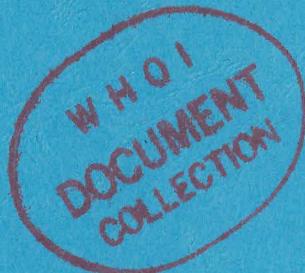
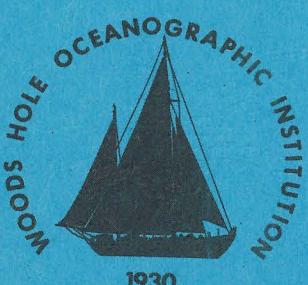


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Woods Hole Oceanographic Institution



ATLANTIS-II (CRUISE 102) MOORED AND SHIPBOARD SURFACE METEOROLOGICAL MEASUREMENTS DURING JASIN 1978

by

Melbourne G. Briscoe, Carol A. Mills,
Richard E. Payne, and Kenneth R. Peal

December 1979

TECHNICAL REPORT

*Prepared for the National Science Foundation
under Grants OCE77-25803 and OCE76-80174, and
for the Office of Naval Research under Contract
Contract N00014-76-C-0197; NR 083-400.*

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WOODS HOLE OCEANOGRAPHIC INSTITUTION
Woods Hole, Massachusetts 02543

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Valentine Worthington, Chairman
Department of Physical Oceanography

ABSTRACT

During cruise 102 of the R/V Atlantis-II in the Joint Air-Sea Interaction Project (JASIN), surface meteorological data were gathered by Woods Hole Oceanographic Institution personnel from two moored buoys and from the ship.

One buoy (JASIN W2/WHOI 651) carried a Vector Averaging Wind Recorder (VAWR) and a Vector Measuring Wind Recorder (VMWR); these instruments provided 18 days of intercomparison data and 38 days of meteorological data from 30 July to 6 September 1978. The other buoy (JASIN H2) carried a VMWR and gave 25 total days of data from 16 July to 10 August, and from 26 August to 1 September.

A PET computer, hardwired to sensors positioned on the ship, displayed data that were logged during both legs of the cruise. Manual data were gathered by the science watches.

This report describes the PET system, and displays and compares all the data. VAWR hourly meteorological data are listed for the 38 day period.

Scientific interpretation of these data, such as calculations of heat fluxes, will be published separately.

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INTRODUCTION

The Joint Air-Sea Interaction Project (JASIN; see Pollard, 1978) was an international study of the atmospheric and oceanic boundary layers, of the fluxes within and between them, and of their interaction on the process scale. Nine countries, fourteen ships, and four aircraft participated in the main field experiment from mid-July to mid-September 1978 in an area northwest of Scotland about half-way to Iceland (see Figure I-1).

The R/V Atlantis-II participated as its Cruise 102 with two legs:

Leg 1: Glasgow - Glasgow, 25 July - 16 August

Leg 2: Glasgow - Woods Hole, 21 August - 21 September

The latter part of Leg 1 and the early part of Leg 2 were spent in CTD work at Anton Dohrn Seamount, and the last two weeks of Leg 2 were spent in passage across the North Atlantic. The actual working periods in the central JASIN area, i.e. the vicinity of the Fixed Intensive Array (FIA) near 59°N, 12°30'W, were: 0600Z/27 July to 2400Z/13 August, and 0700Z/24 August to 1400Z/7 September.

During these periods near the FIA, surface meteorological observations were made from the Atlantis-II using a mix of automatic and manually-operated sensors. The automatic system, called PET here because a small PET computer was used as a data acquisition device, are described in Part II of this report. The PET data were logged approximately hourly by the science watch since the 5-minute automatic recording system was not working. The science watch also took certain observations manually, called MANUAL here, on an hourly or 4-hourly (Leg 1) or 3-hourly (Leg 2) basis, depending on the observation. Figure I-2 locates the observations on the ship.

The PET and MANUAL observations from the ship were meant primarily as backup data in case the meteorological data being recorded on buoy W2 (see Figures I-1 and I-3, and Table I-1) were faulty. The meteorological package (Payne, 1974) was a Vector Averaging Wind Recorder. Only the PET Dew Point and the MANUAL Dew Point and Relative Humidity (calculated from wet and dry bulb temperatures; see PSYCHROMETRY section below) were unique observations from the ship; all the other shipborne meteorological data were redundant to buoy data, called BUOY here. Additional data on wind measurements only were obtained from a Vector Measuring Wind Recorder on buoy H2 and supplement the W2 data by starting earlier.

We expect all the buoy data, but especially wind speed and air pressure and temperature, to be of higher quality than the same data from the ship because of the derogatory influence the ship has on its environment. Also, the motivation for these measurements is as supporting data for the array of current meters and thermistors deployed on the moorings in the FIA, so observations from mooring W2 are in any case preferable to those from a roving ship or from mooring H2. Figure I-4 and Table I-2 give the range and bearing from the Atlantis-II to buoy W2 (nominally 59°01.5'N, 12°33.0'W) during Legs 1 and 2; only during the Leg 1 periods 1600Z/2 August to 0500Z/3 August, 1600Z/8 August to 0400Z/9 August, and 1100-2400Z/9 August was the ship consistently within 10 km of the buoy and were there meteorological measurements being made on the ship. These are the periods used for the ship-to-buoy "10 km" scatterplots (see Table III-4, and figures III-35 to 38).

We present here the BUOY data in some detail, including hourly listings, spectra, statistics, etc. The PET and MANUAL dew point estimates from Leg 2 are compared in Figure III-12 and III-33; there seems to be no reason to choose one as preferable to the other except that the PET estimates are probably less subject to the change of the watch.

No derived data, for example wind stress or surface heat flux, are presented in this report. See also Tarbell, Briscoe, and Weller (1979) for the current meter data from the moorings, and Pennington and Briscoe (1979) for the hydrographic (CTD profiles) data.

OBSERVATIONS

The VAWR and VMWR data were handled as normal current-meter data (see Tarbell, et al., 1979) since both instruments are based on the original VACM and VMCM instruments. Figure I-3 shows buoy W2 on which the VAWR and one of the VMWR instruments were mounted; the H2 VMWR instruments were on a different kind of tower structure but were equally exposed and at about the same height. The W2 VAWR and VMWR were mounted 1 m apart at 3.5 m height above the water line. The vane on the buoy kept the two wind recorders on the upwind side of the buoy; there was free exposure of the wind sensors to the wind. Except for the air pressure sensor, the VAWR was as described in Payne (1974). A Digiquartz pressure sensor provided 0.1 mbar accuracy pressures averaged over the 15 minute recording interval of the VAWR. The VMWR was simply a VMCM turned upside down.

The PET data are described in Part II; see also Peal (1979).

The MANUAL data were taken with a variety of instruments. The winds used the ship's anemometer which was mounted on the port forward yardarm. It yielded (relative to the PET measurements) a diminished wind speed when the winds were from 090° relative, i.e. when the winds had to pass the mast to get to the anemometer. More surprisingly, the measurements were biased high when the winds were from between 070 - 085° and 095 - 110°, apparently because of a funneling effect past the mast. The winds were read on an analog dial (one minute visual average) in the wet lab. Ship speed was from the single-axis Sperry doppler log, which was the same instrument the PET was reading; only time of reading and the variability of visual averaging should produce differences between the PET and MANUAL ship speed. Similarly, the ship's gyro repeater provided ship heading. The MANUAL measurements of sea surface temperature came from a standard bucket thermometer. During Leg 1 the bucket was stored in the main lab and consequently was biased high; for most of Leg 2 the bucket was stored on deck. Air pressure came from an aneroid barometer on the bridge; it was of unknown calibration, but presumably would have only an offset. (It proved to be reading 8.5 mbar high, by correlation comparison with the pressure sensor on the buoy.)

The wet and dry bulb air temperatures were obtained with a Bendix 566-3 Psychron, which is a motor aspirated pair of mercury thermometers, one with a wetted wick, one without. It was used on the exposed side of the bridge wing

or the flying bridge, depending on the severity of the weather. The calculations of dew point and relative humidity were made using algorithms described below, under PSYCHROMETRY. All MANUAL data were logged by hand on an hourly (wind, sea temperature) or four-hourly (Leg 1: wet and dry bulb temperatures, clouds, air pressure, visual wave observations) or three-hourly (Leg 2) basis. The cloud and wave observations are not reported here: they are subjective visual estimates for the JASIN meteorological reporting forms only.

Editing of all three data sets (MANUAL, PET, BUOY) was done by hand; values clearly in error were replaced by a linear interpolation of adjacent points.

Calibrations

None of the ship's sensors were specially calibrated: the ship speed and direction, wind speed and direction, and bridge barometer were simply used as provided. The sea temperature (bucket with integral mercury thermometer) and wet and dry bulb temperatures used precision thermometers but no additional checks were made.

The PET sensors were calibrated as described in Part II of this report.

The VAWR sensors were calibrated as described in Payne (1974) except for the new pressure sensor, which was checked ashore against a mercury barometer. The cups and vane used the existing calibrations, and the temperature sensors were checked before and after the cruise in the WHOI calibration facility.

Note that the solar radiation values are presented in cal cm^{-2} ; in fact, these are values integrated over the 15 minute recording interval of the VAWR and normalized to 1 minute values, so the units should be interpreted as $\text{cal cm}^{-2} \text{ min}^{-1}$, which is the old (prior to 1947) definition of a langley. For reference,

$$\begin{aligned} 1 \text{ cal cm}^{-2} (\text{units on plots}) &= 1 \text{ cal cm}^{-2} \text{ min}^{-1} \\ &= 1 \text{ langley (old)} \\ &= 1 \text{ langley min}^{-1} (\text{new}) \\ &= 697.6 \text{ watts m}^{-2} \end{aligned}$$

CALCULATIONS

All calculations and displays were made on a Xerox Sigma-7 computer. In general, the data displayed here were analyzed with standard programs used for current meter data; see Tarbell, et al. (1979) for detail of the procedures. Brief descriptions follow.

Time Series

All the measured variables as well as some derived quantities (true wind, dew point, relative humidity) are presented versus time in Part III. In addition, the buoy winds (Fig. III-7) are presented as stick plots, i.e. 4-hour average vectors whose length is proportional to the wind speed and whose angle shows the wind direction as the direction to which the wind is blowing. Note that 6520SB and 6520WD are on the same buoy (JASIN W2), but that H2S1B and H2S2B are on JASIN H2, 44 km to the north of W2.

Histograms

Each of the variables from the VAWR are shown as frequency of occurrence versus amplitude; the means over the entire record are marked.

Statistics

Various moments (mean, variance and standard deviation, skewness, kurtosis) and extreme values are given for the entirety of each record (Table III-1) and for consecutive 5-day periods (Table III-2) commencing with 0000Z on 30 July; the final "5-day period" is only 4 days and 7 hours long.

Spectra

The spectra are calculated by breaking the record into one or two equal length segments (as long as possible to fit into the record length), and then frequency - band averaging over 3 bands to give a little more statistical reliability to the estimates. The plotting program additionally averages increasing larger groups of estimates together at the higher frequencies. The spectra therefore have a minimum of 6 degrees of freedom at the lowest frequencies, and as many as several hundred degrees of freedom at the highest frequencies. There was no data windowing or prewhitening prior to the Fourier transformation. The integral under the spectrum equals the variance of the record.

Progressive Vectors

The wind displacement vectors (one hour averages) are placed head-to-tail to show the path a perfect particle would have taken if the fluid were perfectly homogeneous with no spatial gradients. The same data are plotted as North versus East scatter plots with a regression line that denotes the principal axis of the cluster of points.

PSYCHROMETRY

Calculations of dew point and relative humidity were made using formulae from the Smithsonian Meteorological Tables (List, 1951). The lithium chloride cell used in the PET measurements (see Part II) read out directly in dew point; the wet and dry bulb temperatures of the Bendix psychrometer used in the MANUAL observations were therefore converted to dew point, for comparison with the lithium chloride cell, and to relative humidity, for general use.

The algorithm for calculation was:

1. Input T_w , T_d , p , where T_w = wet bulb temperature in degrees Celsius, T_d = dry bulb, and p = observed barometric pressure in millibars.
2. Calculate the saturation vapor pressure e_{sw} in mbar for the wet-bulb temperature:

$$e_{sw} = 1013.25 \times 10^{\frac{f(T_w + 273.16)}{10}} \quad (1)$$

$$\text{where } f(T) = a_1 \left(\frac{T_s}{T} - 1 \right) + a_2 \log_{10} \left(\frac{T_s}{T} \right) \quad (2)$$

$$+ a_3 \left(10^b \left(1 - \frac{T}{T_s} \right) - 1 \right)$$

$$+ a_4 \left(10^c \left(\frac{T_s}{T} - 1 \right) - 1 \right)$$

and $T_s = 373.16$, $a_1 = -7.90298$, $a_2 = 5.02808$,

$a_3 = -1.3816 \times 10^{-7}$, $a_4 = 8.1328 \times 10^{-3}$, $b = 11.344$,

and $c = 3.49149$.

3. Calculate the saturation vapor pressure for the dry-bulb temperature:

$$e_{sd} = 1013.25 \times 10^{\frac{f(T_d + 273.16)}{10}} \quad (3)$$

4. Calculate the mixing ratios for saturated air for the wet and dry-bulb temperatures:

$$r_{sw} = \xi \frac{e_{sw}}{p - e_{sw}} ; \quad r_{sd} = \xi \frac{e_{sd}}{p - e_{sd}} \quad (4)$$

where $\xi = 0.622$ is the ratio of the molecular weight of water to that of dry air; calculate the mixing ratio for the unsaturated air:

$$r = \frac{r_{sw} L - C_p (T_d - T_w)}{L + C_{pv} (T_d - T_w)} \quad (5)$$

where $L = 597.3 \text{ cal/gm}$ is the latent heat of evaporation, $C_p = 0.240 \text{ cal/(gm}^\circ\text{K)}$ is the specific heat of air at constant pressure, and $C_{pv} = 0.432 \text{ cal/(gm}^\circ\text{K)}$ is the specific heat of water vapor.

5. Calculate the relative humidity:

$$U = \frac{r}{r_{sd}} \times 100 \quad (6)$$

6. Calculate the vapor pressure for the unsaturated air:

$$e = \frac{r p}{\xi + r} \quad (7)$$

7. Using equation (1), iterate on the value of T_w until an e_{sw} is found that is equal to e from equation (7); this value of T_w is the dew point temperature.
8. For reference, because it is needed in the bulk aerodynamic flux formulae, the specific humidity is related to the mixing ratios by

$$q = \frac{r}{1+r}$$

so the specific humidity of the moist air is

$$q = \frac{r}{1+r} \quad (8)$$

where r comes from equation (5), and the specific humidity of the saturated air at the sea surface is

$$q_0 = \frac{r_{so}}{1+r_{so}} \quad (9)$$

where the r_{so} comes from equation (4) based on e_{so} from equation (1) evaluated at the sea surface temperature T_0 .

These calculations were checked against examples in the Smithsonian Meteorological Tables and (for relative humidity) against tables in the Instruction Manual (No. 509942, revised March 1968) for the Bendix Psychron.

RESULTS

The purpose of these meteorological measurements was to provide the background information needed for calculations of air-sea fluxes, especially of heat and momentum. The observations are of a kind that is appropriate for the use of bulk aerodynamic formulae (e.g., Bunker, 1976) for which the crucial variables are wind speed, sea and air temperatures, and the specific humidities for the moist air and for the saturated air at the sea surface.

The buoy measurements provide our best estimates of wind speed, sea and air temperatures, and the specific humidity at the sea surface. Since the buoy provides no moist air measurement, we have to use the shipborne measurement of dew point (PET) or wet bulb temperature (MANUAL) to supplement the data set.

The MANUAL measurements in general are noisy, only on a 4 or 3-hourly basis, and are more subjective than the other measurements. The uncalibrated aneroid barometer on the bridge was read by the mates on watch and reported verbally to the science watch. The bucket sea-surface temperatures have all the traditional problems with biases introduced by the storing temperature of the bucket, warming by the ship of the water around it when the ship is on station, and evaporative cooling of the water in the bucket while it is being read.

The PET measurements, except for dew point and incidentally ship speed and heading, provide no information that is unavailable from the buoy. For interest, the PET dew point temperature (Figures III-3 and 4) and the calculated MANUAL dew point temperature (Figures III-1b and 2b) are plotted together (Figure III-12) for Leg II of the cruise, and are given as a scatter plot (Figure III-33) that shows the regression line (MANUAL regressed on PET; Table III-4):

$$T_{\text{MANUAL}} = 0.581^{\circ}\text{C} + 0.945 \times T_{\text{PET}}$$

The standard error of the regression is only 0.5°C , hence it appears that the dew point temperature estimates from the ship are useful to something better than 1°C .

The scatter plots (Figures III-13 to 38) and regressions (Table III-4) display interesting comparisons between the various measurements of the same variable. Some of the comparisons are extraordinarily good, such as the pressure, dew point, and ship speed measurements (Figures III-32 to 34), whereas some are terrible, like BUOY versus MANUAL water temperature (Figure III-26) which is badly biased by the distance between the ship and the buoy (c.f., Figure I-4b). PET versus MANUAL water temperature (Figure III-27), both being made on the ship, compare better with only 0.22°C standard error.

The effect of separation between the buoy and the ship (PET) is minimized in the last four scatter plots, which are restricted to only the periods when the separation is less than 10 km. Unfortunately, these 10 km - plots cannot be directly compared to the other scatter plots because the 10 km - plots are for Leg 1, whereas all the other PET plots are for Leg 2.

A useful number is obtainable from the overall statistics of the BUOY record in Table III-1a. The mean solar radiation is given as $2783 \text{ watt-h m}^{-2}$; it has been normalized to one 24-hour day. In more usual units (divide by 24) the mean insolation during our measurements was

$$116 \text{ watts m}^{-2} = 0.17 \text{ langley (old)} = 0.17 \text{ langley (new) min}^{-1}.$$

For comparison, Bunker (1976) gives about 50 watts m^{-2} for this location for the net average annual radiational flux to the ocean, and a sensible heat flux

and latent heat flux from the ocean of about 30 watts m^{-2} and 135 watts m^{-2} respectively, for a net loss over the year of about 85 watts m^{-2} ; the imbalance in this budget is due to the averaging and contouring used by Bunker (1976), plus the necessity to obtain the numbers by reading small graphs.

ACKNOWLEDGEMENTS

We wish to thank Joe Poirier and Nancy Pennington for instrumental and data processing aspects of the VAWR data on W2, Bob Weller for providing the VMWR data from W2 and H2, and all those watchstanders who acquired the MANUAL and logged the PET data on the Atlantis-II. Sue Slagle is particularly thanked for her continuing, realtime assessment of the quality of the wind data. Nancy Pennington also was responsible for transmission of all the MANUAL and PET data into the computer, and did most of the editing.

This work was supported primarily by the National Science Foundation Grants OCE77-25803 and OCE76-80174 (for Part II), with help from the Office of Naval Research N00014-76-C-0197; NR 083-400.

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TABLE I-1

Summary of Mooring Locations and Dates

Mooring	Location (°N) (°W)	Cruise A-II-102 Date Set (1978)	Cruise A-II-102 Date Recovered (1978)	Purpose of Mooring	Comment
B1	59°00.4' 12°33.1'	1 Aug.	6 Sept.	meteorology thermistors chain	NOTE 1
B2	59°00.2' 12°27.5'	29 July	6 Sept.	thermistors chain	NOTE 1
B3	59°01.6' 12°27.4'	28 July	6 Sept.	thermistors chain	NOTE 1
B4	59°10.7' 12°31.0'	28 July	3 Sept.	thermistors chain	NOTE 1
W1	59°01.1' 12°32.0'	29 July	7 Sept.	subsurface currents	NOTE 2
W2	59°01.5' 12°33.0'	30 July	6 Sept.	meteorology surface currents	NOTE 2
W3	59°01.1' 12°34.3'	30 July	6 Sept.	spar buoy for surface currents	NOTE 2
K1	58°59.8' 12°30.6'	9 July	6 Sept.	subsurface currents	NOTE 3
H2	59°25.0' 12°30.0'	16 July	3 Sept.	meteorology and and surface currents	NOTE 4

- Notes:
1. Oregon State University buoys (W. Burt) deployed and recovered by the A-II.
 2. Woods Hole Oceanographic Institution buoys.
 3. Institut für Meereskunde, Kiel, F. R. Germany, buoy deployed by Meteor, recovered by Planet.
 4. NOAA/PMEL, Seattle, buoy (D. Halpern) deployed by Shackleton, recovered by A-II.

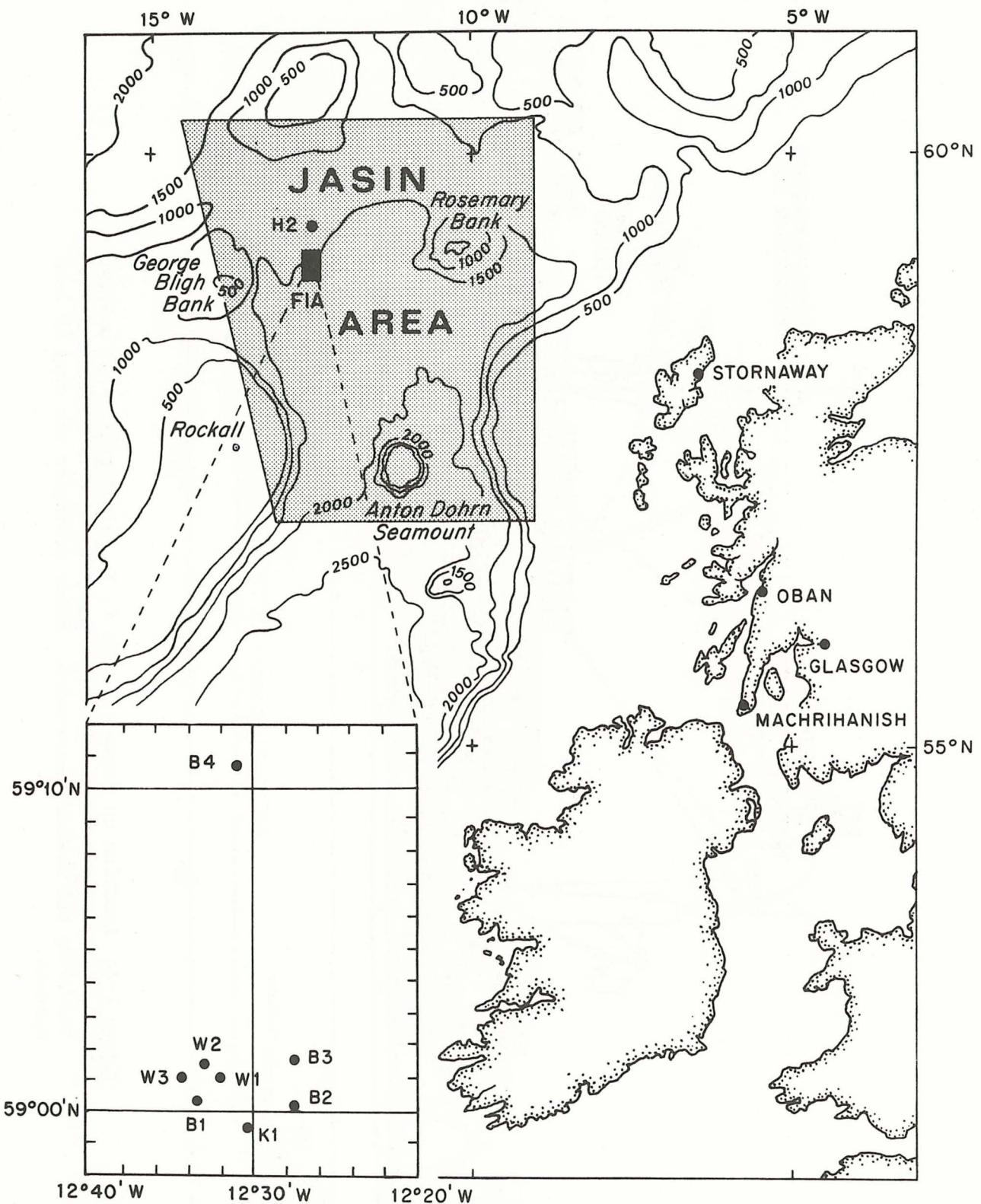


Figure I-1: Chart of the JASIN area. FIA means fixed intensive array, shown in detail at lower left. Glasgow was the main ship port, although Stornaway was also used. Oban was the communications center, and Machrihanish the airfield.

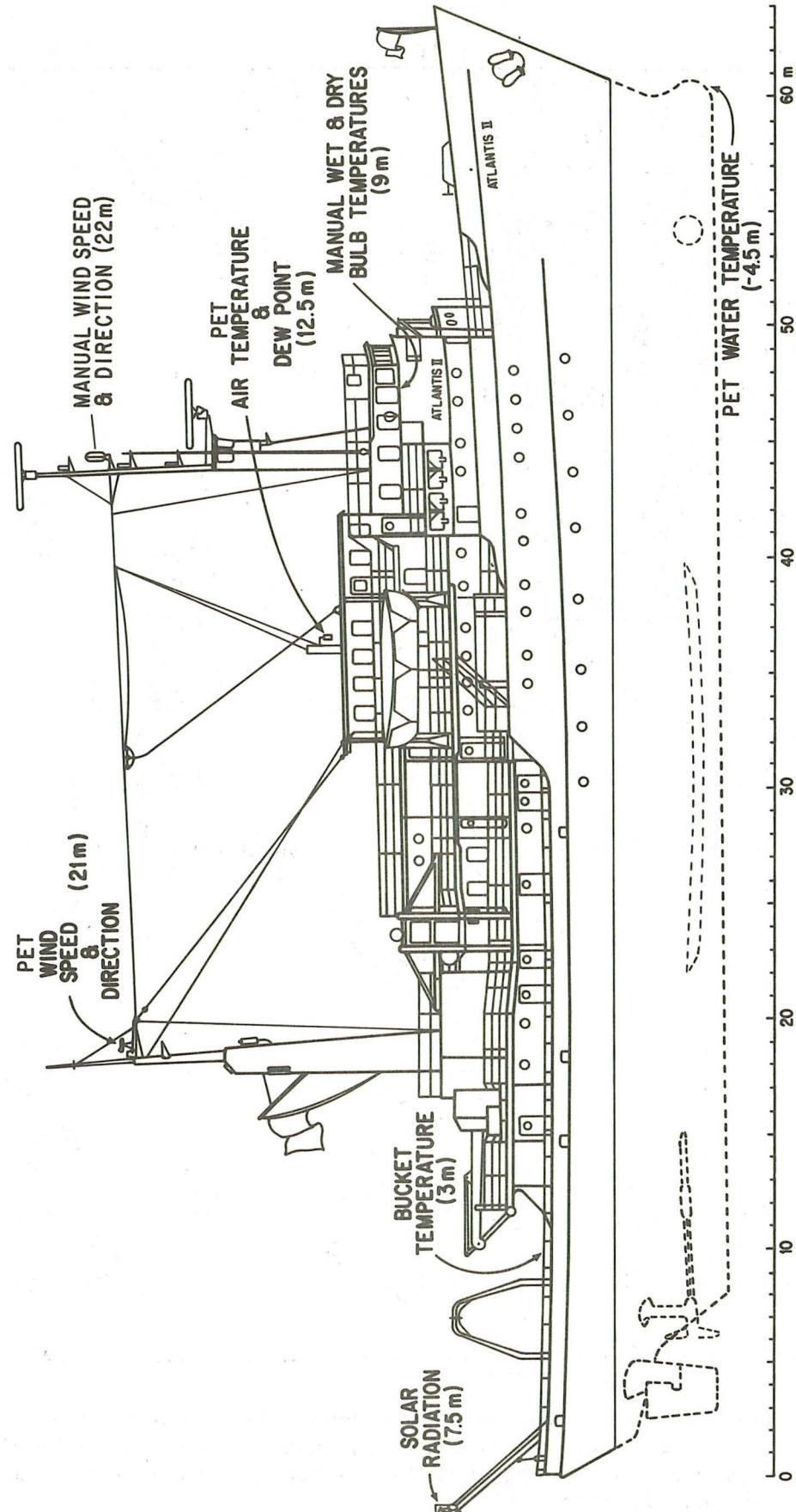


Figure I-2: Location of sensors on the R. V. Atlantis-II. PET means the computer-acquired data set, MANUAL means those data acquired by hand, including the bucket temperature. Solar radiation was read by both systems.

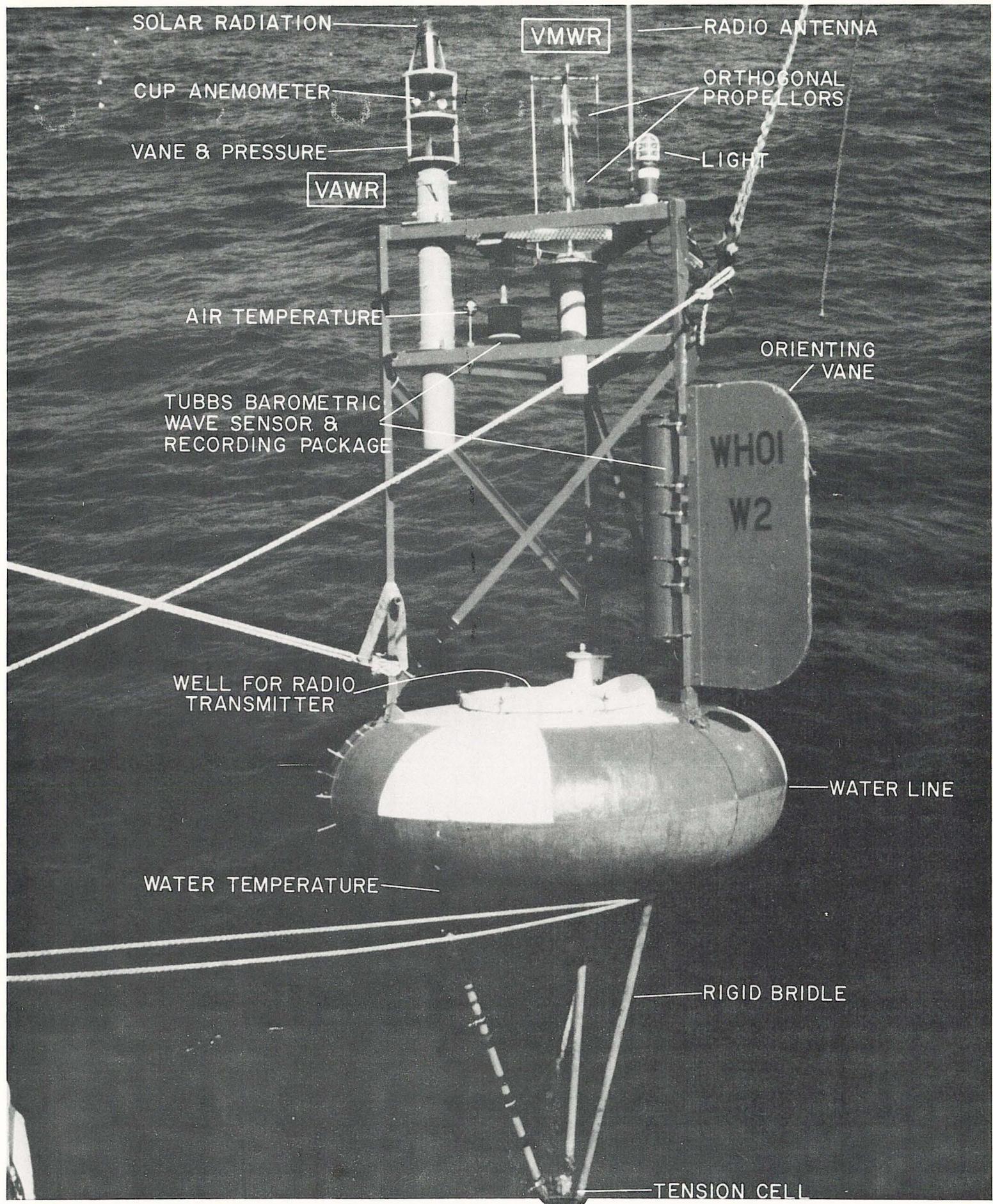


Figure I-3: Detail of buoy W2 and its meteorological sensors. The buoy is 2.4 m in horizontal diameter at its waterline; the wind sensors are at 3.5 m height, and the water temperature sensor is at 60 cm depth.

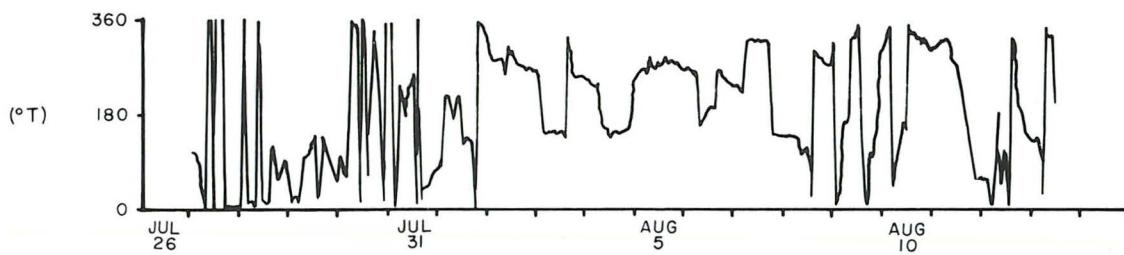
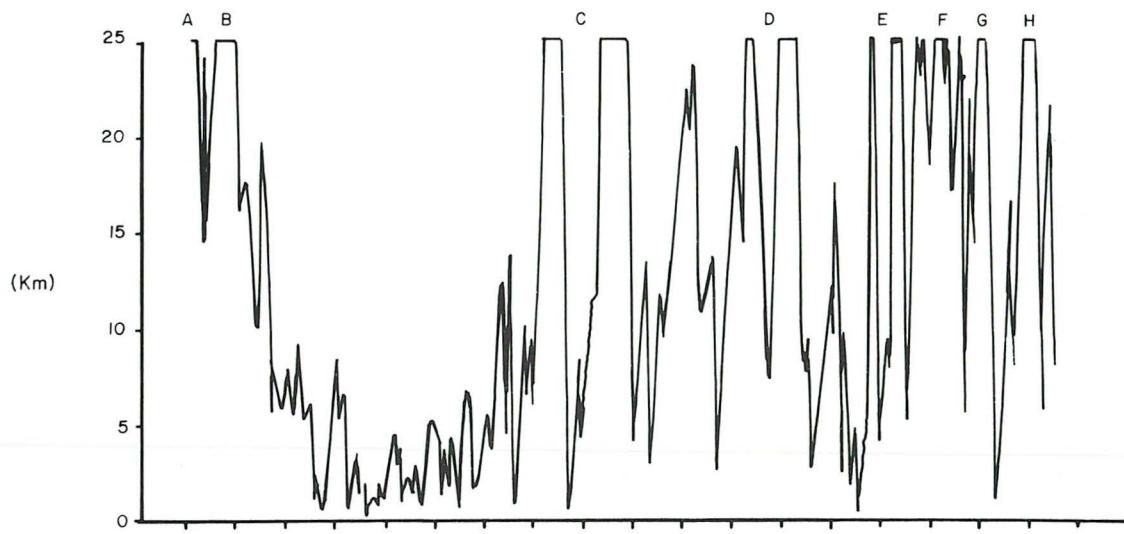


Figure I-4a: Range and bearing from ship to buoy W2.

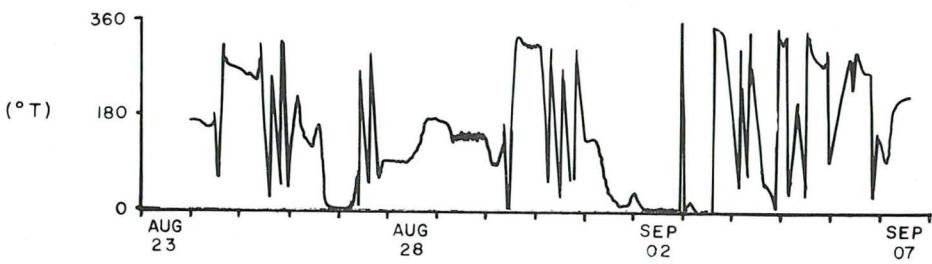
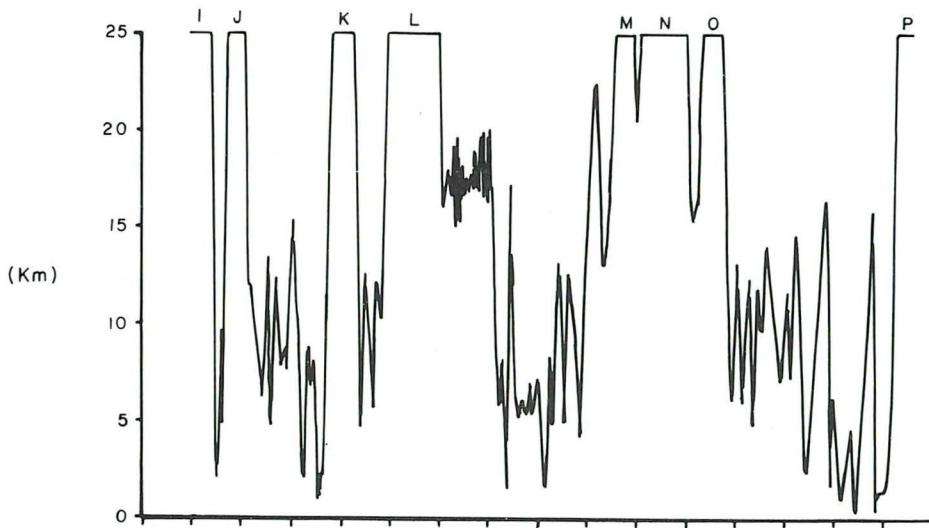


Figure I-4b: Range and bearing from ship to buoy W2.

Table I-2

Range and Bearing from Ship to Buoy W2

(Refers to Figure I-4a,b)

Leg 1

78-VII-26 to 78-VIII-15

- A Glasgow to JASIN site
- B B4 Deployment
- C VCM/3 tracking
- D CTD section (NW \rightarrow SE)
- E XBT section (S \rightarrow SE)
- F CTD section (SW of FIA*)
- G B4 area
- H CTD section (SE of FIA)

Leg 2

78-VIII-23 to 78-IX-08

- I Glasgow to JASIN site
- J CTD section (W of FIA)
- k CTD section (heading North)
- L CTD section (59°N W \rightarrow E)
- M H2 area
- N Multiship experiment (N of FIA)
- O B4 recovery
- P Returning to Woods Hole

* Fixed Intensive Array

PART II
PET SYSTEM

INTRODUCTION

The system provides continuous display and a digital record of several parameters relating to shipboard meteorology. It was designed for the Joint Air-Sea Interaction (JASIN) experiment and was used aboard the Atlantis II to supplement buoy-based recording systems. This report describes the sensors used and data collected during the JASIN cruise. However, the design of the system is such that it can support different sensors and other additional sources of data input in future applications.

The parameters measured by the system are as follows:

1. wind speed and direction
2. ship speed and heading
3. solar radiation
4. sea surface temperature
5. air temperature
6. dew point

Sensors are sampled and displayed several times per minute; six minute averages are recorded on digital tape*. During acquisition, steps are taken to remove the influence of the ship on the parameters being measured. For example, two wind sensors are installed, one on each side of the ship. The system selects data from the upwind sensor for use in true wind calculations. True wind is calculated using ship movement data in conjunction with the data from the selected wind sensor.

During the Atlantis II JASIN cruise, in addition to the nearby buoy measurements, extensive manual meteorological observations were taken on the ship. These served as a valuable reference for evaluation of and comparison with the automatically acquired data. Some of the data appear in Part III of this report.

* The recording system did not function during this test cruise of the prototype system.

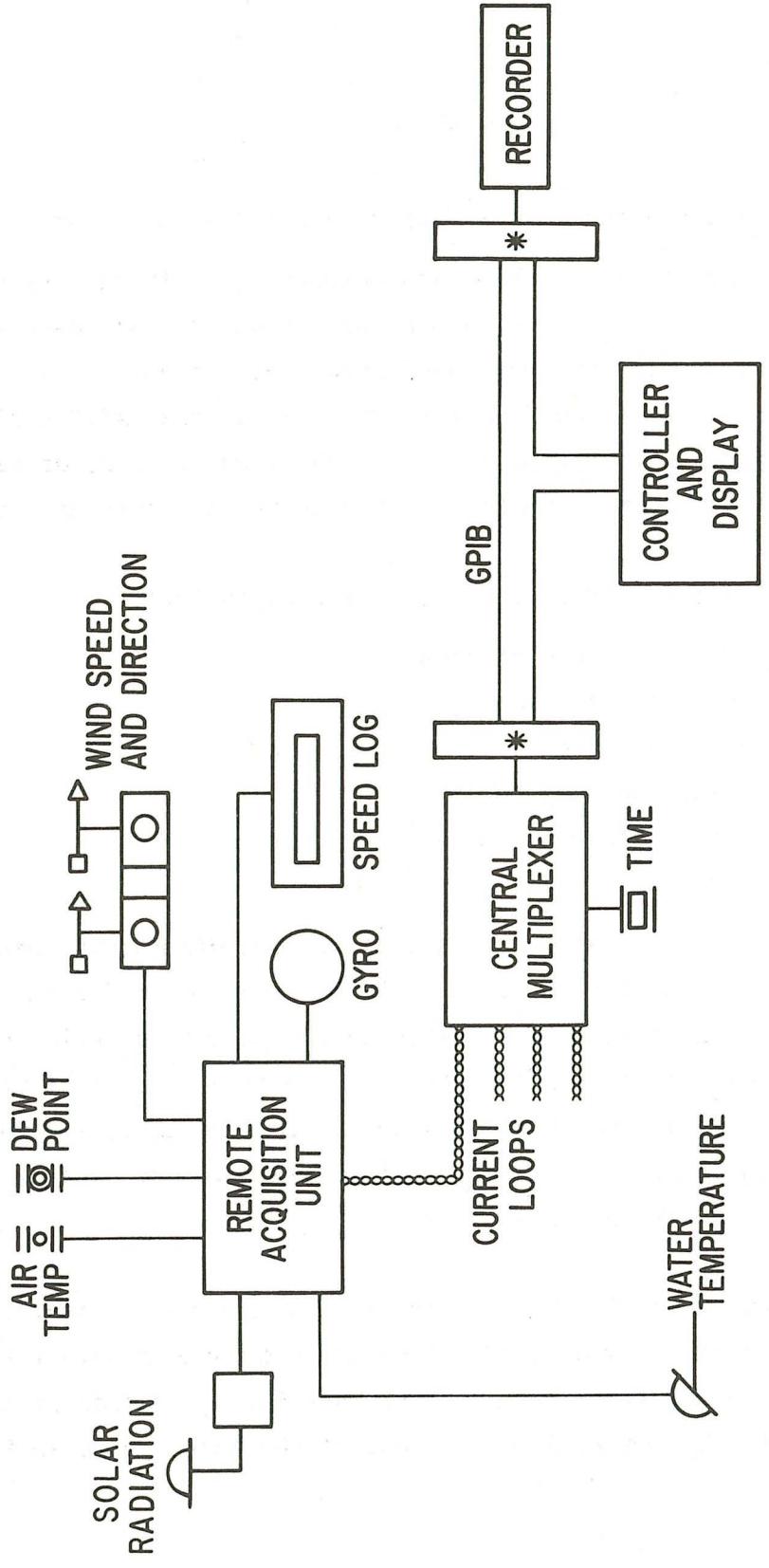


Figure II-1: Block diagram of meteorological data system.

SYSTEM SPECIFICATIONS

The system design described in Peal and Bradley (1978) is based on four main modules as follows (see Figure II-1):

- The remote acquisition unit converts the sensor outputs to digital values and sends the raw numbers to a central location.
- The central multiplexer performs the digital data transmission.
- The controller and display unit controls the data acquisition and recording, and converts the raw data to engineering units for display at the central location and for recording.
- The recorder stores the data for later analysis.

An important feature is the continuously updated display of the measured values converted to engineering units. The display (Figure II-2) is readily understood providing instant access to the data being recorded and verification of system operation.

Another important feature of the system is the ease with which it can transmit data to external devices. Thus, although this system has display and bulk storage capabilities, it can serve as a source of pre-processed real-time data for other systems aboard ship.

The system accuracy for DC inputs is determined by the analog-to-digital conversion in the remote acquisition unit. The conversion is performed by an Analog Devices 7507 multiplexer, a 581 J voltage reference,



Figure II-2: Live data display in main laboratory. Data being recorded are continuously updated.

and a 7550 converter at a clock rate of 614.4 KHz. Figure II-3 shows a calibration of this portion of the system.

This calibration does not apply to devices which are inherently digital since they are read into the system as digits. The ship speed log and gyrocompass are two such devices.

The system is capable of sampling all sensors as frequently as once per second. In this case, the following sample scheme is used:

- | | |
|------------------|---|
| every 30 seconds | - wind speed (both sensors)
- wind direction (both sensors)
- ship speed
- ship heading
- solar radiation (buffered raw output) |
| every 6 minutes | - sea surface temperature
- air temperature
- dew point. |

A tape record is written every 6 minutes and consists of:

- sequential record number
- time of day
- sea surface temperature
- air temperature
- dew point
- ship speed north and east (average of 12 values)
- wind speed relative to ship, forward and starboard beam vectors (average of 12 values)
- true wind speed north and east (average of 12 values)
- solar radiation (average of 12 values).

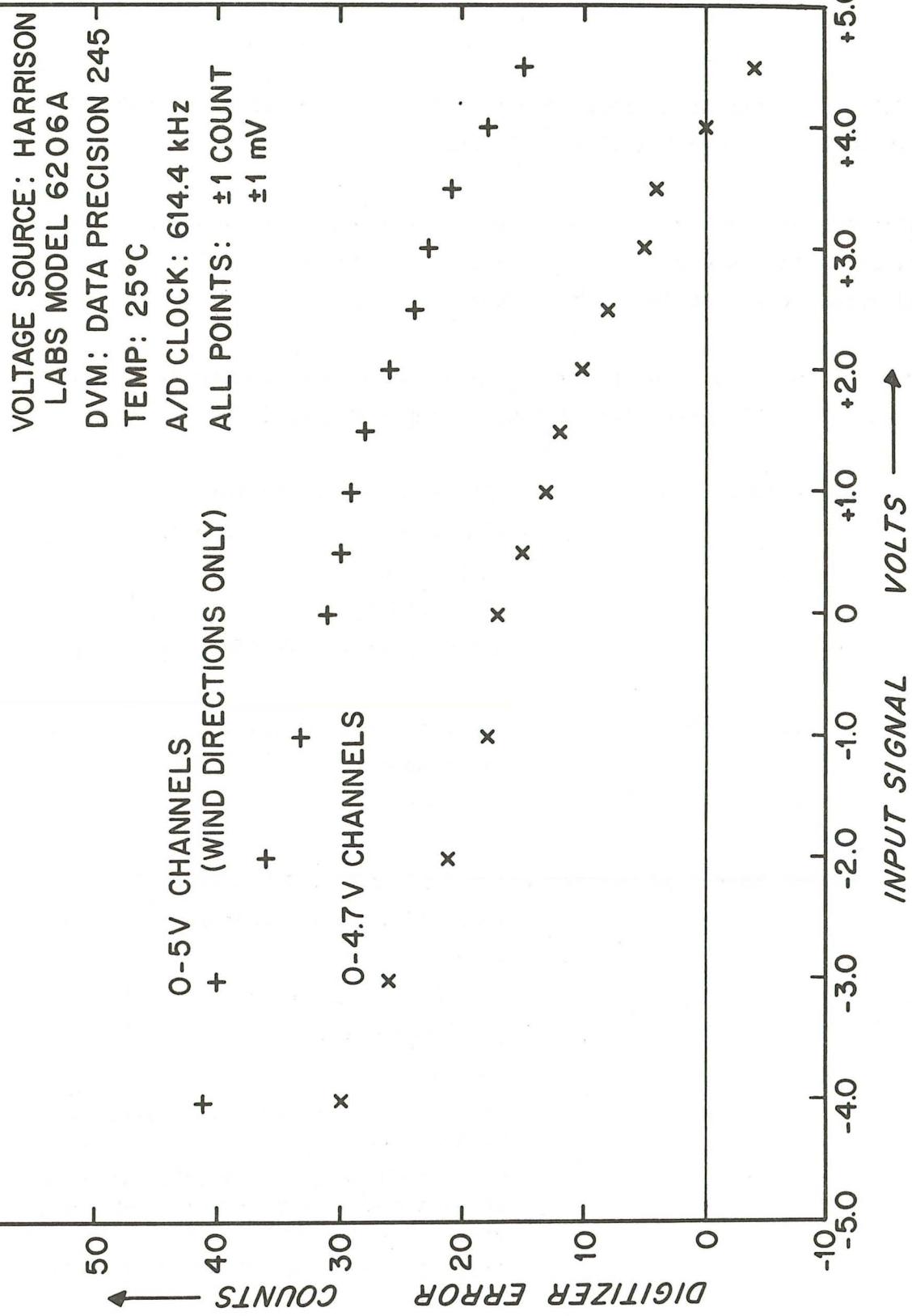


Figure II-3: Calibration of digitizer portion of system.

The data are recorded in a standard code on tape cartridges. In this case, each cartridge holds 468,800 bytes of data, requiring a new cartridge about every 12 days.

SYSTEM OPERATION

Prior to performing data acquisition, it is necessary to initialize the various modules of the system. This process is performed automatically by the control and display unit as a separate program under operator control. Once initialized, the remote acquisition units access all active sensors on a continuous basis. This ensures that current valid data is available for transmission to the central display location at all times.

To perform acquisition, the control and display unit continuously checks the current time of day against a pre-defined sensor acquisition schedule. When a given sensor is to be accessed, a command is sent to the remote acquisition unit which replies with its most recent value. The control display unit performs appropriate conversion and averaging calculations, then displays and records the value in engineering units.

SENSOR SPECIFICATIONS

This section provides specifications for each sensor as used in this system including conversion factors, ranges, accuracy, and response time. A summary is shown in Table II-1.

Wind speed and direction

The anemometer is a vortex counting speed sensor mounted in the tail of a vane which is free to rotate about a vertical axis. Two units are mounted, one on each side of the after mast catwalk approximately 21 meters above the ocean surface. The units are mounted well outboard on each side to minimize the effect of the ship on the wind measurement - see Figure II-4. In the calculation of true wind, the computer uses the data from the upwind anemometer.

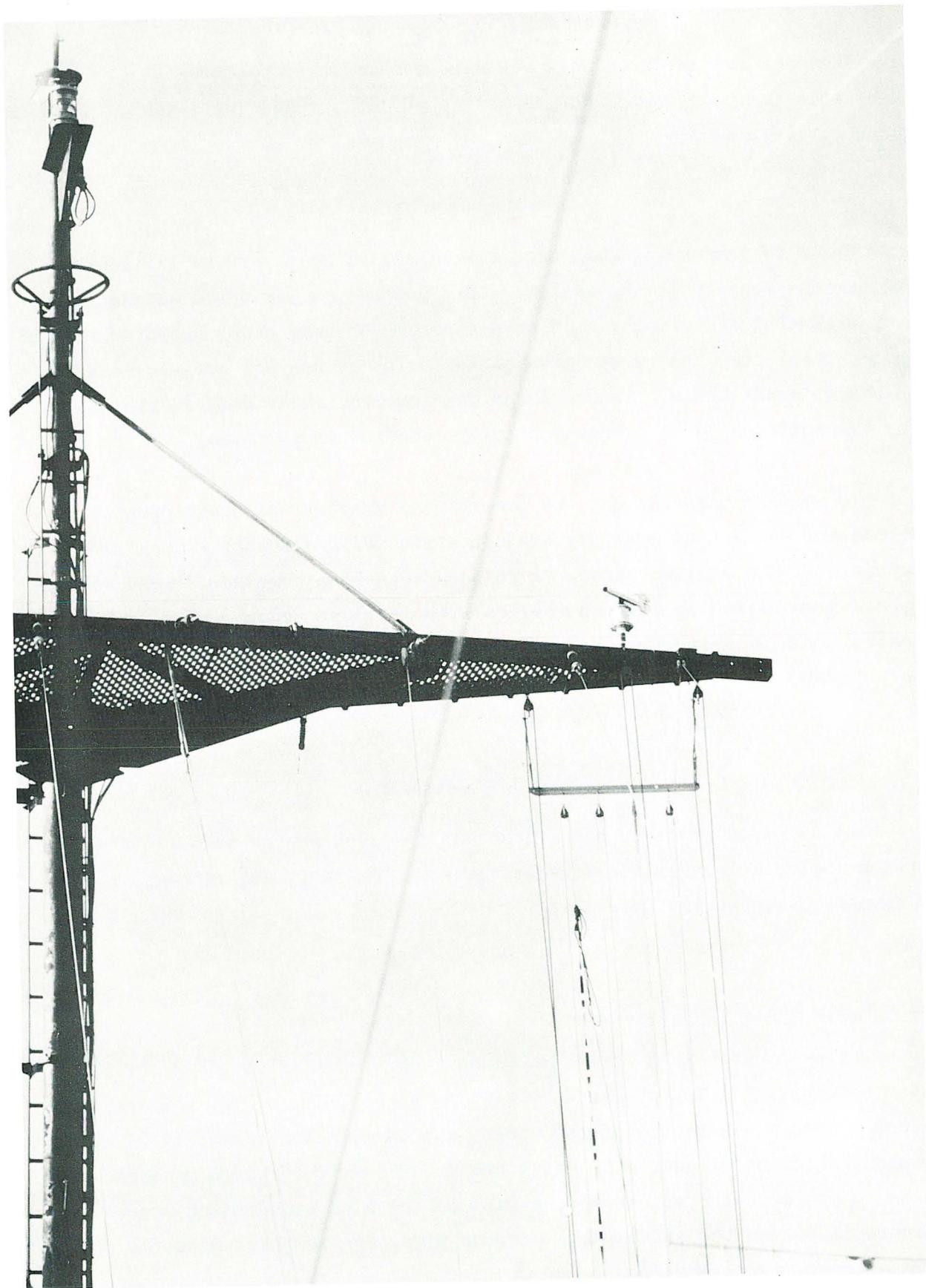


Figure II-4: One of two anemometers mounted on after mast catwalk.

Table III-1

Summary of measurements made

Parameter	Range	Units	Accuracy	Response	Sensor	Sample period	Data recorded every 6 minutes
Wind speed	0 to 60	m/sec	0.6 m/sec	0.33 cm	J-tec VA 320 sonic	30 sec.	average of 12 rel. vectors and
Wind direction	0 to 358	degrees rel. to ship	±2 degrees	10 m.	J-tec vane	30 sec.	average of 12 true vectors (m/sec)
Ship speed	0 to 20	knots	10% (est)	20 sec., integration limited by ship	Sperry SRD 101	30 sec.	average of 12 true vectors.
Ship heading	0 to 359	degree true	1 degree		Sperry Mk37 gyrocompass	30 sec.	(m/sec)
Solar radiation	0 to 5	volt	10% (est)	5 sec. (est)	Eppley/WHOI	30 sec.	average of 12 values
Sea surface temperature	-10 to +40	°C	±0.05 °C	2 min. (est)	RdF platinum	6 mins.	value
Air temperature	-40 to +50	°C	±1 °C	2 min.	General Eastern platinum	6 mins.	value
Dew point	-17.78 to 93.3	°C	±1 °C	3 to 5 mins.	General Eastern LiCl with platinum	6 mins.	value

The unit is a model VA-320, manufactured by J-Tec. The speed sensing unit utilizes the linear relationship between the frequency of vortex formation in the wake of a stationary rod and the speed of the air moving around it. The speed data from the unit is available as a frequency proportional to the rate of vortex shedding and as a voltage which is an analog of the frequency; the voltage is used in this case. The direction output is a linear voltage obtained from a precision, low torque, 358° potentiometer: 0° is wind from dead ahead, 90° is wind from starboard beam, etc.

The speed range is from a threshold of 1 m/sec to 65 m/sec with an accuracy of 0.6 m/sec. The direction range is 0 to 358 degrees with an accuracy of ± 2 degrees for speeds above 5 m/sec. The speed distance constant is 0.33 cm; the direction constant is 10 m.

The conversion factors used by the program are as follows:

$$\begin{aligned} \text{- speed} &= 12 \times (\text{volts}) \text{ m/sec} \\ &= 0.01379012 \times (\text{counts}) \text{ m/sec} \end{aligned}$$

$$\begin{aligned} \text{- direction} &= 72 \times (\text{volts}) \text{ degrees} \\ &= 1.256637062 \times (\text{volts}) \text{ radians} \\ &= 0.08802207194 \times (\text{counts}) \text{ degrees} \\ &= 0.00153627497 \times (\text{counts}) \text{ radians} \end{aligned}$$

Ship speed

Ship speed is measured with a single-axis acoustic doppler log, model SRD101, manufactured by Sperry Marine Systems. A direct interface to the system's data lines reads the speed into the remote acquisition unit.

Speed readings from 0 to ± 19.9 knots are possible. These are converted to m/sec in the program by multiplying by 0.508. Using speed and heading information, ship's velocity is determined as north and east vectors. Values in the range 0 to 10.16 m/sec are recorded; other values are recorded as 99.99 m/sec.

Ship heading

The ship uses a Sperry Mark 37 gyrocompass with step-by-step repeaters. The remote acquisition unit monitors the pulses on the three lines going to these repeaters. From these pulses it tracks the ship's heading from an initial heading entered by an operator.

The ship's heading data are thus available directly in degrees true. This is used in determining the ship's north and east velocity and subsequently in determining true wind.

True wind

This is actually a derived parameter but since it is displayed and recorded in real time, the method is described here.

For both anemometers, the apparent wind (i.e., relative to ship) is resolved into along-ship and athwart-ship vectors. For a given observation the sum of the athwart-ship vectors from the two anemometers is computed. If the sum is negative, data from the port anemometer is

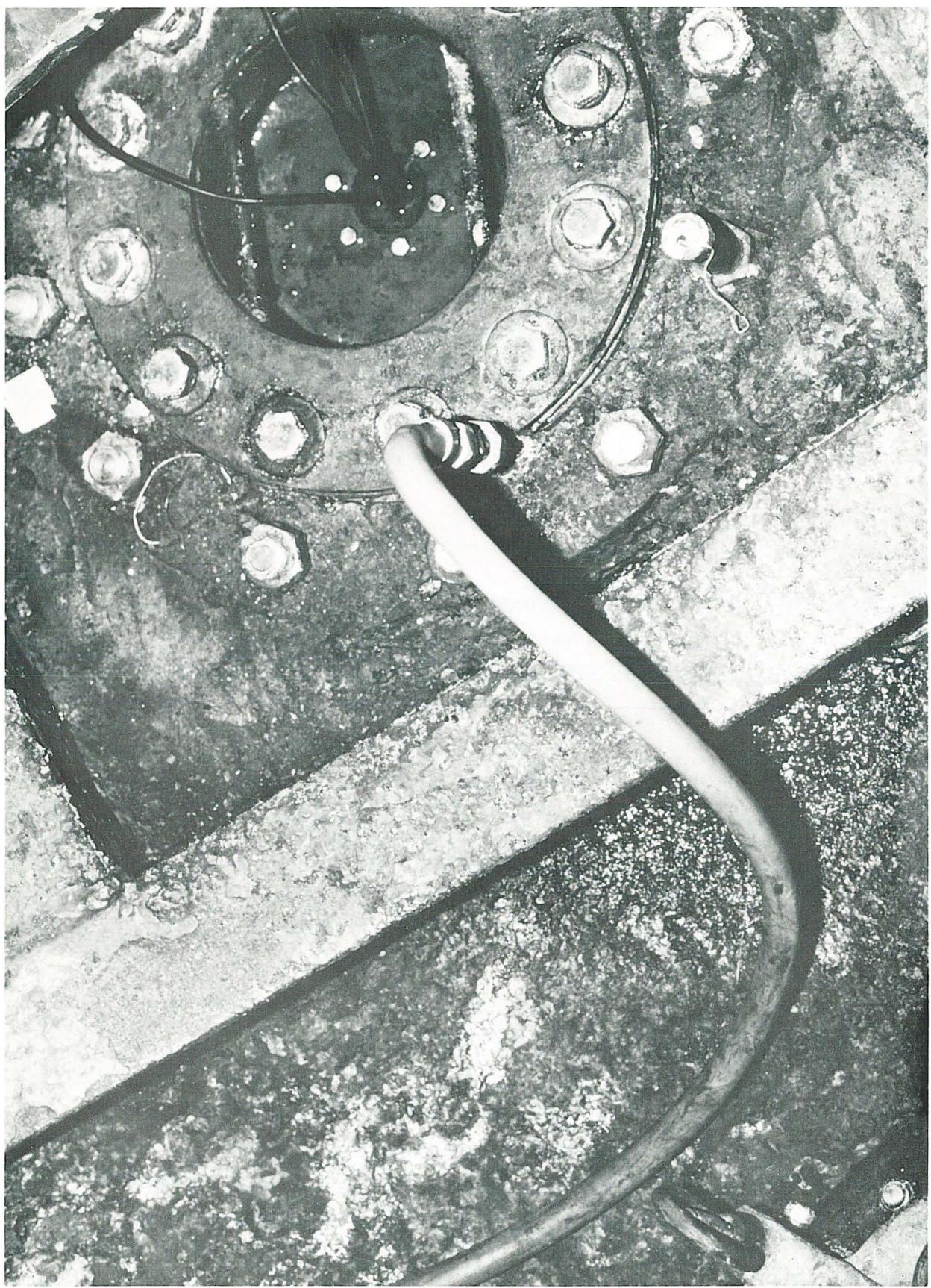


Figure II-5: Sea surface temperature detector mounted in transducer adapter ring in bow chamber.

selected; if it is zero or positive, data from the starboard anemometer is selected. Using ship heading, the selected apparent wind vectors are then resolved to north and east vectors. Finally, the ship's north and east velocities are subtracted leaving true wind.

Note that ship vectors indicate the direction the ship is moving to whereas wind vectors indicate the direction the wind is blowing from.

Solar radiation

The radiation sensor is an Eppley differential thermopile mounted on the top of the stern A-frame about 8 meters above the water surface. The unit is connected to a W.H.O.I.-manufactured device which provides a buffer amplifier with an analog integrator and chart recorder. The 0 to 5 VDC output of the buffer amplifier is digitized and recorded by the computer as a voltage reading. The conversion used for the digitizer output is

$$0.00114918 \times (\text{counts}) \text{ volts.}$$

When the stern frame was tilted from its rest position, the science watch noted the times for later annotation of the solar radiation data series.

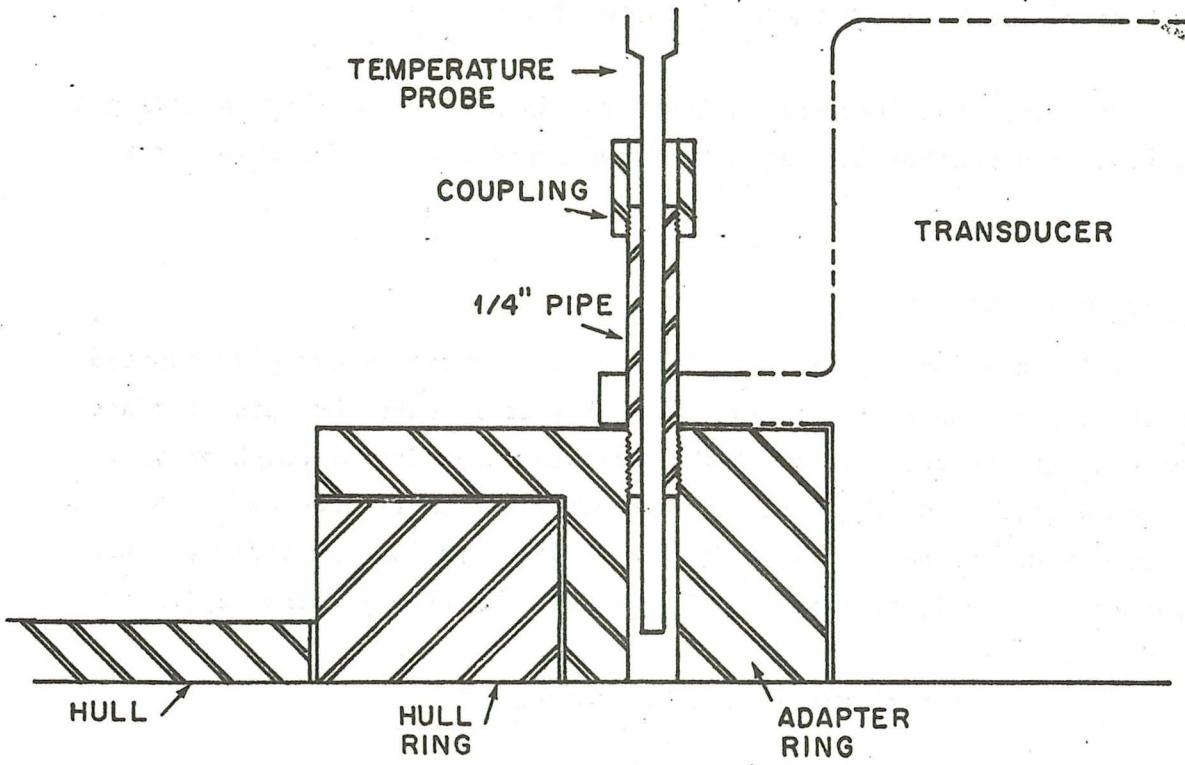


Figure II-6: Detail of mounting arrangement for sea surface temperature detector.

Sea surface temperature

The water temperature sensor is a 100 ohm platinum resistance temperature detector installed in the forward transducer adapter ring in the A-II bow chamber - Figure II-5. The ring is drilled through and tapped for a $\frac{1}{4}$ " pipe; the sensor is mounted in the pipe with its tip flush with the outside surface of the hull as shown in Figure II-6. The measurement is made at about 4.5 meters depth.

The sensor is a 3-wire type 21 connected to a 2-wire transmitter type 2600, both manufactured by RdF Corporation and calibrated for linear output within $\pm 0.05^{\circ}\text{C}$ over a span of -10° to $+40^{\circ}\text{C}$. The transmitter output is a direct current between 4 and 20 milliamperes which is proportional to the water temperature. The current output is passed through a Vishay 250 ohm resistor, type S102, tolerance 0.5%, to generate a voltage which is measured by the remote acquisition unit.

The temperature sensor and transmitter were calibrated before and after the JASIN cruise at the W.H.O.I. temperature calibration facility. This was to verify the quoted accuracy and to allow corrections to be applied to the recorded data if additional accuracy is desired. The calibration results are shown in Figure II-7. Additional accuracy can be obtained by applying a correction as shown in Figure II-8 to the recorded data. A further improvement could be obtained by performing a more accurate digitizer calibration.

The conversion factors used by the program are as follows:

- for transmitter output (volts)

$$\text{temperature} = 12.5 \times (\text{volts}) - 22.5^{\circ}\text{C}$$

- for digitizer output (counts)

$$\text{temperature} = 0.01436471 \times (\text{counts}) - 22.5^{\circ}\text{C}$$

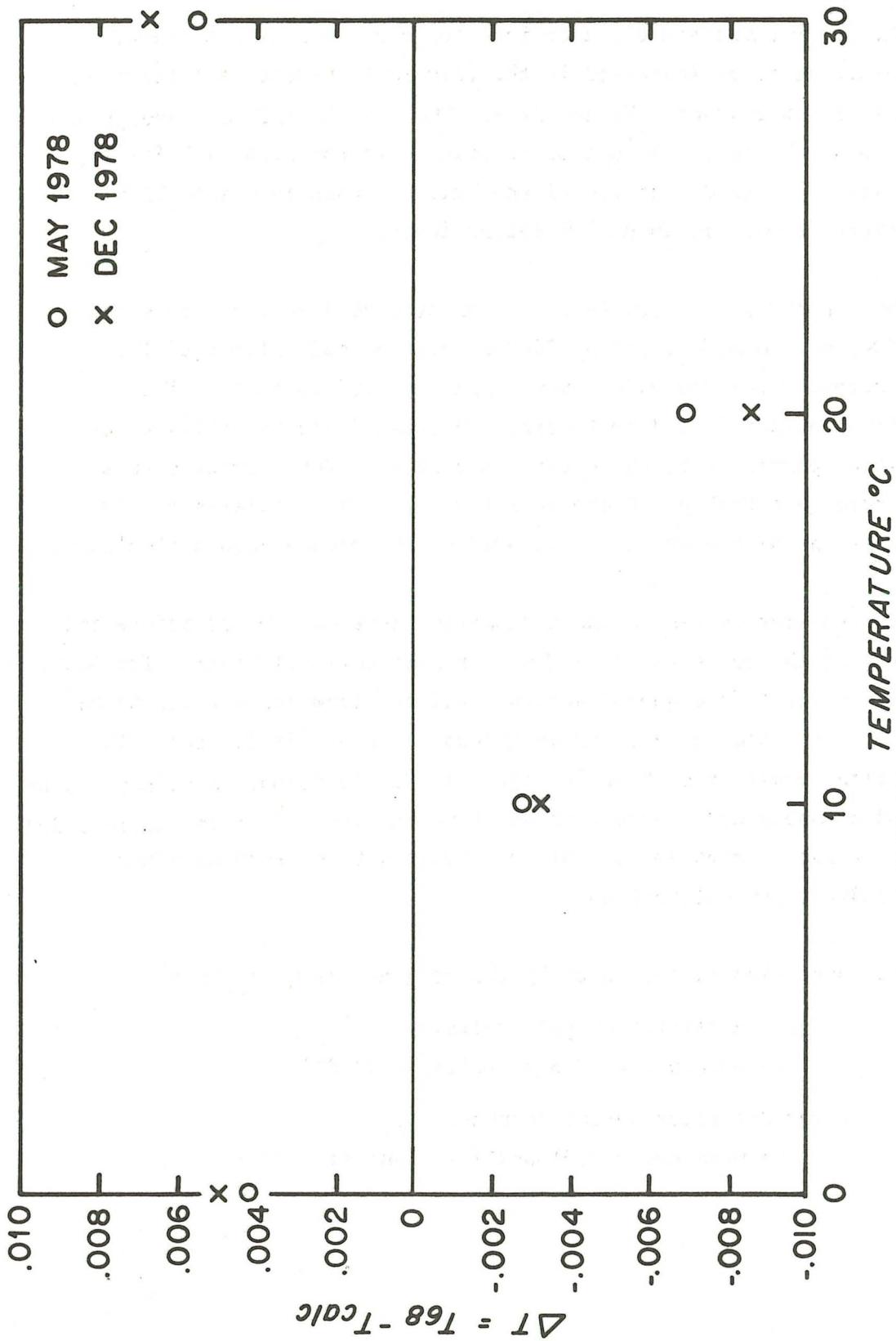


Figure II-7: Calibration of sea temperature detector before and after JASIN cruise. T_{68} is the temperature of the calibration bath, T_{calc} is the temperature calculated from the detector's output.

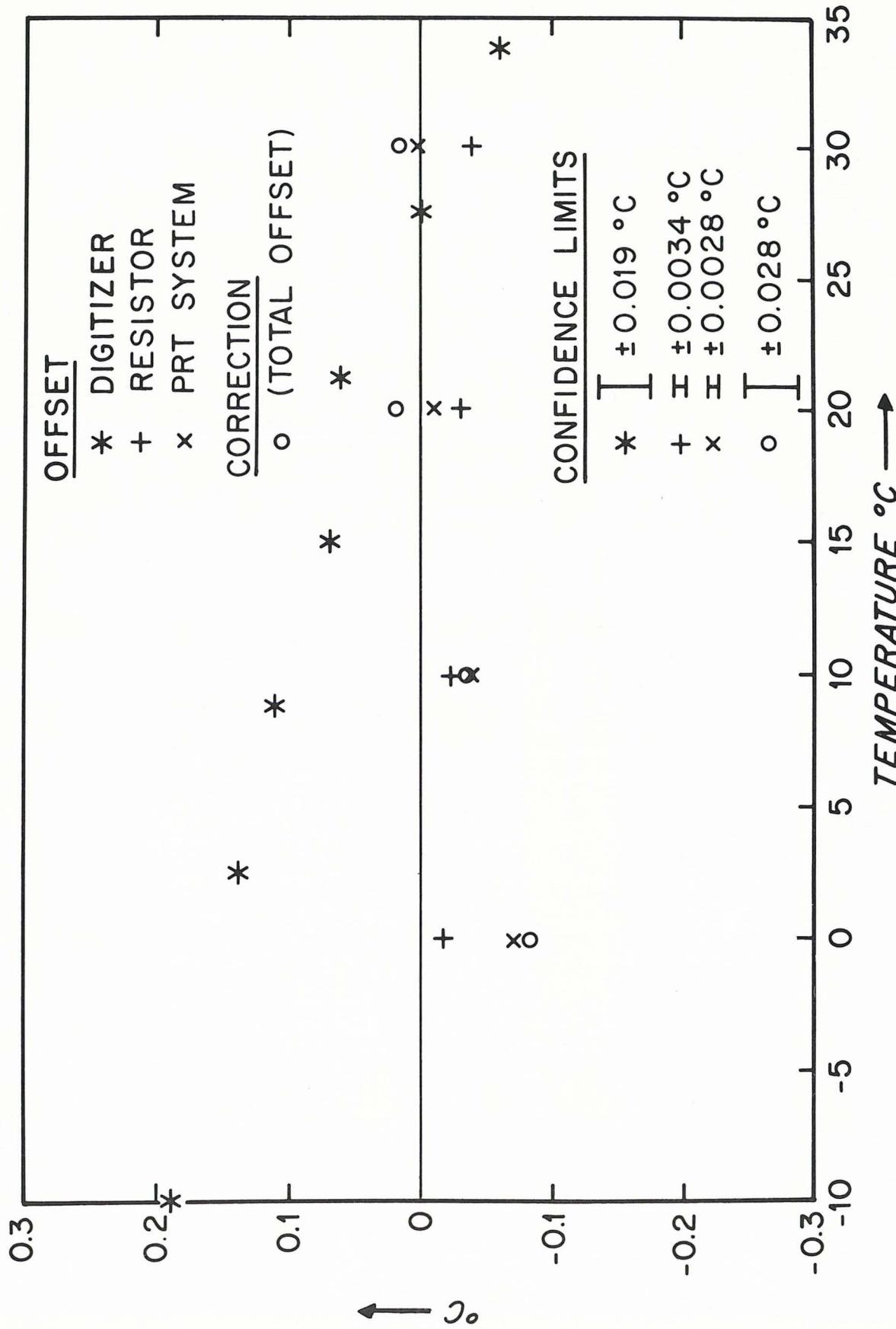


Figure II-8: Net error in observed sea surface temperature caused by digitizer, detector and resistor errors.

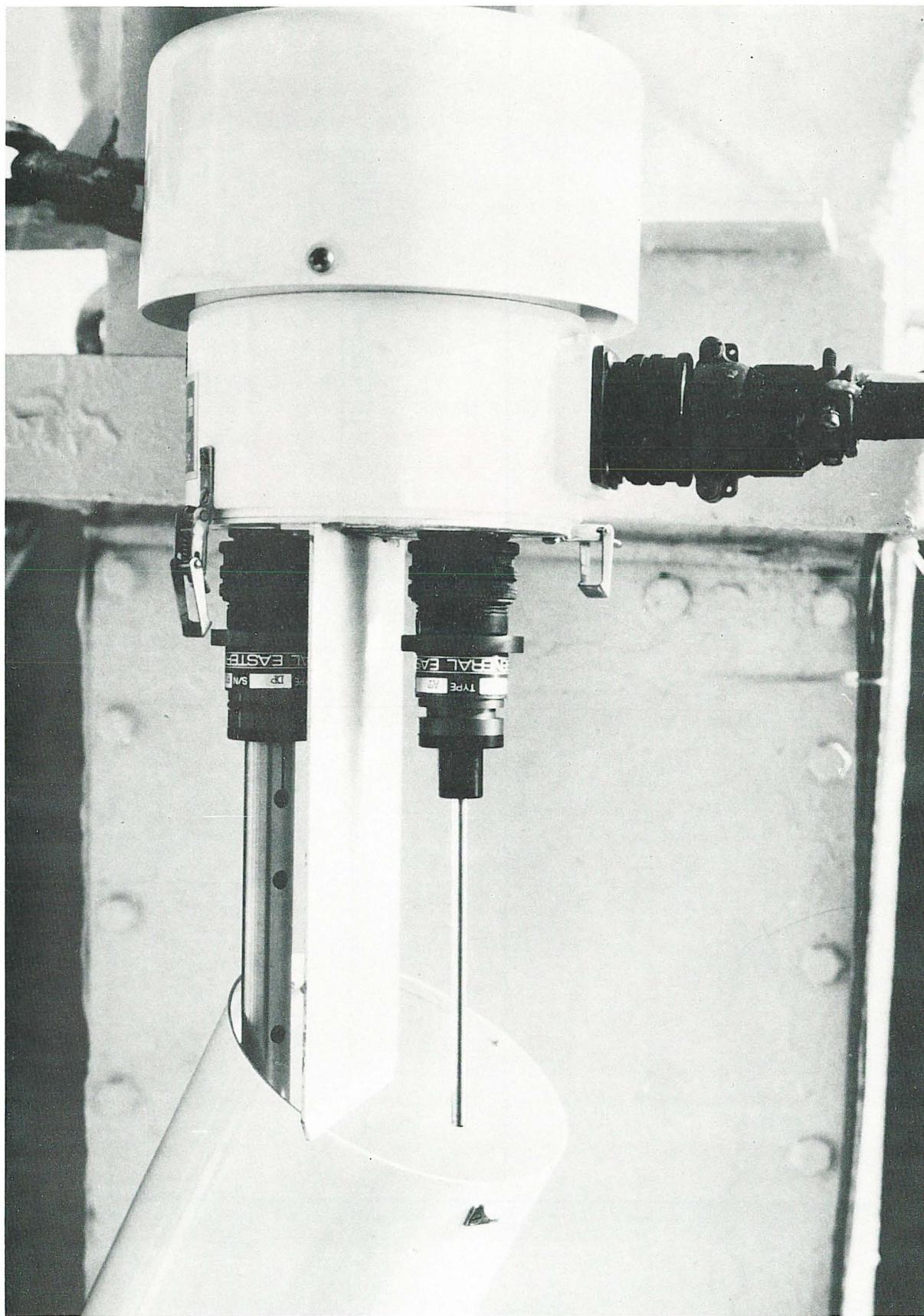


Figure II-9: Dewpoint and air temperature sensors mounted in aspirated sun shield with access cover removed.

Air temperature

The air temperature sensor is a 100 ohm platinum resistance temperature detector mounted in a motor-aspirated sun shield along with the dew point sensor - Figure II-9. The unit is installed on a stanchion on top of the top laboratory about 11.5 meters above the water surface.

The sensor is a model 612A with a model 650 AT transmitter manufactured by General Eastern. The sensor is mounted in a model 706 M aspirated sun shield. The transmitter provides a 0 to 5 VDC output for an air temperature range of -40° to $+50^{\circ}$ C with an accuracy of $\pm 1^{\circ}$ C. With 10 feet per minute aspiration, the response is approximately two minutes.

The conversion factors used by the program are as follows:

- for transmitter output

$$\text{temperature} = 18 \times (\text{volts}) - 40^{\circ}\text{C}$$

- for digitizer output

$$\text{temperature} = 0.2068519 \times (\text{counts}) - 40^{\circ}\text{C}$$

Dew point

The dew point sensor is a 100 ohm platinum resistance temperature detector surrounded by a teflon-sheathed stainless steel bobbin. On the bobbin is an elemental winding of inert platinum wire over a glass wick. The unit is mounted in a motor aspirated sun shield along with the air temperature sensor - Figure II-9. Prior to installation, the wick is coated with a saturated solution of lithium chloride. In operation, the platinum winding is heated to the point where evaporation of water balances condensation. This temperature measured by the platinum detector is a measure of the dew point of the surrounding air.

The sensor is a model 611 A with a model 650 DP transmitter manufactured by General Eastern. The sensor is mounted in a model 706 M aspirated sun shield. The transmitter provides a 0 to 5 VDC output for a dew point range of 0 to 200°F with an accuracy of $\pm 2^{\circ}\text{F}$. With 10 feet per minute aspiration the response is 3 to 5 minutes.

The conversion factors used by the program are as follows:

- for transmitter output

$$\text{dew point} = 18.6666 \times (\text{volts}) \ ^{\circ}\text{C}$$

- for digitizer output

$$\text{dew point} = 0.10725652 \times (\text{counts}) \ ^{\circ}\text{C} .$$

RESULTS

The system was operating for acquisition and display a total of 27.7 days during the two legs of the JASIN cruise. During the first leg, the system operated from 0000, 2 August to 0800, 14 August. However, for an 8-hour period on 6 August some data are missing because of a bad dew point sensor. During the second leg the system operated from 1200, 22 August to 1200, 7 September with a 7-hour outage on 30 August when the computer program failed.

When evaluating a system for collecting data in a shipboard environment, component reliability is as important as accuracy of results. Thus, system operation should not be jeopardized by failure of one module.

In this case, the system failed to provide recorded data due to a hardware problem with the tape drive. The data presented here were logged by watchstanders from the CRT display and subsequently keypunched in a standard format for computer processing. In the future, a hardcopy printer will be added to provide access to previous data during the cruise and to serve as a backup for the tape system.

Reliability problems were encountered with certain sensors. Anemometers and air temperature sensors are required to operate in locations subject to high levels of radio frequency radiation. Modifications were necessary to the circuitry mounted in the sensor unit to provide filtering and decoupling in order to prevent damage and incorrect operation.

Lithium chloride dew point cells are relatively inexpensive but can be contaminated by salt deposits. To minimize this problem we provided a closed, aspirated shield for the dew point cell. In addition, we performed frequent inspection of the cell and we carried a spare cell to simplify servicing when required. The unit was serviced only once (6 August) and appeared to operate successfully for long periods - Figure III-12.

Platinum resistance temperature detectors were chosen in all cases for their long term stability. The calibration of the water temperature unit (Figure II-4) appears to support this choice.

In addition to reliability, however, data validity is important. To evaluate the PET data set, scatter plots were produced of several of the parameters against the corresponding parameters in the manual and the buoy data sets. These appear in Part III.

RECOMMENDED IMPROVEMENTS

In the interests of generating a more complete data set, the system should be upgraded to include inputs from a flow-through conductivity system, and from one or more navigation devices such as a satellite navigator or a Loran C receiver.

To simplify changes required for different cruises, the computer program should be changed to perform a running mean instead of a fixed-length average which it now performs.

Finally, an external digital clock should be added to provide better accuracy and display than the internal PET clock used during the cruise.

REFERENCE

Peal, K. R. and A. M. Bradley, Use of Industry Standards for Shipboard Data Systems, IEEE Oceans '78 Conference Record, 78CH1356-6, pp. 547-551, September, 1978.

PART III
METEROLOGICAL DATA

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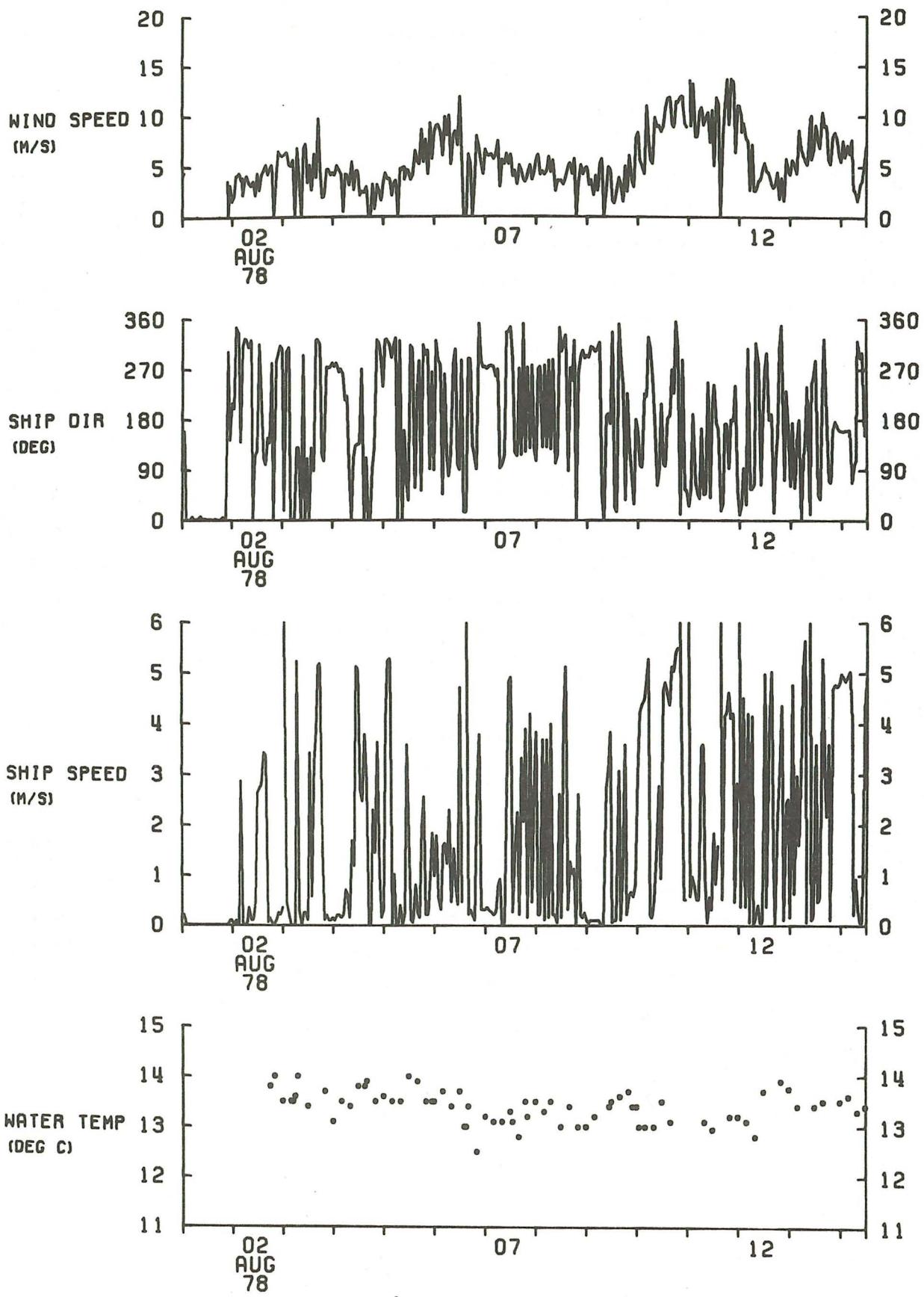


Figure III-1a: Leg 1 MANUAL hourly observations

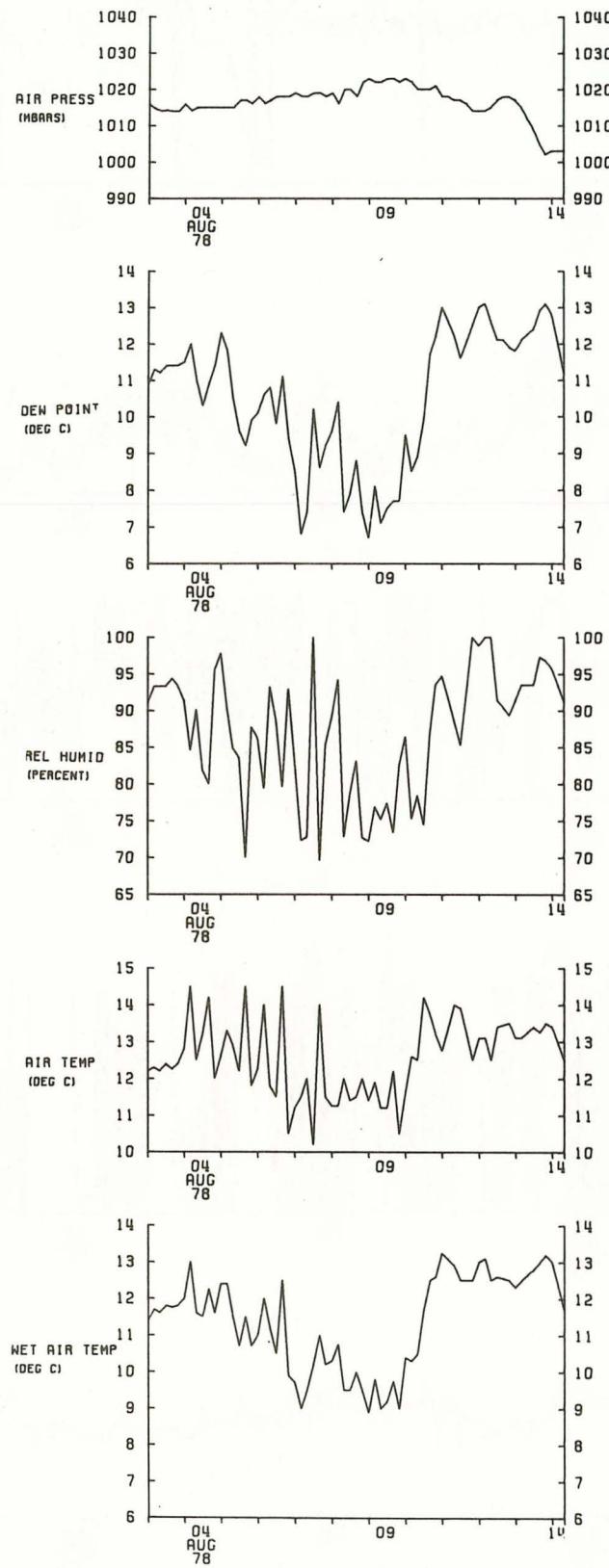


Figure III-1b: Leg 1 MANUAL 4 hour observations

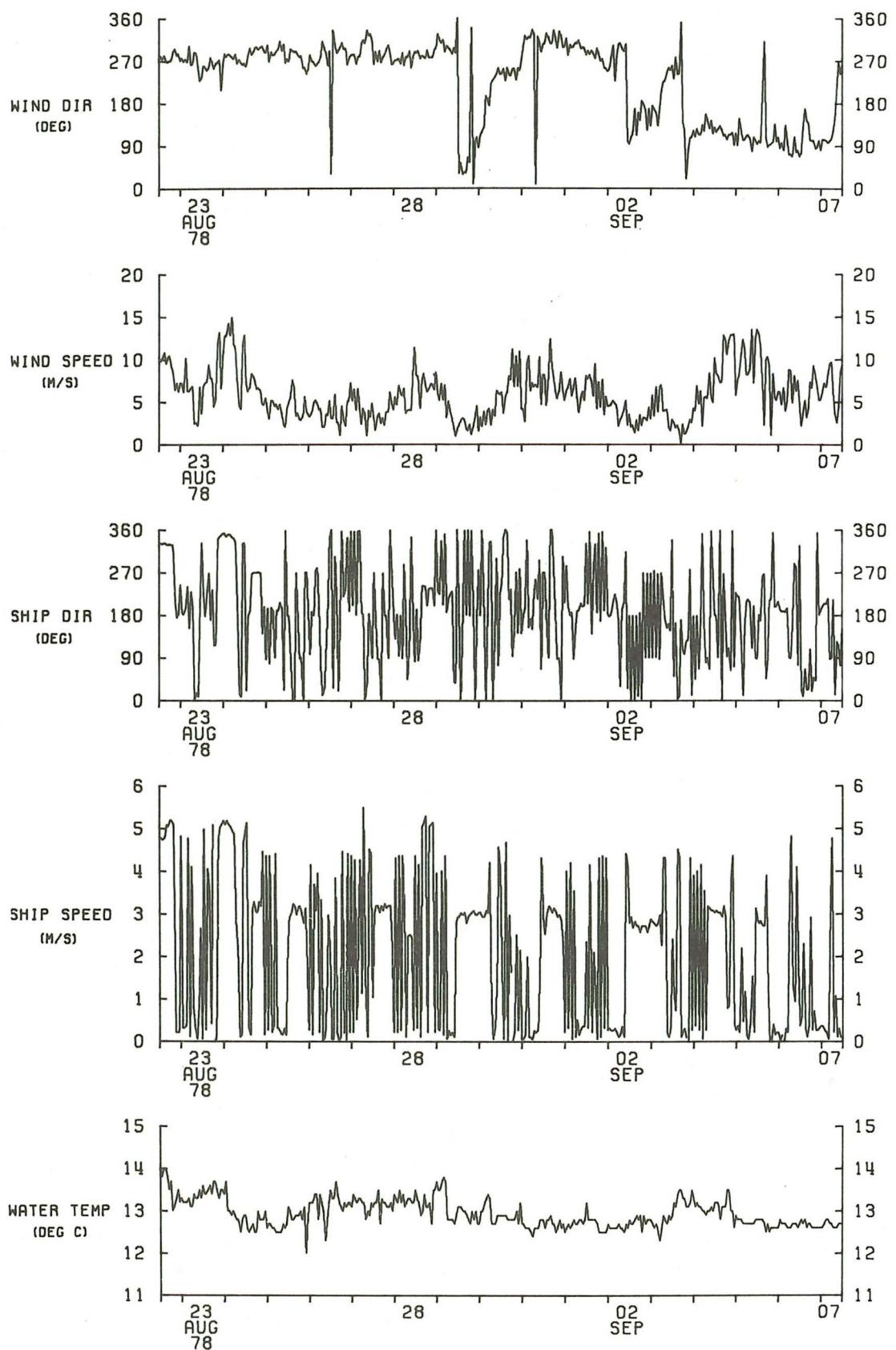


Figure III-2a: Leg 2 MANUAL hourly observations

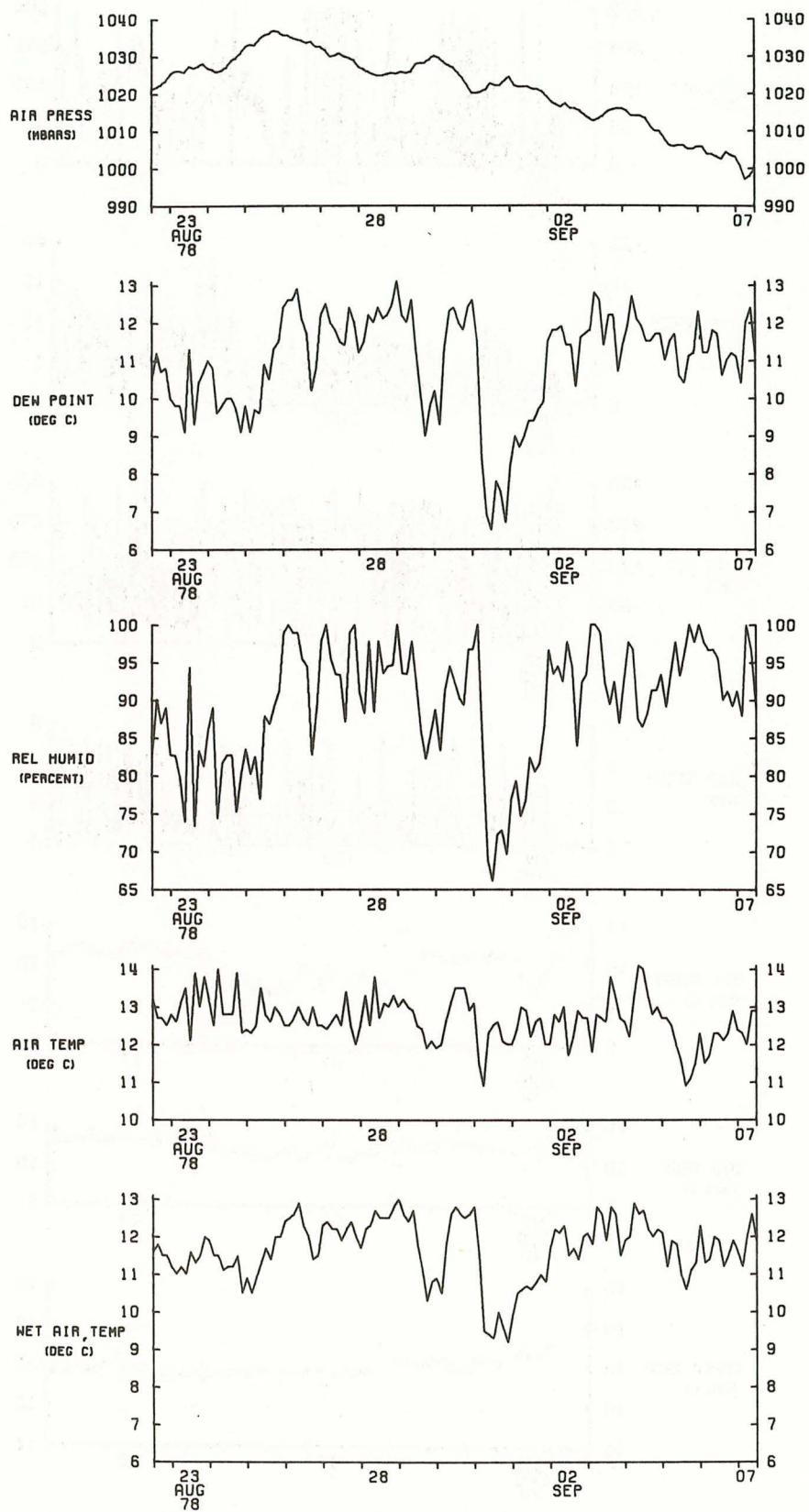


Figure III-2b: Leg 2 MANUAL 3 hour observations

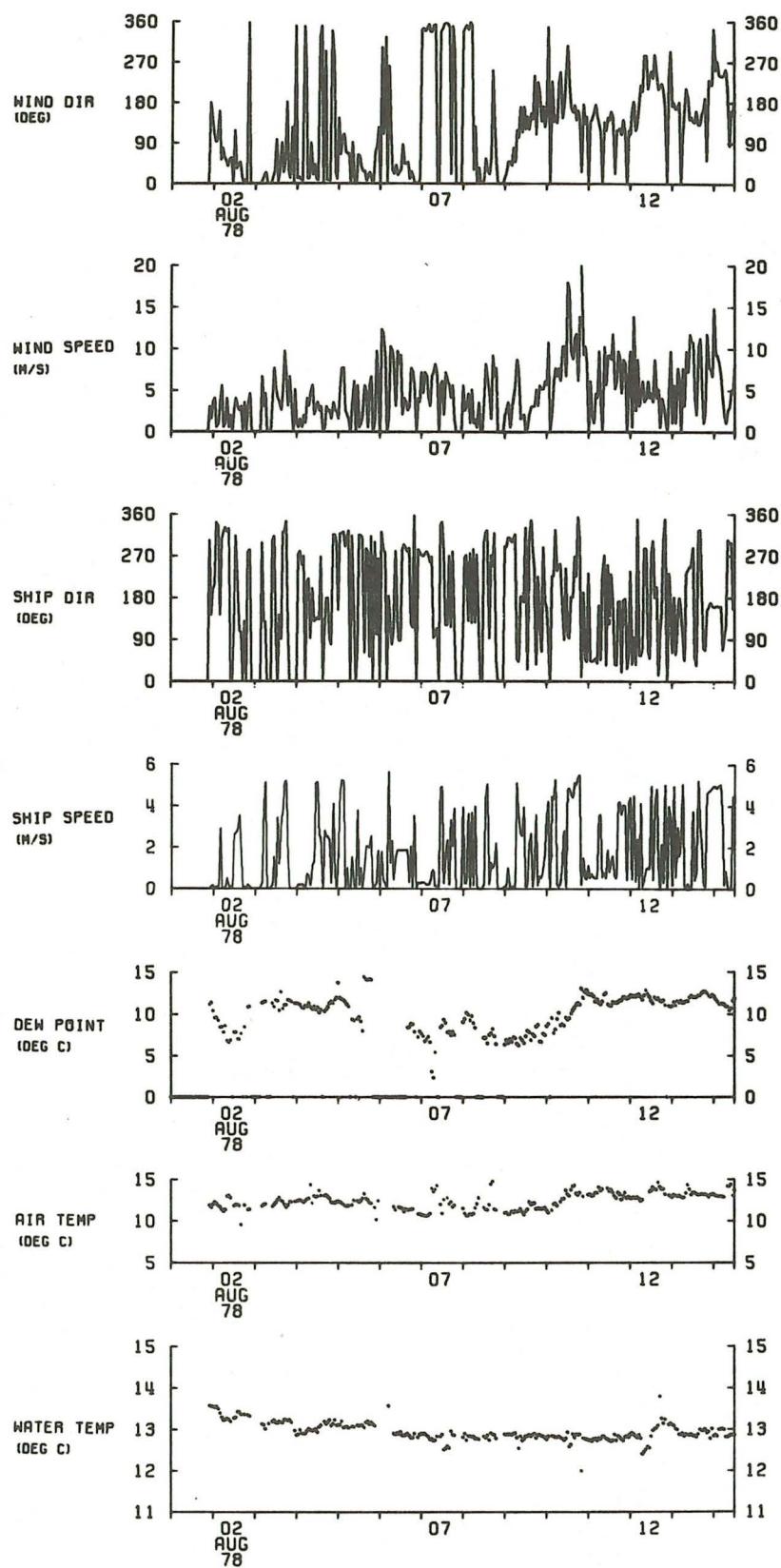


Figure III-3: Leg 1 PET observations

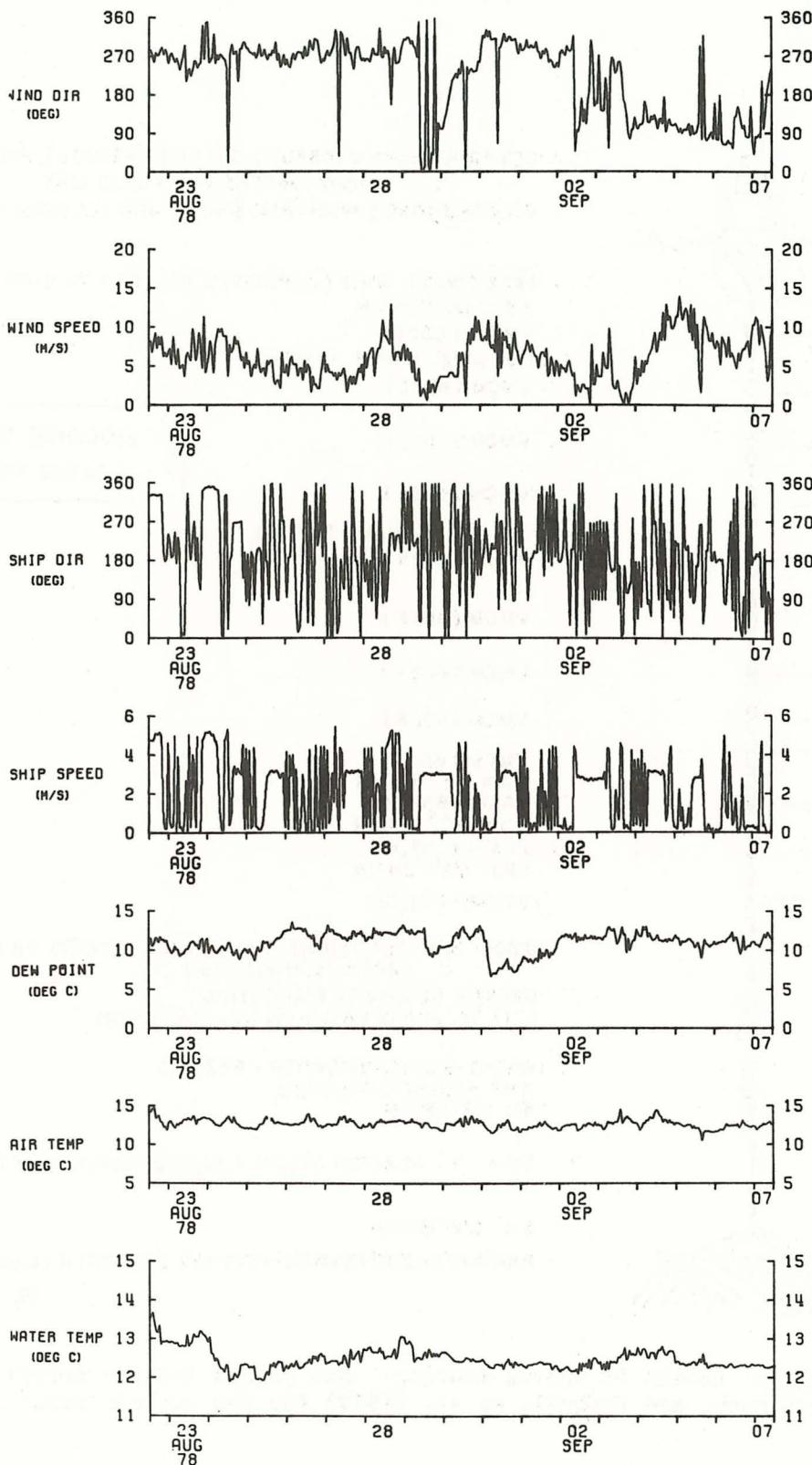


Figure III-4: Leg 2 PET observations

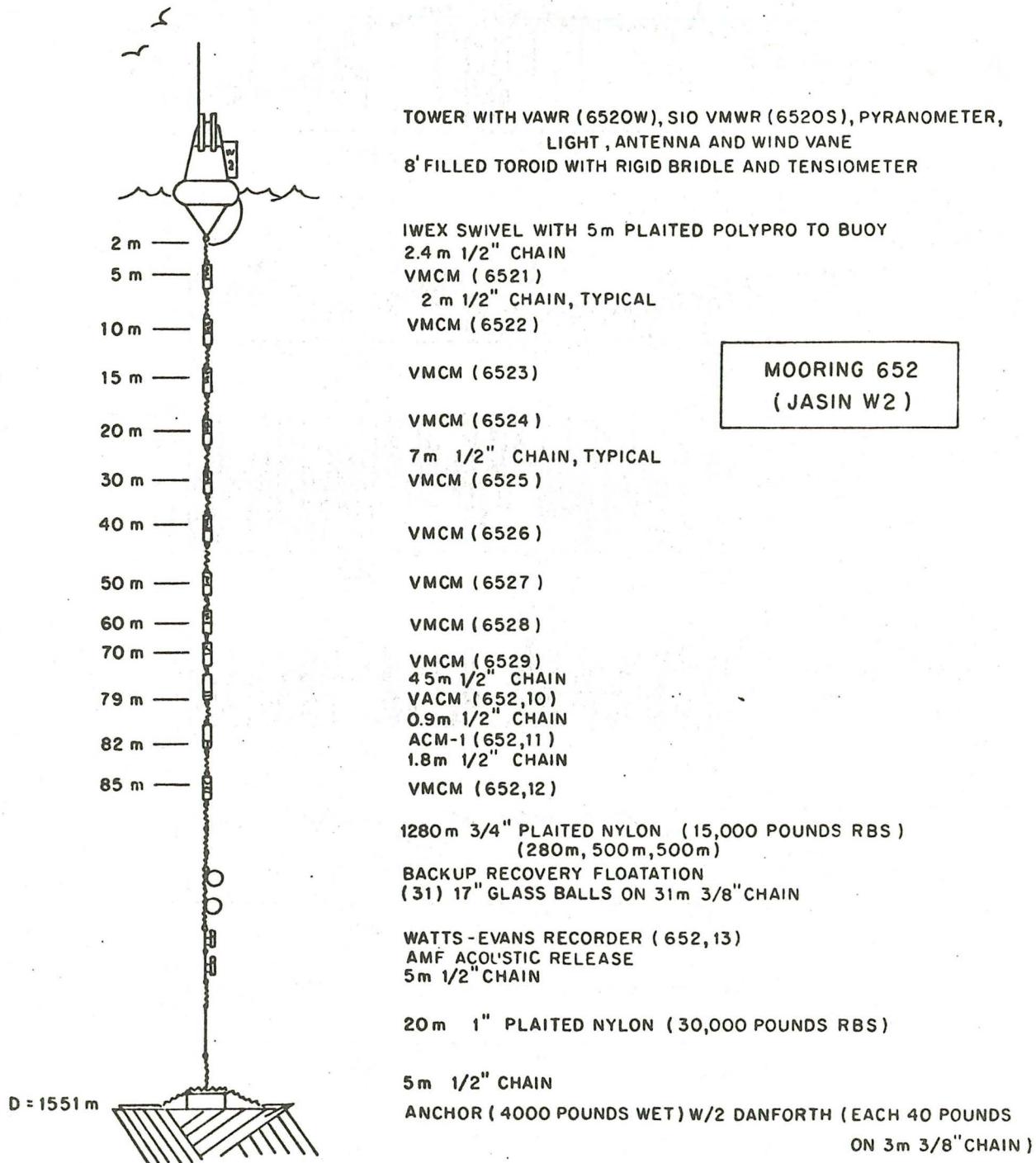


Figure III-5: Design of the W2 mooring. See Figure I-3 for details of the surface buoy, and Tarbell, et al. (1979) for the current meter data.

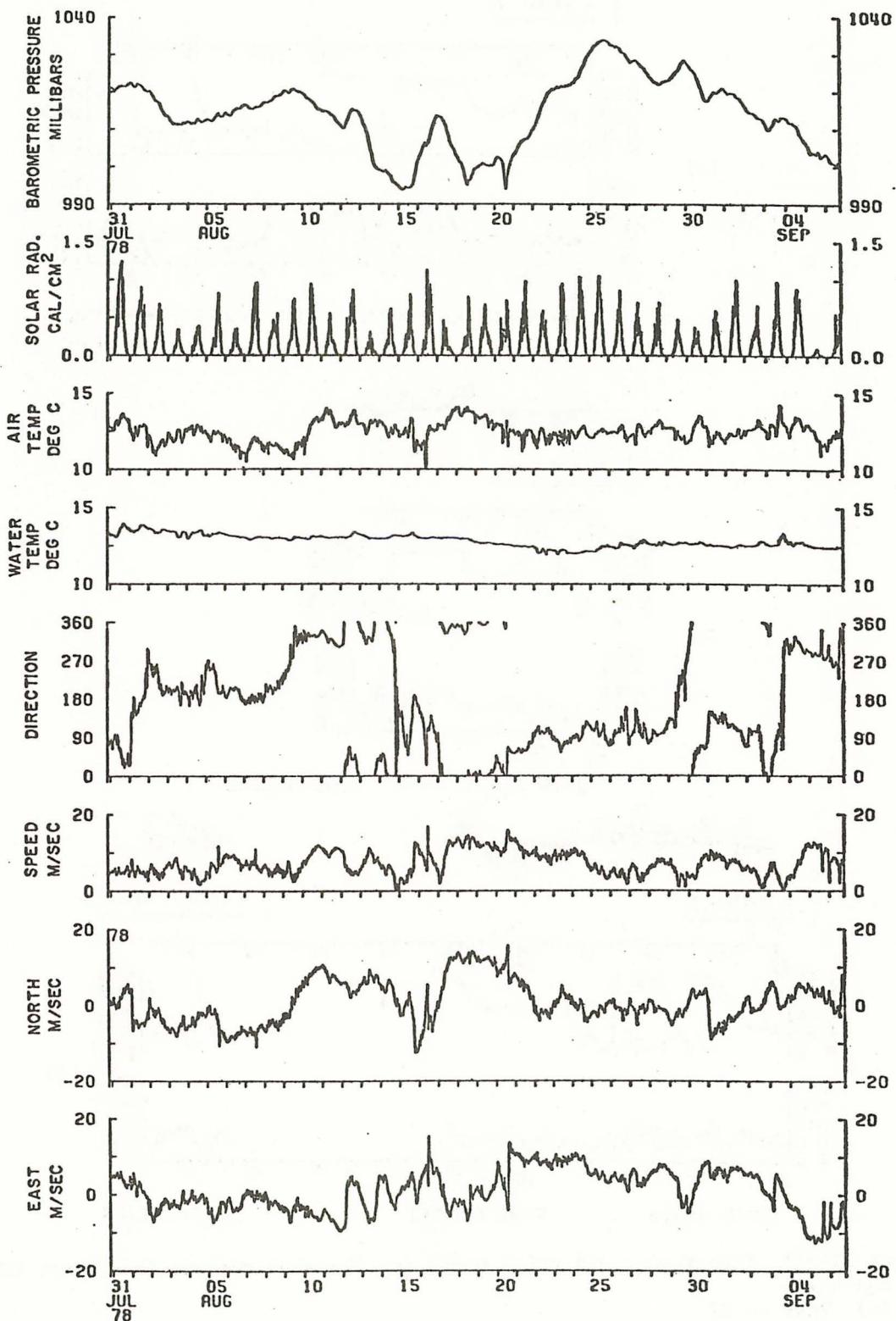


Figure III-6: W2 meteorology

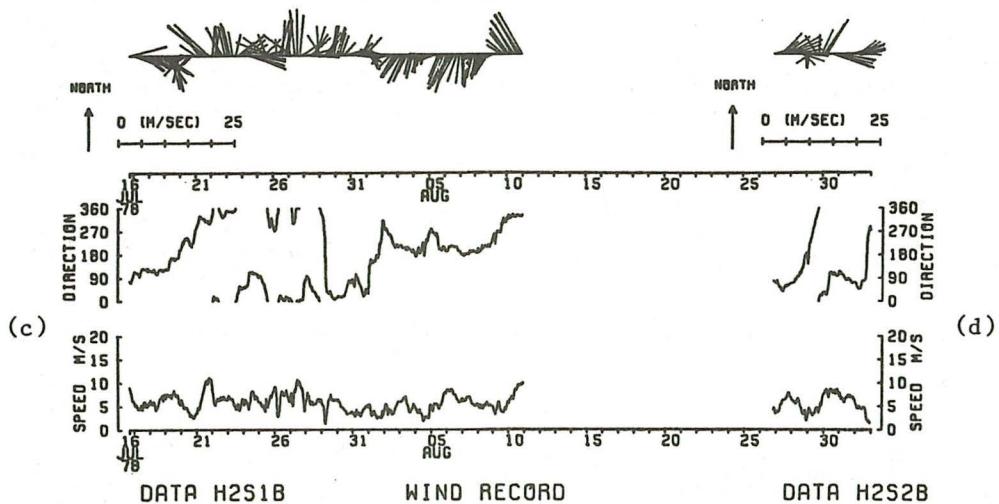
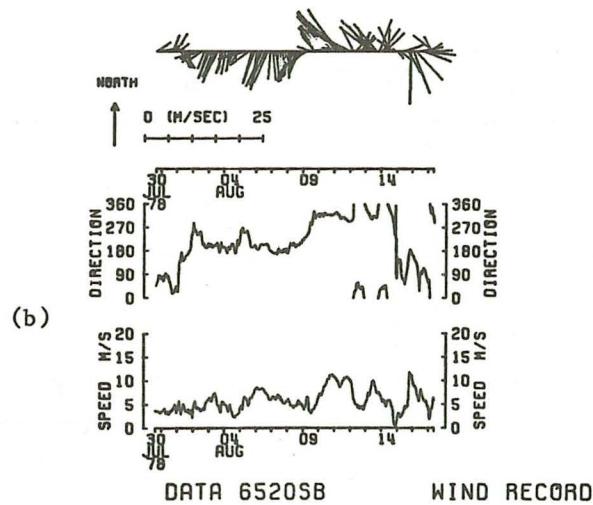
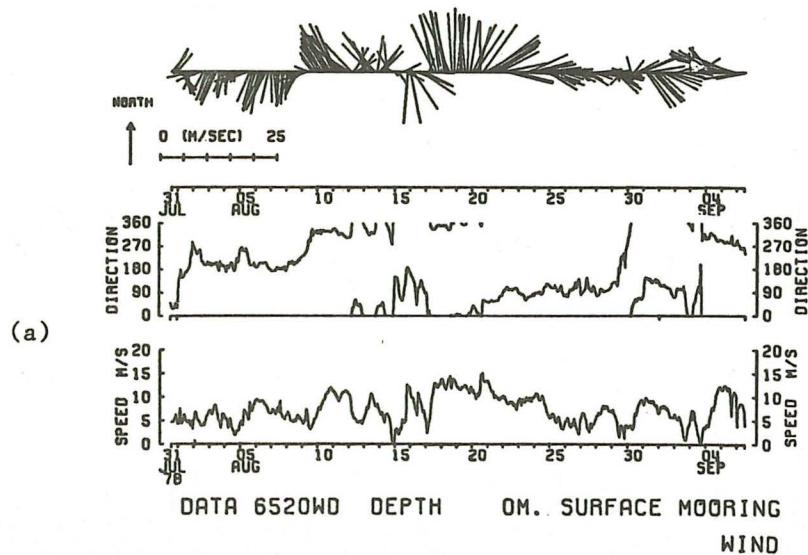


Figure III-7: Time series and stick plots for the wind records from buoys W2 and H2.

- (a) VAWR on W2
- (b) VMWR on W2
- (c) VMWR on H2 (first deployment)
- (d) VMWR on H2 (second deployment)

6520WD

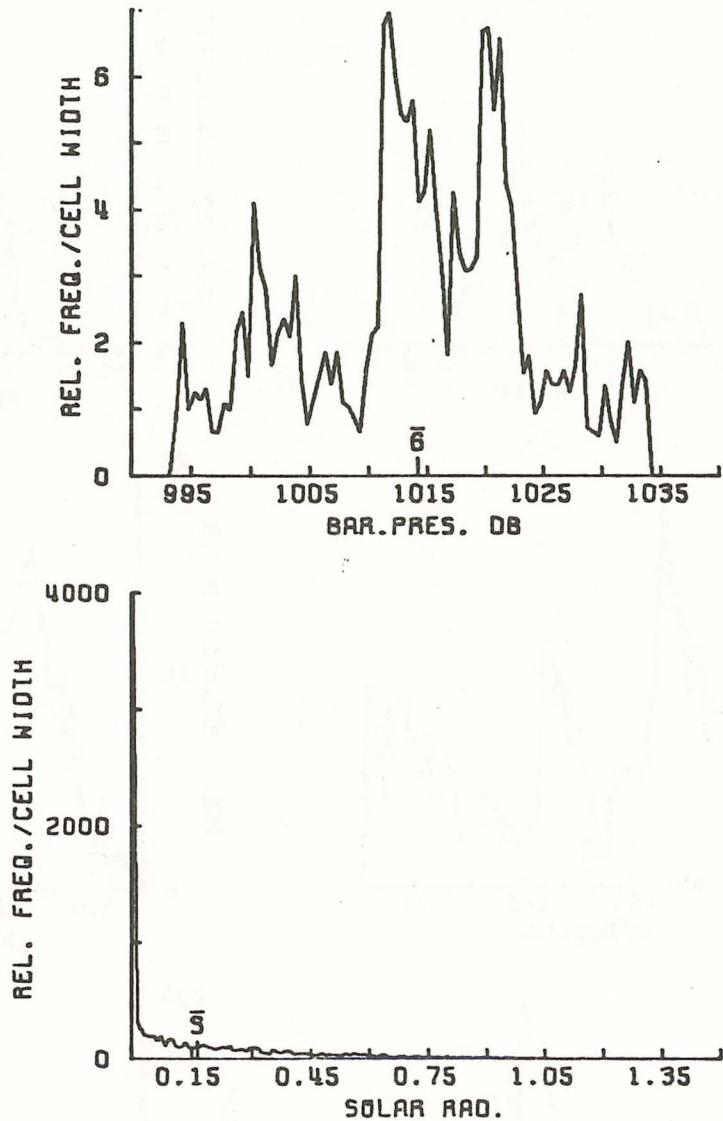
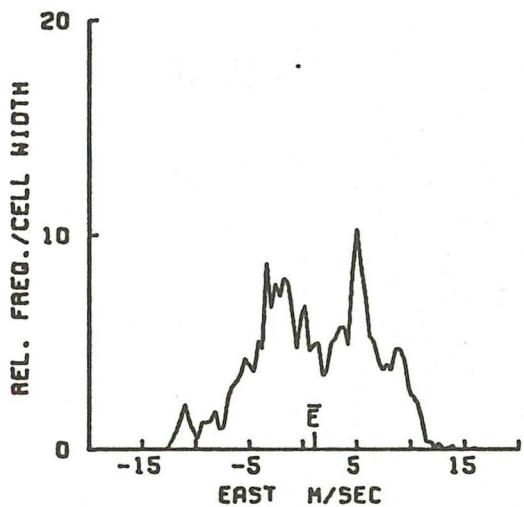


Figure III-8: Histograms of the buoy data from W2 and H2.
(a) VAWR on W2 (6520WD)
(b) VMWR on W2 (6520S)
(c) VMWRs on H2

WIND RECORD



DEPTH -0- M.

6520WD

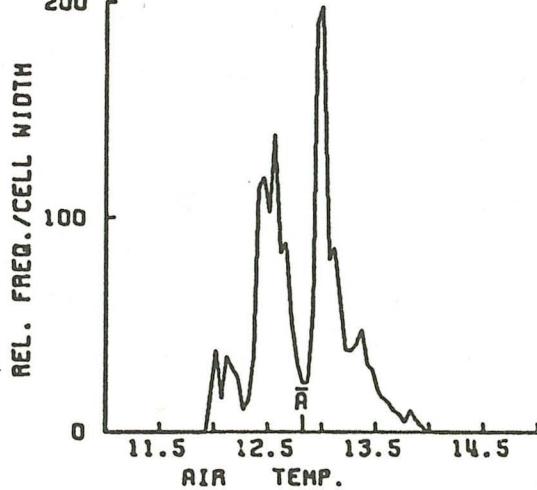
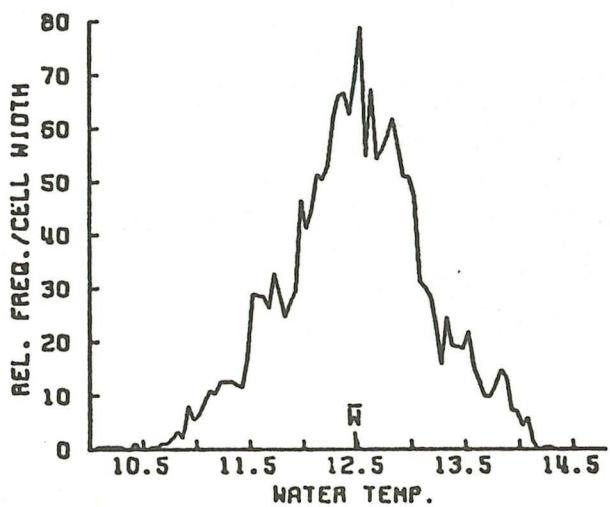
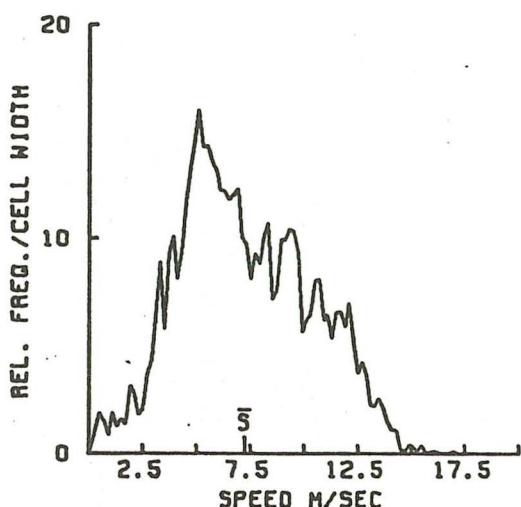
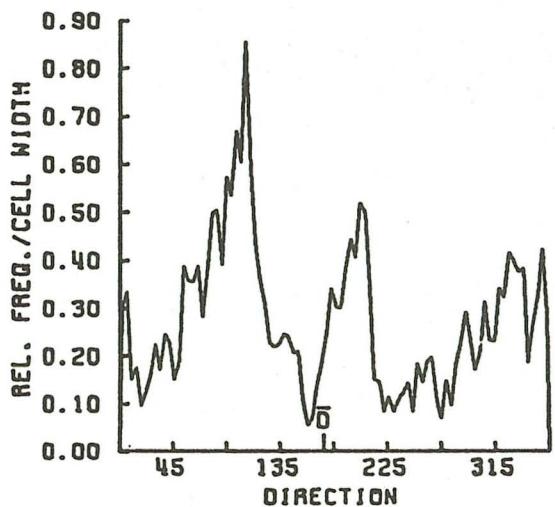
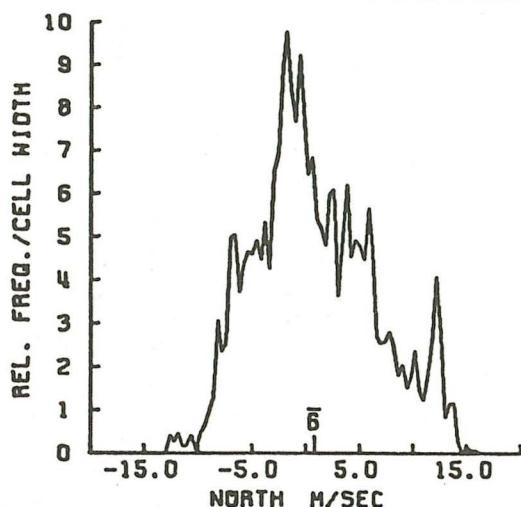


Figure III-8a (continued): VAWR on W2

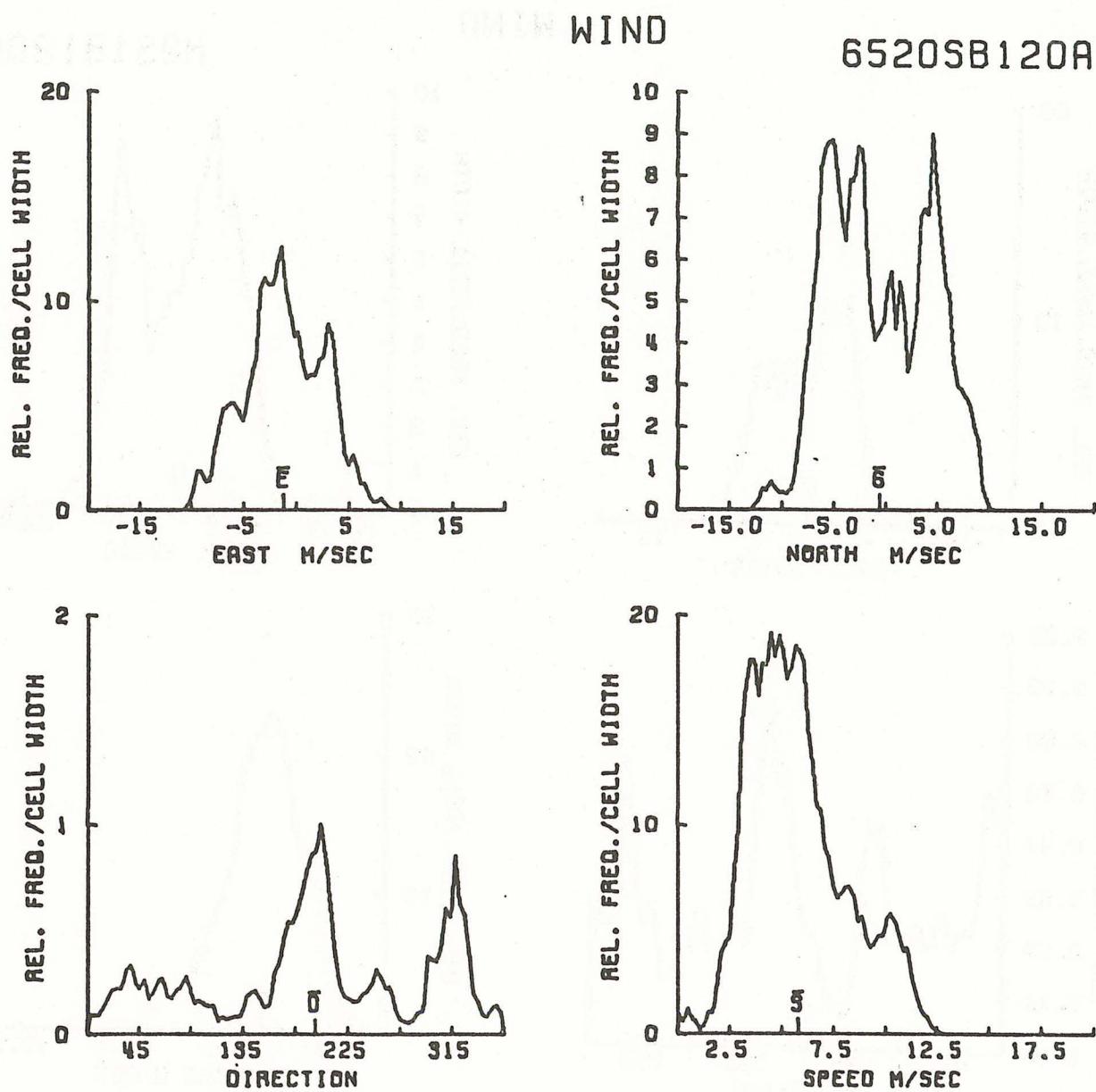


Figure III-8b: VMWR on W2

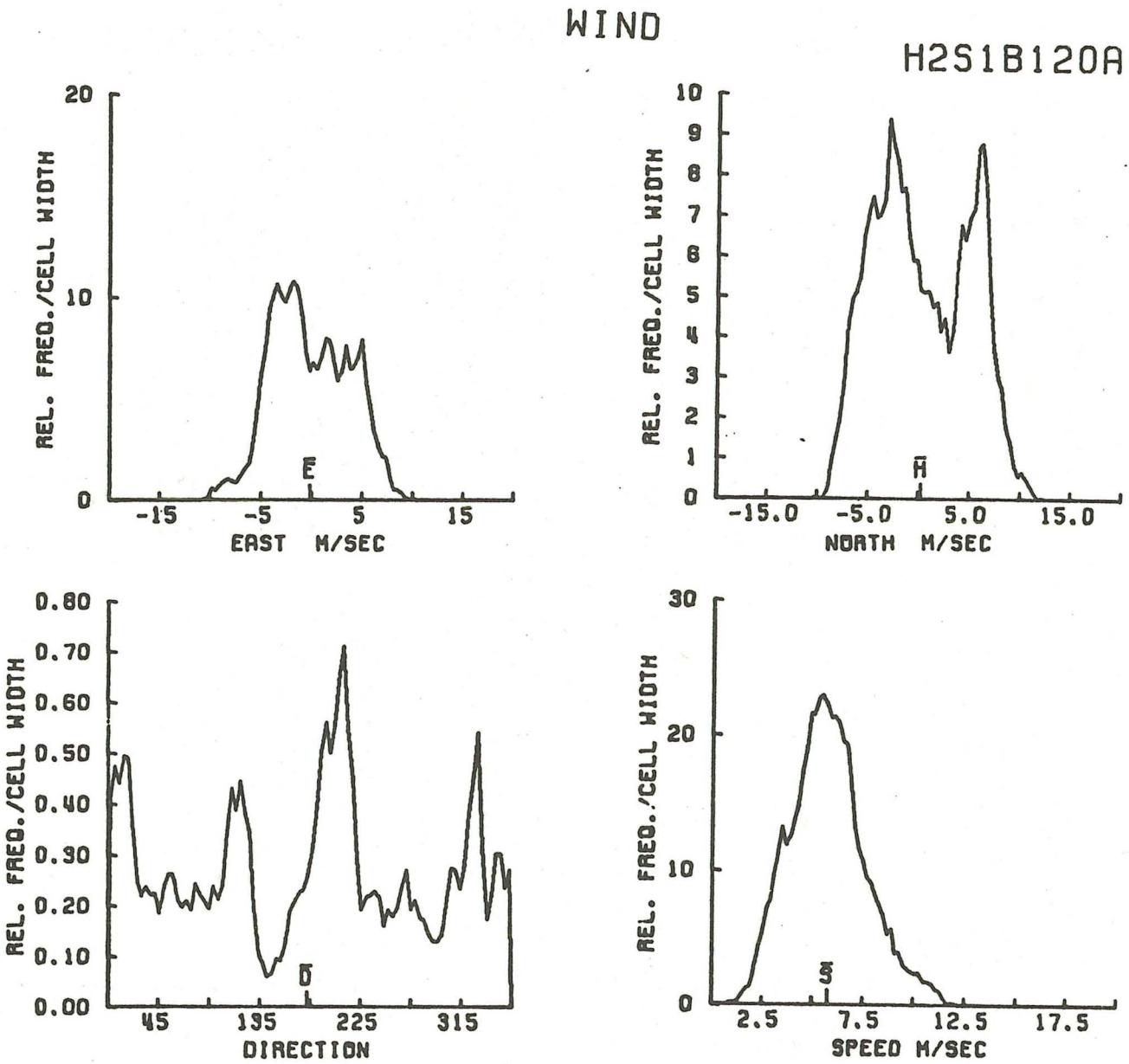


Figure III-8c: First deployment. VMWR on H2.

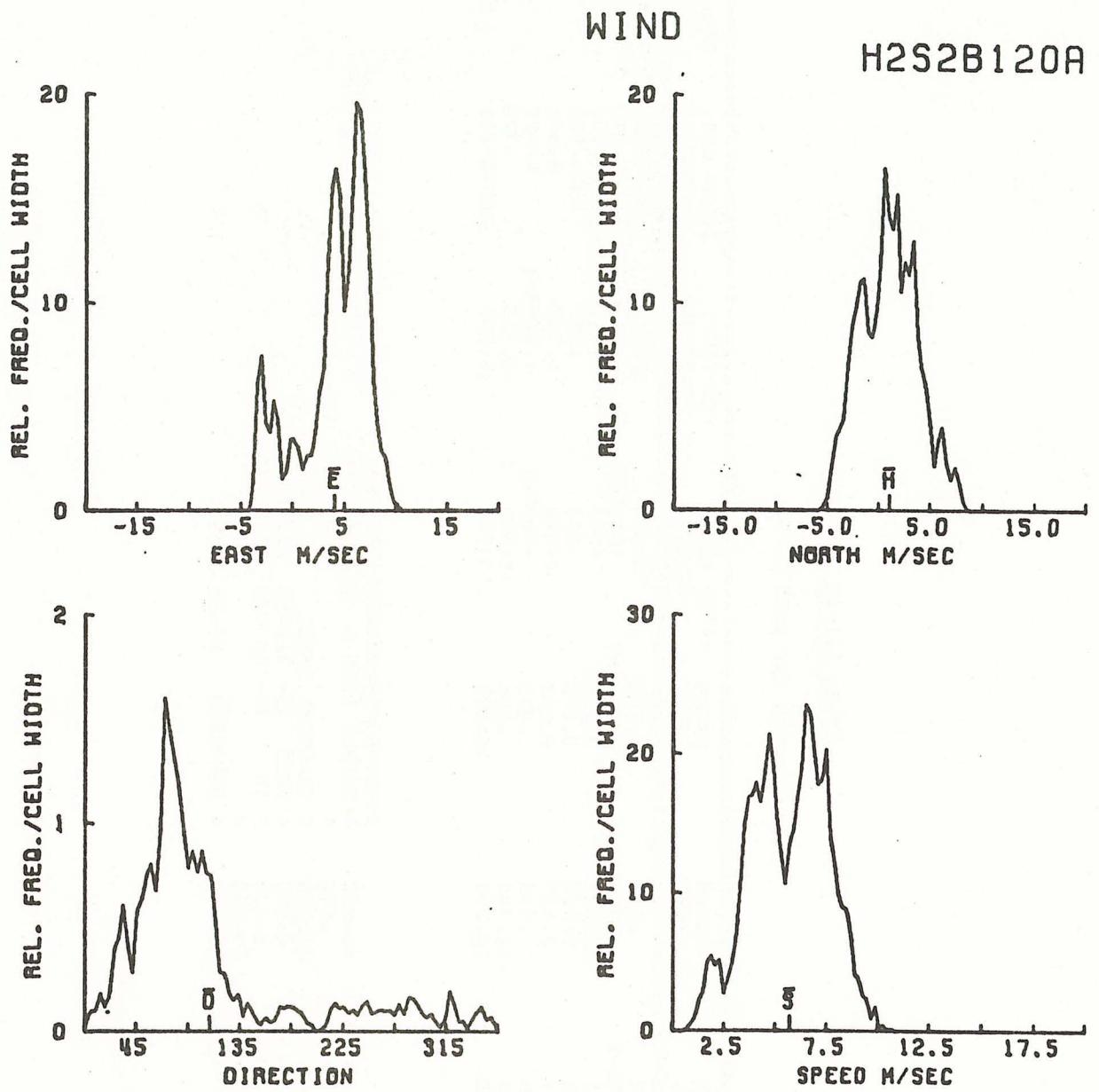


Figure III-8c (continued): Second deployment.

Table III-1a
 Statistics for VAWR on W2.

VARIABLE	*	EAST	NORTH	SPEED	WATER TEMP.	AIR TEMP.	SOLAR RAD.	BAR. PRESS.
UNITS	*	M/SEC	M/SEC	M/SEC	CELSIUS	CELSIUS	WHR/M**2	MILLIBARS
MEAN	=	1.057	.822	7.242	12.823	12.476	2783.098	1014.205
STD. ERR.	=	.393E-1	.919E-1	.504E-1	.664E-2	.109E-1	.64.145	.156
VARIANCE	=	29.101	30.826	9.275	1.61	.434	15010068.150	88.874
STD. DEV.	=	5.394	5.552	3.045	.401	.659	3874.283	9.427
KURTOSIS	=	2.317	2.557	2.403	.2558	.989	5.484	2.464
SKENNESS	=	-1.165	.353	.235	.902E-1	.979E-1	1.697	-1.194
MINIMUM	=	-12.496	-12.734	.106	11.835	10.085	.773	393.787
MAXIMUM	=	15.648	15.774	16.972	13.957	14.295	20953.211	1033.838

EAST & NORTH								
COVARIANCE	=	-4.678	* SAMPLE SIZE = 3648 POINTS					
STD. ERR. OF COVARIANCE	=	.412						
STD. DEV. OF COVARIANCE	=	24.866	* SPANNING RANGE					
CORRELATION COEFFICIENT	=	-.156	* FROM 78- VII-30 17.07.30					
VECTOR MEAN	=	1.339	* TO 78- IX -06 17.52.30					
VECTOR VARIANCE	=	29.963	* DURATION 38.03 DAYS					
VECTOR STD. DEV.	=	5.474						

DATA/ 6520SB120A Table III-1b: Statistics for VMWR on W2.

VARIABLE	EAST	NORTH	SPEED
UNITS	M/SEC	M/SEC	M/SEC
MEAN	-1.210	-0.561	5.779
STD. ERR.	.328E-1	.427E-1	.208E-1
VARIANCE	13.796	23.349	5.527
STD. DEV.	3.714	4.832	2.351
KURTOSIS	2.496	1.952	2.813
SKEWNESS	-0.116E-1	0.112	0.582
MINIMUM	-10.582	-12.550	.673E-1
MAXIMUM	9.218	10.287	12.609

EAST & NORTH		SAMPLE SIZE = 12810 POINTS	
COVARIANCE	-0.789	0.267	SPANNING RANGE
STD. ERR. OF COVARIANCE	.173	.267	FROM 78-VII-30 14:30:00
STD. DEV. OF COVARIANCE	19.604	.333	TO 78-VIII-17 09:28:00
CORRELATION COEFFICIENT	-0.267	18.573	DURATION 17.79 DAYS
VECTOR MEAN	1.333	4.310	
VECTOR VARIANCE	18.573		
VECTOR STD. DEV.	4.310		

DATA/ H2S1B120A Table III-1c: Statistics for VMWR on H2 (first deployment).

VARIABLE	EAST	NORTH	SPEED
UNITS	M/SEC	M/SEC	M/SEC
MEAN	-0.159	-0.289	5.767
STD. ERR.	.283E-1	.349E-1	.140E-1
VARIANCE	14.598	22.107	3.553
STD. DEV.	3.821	4.702	1.885
KURTOSIS	2.270	1.861	3.023
SKEWNESS	-0.976E-1	0.129	0.366
MINIMUM	-10.544	-10.276	.768E-1
MAXIMUM	10.091	12.250	12.403

EAST & NORTH		SAMPLE SIZE = 18180 POINTS	
COVARIANCE	-1.003	0.116	SPANNING RANGE
STD. ERR. OF COVARIANCE	.116	.558E-1	FROM 78-VII-16 16:30:00
STD. DEV. OF COVARIANCE	15.635	.330	TO 78-VIII-10 22:28:00
CORRELATION COEFFICIENT	-0.558E-1	18.353	DURATION 25.25 DAYS
VECTOR MEAN	.330	4.284	
VECTOR VARIANCE	18.353		
VECTOR STD. DEV.	4.284		

DATA/ H2S2B120A Table III-1d: Statistics for VMWR on H2 (second deployment).

VARIABLE	EAST	NORTH	SPEED
UNITS	M/SEC	M/SEC	M/SEC
MEAN	-0.037	1.004	5.660
STD. ERR.	.088E-1	.411E-1	.280E-1
VARIANCE	10.657	7.574	3.809
STD. DEV.	3.264	2.752	1.873
KURTOSIS	2.870	2.486	2.385
SKEWNESS	-0.884	0.128	0.143
MINIMUM	-3.897	-5.474	.788
MAXIMUM	10.305	8.494	10.752

EAST & NORTH		SAMPLE SIZE = 4480 POINTS	
COVARIANCE	-0.168	0.195	SPANNING RANGE
STD. ERR. OF COVARIANCE	.195	.13.056	FROM 78-VIII-26 18:09:00
STD. DEV. OF COVARIANCE	13.056	.186E-1	TO 78-IX-01 23:27:00
CORRELATION COEFFICIENT	-0.186E-1	4.160	DURATION 6.22 DAYS
VECTOR MEAN	4.160	9.115	
VECTOR VARIANCE	9.115	3.019	
VECTOR STD. DEV.	3.019		

Table III-2a: Five-day statistics for VAWR on W2. The five-day periods start at 0000Z/30 July 78; the final period is only 4 days and 7 hours long.

PERIOD # 5 DAYS	EAST		NORTH		SPEED M/SEC	AIR TEMPERATURE CELSIUS	WATER TEMPERATURE CELSIUS	BAROMETRIC PRESSURE DECIBARS	STATISTIC
	M/SEC	M/SEC	M/SEC	CELSIUS					
*** 6520W ***									
(1)	0.162	-2.328	5.420	13.465	12.420	1017.744			
(2)	-1.967	-5.371	6.167	13.127	11.894	1014.925			
(3)	-3.489	5.703	7.954	13.040	12.684	1013.884			
(4)	1.122	3.575	8.278	13.021	12.817	1001.649			
(5)	6.784	5.003	10.542	12.385	12.495	1008.759			MEAN
(6)	5.643	-1.106	5.951	12.417	12.488	1027.988			
(7)	4.000	-1.427	5.956	12.575	12.448	1020.291			
(8)	-5.635	2.559	7.472	12.590	12.574	1007.128			
(1)	12.236	12.977	1.287	0.43	0.430	17.273			
(2)	3.598	5.492	3.777	0.22	0.286	5.464			
(3)	14.887	10.323	6.651	0.11	0.731	30.799			
(4)	14.691	56.229	16.432	0.11	0.616	38.435			
(5)	16.496	26.562	2.970	0.49	0.268	73.753			VARIANCE
(6)	4.976	1.955	4.576	0.057	0.084	15.737			
(7)	11.414	12.053	6.028	0.009	0.183	18.884			
(8)	24.424	5.336	12.227	0.41	0.343	19.385			
(1)	3.498	3.602	1.134	0.209	0.656	4.156			
(2)	1.897	2.343	1.944	0.148	0.535	2.338			
(3)	3.858	3.213	2.579	0.107	0.855	5.550			
(4)	3.833	7.499	4.054	0.109	0.785	6.200			STANDARD
(5)	4.062	5.154	1.723	0.222	0.517	8.588			DEVIATION
(6)	2.231	1.398	2.139	0.240	0.291	3.967			
(7)	3.379	3.472	2.455	0.097	0.428	4.346			
(8)	4.942	2.310	3.497	0.204	0.585	4.403			
(1)	0.039	0.460	0.522	0.101	0.058	0.537			
(2)	0.494	0.230	0.0845	0.656	0.010	0.257			
(3)	0.767	-0.1065	0.181	1.139	0.821	1.089			
(4)	0.262	0.283	0.143	0.155	0.492	0.547			
(5)	0.909	0.017	0.542	0.365	0.351	0.328			SKEWNESS
(6)	0.476	0.403	0.444	0.316	0.085	0.137			
(7)	0.872	0.123	0.289	0.411	0.415	0.0588			
(8)	0.513	0.222	0.255	1.385	0.015	0.0318			
(1)	1.780	2.028	3.101	2.597	2.266	1.588			
(2)	2.825	2.204	2.651	2.518	2.114	2.033			
(3)	2.627	3.987	1.729	4.602	2.546	3.799			
(4)	2.642	2.088	1.779	4.088	3.285	2.031			
(5)	2.526	1.707	2.984	1.827	2.674	1.576			KURTOSIS
(6)	2.755	2.932	2.600	2.013	2.743	1.621			
(7)	2.692	2.058	2.153	2.575	2.775	2.144			
(8)	2.259	2.199	1.978	4.729	2.811	1.388			
(1)	-7.164	-8.223	2.558	13.046	10.869	1011.086			
(2)	-7.268	-11.074	1.601	12.880	10.441	1011.283			
(3)	-9.551	-0.201	2.400	12.840	10.618	999.080			
(4)	-6.989	-12.734	0.106	12.717	10.085	993.787			
(5)	-4.268	-0.327	6.686	11.895	11.139	993.898			MINIMUM
(6)	0.573	-5.488	1.543	11.982	11.606	1021.572			
(7)	-4.821	-9.179	0.555	12.386	11.512	1011.985			
(8)	-12.496	-3.083	0.316	12.381	10.915	1000.457			
(1)	6.262	5.796	8.815	13.957	13.883	1022.466			
(2)	1.611	0.096	11.924	13.533	12.927	1020.130			
(3)	5.266	10.775	12.137	13.384	14.016	1020.829			
(4)	15.648	14.181	16.972	13.339	14.107	1013.659			
(5)	13.889	15.774	16.049	12.722	13.613	1021.859			MAXIMUM
(6)	11.191	1.713	11.197	12.871	13.286	1033.838			
(7)	9.152	4.894	10.687	12.835	13.564	1028.480			
(8)	5.877	8.255	12.766	13.379	14.295	1013.237			

Table III-2b: Five-day statistics for VMWR on W2. The five-day periods start at 0000Z/30 July 78; the final (fourth) period is only 3 days 9.5 hours long.

*PERIOD	EAST	NORTH	*** 6520S WIND ***			STATISTIC
			M/SEC	M/SEC	M/SEC	
* 5 DAYS						
* (1)	-0.003	-1.885	4.356			
* (2)	-1.668	-4.881	5.608			
* (3)	-4.067	4.742	7.456			
* (4)	2.111	-0.292	5.403			
* (5)						MEAN
* (6)						
* (7)						
* (8)						
* (9)						
* (10)	7.354	9.476	1.407			
* (11)	3.405	4.147	2.698			
* (12)	14.775	8.120	6.333			
* (13)	10.752	20.792	6.898			
* (14)						VARIANCE
* (15)						
* (16)						
* (17)						
* (18)						
* (19)						
* (20)	2.712	3.078	1.186			
* (21)	1.845	2.036	1.643			
* (22)	3.844	2.850	2.517			
* (23)	3.279	4.560	2.626			
* (24)						STANDARD
* (25)						DEVIATION
* (26)						
* (27)						
* (28)						
* (29)						
* (30)	-0.130	-0.309	-0.715			
* (31)	-0.415	-0.311	-0.111			
* (32)	-0.743	-1.126	-0.0857			
* (33)	-0.301	-0.926	-0.461			
* (34)						SKEWNESS
* (35)						
* (36)						
* (37)						
* (38)						
* (39)						
* (40)	1.520	1.955	2.767			
* (41)	2.362	2.306	2.542			
* (42)	2.561	4.378	1.715			
* (43)	2.250	3.193	3.071			
* (44)						KURTOSIS
* (45)						
* (46)						
* (47)						
* (48)						
* (49)						
* (50)	-6.462	-7.514	1.260			
* (51)	-7.300	-9.442	1.475			
* (52)	-10.582	-5.753	2.020			
* (53)	-6.036	-12.550	-0.673			
* (54)						MINIMUM
* (55)						
* (56)						
* (57)						
* (58)						
* (59)						
* (60)	5.536	5.096	7.981			
* (61)	2.733	-0.487	9.525			
* (62)	5.240	10.287	12.180			
* (63)	9.218	6.925	12.609			
* (64)						MAXIMUM
* (65)						
* (66)						
* (67)						
* (68)						

Table III-2c: Five-day statistics for VMWRs on H2. The five-day periods start at 0000Z/30 July 78. Periods 1-3 are the first deployment, 6-7 the second deployment. Period 3 is only 1 day 22.5 hours long. Period 6 starts late, is only 2 days 6 hours long. Period 7 is only 3 days, 23.5 hours long.

PERIOD	*** H2 WIND ***			STATISTIC
	EAST	NORTH	SPEED	
5 DAYS	M/SEC	M/SEC	M/SEC	
(1)	-0.025	-0.667	4.331	
(2)	-2.233	-4.544	5.638	
(3)	-4.113	3.945	6.423	
(4)				
(5)				MEAN
(6)	4.407	0.980	5.243	
(7)	3.829	1.018	5.894	
(8)				
(1)	7.817	12.015	1.521	
(2)	2.884	4.985	2.835	
(3)	1.280	12.581	5.088	
(4)				
(5)				VARIANCE
(6)	3.778	5.768	2.437	
(7)	14.417	8.592	3.960	
(8)				
(1)	2.796	3.466	1.233	
(2)	1.698	2.233	1.684	
(3)	1.131	3.547	2.256	
(4)				
(5)				STANDARD
(6)	1.944	2.402	1.561	DEVIATION
(7)	3.797	2.931	1.990	
(8)				
(1)	-0.194	0.190	0.319	
(2)	-0.278	0.495	-0.0666	
(3)	-0.414	-0.255	0.242	
(4)				
(5)				SKENNESS
(6)	-0.783	-0.395	-0.321	
(7)	-0.698	0.284	-0.232	
(8)				
(1)	1.679	1.895	2.469	
(2)	2.252	2.471	2.692	
(3)	2.984	1.759	1.734	
(4)				
(5)				KURTOSIS
(6)	2.974	2.180	2.325	
(7)	2.180	2.457	2.291	
(8)				
(1)	-6.409	-7.247	1.567	
(2)	-6.719	-9.333	0.937	
(3)	-7.009	-4.006	2.200	
(4)				
(5)				MINIMUM
(6)	-0.791	-4.912	0.982	
(7)	-3.897	-5.474	0.788	
(8)				
(1)	5.296	8.062	8.886	
(2)	2.137	1.396	9.577	
(3)	-1.353	10.039	11.246	
(4)				
(5)				MAXIMUM
(6)	7.723	5.596	8.626	
(7)	10.305	8.494	10.752	
(8)				

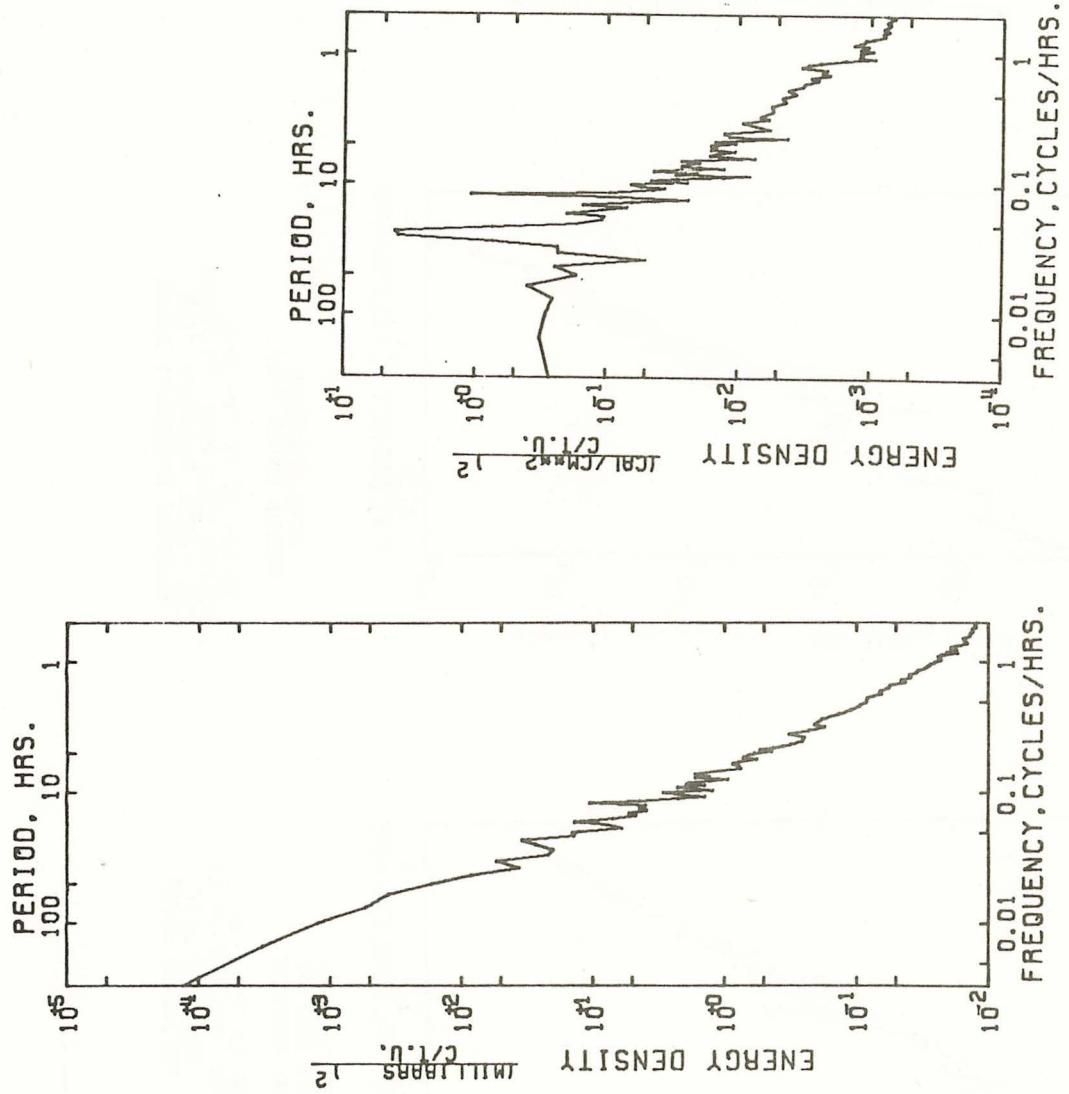


Figure III-9: Spectra from VAWR on W2.

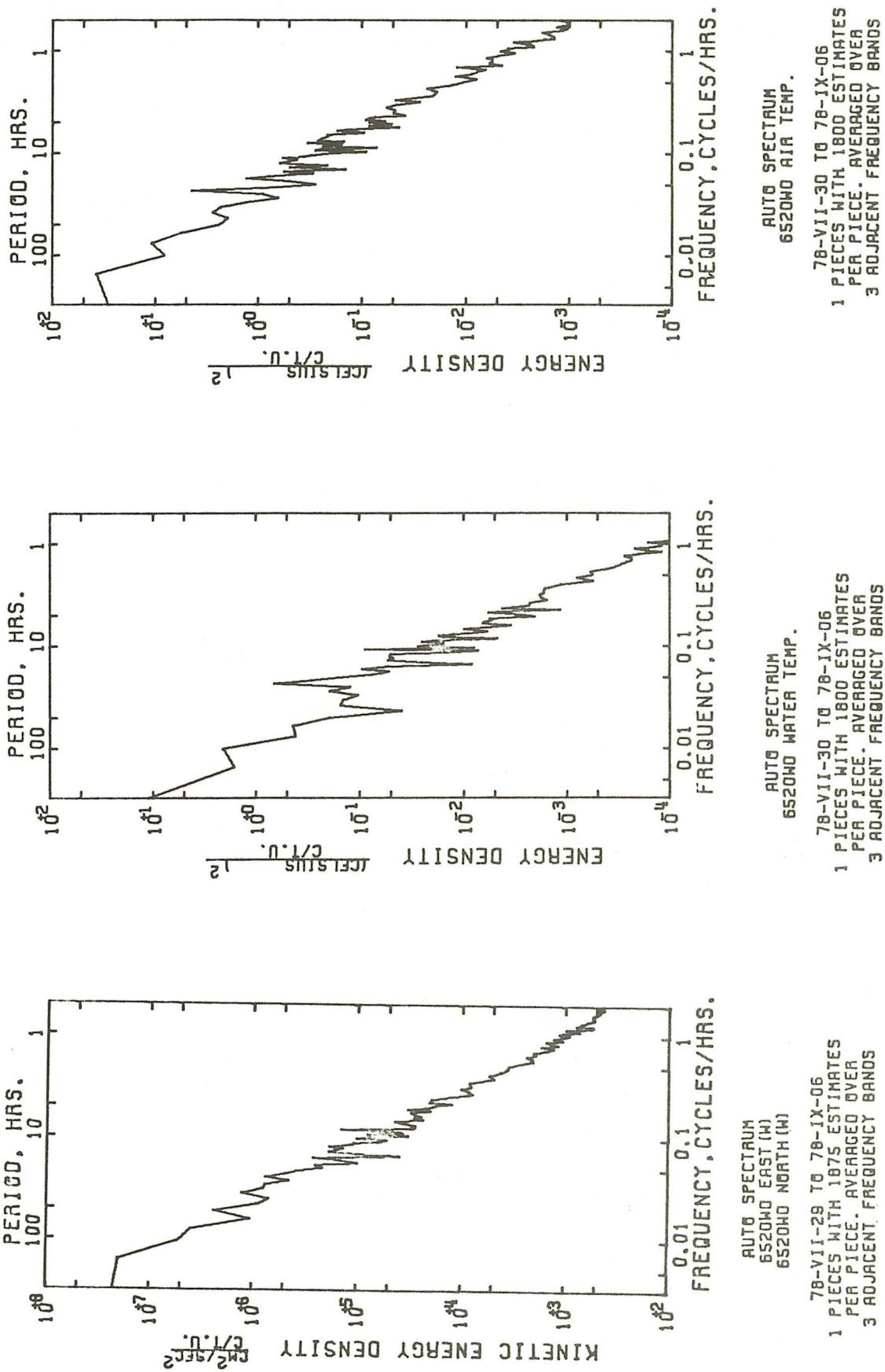
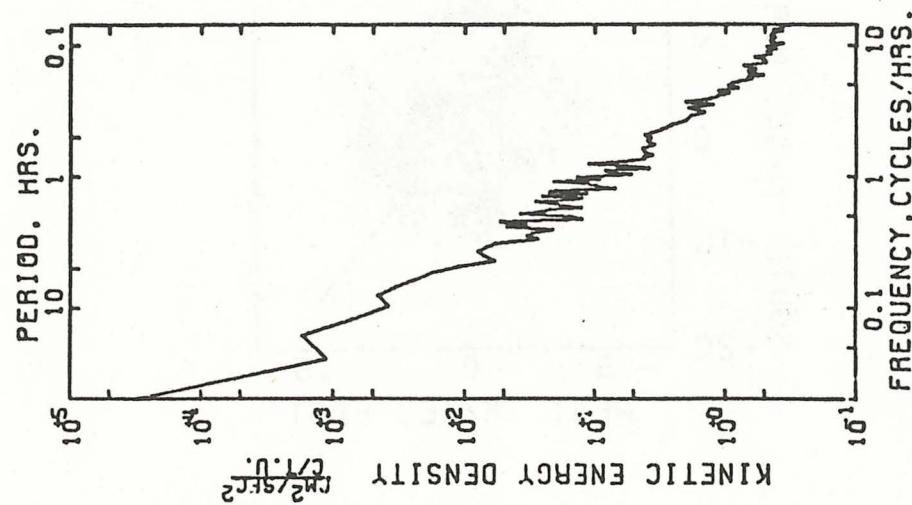
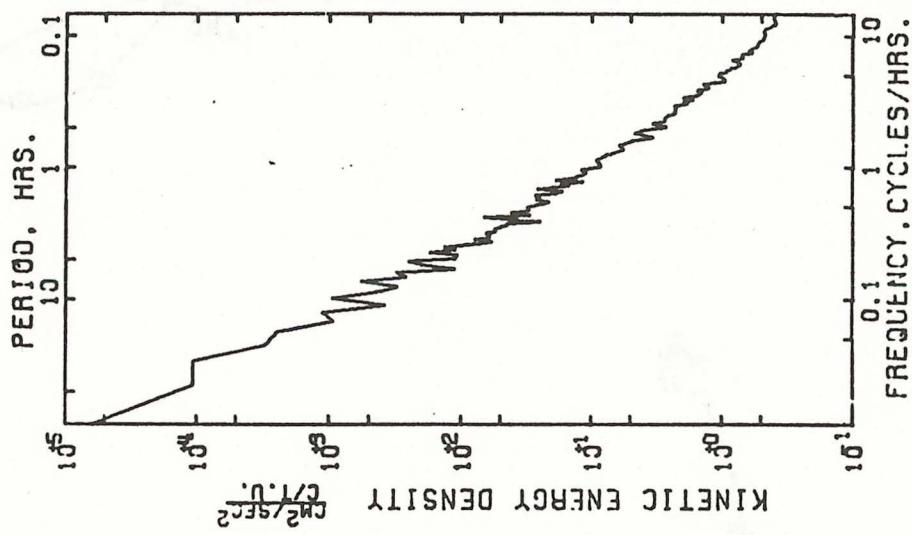


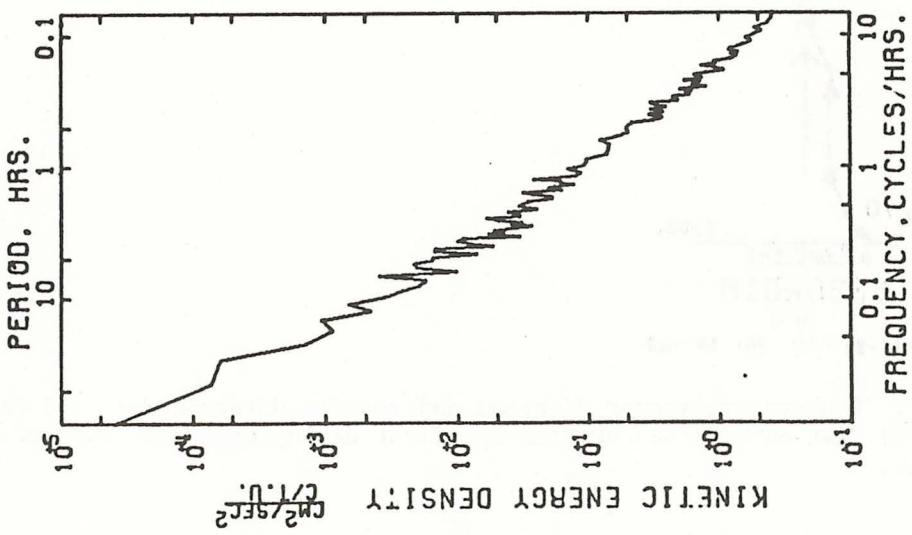
Figure III-9 (continued)



AUTO SPECTRUM
H2S2B120A EAST COMP.
H2S2B120A NORTH COMP.
WIND
78-VIII-26 TO 78-IX-01
1 PIECES WITH 2187 ESTIMATES
1 PER PIECE, AVERAGED OVER
3 ADJACENT FREQUENCY BANDS

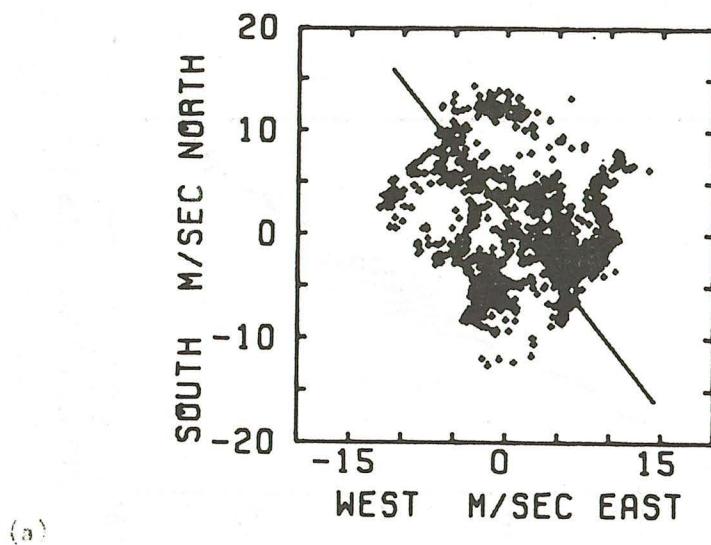


AUTO SPECTRUM
H2S1B120A EAST COMP.
H2S1B120A NORTH COMP.
WIND
78-VII-16 TO 78-VIII-07
2 PIECES WITH 4000 ESTIMATES
1 PER PIECE, AVERAGED OVER
3 ADJACENT FREQUENCY BANDS



AUTO SPECTRUM
6520SB120A EAST COMP.
6520SB120A NORTH COMP.
WIND
78-VII-30 TO 78-VIII-10
1 PIECES WITH 4000 ESTIMATES
1 PER PIECE, AVERAGED OVER
3 ADJACENT FREQUENCY BANDS

Figure III-10: Spectra from VTRs on W2 and U2.



(a)

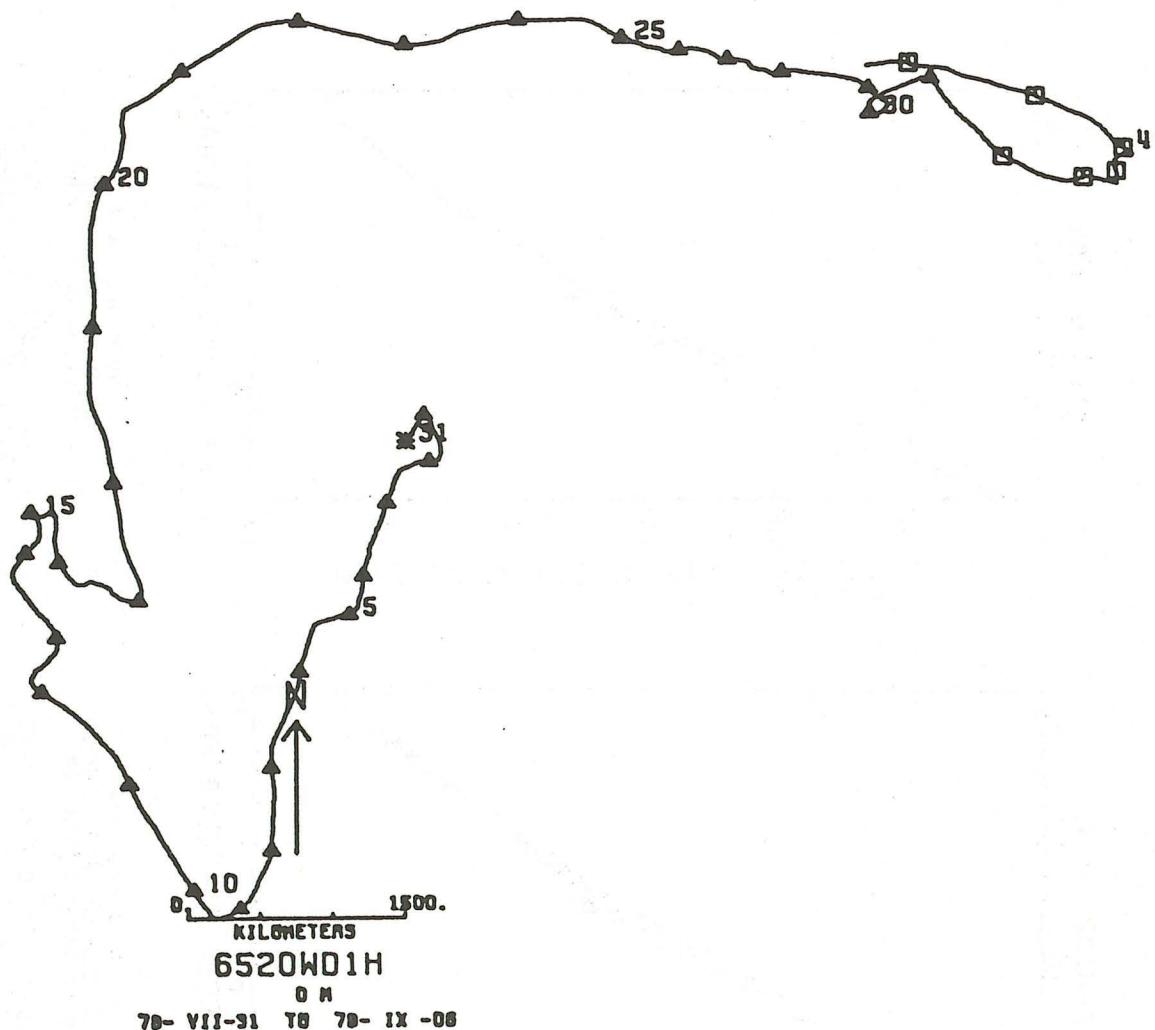


Figure III-11: Progressive vector diagrams and scatter diagrams for (a) VAWR on W2, (b) VMWR on W2, (c) VMWR on H2, first deployment, and (d) second deployment.

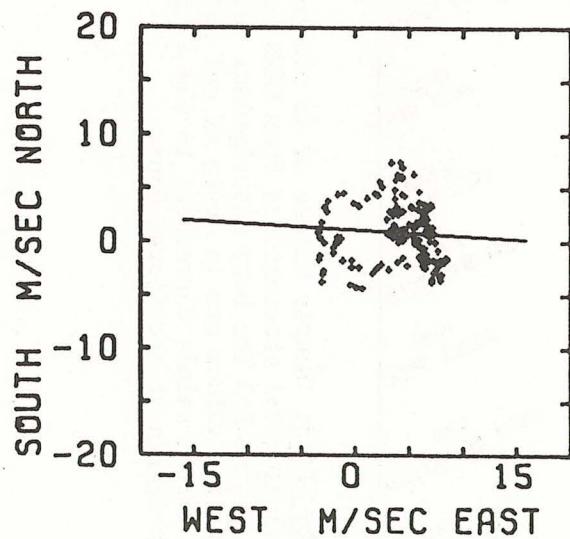
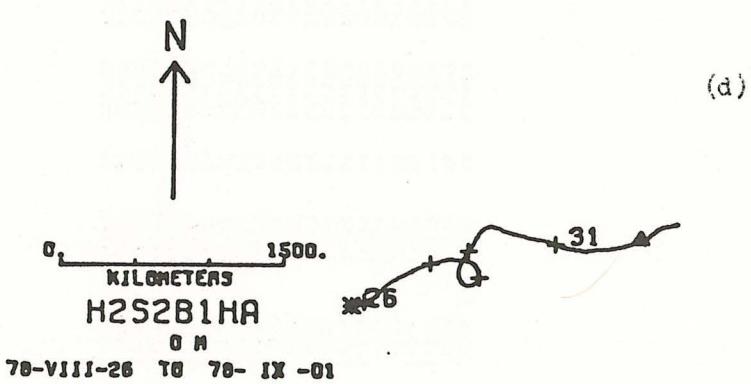
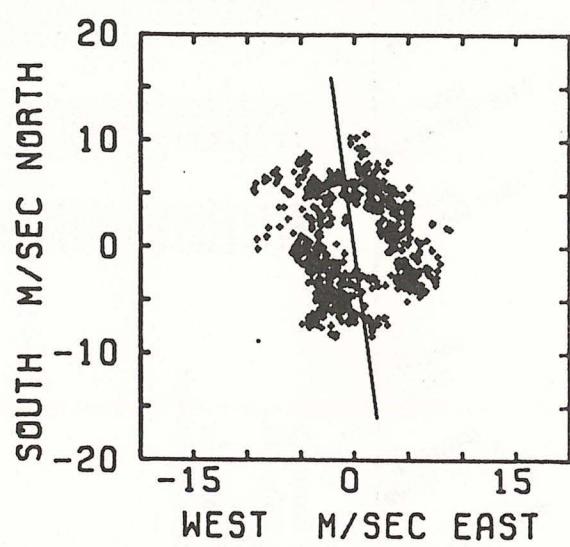
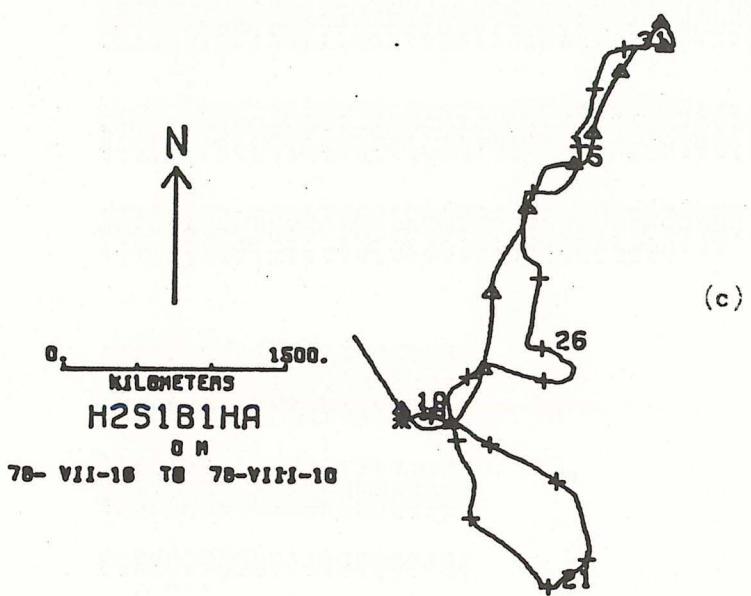
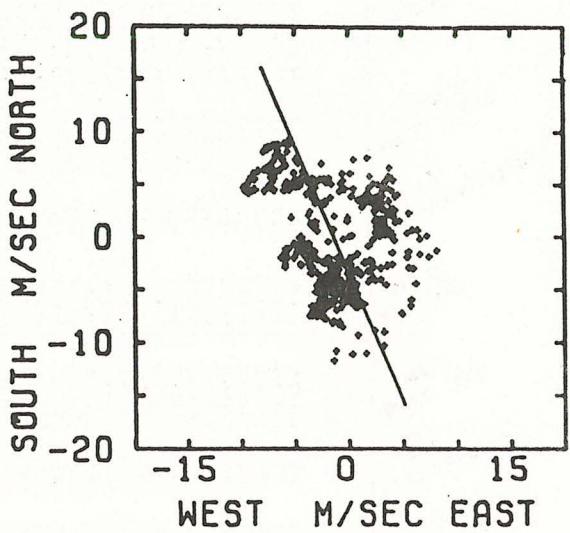
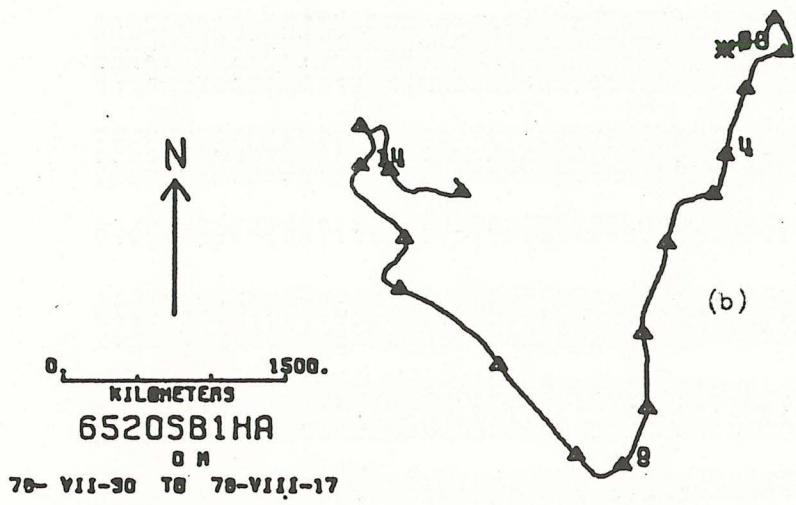


Table III-3: Hourly values of 15 minute average meteorological observations from VAWR on buoy W2. See Figure I-3 for buoy description. Solar radiation values are in units of $\text{cal cm}^{-2} \text{ min}^{-1}$. The listed values correspond to the 15 minute period that starts at the listed hour.

SOLAR RADIATION		WIND SPEED (m/s)		WIND DIRECTION		WATER HEAD (m)		AIR TEMP (deg C)		RH (%)		NORTHWARD WIND		ESTWARD WIND		MILLIBARS		SOLAR RADIATION	
-1.0456	1.0456	-2.725	7.215	202	13.436	11.927	.02	1011.5	78080306	*6.436	194	12.357	.33	1013.3	78080518	THE THERMOGRAPH MILLIBARS			
-1.0456	1.0456	-2.896	7.605	205	13.429	11.765	.05	1011.5	78080307	*7.423	7.477	1.91	13.319	12.340	.07	1013.3	78080519		
-1.0456	1.0456	-2.626	7.550	199	13.406	11.823	.12	1011.2	78080308	*7.487	8.098	1.91	13.283	12.002	.02	1013.6	78080520		
-1.0456	1.0456	-2.779	7.777	201	13.402	11.972	.09	1011.2	78080309	*6.896	8.034	2.14	13.283	12.002	.00	1013.9	78080521		
-1.0456	1.0456	-3.030	7.837	200	13.362	12.081	.14	1011.4	78080310	*4.696	8.119	8.782	2.02	12.162	.00	1014.3	78080522		
-1.0456	1.0456	-2.610	7.612	200	13.264	12.365	.27	1011.4	78080311	*3.137	8.446	8.916	2.00	13.246	12.155	.00	1014.3	78080523	
-1.0456	1.0456	-2.608	7.441	200	13.264	12.365	.27	1011.4	78080312	*3.137	8.446	8.916	2.00	13.246	12.155	.00	1014.3	78080523	
-1.0456	1.0456	-5.015	6.554	209	13.116	12.567	.33	1011.3	78080312	*1.063	9.356	9.416	1.86	13.219	12.134	.00	1013.3	78080600	
-1.0456	1.0456	-2.505	5.631	205	13.066	12.590	.32	1011.3	78080313	*8.669	9.383	9.413	1.85	13.207	11.915	.00	1013.9	78080601	
-1.0456	1.0456	-4.443	4.727	196	13.047	12.549	.20	1011.2	78080313	*5.151	9.669	9.582	1.83	13.200	11.693	.00	1013.9	78080602	
-1.0456	1.0456	-4.942	4.958	175	13.034	12.538	.14	1011.1	78080315	*1.420	8.998	9.010	1.89	13.179	11.847	.00	1013.7	78080603	
-1.0456	1.0456	-5.925	5.936	165	13.104	11.985	.10	1011.1	78080316	*8.662	9.045	9.195	1.89	13.153	11.995	.00	1013.6	78080604	
-1.0456	1.0456	-4.449	5.492	201	13.300	11.960	.05	1011.7	78080317	*2.706	8.650	8.959	1.97	13.155	12.011	.00	1013.6	78080605	
-1.0456	1.0456	-1.295	3.181	202	13.300	11.960	.05	1011.7	78080317	*2.706	8.650	8.959	1.97	13.155	12.011	.00	1013.6	78080605	
-1.0456	1.0456	-1.295	3.181	202	13.300	11.960	.05	1011.7	78080317	*2.706	8.650	8.959	1.97	13.155	12.011	.00	1013.6	78080605	
-1.0456	1.0456	-3.195	3.615	211	13.351	11.986	.05	1011.6	78080318	*3.323	8.397	8.397	2.01	13.152	12.019	.03	1013.8	78080606	
-1.0456	1.0456	-4.240	4.548	201	13.384	11.992	.03	1011.5	78080318	*4.462	8.109	9.256	2.08	13.145	11.811	.04	1014.3	78080607	
-1.0456	1.0456	-6.121	6.711	189	13.397	12.321	.02	1011.3	78080320	*4.027	8.228	9.161	2.06	13.130	11.545	.05	1014.6	78080608	
-1.0456	1.0456	-1.517	1.517	6.238	194	13.390	.00	1011.7	78080321	*8.310	9.267	9.279	2.03	13.124	11.473	.09	1014.5	78080609	
-1.0456	1.0456	-6.022	6.022	175	13.371	12.538	.00	1011.8	78080322	*3.620	8.210	9.028	2.03	13.130	11.392	.16	1014.9	78080610	
-1.0456	1.0456	-1.740	1.740	6.324	195	13.371	.00	1011.9	78080323	*3.261	8.214	8.952	2.01	13.131	11.486	.21	1015.2	78080611	
-1.0456	1.0456	-2.276	5.933	192	13.390	12.590	.00	1011.9	78080323	*4.096	7.576	8.612	2.08	13.131	11.567	.02	1015.4	78080612	
-1.0456	1.0456	-5.631	5.631	189	13.400	12.449	.00	1011.9	78080401	*1.062	9.062	9.062	2.03	13.118	11.536	.03	1015.6	78080613	
-1.0456	1.0456	-5.626	5.626	180	12.971	12.700	.00	1011.7	78080402	*3.949	7.432	8.332	2.03	13.085	11.338	.24	1015.5	78080614	
-1.0456	1.0456	-5.626	5.626	180	13.009	12.700	.00	1011.4	78080403	*3.931	7.135	8.146	2.08	13.086	11.542	.21	1015.5	78080615	
-1.0456	1.0456	-5.246	5.040	165	13.099	12.564	.00	1011.4	78080404	*1.061	9.399	6.934	2.05	13.079	11.693	.14	1015.5	78080616	
-1.0456	1.0456	-4.769	4.778	183	13.141	12.702	.00	1011.3	78080405	*3.364	6.919	7.693	2.05	13.063	11.369	.10	1015.5	78080617	
-1.0456	1.0456	-3.125	3.185	191	13.181	12.614	.01	1011.5	78080406	*2.046	7.422	7.693	1.95	13.050	12.206	.07	1015.4	78080618	
-1.0456	1.0456	-1.121	1.121	3.111	193	13.276	12.825	.08	1011.5	78080407	*1.537	6.615	6.615	1.93	13.042	10.659	.07	1016.0	78080619
-1.0456	1.0456	-6.443	6.443	205	13.284	12.982	.00	1011.4	78080407	*7.56	7.132	8.075	2.09	13.052	11.444	.00	1016.4	78080620	
-1.0456	1.0456	-3.113	3.113	195	13.284	12.982	.00	1011.4	78080407	*1.92	7.075	7.075	1.78	13.052	11.444	.00	1016.4	78080621	
-1.0456	1.0456	-2.296	3.874	203	13.336	12.531	.13	1012.2	78080410	*1.92	6.581	6.581	1.78	13.052	11.118	.00	1016.5	78080622	
-1.0456	1.0456	-3.773	3.773	209	13.361	12.691	.25	1012.0	78080411	*0.41	6.663	6.663	1.80	13.040	11.153	.00	1016.5	78080623	
-1.0456	1.0456	-1.875	1.875	4.034	202	13.391	12.816	.26	1012.6	78080412	*4.882	6.477	6.495	1.75	13.031	11.052	.00	1016.5	78080624
-1.0456	1.0456	-5.424	5.424	177	13.371	12.816	.07	1011.9	78080413	*1.611	7.428	7.428	1.67	13.016	11.049	.00	1016.4	78080625	
-1.0456	1.0456	-2.257	1.857	1.875	187	13.379	12.922	.35	1012.2	78080413	*1.611	6.615	6.615	1.93	13.024	10.659	.07	1016.0	78080626
-1.0456	1.0456	-6.443	5.374	186	13.405	12.559	.08	1011.4	78080417	*7.56	7.132	8.075	2.09	13.045	11.717	.01	1016.4	78080627	
-1.0456	1.0456	-5.030	5.030	192	13.446	12.411	.08	1011.4	78080418	*1.92	6.581	6.581	1.78	13.052	11.444	.00	1016.4	78080628	
-1.0456	1.0456	-4.424	4.424	193	13.446	12.460	.13	1011.4	78080419	*1.92	6.581	6.581	1.78	13.052	11.444	.00	1016.4	78080629	
-1.0456	1.0456	-3.542	3.874	203	13.436	12.531	.13	1011.4	78080419	*1.92	6.581	6.581	1.78	13.052	11.444	.00	1016.4	78080630	
-1.0456	1.0456	-1.875	1.875	3.773	209	13.436	12.691	.25	1012.0	78080419	*0.41	7.333	7.333	1.77	13.040	11.320	.01	1015.5	78080631
-1.0456	1.0456	-5.424	5.424	205	13.436	12.816	.07	1011.9	78080418	*6.621	5.584	5.584	1.86	12.905	11.250	.04	1015.4	78080632	
-1.0456	1.0456	-1.937	1.814	226	13.434	12.922	.35	1012.2	78080419	*1.611	7.428	7.428	1.67	13.024	12.880	.08	1015.5	78080633	
-1.0456	1.0456	-1.218	2.187	217	13.380	12.363	.04	1011.9	78080420	*1.247	6.257	6.257	1.67	13.016	11.743	.14	1015.5	78080634	
-1.0456	1.0456	-1.938	1.938	183	13.403	12.438	.37	1012.2	78080421	*1.17	7.775	7.775	1.77	12.999	10.459	.00	1016.3	78080635	
-1.0456	1.0456	-1.04	2.05	177	13.454	12.766	.33	1012.2	78080422	*6.76	6.351	6.351	1.77	12.999	10.823	.58	1015.5	78080636	
-1.0456	1.0456	-2.078	2.078	217	13.464	12.604	.17	1011.8	78080416	*1.17	7.279	7.279	1.77	12.933	11.236	.00	1015.7	78080637	
-1.0456	1.0456	-1.217	2.132	176	13.376	12.581	.15	1012.7	78080417	*1.17	7.403	7.403	1.77	12.931	11.320	.01	1015.5	78080638	
-1.0456	1.0456	-2.265	2.265	205	13.376	12.691	.07	1011.9	78080418	*8.383	8.135	8.135	1.77	12.979	12.016	.88	1015.8	78080639	
-1.0456	1.0456	-1.937	1.814	226	13.434	12.543	.04	1011.9	78080419	*6.621	5.584	5.584	1.86	12.905	11.250	.80	1015.9	78080640	
-1.0456	1.0456	-2.187	2.187	217	13.380	12.363	.04	1012.0	78080420	*1.247	6.257	6.257	1.67	13.024	12.880	.07	1015.5	78080641	
-1.0456	1.0456	-0.97	3.021	271	13.124	12.035	.23	1011.3	78080503	*1.171	6.154	6.154	1.77	12.996	11.788	.26	1015.9	78080642	
-1.0456	1.0456	-2.631	2.631	217	13.084	12.454	.22	1012.3	78080504	*5.351	6.334	6.351	1.77	13.024	12.990	.91	1016.0	78080643	
-1.0456	1.0456	-2.333	2.333	232	13.142	12.557	.00	1012.5	78080502	*5.672	5.224	5.224	1.77	12.979	12.027	.48	1015.9	78080644	
-1.0456	1.0456	-1.674	4.3																

TIME (hrs)		WIND SPEED (m/s)		WIND HEADING (deg T)		WATER TEMP (deg C)		AIR TEMP (deg C)		BRAKE PRESSURE		TIME (hrs)		WIND SPEED (m/s)		WIND HEADING (deg T)		WATER TEMP (deg C)		AIR TEMP (deg C)		BRAKE PRESSURE	
0.0	0.0	10.965	0.03	1017.5	78080806	-6.544	9.526	11.557	325	13.067	*1.4	1015.6	78081019	10.965	0.03	1017.5	78081019	10.965	0.02	1015.3	78081020		
0.5	0.5	2107	13.011	11.733	1017.6	78080807	-6.587	9.940	11.025	326	13.071	*1.4	1015.6	78081020	11.733	0.01	1015.2	78081021	11.733	0.01	1015.3	78081022	
1.0	1.0	319	13.003	11.665	22	1017.7	78080808	-6.662	10.111	12.018	326	13.076	*1.4	1015.6	78081022	11.665	0.01	1015.2	78081023	11.665	0.01	1015.3	78081024
1.5	1.5	4272	5.052	12.981	11.592	78080809	-6.124	9.640	11.613	327	13.066	*1.4	1015.6	78081024	11.592	0.01	1015.2	78081025	11.592	0.01	1015.3	78081026	
2.0	2.0	6697	4.227	12.981	11.592	78080810	-5.428	10.024	11.399	331	13.110	*1.4	1015.6	78081026	11.592	0.01	1015.2	78081027	11.592	0.01	1015.3	78081028	
2.5	2.5	9430	4.386	12.981	11.592	78080811	-5.120	1018.1	12.025	333	13.121	*1.4	1015.6	78081028	11.592	0.01	1015.2	78081029	11.592	0.01	1015.3	78081030	
3.0	3.0	1124	4.835	204	12.973	78080812	-5.120	1018.6	10.365	337	13.030	*1.4	1015.6	78081030	12.973	0.01	1015.2	78081031	12.973	0.01	1015.3	78081032	
3.5	3.5	1885	4.835	204	12.973	78080813	-5.120	1018.6	10.994	340	13.081	*1.4	1015.6	78081032	12.973	0.01	1015.2	78081033	12.973	0.01	1015.3	78081034	
4.0	4.0	1345	4.498	196	12.979	78080814	-4.40	1018.6	10.994	340	13.085	*1.4	1015.6	78081034	12.979	0.01	1015.2	78081035	12.979	0.01	1015.3	78081036	
4.5	4.5	2267	4.915	209	12.990	78080815	-4.40	1018.9	10.989	340	13.085	*1.4	1015.6	78081036	12.990	0.01	1015.2	78081037	12.990	0.01	1015.3	78081038	
5.0	5.0	2250	5.426	202	12.999	78080816	-4.40	1018.9	10.989	340	13.085	*1.4	1015.6	78081038	12.999	0.01	1015.2	78081039	12.999	0.01	1015.3	78081040	
5.5	5.5	4776	5.922	199	12.999	78080817	-4.40	1018.9	10.989	340	13.085	*1.4	1015.6	78081040	12.999	0.01	1015.2	78081041	12.999	0.01	1015.3	78081042	
6.0	6.0	879	5.455	199	12.999	78080818	-4.40	1018.9	10.989	340	13.085	*1.4	1015.6	78081042	12.999	0.01	1015.2	78081043	12.999	0.01	1015.3	78081044	
6.5	6.5	5759	5.770	203	12.999	78080819	-4.40	1018.9	10.989	340	13.085	*1.4	1015.6	78081044	12.999	0.01	1015.2	78081045	12.999	0.01	1015.3	78081046	
7.0	7.0	9249	5.873	225	12.998	78080820	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081046	12.998	0.01	1015.2	78081047	12.998	0.01	1015.3	78081048	
7.5	7.5	514	5.514	225	12.998	78080821	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081048	12.998	0.01	1015.2	78081049	12.998	0.01	1015.3	78081050	
8.0	8.0	924	5.514	225	12.998	78080822	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081050	12.998	0.01	1015.2	78081051	12.998	0.01	1015.3	78081052	
8.5	8.5	924	5.514	225	12.998	78080823	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081052	12.998	0.01	1015.2	78081053	12.998	0.01	1015.3	78081054	
9.0	9.0	924	5.514	225	12.998	78080824	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081054	12.998	0.01	1015.2	78081055	12.998	0.01	1015.3	78081056	
9.5	9.5	924	5.514	225	12.998	78080825	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081056	12.998	0.01	1015.2	78081057	12.998	0.01	1015.3	78081058	
10.0	10.0	924	5.514	225	12.998	78080826	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081058	12.998	0.01	1015.2	78081059	12.998	0.01	1015.3	78081060	
10.5	10.5	924	5.514	225	12.998	78080827	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081060	12.998	0.01	1015.2	78081061	12.998	0.01	1015.3	78081062	
11.0	11.0	924	5.514	225	12.998	78080828	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081062	12.998	0.01	1015.2	78081063	12.998	0.01	1015.3	78081064	
11.5	11.5	924	5.514	225	12.998	78080829	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081064	12.998	0.01	1015.2	78081065	12.998	0.01	1015.3	78081066	
12.0	12.0	924	5.514	225	12.998	78080830	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081066	12.998	0.01	1015.2	78081067	12.998	0.01	1015.3	78081068	
12.5	12.5	924	5.514	225	12.998	78080831	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081068	12.998	0.01	1015.2	78081069	12.998	0.01	1015.3	78081070	
13.0	13.0	924	5.514	225	12.998	78080832	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081070	12.998	0.01	1015.2	78081071	12.998	0.01	1015.3	78081072	
13.5	13.5	924	5.514	225	12.998	78080833	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081072	12.998	0.01	1015.2	78081073	12.998	0.01	1015.3	78081074	
14.0	14.0	924	5.514	225	12.998	78080834	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081074	12.998	0.01	1015.2	78081075	12.998	0.01	1015.3	78081076	
14.5	14.5	924	5.514	225	12.998	78080835	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081076	12.998	0.01	1015.2	78081077	12.998	0.01	1015.3	78081078	
15.0	15.0	924	5.514	225	12.998	78080836	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081078	12.998	0.01	1015.2	78081079	12.998	0.01	1015.3	78081080	
15.5	15.5	924	5.514	225	12.998	78080837	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081080	12.998	0.01	1015.2	78081081	12.998	0.01	1015.3	78081082	
16.0	16.0	924	5.514	225	12.998	78080838	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081082	12.998	0.01	1015.2	78081083	12.998	0.01	1015.3	78081084	
16.5	16.5	924	5.514	225	12.998	78080839	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081084	12.998	0.01	1015.2	78081085	12.998	0.01	1015.3	78081086	
17.0	17.0	924	5.514	225	12.998	78080840	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081086	12.998	0.01	1015.2	78081087	12.998	0.01	1015.3	78081088	
17.5	17.5	924	5.514	225	12.998	78080841	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081088	12.998	0.01	1015.2	78081089	12.998	0.01	1015.3	78081090	
18.0	18.0	924	5.514	225	12.998	78080842	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081090	12.998	0.01	1015.2	78081091	12.998	0.01	1015.3	78081092	
18.5	18.5	924	5.514	225	12.998	78080843	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081092	12.998	0.01	1015.2	78081093	12.998	0.01	1015.3	78081094	
19.0	19.0	924	5.514	225	12.998	78080844	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081094	12.998	0.01	1015.2	78081095	12.998	0.01	1015.3	78081096	
19.5	19.5	924	5.514	225	12.998	78080845	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081096	12.998	0.01	1015.2	78081097	12.998	0.01	1015.3	78081098	
20.0	20.0	924	5.514	225	12.998	78080846	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081098	12.998	0.01	1015.2	78081099	12.998	0.01	1015.3	78081099	
20.5	20.5	924	5.514	225	12.998	78080847	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081099	12.998	0.01	1015.2	78081100	12.998	0.01	1015.3	78081100	
21.0	21.0	924	5.514	225	12.998	78080848	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081100	12.998	0.01	1015.2	78081101	12.998	0.01	1015.3	78081101	
21.5	21.5	924	5.514	225	12.998	78080849	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081101	12.998	0.01	1015.2	78081102	12.998	0.01	1015.3	78081102	
22.0	22.0	924	5.514	225	12.998	78080850	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081102	12.998	0.01	1015.2	78081103	12.998	0.01	1015.3	78081103	
22.5	22.5	924	5.514	225	12.998	78080851	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081103	12.998	0.01	1015.2	78081104	12.998	0.01	1015.3	78081104	
23.0	23.0	924	5.514	225	12.998	78080852	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081104	12.998	0.01	1015.2	78081105	12.998	0.01	1015.3	78081105	
23.5	23.5	924	5.514	225	12.998	78080853	-4.40	1019.1	10.980	340	13.085	*1.4	1015.6	78081105	12.998	0.01	1015.2	78081106	12.998	0.01	1015.3	78081106	
24.0	24.0	924	5.514																				

SOLAR RADIATION									
WATER TEMP DEG C									
AIR TEMP DEG C									
WIND SPEED M/S									
ERSTWORLD WIND	NORTHWARD WIND	THEMODYNAMIC	WATER HEAD M/S	WIND SPEED M/S	WATER HEAD M/S	THEMODYNAMIC	WATER TEMP DEG C	SOLAR RADIATION	BRIGHTNESS PRESSURE
9.566	9.623	11.952	12.310	*02	1021.0	11.961	11.71	1021.2	74082306
9.133	9.391	11.961	11.71	*05	1021.2	11.661	12.09	1021.0	73082307
9.652	9.481	12.099	11.661	*09	1021.4	12.052	12.24	1021.0	73082308
7.573	3.939	8.536	12.152	*25	1021.0	12.191	12.33	1021.0	78082309
7.281	5.272	5.932	12.162	*21	1020.9	12.162	12.33	1020.9	78082310
10.004	3.502	10.613	12.168	*18	1020.9	12.168	12.33	1020.9	78082310
8.053	4.282	9.118	12.224	*08	1021.3	12.213	12.44	1021.3	73082312
8.226	3.405	9.874	12.213	*08	1021.3	11.876	12.05	1021.3	74082313
8.250	2.545	8.705	12.222	*00	1021.5	12.035	12.35	1021.5	78082314
9.191	5.211	9.205	12.195	*62	1021.5	11.951	12.08	1021.5	78082315
9.177	1.397	9.282	12.190	*00	1021.7	12.029	12.08	1021.7	78082316
9.019	2.338	9.317	12.152	*24	1020.6	12.006	12.06	1021.4	73082317
10.193	1.654	10.360	12.152	*79	1021.4	11.987	12.06	1021.4	74082318
10.153	1.053	10.155	12.152	*83	1020.6	12.006	12.06	1021.7	78082319
8.894	6.292	9.629	9.747	*79	12.010	12.361	12.46	1021.7	78082320
9.443	2.871	7.73	12.222	*00	1021.4	12.956	12.35	1021.3	78082321
9.205	8.352	8.765	12.195	*62	1021.5	12.029	12.35	1021.4	78082322
9.026	1.422	9.090	12.190	*00	1021.7	11.929	12.08	1021.7	78082323
9.177	1.397	9.282	12.190	*12	1021.8	12.014	12.08	1021.7	78082323
9.019	2.338	9.317	12.152	*75	1020.6	12.006	12.06	1021.7	78082323
10.014	1.654	10.155	8.8	11.999	12.489	*00	1021.7	78082323	3.574
10.152	1.052	10.155	8.8	11.999	12.489	*00	1021.7	78082323	9.71
11.111	**731	1.135	9.3	11.983	12.496	*00	1021.7	78082340	**573
10.961	**1.008	1.007	9.5	11.983	12.496	*00	1022.1	74082401	**3.573
10.350	1.008	10.867	8.9	11.985	12.280	*00	1022.1	74082402	**3.426
10.586	**1.67	10.587	8.9	11.995	12.295	*00	1022.6	74082404	**3.450
10.011	1.667	10.146	9.9	11.997	12.032	*03	1022.6	74082406	**3.429
9.013	0.74	9.024	9.4	11.997	12.162	*08	1023.1	74082407	**3.450
9.443	**283	9.447	9.1	12.015	12.036	*17	1023.1	74082407	**3.450
9.472	1.668	9.618	8.0	12.026	12.340	*41	1023.3	74082409	**3.450
9.351	2.523	9.545	8.6	12.033	12.426	*37	1023.6	74082410	**3.450
9.222	1.175	9.792	8.3	12.029	12.347	*04	1023.9	74082411	**3.450
10.286	1.0286	10.454	1.04	12.054	12.534	*10	1024.4	74082412	**3.450
10.074	**774	10.054	9.4	12.082	12.643	*90	1024.4	74082413	**3.450
9.338	2.942	9.790	10.7	12.087	12.764	*87	1025.6	74082414	**3.450
7.859	4.472	8.382	11.4	12.110	12.764	*86	1026.1	74082415	**3.450
5.301	3.032	8.094	11.2	12.119	12.861	*68	1026.6	74082416	**3.450
7.604	**690	8.452	11.5	12.131	12.851	*47	1026.8	74082417	**3.450
6.791	**3.038	7.901	11.0	12.149	12.759	*23	1027.0	74082418	**3.450
5.058	5.525	6.923	12.0	12.143	12.457	*03	1027.4	74082419	**3.450
5.098	**3.791	6.603	12.0	12.151	12.850	*01	1028.4	74082420	**3.450
4.909	3.327	5.976	12.3	12.138	12.950	*00	1029.0	74082421	**3.450
4.944	3.327	5.933	10.5	12.138	12.950	*00	1029.5	74082501	**3.450
5.301	1.774	6.545	10.5	12.138	12.950	*00	1029.5	74082502	**3.450
6.301	1.774	6.597	10.3	12.138	12.950	*00	1030.1	74082505	**3.450
5.039	2.816	5.705	11.8	12.123	12.938	*00	1030.6	74082506	**3.450
5.129	1.914	5.372	11.0	12.104	12.938	*09	1031.1	74082507	**3.450
5.044	**849	5.802	11.9	12.132	12.938	*20	1032.1	74082507	**3.450
5.125	1.901	5.466	11.0	12.115	12.938	*00	1032.6	74082508	**3.450
5.741	1.787	6.013	10.7	12.117	12.938	*00	1033.4	74082509	**3.450
4.055	**316	4.774	10.6	12.114	12.950	*00	1034.4	74082510	**3.450
5.912	1.045	4.554	9.7	12.268	12.75	*51	1032.6	74082511	**3.450
6.301	1.774	6.545	10.5	12.134	12.950	*00	1032.6	74082511	**3.450
5.162	**165	5.103	9.1	12.287	12.915	*80	1032.8	74082512	**3.450
4.955	**712	5.032	9.8	12.349	12.938	*103	1033.1	74082512	**3.450
6.072	**582	6.076	10.9	12.377	12.938	*105	1033.1	74082513	**3.450
6.072	1.224	5.160	10.4	12.426	12.938	*73	1033.3	74082514	**3.450
4.836	**343	5.019	10.5	12.461	12.938	*73	1033.4	74082515	**3.450
3.533	**2.192	4.419	11.9	12.481	12.938	*40	1033.4	74082515	**3.450
3.533	**666	3.552	11.8	12.499	12.938	*25	1033.6	74082517	**3.450

ERTHWARD WIND		NORTHWARD WIND		WIND SPEED		WIND HEADING		WATER TEMP		AIR TEMP (°C)		SOLAR RADIATION		RADAR BARS		TIME (HH:MM:SS)	
*10.275	3.4486	10.850	288	12.668	12.700	*14	1008.1	78090418		*008.7	*02	1007.4	78090419			07:30	VII-30
*11.392	3.879	11.945	288	12.602	12.612	*00	1006.9	78090420		1006.7	*00	1006.7	78090421			17:30	IX-06
*10.973	4.545	11.877	292	12.603	12.723	*00	1007.4	78090422		1006.7	*00	1006.7	78090422			3600-000	SECONDS BETWEEN CYCLES
*11.164	5.347	12.361	295	12.560	12.997	*00	1006.7	78090423		1006.7	*00	1006.7	78090423				
*10.657	5.076	11.813	295	12.570	12.934	*00	1008.2	78090500		1008.1	*00	1006.1	78090500				
*11.179	4.998	12.215	294	12.559	13.032	*00	1006.1	78090501		1005.9	*00	1005.5	78090502				
*10.677	3.910	11.370	290	12.533	12.957	*00	1005.8	78090503		1005.8	*00	1005.8	78090503				
*10.812	4.274	11.676	291	12.537	12.900	*00	1005.5	78090504		1004.8	*00	1004.1	78090504				
*10.421	4.310	11.277	292	12.537	12.909	*00	1004.8	78090505		1004.1	*00	1003.6	78090505				
*11.081	3.555	11.636	287	12.505	12.809	*00	1003.6	78090506		1003.6	*00	1003.6	78090506				
*12.032	5.577	12.517	282	12.473	12.837	*00	1003.4	78090507		1003.4	*00	1003.4	78090507				
*12.293	2.240	12.476	280	12.502	12.840	*00	1003.4	78090508		1003.4	*00	1003.4	78090508				
*12.044	3.242	12.472	285	12.449	12.864	*01	1003.6	78090509		1003.6	*01	1003.6	78090509				
*11.595	3.760	12.135	287	12.438	12.835	*02	1003.6	78090510		1003.6	*02	1003.8	78090510				
*11.534	4.505	12.343	291	12.447	12.881	*03	1003.8	78090511		1003.9	*03	1003.9	78090511				
*10.826	2.763	11.173	284	12.465	12.829	*03	1003.9	78090512		1003.6	*02	1003.6	78090512				
*11.393	2.266	11.616	281	12.440	12.898	*02	1003.8	78090513		1003.8	*02	1003.8	78090513				
*11.997	2.549	12.205	281	12.444	12.961	*10	1003.4	78090514		1003.4	*10	1003.4	78090514				
*11.358	2.579	11.759	287	12.454	11.943	*10	1003.4	78090515		1003.4	*10	1003.4	78090515				
*11.431	2.692	11.744	283	12.451	11.997	*09	1003.3	78090516		1003.3	*09	1003.3	78090516				
*8.619	4.619	10.059	297	12.447	11.985	*04	1003.9	78090517		1003.9	*04	1003.9	78090517				
*5.185	4.996	5.105	344	12.424	11.987	*02	1004.2	78090518		1004.2	*02	1004.2	78090518				
*1.385	2.797	9.199	287	12.413	11.883	*02	1003.8	78090519		1003.8	*02	1003.8	78090519				
*8.764	2.797	9.199	287	12.405	11.956	*02	1003.2	78090520		1003.2	*02	1003.2	78090520				
*9.756	4.406	9.856	278	12.391	11.956	*02	1002.7	78090521		1002.7	*02	1002.7	78090521				
*10.161	5.66	10.177	273	12.405	11.976	*00	1002.7	78090522		1002.7	*00	1002.7	78090522				
*11.358	2.569	11.589	273	12.451	11.997	*09	1003.3	78090523		1003.3	*09	1003.3	78090523				
*11.431	2.692	11.744	283	12.451	11.997	*09	1003.3	78090524		1003.3	*09	1003.3	78090524				
*8.619	4.619	10.059	297	12.447	11.985	*04	1003.9	78090525		1003.9	*04	1003.9	78090525				
*5.185	4.996	5.105	344	12.424	11.987	*02	1004.2	78090526		1004.2	*02	1004.2	78090526				
*1.385	2.797	9.199	287	12.413	11.883	*02	1003.8	78090527		1003.8	*02	1003.8	78090527				
*8.764	2.797	9.199	287	12.405	11.956	*02	1003.2	78090528		1003.2	*02	1003.2	78090528				
*9.756	4.406	9.856	278	12.391	11.956	*02	1002.7	78090529		1002.7	*02	1002.7	78090529				
*10.161	5.66	10.177	273	12.405	11.976	*00	1002.7	78090530		1002.7	*00	1002.7	78090530				
*11.431	2.692	11.744	283	12.451	11.997	*09	1003.3	78090531		1003.3	*09	1003.3	78090531				
*8.619	4.619	10.059	297	12.447	11.985	*04	1003.9	78090532		1003.9	*04	1003.9	78090532				
*5.185	4.996	5.105	344	12.424	11.987	*02	1004.2	78090533		1004.2	*02	1004.2	78090533				
*1.385	2.797	9.199	287	12.413	11.883	*02	1003.8	78090534		1003.8	*02	1003.8	78090534				
*8.764	2.797	9.199	287	12.405	11.956	*02	1003.2	78090535		1003.2	*02	1003.2	78090535				
*9.756	4.406	9.856	278	12.391	11.956	*02	1002.7	78090536		1002.7	*02	1002.7	78090536				
*10.161	5.66	10.177	273	12.405	11.976	*00	1002.7	78090537		1002.7	*00	1002.7	78090537				
*11.431	2.692	11.744	283	12.451	11.997	*09	1003.3	78090538		1003.3	*09	1003.3	78090538				
*8.619	4.619	10.059	297	12.447	11.985	*04	1003.9	78090539		1003.9	*04	1003.9	78090539				
*5.185	4.996	5.105	344	12.424	11.987	*02	1004.2	78090540		1004.2	*02	1004.2	78090540				
*1.385	2.797	9.199	287	12.413	11.883	*02	1003.8	78090541		1003.8	*02	1003.8	78090541				
*8.764	2.797	9.199	287	12.405	11.956	*02	1003.2	78090542		1003.2	*02	1003.2	78090542				
*9.756	4.406	9.856	278	12.391	11.956	*02	1002.7	78090543		1002.7	*02	1002.7	78090543				
*10.161	5.66	10.177	273	12.405	11.976	*00	1002.7	78090544		1002.7	*00	1002.7	78090544				
*11.431	2.692	11.744	283	12.451	11.997	*09	1003.3	78090545		1003.3	*09	1003.3	78090545				
*8.619	4.619	10.059	297	12.447	11.985	*04	1003.9	78090546		1003.9	*04	1003.9	78090546				
*5.185	4.996	5.105	344	12.424	11.987	*02	1004.2	78090547		1004.2	*02	1004.2	78090547				
*1.385	2.797	9.199	287	12.413	11.883	*02	1003.8	78090548		1003.8	*02	1003.8	78090548				
*8.764	2.797	9.199	287	12.405	11.956	*02	1003.2	78090549		1003.2	*02	1003.2	78090549				
*9.756	4.406	9.856	278	12.391	11.956	*02	1002.7	78090550		1002.7	*02	1002.7	78090550				
*10.161	5.66	10.177	273	12.405	11.976	*00	1002.7	78090551		1002.7	*00	1002.7	78090551				
*11.431	2.692	11.744	283	12.451	11.997	*09	1003.3	78090552		1003.3	*09	1003.3	78090552				
*8.619	4.619	10.059	297	12.447	11.985	*04	1003.9	78090553		1003.9	*04	1003.9	78090553				
*5.185	4.996	5.105	344	12.424	11.987	*02	1004.2	78090554		1004.2	*02	1004.2	78090554				
*1.385	2.797	9.199	287	12.413	11.883	*02	1003.8	78090555		1003.8	*02	1003.8	78090555				
*8.764	2.797	9.199	287	12.405	11.956	*02	1003.2	78090556		1003.2	*02	1003.2	78090556				
*9.756	4.406	9.856	278	12.391	11.956	*02	1002.7	78090557		1002.7	*02	1002.7	78090557				
*10.161	5.66	10.177	273	12.405	11.976	*00	1002.7	78090558		1002.7	*00	1002.7	78090558				
*11.431	2.692	11.744	283	12.451	11.997	*09	1003.3	78090559		1003.3	*09	1003.3	78090559				
*8.619	4.619	10.059	297	12.447	11.985	*04	1003.9	78090560		1003.9	*04	1003.9	78090560				
*5.185	4.996	5.105	344	12.424	11.987	*02	1004.2	78090561		1004.2	*02	1004.2	78090561				
*1.385	2.797	9.199	287	12.413	11.883	*02	1003.8	78090562		1003.8	*02	1003.8	78090562				
*8.764	2.797	9.199	287	12.405	11.956	*02	1003.2	78090563		1003.2	*02	1003.2	78090563				
*9.756	4.406	9.856	278	12.391	11.956	*02	1002.7	78090564		1002.7	*02	1002.7	78090564				
*10.161	5.66	10.177	273	12.405	11.976	*00	1002.7	78090565		1002.7	*00	1002.7	78090565				
*11.431	2.692	11.744	283	12.451	11.997	*09	1003.3	78090566		1003.3	*09	1003.3	78090566				
*8.619	4.619	10.059	297	12.447	11.985	*04	1003.9	78090567		1003.9	*04	1003.9	78090567				
*5.185	4.996	5.105	344	12.424	11.987	*02	1004.2	78090568		1004.2	*02	1004.2	78090568				
*1.385	2.797	9.199	287	12.413	11.883	*02	1003.8	78090569		1003.8	*02	1003.8	78090569				
*8.764	2.797	9.199	287	12.405	11.956	*02	1003.2	78090570		1003.2	*02	1003.2	78090570				
*9.756	4.406	9.856	278	12.391	11.												

DEW POINT
(PET —————)
(MANUAL)

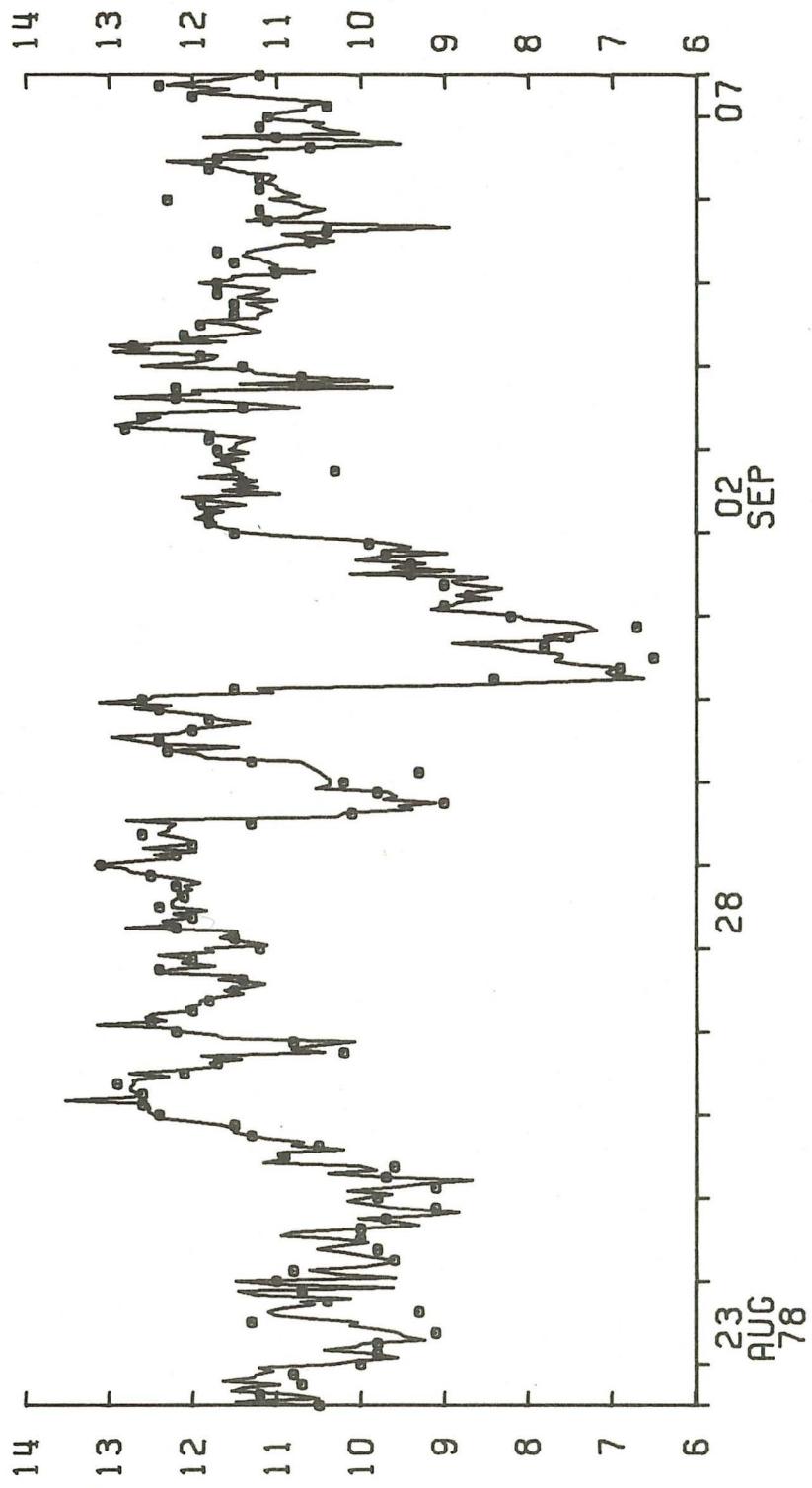
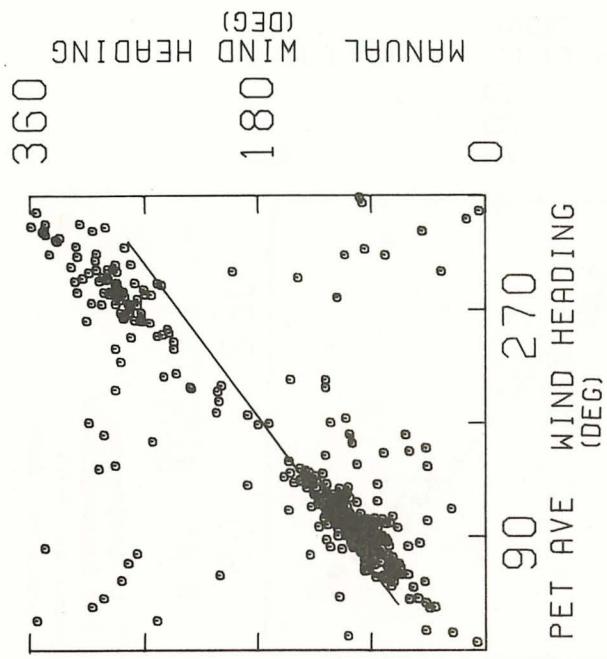
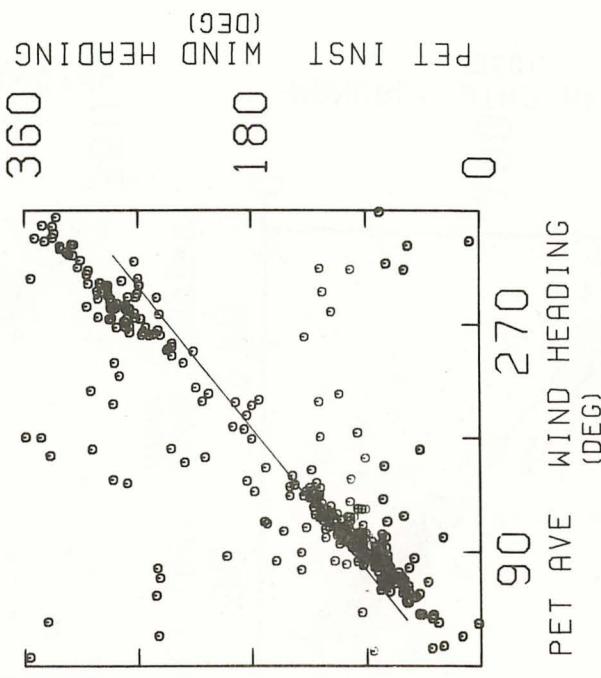


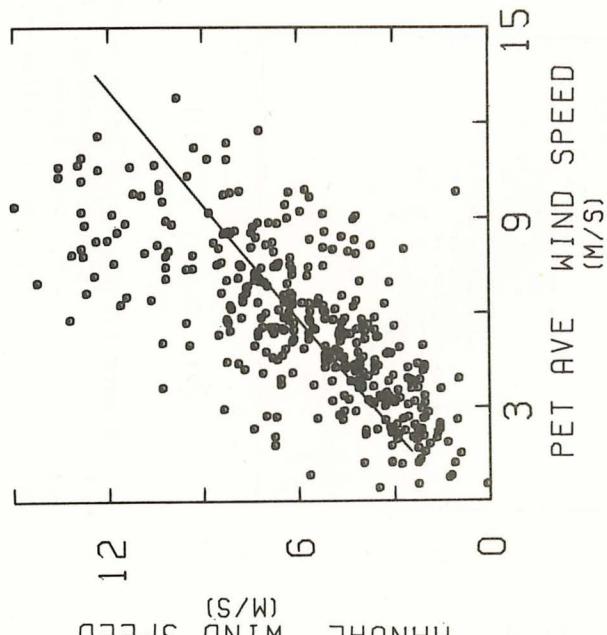
Figure III-12: Leg II Dew Point Intercomparison. PET reading from lithium chloride cell, MANUAL reading from Bendix psychrometer and conversion to dewpoint (see text).



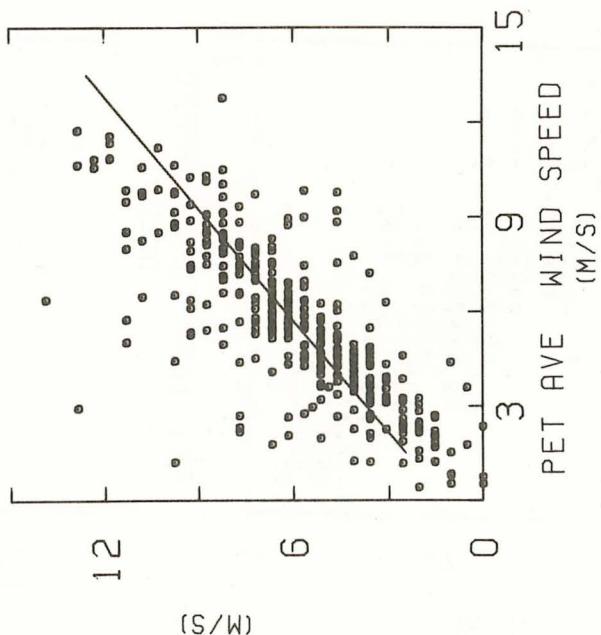
(c)



(d)

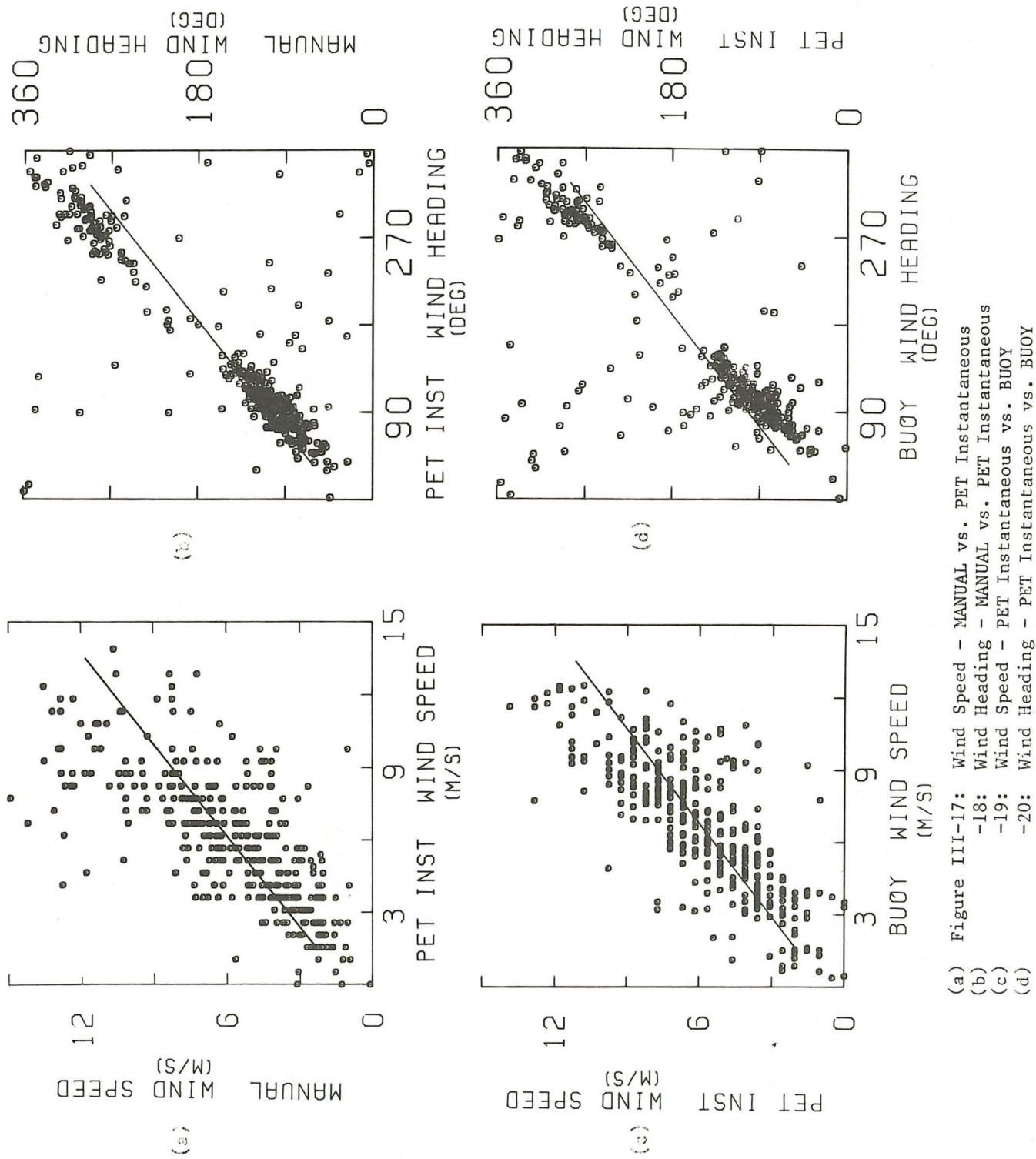


(a)

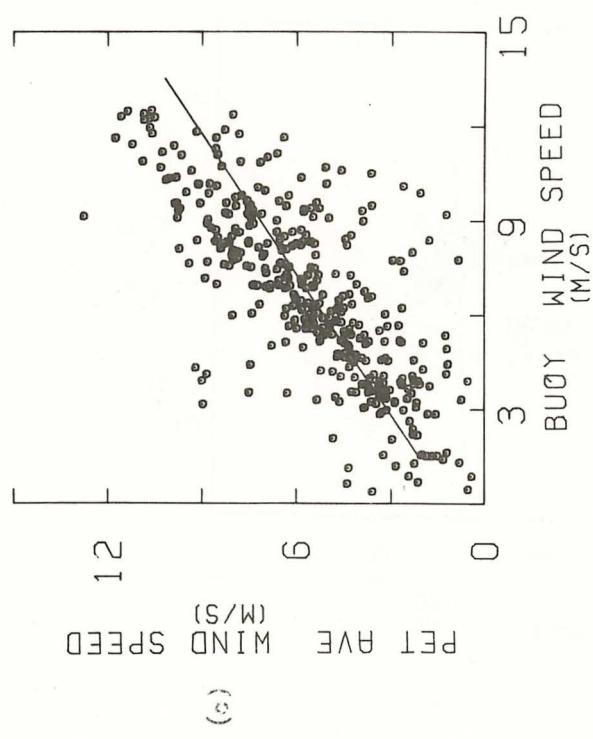
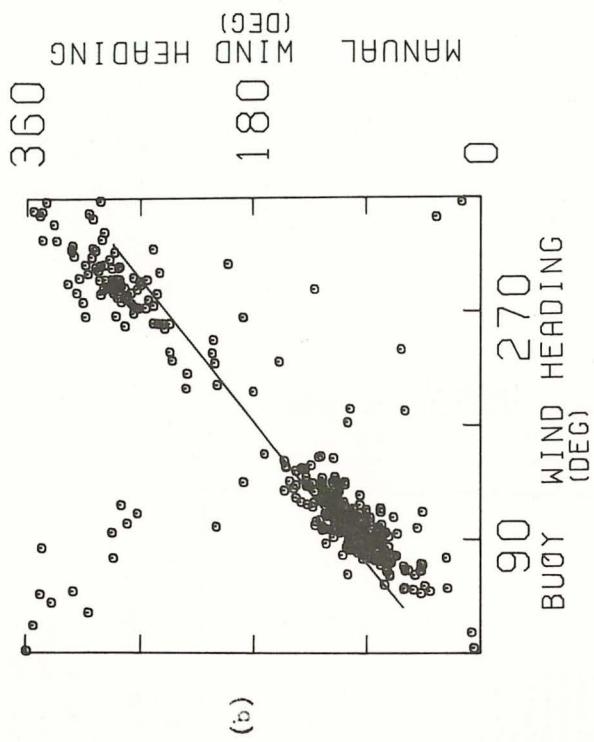
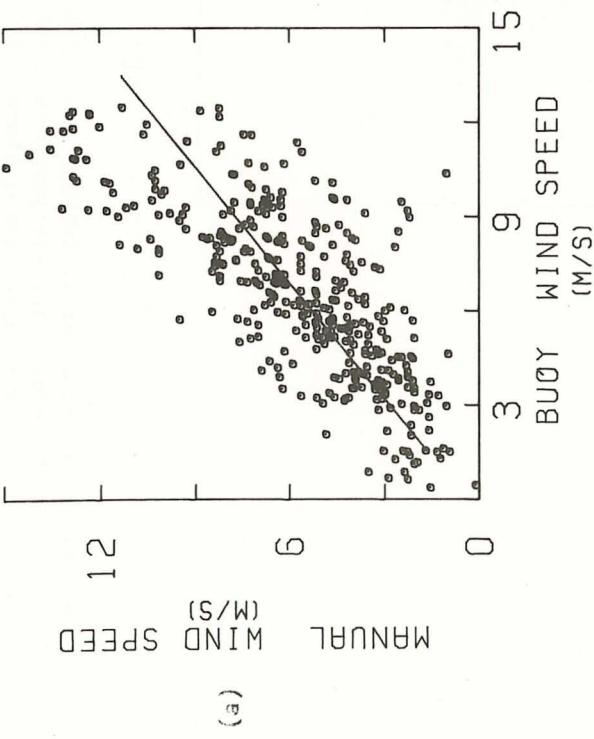


(b)

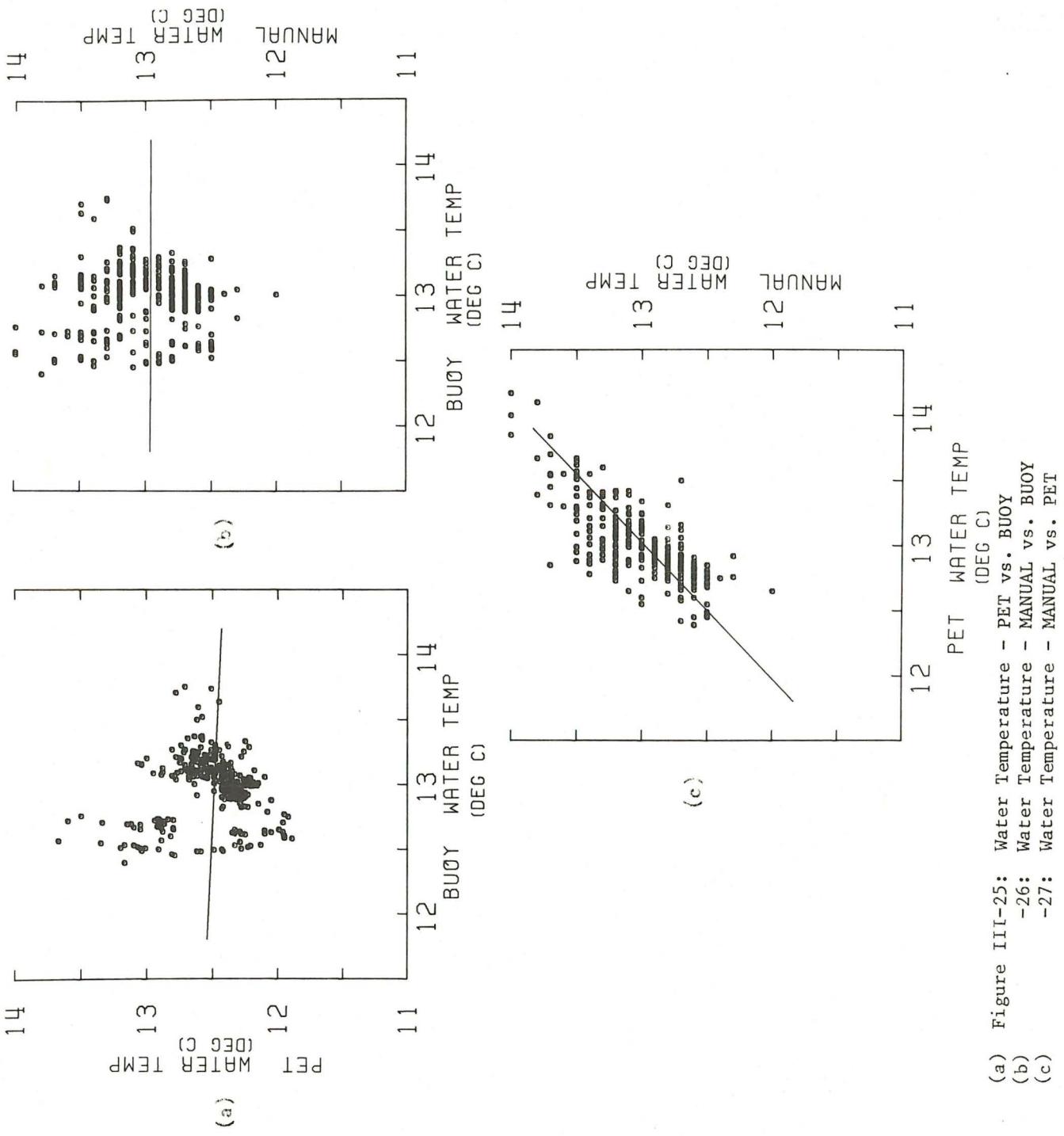
- (a) Figure 11-13: Wind Speed - MANUAL vs. PET Average
 (b) -14: Wind Heading - MANUAL vs. PET Average
 -15: Wind Speed - PET Instantaneous vs. PET Average
 (c) -16: Wind Heading - PET Instantaneous vs. PET Average



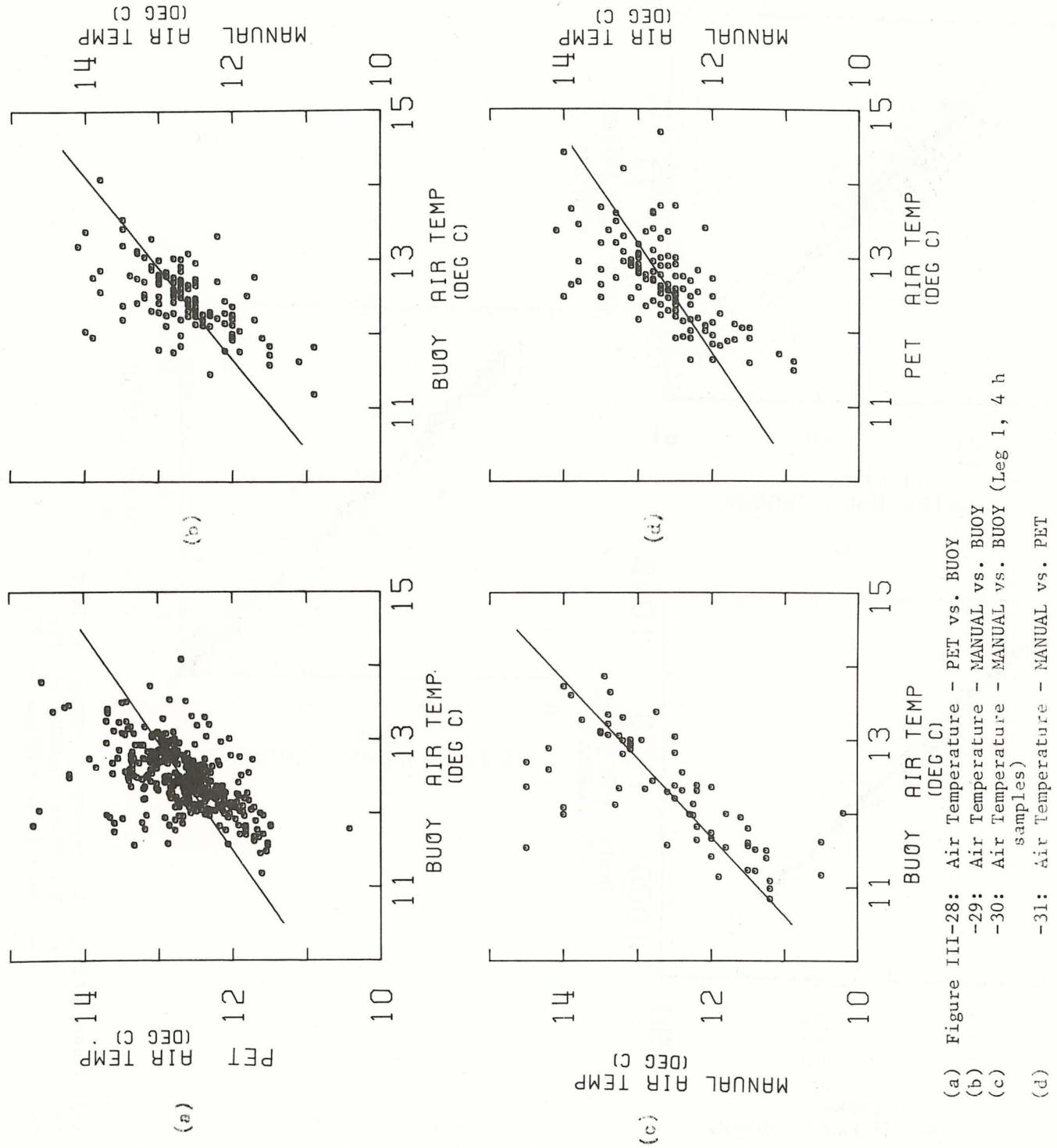
(a) Figure III-17: Wind Speed - MANUAL vs. PET Instantaneous
 (b) -18: Wind Heading - MANUAL vs. PET Instantaneous
 (c) -19: Wind Speed - PET Instantaneous vs. BUOY
 (d) -20: Wind Heading - PET Instantaneous vs. BUOY

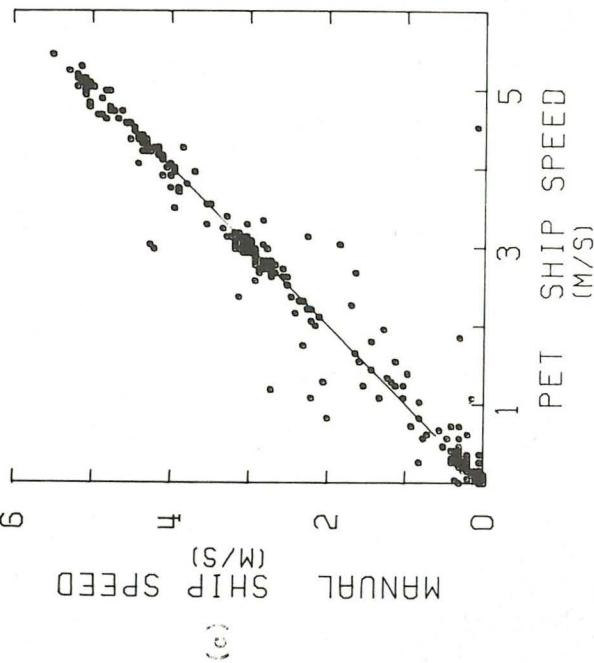
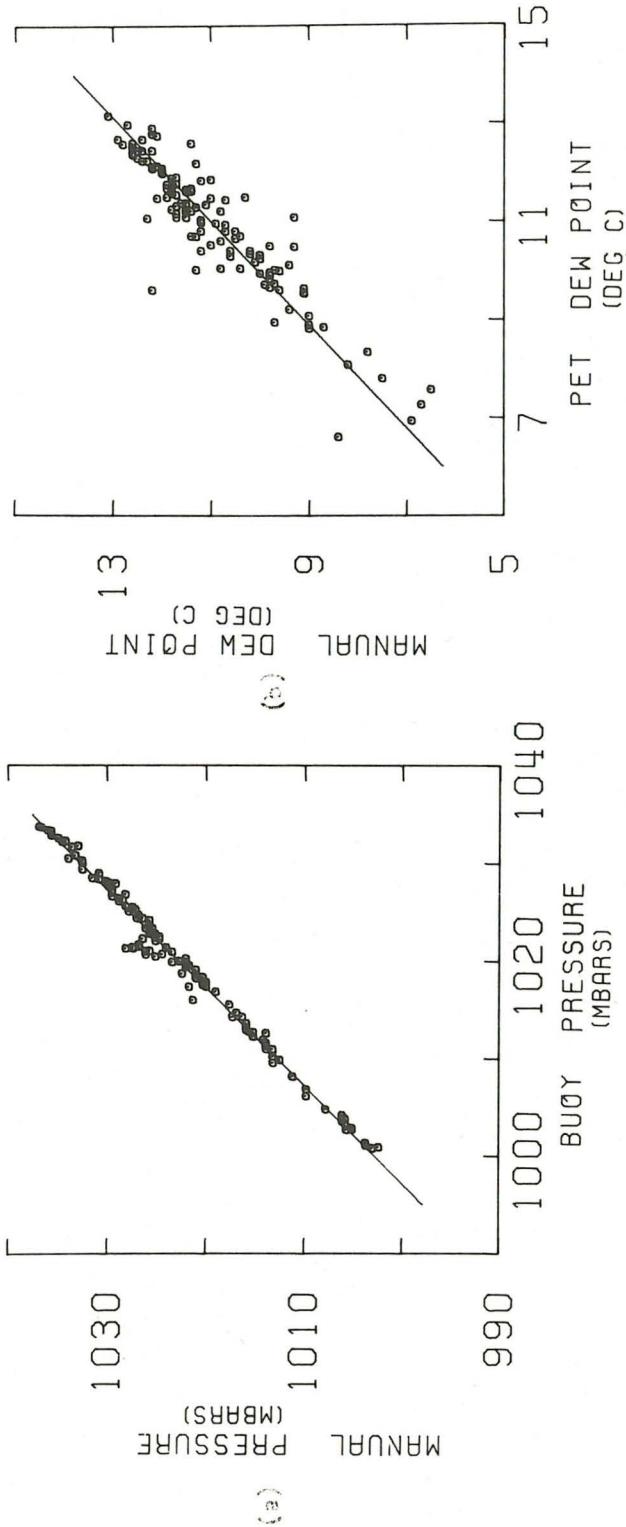


(a) Figure III-21: Wind Speed - MANUAL vs. BUOY
 (b) -22: Wind Heading - MANUAL vs. BUOY
 (c) -23: Wind Speed - PET Average vs. BUOY
 (d) -24: Wind Heading - PET Average vs. BUOY

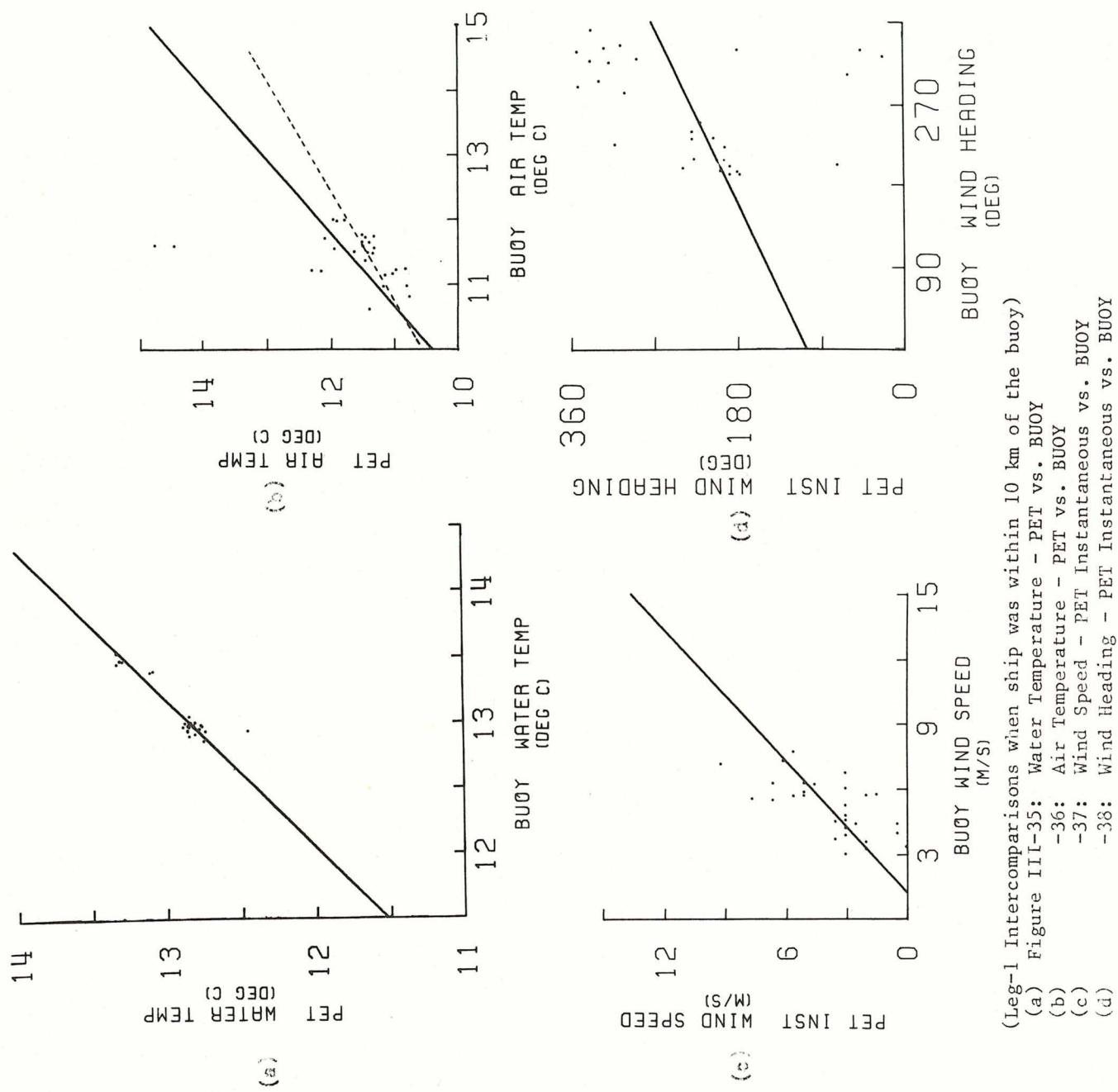


(a) Figure III-25: Water Temperature - PET vs. BUOY
 (b) -26: Water Temperature - MANUAL vs. BUOY
 (c) -27: Water Temperature - MANUAL vs. PET





(a) Figure III-32: Air Pressure - MANUAL vs. BUOY
 (b) -33: Dew Point - MANUAL vs. PET
 (c) -34: Ship Speed - MANUAL vs. PET



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provided 18 days of intercomparison data and 38 days of meteorological data from 30 July to 6 September 1978. The other buoy (JASIN H2) carried a VMNR and gave 25 total days of data from 16 July to 10 August, and from 26 August to 1 September.

A PET computer, hardwired to sensors positioned on the ship, displayed data that were logged during both legs of the cruise. Manual data were gathered by the science watches.

This report describes the PET system, and displays and compares all the data. VAWR hourly meteorological data are listed for the 38 day period.

Scientific interpretation of these data, such as calculations of heat fluxes, will be published separately.

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