or eddies – of size η with local velocity increments corresponding to Reynolds numbers $Re_\eta = (\delta_\eta u_i)\eta/\nu \approx 1$. The scale η is thus associated with structures where viscous and inertial effects are in approximate balance (Yakhot & Sreenivasan 2005). Probability density functions (p.d.f.s) of η , denoted $Q(\eta)$, have been calculated previously using DNS of homogeneous isotropic turbulence (Schumacher 2007) and in experiments on turbulent pipe flow (Bailey *et al.* 2009) and buoyancy-driven turbulence (Zhou & Xia 2010). Comparisons of $Q(\eta)$ in isotropic turbulence and on the pipe flow centreline have shown qualitative agreement, indicating that $Q(\eta)$ may have a universal form that is independent of the large-scale turbulence generation mechanism.

Here we extend these prior comparisons by performing the first computational study of $Q(\eta)$ in a wall-bounded turbulent shear flow. We examine $Q(\eta)$ as a function of both the friction Reynolds number, $Re_\tau = u_\tau L/\nu$, and wall distance, $y^+ = yu_\tau/\nu$, where u_τ is the friction velocity, L is the channel half-height, and y is the direction normal to the channel walls. Three different Reynolds numbers, $Re_\tau = 180, 381$ and 590 , are examined, and we consider wall distances spanning the full extent of the channel, from the viscous sublayer ($y^+ = 2$) to the channel centreline. This approach allows us to separate near-wall and bulk-flow regions on the basis of dissipation statistics. We also study the height and Reynolds-number dependence of dissipation moments up to fourth order. The scaling of these moments with the global large-scale Reynolds number, $Re = u'L/\nu$, is compared with results from prior studies (Schumacher, Sreenivasan & Yakhot 2007; Donzis, Yeung & Sreenivasan 2008) of homogeneous isotropic turbulence, where $u' = \langle (u'_x)^2 + (u'_y)^2 + (u'_z)^2 \rangle_{x,t}^{1/2}$. Dissipation moments were examined in Boeck, Krasnov & Schumacher (2010) and Hamlington *et al.* (2012) for $Re_\tau = 180$ and 381 , and here we include a third, higher, value of Re_τ in order to test the scaling with Re . We will show that the scaling of the moments in the bulk flow near the centreline coincides with the isotropic case if the Reynolds number is sufficiently large.

2. Direct numerical simulations

DNS is currently the most feasible approach for studying high-order statistics of ε in turbulent channel flows, since experimental measurements covering the full channel

Re_τ	Re	Re_U	$N_x \times N_y \times N_z$	N_t	Δx^+	Δy_c^+	Δz^+	$\Delta t/t_c$
180	339	2 800	$512 \times 1025 \times 512$	403	4.4	0.55	2.2	0.1
381	712	6 667	$1024 \times 1025 \times 512$	134	2.3	1.2	2.3	0.2
590	1160	11 000	$2048 \times 2049 \times 1024$	81	1.8	0.91	1.8	0.2

TABLE 1. Simulation parameters: friction Reynolds number Re_τ ; global Reynolds number $Re = u'L/v$; flux-based Reynolds number $Re_U = UL/v$; grid dimensions $N_x \times N_y \times N_z$; number of temporal snapshots N_t ; streamwise, $\Delta x^+ \equiv \Delta x u_\tau/v$, spanwise, $\Delta z^+ \equiv \Delta z u_\tau/v$, and centreline wall-normal, $\Delta y_c^+ \equiv \Delta y(y/L=1)u_\tau/v$ resolutions; and time step between snapshots, Δt , normalized by $t_c = L/U$. Grid sizes are listed without 2/3 de-aliasing.

height can be complicated by the required small-scale resolution and the need to measure all nine components of $\partial_j u_i$ (see Wallace & Vukoslavcević 2010 for a review). Compared to many previous numerical studies at similar or higher values of Re_τ (e.g. Kim, Moin & Moser 1987; Moser, Kim & Mansour 1999; Hoyas & Jimenez 2006), the resolution of the present DNS has been increased by up to a factor of approximately five in each spatial direction in order to accurately measure high-order moments and small-scale statistics; calculation of the fourth-order moment of ε , for example, requires accurate resolution of at least an eighth-order velocity derivative, as discussed in Schumacher *et al.* (2007). Measuring such high-order derivative moments – which are associated with the finest structures or the steepest gradients in the channel – thus requires resolutions that substantially exceed those used in many prior studies, as shown by Boeck *et al.* (2010) for $Re_\tau = 180$. Similarly high resolutions are also used in recent dissipation-rate studies of turbulent channel flow by Abe & Antonia (2011).

The present simulations are performed using a Fourier–Chebyshev pseudospectral method with 2/3 de-aliasing in all three directions and a second-order time discretization. We solve the Navier–Stokes equations for an incompressible flow given by

$$\partial_i u_i = 0, \quad \partial_i u_i + u_j \partial_j u_i = -\partial_i p + \nu \partial_j^2 u_i, \quad (2.1)$$

where u_i is the total velocity and p is the kinematic pressure field. Time discretization of the governing equations is carried out using implicit representations for linear terms and the explicit, second-order Adams–Bashforth method for nonlinear terms, resulting in an overall second-order-accurate discretization (Boeck *et al.* 2010; Hamlington *et al.* 2012).

The size of the computational domain is $(L_x \times L_y \times L_z)/L = 4\pi \times 2 \times 2\pi$ for $Re_\tau = 180$ and $2\pi \times 2 \times \pi$ for $Re_\tau = 381$ and 590. Temporal snapshots of the velocity and velocity gradient fields are stored every 0.1 convective time units, $t_c = L/U$ (where U is the bulk flow velocity at constant flux), for $Re_\tau = 180$, and every $0.2t_c$ for $Re_\tau = 381$ and 590. This results in 403, 134 and 81 total snapshots for $Re_\tau = 180$, 381 and 590, respectively. Analysis of the data is carried out in x – z planes parallel to the channel walls and statistical convergence is improved by averaging over all available temporal snapshots, as well as using symmetric planes from the top and bottom halves of the channel. In the following, $\langle \cdot \rangle$ denotes an average over x – z planes, at all times, and at both symmetric planes, and is generally a function of y . The fluctuating velocity gradient, $\partial_j u'_i$, necessary to obtain ε is calculated by subtracting $\langle \partial_j u_i \rangle$ at each y from $\partial_j u_i$ in the corresponding x – z plane. Reynolds numbers and resolution details (both temporal and spatial) for the present simulations are summarized in table 1.

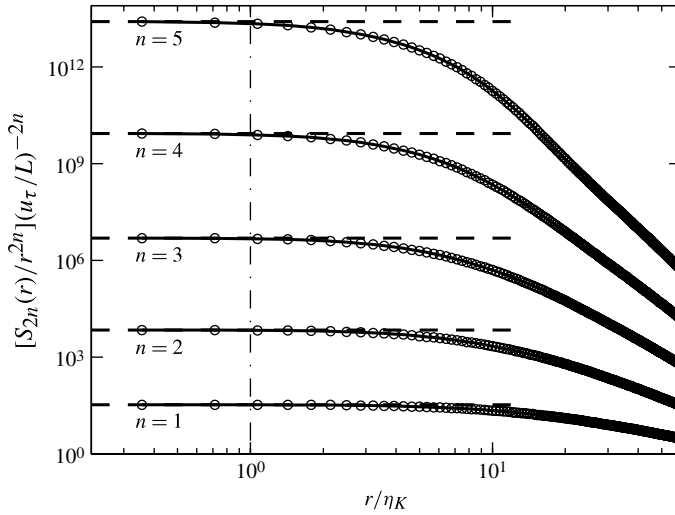


FIGURE 1. Longitudinal structure functions $S_{2n}(r)/r^{2n} = \langle (\delta_r u_x)^{2n} \rangle / r^{2n}$, normalized by $(u_\tau/L)^{-2n}$, at the centreline for $Re_\tau = 590$. Horizontal dashed lines show analytic-range scaling $S_{2n}(r)/r^{2n} = \text{const.}$, and vertical dash-dot line shows $r/\eta_K = 1$.

The adequacy of the resolution used in the present simulations can be examined from the scaling of longitudinal structure functions of the streamwise velocity, denoted $S_{2n}(r) = \langle (\delta_r u_x)^{2n} \rangle$. From Taylor expansion of $S_{2n}(r)$, it follows analytically that $S_{2n}(r) \sim r^{2n}$ when r is small. Very fine resolutions are required to recover this analytic-range behaviour, particularly for high Reynolds numbers and large n (Schumacher *et al.* 2007). Figure 1 shows that, at the centreline for $Re_\tau = 590$, $S_{2n}(r)/r^{2n} \approx \text{const.}$ for small r up to $n = 5$ and for $n = 4$ the analytic range is still approximately recovered up to $r \approx 2\eta_K$.

3. Distributions of local dissipation scales

Local dissipation-scale p.d.f.s, $Q(\eta)$, are calculated by constructing conditional histograms of the scale r when the local Reynolds number, $(\delta_r u_i)r/\nu$, is near 1, or more precisely when $0.9 \leq (\delta_r u_i)r/\nu \leq 1.1$. The p.d.f.s $Q(\eta)$ can then be formally written as $Q(\eta) = P_r[\eta | (\delta_r u_i)r/\nu = 1]$, where $r \in (0, L_i]$ represents all possible values of the spatial increment, P_r is the p.d.f. of r , and the conditional set contains all increments, over all points, where $(\delta_r u_i)r/\nu = 1$ (Schumacher 2007). Including only values of r satisfying this Reynolds-number criterion isolates flow structures occurring at the cutoff between the inertial and dissipative ranges. Since the analysis is carried out in x - z planes, either streamwise, $\delta_r u_x = |u_x(x+r, y, z, t) - u_x(x, y, z, t)|$, or spanwise, $\delta_r u_z = |u_z(x, y, z+r, t) - u_z(x, y, z, t)|$, longitudinal velocity increments can be used to obtain $Q(\eta)$.

Yakhot (2006) showed that one consequence of the continuum of local dissipation scales is that the crossover scale, denoted η_{2n} , between the dissipative and inertial ranges of $S_{2n}(r)$ depends on n and is given by

$$\eta_{2n} = \ell Re_\ell^{1/(\zeta_{2n} - \zeta_{2n+1} - 1)} \quad (3.1)$$

where ℓ is the turbulent integral scale, we take $Re_\ell = u'\ell/\nu$ as the corresponding Reynolds number, and ζ_{2n} are the scaling exponents of $S_{2n}(r)$ in the inertial range. Inserting $\zeta_{2n} = 2n/3$ from the Kolmogorov hypothesis (Kolmogorov 1941) into (3.1)

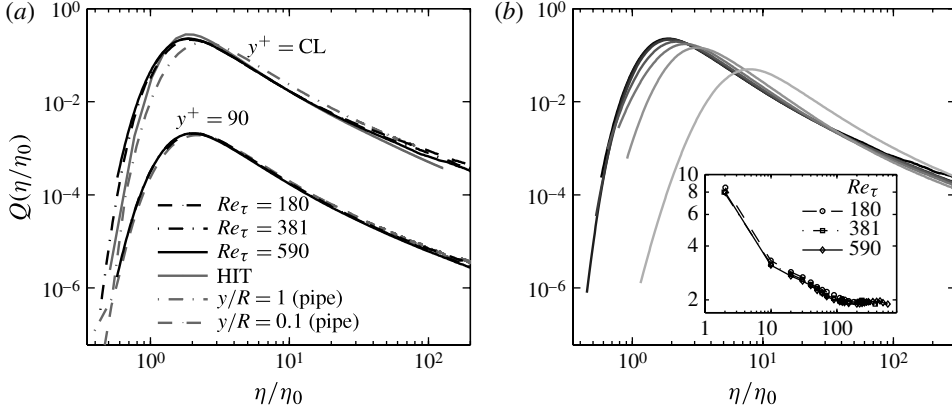


FIGURE 2. (a) Local dissipation scale p.d.f.s $Q(\eta/\eta_0)$ for $Re_\tau = 180, 381$ and 590 at $y^+ = 90$ and the centreline (CL) using streamwise (u_x) velocity increments. Solid lines are cubic splines through the DNS results, and the p.d.f.s for $y^+ = 90$ are shifted down by two decades. Results from DNS of homogeneous isotropic turbulence (HIT) by Schumacher (2007) and turbulent pipe flow experiments by Bailey *et al.* (2009), with pipe radius R , are also shown. (b) Variation of $Q(\eta/\eta_0)$ with y^+ for $Re_\tau = 590$ using streamwise (u_x) velocity increments. P.d.f.s are shown for $y^+ = 2, 10, 30, 60, 120, 200$ and 590 , corresponding to shades from grey (low y^+) to black (high y^+). Solid lines are cubic splines through the DNS data. Inset shows locations of maximum $Q(\eta/\eta_0)$ (vertical axis), denoted $(\eta/\eta_0)_{\max}$, as a function of y^+ (horizontal axis) for all Re_τ .

then gives the classical result $\eta_{2n} = \ell Re_\ell^{-0.75} = \eta_K$. The Kolmogorov scale thus appears only if we make explicit use of the classical Kolmogorov theory. A new scale within this framework, η_0 , follows by using the well-known intermittency corrections that lead to anomalous scaling exponents (e.g. She & Lévéque 1994; Sreenivasan & Antonia 1997). A good approximation for $n < 5$ is $\zeta_{2n} = 2an - 4bn^2$, and using $a = (1 + 9b)/3 = 0.383$ (which is a consequence of $\zeta_3 = 1$) and $b = 0.0166$ then gives

$$\eta_0 \simeq \ell Re_\ell^{-1/(1+a)} = \ell Re_\ell^{-0.72}. \quad (3.2)$$

For the channel flow, the y -dependence of ℓ and Re_ℓ must also be taken into account, giving $\eta_0(y) = \ell(y) Re_\ell(y)^{-0.72}$, where $u'(y) = \langle (u'_x)^2 + (u'_y)^2 + (u'_z)^2 \rangle_{x,z,t}^{1/2}$ is used in $Re_\ell(y)$. This y -dependent normalization is similar to that used in prior studies (Schumacher 2007; Bailey *et al.* 2009) and is related to $\eta_K(y)$ by $\eta_0(y) = \eta_K(y)^{1.12} [u'(y)/v]^{0.12}$. Values of η_0 are always close to the classical Kolmogorov scale η_K , with $\eta_0(y)/\eta_K(y) = Re_\ell(y)^{0.03}$.

Figure 2(a) shows $Q(\eta/\eta_0)$ at $y^+ = 90$ and at the centreline using streamwise velocity increments, $\delta_r u_x$. At both locations, there are only weak variations in $Q(\eta/\eta_0)$ with Re_τ ; similarly weak Reynolds-number dependence was observed for the pipe flow experiments by Bailey *et al.* (2009). For large η/η_0 , all p.d.f.s at both values of y^+ are in close agreement with the pipe-flow measurements and DNS of isotropic turbulence. For small η/η_0 , $Q(\eta/\eta_0)$ at the centreline varies only weakly with Reynolds number, and the magnitude and location of the maxima in the p.d.f.s are close to those found in homogeneous isotropic turbulence. There is also good agreement with the pipe-flow results at $y^+ = 90$ for small η/η_0 , despite the substantially lower Reynolds numbers used in the present simulations.

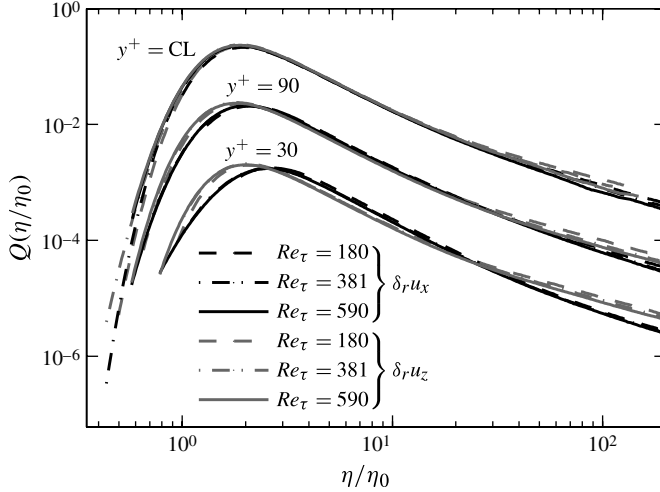


FIGURE 3. Local dissipation-scale p.d.f.s $Q(\eta/\eta_0)$ for $Re_\tau = 180, 381$ and 590 at $y^+ = 30, 90$, and the centreline (CL) using streamwise (u_x) and spanwise (u_z) velocity increments. Lines are cubic splines through the DNS data, and p.d.f.s for $y^+ = 90$ and $y^+ = 30$ are shifted down by one and two decades, respectively.

While there are relatively weak changes in $Q(\eta/\eta_0)$ with Re_τ , the p.d.f.s vary considerably in the near-wall region of the channel. Figure 2(b) shows that $Q(\eta/\eta_0)$ is essentially unchanged for $y^+ \gtrsim 100$, but the location of maximum $Q(\eta/\eta_0)$, denoted $(\eta/\eta_0)_{max}$, increases as the wall is approached (as seen in the inset). At all Re_τ , $(\eta/\eta_0)_{max}$ is close to 2 for $y^+ \gtrsim 100$, but increases for smaller y^+ , with $(\eta/\eta_0)_{max} \approx 8$ at $y^+ = 2$. Interestingly, the rescaling using viscous wall units results in a near-perfect collapse of the $(\eta/\eta_0)_{max}$ curves for the two larger values of Re_τ , suggesting a robustness of the variations in the p.d.f.s with respect to Reynolds number. The increase in $(\eta/\eta_0)_{max}$ in figure 2 may be explained by the presence of extended coherent vortices near the wall (Adrian 2007). These vortices increase the velocity correlation length, particularly in the streamwise (x) direction. The condition $(\delta_r u_x)r/\nu \approx 1$ may thus be satisfied for increasingly large r , resulting in increased $(\eta/\eta_0)_{max}$. The fact that this increase occurs over nearly all y^+ in the $Re_\tau = 180$ case suggests that coherent vortices generated near the wall may dominate the entire channel for small Re_τ .

Comparisons of $Q(\eta/\eta_0)$ calculated using streamwise ($\delta_r u_x$) and spanwise ($\delta_r u_z$) velocity increments in figure 3 give similar insights into the channel flow structure. At the centreline and near the wall, there is little difference in $Q(\eta/\eta_0)$ obtained using $\delta_r u_x$ and $\delta_r u_z$. As the wall is approached, however, the streamwise p.d.f.s shift to larger η/η_0 more rapidly than the spanwise p.d.f.s. This can again be attributed to the presence of extended streamwise vortices near the wall, which result in stronger streamwise velocity correlations and hence smaller differences in u_x (as compared to the spanwise differences in u_z) at any given η/η_0 .

4. Moments of the energy dissipation rate

Dissipation moments $\langle \varepsilon^n \rangle / \langle \varepsilon \rangle^n$ reflect variations in the smallest dissipation scales as a function of y^+ and Re_τ , particularly for high n . Figure 4 shows that the $n = 2-4$

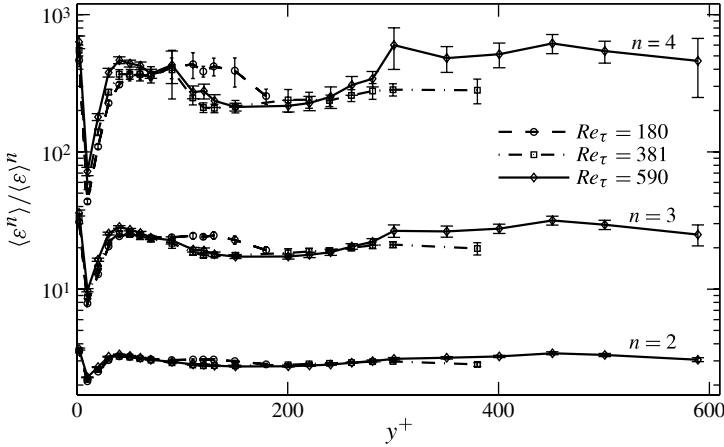


FIGURE 4. Variation of local dissipation moments $\langle \varepsilon^n \rangle / \langle \varepsilon \rangle^n$ with y^+ for $n = 2-4$. Error bars show 90% confidence limits.

moments are similar for all values of Re_τ for $y^+ \lesssim 100$, but above this location, the $Re_\tau = 180$ moments are larger than those for the higher values of Re_τ . This difference may be explained by the bursting (Adrian 2007) of coherent structures away from the wall towards the channel centreline. For small Re_τ , this would introduce high ε amplitudes into the bulk flow region and give the increased $\langle \varepsilon^n \rangle / \langle \varepsilon \rangle^n$ observed for $Re_\tau = 180$ in figure 4. The moments for $Re_\tau = 381$ and 590 , by contrast, remain similar up to $y^+ \approx 200$, and are relatively constant in both cases from $y/L \approx 0.5$ to the centreline.

Estimates of the 90% confidence intervals in figure 4 indicate that there is relatively large statistical variability in the $n = 4$ moments, particularly for $Re_\tau = 590$. These intervals have been estimated using a moving-block bootstrap method (Garcia, Jackson & Garcia 2005) on the time-varying values of $\langle \varepsilon^n \rangle_{xz,s}$, i.e. the normalized moments are calculated separately in each snapshot over x - z planes and symmetric (s) halves of the channel. The block sizes used in the bootstrap analysis are equal to one convective time unit, t_c , for each Re_τ . This corresponds to blocks consisting of 10, 5 and 5 snapshots for $Re_\tau = 180, 381$ and 590 , respectively. Obtaining greater convergence for the high-order moments shown in figure 4 requires even longer time series than those used here, which is currently beyond the limit of our available computational resources.

At the centreline, the turbulence is found to be essentially homogeneous and isotropic, and the resulting moments can be compared with prior results for homogeneous isotropic turbulence (Schumacher *et al.* 2007; Donzis *et al.* 2008). Figure 5 shows that the moments for the two higher values of Re_τ follow similar scaling with large-scale Reynolds number Re (table 1). In particular, the $n = 2-4$ moments for $Re_\tau = 381$ and 590 are in good agreement with the scaling

$$\langle \varepsilon^n \rangle \sim Re^{d_n}, \quad (4.1)$$

where $d_n = n + \zeta_{4n} / (\zeta_{4n} - \zeta_{4n+1} - 1)$, as shown by Yakhot (2006). Calculation of these exponents for homogeneous isotropic turbulence was shown to give $d_2 = 0.152$, $d_3 = 0.476$, and $d_4 = 0.978$ (Schumacher *et al.* 2007). Figure 5 shows, however, that the moments for the $Re_\tau = 180$ case are systematically greater than the scaling laws

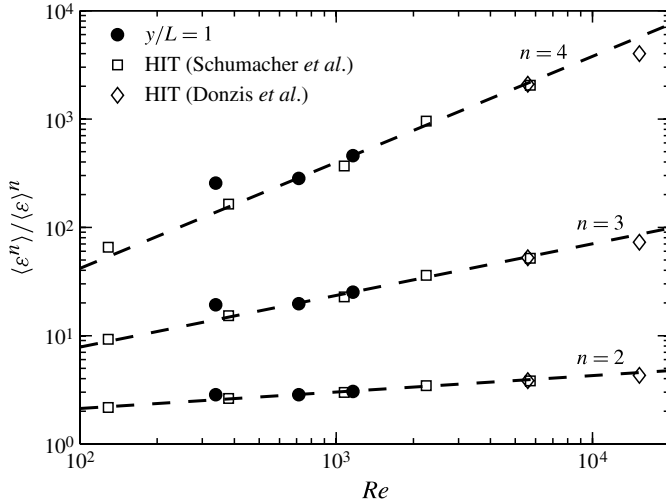


FIGURE 5. Scaling of dissipation moments $\langle \varepsilon^n \rangle / \langle \varepsilon \rangle^n$ with Re from table 1 for $n = 2$ –4. Centerline ($y/L = 1$) moments are compared with DNS of homogeneous isotropic turbulence (HIT) from Schumacher *et al.* (2007) and Donzis *et al.* (2008). DNS results of HIT have been rescaled by constant factors at each n to allow comparisons with the present results.

and all other data. This may again be due to the bursting of coherent structures away from the walls, which dominate the entire channel for small Re_τ (see Boeck *et al.* 2010).

5. Summary and conclusions

Our analysis shows that p.d.f.s of the local dissipation scale and the Reynolds-number dependence of the high-order dissipation moments agree closely with results in homogeneous isotropic turbulence for the bulk of the channel and for sufficiently large Re_τ . The p.d.f.s $Q(\eta/\eta_0)$ are also consistent with those from prior turbulent pipe-flow experiments by Bailey *et al.* (2009). These results suggest that there is a universal (flow-independent) behaviour of the scales, η , at which inertial and viscous processes are in approximate balance. This universality persists for much of the channel (particularly for the highest Re_τ examined here) and is only lost in the near-wall region. The p.d.f.s $Q(\eta/\eta_0)$ remain essentially unchanged for $y^+ \gtrsim 100$ (even when using velocity increments in spanwise and streamwise directions), but systematic variations are observed for all Re_τ as the wall is approached. Similar variations were also observed in the moments of ε , most likely due to the presence of coherent vortical structures near the walls (Adrian 2007). For small Re_τ , these structures dominate the entire channel, resulting in departures of the dissipation moments from the predicted Re -scaling observed at $Re_\tau = 180$ (see figure 5). In order to further examine the universality of η and ε , in the future we would like to explore the robustness of these results for further shear flows, e.g. flows affected by Lorentz forces.

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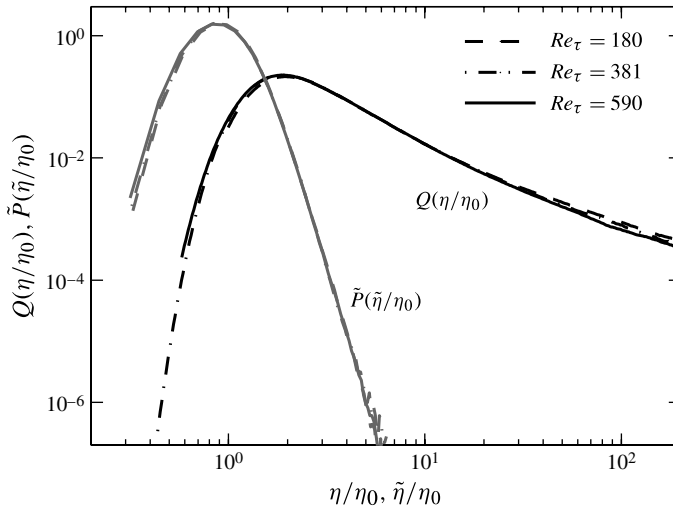


FIGURE 6. Comparisons of $Q(\eta/\eta_0)$ and $\tilde{P}(\tilde{\eta}/\eta_0)$ at the centreline for $Re_\tau = 180, 381$ and 590 .

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Appendix

This appendix explains the relation between the scales η and $\tilde{\eta}$. The length scale, $\tilde{\eta}$, can be constructed from the local, instantaneous value of ε as $\tilde{\eta}(\mathbf{x}, t) = [v^3/\varepsilon(\mathbf{x}, t)]^{1/4}$ (Sreenivasan 2004; Schumacher, Sreenivasan & Yeung 2005). This scale is based on an analogy with the classical Kolmogorov scale η_K , and is distinct from the dissipation scale, η , examined here. The scale η is obtained by requiring that the Reynolds number associated with eddies of size η be $O(1)$. This ensures that the resulting eddies are quasi-laminar (Yakhot & Sreenivasan 2005), and that they are thus associated with the energy-dissipating scales of motion where viscous effects become important. The Kolmogorov-type scale $\tilde{\eta}$ is, by contrast, based on dimensional arguments, and is not necessarily connected to the wide range of quasi-laminar eddy sizes at which dissipation occurs. As a result of this distinction, p.d.f.s of $\tilde{\eta}/\eta_0$, denoted $\tilde{P}(\tilde{\eta}/\eta_0)$, are considerably different from the corresponding p.d.f.s of η/η_0 , as shown at the centreline in figure 6. In particular, $\tilde{P}(\tilde{\eta}/\eta_0)$ has a maximum at $\tilde{\eta}/\eta_0 \approx 1$, and a substantially less broad right tail than $Q(\eta/\eta_0)$. Similar differences between the two p.d.f.s have been observed in prior studies of homogeneous isotropic turbulence (e.g. in Schumacher *et al.* 2005; Schumacher 2007). It should be noted, however, that – consistent with the behaviour of $Q(\eta/\eta_0)$ – there are only weak variations in the p.d.f.s of $\tilde{\eta}/\eta_0$ with Re_τ for the present data.

The differences between $\tilde{P}(\tilde{\eta})$ and $Q(\eta)$ can be examined analytically by considering homogeneous isotropic turbulence (which, as shown in the present study, is approximately the type of turbulence found at the centreline for large Re_τ) and by

noting that ε in such situations is given by

$$\varepsilon = 15\nu(\partial_x u'_x)^2 \approx 15\nu u_\eta^2/\eta^2, \quad (\text{A } 1)$$

where η is small and we have introduced $u_\eta \equiv (\delta_\eta u'_x)$ to simplify the notation. Equation (A 1) is approximately valid for a range of small η and becomes exact as $\eta \rightarrow 0$. From (A 1) and the definition of $\tilde{\eta}$, for a given small η we can write

$$\tilde{\eta} \approx \frac{\eta}{(15Re_\eta^2)^{1/4}}, \quad (\text{A } 2)$$

where $Re_\eta \equiv u_\eta\eta/\nu$. The p.d.f. of $\tilde{\eta}$ is then given by

$$\tilde{P}(\tilde{\eta}) \approx \left| \frac{dRe_\eta}{d\tilde{\eta}} \right| P_{Re_\eta} \left(\frac{\eta^2}{15^{1/2}\tilde{\eta}^2} \right) = \frac{2\eta^2}{15^{1/2}\tilde{\eta}^3} P_{Re_r} \left(\frac{\eta^2}{15^{1/2}\tilde{\eta}^2} \middle| r = \eta \right), \quad (\text{A } 3)$$

where P_{Re_η} denotes the p.d.f. of all Reynolds numbers in the flow over the scale η . We have defined $P_{Re_\eta}(c) \equiv P_{Re_r}(c|r = \eta)$, where r is an arbitrary scale and c is some value of Re_r . This conditional p.d.f. is formed from the set of all Reynolds numbers, Re_r , over the scale $r = \eta$ in the flow. Equation (A 3) can be related to $Q(\eta) = P_r(\eta|Re_r = c)$ by noting that (using Bayes' theorem)

$$Q(\eta) = A(\eta, c)P_{Re_r}(c|r = \eta), \quad (\text{A } 4)$$

where $A(\eta, c) \equiv P_r(\eta)/P_{Re_r}(c)$, and P_r and P_{Re_r} are unconditional p.d.f.s over the entire flow. Comparison of (A 3) and (A 4) reveals several differences between $\tilde{P}(\tilde{\eta})$ and $Q(\eta)$. Most notably, for a given η , each value of $\tilde{\eta}$ in (A 3) corresponds to a different value of Re_η , which is not necessarily $O(1)$. The p.d.f. $\tilde{P}(\tilde{\eta})$ thus includes contributions from regions of size η over which inertial and viscous forces are not in approximate balance. By contrast, $Q(\eta)$ in (A 4) is restricted to $Re_\eta = c$ for all η , where $c \approx 1$ is used in the present study to isolate quasi-laminar regions in the flow. It should also be noted that (A 1) and (A 3) are only accurate for small η , and thus $\tilde{P}(\tilde{\eta})$ is only connected here to $Q(\eta)$ at small scales.

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