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Effects of Changes in Surface Water Regime and/or Land Use on the Vertical Distribution of Water Available for Wetland Vegetation: Dynamic Model of the Zone of Aeration (Appendix to Part 1 of Completion Report for Project A-023-ARK)

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**APPENDIX
for
DYNAMIC MODEL OF THE ZONE OF AERATION**

(Appendix to Part I of Completion Report for Project A-023-ARK)

Documentation of Computer Program

by
Robert N. MacCallum
Principal Investigator



Arkansas Water Resources Research Center

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Appendix to Publication No. 70

1980

Research Project Technical Completion Report

OWRT Project No. A-023-ARK

Effects of Changes in Surface Water Regime and/or
Land Use on the Vertical Distribution of Water Available for
Wetland Vegetation

by

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R. A. Sims
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University of Arkansas

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June 1980

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REPORT FORMAT

PART I - DYNAMIC MODEL OF THE ZONE OF AERATION
(Included herein)

PART I (Appendix) - DOCUMENTATION OF COMPUTER PROGRAM
(Included as a separate document and available upon
request from the Arkansas Water Resources Research
Center, University of Arkansas, Fayetteville, AR 72701.

PART II - PORTABLE ENVIRONMENTAL DATA LOGGER AND SENSORS
(Included as a separate document)

Each of parts I and II is complete within itself, and may
be distributed separately or as a single report.

PART I

APPENDIX

DOCUMENTATION OF COMPUTER PROGRAM

by

Robert N. MacCallum

Principal Investigator

June, 1980

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APPENDIX I-A
Documentation of Computer Program

I. Program Information

Origin of Program:

General Office:

Director, Arkansas Water Resources Research Center
University of Arkansas
Fayetteville, AR 72701

Principal Investigator:

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Benton, Arkansas

Purpose of Program:

The program documented here describes the vertical distribution of water in the zone of aeration available for use by vegetation in a wetlands environment.

Problem Statement:

Vegetation is generally thought to be in dynamic equilibrium with the environment. As the environment changes, vegetation can be expected to change until a new balance is approached or achieved. Flood control measures put into effect in

Eastern Arkansas during the last twenty-five years have allowed previously flood-prone areas to be cleared of wetland forests for agriculture. Parts of the remaining wetland forests, which were in equilibrium with environmental conditions typically including extensive annual flooding, are now thought to be out of balance with an environment characterized by reduced flooding or no flooding. A study of relationship between hydrologic change and vegetation change should be invaluable as a planning tool for future use of wetland forest areas.

Areas of Application:

This program may be used to determine the optimum use of wetlands of any region by predicting the impact of proposed flood control and drainage projects on the wetlands environment.

Methods of Computation:

The basic equations are the differential equations which describe isothermal, one-dimensional, unsteady-state, simultaneous flow of water and air in a porous medium. These are a set of two second order, non-linear, partial differential equations. Because of the complexity of these equations, it was necessary to use numerical techniques. The partial differential equations were converted to a finite difference form and solved using an iterative implicit procedure.

Basis for Selection of Method:

Because of the complexity of the partial differential equations, an analytical solution could not be achieved, and the numerical solution was the only available technique.

Limitations and Restrictions:

The Theoretical Development section of the body of the report includes the assumptions which were made in the development of the model.

Equations and Derivations:

Derivation of the basic equations of the model is shown in the Theoretical Development section of the report.

Definition of Technical Terms:

The definition of all variable and constant names used in the computer program is given by comment statements in the main program body.

Physical Constants:

The physical constants and program parameter values used in the model are listed in Appendix I-C.

Functional Information:

The finite difference approximations of the partial differential equations was solved numerically. The depth of the soil column was directed into intervals and the differential terms in each of the partial differential equations were

replaced by finite differences. Essentially a iterative implicit procedure was used to calculate pressures and saturation at each time step, converging after meeting a maximum allowable residual mass or pressure. Briefly, the computation for each time step is:

1. The coefficients of the difference are calculated.
2. The residual mass values are determined.
3. The difference equations are solved by the Gaussian elimination method yielding pressure residuals.
4. New values of pressure are calculated at each grid node.
5. The iteration parameter is advanced by one and the residuals are recalculated. Convergence is checked by comparing residuals to the maximum allowable residuals.
6. If convergence criteria are not met, steps 3, 4 and 5 are repeated. This cyclical process continues until a preset maximum number of iterations is reached. The program continues after an error message if convergence is not attained.
7. New values of saturation are calculated using the capillary pressure-saturation relationship once convergence has been reached.

8. At the end of each time step a material balance calculation is made.

II. Usage Information

Programming Language, Equipment, and Operating System:

The computer program was written in FORTRAN IV for the IBM 360 system. The model requires 24k of 36 bit-word of core storage. It uses a magnetic tape for restart purposes.

Input Requirements:

Data input is by cards, and no special input is necessary.

Secondary Storage Input Format:

None

Input Data Description:

Data input is by punched card. Input requirements and formats are given by comments in the data input subroutine, LNKA.

Program Output:

Sample program output is shown in the example case.

Operator Instructions:

No special instructions are required.

Off-Line Error Messages:

No error messages are generated by the program.

Definition of Technical Terms:

A complete listing of all terms used in the program is given by comment cards in the main program.

Example Case:

An example case is included as Appendix I-D.

Job Processing Time:

Computer time usage varied from less than two minutes per year to about six minutes per year of simulation time.

APPENDIX I-B
Computer Program Listing

V G LEVEL 21 MAIN DATE = 74186 17/44/00

- C MNEMCNICS
- C
- C AAAA WETTING PHASE ACCUMULATION IN THE SYSTEM AT EACH TIME
- C STEP BASED ON SOURCE/SINK TERMS (LBM)
- C AANTRY NUMBER OF ITERATIONS IN EACH TIME CONSTANT
- C ACG MATERIAL BALANCE RATIO, NON-WETTING PHASE (FFFF-RESG)/
- C CDDD
- C AG (RESG-CDDD) (LBM)
- C ACW MATERIAL BALANCE RATIO, WETTING PHASE (EEEE-RESW)/CCCC
- C AIRKG EVAP. MASS-TRANSFER (LBM/SQ.FT/ R) (HR/MILE)**.8(1/PSI)
- C AKGLEA TRAN. MASS-TRANSFER (LBM/SQ.FT/HR) (HR/MILE)**.8(1/PSI)
- C AKXML ABS. PERM. MULTIPLIER
- C AIRRE AIR FILM RESISTANCE AT SOIL SURFACE
- C APOR AVERAGE POROSITY IN SOIL ROOT ZONE
- C (CU FT WETTING PHASE/CU FT ROCK)
- C ASSS CAPILLARY PRESSURE INTERCEPT FOR SW .LE. WILPO
- C AS(LAYER,NKK) INTERCEPT OF A TANGENT CURVE TO THE CAPILLARY
- C PRESSURE-WETTING PHASE SATURATION CURVE
- C AVG NCN-WETTING PHASE VISCOSITY AT I-TH GRID POINT (CP)
- C AVGF NCN-WETTING PHASE VISCOSITY AT (I+1) TH GRID POINT (CP)
- C AVWF WETTING PHASE VISCOSITY AT (I+1) TH GRID POINT (CP)
- C AVSATL AVERAGE SATURATION IN ROOT ZONE
- C AVW WETTING PHASE VISCOSITY AT I-TH GRID POINT (CP)
- C AW (RESW-CCCC) (LBM)
- C AWSAT AVERAGE SATURATION IN SOIL ROOT ZONE
- C BBBB NCN-WETTING PHASE ACCUMULATED IN THE SYSTEM AT
- C EACH TIME STEP (LBM)
- C BSSS CAPILLARY PRESSURE SLOPE FOR SW .LE. WILPC
- C BS(LAYER,NKK) SLOPE OF A TANGENT TO THE CAPILLARY PRESSURE-
- C WETTING PHASE SATURATION CURVE
- C BW(I) DUMMY VARIABLE USED FOR WETTING PHASE SATURATION
- C (CU.FT. OF WETTING PHASE / CU.FT. PORE)
- C C(I)(N) MATRIX COEFFICIENTS
- C CCCC TOTAL WETTING PHASE ACCUMULATION BASED ON SOURCE/SINK
- C TERMS (LBM)
- C C AND CD MATRIX MULTIPLIERS
- C DDDD TOTAL NCN-WETTING PHASE ACCUMULATION BASED ON SOURCE/
- C SINK TERMS (LBM)
- C DG(I) NCN-WETTING PHASE DENSITY (LBM PER CU. FT.)
- C DIPG STARTING POINT COORDINATE ON NON-WETTING PHASE DENSITY-
- C PRESSURE CURVE
- C DIPW STARTING POINT COORDINATE ON WETTING PHASE DENSITY-
- C PRESSURE CURVE
- C DISKG STARTING POINT COORDINATE ON NCN-WETTING PHASE RELATIVE
- C PERMEABILITY-WETTING PHASE SATURATION CURVE
- C DISKW STARTING POINT COORDINATE ON WETTING PHASE RELATIVE
- C PERMEABILITY-WETTING PHASE SATURATION CURVE
- C DIP STARTING POINT COORDINATE ON VISCOSITY CURVE
- C DIQW STARTING POINT COORDINATE ON WETTING PHASE INJECTION
- C CURVE
- C DISW(LAYER) STARTING POINT ON WETTING PHASE SATURATION-
- C DP PRESSURE INCREMENT ON VISCOSITY CURVE (PSI)
- C DLTMAX MAX. SIZE OF TIME STEP
- C DMGX NCN-WETTING PHASE MOBILITY RATIO
- C DMWX WETTING PHASE MOBILITY RATIO
- C CPC CAPILLARY PRESSURE INCREMENT (PSI)
- C DPG PRESSURE INCREMENT ON NCN-WETTING PHASE DENSITY-
- C PRESSURE CURVE (PSI)

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C DPW PRESSURE INCREMENT ON WETTING PHASE DENSITY-
C PRESSURE CURVE (PSI)
C DSKG NCN-WETTING PHASE SATURATION INCREMENT ON ON-WETTING
C PHASE RELATIVE PERMEABILITY CURVE
C (CU.FT. / CU.FT. PORE)
C DSKW WETTING PHASE SATURATION INCREMENT ON WETTING PHASE
C RELATIVE PERMEABILITY CURVE
C (CU.FT. / CU.FT. PORE)
C DSW STARTING PCINT CCOORDINATE ON WETTING PHASE SATURATION-
C CAPILLARY PRESSURE CURVE (PSI)
C DSW(LAYER)STARTING PCINT CCOORDINATE ON WETTING PHASE SATURATION-
C CAPILLARY PRESSURE CURVE (PSI)
C DT TIME INCREMENT (HCLR)
C CW(I) WETTING PHASE DENSITY (LBM / CU. FT.)
C DX1 AND DX2 SPACE INCREMENTS
C EEEE WETTING PHASE INITIALLY IN SYSTEM (LBM)
C EKGM CONVERGENCE CRITERIA FOR NON-WETTING PHASE PRESSURE
C EKWM CONVERGENCE CRITERIA FOR WETTING PHASE PRESSURE
C ESTAR MAX. NUMBER OF TIME STEPS TO BE COMPUTED
C EVALEN DISTANCE TO EVAPC. SURFACE (FOOT)
C FCONV CONVERSION FACTOR FOR PSI TO PSF
C FFFF NCN WETTING PHASE INITIALLY IN THE SYSTEM
C FINAL KEY VARIABLE FOR TAPE USAGE AND CALL EXIT
C GGGG MATERIAL BALANCE RATIO, WETTING PHASE BASED ON AMOUNT
C INITIALLY IN PLACE (RESW-CCCC)/EEEE
C GRESG MAX. RESIDUAL FOR NCN-WETTING PHASE
C GRESW MAX. RESIDUAL FOR WETTING PHASE
C GSUM AMOUNT OF NON-WETTING PHASE IN MODEL (LBM)
C H(N) HEIGHT (FEET)
C HHHH MATERIAL BALANCE RATIO, NON-WETTING PHASE BASED ON
C AMOUNT INITIALLY IN PLACE (RESG-DDDD)/FFFF
C HK(I) ITERATION PARAMETER
C IT IS THE MIN. TIME (SEC) FOR THE RUN TO WRITE ON TAPE AND EXIT
C ITSTOP IS NO LONGER USED. REMAINING TIME ROUTINE IS NOW USED.
C HOFLEAF HEIGHT OF THE PLANT FROM A DATUM PLANE
C IOUTPT KEY TO SPECIFY OUTPUT
C INSW =0 , INITIAL SAT. WILL BE AS READ, =1, INITIAL SAT.
C WILL BE CALCULATED FROM CAPILLARY CURVE
C ITAPE KEY FOR THE USE OF THE RESTART TAPE
C KC ITERATION INDEX
C KX(N) ABSOLUTE PERMEABILITY (CARCYS)
C LAYER, LAY NUMBER OF SCIL LAYER IN MODEL
C MAXG LOCATION OF MAXIMUM NON-WETTING PHASE RESIDUAL
C MAXW LOCATION OF MAXIMUM WETTING PHASE RESIDUAL
C MTRY MAX. NUMBER OF ITERATION STEPS
C NBUG KEY VARIABLE FOR DEBUGGING PURPOSES
C NOLAY NO. OF CAPILLARY PRESSURE CURVE
C NHK NUMBER OF ITERATION PARAMETERS IN A CYCLE
C NPCC NUMBER OF PCINTS ON CAPILLARY PRESSURE-WETTING PHASE
C SATURATION CURVE
C NSTAR TAPE USAGE INDICATION
C NTRY NUMBER OF ITERATION STEPS
C NWELLS NUMBER OF SINK (SCLRCE)
C NX, NA, NL NUMBER OF GRID PCINTS
C PC(I) CAPILLARY PRESSURE (PSI)
C PCI STARTING PCINT CCOORDINATE ON CAPILLARY PRESSURE WETTING
C PHASE SATURATION CURVE
C PG(N) NCN-WETTING PHASE PRESSURE CALCULATED AT OLD TIME STEP

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C	(PSI)			
C	PGA(N)	NON-WETTING PHASE PRESSURE CALCULATED AT NEW TIME STEP		
C	(PSI)			
C	P GCFV	PER CENT GRCOND COVERC BY VEGETATION		
C	PGB(N)	NON-WETTING PHASE PRESSURE DIFFERENCE BETWEEN TWO		
C	SATURATCN	(PSI)		
C	PGIN(N)	NCN-WETTING PHASE PRESSURE AT BOUNCARY OF N-TH GRID		
C	(PSI)			
C	PKEY(N)	KEY VARIABLE FOR INJECTION/PRODUCTION FROM A GRID PT.		
C	PLCCNCU	PLANT CONDUCTIVITY LBM/SQ FT-HR-PSI		
C	POFLAW	CRITICAL LEAF PCTENTIAL FT-HR-PSI		
C	POR(N)	PCFCSTY		
C	POTCFR	WETTING PHASE PCTENTIAL AT ROOT SURFACE (PSI)		
C	POTPFL	WETTING PHASE PCTENTIAL AT LEAF SURFACE (PSI)		
C	PMCHG	CONVERGENCE CRITERIA FOR PGB(N)		
C	PMCHW	CONVERGENCE CRITERIA FOR PWB(N)		
C	PW(N)	WETTING PHASE PRESSURE AT OLD TIME STEP (PSI)		
C	PWA(N)	WETTING PHASE PRESSURE AT NEW TIME STEP (PSI)		
C	PWB(N)	WETTING PHASE PRESSURE DIFFERENCE BETWEEN TWO		
C	SATURATCN	(PSI)		
C	PWIN(N)	WETTING PHASE PRESSURE AT BOUNDARY OF N-TH GRID		
C	(PSI)			
C	QDD	IS THE DRAINAGE FUNCTION CONSTANT		
C	QEVA(N)	EVAPORATION FRCH N-TH CELL (LBM/HR/SQ FT)		
C	QG(N)	RATE OF NCN-WETTING PHASE IN (OUT) (LBM/HR/FT SQ)		
C	QQQEVA	CUMULATIVE EVAPCRATION (LBM/SQ FT)		
C	QQQTRA	CUMULATIVE TRANSPIRATION (LBM/SQ FT)		
C	QTA, QTB, AND QTC	ARE ALL SEASONAL TRANSPIRATION FUNCTION CONST.		
C	QTRAN(N)	TRANSPIRATION FRCH N-TH GRID POINT DURING ONE TIME		
C	INTERVAL	(LBM/SQ FT/HR)		
C	QTRANT	TRANSPIRATION CURING ONE TIME INTERVAL (LBM/SQ FT/HR)		
C	QW(N)	RATE OF WETTING PHASE IN (OUT) (LBM/HR/FT SQ)		
C	QWF	PRECIPITATION (INCH/DATA POINT INTERVAL)		
C	RESG	TCTAL AMCNT CF NCN-WETTING PHASE REMAINING IN SYSTEM		
C	(LBM)			
C	RESTAR	TAPE USAGE INDICATOR		
C	RESW	TCTAL AMPLNT CF WETTING PHASE REMAINING IN SYSTEM (LBM)		
C	RG	NCN-WETTING PHASE DENSITY AT I-TH GRID POINT CALCULATED		
C	AT CLD	PRESSURE (LBM/CU FT)		
C	RGA	NCN-WETTING PHASE DENSITY AT I-TH GRID POINT CALCULATED		
C	AT NEW	PRESSURE (LBM/CU FT)		
C	RGF	NCN-WETTING PHASE DENSITY AT (I+1)TH GRID POINT		
C	CALCLLATED	AT CLD PRESSURE (LBM/CU FT)		
C	RGXB	NCN-WETTING PHASE DENSITY AT (I+1)TH GRID POINT		
C	CALCLLATED	AT NEW PRESSURE (LBM/CU FT)		
C	RGXF	NCN-WETTING PHASE DENSITY AT (I+1)TH GRID POINT		
C	CALCLLATED	AT NEW PRESSURE (LBM/CU FT)		
C	RKG	NCN-WETTING PHASE RELATIVE PERMEABILITY		
C	(DIMENSIONLESS)			
C	RKGB	NCN-WETTING PHASE RELATIVE PERMEABILITY		
C	AT (I+1)TH	GRID PCINT (DIMENSIONLESS)		
C	RKGC	NCN-WETTING PHASE RELATIVE PERMEABILITY		
C	AT I-TH	GRID PCINT (DIMENSIONLESS)		
C	RKGF	NCN-WETTING PHASE RELATIVE PERMEABILITY		
C	AT (I+1)TH	GRID POINT (DIMENSIONLESS)		
C	RKW	WETTING PHASE RELATIVE PERMEABILITY (DIMENSIONLESS)		
C	RKWB	WETTING PHASE RELATIVE PERMEABILITY AT (I+1)TH GRID		
C	POINT	(DIMENSIONLESS)		

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C RKWC WETTING PHASE RELATIVE PERMEABILITY AT I-TH GRID POINT
C (DIMENSIONLESS)
C RKWF WETTING PHASE RELATIVE PERMEABILITY AT (I+1)TH GRID
C POINT (DIMENSIONLESS)
C RHUM(NN) AIR HUMIDITY
C RROOTN NUMBER OF GRID POINTS IN WHICH ROOTS PENETRATE
C RSGA SUM OF NON-WETTING PHASE RESIDUAL
C RSWA SUM OF WETTING PHASE RESIDUAL
C RW WETTING PHASE DENSITY AT I-TH GRID POINT CALCULATED AT
C OLD PRESSURE (LBM/CU FT)
C RTDEN(NN) ROOT DENSITY (FT ROOT/CU.FT SOIL)
C RWA WETTING PHASE DENSITY AT I-TH GRID POINT CALCULATED AT
C OLD PRESSURE (LBM/CL FT)
C RWF WETTING PHASE DENSITY AT (I+1)TH GRID POINT CALCULATED
C AT OLD PRESSURE (LBM/ CU FT)
C RWXB WETTING PHASE DENSITY AT (I+1)TH GRID POINT CALCULATED
C AT NEW PRESSURE (LBM/ CU FT)
C RWXF WETTING PHASE DENSITY AT (I+1)TH GRID POINT CALCULATED
C AT NEW PRESSURE (LBM/ CU FT)
C S(N) WETTING PHASE SATURATION (CU FT WETTING PHASE/
C CU FT PORE SPACE)
C SCALE SAT. MULTIPLIER
C SGK(N) NON-WETTING PHASE NORMALIZATION FACTOR
C SOILPC AVERAGE SOIL POTENTIAL IN ROOT ZONE (PSI)
C SOILRE SOIL FLOW RESISTANCE IN VAPOR ZONE
C SRESG SQUARE OF NON-WETTING PHASE RESIDUAL
C SRESW SQUARE OF WETTING PHASE RESIDUAL
C STEM(NN) SOIL TEMP. DEGREE F.
C STAR TAPE USAGE INDICATOR
C STRP(NN) VAPOR PRESSURE VS. TEMP.
C SWK WETTING PHASE NORMALIZATION FACTOR
C TCCN MAX. SIMULATION TIME (HOURS)
C TH(N) THICKNESS (FOOT)
C TIMEA, TIMEB PROCESSOR TIME CONTROL
C TIMEPU TIME STEP SIZE MULTIPLIER
C TOLG CONVERGENCE CRITERIA FOR GRESG
C TCLW CONVERGENCE CRITERIA FOR GRESW
C TTOT CURRENT SIMULATION TIME (HOURS)
C TIRE TOTAL RESISTANCE
C VG(I) NON-WETTING PHASE VISCOSITY (CP)
C VW(I) WETTING PHASE VISCOSITY (CP)
C WSUM AMOUNT OF WETTING PHASE IN MODEL (LBM)
C WILPC WILTING SAT. (CF/CF PORE)
C WINDV WIND VELOCITY (MPH)
C WHEAD(N) PRECIPITATION IN./MO. OR WATER HEAD (PSI)
C X(N) SPACE COORDINATE (FOOT)
C MAINLINE
C
C CCMCN PG(50),PW(50),PGA(50),PWA(50),S(50),AS(10,100),BS(10,100)
C CCMCN C(12,50),DMWX(50),DMGX(50),QEVA(50)
C CCMCN SGK(50),SWK(50),FK(50),D,DD,DT,AAAA,BBBB,CCCC,DDDD,EEEE,FFF
C 1F,GGGG,HHHH,ASSS,BSSS
C CCMCN SUMMM,SUMNN,DENAM1,ANUMER
C CCMCN RKWC,RKWP,RKWF,RKGC,RKGB,RKGF,RW,RWF,RG,RGF,AVW,AVWF,AVG
C CCMCN RWA,RWXF,PTC,RGA,RGXF,RGXB,RWXB,AVGF
C CCMCN CW(50),QG(50),PWIN(50),PGIN(50),QTRAN(50)
C CCMCN WHEAD(998),RTDEN(50),PKEY(50),LAY(50)
C CCMCN RHUM(999),ATEM(999),STEM(999),STARP(100),WINDV(999)

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CCMMCN VW(100),PC(10,100),DW(100),DG(100),RKW(100),RKG(100),VG(100
 1),POR(50),PWB(50),X(50),KX(50),PGB(50),TH(50),H(50)
 CCMMCN FCCNV,CSW(10),CISW(10),DPW,DIPW,DPG,DIPG,DP,DIP,DPC,PCI,NX,
 IDISKW,DSKG,DISKG,NHK,LAYER,NPCC,DSKW,DHEAD,DIHEAD
 CCMMCN MTRY,KC,NBUG,NTRY,MAXW,MAXG,SRESG,SRESW,GRESW,GRESG,RSWA,RS
 1GA,HOFLEA,AKGLEA,DIWIND,AIRKG,WILPO,PLCOND
 CCMMCN RESTAR,STAR,FINAL,TCLW,TOLG,TCCN,PMCHW,PMCHG,EKGM
 CCMMCN TTCT,ITAPE,DLTMAX,ESTAR,NSTAR,IOUPTY,IT,TIMA,TIMB,TIMC
 CCMMCN CATEM,DIATEM,CSTEM,CISTEM,DSTP,DISTP,DRHUM,DIRHUM,CWIND
 CCMMCN PGCBV,SATURA,TIMEMU,QQEVA,QQQEVA,AVSATU,QTRANT,QQQTRA
 CCMMCN PDFLAW,JCUTPT,CTA,CTB,QTG,QDD,IQT,IQD
 DOUBLE PRECISION ATEMP,RHL,STEMP,PSTAR,ASTAR,WINDVC,QTRAN
 DOUBLE PRECISION QEVA,TTRE,SOILRE,AIRRE
 DOUBLE PRECISION PG,PGA,PH,PWA,S,AS,BS,ASSS,BSSS
 DOUBLE PRECISION C,DMWX,DMGX,SWK,SGK,HK
 DOUBLE PRECISION RKWC,RKWB,RKWF,RWXB,RGXB,RKGC,RKGB,RKGF,RWXF,RGXB
 L,RW,AVGF,RWF,RG,RGA,RGF,AVH,RWA,AVWF,AVG,PTC,RGXF
 DOUBLE PRECISION TPT,DT,Q3,Q5,Q9,Q11,AG,RESW,RESG,ACW,GSUM,WSUM
 DOUBLE PRECISION D,CC,AAAA,BBBB,CCCC,DDDD,EEEE,FFFF,GGGG,HHHH,AW
 DOUBLE PRECISION SATW,QWF,TTOT,PWIN,PGIN,ACG,QW,QG
 DOUBLE PRECISION SUMMM,SUMNN,DENAMI,ANUMER
 REAL *XX

C LNKA IS DATA INPUT LINK
 CALL LNKA
 C LNKB IS MAIN CALCULATIONAL LINK
 CALL LNKB
 STOP
 END

S IN EFFECT* NCID,EBCDIC,SOURCE,NOLIST,NODECK,LOAD,NOMAP
 S IN EFFECT* NAME = MAIN , LINECNT = 60
 TICS* SOURCE STATEMENTS = 31,PROGRAM SIZE = 322
 TICS* NC DIAGNOSTICS GENERATED

V G LEVEL 21 LNKA DATE = 74186 17/44/00

SUBRCLTINE LNKA

C THIS SUBROUTINE IS A DATA INPUT SUBROUTINE
 COMMON PG(50),Ph(50),PGA(50),PMA(50),S(50),AS(10,100),BS(10,100)
 COMMON C(12,50),DMWX(50),DMGX(50),QEVA(50)
 COMMON SGK(50),SWK(50),HK(50),D,DD,DT,AAAA,BBBB,CCCC,DDDD,EEEE,FFF
 1F,GGGG,HHHH,ASSS,BSSS
 COMMON SUMM,SUMN,DENAMI,ANUMER
 COMMON RKWC,RKWB,RKWF,RKGC,RKGB,RKGF,RW,RWF,RG,RGF,AVW,AVWF,AVG
 COMMON RWA,RWRF,PTC,REA,REXF,RGXB,RWXB,AVGF
 COMMON QW(50),CG(50),PWIN(50),PGIN(50),QTRAN(50)
 COMMON WHEAD(558),RTDEN(50),PKEY(50),LAY(50)
 COMMON RHUM(999),ATEM(999),STEM(999),STARP(100),WINDV(999)
 COMMON VW(100),PC(10,100),CH(100),CG(100),RKW(100),RKG(100),VG(100
 1),POR(50),PWB(50),X(50),KX(50),PGB(50),TH(50),H(50)
 COMMON FCCNV,CSW(10),DISW(10),DPW,DIPW,DPG,DIPG,DP,DPC,PCI,NX,
 1DISKW,DSKG,DISKG,AHK,LAYER,NPCC,DSKW,DHEAD,DIHEAD
 COMMON MTRY,KC,NBUG,NTRY,MAXW,MAXG,SRESG,SRESW,GRESW,GRESG,RSWA,RS
 1GA,HCFLEA,AKGLEA,DIWIND,AIRKG,WILPO,PLCOND
 COMMON RESTAR,STAR,FINAL,TCLW,TOLG,TCGN,PMCHW,PMCHG,EKGM
 COMMON TTOT,ITAPE,DLTMAX,ESTAR,NSTAR,IOUTPT,IT,TIMA,TIMB,TIMC
 COMMON CATEM,CIATEM,DSTEM,CISTEM,OSTP,DISTP,DRHUM,DIRHUM,DWIND
 COMMON PGBV,SATURA,TIMEMU,QQEVA,QQEVA,AVSATU,QTRAN,QQQTRA
 COMMON POFLAW,IOUTPT,CTA,QTB,QTC,QDD,IQT,IQD
 DIMENSION PCDUM(100), Ph(100)
 DOUBLE PRECISION ATEMP,RHL,STEMP,PSTAR,ASTAR,WINDVO,BW,QTRAN
 DOUBLE PRECISION QEVA,TTRE,SUILRE,AIRRE
 DOUBLE PRECISION PG,PGA,Ph,PWA,S,AS,BS,ASSS,BSSS
 DOUBLE PRECISION PWTE,PGTE,PWI,PGI
 DOUBLE PRECISION C,DMWX,CMGX,SWK,SGK,HK
 DOUBLE PRECISION RKWC,RKWB,RKWF,RWXB,RGXB,RKGC,RKGB,RKGF,RWRF,RGXB
 1,RW,AVGF,RWF,RG,RGA,RGF,AVW,RWA,AVWF,AVG,PTC,RGXF
 DOUBLE PRECISION TPT,DT,Q3,Q5,Q9,Q11,AG,RESW,RESG,ACW,GSUM,WSUM
 DOUBLE PRECISION D,DD,AAAA,BBBB,CCCC,DDDD,EEEE,FFFF,GGGG,HHHH,AW
 DOUBLE PRECISION SATW,QWF,TTOT,PWIN,PGIN,ACG,QW,QG
 DOUBLE PRECISION SUMM,SUMN,DENAMI,ANUMER
 REAL KX

C
 C START
 C
 C NSTAR=2
 C FCCNV=1.0/144.0
 C
 C IOUTPT CNTRLCLS OUTPUT OF RESULTS, PW(N), PG(N), S(N) - OUTPUT
 C WILL BE WRITTEN AFTER FIRST TIME STEP AND SUBSEQUENTLY AFTER
 C EACH IOUTPT TIME STEPS
 C
 C READ (5,320) RESTAR,FINAL,ESTAR,AKXMU,AIRKG,WILPO,POFLAW
 C
 C RESTAR = 0, START FROM INITIAL TIME, RESTAR NEO, START FROM TAPE
 C
 C WRITE (6,490) RESTAR,FINAL,POFLAW
 C WRITE (6,220)
 C
 C ESTAR = NUMBER OF TIME STEPS TO BE CALCULATED
 C
 C WRITE (6,500) AKXMU,ESTAR,AIRKG,WILPO
 C
 C NBUG IS A WRITE CONTROL: = -2 WRITE AFTER EACH TIME STEP

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C                      = 0 WRITE AFTER EACH ITERATION
C                      = 0 WRITE MATRIX SOLN AND PROPERTIES
C      ITAPE IS RESTART TAPE CONTROL: ITAPE =0,NO RESTART; ITAPE =1,RESTA
C      ART
C
C      REAC (5,290) NBUG,IT,INSh,ITAPE,IOUTPT,IQT,IQD
C      WRITE (6,550) NBUG,IT,INSh,ITAPE,IOUTPT,IQT,IQD
C
C      INITIAL SAT. WILL BE MODIFIED IF INSW = 1: THE WATER PRESSURE WILL
C      BE SET IN ACCORD. WITH GRAVITY HEAD, WHICH SETS PC AND THUS SW.
C      IF INSW = 0 THEN INITIAL SATURATION WILL BE AS FOLLOWS (SEE
C      ROUTINE THAT FLLCHS)
C
C      REAC (5,510) DLTMAX,PLCCND,HOFLEA,AKGLEA,ASSS,BSSS,PGCBV,TIMEMU
C      WRITE (6,540) DLTMAX,PLCCND,HOFLEA,AKGLEA,ASSS,BSSS,PGCBV,TIMEMU
C      ITSTCP=IT
C
C      THE VALUE OF RESTAR IS SAVED FOR TAPE USAGE
C
C      STAR=RESTAR
C      IF (RESTAR.GT.C.0001) GO TO 190
C
C      REAC VISCOSITY TABLES
C      AN = NC. OF PTS. IN TABLE, DP = PRESS. INCR., DIPW = INIT. TABLE
C      VW (N) = WATER VISCOSITY
C      VG (N) = GAS VISCOSITY
C
C      REAC (5,300) AN,DP,DIP
C      WRITE (6,310) AN,DP,DIP
C      N=AN
C      REAC (5,320) (VW(NN),NN=1,N)
C      REAC (5,320) (VG(NN),NN=1,N)
C      DO 10 M=N,100
C      VW(M)=VW(N)
10  VG(M)=VG(N)
C      WRITE (6,360)
C      WRITE (6,310) (VW(NN),NN=1,100)
C      WRITE (6,370)
C      WRITE (6,310) (VG(NN),NN=1,100)
C
C      REAC DENSITY TABLES
C      CW (N) = WATER DENSITY
C      DG (N) = GAS DENSITY
C
C      REAC (5,300) AN,CPW,DIPW
C      N=AN
C      REAC (5,320) (DW(NN),NN=1,N)
C      DO 20 M=N,100
C      CW(M)=CW(N)
20  DW(M)=DW(N)
C      WRITE (6,350)
C      WRITE (6,310) AN,CPW,DIPW
C      WRITE (6,310) (DW(NN),NN=1,100)
C      REAC (5,300) AN,DPG,DIPG
C      N=AN
C      REAC (5,510) (DG(NN),NN=1,N)

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DO 30 N=N,100
30  DG(M)=CG(N)
    WRITE (6,340)
    WRITE (6,310) AN,DPG,DIPG
    WRITE (6,310) (DG(NN),NN=1,100)
C
C   REAC CAPILLIARY PRESS. DATA - READ SW AT EQUAL INCR. OF CAP. PRESS
C   AN = NC. OF PTS. IN TABLE
C   PCI = INIT. CAP. PRESS. IN TABLE
C   DPC = INCREMENT IN CAP. PRESS.
C   SCALE = SCALE FACTOR - PURPOSE IS TO EASILY SHIFT CAP. PRESS. CUR
C   BW(N) = SW (WATER SATURATION)
C
C   NCLAY = NUMBER OF LAYERS WITH DIFFERENT CAPILLARY PRESS. CURVES
C
    REAC (5,290) NCLAY
    DO 40 I=1,NCLAY
    REAC (5,300) AN,PCI,DPC,SCALE
    N=AN
    NPCC=N
    WRITE (6,310) AN,PCI,DPC,SCALE
    LAYER=I
    REAC (5,510) (BW(NN),NN=1,N)
C
C   CAPILLIARY PRESS. DATA CONVERTED TO EQUAL INCREMENTS OF SATURATION
C   BS(J) AND AS (J) CALCULATED FOR EACH TABLE ENTRY
C   SW = AS(J) + BS(J) * PC
    CALL CAPPR (AN,PCI,DPC,SCALE,LAYER,BW,AS,BS,DSW,DISW,PC)
    WRITE (6,330)
    WRITE (6,310) AN,DSW(LAYER),DISW(LAYER)
    WRITE (6,310) (PC(LAYER,J),J=1,N)
40  CCNTINE
C
C   READ IN GRID DATA
C   PERP., POR(POR CENT), INIT. GAS PRESS., INIT. SAT., THICKNESS
C   X LOCATION, WATER INJECTION RATE, AIR INJECTION RATE, WELL WATER
C   PRESS., WELL GAS PRESS., BOUNCARY CONDITION CONTROL
C   KX(N)=CARCIES
C   WATER AND AIR INJECTION RATES AND BOUNDARY PRESSURES NEED ONLY BE
C   SPECIFIED IN ACCORDANCE WITH PKEY(N)
C
C
    REAC (5,290) NX
    WRITE (6,230) NX
    WRITE (6,240)
    LAYDUM=1
50  DO 50 II=1,100
    PCDUM(II)=PC(1,II)
    DO 100 N=1,NX
    READ (5,520) KX(N),LAY(N),POR(N),PG(N),S(N),TH(N),H(N),X(N),QW(N),
    1QG(N),PWIN(N),RTDEN(N),PGIN(N),PKEY(N)
    C   POR(N)=POR(N)*0.01
    C   S(N)=S(N)/POR(N)
    LAYER=LAY(N)
    KX(N)=KX(N)*AKXPMU
    IF (LAYDUM.EQ.LAYER) GC TC 70
    DO 60 II=1,100
60  PCDUM(II)=PC(LAYER,II)

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LAYER=LAYER
C PCDUM IS A DUMMY CAP. PRESS. ARRAY FOR USE IN SUBROUTINE TAB
70 CALL TAB (DSW(LAYER),DISW(LAYER),PCDUM,S(N),PTC)
PW(N)=PG(N)-PTC
H(N)=F(N)*FCCNV
IF (INSH.NE.1) GO TO 90
PWI=Ph(N)
PGI=PG(N)
80 PhTE=Ph(N)
PGTE=PG(N)
CALL TAB (CPG,CIPG,CG,PGTE,RG)
CALL TAB (CPW,CIPW,DW,PhTE,RW)
PW(N)=PWI-H(N)*RW
PG(N)=PGI-H(N)*RG
ABPW=CABS(PW(N))
ABPG=CABS(PG(N))
IF (ABPW.LT.0.1) ABPW=0.1
IF (ABPG.LT.0.1) ABPG=0.1
IF (CABS(PhTE-PW(N))/ABPW.GT.0.2D-14) GO TO 80
IF (CABS(PGTE-PG(N))/ABPG.GT.0.2D-14) GO TO 80
NKK=(PG(N)-PW(N)-PCI)/DPC+1.0
IF (NKK.GT.NPCC) NKK=NPCC
IF (NKK.LT.1) NKK=1
IF ((AS(LAYER,NKK)+BS(LAYER,NKK)*(PG(N)-PW(N))).LT.WILPO) LAYER=10
AS(10,NKK)=ASSS
BS(10,NKK)=BSSS
S(N)=AS(LAYER,NKK)+BS(LAYER,NKK)*(PG(N)-PW(N))
90 HWRT=F(N)/FCCNV
WRITE (6,530) KX(N),LAY(N),POR(N),PW(N),PG(N),S(N),TH(N),HWRT,X(N)
1,QW(N),QG(N),PWIN(N),PGIN(N),PKEY(N),RTDEN(N)
C
C 0.2637 IS CONVERGENCE FACTOR FOR CARCY TO CP.FT**2 PSI/HR
C
KX(N)=KX(N)*.2637
PWA(N)=PW(N)
PGA(N)=PG(N)
100 CONTINUE
C
C READ RELATIVE PERM. DATA
C DSKG = INCREMENT IN SAT.
C DISKW = FIRST SAT. IN TABLE
C
REAC (5,300) AN,DSKW,DISKW
N=AN
REAC (5,510) (RKW(NN),NN=1,N)
DO 110 M=N,100
110 RKW(M)=RKW(N)
WRITE (6,380)
WRITE (6,310) (RKW(NN),NN=1,100)
WRITE (6,310) AN,DSKW,DISKW
REAC (5,300) AN,DSKG,DISKG
N=AN
REAC (5,510) (RKG(NN),NN=1,N)
DO 120 M=N,100
120 RKG(M)=RKG(N)
WRITE (6,390)
WRITE (6,310) AN,DSKG,DISKG
WRITE (6,310) (RKG(NN),NN=1,100)

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C READ AIR TEMP. VS. TIME , (F.)

C READ (5,300) AN,DATEM,DIATEM
N=AN
READ (5,510) (ATEM(NN),NN=1,N)
CO 130 M=N,100

130 ATEM(M)=ATEM(N)

C READ SOIL TEMP. VS. TIME , (F.)

C READ (5,300) AN,DSTEM,DISTEM
N=AN
READ (5,510) (STEM(NN),NN=1,N)
CO 140 M=N,100

140 STEM(M)=STEM(N)

C READ AIR HUMIDITY VS. TIME

C READ (5,300) AN,DRHUM,DIRHUM
N=AN
READ (5,510) (RHUM(NN),NN=1,N)
CO 150 M=N,100

150 RHUM(M)=RHUM(N)

C READ WIND VELOCITY VS. TIME (MPH)

C READ (5,300) AN,DWIND,DIWIND
N=AN
READ (5,510) (WINDV(NN),NN=1,N)
CO 160 M=N,100

160 WINDV(M)=WINDV(N)

WRITE (6,420)
WRITE (6,310) AN,CATEM,DIATEM
WRITE (6,310) (ATEM(NN),NN=1,N)
WRITE (6,430)
WRITE (6,310) AN,DSTEM,DISTEM
WRITE (6,310) (STEM(NN),NN=1,N)
WRITE (6,410)
WRITE (6,310) AN,DRHUM,DIRHUM
WRITE (6,310) (RHUM(NN),NN=1,N)
WRITE (6,440)
WRITE (6,310) AN,DWIND,DIWIND
WRITE (6,310) (WINDV(NN),NN=1,N)

C READ VAPOR PRESSURE VS. TEMP

C READ (5,300) AN,DSTP,DISTP
N=AN
READ (5,510) (STARP(NN),NN=1,N)
WRITE (6,450)

170 STARP(M)=STARP(N)

WRITE (6,310) AN,DSTP,DISTP
CO 170 M=N,100
WRITE (6,310) (STARP(NN),NN=1,100)
WRITE (6,400)

C READ SCHEDULE OF WATER HEAD AT BOUNCARY - FOR VARIABLE HEAD BOUND.

C CHEAD = TIME INCREMENT FOR TABLE

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C   DIHEAD = INITIAL TIME CORRESPONDING TO FIRST TABLE VALUE
    REAC (5,300) AN,DIHEAD,CIHEAD
    N=AN
    READ (5,510) (WHEAD(NN),NN=1,N)
180  CO 180 M=N,100
    WHEAD(M)=WHEAD(N)
    WRITE (6,310) AN,DIHEAD,CIHEAD
    WRITE (6,310) (WHEAD(NN),NN=1,N)
C   MTRY = MAX. NO. OF ITERATIONS PER TIME STEP
    REAC (5,290) MTRY
    CMIA=MTRY
C   TSTEP = NO. OF ITERATION PARAMETERS
C
    REAC (5,320) TSTEP
    WRITE (6,460)
    WRITE (6,310) DMIN,TSTEP
    NHK=TSTEP
C
C   HK = ITERATION PARAMETERS - WILL BE USED IN CYCLICAL MANNER
    READ (5,320) (HK(I),I=1,NHK)
    WRITE (6,250)
    WRITE (6,310) (HK(I),I=1,NHK)
C   CONVERGENCE CRITERIA
C   TOLG IS MAX. GAS PHASE RESIDUAL ALLOWED, TOLW IS MAX. WATER RESID.
C   PMCHG IS MAX. CHANGE IN GAS PRESS. ALLOWED AT ANY GRID POINT
C   PMCHW IS MAX. CHANGE IN WATER PRESS. ALLOWED AT ANY GRID POINT
C
    REAC (5,320) TCLW,TCLG,PMCHW,PMCHG
    WRITE (6,260)
    WRITE (6,480) TCLW,TCLG,PMCHW,PMCHG
    WRITE (6,270)
    TTOT=C.0
    GO TO 210
C
C   RESTART FROM TAPE
C
190  REWIND 2
    NSTAR=0
200  READ (2) TOLW,TOLG,AAAA,BBBB,CCCC,DDDD,EEEE,FFFF,GGGG,HHHH,MTRY,NH
    LK,PMCHW,PMCHG,TTCT,NX,D,DC,NPCC,SATURA,QQEVA,AVSATU,QTRANT,QQQTRA
    READ (2) DSW,DISW,PC,DPC,PCI,AS,BS,ASSS,BSSS
    REAC (2) DP,DIP,VW,VG
    READ (2) CPW,DIPW,DW,DPG,CIPG,CG
    READ (2) DIHEAD,DIHEAD,WHEAD,DSKW,DISKW,RKW,DSKG,DISKG,RKG
    REAC (2) LAY,RTDEN,PKEY,QW,QG,PWIN,PGIN
    REAC (2) CATEM,DIATEM,DSTEM,CISTEM,OSTP,DISTP,DRHUM,DIRHUM,DWIND
    REAC (2) RFUM,ATEM,STEM,STARP,WINDV,DIWIND
    REAC (2) (KX(I),POR(I),PG(I),PW(I),PGA(I),PGB(I),PWA(I),PWB(I),X(I
1) ,S(I),TH(I),H(I),DMGX(I),DMWX(I),SGK(I),SWK(I),I=1,NX)
    REAC (2) NTRY,MAXW,MAXG,SRESW,SRESG,GRESW,GRESG,EKWM,EKGM,RSWA,RSW
1A,KC,FK(KC),HK,INL,PKEY(INL),CEVA,QQEVA,JOUTPT,SUMMM,SUMNN
    REAC (2) RESTAR,FINAL,DT,TCON,PCTOFR,POTOFI,Q1111,Q2222,TIMA,TIMB,
1TIMC
    WRITE(6,491) RESTAR,FINAL,CT,TTOT
    AANTRY = NTRY
    IF (RESTAR+0.0001.GE.STAR) GO TO 210
    GO TO 200
210  READ (5,470) DT,TCON,TIMA,TIMB,TIMC,QTA,QTB,QTC,QDD

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WRITE (6,280) DT,TCCN,TIMA,TIMB,TIMC,QTA,QTB,QTC,QDD
ESTAR=RESTAR+ESTAR
RETURN

C

- 220 FCRMAT (1HC,47HAKXMU IS PERM MULTIPLIER FOR EASY PERM CHANGE)
230 FCRMAT (1HC,26HNUMBER CF GRID POINTS,NX =,I5)
240 FCRMAT (1HC,3X,4HK(X),4X,5H LAY ,1X,5H POR ,8HWAT. PR.,8HGAS. PR.,
11H WAT. SAT. ,5H TH ,6H DEPTH,4X,5H XLOC,2X,5H QW ,2X,5H QG ,2
2X,5H PWIN,5X,4HPGIN,4X,5H PKEY,2X,5HR.DEN,/,126H DARC NO.
3PRC. PSI CFT/CFT P. FT FT FT LBM/OY**2-HR
4 PSI NO. FT/CFT)
250 FCRMAT (1HC,25HITERATICN PARAMETERS - HK)
260 FCRMAT (1HC,20HCCNVERGENCE CRITERIA/,4X,4HTOLW,4X,4HTOLG,4X,5HPMCH
1W,3X,5HPMCHG)
270 FCRMAT (1H ,26HTCLW = MAX WAT PHASE RESID,3X,27HTOLG IS MAX GAS PH
1ASE RESID/1X,37HPMCHW = MAX CHANGE IN WAT PHASE PRESS,3X,45HPMCHG
2= MAX CHANGE IN GAS PHASE PRESS ALLOWED)
280 FCRMAT (1HC,16HDELTA TIME(DT) =,F8.4,3X,11HMAX TIME = ,F8.2,3X,7H
1TIMA = ,F8.2,3X,7HTIMB = ,F8.2,3X,7HTIMC = ,F8.2/5X,81HTIMA SETS T
IIME LIMIT FOR DT TO BE DLTMAX, TIMB SET TIME LIMIT FOR DO TO BE TI
1MC. /47HSEASONAL TRANSPIRATION FUNCTION CONSTANTS, QTA=,F8.4,3X,4
1HQTB=,F8.4,3X,4HQTC=,F8.4, /32HDRAINAGE FUNCTION CONSTANT, QDD=,F8
1.4)
290 FCRMAT (8I10)
300 FCRMAT (10F8.4)
310 FCRMAT(1H ,10F12.6)
320 FCRMAT (8F10.3)
330 FCRMAT (1H1,26H CAPILLARY PRESSURE, (PSI))
340 FCRMAT (1HC,27H GAS DENSITY, (LBM/CU. FT.))
350 FCRMAT (1HC,29H WATER DENSITY, (LBM./CU.FT.))
360 FCRMAT (30H0WATER VISCOSITY, (CENTIPOISE))
37C FCRMAT (28H0GAS VISCOSITY, (CENTIPOISE))
380 FCRMAT (28HCRELATIVE PERMEABILITY WATER)
390 FCRMAT (26HCRELATIVE PERMEABILITY GAS)
400 FCRMAT (40HOPRECIPITACIN, (INCH/DATA PT. INTERVAL))
410 FCRMAT (29HORELATIVE HUMICITY, (PERCENT))
420 FCRMAT (24HCAIR TEMP., (FAHRENHEIT))
430 FCRMAT (25HOSCIL TEMP., (FAHRENHEIT))
440 FCRMAT (32H0WIND VELCCITY, (MILES PER HOUR))
450 FCRMAT (38H0SATURATED WATER VAPOR PRESSURE, (PSI))
460 FCRMAT (7X,19H-MTRY TSTEP)
470 FCRMAT (9F8.4)
480 FCRMAT (1H ,5F8.4,2I8,2F20.4)
490 FCRMAT (1HC,6HRESTART=,F10.1,3X,6HFINAL=,F10.5,3X,7HPOFLAW=,F10.5
1)
491 FCRMAT (1HC,8HRESTART=,F8.1,3X,6HFINAL=,F8.1,3X,4HDT =,F8.5,3X,7HTT
1OT = ,F10.2)
500 FCRMAT (8H AKXMU=,F10.5,10H ESTAR=,F10.1,7HAIRKG =,F10.4,5HWIL
1P=,F10.4)
510 FCRMAT (8F10.6)
520 FCRMAT (F5.0,I5,F5.0,F10.0,10F5.0)
530 FCRMAT (1H ,F8.3,I5,13F8.3)
540 FCRMAT (1H ,11H MAX DEL T=,F6.2,2X,19HPLANT CCNDUCTIVITY=,F7.5,2X,
137HHEIGHT OF LEAVES FRCM A CATUM PLANE=,F6.2,2X,20HAIR-LEAF EVAP.C
2OEF.=,F7.5, /11H INTERCEPT=,F8.5,2X,6HSLOPE=,F8.5,2X,35HPERCENT GRO
3UND COVER BY VEGETACIN=,F6.2,2X,12HDEL T MULT.=,F5.2)
550 FCRMAT (1HC,20HWRITE CCNTRGL(NBUG)=,I5,3X,4HIT =,I5,3X,6HINSW =,I5
1,7HITAPE =,I5,3X,7HICLPT= ,I5,3X,4HIQT=,I8,3X,4HIQD=,I8)

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580  FORMAT(1H0,120H-RESTAR IT DELT    TIME    ROOT PCT.  LEAF POT.
1  SUPPLY F.    POT. EVAP  EVAPORATION TRANSPIRATION CUM.EVAP. CUM.TR
2AN./112H  NG.   NO.   CAY    DAY          PSI
3          LBM/DY-SQ.FT.                    LBM/)
600  FORMAT (1H ,F4.0,1X,F3.0,F7.4,F10.2,8(2X,E10.4))
      END

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NS IN EFFECT*  NCIC,EBCCIC,SCURCE,NCLIST,NODECK,LOAD,NOMAP
NS IN EFFECT*  NAME = LNKA      , LINECNT =      60
STICS*  SOURCE STATEMENTS =      267,PROGRAM SIZE = 13524
STICS*  NC DIAGNOSTICS GENERATED

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SUBROUTINE LNKB

CCMMCN PG(50),PW(50),PGA(50),PWA(50),S(50),AS(10,100),BS(10,100)
 COMMON C(12,50),CMWX(50),CMGX(50),QEVA(50)
 CCMMCN SGK(50),SWK(50),HK(50),D,DD,DT,AAAA,BBBB,CCCC,DDDD,EEEE,FFF

1F,GGGG,HHHH,ASSS,BSSS

CCMMCN SUMPM,SUMNN,DENAMI,ANUMER

COMMON RKWC,RKWB,RKWF,RKGC,RKGB,RKGF,RW,RWF,RG,RGF,AVW,AVWF,AVG

CCMMCN RWA,RWXF,FTC,REA,RGXF,RGXB,RWXB,AVGF

CCMMCN QH(50),QG(50),PHIN(50),PGIN(50),QTRAN(50)

CCMMCN WHEAD(558),RTDEN(50),PKEY(50),LAY(50)

CCMMCN RHUM(999),ATEM(999),STEM(999),STARP(100),WINDV(999)

COMMON VW(100),PC(10,100),DW(100),DG(100),RKW(100),RKG(100),VG(100)
 1),POR(50),PWB(50),X(50),KX(50),PGB(50),TH(50),H(50)

CCMMCN FCCNV,CSW(10),DISW(10),DPW,DIPW,DPG,DIPG,DP,DPC,PCI,NX,
 1DISKW,DSKG,DISKG,NHK,LAYER,NPCC,DSKW,DHEAD,OIHEAD

COMMON MTRY,KC,NBUG,NTRY,MAXW,MAXG,SRESG,SRESW,GRESW,GRESG,RSWA,RS

1GA,HCFLEA,AKGLEA,DIWINC,AIRKG,WILPO,PLCOND

COMMON RESTAR,STAR,FINAL,TCLW,TOLG,TCCN,PMCHW,PMCHG,EKGM

CCMMCN TTOT,ITAPE,DLTMAX,ESTAR,NSTAR,IOUTPT,IT,TIMA,TIMB,TIMC

COMMON DATEM,CIATEM,OSTEM,DISTEM,OSTP,DISTP,DRHUM,DIRHUM,CWIND

CCMMCN PGCBV,SATURA,TIMEMU,QQEVA,QQQEVA,AVSATU,QTRANT,QQQTRA

CCMMCN POFLAW,JCUTPT,CTA,CTE,QTC,QCD,IQT,IQD

DIMENSION QCTR(50)

DOUBLE PRECISION ATEMP,RHU,STEM,PSTAR,ASTAR,WINDVD,QTRAN

DOUBLE PRECISION QEVA,TTRE,SOILRE,AIRRE

DOUBLE PRECISION PG,PGA,PW,PWA,S,AS,BS,ASSS,BSSS

DOUBLE PRECISION C,CMWX,CMGX,SWK,SGK,HK

DOUBLE PRECISION RKWC,RKWB,RKWF,RWXB,RGXB,RKGC,RKGB,RKGF,RWXF,RGXB

1,RW,AVGF,RWF,RG,REA,RGF,AVW,RWA,AVWF,AVG,PTC,RGXF

DOUBLE PRECISION TPT,DT,Q3,Q5,Q9,Q11,AG,RESW,RESG,ACH,GSUM,WSUM

DOUBLE PRECISION D,DC,AAAA,BBBB,CCCC,DDDD,EEEE,FFFF,GGGG,HHHH,AM

DOUBLE PRECISION SATW,QCTR,QWF,TTOT,PWIN,PGIN,ACG,QW,QG

DOUBLE PRECISION SUMPM,SUMNN,DENAMI,ANUMER,QC21,QC22,QC20,QC23

DOUBLE PRECISION ACUMO,ACUM1,ACUM2,PPWA,DABIRI

REAL KX

FINAL=0.0

KC = 1

ITIM1 = 480

ITIM2 = 480

ITIM3 = 480

WRITE (6,680)

C

FOR TAPE RESTART, NSTAR = 0

C

IF (NSTAR.LT.1) GO TO 130

IF (ITAPE.EQ.0) GO TO 10

10

REWIND 2

QQQEVA=0.

QTRANT=0.

QQQTRA=0.

Q2222=0.

Q1111=0.

QQEVA=0.

NTRY=0

PCTOFL=0.

PCTOFR=0.

AAAA=0.

BBBB=0.

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CCCC=0.
DDDC=0.
ACW=0.
ACG=0.
DO 15 K=1,NX
15 QEVA(K) = 0.0
QTRAN(K) = 0.0
INL=1
20 JOUTPT=ICUTPT-1
CONTINUE
IF (QTRANT.EC.0.) GO TO 30
POTCFR=SRESUL-ANDDEN
POTCFL=POTCFR-CTRANT/(FLCCND*PGCBV*.01)
30 CONTINUE
RESG=0.0
RESW=C.0
NXX=NX+100
GSUM=0.0
WSUM=0.0
SATURA=0.
SOILFC=0.
ROOTN=0.
XC=0.C
XF=0.0
C DETERMINATION OF MATERIAL BALANCE, INITIAL WATER PRESSURE, AIR
C PRESSURE AND INITIAL SATURATION
C
DO 40 N=1,NX
PWB(N)=0.
LAYER=LAY(N)
PG(N)=PGA(N)
PW(N)=PWA(N)
NKK=(PG(N)-PW(N)-PCI)/CPC+1.0
IF (NKK.LT.1) NKK=1
IF (NKK.GT.NPCC) NKK=NPCC
IF ((AS(LAYER,NKK)+BS(LAYER,NKK)*(PG(N)-PW(N))).LT.WILPO) LAYER=10
AS(10,NKK)=ASSS
BS(10,NKK)=BSSS
S(N)=AS(LAYER,NKK)+BS(LAYER,NKK)*(PG(N)-PW(N))
CALL TAB (DPG,CIPG,DG,PG(N),RG)
CALL TAB (CPW,DIPW,CW,PW(N),RW)
XB=XC
XC=XF
XF=X(N+1)
IF (N.EQ.1) XB=0.0
IF (N.EQ.1) XC=0.0
IF (N.EC.NX) XF=XC
GSUM=(XF-XB)*C.5*TH(N)*(1.0-S(N))*POR(N)*RG+GSUM
WSUM=(XF-XB)*C.5*TH(N)*S(N)*POR(N)*RW+WSUM
IF (RTDEN(N).EC.0.) GO TO 40
ROOTN=ROCTN+1.
SATURA=SATURA+S(N)*POR(N)
SOILPC=SCILPC+PWA(N)+RW*P(N)
40 CONTINUE
C CALC. OF AVE. SAT. , AVE SCIL WATER POT. IN THE ROOT ZONE
C
IF (ROCTN.EQ.C.) GO TO 50
AVSATU=SATURA/ROCTN

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SOILPC=SCILPC/ROOTN
50  CQQTRA=CQQTRA+QTRANT*CT
    AANTRY=NTRY
C   *****
C   THIS IS ONE OF THE MAIN WRITING STATEMENTS
C   *****
WRITE (6,700) RESTAR,AANTRY,DT,TTOT,POTOFR,POTOFL,Q1111,Q2222,QQEV
1A,QTRANT,QQEVA,CQQTRA
C   SET TIME STEP
C
DT = CT*(1.+TIMEMU)
IF (DT.GE.DLTMAX) DT=DLTMAX
IF(TTCT.GE.TIMA) DT = DLTMAX
IF(TTCT.GE.TIMB) DT = TIMC
JOUTPT=JOUTPT+1
IF (NTRY.GE.(MTRY/3)) DT=CT/10.
RESG=GSUM
RESW=WSUM
CCCC=AAAA+CCCC
DDDD=BBBB+DDDD
AW=RESW-CCCC
AG=RESG-DDDD
IF (TTCT.EQ.0) EEEE=RESW
IF (TTOT.EQ.0.) FFFF=RESG
GGGG=AW/EEEE
HHHH=AG/FFFF
IF (TTCT.GE.TCON) GO TO 70
70  IF(CABS(CCCC).GT.0.0001) ACW=(EEEE-RESW)/CCCC
80  IF(DABS(DDDD).GT.0.0001) ACG=(FFFF-RESG)/DDDD
    NTRY=0
    IF (TTCT.EQ.0.) GO TO 100
C   CHECK CN PROCESSOR AND SIMULATION TIME
C
C   RTIME GIVES THE REMAINING TIME IN SECCNDS
C   IT IS THE MIN. TIME (SEC) FOR THE RUN TO WRITE ON TAPE AND EXIT
CALL RTIME(ITIMI)
IF(IABS(ITIMI).LE.IT) FINAL = 2.
GO TO 93
92  FINAL = 2.
93  CONTINUE
    IF (ESTAR.LE.RESTAR) FINAL=2.
    IF (TTOT.GE.TCCN) FINAL=2.
    IF (FINAL.EQ.2.) GO TO 100
C   CHECK OUTPUT CCNTFCL
IF (JOUTPT.EQ.ICUTPT) GO TO 100
IF(JOUTPT.EQ.2.000*ICUTPT) GO TO 100
IF(JOUTPT.EQ.3.000*ICUTPT) GO TO 100
IF(JOUTPT.EQ.4.000*ICUTPT) GO TO 100
IF(JOUTPT.EQ.5.000*ICUTPT) GO TO 100
IF (JOUTPT.GE.6.000*ICUTPT) GO TO 100
GO TO 120
100 WRITE (6,710)
C   *****
C   THIS IS ONE OF THE MAIN WRITING STATEMENTS
C   *****
WRITE (6,600) AAAA,RESW,CCCC,AW,EEEE,GGGG,ACW,BBBB,RESG,DDDD,AG,FF
1FF,HHHH,ACG

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```

WRITE (6,640)
DO 110 I=1,NX
PGB(I)=PQR(I)*S(I)
110 WRITE (6,650) X(I),PKEY(I),PWIN(I),PGIN(I),QEVA(I),QTRAN(I),QW(I),
1QG(I),PW(I),PG(I),S(I)
IF(RESTAR.EQ.C.) WRITE(6,680)
IF (ITAPE.EQ.0) GO TO 120
IF(RESTAR.EQ.0.) GC TC 120
IF(FINAL.EQ.2.) GO TO 111
IF(JOUTPT.LT.(6.0*ICUTPT)) GO TO 112
111 WRITE (2) TOLW,TCLG,AAAA,BBBB,CCCC,DDDD,EEEE,FFFF,GGGG,HHHH,MTRY,N
1HK,FMCHW,FMCHG,TTOT,NX,D,CD,NPCC,SATURA,QEVA,AVSATU,QTRAN,QQTRA
JOUTPT=0
WRITE (2) DSW,DISW,PC,DPC,PCI,AS,BS,ASSS,BSSS
WRITE (2) CP,CIP,VW,VG
WRITE (2) DPH,DIPW,DW,DPG,DIPG,CG
WRITE (2) DHEAD,DIHEAD,WHEAD,DSKW,DISKW,RKW,DSKG,DISKG,RKG
WRITE (2) LAY,RTDEN,PKEY,QW,QG,PWIN,PGIN
WRITE (2) DATEP,DIATEP,DSTEP,DISTEM,CSTP,DISTP,DRHUM,DIRHUM,CWIND
WRITE (2) RHUM,ATEP,STEM,STARP,WINDV,DIWIND
WRITE (2)(KX(I),PQR(I),PG(I),PW(I),PGA(I),PGB(I),PWA(I),PWB(I),X(I)
1),S(I),TH(I),H(I),DMGX(I),DMWX(I),SGK(I),SWK(I),I=1,NX)
WRITE (2) NTRY,MAXW,MAXG,SRESW,SRESG,GRESW,GRESG,EKWM,EKGM,RSWA,RS
1GA,KC,HK(KC),HK,IAL,PKEY(IAL),QEVA,QQEVA,JOUTPT,SUMMM,SUMNN
WRITE(2) RESTAR,FINAL,DT,TCN,PGTOFR,POTOFI,Q1111,Q2222,TIMA,TIMB,
ITIMC
112 CALL RTIME(ITIM3)
IF (NBUG.LT.(-4)) GO TO 114
WRITE (6,820)
WRITE (6,800) ITIM1,ITIM2,ITIM3
114 WRITE (6,680)
120 IF (FINAL.EQ.2.) CALL EXIT
130 TTOT=TTOT+DT
IF (TTOT.GT.TCCN) DT=TCCN-TTOT+DT
IF (TTOT.GT.TCCN) TTOT=TCCN
RESTAR=RESTAR+1.0
KC=0

```

C
C
C

EVAPORATION CALC.

```

INL=1
AIRRE=0.
SOILRE=0.
SUMSA=0.
SUMPOR=0.
APOR = 0.0
AVSAT = 0.0
ABAB = 0.0
EVALEN = 0.0
FXPCN = 0.0
PGCAP=PGA(1)
PWCAP=PWA(1)
DO 140 M=1,NX
140 QEVA(M)=0.
IRAIN=TTCT/DHEAD+1.
IATEP=TTCT/CATEP+1.
ISTEM=TTOT/DSTEM+1.
IWIND=TTCT/CWIND+1.

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IRHUM=TTCT/DRHUM+1.
ATEMP=ATEM(IATEM)
STEMP=STEM(ISTEM)
WINDVO=WINDV(IWIND)
RHU=RFUM(IRHUM)
IF ((TTOT-DT).LT.FLOAT(IWIND-1)*DWIND) CALL TAB (DWIND,DIWIND,WIND
1V,(TTCT-DT),WINDVO)
IF ((TTOT-DT).LT.FLCAT(IRHUM-1)*DRHUM) CALL TAB (DRHUM,DIRHUM,RHUM
1,(TTOT-DT),RHU)
IF ((TTOT-DT).LT.FLCAT(IATEM-1)*CATEM) CALL TAB (DATEM,DIATEM,ATEM
1,(TTCT-DT),ATEMP)
IF ((TTOT-DT).LT.FLCAT(ISTEM-1)*DSTEM) CALL TAB (DSTEM,DISTEM,STEM
1,(TTCT-DT),STEMP)
CALL TAB (DSTP,DISTP,STARF,STEMP,PSTAR)
CALL TAB (DSTP,DISTP,STARF,ATEMP,ASTAR)
DABIRI=STEMP
IF (PGCBV.EQ.100.) GO TO 160
IF (S(1).GE.WILPC) GO TO 160
CO 150 NI=1,NX
STEMP=STEM(ISTEM)
IF((TTCT-DT).LT.FLGAT(ISTEM-1)*CSTEM) CALL TAB (DSTEM,DISTEM,STEM
1,TTCT,STEMP)
IF (S(INL).LT.WILPC) STEMP=(STEMP+ATEMP)/2.
CALL TAB (DSTP,DISTP,STARF,STEMP,PSTAR)
FXPCN=DEXP(.0268857*(PGA(INL)-PWA(INL))/(460.+STEMP))
SRHU=PSTAR/FXPCN
IF (SRHU.LT.RHU*.01*ASTAR) INL=INL+1
EVALEN=X(INL)
IF (INL.EQ.1) EVALEN=X(2)/4.
PGCAP=PGA(INL)
PWCAP=PWA(INL)
IF (INL.LT.NI) GO TO 150
SUMPCR=SUMPOR+POR(NI)
SUMSA=SUMSA+S(NI)
APOR=SUMPCR/FLCAT(NI)
AWSAT=SUMSA/FLCAT(NI)
FNI = NI
FINL = INL
150 CCNTINUE
C
C SEE REPCRT, EGN. (2-12)
C
ABAB=18.*144.*.62*APOR*(1.-AWSAT)*.853*(((460.+STEMP)/492.)**1.5)
C
C AIR RESISTANCE
C
SOILRE=1545.*(460.+STEMP)*EVALEN/ABAB
160 ACAC=AIRKG*WINDVO**.8
AIRRE=1./ACAC
TTRE=AIRRE+SOILRE
EXOPN=DEXP(.0268857*(PGA(INL)-PWA(INL))/(460.+STEMP))
QEVA(INL)=((PSTAR/EXOPN-.01*RHU*ASTAR)/TTRE)*.01*(100.-PGCBV)
QQEVA=QEVA(INL)
QQQEVA=QQQEVA+QQEVA*DT
170 IF (NBUG.LT.(-2)) GO TO 180
WRITE (6,591) RHU,PSTAR,ASTAR,STEMP,APOR,AWSAT,ABAB,EVALEN,SOILRE,
1AIRRE,TTRE,WINDVO,QEVA(INL),PGCAP,PWCAP,ACAC,SRHU,PLCOND,EXOPN,FXP
2CN

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WRITE (6,596) NTRY,INL,JOUTPT,QTRANT,POTOFR,POTOFL,ATEMP,ROOTN
180 IF (NTRY.EQ.0) GO TC 220
    IF (NEUG.LT.(-3)) GO TO 190
C
C WRITE THE RESULTS OF ITERATION
C
WRITE (6,671)
WRITE (6,670) NTRY,MAXW,MAXG,GRESW,GRESG,EKWM,EKGM,HK(KC)
190 IF (NTRY.GE.MTRY) GO TO 200
    GO TO 210
200 WRITE (6,690)
C *****
C THIS STATEMENT ONLY WRITES IF THERE IS NO CONVERGENCE
C *****
GO TC 20
210 IF (ABS(GRESG).GT.TCLG) GO TO 220
    IF (ABS(GRESW).GT.TCLW) GO TO 220
    IF (ABS(EKGM).GT.FMCHG) GO TO 220
    IF (ABS(EKWM).GT.FMCHW) GO TO 220
C *****
C ANSWER WRITING ONLY OCCURS IF THE FLCW RETURNS TO 20 (CONVERGENCE)
C *****
GO TO 20
C RTIME GIVES THE REMAINING TIME IN SECCNDS
220 CALL RTIME(ITIM2)
    IF (IABS(ITIM2).LE.IT) GO TO 92
    EKWM=0.0
    EKGM=C.0
    GRESG=0.0
    GRESW=0.0
    AAAA=C.0
    BBBB=C.0
    NTRY=NTRY+1
    KC=KC+1
    IF (KC.GT.NHK) KC=1
    SUMMM=0.
    SUMNN=0.
    IF (PCCBV.EQ.C.) GO TC 250
    CALL TAB (DSTP,DISTP,STARP,CABIRI,PSTAR)
C
C TRANSPIRATION CALCULATION
C
DO 230 N=1,NX
NXB=N-1
NXF=N+1
IF (N.EQ.1) NXB=NXF
IF (N.EQ.NX) NXF=NXB
XP=0.5*(X(NXF)-X(NXB))
IF (N.EQ.1) XF=0.5*(X(NXF)-X(N))
IF (N.EC.NX) XP=0.5*(X(N)-X(NXB))
CALL TAB (CP,CIP,VW,PW(N),AVW)
CALL TAB (DPW,DIPW,DW,PW(N),RW)
CALL TAB (CSKW,DISKW,RKW,S(N),RKWC)
C CALCULATION OF F
SUMMM=SUMMM+RTDEN(N)*XP*RW*RKWC*KX(N)/AVW
C CALCULATION OF N

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SUMNN=SUMNN+RTDEN(N)*(PWA(N)+RW*H(N))*XP*RW*KX(N)*RKWC/AVW
QCTR(N)=KX(N)*RW*RKWC*RTDEN(N)*XP/AVW
230 CONTINUE
IF (SUMMM.EQ.0.) GO TO 250
Q1111=(SUMNN/SUMMM-POFLAW)/(1./SUMMM+1./PLCOND)
Q2222=AKGLEA*WINDVO**.8*(PSTAR+PSTAR*(POFLAW-PGIN(1)-DW(1)*HOFLEA/
1144.)/(37.135*(STEMP+460.))-01*RHU*ASTAR)
C CALCULATION OF C
AANUME=-PGIN(1)-RW*HOFLEA/144.+37.135*(STEMP+460.)*(PSTAR-.01*RHU*
1ASTAR)/PSTAR
DDNAMI=37.135*(STEMP+460.)/(PSTAR*AKGLEA*WINDVO**.8)

```

C CHECK WHETHER SUPPLY FUNCTION IS CONTROLLING OR POT. EVAP. CONT.

```

C IF (C1111.LE.C2222) AANUME=-POFLAW
C IF (Q1111.LE.Q2222) DDNAMI=0.
240 CONTINUE
ANUMER=SUMNN/SUMMM+AANUME
DENAMI=SUMMM*(1./SUMMM+1./PLCOND)+DDNAMI
SRESUL=SUMNN/SUMMM
ANDCEN=ANUMER/DENAMI
250 CONTINUE
IF (NBUG.LT.(-2)) GO TO 260
WRITE (6,592) SUMMM,SUMNN,DENAMI,ANUMER,SRESUL,ANDCEN,AANUME,DDNAM
11

```

260 QTRANT=0. C SOLVE THE SIMULTANEOUS DIFFERENCE EQ.

```

C DO 520 NCC=1,NX
C QWF=0.
C N=NCC
C QW(N)=0.
C QTRAN(N)=0.
C LAYER=LAY(N)
C NXB=N-1
C NXF=N+1
IF (NCC.EQ.1) NXB=NXF
IF (NCC.EQ.NX) NXF=NXB
IF (NTRY.NE.1) GO TO 270
CALL TAB (CPW,DIPW,CW,PW(N),RW)
CALL TAB (DSKW,DISKW,RKW,S(N),RKWC)
CALL TAB (DSKW,DISKW,RKW,S(NXF),RKWF)
CALL TAB (DSKG,DISKG,RKG,S(N),RKGC)
CALL TAB (DSKG,DISKG,RKG,S(NXB),RKGB)
CALL TAB (DSKG,DISKG,RKG,S(NXF),RKGF)
CALL TAB (DSKW,DISKW,RKW,S(NXB),RKWB)
CALL TAB (DPW,CIPW,DW,PW(NXF),RWF)
CALL TAB (CPG,DIPG,CG,PG(N),RG)
CALL TAB (CPG,CIPG,CG,PG(NXF),RGF)
CALL TAB (DP,CIP,VW,PW(N),AVW)
CALL TAB (DP,CIP,VG,PG(N),AVG)
CALL TAB (DP,CIP,VW,PW(NXF),AVWF)
CALL TAB (DP,DIP,VG,PG(NXF),AVGF)
DMWX(N)=(RWF*RKWF*KX(NXF)*TH(NXF)/AVWF)+(RW*RKWC*KX(N)*TH(N)/AVW)
1) DMGX(N)=(RGF*RKGF*KX(NXF)*TH(NXF)/AVGF)+(RG*RKGC*KX(N)*TH(N)/AVG)
1)

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270 MBX=NXB
  IF (NCC.EQ.1) MBX=N
  DX1=(X(N)-X(NXB))*(X(NXF)-X(NXB))
  DX2=(X(NXF)-X(N))*(X(NXF)-X(NXB))
  IF (NCC.EQ.1) CX1=2.0*((X(NXF)-X(N))**2)
  IF (NCC.EQ.NX) DX1=2.0*((X(N)-X(NXB))**2)
  IF (NCC.EQ.1) CX2=2.0*((X(NXF)-X(N))**2)
  IF (NCC.EQ.NX) DX2=2.0*((X(N)-X(NXB))**2)
  CALL TAB (CPG,CIPG,CG,PG(N),RG)
  CALL TAB (CPG,CIPG,CG,PG(NXB),RGXB)
  CALL TAB (CPG,CIPG,CG,PG(N),RGA)
  CALL TAB (CPG,CIPG,CG,PG(NXF),RGXF)
  CALL TAB (DPW,CIPW,CW,PW(N),RW)
  CALL TAB (DPW,CIPW,CW,PW(NXB),RWXB)
  CALL TAB (CPW,CIPW,CW,PW(N),RWA)
  CALL TAB (DPW,CIPW,CW,PW(NXF),RWXF)
  CALL TAB (DSKW,DISKW,RKW,S(N),RKWC)
  CALL TAB (DP,CIP,VW,PW(N),AVW)
  IF (RHU.GE.10C.) GC TC 280
  PPPWA=PGA(N)+37.135*DLG(-.01*RHU)*(460.+STEMP)
  IF (PWA(N).LT.PPPWA) FWA(N)=PPPWA
280 PCC=PGA(N)-PWA(N)
  NKK=(PCC-PCY)/EPC+1.0
  IF (NKK.LT.1) NKK=1
  IF (NKK.GT.NPCC) NKK=NPCC
  IF ((AS(LAYER,NKK)+BS(LAYER,NKK)*PCC).LT.WILPO) LAYER=10
  AS(10,NKK)=ASSS
  BS(10,NKK)=BSSS
  TPT=TF(N)*POF(N)/DT
  IF (NCC.GT.NBUG) GC TC 290
  WRITE (6,620) NKK,INL
  WRITE (6,600) AS(LAYER,NKK),BS(LAYER,NKK),PCC
  WRITE (6,620) N,NXB,NXF,NCC,MBX,NTRY
  WRITE (6,610) RKWC,RKWB,RKWF
  WRITE (6,610) RKGC,RKGB,RKGF
  WRITE (6,610) PW,RWF,RG,RGF
  WRITE (6,610) AVW,AVWF,AVE,AVGF
  WRITE (6,610) CX2,X(NXF),X(N),X(NXB)
  WRITE (6,580) DMWX(N),DMGX(N),TPT
290 CONTINUE
  SWK(N)=DMWX(MBX)+DMWX(N)
  SGK(N)=DMGX(MBX)+DMGX(N)
C
C  CALC. CF RESICLAL
C
  RSG=DMGX(MBX)*(PGA(NXF)-PGA(N)-RGA*H(N)+RGXB*H(NXB))/DX1+DMGX(N)*(
  1PGA(NXF)-PGA(N)+RGXF*H(NXF)-RGA*H(N))/DX2+TPT*(RGA*(AS(LAYER,NKK)+
  2BS(LAYER,NKK)*(PGA(N)-PWA(N)))-RG*S(N))
  RSW=DMWX(MBX)*(PWA(NXB)-PWA(N)-RWA*H(N)+RWXB*H(NXB))/DX1+DMWX(N)*(
  1PWA(NXF)-PWA(N)+RWXF*H(NXF)-RWA*H(N))/DX2-TPT*(RWA*(AS(LAYER,NKK)+
  2BS(LAYER,NKK)*(PGA(N)-PWA(N)))-RW*S(N))
  CC3=0.0
  QC5=0.0
  QC9=0.0
  QC11=0.0
  QC20=C.
  QC21=C.
  QC22=0.

```

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C
C
C

DECISION ON THE BOUNDARIES

```

QC23=0.
IF (PKEY(N).EC.0.) GC TO 390
IF (PKEY(N).EC.1.0) GC TO 350
IF (PKEY(N).EC.2.0) GC TO 320
IF (PKEY(N).EC.3.0) GC TO 340
IF (PKEY(N).EC.5.) GC TO 300
PGIN(N)=PGA(N)+RGA*H(N)
PWIN(N)=PWA(N)+RWA*H(N)
GO TO 330
300 QG(N)=CMGX(N)+0.5*(PGIN(N)-PGA(NXF)-RGXF*H(NXF))/(X(NXF)-X(N))
IF (PKEY(N).EC.5.0) QC11=-DMGX(N)+0.5/(X(NXF)-X(N))
QWF=WHEAD(IRAIN)
IF ((TTOT-DT).LT.FLCAT(IRAIN-1)*DHEAD) CALL TAB (DHEAD,DIHEAD,WHEA
10,(TTCT-DT),QWF)

```

C
C
C

DRAINAGE FUNCTION

```

IF (IQD.LT.1) GO TO 310
IF (S(N).LT.(QDD-0.1000)) GC TO 310
QWF=10.0*(QDD-S(N))*CWF
IF (S(N).GT.QDC) QWF=0.0
310 QW(N)=RW*QWF/(12.*DHEAD)
GO TO 350
320 CALL TAB (DHEAD,DIHEAD,WHEAD(N),TTOT,PWIN(N))
330 QW(N)=CPWX(N)+0.5*(PWIN(N)-PWA(NXF)-RWXF*H(NXF))/(X(NXF)-X(N))
IF (PKEY(N).EC.2.0) PGIN(N)=PWIN(N)
QG(N)=CMGX(N)+0.5*(PGIN(N)-PGA(NXF)-RGXF*H(NXF))/(X(NXF)-X(N))
IF (PKEY(N).EC.2.0) QC5=-DMWX(N)+0.5/(X(NXF)-X(N))
IF (PKEY(N).EC.4.0) CC3=CPWX(N)+0.5/(X(NXF)-X(N))
IF (PKEY(N).EC.4.0) QC5=-DMWX(N)+0.5/(X(NXF)-X(N))
IF (PKEY(N).EC.2.0) QC11=-DMGX(N)+0.5/(X(NXF)-X(N))
IF (PKEY(N).EC.4.0) QC9=CPGX(N)+0.5/(X(NXF)-X(N))
IF (PKEY(N).EC.4.0) QC11=-DMGX(N)+0.5/(X(NXF)-X(N))
IF (PKEY(N).EC.3.0) QC11=-DMGX(N)+0.5/(X(NXF)-X(N))
IF (N.NE.NX) GC TO 350
CW(N)=-CW(N)
QG(N)=-QG(N)
QC3=-QC3
QC5=-QC5
QC9=-QC9
QC11=-QC11
GO TO 350
340 PWIN(N)=PWA(NXF)+RWXF*H(NXF)
GO TO 330
350 XP=0.5*(X(NXF)-X(NXB))
IF (NCC.EQ.1) XP=C.5*(X(NXF)-X(N))
IF (NCC.EC.NX) XP=0.5*(X(N)-X(NXB))
IF (PGCBV.EQ.0.) GC TO 360
IF (SUMMM.EQ.0.) GC TO 360
QTRAN(N)=(RTDEN(N)*RW*RWKC*KX(N)/AVW*XP*(PWA(N)+RW*H(N)-SUMMN/SUMM
1M+ANUMER/DENAI))*0.01*PGCBV

```

C
C
C

SEASONAL TRANSPIRATION FUNCTION

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IF (IQT.LT.1) GC TO 360

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QT=(TTOT/360.)*(6.254)-QTA
QTT=(QTB)*SIN(CT)+QTC
IF(QTT.GT.1.0)CTT=1.00
IF(QTT.LT.0.C)QTT=0.050
360 QTRAN(N)=QTT+CTRAN(N)
QTRANT=QTRANT+QTRAN(N)
QW(N)=QW(N)-QTRAN(N)-CEVA(N)
RSW=RSW+QW(N)/XP
RSG=RSG+QG(N)/XP
AAAA=AAAA+CW(N)*DT
BBBB=BBBB+QG(N)*DT
ACUM0=0.
ACUM1=0.
ACUM2=0.
IF (PGCBV.EQ.C.) GC TC 380
IF (SUMMM.EQ.C.) GO TC 38C
DO 370 ICC=1,NX
IF (IOC.EQ.N.CR.IOC.EC.NXB.OR.IOC.EQ.NXF) GO TC 370
ACUM1=ACUM0/SUMMM
370 CONTINUE
ACUM0=ACUM0+QCTR(ICC)*PWB(IOC)
ACUM2=ACUM1-ACUM1/DENAMI
QC20=.01*PGCBV*QCTR(N)*(QCTR(NXB)/SUMMM-QCTR(NXB)/(SUMMM*DENAMI))
QC21=-.01*PGCBV*QCTR(N)*(1.-QCTR(N)/SUMMM+QCTR(N)/(SUMMM*DENAMI))
QC22=.01*PGCBV*QCTR(N)*(QCTR(NXF)/SUMMM-QCTR(NXF)/(SUMMM*DENAMI))
QC23=-.01*PGCBV*QCTR(N)*ACUM2
380 IF (NBUG.LT.(-1)) GC TC 390
WRITE (6,630) X(N),PKEY(N),QW(N),QG(N),PW IN(N),PGIN(N),QEVA(N),QTR
IAN(N),QWF,QTRANT,DMWX(N),RTDEN(N),PW(N),PWA(N),QC3,QC5,QC9,QC11,H(
2N),CC20,QC21,CC22,QCTR(N),SUMMM,SUMNN,ANUMER,DENAMI,SRESUL,ANDDEN,
3QC23,ACUM0,ACUM1,ACUM2,ANUME,DDNAMI
C
C CALC. THE COEFICIENT OF DIFFERENCE EQ.
C
390 CONTINUE
C(1,N)=CMWX(MBX)/DX1
C(2,N)=0.0
C(3,N)=-DMWX(N)/DX2
C(3,N)=C(3,N)-CMWX(MBX)/DX1
C(3,N)=C(3,N)+TPT*RWA*BS(LAYER,NKK)
C(3,N)=C(3,N)-FK(KC)*SWK(N)
C(4,N)=-TPT*RWA*BS(LAYER,NKK)
C(5,N)=DMWX(N)/DX2
C(7,N)=DMGX(MBX)/DX1
C(8,N)=-TPT*RG*BS(LAYER,NKK)
C(9,N)=-DMGX(N)/DX2
C(9,N)=C(9,N)-DMGX(MBX)/DX1
C(9,N)=C(9,N)+TPT*RG*BS(LAYER,NKK)
C(9,N)=C(9,N)-FK(KC)*SGK(N)
C(10,N)=0.0
C(11,N)=DMGX(N)/DX2
RSGS=RSGS+RSG
RSWS = RSWS + RSW
RSGA=RSGA+ ABS(RSG)
RSWA=RSWA+ ABS(RSW)
IF (NCC.GT.NBUG) GC TC 400
WRITE (6,660) N,N,(C(I,N),I=1,12)
WRITE (6,610) RSW,RSG,RSWA,RSGS,RSWS

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400 CONTINUE

C(6,N)=-RSW+QC23/XP
C(12,N)=-RSG
C(1,N)=C(1,N)+QC20/XP
C(3,N)=C(3,N)+QC3/XP+CC21/XP
C(5,N)=C(5,N)+QC5/XP+CC22/XP
C(9,N)=C(9,N)+CC9/XP
C(11,N)=C(11,N)+QC11/XP

C

C

C

LOCATE THE LOCATION OF MAX. RESIDUALS

IF (ABS(GRESW).LT. ABS(RSW)) MAXW=NCC
IF (ABS(GRESW).LT. ABS(RSW)) GRESW=RSW
IF (ABS(GRESG).LT. ABS(RSG)) MAXG=NCC
IF (ABS(GRESG).LT. ABS(RSG)) GRESG=RSG
IF (NCC.NE.1) GC TC 420

C(5,N)=C(5,N)+C(1,N)
C(1,N)=0.0
IF (C(3,N).EQ.0.0) GC TO 410

DD=1.0/C(3,N)
C(3,N)=1.0
C(4,N)=C(4,N)*DD
C(5,N)=C(5,N)*DD
C(6,N)=C(6,N)*DD

410 CONTINUE

C(11,N)=C(11,N)+C(7,N)
C(7,N)=0.0
GO TC 480

420 IF (NCC.NE.NX) GC TC 440

C(1,N)=C(1,N)+C(5,N)
C(5,N)=0.0
C(7,N)=C(7,N)+C(11,N)
C(11,N)=0.0
C(10,N)=0.0

IF (N.NE.1) GC TC 430
WRITE (6,660) N,N,(C(I,N),I=1,12)

430 CONTINUE

440 IF (C(1,N).EQ.0.0) GO TC 450

C(2,N)=-C(4,NXB)*C(1,N)
C(3,N)=C(3,N)-C(5,NXB)*C(1,N)
C(6,N)=C(6,N)-C(6,NXB)*C(1,N)
C(1,N)=0.0

450 IF (C(2,N).EQ.0.0) GC TO 460

C(3,N)=C(3,N)-C(10,NXB)*C(2,N)
C(6,N)=C(6,N)-C(12,NXB)*C(2,N)
C(2,N)=0.0

460 IF (C(3,N).EQ.0.0) GC TC 470

C(4,N)=C(4,N)/C(3,N)
C(5,N)=C(5,N)/C(3,N)
C(6,N)=C(6,N)/C(3,N)
C(3,N)=1.0

470 IF (C(7,N).EQ.0.0) GC TC 480

C(8,N)=C(8,N)-C(10,NXB)*C(7,N)
C(9,N)=C(9,N)-C(11,NXB)*C(7,N)
C(12,N)=C(12,N)-C(12,NXB)*C(7,N)

C(7,N)=0.0

480 IF (C(8,N).EQ.0.0) GC TC 490

C(9,N)=C(9,N)-C(4,N)*C(8,N)

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C(10,N)=C(10,N)-C(5,N)*C(8,N)
C(12,N)=C(12,N)-C(6,N)*C(8,N)
C(8,N)=0.0
490 IF (C(9,N).EQ.0.0) GO TO 500
D=1.0/C(9,N)
C(9,N)=1.0
C(10,N)=C(10,N)*D
C(11,N)=C(11,N)*D
C(12,N)=C(12,N)*D
500 IF (ACC.GT.NBUG) GO TO 510
WRITE (6,660) N,N,(C(I,N),I=1,12)
510 CONTINUE
520 CCNTINUE
C
C BAC SOLUTION ( THCMAS METHCD)
C
NA=NX
NL=NX
PGB(NL)=C(12,NL)
PWB(NL)=C(6,NL)-C(4,NL)*FGB(NL)
530 NL=NL-1
NA=NA-1
PGB(NL)=C(12,NL)-C(10,NL)*PWB(NL+1)-C(11,NL)*PGB(NL+1)
PWB(NL)=C(6,NL)-C(4,NL)*PGB(NL)-C(5,NL)*PWB(NL+1)
IF (ABS(EKGM).LT.ABS(FGB(NL))) EKGM=PGB(NL)
IF (ABS(EKWM).LT.ABS(PWB(NL))) EKWM=PWB(NL)
IF (NA.NE.1) GO TO 530
C
C CALC. NEW PRESSURE
C
DO 540 I=1,NX
540 PGA(I)=PGA(I)+FGB(I)
PWA(I)=PWA(I)+PWB(I)
IF (NPUG.LT.(G)) GO TO 570
DO 560 I=1,NX
LAYER=LAY(I)
IF (RHU.GE.100.) GO TO 550
PPPWA=PGA(I)+37.135*DLOG(.01*RHU)*(460.+STEMP)
IF (PWA(I).LT.PPPWA) PWA(I)=PPPWA
550 PCC=PGA(I)-PWA(I)
NKK=(PCC-PCI)/DPC+1.0
IF (NKK.LT.1) NKK=1
IF (NKK.GT.NPCC) NKK=NPCC
IF ((AS(LAYER,NKK)+BS(LAYER,NKK)*PCC).LT.WILPO) LAYER=10
AS(10,NKK)=ASSS
BS(10,NKK)=BSSS
C
PGB IS USED TEMPORARILY FOR SATURATION
560 PGB(I)=(AS(LAYER,NKK)+BS(LAYER,NKK)*PCC)*POR(I)
WRITE (6,650) (PWA(I),PGA(I),PGB(I),X(I),I=1,NX)
570 CCNTINUE
GO TO 180
C
580 FCRMAT (1H,10F11.4)
590 FCRMAT (1H0,2X,10E11.5/)
595 FORMAT(/,10X,2F3.0,7E11.5/16X,6E11.5)
591 FORMAT (1F0,4FEVAP,10E11.5/)
592 FCRMAT (1H0,5HTRANS,10E11.5/)
596 FCRMAT (1H0,7X,3I3,4X,5E11.5/)

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V G LEVEL 21          LNKB          DATE = 74186          17/44/00

600  FORMAT (1H0,16X,1C7HAAAA (1)      RESW (2)      CCCC (3)
1    AW (4)      EEEE (5)      GGGG (2-3)/5      ACW (5-2)/3,/,1X
2,8HW. PHASE,4X,7E16.6,/,17X,107H8888 (1)      RESG (2)      DD
3DD (3)      AG (4)      FFFF (5)      HHHH (2-3)/5      ACG
4(5-2)/3,/,13H NCN W. PHASE,7E16.6)
610  FORMAT (1H ,1CE11.4)
620  FCRMAT (1H0,1CI11)
630  FORMAT (1H0,8F14.5)
640  FORMAT (1H0,4FXLCC,2X,4HPKEY,2X,4HPWIN,9X,4HPGIN,7X,26HEVAPORATION
1  TRANSPIRATION,5X,2HCW,11X,2HQG,11X,2HPW,11X,2HPG,6X,10HSATURATIO
2N/1X,3HFT.,3X,3HNC.,10X,3HPSI,21X,12HLBM/SQ FT-DY44X,3HPSI,12X,10H
3CFT/CFT P.)
650  FCRMAT (1H ,F5.2,1X,F2.0,9(2X,E11.4))
660  FCRMAT (5HOC(1,,13,5H) TO ,5HC(12,,13,1H),/,1H0,6E18.6,/,1H0,6E18.
16)
670  FCRMAT (1H0,12,2I6,9E11.3)
671  FORMAT (1H0,5X,25HITER. RESULTS - NTRY,ETC./)
680  FCRMAT(1H0,120HRESTAR IT DELT      TIME      ROOT POT.      LEAF POT.
1 SUPPLY F.      FCT. EVAP      EVAPORATION TRANSPIRATION CUM.EVAP. CUM.TR
2AN./112H NO.      NO.      DAY      CAY      PSI
3      LBM/DY-SQ.FT.      LBM/)
69C  FORMAT (1H0,59HNO CONVERGENCE AT THIS TIME STEP. GO TO THE NEXT TI
1ME STEP.)
700  FCRMAT(1H ,F5.0,1X,F4.0,1X,F7.3,1X,F10.2,8(2X,E10.4))
710  FORMAT (1H0,51X,24HMATERIAL BALANCE RESULTS)
800  FCRMAT(/15X,14FTIME1 (SEC) = ,14,5X,14HTIME2 (SEC) = ,14,5X,14HTIM
1E3 (SEC) = ,14)
81C  FORMAT(/2X,5HCHECK,10E11.4)
820  FCRMAT(/110H TIME1.LE.IT SETS FINAL=2. TIME2.LE.IT GOES TO 92 TO S
1ET FINAL=2. TIME3 GIVES TIME LEFT AFTER TAPE IS WRITTEN.)
825  FORMAT(/2X,2H+=,E10.4,2X,3HRW=,E10.4,2X,4HPWA=,E10.4,2X,6HRTDEN=,E
110.4,2X,3HXP=,E10.4)
830  RETLRN
      END

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S IN EFFECT* NOID,EBCDIC,SOURCE,NCLIST,NODECK,LOAD,NOMAP
S IN EFFECT* NAME = LAKE , LINECNT = 60
TICS* SCURCE STATEMENTS = 601,PROGRAM SIZE = 24930
TICS* NO DIAGNCSTICS GENERATED

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TICS* NO DIAGNCSTICS THIS STEP

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V G LEVEL 21 CAPPR DATE = 74186 17/44/00

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SUBROUTINE CAPPR (AN,PCI,DPC,SCALE,LAYER,BW,AS,BS,DSW,DISW,PC)
C
C THIS SUBROUTINE FITS SECOND DEGREE POLY. THROUGH EACH VALUE
C OF SW. USES THIS POLY. TO CALCULATE INTERCEPT AND SLOPE OF
C TANGENT AT THE POINT.
C
DIMENSION BW(100), AS(10,100), BS(10,100), PC(10,100), DSW(10), DISW(10)
DOUBLE PRECISION AS,BS,BW
N=AN
MPC=N
DO 10 NN=1,N
  BW(NN)=BW(NN)*SCALE
  WRITE (6,70)
  WRITE (6,60) (BW(NN),NN=1,N)
  DISW(LAYER)=BW(N)
  DSW(LAYER)=(BW(1)-BW(N))/(AN-1.0)
  PCC=PCI+DPC*(AN)
  ACC=DISW(LAYER)-DSW(LAYER)
  JJ=N+1
  DO 40 J=1,N
    JJ=JJ-1
    ACC=ACC+DSW(LAYER)
    M=0
  20 M=M+1
    IF (M.GE.N-1) GO TO 30
    IF (BW(M).GT.ACC) GO TO 20
    IF (M.EQ.1) M=2
  30 IF (N.LT.M+1) M=N-1
    AM=M-2
    PSA=PCI+DPC*AM
    PSB=PSA+DPC
    PSC=PSB+DPC
    C3=(PSC-PSA)/(BW(M+1)-BW(M-1))-(PSB-PSA)/(BW(M)-BW(M-1))
    C3=C3/((BW(M+1)**2-BW(M-1)**2)/(BW(M+1)-BW(M-1))-(BW(M)**2-BW(M-1)**2)/(BW(M)-BW(M-1)))
    C2=(PSB-PSA-C3*(BW(M)**2-BW(M-1)**2))/(BW(M)-BW(M-1))
    C1=PSA-C2*BW(M-1)-C3*(BW(M-1)**2)
    PC(LAYER,J)=C1+(C2+C3*ACC)*ACC
    NN=J
    PCC=PCC-DPC
    IF (JJ.LE.1) GO TO 40
    BS(LAYER,J)=(BW(JJ)-BW(JJ-1))/DPC
    AS(LAYER,J)=BW(JJ)-BS(LAYER,J)*PCC
  40 CONTINUE
    AS(LAYER,N)=AS(LAYER,N-1)
    BS(LAYER,N)=BS(LAYER,N-1)
    PCI=PCI+DPC*(AN-1.0)
    DPC=-DPC
    PCC=PCI-DPC
    WRITE (6,80)
    DO 50 J=1,N
      PCC=PCC+DPC
  50 WRITE (6,60) PCC,AS(LAYER,J),BS(LAYER,J)
  RETURN
C
60 FORMAT (1H ,6F10.6)
70 FORMAT (1H1,31H WATER SATURATION (CFT/CFT P.))

```


96
V G LEVEL 21 CAPPR DATE = 74186 17/44/00
80 FORMAT (1HC,10FCAP. PRESS,3X,2HAS,8X,2HBS)
 END

S IN EFFECT* NCID,EBCCIC,SCURCE,NCLIST,NODECK,LOAD,NOMAP
S IN EFFECT* NAME = CAPPR , LINECNT = 60
TICS* SCURCE STATEMENTS = 52,PROGRAM SIZE = 2076
TICS* NO DIAGNOSTICS GENERATED

V G LEVEL 21 TAB DATE = 74186 17/44/00

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SUBROUTINE TAB (DP,PF,VIS,FIN,PVZA)
C THIS SUBROUTINE IS A TABLE LOOK UP WITH LINEAR INTERPOLATION
C DP INCREMENT IN THE INDEPENDENT VARIABLE
C PF INITIAL VALUE OF INDEPENDENT VARIABLE
C VIS DEPENDENT VARIABLE ARRAY - SPACED AT EQUAL INCREMENTS DP
C PIN VALUE OF INDEPENDENT VARIABLE AT WHICH PARTICULAR VIS WANTED
C PVZA VALUE OF DEPENDENT VARIABLE AT PIN
DIMENSION VIS(500)
DOUBLE PRECISION PVZA,P,PIN,PI
P=PIN
P=P-PF
I=P/DP+1.0
IF (I.GT.500.OR.I.LT.(-9999)) GO TO 10
IF (I.GT.500) PVZA=VIS(500)
IF (I.LT.1) PVZA=VIS(1)
IF (I.LT.1.OR.I.GT.500) RETURN
PI=I-1
PI=PI*DP
PX=P-PI
PVZA=VIS(I)+(VIS(I+1)-VIS(I))*PX/DP
RETURN
10 PFF=PF+DP*99.0
WRITE (6,20) DP,FIN,PF,VIS(1),PFF,VIS(100)
STOP
C
20 FORMAT (4I1HREQUESTING VALUE NOT WITHIN TABLE RANGE ,/,11HARG. DEL
1TA=,E16.8,5HARG.=,E16.8,/,11HFIRST ARG.=,E16.8,5HF(X)=,E16.8,/,10H
2LAST ARG.=,E16.8)
END

```

```

S IN EFFECT* NCID,EBCDIC,SOURCE,NCLIST,NODECK,LOAD,NOMAP
S IN EFFECT* NAME = TAB , LINECNT = 60
TICS* SOURCE STATEMENTS = 20,PROGRAM SIZE = 1022
TICS* NO DIAGNOSTICS GENERATED

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APPENDIX I-C
Input Data and Program Parameters

CONTINUOUS SYSTEM MODELING PROGRAM

*** VERSICN 1.3 ***

CONSTANT ZERO=1.E-36,Y1=1.9155E 8,Y2=1.0027E-1,Y3=5.1010E-3
 FUNCTION CAP1=0.,1.E12,0.0697,49.5,0.07,47.5,0.08,36.,0.09,26.0,....
 0.10,16.,0.11,6.,0.12,2.5,0.135,2.,0.15,1.7,0.18,1.5,0.26,1.,0.42,....
 0.5,0.6,0.2,0.7,0.1,0.809,0.001,0.9,0.001,1.,0.001
 FUNCTION CAP2=0.,1.E12,0.05,1.E6,0.091,89.091,0.095,44.545,0.096,....
 40.09,0.10,17.818,0.101,13.364,0.105,8.909,0.11,7.573,0.12,6.682,....
 0.15,5.123,0.171,4.455,0.18,4.276,0.19,4.098,0.20,3.965,0.25,3.475,....
 0.30,3.207,0.35,3.209,0.40,2.940,0.45,2.855,0.50,2.829,0.55,2.762,....
 0.60,2.717,0.65,2.628,0.70,2.483,0.75,2.450,0.80,2.361,0.85,2.272,....
 0.87,2.227,0.90,2.138,0.92,2.049,0.94,1.938,0.95,1.849,0.96,1.782,....
 0.98,1.336,1.0,0.445
 FUNCTION CAP3=0.,1.E12,0.05,1.E6,0.1,1.E4,0.15,1.E3,0.185,89.09,....
 0.201,44.55,0.221,40.09,0.251,35.64,0.291,31.18,0.36,26.73,0.40,....
 24.95,0.42,24.28,0.45,23.65,0.48,23.16,0.5,22.94,0.55,22.50,0.6,22.5,....
 0.7,22.27,0.8,21.38,0.91,17.82,0.972,13.36,0.986,8.91,0.992,4.455,....
 1.0,0.445

DYNAMIC

P1=AFGEN(CAP1,TIME)
 P2=AFGEN(CAP2,TIME)
 P3=AFGEN(CAP3,TIME)
 AR1=1./(P1**3.)
 AR2=1./(P2**3.)
 AR3=1./(P3**3.)
 X1=INTGRL(ZERO,AR1)
 X2=INTGRL(ZERO,AR2)
 X3=INTGRL(ZERO,AR3)
 RK1=X1/Y1
 RK2=X2/Y2
 RK3=X3/Y3

TIMER DELT=0.0001,PRDEL=0.05,CLTDEL=0.05,FINTIM=1.
 PRINT RK1,RK2,RK3
 PRTPLT RK1,RK2,RK3
 END
 STOP

VARIABLE SEQUENCE

AR1	X1	P2	AR2	X2	P3	AR3	X3	RK1
RK3								

TS	INPLTS	PARAMS	INTEGS	MEM	BLKS	FORTTRAN	DATA	CDS
0)	41(1400)	11(400)	3+	0=	3(300)	13(600)		20

ENDJOB

APPENDIX I-D
Sample Print-Out

RESTART= 0.0 FINAL= 0.0 POFLOW=-225.0000
 AKXMU IS PERM MULTIPLIER FOR EASY FERM CHANGE
 AKXMU= 1.00000 ESTAR= 100.0AIRKG = 0.4200WILP= 0.1500
 WHITE CONTRL(NBUC)= -4 IT = 20 INSW = 0ITAPE = 1 IOUPT= 2 IQT= 1 IOD= 1
 MAX DEL T= 15.00 PLANT CONDUCTIVITY=0.14400 HEIGHT OF LEAVES FROM A DATUM PLANE=, 20.00 AIR-LEAF EVAP.COEF.=3.00000
 INTERCEPT= 0.23500 SLOPE=-0.02550 PERCENT GRCLND COVER BY VEGETATION= 95.00 DEL T MULT.= 0.10

24.000000 1.000000 10.000000

WATER VISCOSITY, (CENTIPOISE)

1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000
1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000
1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000
1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000
1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000
1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000
1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000
1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000
1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000
1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000	1.000000

GAS VISCOSITY, (CENTIPOISE)

0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000
0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000
0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000
0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000
0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000
0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000
0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000
0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000
0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000
0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000	0.018000

WATER DENSITY, (LBM./CU.FT.)

62.265589	62.269989	62.265589	62.265589	62.269989	62.269989	62.269989	62.269989	62.269989	62.269989
62.265589	62.269989	62.265589	62.265589	62.269989	62.269989	62.269989	62.269989	62.269989	62.269989
62.265589	62.269989	62.265589	62.265589	62.269989	62.269989	62.269989	62.269989	62.269989	62.269989
62.265589	62.269989	62.265589	62.265589	62.269989	62.269989	62.269989	62.269989	62.269989	62.269989
62.265589	62.269989	62.265589	62.265589	62.269989	62.269989	62.269989	62.269989	62.269989	62.269989
62.265589	62.269989	62.265589	62.265589	62.269989	62.269989	62.269989	62.269989	62.269989	62.269989
62.265589	62.269989	62.265589	62.265589	62.269989	62.269989	62.269989	62.269989	62.269989	62.269989
62.265589	62.269989	62.265589	62.265589	62.269989	62.269989	62.269989	62.269989	62.269989	62.269989
62.265589	62.269989	62.265589	62.265589	62.269989	62.269989	62.269989	62.269989	62.269989	62.269989
62.265589	62.269989	62.265589	62.265589	62.269989	62.269989	62.269989	62.269989	62.269989	62.269989

GAS DENSITY, (LBM./CU. FT.)

0.045400	0.047900	0.050500	0.053000	0.055500	0.058000	0.060100	0.063100	0.065600	0.068100
0.070600	0.073200	0.075700	0.078200	0.080000	0.083300	0.085800	0.088300	0.090800	0.093400
0.095900	0.098400	0.100000	0.103400	0.106000	0.108500	0.111000	0.113500	0.116100	0.118600
0.121000	0.123600	0.126200	0.128700	0.131200	0.133700	0.136200	0.138800	0.141100	0.143800
0.146300	0.148900	0.151400	0.153900	0.156400	0.159000	0.161100	0.164000	0.166500	0.169000
0.171600	0.174100	0.176600	0.179100	0.181100	0.184200	0.186700	0.189200	0.191800	0.194300
0.196800	0.199300	0.201000	0.204400	0.206900	0.209400	0.211900	0.214500	0.217000	0.219500
0.222000	0.224600	0.227300	0.229800	0.252300	0.254800	0.257400	0.259900	0.262100	0.264900
0.267400	0.270000	0.272500	0.275000	0.277500	0.280100	0.282100	0.285100	0.285100	0.285100
0.285100	0.285100	0.285100	0.285100	0.285100	0.285100	0.285100	0.285100	0.285100	0.285100
100.000000	0.0	1.000000	1.000000						

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WATER SATURATION (CFY/CFY P.S.)					
1.010000	1.000000	0.990000	0.989000	0.988000	0.987000
0.986000	0.985000	0.984000	0.983000	0.982000	0.981000
0.962000	0.950000	0.935000	0.915000	0.895000	0.865000
0.825000	0.760000	0.435000	0.390000	0.360000	0.335000
0.315000	0.300000	0.285000	0.275000	0.265000	0.255000
0.245000	0.240000	0.235000	0.230000	0.225000	0.220000
0.215000	0.213000	0.210000	0.207000	0.205000	0.204250
0.203500	0.202750	0.202000	0.201250	0.200500	0.199750
0.190000	0.182500	0.175000	0.170000	0.167500	0.165000
0.194500	0.193750	0.193000	0.192250	0.191500	0.190750
0.190000	0.189250	0.188500	0.187750	0.187000	0.186250
0.185500	0.184750	0.184000	0.183250	0.182500	0.181750
0.181000	0.180250	0.179500	0.178750	0.178000	0.177250
0.176500	0.175750	0.175000	0.174250	0.173500	0.172750
0.172000	0.171250	0.170500	0.169750	0.169000	0.168250
0.167500	0.166750	0.166000	0.165250	0.164500	0.163750
0.163000	0.162250	0.161500	0.160750		

CAF. PRESS AS BS

106.919968	0.235000	-0.000694
105.639966	0.235000	-0.000694
104.759964	0.235000	-0.000694
103.679962	0.235000	-0.000694
102.559960	0.235000	-0.000694
101.519958	0.235000	-0.000694
100.439957	0.235000	-0.000694
99.359955	0.235000	-0.000694
98.279953	0.235000	-0.000694
97.199951	0.235000	-0.000694
96.119949	0.235000	-0.000694
95.039948	0.235000	-0.000694
93.959946	0.235000	-0.000694
92.879944	0.235000	-0.000694
91.799942	0.235000	-0.000694
90.719940	0.235000	-0.000694
89.639938	0.235000	-0.000694
88.559937	0.235000	-0.000694
87.479935	0.235000	-0.000694
86.399933	0.235000	-0.000694
85.319931	0.235000	-0.000694
84.239929	0.235000	-0.000694
83.159927	0.235000	-0.000694
82.079926	0.235000	-0.000694
80.999924	0.235000	-0.000694
79.919922	0.235000	-0.000694
78.839920	0.235000	-0.000694
77.759918	0.235000	-0.000694
76.679916	0.235000	-0.000694
75.599915	0.235000	-0.000694
74.519913	0.235000	-0.000694
73.439911	0.235000	-0.000694
72.359909	0.235000	-0.000694
71.279907	0.235000	-0.000694
70.199905	0.235000	-0.000694
69.119904	0.235000	-0.000694
68.039902	0.235000	-0.000694
66.959900	0.235000	-0.000694
65.879898	0.235000	-0.000694
64.799896	0.235000	-0.000694
63.719894	0.235000	-0.000694
62.639893	0.235000	-0.000694

61.959891	0.235000	-0.000694
60.479889	0.235000	-0.000694
59.399887	0.235000	-0.000694
58.319885	0.235000	-0.000694
57.239883	0.235000	-0.000694
56.159882	0.235000	-0.000694
55.079880	0.235000	-0.000694
53.999878	0.235000	-0.000694
52.919876	0.235000	-0.000694
51.839874	0.235000	-0.000694
50.759872	0.235000	-0.000694
49.679871	0.235000	-0.000694
48.599869	0.235000	-0.000694
47.519867	0.235000	-0.000694
46.439865	0.235000	-0.000694
45.359863	0.235000	-0.000694
44.279861	0.235000	-0.000694
43.199860	0.285000	-0.001852
42.119858	0.324000	-0.002778
41.039856	0.324000	-0.002778
39.959854	0.287000	-0.001852
38.879852	0.394999	-0.004630
37.799850	0.394999	-0.004630
36.719849	0.394999	-0.004630
35.639847	0.394999	-0.004630
34.559845	0.394999	-0.004630
33.479843	0.394999	-0.004630
32.399841	0.544999	-0.009259
31.319839	0.544999	-0.009259
30.239838	0.544999	-0.009259
29.159836	0.544999	-0.009259
28.079834	0.674998	-0.013889
26.999832	0.674998	-0.013889
25.919830	0.794997	-0.018519
24.839828	0.909996	-0.023148
23.759827	1.019996	-0.027778
22.679825	1.334993	-0.041667
21.599823	6.934952	-0.300926
20.519821	1.994990	-0.060185
19.439819	1.544994	-0.037037
18.359818	1.374995	-0.027778
17.279816	1.214997	-0.018519
16.199814	1.214997	-0.018519
15.119814	1.144998	-0.013889
14.039814	1.105998	-0.011111
12.959814	1.105998	-0.011111
11.879814	1.039999	-0.005556
10.799814	1.010000	-0.002778
9.719814	0.992000	-0.000926
8.639814	0.992000	-0.000926
7.559814	0.992000	-0.000926
6.479815	0.992000	-0.000926
5.399815	0.992000	-0.000926
4.319815	0.992000	-0.000926
3.239815	0.992000	-0.000926
2.159815	1.009998	-0.005259
1.079815	1.009998	-0.005259
-0.000185	1.009998	-0.005259

3.080000	2.679999	4.440000	5.259999	4.750000	5.669999	4.750000	5.660000	5.000000
4.790000	3.080000	3.080000	2.679999	4.440000	5.259999	5.469999	4.750000	5.660000
4.549999	3.259999	4.790000	3.080000	3.080000	2.679999	4.440000	5.259999	5.469999
5.660000	5.000000	4.549999	3.259999	4.790000	3.080000	3.080000	2.679999	4.440000

MTPY TSTEP
400.000000 5.000000
ITERATION PARAMETERS - HK
1.000000 0.500000 0.250000 0.125000 0.062500

CONVERGENCE CRITERIA
TOLW TOLG PMCHW FPMCH
0.0360 0.0360 0.0360 0.0360
TCLW = MAX WAT PHASE RESID TOLG IS MAX GAS PHASE RESID
PMCHW = MAX CHANGE IN WAT PHASE PRESS FPMCHG = MAX CHANGE IN GAS PHASE PRESS ALLOWED

DELTA TIME(DT) = 0.1000 MAX TIME = 18000.00 TIMA = 100.00 TIMB = 999.00 TIMC = 15.00
TIMA SETS TIME LIMIT FOR CY TO BE CLIMAX, TIMB SET TIME LIMIT FOR DO TO BE TIMC.

EASONAL TRANSPIRATION FUNCTION CONSTANTS, QTA= 1.4000 QTB= 2.0000 QTC= 0.6800
RAINFAGE FUNCTION CONSTANT, QDC= 1.0000

RESTAR NC.	IT NC.	DELT DAY	TIME DAY	ROOT PCT. PSI	LEAF PCT.	SUPPLY F.	POT. EVAP LBM/DY-SQ.FT.	EVAPORATION	TRANSPIRATION	CUM.EVAP. LBM	CUM.TRAN.
0.	0.	0.100	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

MATERIAL BALANCE RESULTS

W. PHASE	AAAA (1)	RESW (2)	CCCC (3)	AW (4)	EEEE (5)	GGGG (2-3)/5	ACW (5-2)/3
0.0	0.0	0.215355D 03	0.0	0.215355D 03	0.215355D 03	0.100000D 01	0.0
NCA W. PHASE	0.0	0.772975D-01	0.0	0.772975D-01	0.772975D-01	0.100000D 01	0.0

XLCC FT.	PKEY NO.	PWIN PSI	PCIN	EVAPORATION LBM/SQ FT-DY	TRANSPIRATION	QW	QG	PW PSI	PG	SATURATION CFT/CFT P.
0.0	5.	0.0	0.14700 02	0.0	0.0	0.0	0.0	-0.56780 01	0.14700 02	0.76850 00
1.00	1.	0.0	0.0	0.0	0.0	0.0	0.0	-0.56780 01	0.14700 02	0.76850 00
2.00	1.	0.0	0.0	0.0	0.0	0.0	0.0	-0.56770 01	0.14700 02	0.76850 00
3.00	1.	0.0	0.0	0.0	0.0	0.0	0.0	-0.56770 01	0.14700 02	0.76850 00
4.00	1.	0.0	0.0	0.0	0.0	0.0	0.0	-0.56760 01	0.14700 02	0.76850 00
5.00	1.	0.0	0.0	0.0	0.0	0.0	0.0	-0.56760 01	0.14700 02	0.76850 00
6.00	1.	0.0	0.0	0.0	0.0	0.0	0.0	-0.56750 01	0.14700 02	0.76850 00
7.00	1.	0.0	0.0	0.0	0.0	0.0	0.0	-0.56750 01	0.14700 02	0.76850 00
8.00	1.	0.0	0.0	0.0	0.0	0.0	0.0	-0.56740 01	0.14700 02	0.76850 00
9.00	4.	0.0	0.0	0.0	0.0	0.0	0.0	-0.56740 01	0.14700 02	0.76850 00

RESTAR NC.	IT NO.	DELT DAY	TIME DAY	ROOT PCT. PSI	LEAF POT.	SUPPLY F.	POT. EVAP LBP/DY-SQ.FT.	EVAPORATION	TRANSPIRATION	CUM.EVAP. LBM	CUM.TRAN.
1.	4.	0.110	0.11	-.7049E 01	-.7470E 01	0.3082E 02	0.1178E 01	0.8515E-02	0.5763E-01	0.9367E-03	0.6340E-02
2.	3.	0.121	0.23	-.7022E 01	-.7443E 01	0.3083E 02	0.1178E 01	0.8515E-02	0.5763E-01	0.1967E-02	0.1331E-01

MATERIAL BALANCE RESULTS

W. PHASE	AAAA (1)	RESW (2)	CCCC (3)	AW (4)	EEEE (5)	GGGG (2-3)/5	ACW (5-2)/3
0.0	0.100801D 00	0.215540D 03	0.192463D 00	0.215347D 03	0.215355D 03	0.999963D 00	-0.958353D 00
NCA W. PHASE	-0.733516C-04	0.772147C-01	-0.113138C-03	0.773275D-01	0.772975D-01	0.100039D 01	-0.731168D 00

XLCC FT.	PKEY NO.	PWIN PSI	PCIN	EVAPORATION LBM/SQ FT-DY	TRANSPIRATION	QW	QG	PW PSI	PG	SATURATION CFT/CFT P.
0.0	5.	0.0	0.14700 02	0.65150-02	0.65190-01	0.87240 00	-0.57360-03	-0.53890 01	0.14790 02	0.78050 00
1.00	1.	0.0	0.0	0.0	0.75020-01	-0.75020-01	0.0	-0.56270 01	0.14760 02	0.76800 00

51.	3.	15.000	150.62	-.6778E 01	-.1316E 02	0.3083E 02	0.8612E 00	0.6460E-02	0.8726E 00	0.1517E 01	0.1063E 03
52.	3.	15.000	165.62	-.6849E 01	-.1292E 02	0.3080E 02	0.8133E 00	0.6146E-02	0.8298E 00	0.1609E 01	0.1187E 03

MATERIAL BALANCE RESULTS

W. PHASE	AAAA (1)	RESW (2)	CCCC (3)	AW (4)	EEEE (5)	GGGG (2-3)/5	ACW (5-2)/3
	-0.404372D C1	0.216296D 03	-0.597072D 01	0.222266D 03	0.215355D 03	0.103209D 01	0.157501D 00
NCA W. PHASE	BBBB (1)	RESG (2)	DDDD (3)	AG (4)	FFFF (5)	MMMM (2-3)/5	ACG (5-2)/3
	0.171442D-C2	0.774294C-C1	0.140291D-01	0.634003D-01	0.772975D-01	0.820212D 00	-0.940379D-02

XLCC FT.	PKEY NC.	PWIN PSI	PGIN	EVAPORATION LBM/SQ FT-DY	TRANSPIRATION FT-DY	QW	QG	PW	PG	SATURATION CFT/CFT P.
0.0	5.	0.0	0.1470D 02	0.6146C-02	0.5489D 00	0.8852D-02	-0.8111D-03	-0.6077D 01	0.1470D 02	0.6832D 00
1.00	1.	0.0	0.0	0.0	0.1028D 00	-0.1028D 00	0.0	-0.6329D 01	0.1474D 02	0.5951D 00
2.00	1.	0.0	0.0	0.0	0.4796D-01	-0.4796D-01	0.0	-0.5953D 01	0.1478D 02	0.6957D 00
3.00	1.	0.0	0.0	0.0	0.2942D-01	-0.2942D-01	0.0	-0.5549D 01	0.1485D 02	0.7672D 00
4.00	1.	0.0	0.0	0.0	0.2272D-01	-0.2272D-01	0.0	-0.5116D 01	0.1494D 02	0.7881D 00
5.00	1.	0.0	0.0	0.0	0.2674D-01	-0.2674D-01	0.0	-0.4681D 01	0.1503D 02	0.8087D 00
6.00	1.	0.0	0.0	0.0	0.1767D-01	-0.1767D-01	0.0	-0.4242D 01	0.1513D 02	0.8273D 00
7.00	1.	0.0	0.0	0.0	0.2159D-01	-0.2159D-01	0.0	-0.3802D 01	0.1525D 02	0.8394D 00
8.00	1.	0.0	0.0	0.0	0.9129D-02	-0.9129D-02	0.0	-0.3341D 01	0.1537D 02	0.8519D 00
9.00	4.	-0.6759C 01	0.1550D 02	0.0	0.2970D-02	-0.4494D-03	0.9254D-03	-0.2884D 01	0.1551D 02	0.8639D 00

TIME1.LE.IT SETS FINAL=2. TIME2.LE.IT GOES TO 92 TO SET FINAL=2. TIME3 GIVES TIME LEFT AFTER TAPE IS WRITTEN.

TIME1 (SEC) = 144 TIME2 (SEC) = 144 TIME3 (SEC) = 143

RESTAR NC.	IT NC.	DELT CAY	TIME CAY	ROOT PCT. PSI	LEAF PCT.	SUPPLY F.	POT. EVAP LBM/DY-SQ.FT.	EVAPORATION	TRANSPIRATION	CUM.EVAP. LBM	CUM.TRAN.
53.	2.	15.00C	180.62	-.6849E 01	-.1168E 02	0.3078E 02	0.6314E 00	0.4898E-02	0.6606E 00	0.1682E 01	0.1287E 03
54.	4.	15.000	195.62	-.6703E 01	-.1024E 02	0.3080E 02	0.4408E 00	0.3590E-02	0.4833E 00	0.1736E 01	0.1359E 03

MATERIAL BALANCE RESULTS

W. PHASE	AAAA (1)	RESW (2)	CCCC (3)	AW (4)	EEEE (5)	GGGG (2-3)/5	ACW (5-2)/3
	0.511405D 01	0.220030D 03	-0.261697D 00	0.220292D 03	0.215355D 03	0.102292D 01	0.178625D 02
NCA W. PHASE	BBBB (1)	RESG (2)	DDDD (3)	AG (4)	FFFF (5)	MMMM (2-3)/5	ACG (5-2)/3
	-0.885249C-03	0.729714C-C1	0.130431D-01	0.599283D-01	0.772975D-01	0.775294D 00	0.331676D 00

XLCC FT.	PKEY NC.	PWIN PSI	PGIN	EVAPORATION LBM/SQ FT-DY	TRANSPIRATION FT-DY	QW	QG	PW	PG	SATURATION CFT/CFT P.
0.0	5.	0.0	0.1470D 02	0.3590C-02	0.6950D 00	0.1299D 00	-0.9836D-03	-0.5702D 01	0.1470D 02	0.7670D 00
1.00	1.	0.0	0.0	0.0	0.5892D-02	-0.5892D-02	0.0	-0.6245D 01	0.1475D 02	0.6185D 00
2.00	1.	0.0	0.0	0.0	-0.5640D-01	0.5640D-01	0.0	-0.5877D 01	0.1478D 02	0.7174D 00
3.00	1.	0.0	0.0	0.0	-0.4002D-01	0.4002D-01	0.0	-0.5413D 01	0.1485D 02	0.7753D 00
4.00	1.	0.0	0.0	0.0	-0.3032D-01	0.3032D-01	0.0	-0.4983D 01	0.1494D 02	0.7958D 00
5.00	1.	0.0	0.0	0.0	-0.3431D-01	0.3431D-01	0.0	-0.4552D 01	0.1504D 02	0.8160D 00
6.00	1.	0.0	0.0	0.0	-0.2111D-01	0.2111D-01	0.0	-0.4125D 01	0.1514D 02	0.8314D 00
7.00	1.	0.0	0.0	0.0	-0.2427D-01	0.2427D-01	0.0	-0.3698D 01	0.1526D 02	0.8430D 00
8.00	1.	0.0	0.0	0.0	-0.8751D-02	0.8751D-02	0.0	-0.3287D 01	0.1538D 02	0.8538D 00
9.00	4.	-0.6777D 01	0.1550D 02	0.0	-0.2432D-02	0.1757D-02	0.9246D-03	-0.2867D 01	0.1551D 02	0.8645D 00

TIME1.LE.IT SETS FINAL=2. TIME2.LE.IT GOES TO 92 TO SET FINAL=2. TIME3 GIVES TIME LEFT AFTER TAPE IS WRITTEN.

TIME1 (SEC) = 143 TIME2 (SEC) = 143 TIME3 (SEC) = 140

RESTAR NC.	IT NC.	DELT CAY	TIME CAY	ROOT PCT. PSI	LEAF PCT.	SUPPLY F.	POT. EVAP LBM/DY-SQ.FT.	EVAPORATION	TRANSPIRATION	CUM.EVAP. LBM	CUM.TRAN.
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55.	2.	15.000	210.62	-.6643E 01	-.9854E 01	0.3084E 02	0.3999E 00	0.3263E-02	0.4392E 00	0.1785E 01	0.1425E 03
56.	2.	15.000	225.62	-.6610E 01	-.9529E 01	0.3085E 02	0.3630E 00	0.2966E-02	0.3994E 00	0.1829E 01	0.1485E 03

MATERIAL BALANCE RESULTS

W. PHASE	AAAA (1) 0.188930D 01	RESW (2) 0.222160D C3	CCCC (3) 0.506756D 01	AW (4) 0.217093D 03	EEEE (5) 0.215355D 03	GGGG (2-3)/5 0.100807D 01	ACW (5-2)/3 -0.134286D 01
NCA W. PHASE	PPRR (1) 0.15E772D-C2	RESE (2) C.704C82D-C1	DDDD (3) 0.154474D-01	AG (4) 0.549608D-01	FFFF (5) 0.772975D-01	HHHH (2-3)/5 0.711029D 00	ACG (5-2)/3 0.445983D 00

XLCC FT.	PKEY NC.	PWIN	PGIN PSI	EVAPORATION LBM/SQ FT-DY	TRANSPIRATION	QW	QG	PW	PG	SATURATION CFT/CFT P.
0.0	5.	0.0	0.1470D 02	0.2566D-02	0.5056D 00	0.2424D-01	-0.7851D-03	-0.5941D 01	0.1470D 02	0.7240D 00
1.00	1.	0.0	0.0	0.0	0.1822D-01	-0.1822D-01	0.0	-0.6148D 01	0.1475D 02	0.6476D 00
2.00	1.	0.0	0.0	0.0	-0.2837D-01	0.2837D-01	0.0	-0.5761D 01	0.1479D 02	0.7507D 00
3.00	1.	0.0	0.0	0.0	-0.1479D-01	0.1479D-01	0.0	-0.5314D 01	0.1486D 02	0.7808D 00
4.00	1.	0.0	0.0	0.0	-0.1466D-01	0.1466D-01	0.0	-0.4884D 01	0.1494D 02	0.8016D 00
5.00	1.	0.0	0.0	0.0	-0.1848D-01	0.1848D-01	0.0	-0.4453D 01	0.1504D 02	0.8218D 00
6.00	1.	0.0	0.0	0.0	-0.1448D-01	0.1448D-01	0.0	-0.4028D 01	0.1514D 02	0.8349D 00
7.00	1.	0.0	0.0	0.0	-0.1958D-01	0.1958D-01	0.0	-0.3605D 01	0.1526D 02	0.8464D 00
8.00	1.	0.0	0.0	0.0	-0.1029D-01	0.1029D-01	0.0	-0.3211D 01	0.1538D 02	0.8565D 00
9.00	4.	-0.6723D 01	0.1550D 02	0.0	-0.3727D-02	-0.7314D-03	0.8909D-03	-0.2814D 01	0.1551D 02	0.8661D 00

TIME1.LE.IT SETS FINAL=2. TIME2.LE.IT GOES TO 52 TO SET FINAL=2. TIME3 GIVES TIME LEFT AFTER TAPE IS WRITTEN.

TIME1 (SEC) = 139 TIME2 (SEC) = 139 TIME3 (SEC) = 138

RESTAR NC.	IT NC.	DELT CAY	TIME CAY	RCOT PCT. PSI	LEAF PCT.	SUPPLY F.	POT. EVAP LBM/DY-SQ.FT.	EVAPORATION	TRANSPIRATION	CUM.EVAP. LBM	CUM.TRAN.
57.	2.	15.000	240.62	-.6573E 01	-.8554E 01	0.3086E 02	0.2877E 00	0.2421E-02	0.3257E 00	0.1866E 01	0.1534E 03
58.	3.	15.000	255.62	-.6485E 01	-.8211E 01	0.3088E 02	0.2288E 00	0.1993E-02	0.2381E 00	0.1896E 01	0.1569E 03

MATERIAL BALANCE RESULTS

W. PHASE	AAAA (1) 0.432471D 01	RESW (2) 0.225272C 03	CCCC (3) 0.123831D 02	AW (4) 0.212889D 03	EEEE (5) 0.215355D 03	GGGG (2-3)/5 0.988546D 00	ACW (5-2)/3 -0.800795D 00
NCA W. PHASE	BBBB (1) 0.170592D-02	RESE (2) 0.666892C-01	DDDD (3) 0.167221D-01	AG (4) 0.479671D-01	FFFF (5) 0.772975D-01	HHHH (2-3)/5 0.620553D 00	ACG (5-2)/3 0.566615D 00

XLCC FT.	PKEY NC.	PWIN	PGIN PSI	EVAPORATION LBM/SQ FT-DY	TRANSPIRATION	QW	QG	PW	PG	SATURATION CFT/CFT P.
0.0	5.	0.0	0.1470D 02	0.1993D-02	0.4263D 00	0.1045D 00	-0.7542D-03	-0.5786D 01	0.1470D 02	0.7620D 00
1.00	1.	0.0	0.0	0.0	-0.1224D-02	0.1224D-02	0.0	-0.6033D 01	0.1475D 02	0.6810D 00
2.00	1.	0.0	0.0	0.0	-0.3030D-01	0.3030D-01	0.0	-0.5622D 01	0.1480D 02	0.7660D 00
3.00	1.	0.0	0.0	0.0	-0.3289D-01	0.3289D-01	0.0	-0.5190D 01	0.1487D 02	0.7876D 00
4.00	1.	0.0	0.0	0.0	-0.2766D-01	0.2766D-01	0.0	-0.4762D 01	0.1495D 02	0.8084D 00
5.00	1.	0.0	0.0	0.0	-0.3189D-01	0.3189D-01	0.0	-0.4331D 01	0.1505D 02	0.8273D 00
6.00	1.	0.0	0.0	0.0	-0.2139D-01	0.2139D-01	0.0	-0.3911D 01	0.1515D 02	0.8391D 00
7.00	1.	0.0	0.0	0.0	-0.2741D-01	0.2741D-01	0.0	-0.3492D 01	0.1526D 02	0.8504D 00
8.00	1.	0.0	0.0	0.0	-0.1280D-01	0.1280D-01	0.0	-0.3108D 01	0.1538D 02	0.8602D 00
9.00	4.	-0.6644D 01	0.1550D 02	0.0	-0.4633D-02	-0.1702D-02	0.8680D-03	-0.2723D 01	0.1551D 02	0.8686D 00

TIME1.LE.IT SETS FINAL=2. TIME2.LE.IT GOES TO 52 TO SET FINAL=2. TIME3 GIVES TIME LEFT AFTER TAPE IS WRITTEN.

TIME1 (SEC) = 138 TIME2 (SEC) = 138 TIME3 (SEC) = 135

RESTAR NC.	IT NC.	DELT CAY	TIME CAY	RCOT PCT. PSI	LEAF PCT.	SUPPLY F.	POT. EVAP LBM/DY-SQ.FT.	EVAPORATION	TRANSPIRATION	CUM.EVAP. LBM	CUM.TRAN.
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59. 7. 15.000 270.62 -.6350E 01 -.7591E 01 0.3092E 02 0.6028E 00 0.4990E-02 0.2277E 00 0.2063E 01 0.1609E 03
 60. 18. 15.000 285.62 -.5E57E 01 -.6181E 01 0.3101E 02 0.8882E 00 0.6569E-02 0.4441E-01 0.2063E 01 0.1609E 03

MATERIAL BALANCE RESULTS

W. PHASE	AAAA (1) 0.602946D 01	RESW (2) 0.233099C 03	CCCC (3) 0.223214D 02	AW (4) 0.210778D 03	EEEE (5) 0.215355D 03	GGGG (2-3)/5 0.978745D 00	ACW (5-2)/3 -0.794929D 00
NCA W. PHASE	BPBB (1) -0.493442C-02	RESG (2) 0.574849D-C1	DDDD (3) 0.128777D-01	AG (4) 0.446072D-01	FFFF (5) 0.772975D-01	HHHH (2-3)/5 0.577085D 00	ACG (5-2)/3 0.153851D 01

XLCC	PKEY	PWIN	PGIN	EVAPCRATION	TRANSPARATION	QW	QG	PW	PG	SATURATION
FT.	AC.		PSI	LBM/SQ	FT-DY			PSI		CFT/CFT P.
0.0	5.	0.0	0.1470D 02	0.6569C-02	0.1131D 00	0.3439D 00	-0.1071D-02	-0.3175D 01	0.1471D 02	0.8782D 00
1.00	1.	0.0	0.0	0.0	0.2321D-01	-0.2321D-01	0.0	-0.5075D 01	0.1480D 02	0.7991D 00
2.00	1.	0.0	0.0	0.0	-0.1008D-01	0.1008D-01	0.0	-0.5152D 01	0.1486D 02	0.7904D 00
3.00	1.	0.0	0.0	0.0	-0.1969D-01	0.1969D-01	0.0	-0.4866D 01	0.1494D 02	0.8031D 00
4.00	1.	0.0	0.0	0.0	-0.1650D-01	0.1650D-01	0.0	-0.4494D 01	0.1502D 02	0.8207D 00
5.00	1.	0.0	0.0	0.0	-0.1830D-01	0.1830D-01	0.0	-0.4084D 01	0.1511D 02	0.8343D 00
6.00	1.	0.0	0.0	0.0	-0.1045D-01	0.1045D-01	0.0	-0.3702D 01	0.1520D 02	0.8450D 00
7.00	1.	0.0	0.0	0.0	-0.1202D-01	0.1202D-01	0.0	-0.3323D 01	0.1530D 02	0.8553D 00
8.00	1.	0.0	0.0	0.0	-0.3796D-02	0.3796D-02	0.0	-0.2975D 01	0.1541D 02	0.8642D 00
9.00	4.	-0.6514D 01	0.1551D 02	0.0	-0.1098D-02	-0.9526D-02	0.7417D-03	-0.2621D 01	0.1552D 02	0.8711D 00

TIME1.LE.IT SETS FINAL=2. TIME2.LE.IT GOES TO 92 TO SET FINAL=2. TIME3 GIVES TIME LEFT AFTER TAPE IS WRITTEN.

TIME1 (SEC) = 132 TIME2 (SEC) = 132 TIME3 (SEC) = 126

RESTAR	IT	DELT	TIME	RCCT	POT.	LEAF	PCT.	SUPPLY	F.	POT.	EVAP	EVAPORATION	TRANSPARATION	CUM.EVAP.	CUM.TRAN.
NO.	NO.	CAY	CAY		PSI							LBM/DY-SQ.FT.		LBM	
61.	23.	15.000	300.62	-0.4844E 01	-0.5208E 01	0.3120E 02	0.1006E 01	0.7372E-02	0.4986E-01	0.2174E 01	0.1617E 03				
62.	15.	15.000	315.62	-0.3567E 01	-0.4357E 01	0.3137E 02	0.1083E 01	0.7883E-02	0.5332E-01	0.2292E 01	0.1625E 03				

MATERIAL BALANCE RESULTS

W. PHASE	AAAA (1) 0.758457D C1	RESW (2) 0.245382D C3	CCCC (3) 0.380376D 02	AW (4) 0.207345D 03	EEEE (5) 0.215355D 03	GGGG (2-3)/5 0.962802D 00	ACW (5-2)/3 -0.789398D 00
NCA W. PHASE	BPBB (1) -0.441952C-C2	RESG (2) 0.429135C-01	DDDD (3) 0.194117D-02	AG (4) 0.489723D-01	FFFF (5) 0.772975D-01	HHHH (2-3)/5 0.530080D 00	ACG (5-2)/3 0.177131D 02

XLCC	PKEY	PWIN	PGIN	EVAPORATION	TRANSPARATION	QW	QG	PW	PG	SATURATION
FT.	AC.		PSI	LBM/SQ	FT-DY			PSI		CFT/CFT P.
0.0	5.	0.0	0.1470D 02	0.7883C-02	0.2091D 00	0.3905D 00	-0.8364D-03	-0.4881D 00	0.1470D 02	0.9337D 00
1.00	1.	0.0	0.0	0.0	0.1081D 00	-0.1081D 00	0.0	-0.2431D 01	0.1488D 02	0.8941D 00
2.00	1.	0.0	0.0	0.0	-0.8745D-02	0.8745D-02	0.0	-0.3201D 01	0.1499D 02	0.8697D 00
3.00	1.	0.0	0.0	0.0	-0.4979D-01	0.4979D-01	0.0	-0.3364D 01	0.1508D 02	0.8619D 00
4.00	1.	0.0	0.0	0.0	-0.4927D-01	0.4927D-01	0.0	-0.3260D 01	0.1516D 02	0.8628D 00
5.00	1.	0.0	0.0	0.0	-0.6035D-01	0.6035D-01	0.0	-0.3035D 01	0.1524D 02	0.8674D 00
6.00	1.	0.0	0.0	0.0	-0.3617D-01	0.3617D-01	0.0	-0.2840D 01	0.1532D 02	0.87C5D 00
7.00	1.	0.0	0.0	0.0	-0.4237D-01	0.4237D-01	0.0	-0.2624D 01	0.1540D 02	0.8743D 00
8.00	1.	0.0	0.0	0.0	-0.1336D-01	0.1336D-01	0.0	-0.2504D 01	0.1548D 02	0.8753D 00
9.00	4.	-0.6261D 01	0.1556D 02	0.0	-0.3870D-02	-0.3673D-01	0.5418D-03	-0.2364D 01	0.1557D 02	0.8768D 00

TIME1.LE.IT SETS FINAL=2. TIME2.LE.IT GOES TO 92 TO SET FINAL=2. TIME3 GIVES TIME LEFT AFTER TAPE IS WRITTEN.

TIME1 (SEC) = 126 TIME2 (SEC) = 126 TIME3 (SEC) = 110

RESTAR	IT	DELT	TIME	RCCT	FCT.	LEAF	PCT.	SUPPLY	F.	POT.	EVAP	EVAPORATION	TRANSPARATION	CUM.EVAP.	CUM.TRAN.
NO.	NO.	CAY	CAY		PSI							LBM/DY-SQ.FT.		LBM	

63. 18. 15.000 330.62 -0.3288E 01 -0.3210E 01 0.3162E 02 0.8952E 00 0.6529E-02 0.4417E-01 0.2496E 01 0.1639E 03
 64. 20. 15.000 345.62 -0.2565E 01 -0.2888E 01 0.3162E 02 0.8952E 00 0.6529E-02 0.4417E-01 0.2496E 01 0.1639E 03

MATERIAL BALANCE RESULTS

	AAAA (1)	RESW (2)	CCCC (3)	AW (4)	EEEE (5)	GGGG (2-3)/5	ACW (5-2)/3
W. PHASE	0.6273280 C1	0.2533250 C3	0.5054470 02	0.2023800 03	0.2153550 03	0.9397510 00	-0.7453140 00
	PPPP (1)	RESG (2)	DDDD (3)	AG (4)	FFFF (5)	HMMM (2-3)/5	ACG (5-2)/3
NCA W. PHASE	-0.2805610-C2	0.3333380-C1	-0.4040270-02	0.3737410-01	0.7729750-01	0.4835100 00	-0.1088140 02

XLCC FT.	PKEY NC.	PWIN PSI	PGIN	EVAPCRATICN LBM/SQ FT-DY	TRANSPIRATION	QW	QG	PW PSI	PG	SATURATION CFT/CFT P.
0.0	5.	0.0	0.14700 02	0.65290-02	0.19460 00	0.35230 00	-0.61610-03	0.47310 00	0.14700 02	0.94740 00
1.00	1.	0.0	0.0	0.0	0.12010 00	-0.12010 00	0.0	-0.10520 01	0.14930 02	0.91910 00
2.00	1.	0.0	0.0	0.0	0.73700-02	-0.73700-02	0.0	-0.15800 01	0.15050 02	0.90690 00
3.00	1.	0.0	0.0	0.0	-0.39150-01	0.39150-01	0.0	-0.17270 01	0.15160 02	0.90230 00
4.00	1.	0.0	0.0	0.0	-0.47890-01	0.47890-01	0.0	-0.17020 01	0.15260 02	0.90100 00
5.00	1.	0.0	0.0	0.0	-0.66580-01	0.66580-01	0.0	-0.16150 01	0.15350 02	0.90090 00
6.00	1.	0.0	0.0	0.0	-0.44030-01	0.44030-01	0.0	-0.16060 01	0.15430 02	0.89950 00
7.00	1.	0.0	0.0	0.0	-0.55900-01	0.55900-01	0.0	-0.16230 01	0.15510 02	0.89770 00
8.00	1.	0.0	0.0	0.0	-0.18720-01	0.18720-01	0.0	-0.17890 01	0.15590 02	0.89230 00
9.00	4.	-0.58430 01	0.15650 02	0.0	-0.58520-02	-0.78850-01	0.42880-03	-0.19410 01	0.15660 02	0.88600 00

TIME1.LE.IT SETS FINAL=2. TIME2.LE.IT GCS TO 92 TO SET FINAL=2. TIME3 GIVES TIME LEFT AFTER TAPE IS WRITTEN.

TIME1 (SEC) = 104 TIME2 (SEC) = 104 TIME3 (SEC) = 96

RESTAR NO.	IT NC.	DELT CAY	TIME CAY	RCOT PCT. PSI	LEAF PCT.	SUPPLY F.	POT. EVAP LBM/DY-SQ.FT.	EVAPORATION	TRANSPIRATION	CUM.EVAP. LBM	CUM.TRAN.
65.	13.	15.000	360.62	-0.2191E 01	-0.2565E 01	0.3169E 02	0.1042E 01	0.7562E-02	0.5117E-01	0.2609E 01	0.1646E 03
66.	10.	15.000	375.62	-0.1916E 01	-0.2338E 01	0.3174E 02	0.1178E 01	0.8523E-02	0.5768E-01	0.2737E 01	0.1655E 03

MATERIAL BALANCE RESULTS

	AAAA (1)	RESW (2)	CCCC (3)	AW (4)	EEEE (5)	GGGG (2-3)/5	ACW (5-2)/3
W. PHASE	0.4642880 C1	0.2568820 03	0.6047780 02	0.1964650 03	0.2153550 03	0.9120030 00	-0.6866500 00
	PPPP (1)	RESG (2)	DDDD (3)	AG (4)	FFFF (5)	HMMM (2-3)/5	ACG (5-2)/3
NCA W. PHASE	-0.6044830-C3	0.2900200-C1	-0.5614600-02	0.3461660-01	0.7729750-01	0.4478360 00	-0.8601770 01

XLCC FT.	PKEY NC.	PWIN PSI	PGIN	EVAPCRATICN LBM/SQ FT-DY	TRANSPIRATION	QW	QG	PW PSI	PG	SATURATION CFT/CFT P.
0.0	5.	0.0	0.14700 02	0.85230-02	0.17470 00	0.30900 00	-0.41490-03	0.73300 00	0.14700 02	0.95080 00
1.00	1.	0.0	0.0	0.0	0.11710 00	-0.11710 00	0.0	-0.49500 00	0.14950 02	0.92890 00
2.00	1.	0.0	0.0	0.0	0.15150-01	-0.15150-01	0.0	-0.84920 00	0.15090 02	0.91990 00
3.00	1.	0.0	0.0	0.0	-0.26920-01	0.26920-01	0.0	-0.89450 00	0.15200 02	0.91700 00
4.00	1.	0.0	0.0	0.0	-0.38870-01	0.38870-01	0.0	-0.81940 00	0.15300 02	0.91660 00
5.00	1.	0.0	0.0	0.0	-0.59350-01	0.59350-01	0.0	-0.73930 00	0.15390 02	0.91620 00
6.00	1.	0.0	0.0	0.0	-0.41880-01	0.41880-01	0.0	-0.75680 00	0.15490 02	0.91420 00
7.00	1.	0.0	0.0	0.0	-0.56390-01	0.56390-01	0.0	-0.85890 00	0.15570 02	0.91070 00
8.00	1.	0.0	0.0	0.0	-0.19740-01	0.19740-01	0.0	-0.11540 01	0.15650 02	0.90380 00
9.00	4.	-0.54120 01	0.15710 02	0.0	-0.62010-02	-0.11040 00	0.37460-03	-0.14990 01	0.15730 02	0.89600 00

TIME1.LE.IT SETS FINAL=2. TIME2.LE.IT GCS TO 92 TO SET FINAL=2. TIME3 GIVES TIME LEFT AFTER TAPE IS WRITTEN.

TIME1 (SEC) = 96 TIME2 (SEC) = 96 TIME3 (SEC) = 87

RESTAR NO.	IT NC.	DELT CAY	TIME CAY	RCOT PCT. PSI	LEAF PCT.	SUPPLY F.	POT. EVAP LBM/DY-SQ.FT.	EVAPORATION	TRANSPIRATION	CUM.EVAP. LBM	CUM.TRAN.
67.	6.	15.000	390.62	-0.1787E 01	-0.2269E 01	0.3177E 02	0.1348E 01	0.9728E-02	0.6583E-01	0.2883E 01	0.1665E 03

MATERIAL BALANCE RESULTS

W. PHASE	AAAA (1) 0.306474D G1	RESW (2) 0.258383D 03	CCCC (3) 0.671410D 02	AW (4) 0.191242D 03	EEEE (5) 0.215355D 03	GGGG (2-3)/5 0.888032D 00	ACW (5-2)/3 -0.640862D 00
NCN W. PHASE	BBBB (1) -0.269915D-C3	RESG (2) 0.271520D-C1	DDDD (3) -0.614413D-02	AG (4) 0.332962D-01	FFFF (5) 0.772975D-01	HHHH (2-3)/5 0.430754D 00	ACG (5-2)/3 -0.816152D 01

XLOC FT.	PKEY NC.	PWIN PSI	PGIN	EVAPCRATICN LBM/SQ FT-DY	TRANSPARATION	QW	QG	PW	PG	SATURATION CFT/CFT P.
0.0	5.	0.0	0.1470D 02	0.1168D-01	0.1562D 00	0.2419D 00	-0.3356D-03	0.6291D 00	0.1470D 02	0.9496D 00
1.00	1.	0.0	0.0	0.0	0.1146D 00	-0.1146D 00	0.0	-0.3392D 00	0.1496D 02	0.9317D 00
2.00	1.	0.0	0.0	0.0	0.2119D-01	-0.2119D-01	0.0	-0.5882D 00	0.1509D 02	0.9246D 00
3.00	1.	0.0	0.0	0.0	-0.1727D-01	0.1727D-01	0.0	-0.5765D 00	0.1520D 02	0.9228D 00
4.00	1.	0.0	0.0	0.0	-0.3129D-01	0.3129D-01	0.0	-0.4701D 00	0.1531D 02	0.9228D 00
5.00	1.	0.0	0.0	0.0	-0.5168D-01	0.5168D-01	0.0	-0.3746D 00	0.1541D 02	0.9227D 00
6.00	1.	0.0	0.0	0.0	-0.3831D-01	0.3831D-01	0.0	-0.3845D 00	0.1551D 02	0.9207D 00
7.00	1.	0.0	0.0	0.0	-0.5341D-01	0.5341D-01	0.0	-0.4870D 00	0.1560D 02	0.9171D 00
8.00	1.	0.0	0.0	0.0	-0.1902D-01	0.1902D-01	0.0	-0.7749D 00	0.1568D 02	0.9103D 00
9.00	4.	-0.5011D 01	0.1574D 02	0.0	-0.6009D-02	-0.1128D 00	0.3176D-03	-0.1112D 01	0.1575D 02	0.9028D 00

TIME1.LE.IT SETS FINAL=2. TIME2.LE.IT GOES TO 92 TO SET FINAL=2. TIME3 GIVES TIME LEFT AFTER TAPE IS WRITTEN.

TIME1 (SEC) = 85 TIME2 (SEC) = 85 TIME3 (SEC) = 83

RESTAR NC.	IT NC.	DELT CAY	TIME CAY	RCOT PSI	PCT.	LEAF PCT.	SUPPLY F.	POT. EVAP LBM/DY-SQ.FT.	EVAPORATION	TRANSPARATION	CUM.EVAP. LBM	CUM.TRAN.
69.	10.	15.000	420.62	-0.1512E 01		-0.2139E 01	0.3182E 02	0.1761E 01	0.1268E-01	0.8579E-01	0.3240E 01	0.1689E 03
70.	28.	15.000	435.62	-0.2963E 01		-0.9285E 01	0.3162E 02	0.1976E 01	0.1422E-01	0.8649E 00	0.3453E 01	0.1819E 03

MATERIAL BALANCE RESULTS

W. PHASE	AAAA (1) -0.712057D 01	RESW (2) 0.255148D C3	CCCC (3) 0.635705D 02	AW (4) 0.191577D 03	EEEE (5) 0.215355D 03	GGGG (2-3)/5 0.889587D 00	ACW (5-2)/3 -0.625959D 00
NCN W. PHASE	BBBB (1) 0.611640D-02	RESG (2) 0.211892D-C1	DDDD (3) -0.464622D-03	AG (4) 0.316538D-01	FFFF (5) 0.772975D-01	HHHH (2-3)/5 0.409507D 00	ACG (5-2)/3 -0.992382D 02

XLOC FT.	PKEY NC.	PWIN PSI	PGIN	EVAPCRATICN LBM/SQ FT-DY	TRANSPARATION	QW	QG	PW	PG	SATURATION CFT/CFT P.
0.0	5.	0.0	0.1470D 02	0.1422D-01	0.4241D 00	0.2582D-01	-0.1559D-03	-0.2283D 01	0.1464D 02	0.9015D 00
1.00	1.	0.0	0.0	0.0	0.1982D 00	-0.1982D 00	0.0	-0.2380D 01	0.1484D 02	0.8961D 00
2.00	1.	0.0	0.0	0.0	0.9085D-01	-0.9085D-01	0.0	-0.2013D 01	0.1499D 02	0.9001D 00
3.00	1.	0.0	0.0	0.0	0.7727D-01	-0.7727D-01	0.0	-0.1596D 01	0.1515D 02	0.9049D 00
4.00	1.	0.0	0.0	0.0	0.5485D-01	-0.5485D-01	0.0	-0.1158D 01	0.1532D 02	0.9099D 00
5.00	1.	0.0	0.0	0.0	0.4877D-01	-0.4877D-01	0.0	-0.7364D 00	0.1551D 02	0.9142D 00
6.00	1.	0.0	0.0	0.0	0.1645D-01	-0.1645D-01	0.0	-0.3306D 00	0.1570D 02	0.9180D 00
7.00	1.	0.0	0.0	0.0	-0.1180D-01	0.1180D-01	0.0	0.1447D-03	0.1589D 02	0.9207D 00
8.00	1.	0.0	0.0	0.0	-0.2214D-01	0.2214D-01	0.0	0.1620D 00	0.1606D 02	0.9206D 00
9.00	4.	-0.3657D C1	0.1619D 02	0.0	-0.1166D-01	-0.4809D-01	0.5637D-03	0.2276D 00	0.1620D 02	0.9192D 00

TIME1.LE.IT SETS FINAL=2. TIME2.LE.IT GOES TO 52 TO SET FINAL=2. TIME3 GIVES TIME LEFT AFTER TAPE IS WRITTEN.

TIME1 (SEC) = 83 TIME2 (SEC) = 83 TIME3 (SEC) = 68

RESTAR NC.	IT NC.	DELT CAY	TIME CAY	RCOT PSI	PCT.	LEAF PCT.	SUPPLY F.	POT. EVAP LBM/DY-SQ.FT.	EVAPORATION	TRANSPARATION	CUM.EVAP. LBM	CUM.TRAN.
71.	32.	15.000	450.62	-0.4670E 01		-0.1693E 02	0.3134E 02	0.1770E 01	0.1279E-01	0.1677E 01	0.3645E 01	0.2070E 03
72.	16.	15.000	465.62	-0.5424E 01		-0.1640E 02	0.3118E 02	0.1526E 01	0.1110E-01	0.1502E 01	0.3811E 01	0.2295E 03

	AAAA (1)	RFSW (2)	CCCC (3)	AW (4)	EEEE (5)	GGGG (2-3)/5	ACW (5-21/3)
W. PHASE	-0.943974D 01	0.239553D 03	0.425723D 02	0.197021D 03	0.215355D 03	0.914864D 00	-0.569332D 00
	RFRF (1)	RESE (2)	DDDD (3)	AG (4)	FFFF (5)	HHHH (2-3)/5	ACG (5-21/3)
NCN W. PHASE	0.556286C-02	0.498154D-01	0.133431D-01	0.364723D-01	0.772975D-01	0.471844D 00	0.205965D 01

XLCC FT.	PKEY NC.	PWIN	PGIN PSI	EVAPCRATICA LBM/SQ FT-DY	TRANSPIRATION	QW	QG	PW	PG PSI	SATURATION CFT/CFT P.
0.0	5.	0.0	0.1470D 02	0.1110C-01	0.8030D 00	0.5076D-01	-0.5133D-03	-0.4632D 01	0.1470D 02	0.8292D 00
1.00	1.	0.0	0.0	0.0	0.1941D 00	-0.1941D 00	0.0	-0.4911D 01	0.1477D 02	0.8103D 00
2.00	1.	0.0	0.0	0.0	0.9043D-01	-0.9043D-01	0.0	-0.4518D 01	0.1486D 02	0.8272D 00
3.00	1.	0.0	0.0	0.0	0.9010D-01	-0.9010D-01	0.0	-0.4088D 01	0.1497D 02	0.8392D 00
4.00	1.	0.0	0.0	0.0	0.7330D-01	-0.7330D-01	0.0	-0.3643D 01	0.1509D 02	0.8512D 00
5.00	1.	0.0	0.0	0.0	0.7672D-01	-0.7672D-01	0.0	-0.3209D 01	0.1523D 02	0.8622D 00
6.00	1.	0.0	0.0	0.0	0.5635D-01	-0.5635D-01	0.0	-0.2740D 01	0.1538D 02	0.8717D 00
7.00	1.	0.0	0.0	0.0	0.6875D-01	-0.6875D-01	0.0	-0.2286D 01	0.1554D 02	0.8797D 00
8.00	1.	0.0	0.0	0.0	0.3541D-01	-0.3541D-01	0.0	-0.1733D 01	0.1572D 02	0.8900D 00
9.00	4.	-0.5066D 01	0.1552D 02	0.0	0.1349D-01	0.5055D-02	0.8841D-03	-0.1180D 01	0.1592D 02	0.8983D 00

TIME1.LE.IT SETS FINAL=2. TIME2.LE.IT GCES TO SET FINAL=2. TIME3 GIVES TIME LEFT AFTER TAPE IS WRITTEN.

TIME1 (SEC) = 57 TIME2 (SEC) = 57 TIME3 (SEC) = 51

RESTAR NC.	IT NC.	DELT DAY	TIME DAY	ROOT PCT. PSI	LEAF PCT.	SUPPLY F.	POT. EVAP LBM/DY-SQ.FT.	EVAPORATION	TRANSPIRATION	CUM.EVAP. LBM	CUM.TRAN.
73.	7.	15.000	480.62	-0.5643E 01	-0.1446E 02	0.3111E 02	0.1218E 01	0.8925E-02	0.1207E 01	0.3945E 01	0.2476E 03
74.	1.	15.000	455.62	-0.5637E 01	-0.1229E 02	0.3110E 02	0.9038E 00	0.6736E-02	0.9103E 00	0.4046E 01	0.2613E 03

MATERIAL BALANCE RESULTS

	AAAA (1)	RESW (2)	CCCC (3)	AW (4)	EEEE (5)	GGGG (2-3)/5	ACW (5-21/3)
W. PHASE	-0.174463D 01	0.236571D 03	0.351557D 02	0.201415D 03	0.215355D 03	0.935269D 00	-0.603471D 00
	RFRF (1)	RESE (2)	DDDD (3)	AG (4)	FFFF (5)	HHHH (2-3)/5	ACG (5-21/3)
NCN W. PHASE	0.348245C-02	0.535657D-01	0.201455D-01	0.334242D-01	0.772975D-01	0.432410D 00	0.117782D 01

XLCC FT.	PKEY NC.	PWIN	PGIN PSI	EVAPCRATICA LBM/SQ FT-DY	TRANSPIRATION	QW	QG	PW	PG PSI	SATURATION CFT/CFT P.
0.0	5.	0.0	0.1470D 02	0.6736D-02	0.7025D 00	0.7777D-01	-0.8171D-03	-0.4861D 01	0.1470D 02	0.8178D 00
1.00	1.	0.0	0.0	0.0	0.8830D-01	-0.8830D-01	0.0	-0.5157D 01	0.1479D 02	0.7944D 00
2.00	1.	0.0	0.0	0.0	0.1377D-01	-0.1377D-01	0.0	-0.4768D 01	0.1489D 02	0.8121D 00
3.00	1.	0.0	0.0	0.0	0.4856D-02	-0.4856D-02	0.0	-0.4340D 01	0.1499D 02	0.8289D 00
4.00	1.	0.0	0.0	0.0	0.1109D-01	-0.1109D-01	0.0	-0.3904D 01	0.1511D 02	0.8406D 00
5.00	1.	0.0	0.0	0.0	0.1538D-01	-0.1538D-01	0.0	-0.3469D 01	0.1525D 02	0.8518D 00
6.00	1.	0.0	0.0	0.0	0.1727D-01	-0.1727D-01	0.0	-0.3023D 01	0.1539D 02	0.8630D 00
7.00	1.	0.0	0.0	0.0	0.2794D-01	-0.2794D-01	0.0	-0.2572D 01	0.1555D 02	0.8717D 00
8.00	1.	0.0	0.0	0.0	0.2057D-01	-0.2057D-01	0.0	-0.2053D 01	0.1572D 02	0.8814D 00
9.00	4.	-0.5395D 01	0.1550D 02	0.0	0.8564D-02	0.5052D-02	0.1049D-02	-0.1527D 01	0.1590D 02	0.8908D 00

TIME1.LE.IT SETS FINAL=2. TIME2.LE.IT GCES TO SET FINAL=2. TIME3 GIVES TIME LEFT AFTER TAPE IS WRITTEN.

TIME1 (SEC) = 50 TIME2 (SEC) = 50 TIME3 (SEC) = 47

RESTAR NC.	IT NC.	DELT DAY	TIME DAY	ROOT PCT. PSI	LEAF PCT.	SUPPLY F.	POT. EVAP LBM/DY-SQ.FT.	EVAPORATION	TRANSPIRATION	CUM.EVAP. LBM	CUM.TRAN.
75.	3.	15.000	510.62	-0.5679E 01	-0.1201E 02	0.3109E 02	0.8537E 00	0.6409E-02	0.8658E 00	0.4142E 01	0.2743E 03
76.	3.	15.000	525.62	-0.5751E 01	-0.1171E 02	0.3107E 02	0.7973E 00	0.6036E-02	0.8150E 00	0.4233E 01	0.2865E 03

MATERIAL BALANCE RESULTS

