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Synthesis of Initial Plane-Symmetric Optical Systems using Parabasal Theory

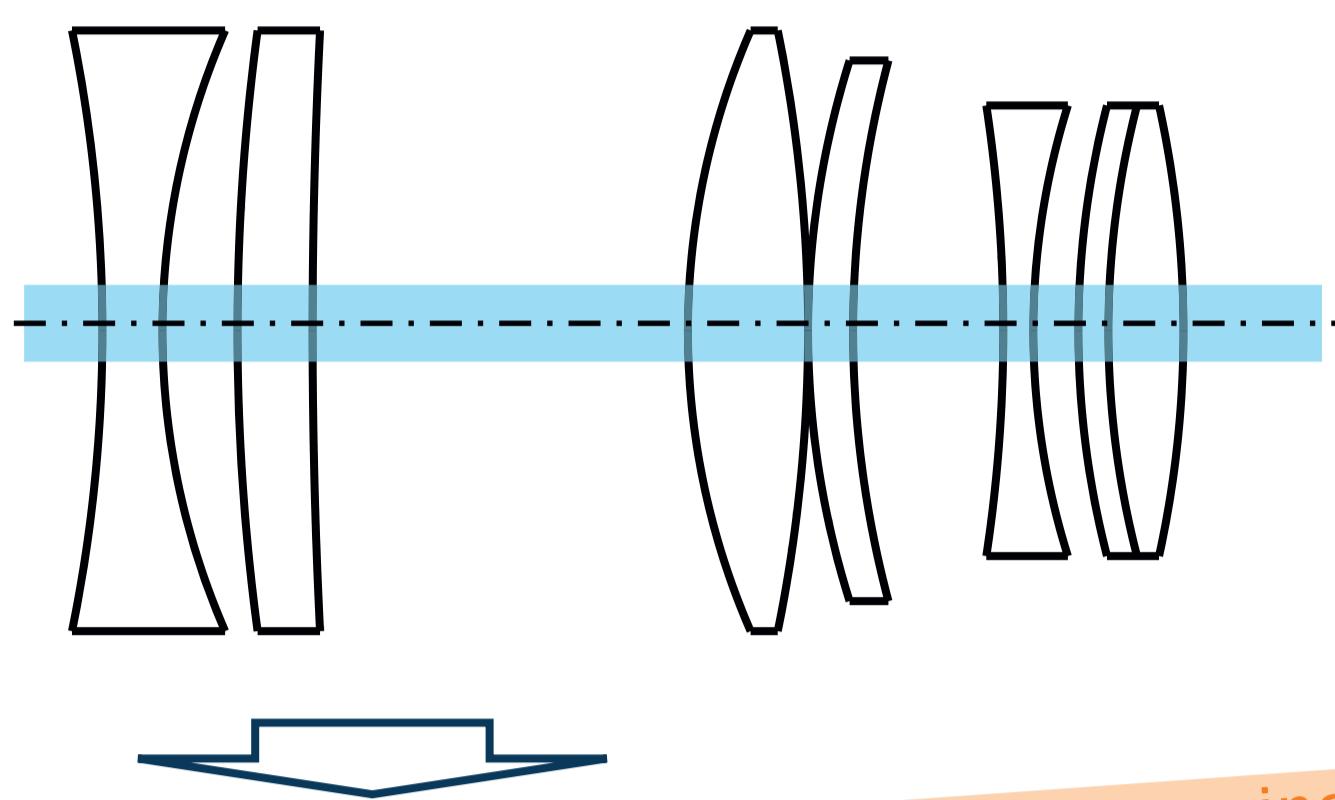


R. Kleindienst, C. Geyer, A. Grewe, B. Mitschunas, S. Sinzinger
Fachgebiet Technische Optik, Technische Universität Ilmenau



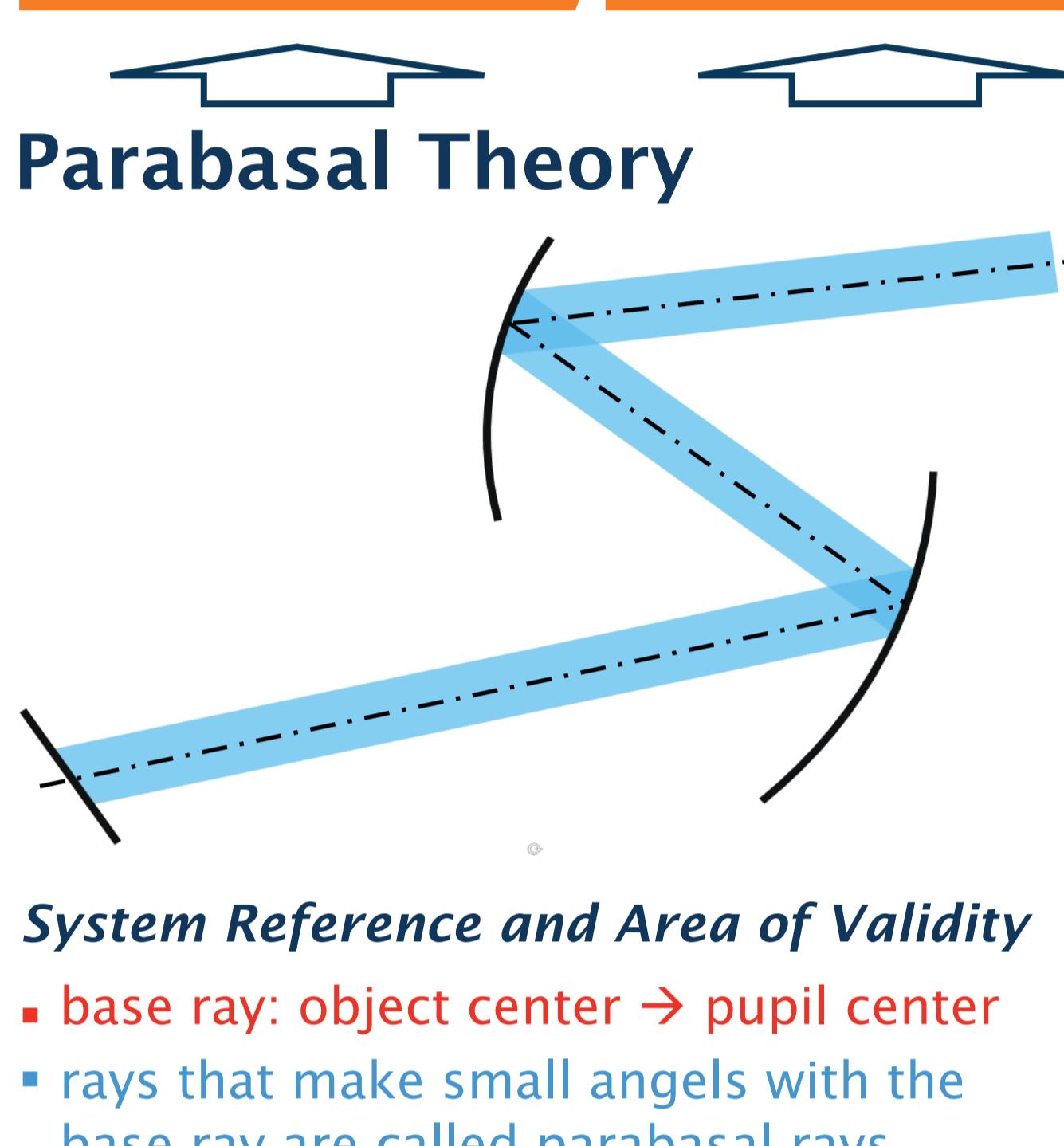
Motivation - From Paraxial (PA) to Parabasal (PB)

Paraxial Theory



- differential region around the reference → optical axis
- valid for rotational symmetric systems only
- single Gaussian image plane

Parabasal Theory



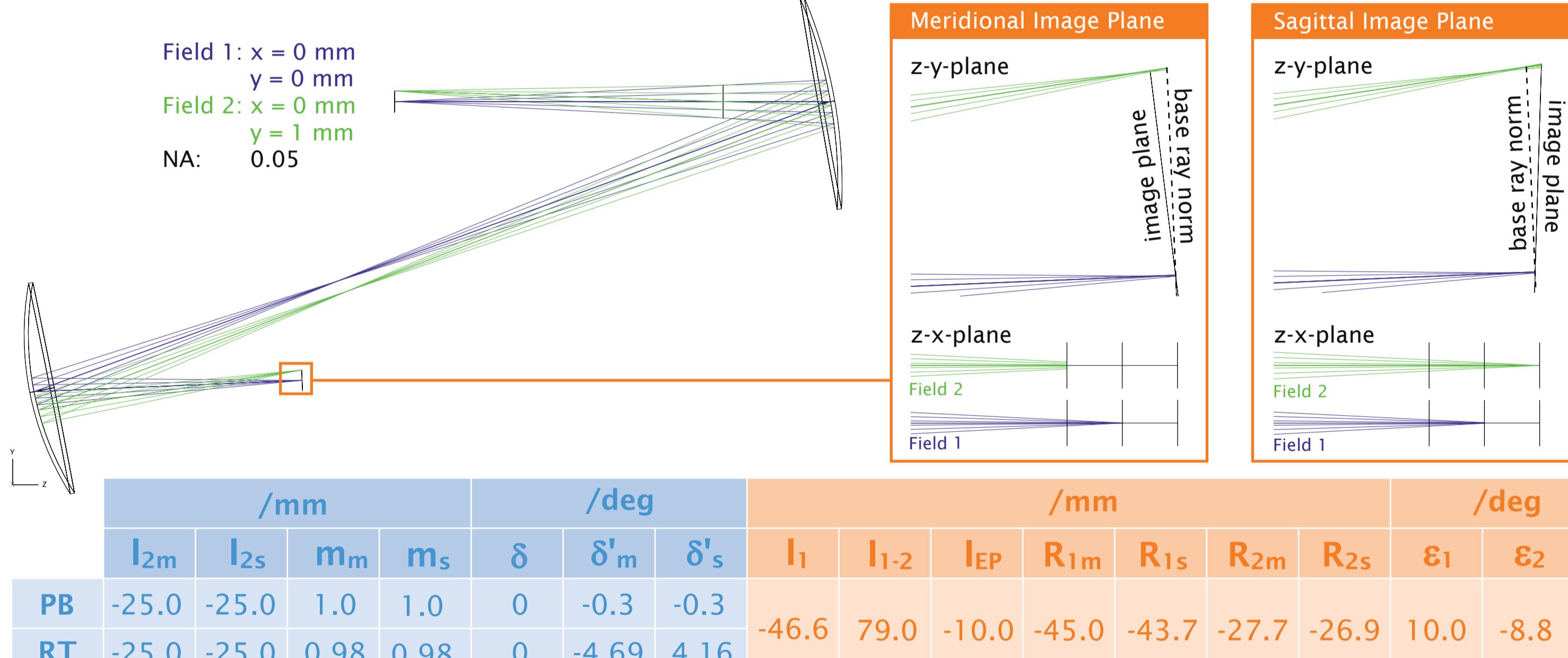
- differential region around the reference → base ray (center object-EP)
- valid for generalized systems
- meridional and sagittal image plane (astigmatism)

Derivation of 1st order imaging properties for tilted systems

Real Raytracing Simulation & Final Optimization

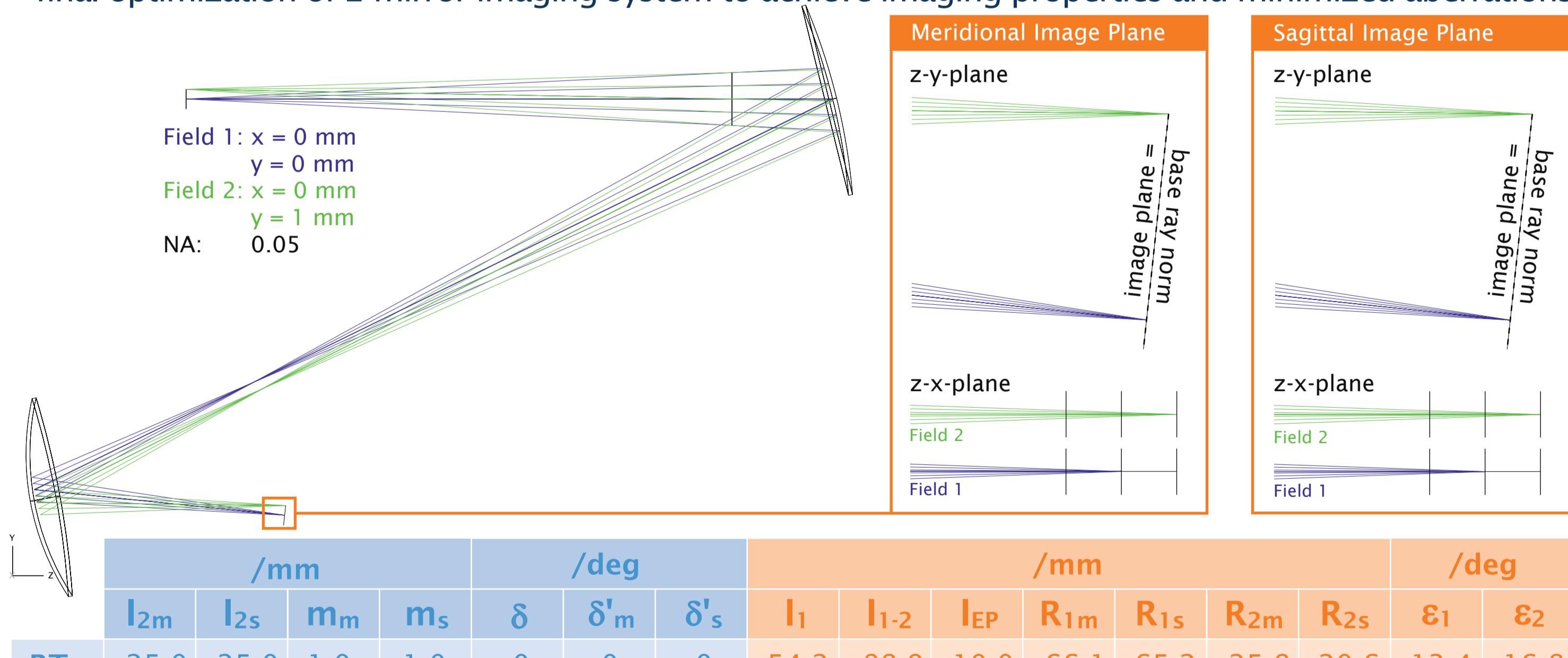
Raytracing Simulation of Initial System

- comparison of 1st order imaging properties derived from parabasal theory (PB) with raytracing (RT) results



Raytracing based Optimization of Initial System

- final optimization of 2 mirror imaging system to achieve imaging properties and minimized aberrations



Imaging properties & aberration optimized tilted optical system

Conclusion

- analytical expressions for 1st order imaging properties of plane-symmetric optical systems
- analytical & optimization based determination of highly tilted, plane-symmetric initial systems
- automatic transfer of initial lens data to commercial raytracing software for final optimization

References

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- R. Abd El-Maksoud, M. Hillenbrand, S. Sinzinger, "Parabasal theory for plane-symmetric systems including freeform surfaces," Opt. Eng. 53(3) (2013)

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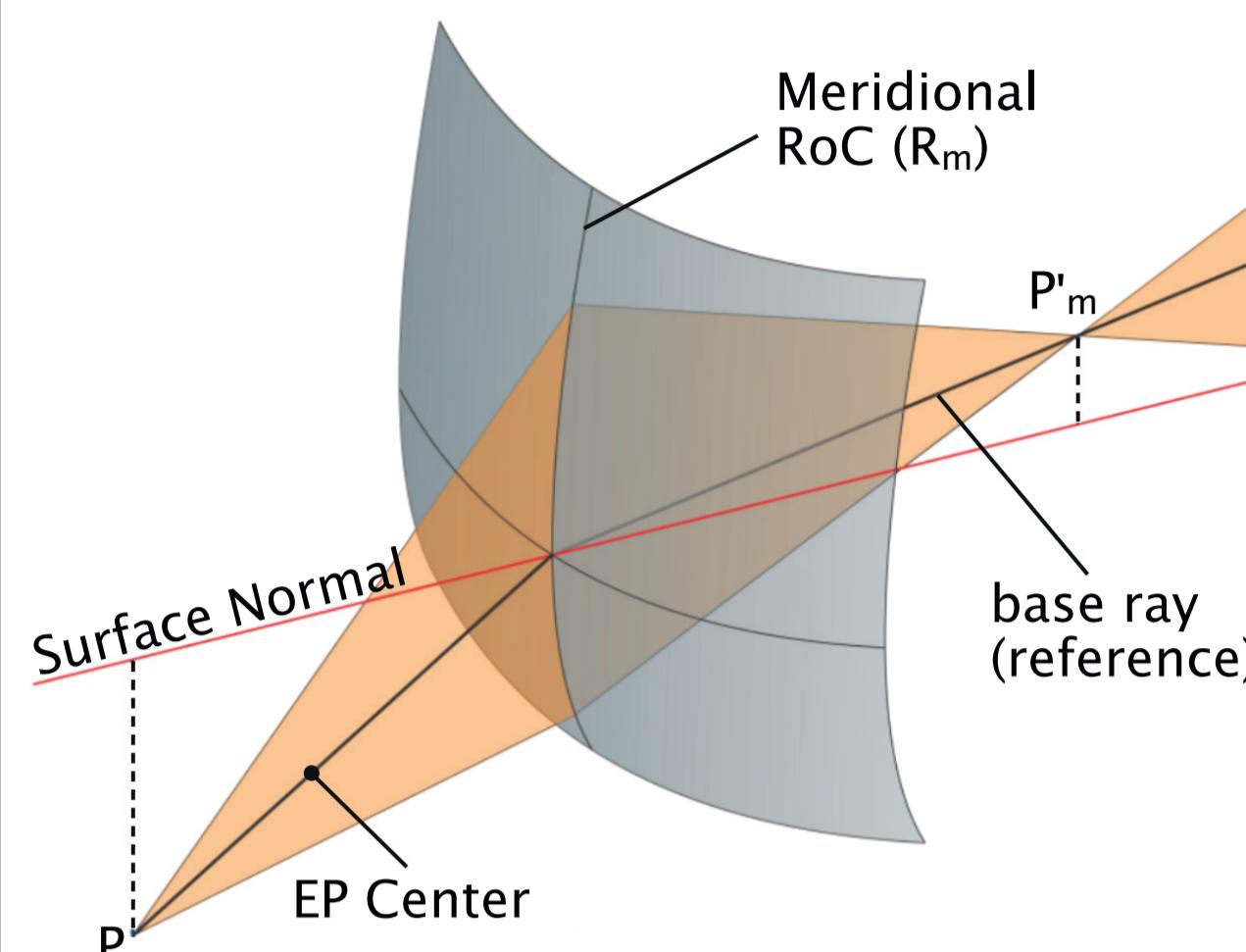
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Derivation of Parabasal Imaging Framework

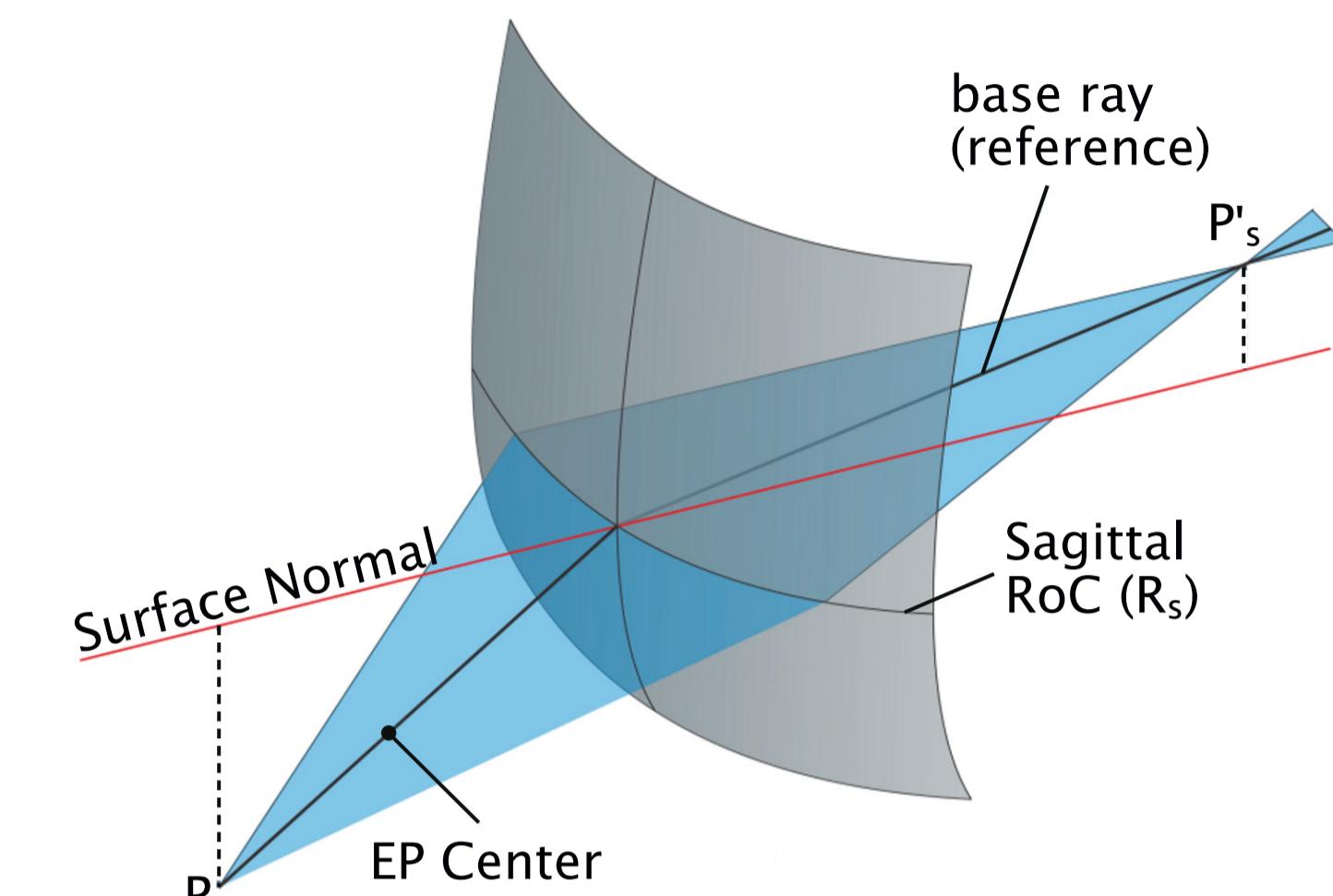
Characteristics in Differential Regime around the Base Ray

- any surface in the vicinity of a specific point is appropriately described by two curvatures
- object / entrance pupils are imaged into meridional & sagittal image points / exit pupils

Meridional Imaging



Sagittal Imaging



Concept for Parabasal Imaging Framework Derivation

- infinitesimal object point shift → determination of image point shift using Coddingtons eq.

Coddingtons Equations

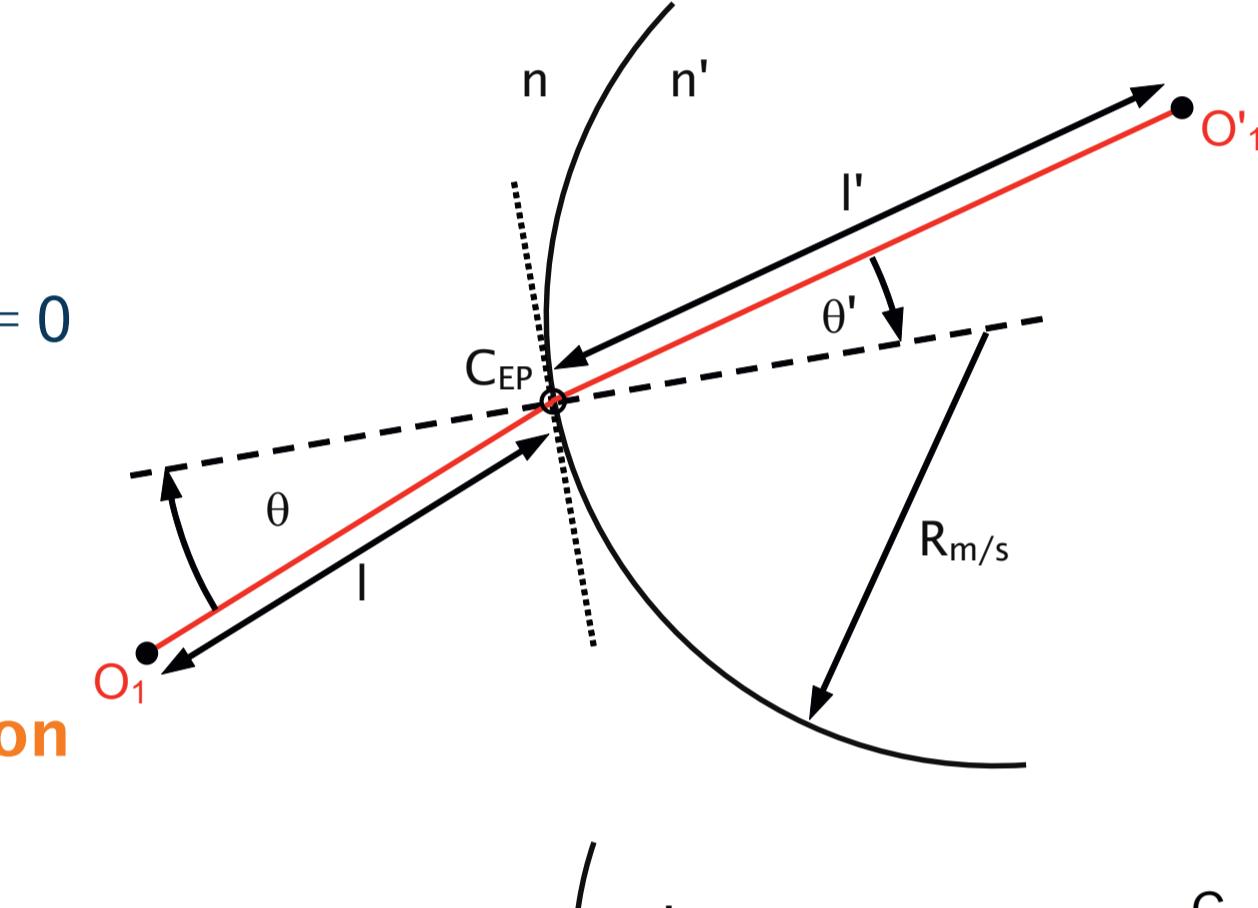
meridional

$$F_m(l_m, l'_m, \theta_m, \theta'_m) = \frac{n' \cos^2 \theta'_m}{l'_m} - \frac{n \cos^2 \theta_m}{l_m} - \frac{n' \cos \theta'_m - n \cos \theta_m}{R_m} = 0$$

sagittal

$$F_s(l_s, l'_s, \theta_s, \theta'_s) = \frac{n'}{l'_s} - \frac{n}{l_s} - \frac{n' \cos \theta'_s - n \cos \theta_s}{R_s} = 0$$

⇒ meridional & sagittal image & pupil center position



Differential Geometry and Geometric Relations

O₁ to O₂ by dI, dq → dθ, dθ' → O₁' to O₂' by dI', dq'

with total derivatives dF_m, dF_s → δ'_m, δ'_s

⇒ meridional & sagittal image plane tilt

obj. shift along base ray, i.e. dq = dq' = 0 → M_m, M_s

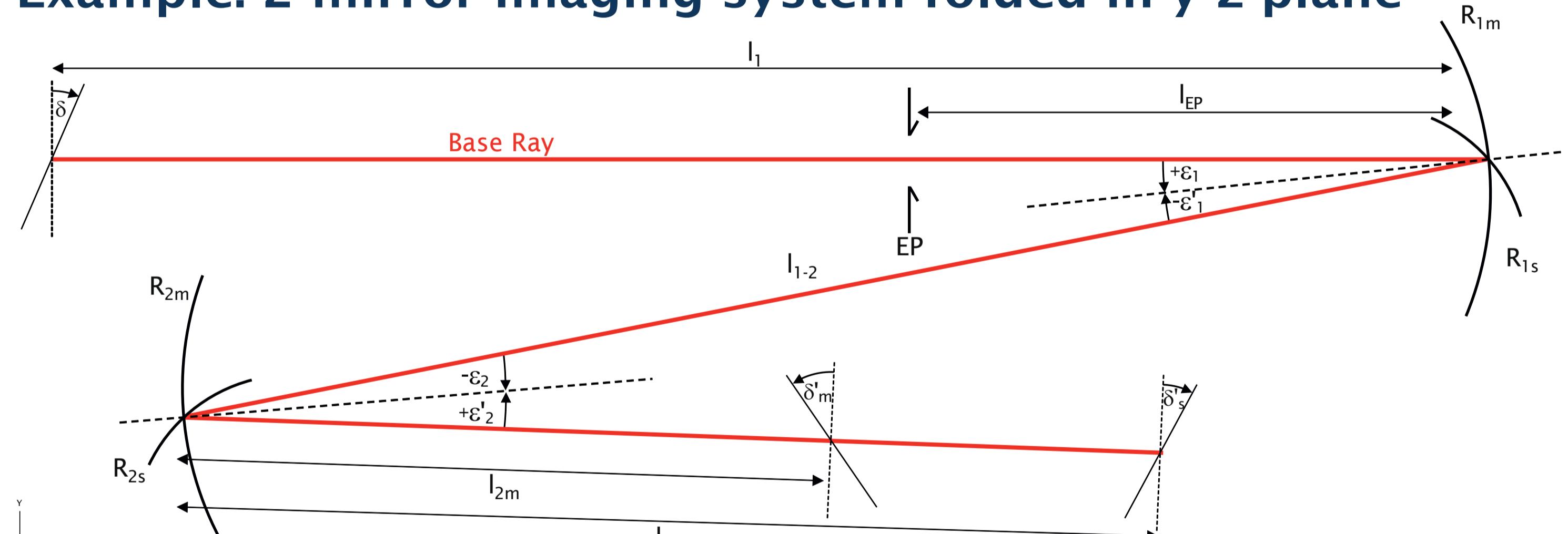
obj. shift perp. to base ray, i.e. dθ = dθ' = 0 → m_m, m_s

⇒ meridional & sagittal axial (M_{m/s}) & lateral (m_{m/s}) magnification

1st order imaging properties as optimization objective functions

Efficient Synthesis of an Initial System

Example: 2 mirror imaging system folded in y-z-plane



Imaging Requirements

image distances I_{2m} = I_{2s} = -25 mm

lateral magnification m_m = m_s = 1

object plane tilt δ = 0°

image plane tilt δ'_m = δ'_s = 0°

Variable System Parameters

object distance I₁

mirror distance I₁₋₂

EP distance I_{EP}

mirror RoCs R_{1m/s}, R_{2m/s}

mirror tilts ε₁, ε₂

Constants

n_{1-mirror1} = n_{1-mirror2} = 1

n_{2-mirror1} = n_{2-mirror2} = -1

Optimization of System Parameters based on Objective/Merit Functions derived from Coddingtons Equations

	/mm	/deg	/mm	/deg
I _{2m}	-25.0	-25.0	1.0	1.0
I _{2s}	-25.0	-25.0	1.0	1.0

Automatic transfer of initial system parameters to raytracer

Outlook

- derivation of more accurate expression of image plane tilts
- application of imaging framework for initial freeform surface synthesis
- extension of parabasal imaging framework to optical systems without symmetry