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- The time independent nonlinear reaction-diffusion equations have been formulated and solved analytically for the first time
- Applied the new approach of Homotopy perturbation method
- Analytical solutions are compared with zero order analytical solutions.

### A New Mathematical Modelling Using Homotopy Perturbation Method to Solve Nonlinear Equations in Enzymatic Glucose Fuel Cells J. Saranya<sup>1</sup>, L. Rajendran<sup>2\*</sup>, L. Wang<sup>3</sup> and C. Fernandez<sup>4</sup>

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#### Abstract

For the first time a mathematical modelling of the enzymatic glucose membraneless fuel cell with direct electron transfer has been reported. The niche of this mathematical modelling is the description of the new Homotopy perturbation method to solve the nonlinear differential equations that describes glucose concentration and hydrogen ions respectively. The analytical results of an enzymatic fuel cell should be used, while developing fuel cell, to estimate its various kinetic parameters to attain the highest power value. Our analytical results are compared with limiting case results and satisfactory agreement is noted. The influence of parameters on the concentrations are discussed.

**Keywords:** Mathematical modelling; Nonlinear differential equation; Enzyme; Biofuel cell; New Homotopy perturbation method.

#### 1. Introduction

Glucose cells are energy devices that convert chemical energy from glucose fuel to electricity [1-2]. Theoretically, glucose can be completely oxidized to carbon dioxide and water, releasing 24 electrons per glucose molecule [3]. An enzymatic glucose biofuel cell uses glucose as fuel and

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enzymes as biocatalyst, to transform biochemical energy into electrical energy [4]. Enzymatic fuel cells convert the chemical energy of biofuels into electrical energy. Unlike traditional fuel cell types, which are mainly based on metal catalysts, the enzymatic fuel cells employ enzymes as catalysts [5].

Enzymatic fuel cells (EFCs) have been proposed that can catalyse oxidation of fuels at anodes and/or reduction of oxidants at cathodes to provide electrical power. Electron transfer as opposed to hydrogen transfer was demonstrated in the oxidation-reduction of the flavour protein enzyme system [6]. Recent research into enzymatic fuel cells has focused on the use of glucose as a fuel [7].

Modeling biofuel cells play an important role in understanding and developing new energy devices. The enzymatic fuel cells mathematical models are based on a system of non-linear equations, including reaction and transport kinetics [8, 9], statistical analysis [10] and metabolic control analysis [11]. Theoretical, numerical and experimental methods for estimating the biofuel cell performance was discussed by various authors [12 - 15]. Ivan Ivanov presented the major research activities concerned with the enzymatic biofuel cells by highlighting the current problems [5]. Osman et al. [15] developed a two-dimensional steady-state and dynamic models for an enzymatic fuel cell. Baronas et al. [16], discussed a mathematical model of a chemically modified amperometric biosensor. Nonlinear reaction-diffusion equations in this model are solved using the finite difference technique. Saravanakumar et al. [17] analyzed the currentpotential response of the enzyme-catalyzed as well as the redox polymer mediated kinetic scheme pertaining to biofuel cells. Saravanakumar et al. [18] discussed theoretical treatment of a reaction and diffusion processes in a biofuel cell electrode, for the steady and non-steady state condition. Rasi et al. [19] solved the one-dimensional nonlinear reaction-diffusion equation in an enzyme-catalyzed oxygen reduction reaction in biofuel cells. Malini Devi et al. [20] analyzed the theoretical behavior of biofuel cell/biosensor.

Rubin developed an analytical model for enzymatic glucose membraneless fuel cell with direct electron transfer [1]. Though there are several models and expressions available in the literature that corresponds to various phenomena and processes at biofuel cells, to the best of our knowledge, there are not rigorous analytical expressions for the steady state current for enzymatic glucose biofuel cells. In this paper we have derived the analytical expression for the

concentration of glucose and hydrogen ions in the enzyme layer and outside the enzyme layer, corresponding current density and electrical power in the enzymatic fuel cells.

#### 2. Mathematical formulation of the problem

The change of hydrogen ions concentration and glucose is associated with the diffusion and the enzymatic reaction. The kinetics and mass transport in the enzyme layer (0 < x < L) can be represented by the following non-linear differential equations for steady state condition.

$$D_{H^{+}} \frac{d^2 c_{H^{+}}}{dx^2} + \frac{2k_{cat}[E_T][G]}{K_M + [G]} = 0$$
(1)

$$D_G \frac{d^2[G]}{dx^2} - \frac{2k_{cat}[E_T][G]}{K_M + [G]} = 0$$
(2)

where  $D_G$ ,  $D_{H^+}$  are the diffusion coefficients of glucose and hydrogen ions respectively,  $c_{H^+}$  is the concentration of hydrogen ions and [G] is the concentration of glucose.

Outside of the enzyme layer (L < x < d), the hydrogen ions diffusion can be expressed by the following equation: [1].

$$D_{bH^+} \frac{d^2 c_{H^+}}{dx^2} = 0$$
(3)

#### **Boundary conditions**

Let x = 0 represents the anode surface, while x = L is the boundary between the anode and the buffer solution. The concentration of hydrogen ions and glucose at the anode surface (x = 0) are represented by the following equations: [1].

$$c_{H^+}\Big|_{x=0} = c_0$$
 (4)

$$[G]|_{x=0} = [G_0] \tag{5}$$

where  $c_0$  is the hydrogen ions concentration between the glucose reservoir and an anode and  $[G_0]$  is the glucose concentration in the glucose reservoir. Since the amount of charge is proportional to the amount of material passed through the interface, another boundary condition is represented by the following equation:

$$\left. \frac{\mathrm{d}[G]}{\mathrm{d}x} \right|_{x=0} = \frac{-g_{1s}}{zD_G} \tag{6}$$

where  $g_{1s} = \frac{k_{cat}[E_s][G]}{K_M + [G]}$  is the surface reaction rate and z is the number of elementary ionic

charges. In the bulk solution the hydrogen ions concentration remain constant [1].

$$c_{H^+}\Big|_{x=d} = c_d \tag{7}$$

On the boundary between two regions having different diffusivities, the matching conditions are defined by the Eq. (8) and Eq. (9) [1].

$$D_{H^{+}} \frac{dc_{H^{+}}}{dx} \text{(flux of the hydrogen ions inside the enzyme layer)} \bigg|_{x=L}$$
$$= D_{bH^{+}} \frac{dc_{H^{+}}}{dx} \text{(flux of the hydrogen ions outside the enzyme layer)} \bigg|_{x=L} (8)$$

 $c_{H^+}$  (concentration of hydrogen ions inside the enzyme layer)  $\Big|_{x=L}$ 

 $= c_{H^+}$  (concentration of hydrogen ions outside the enzyme layer) $\Big|_{x=L}$  (9)

These conditions mean that the equal species fluxes through the same surface and conditions of a continuity for concentrations. Eq. (8) and Eq. (9) describe the boundary conditions between the anode and the bulk where x = L for hydrogen ions. Boundary conditions employed in the enzymatic glucose fuel cell for the glucose and hydrogen ions are also represented in Figure 1. Current density *j* occurring at the electrode surface due to reduction or oxidation of  $c_{H^+}$  is given by Eq. (10):

$$j = zFD_{H^+} \left(\frac{\mathrm{d}c_{H^+}}{\mathrm{d}x}\right)_{x=0}$$
(10)

#### **3.** Dimensionless form

We make the nonlinear PDE (Eqs. (1) - (3)) dimensionless by defining the following parameters which are depicted in Eq. (11):

$$\bar{c}_{H^{+}} = \frac{c_{H^{+}}}{c_{0}}, \quad [\bar{G}] = \frac{[G]}{[G_{0}]}, \quad \bar{X} = \frac{x}{d}, \alpha = \frac{2d^{2}k_{cal}[E_{T}]}{D_{G}K_{M}}, \quad \beta = \frac{[G_{0}]}{K_{M}}, \quad \xi_{1} = \frac{D_{G}}{D_{H^{+}}}, \xi_{2} = \frac{D_{H^{+}}}{D_{bH^{+}}} \quad \text{and}$$

$$c_{i} = \frac{[G_{0}]}{c_{0}} \qquad (11)$$

where  $\bar{c}_{H^+}$ ,  $[\bar{G}], \bar{X}, \alpha, \beta, \xi_1, \xi_2$  and  $c_i$  represent dimensionless concentration of hydrogen ions for glucose, distance, reaction diffusion parameter, saturation parameter, ratio between diffusion coefficients and ratio between initial concentration of glucose and hydrogen ions respectively. Now in  $(0 < \bar{X} < L/d)$ , Eq. (1) and Eq. (2) reduces to the following dimensionless forms which are represented by Eqs. (12) and (13):

$$\frac{\mathrm{d}^{2}\bar{c}_{H^{+}}}{\mathrm{d}\bar{X}^{2}} + \frac{\alpha\,\xi_{1}\,c_{i}[\overline{G}\,]}{1+\beta[\overline{G}\,]} = 0 \tag{12}$$

$$\frac{\mathrm{d}^{2}[\overline{G}]}{\mathrm{d}\overline{X}^{2}} - \frac{\alpha[\overline{G}]}{1 + \beta[\overline{G}]} = 0 \tag{13}$$

In the bulk  $(L/d < \overline{X} < 1)$ , the hydrogen ions (Eq. (3)) reduced to

$$\frac{\mathrm{d}^2 \bar{c}_{H^+}}{\mathrm{d} \bar{X}^2} = 0 \tag{14}$$

The boundary conditions Eqs. (4) - (7) are reduced to [1].

$$\overline{c}_{H^+} = 1 \text{ at } \overline{X} = 0 \text{ when } (0 < \overline{X} < L/d)$$
 (15)

$$\overline{c}_{H^+} = \frac{c_d}{c_0} \text{ at } \overline{X} = 1 \text{ when } (L/d < \overline{X} < 1)$$
(16)

$$[\overline{G}] = 1 \text{ at } \overline{X} = 0 \ (0 < \overline{X} < L/d) \tag{17}$$

$$\frac{\mathrm{d}[G]}{\mathrm{d}\overline{X}}\Big|_{\overline{X}=0} = \frac{-dg_{1s}}{zG_0D_G} = \frac{-\alpha L}{2dz(1+\beta)} \text{ when } (0 < \overline{X} < L/d)$$

$$\tag{18}$$

The matching boundary conditions (8) and (9) are defined in dimensionless form as follows.

$$\xi_2 \frac{d\bar{c}_{H^+}}{d\bar{X}} \Big|_{\bar{X}=L/d} \text{ (flux inside the enzyme layer)} = \frac{d\bar{c}_{H^+}}{d\bar{X}} \Big|_{\bar{X}=L/d} \text{ (flux outside the enzyme layer)} (19)$$

$$\bar{c}_{H^+}\Big|_{\bar{X}=L/d}$$
 (concentrat ion inside the enzyme layer) =  $\bar{c}_{H^+}\Big|_{\bar{X}=L/d}$  (concentrat ion outside the enzyme layer) (20)

The dimensionless current density I becomes

$$I = \frac{jd}{zFD_{H^+}c_0} = \left(\frac{d\bar{c}_{H^+}}{d\bar{X}}\right)_{\bar{X}=0}$$
(21)

## 4. Analytical expression of substrate and products concentration using new Homotopy perturbation method

By solving the Eqs. (12) and (13) using boundary conditions Eqs. (15) - (20), we can obtain the glucose concentration and hydrogen ions (Appendix A) inside the enzyme layer  $(0 < \overline{X} < L/d)$  as follows:

$$[\overline{G}](\overline{X}) = \cosh\left(\sqrt{\frac{\alpha}{1+\beta}}\overline{X}\right) - \left(\frac{L}{2dz}\sqrt{\frac{\alpha}{1+\beta}}\right)\left(\sinh\left(\sqrt{\frac{\alpha}{1+\beta}}\overline{X}\right)\right)$$
(22)

$$\overline{c}_{H^{+}}(\overline{X}) = 1 + \frac{1}{\mu_{2}} \left[ \mu_{0} + \mu_{1} \left( 1 - \frac{L}{d} \right) \right] \overline{X} + \xi_{1} c_{i} \left[ 1 - \cosh\left(\sqrt{\frac{\alpha}{1+\beta}}\overline{X}\right) + \sqrt{\frac{\alpha}{1+\beta}} \left(\frac{L}{2dz}\right) \sinh\left(\sqrt{\frac{\alpha}{1+\beta}}\overline{X}\right) \right]$$
(23)

By solving the Eq. (14) using boundary conditions (Eqs. (15)- (20)), we can obtain the concentration of hydrogen ions in outside the enzyme layer  $(L/d < \overline{X} < 1)$  as follows:

$$\bar{c}_{H^{+}}(\bar{X}) = \frac{c_{d}}{c_{0}} + \frac{1}{\mu_{2}} \left( \xi_{2} \mu_{0} - \frac{\mu_{1} L}{d} \right) (\bar{X} - 1)$$
(24)

The dimensionless current density becomes

$$I = \frac{jd}{zFD_{H^+}c_0} = \left(\frac{d\bar{c}_{H^+}}{d\bar{X}}\right)_{\bar{X}=0} = \frac{1}{\mu_2} \left[\mu_0 + \mu_1 \left(1 - \frac{L}{d}\right)\right] - \xi_1 c_i \sqrt{\frac{\alpha}{1+\beta}} \left(\frac{L}{2dz}\right)$$
(25)

where 
$$\mu_0 = \frac{c_d}{c_0} - \xi_1 c_i \left[ 1 - \cosh\left(\sqrt{\frac{\alpha}{1+\beta}} \frac{L}{d}\right) + \sqrt{\frac{\alpha}{1+\beta}} \left(\frac{L}{2dz}\right) \sinh\left(\sqrt{\frac{\alpha}{1+\beta}} \frac{L}{d}\right) \right] - 1$$
 (26)

$$\mu_{1} = \xi_{2} \left[ \xi_{1} c_{i} \sqrt{\frac{\alpha}{1+\beta}} \sinh\left(\sqrt{\frac{\alpha}{1+\beta}} \frac{L}{d}\right) - \left(\frac{\alpha}{1+\beta} \frac{\xi_{1} c_{i}}{1+\beta}\right) \left(\frac{L}{2dz}\right) \cosh\left(\sqrt{\frac{\alpha}{1+\beta}} \frac{L}{d}\right) \right]$$
(27)

and 
$$\mu_2 = \xi_2 \left( 1 - \frac{L}{d} \right) + \frac{L}{d}$$
 (28)

Electrical power is given by the Eq. (29)

$$p = \frac{\overline{P}d^2}{RT[G_0]D_GL} = \frac{\alpha z[\overline{G}]\left(\ln\frac{c_L}{c_d}\right)}{2\left(1 + \beta[\overline{G}]\right)}$$
(29)

The kinetic response of an enzymatic fuel cell depends on concentrations of  $[\overline{G}]$  and  $\overline{c}_{H^+}$ . The concentrations of the species depend upon concentration of the substrate  $[\overline{G}]$ . However, the substrate  $[\overline{G}]$  also depends on two factors which are  $\alpha$  and  $\beta$ .  $K_M$  is the Michaelis-Menten constant, an intrinsic character of an enzyme.

#### 5. Limiting case results

#### 5.1. Saturated (zero order) catalytic kinetics

We initially consider the situation where the concentration of glucose is very much greater than Michaelis-Menten constant  $K_M$ . In this case  $\beta > 1$  and Eqs. (12) and (13) reduced to:

$$\frac{\mathrm{d}^2 \bar{c}_{H^+}}{\mathrm{d}\bar{X}^2} + \frac{\alpha \,\xi_1 c_i}{\beta} = 0 \tag{30}$$

$$\frac{\mathrm{d}^2[\overline{G}]}{\mathrm{d}\overline{X}^2} - \frac{\alpha}{\beta} = 0 \tag{31}$$

Solving the Eqs. (30) and (31) using boundary conditions (Eqs. (15) - (20)), we can obtain the concentration of glucose and hydrogen ions inside the enzyme layer ( $0 < \overline{X} < L/d$ ) as follows;

$$[\overline{G}](\overline{X}) = 1 - \left(\frac{\alpha}{\beta}\right) \left(\frac{L}{2dz}\right) \overline{X} + \frac{\alpha}{2\beta} \overline{X}^2$$
(32)

$$\bar{c}_{H^+}(\bar{X}) = 1 + \left[\frac{\alpha \,\xi_1 c_i}{\beta} \left(\frac{L}{d}\right) - \frac{1}{\mu_2} \left(1 + \frac{\alpha \,\xi_1 c_i}{2\beta} \left(\frac{L}{d}\right)^2 - \frac{c_d}{c_0}\right)\right] \bar{X} - \frac{\alpha \,\xi_1 c_i}{2\beta} \,\bar{X}^2 \tag{33}$$

Solving the Eq. (13) using boundary conditions (Eqs. (15) - (20)), we can obtain the concentration of hydrogen ions outside the enzyme layer  $(L/d < \overline{X} < 1)$  as follows;

$$\bar{c}_{H^+}(\bar{X}) = \frac{1}{\mu_2} \left( \xi_2 \left( \frac{\alpha \, \xi_1 c_i}{2\beta} \left( \frac{L}{d} \right)^2 + 1 - \frac{c_d}{c_0} \right) \right) \left( 1 - \bar{X} \right) + \frac{c_d}{c_0}$$
(34)

The current density becomes

$$I = \frac{jd}{zFD_{H^+}c_0} = \left(\frac{d\overline{c}_{H^+}}{d\overline{X}}\right)_{\overline{X}=0} = \frac{\alpha\,\xi_1c_i}{\beta} \left(\frac{L}{d}\right) - \frac{1}{\mu_2} \left(\frac{\alpha\,\xi_1c_i}{2\beta} \left(\frac{L}{d}\right)^2 + 1 - \frac{c_d}{c_0}\right)$$
(35)

where  $\mu_2$  is defined by Eq. (28). In this case electrical power becomes:

Electrical power 
$$p = \frac{\overline{P}d^2}{RT[G_0]D_GL} = \frac{\alpha z \left(\ln \frac{c_L}{c_d}\right)}{2\beta}$$
 (36)

#### 5.2. Unsaturated (first order) catalytic kinetics

Now we consider the second major limiting situation found in practice, when the glucose concentration is less than Michaelis-Menten constant  $K_M$ . This situation will pertain when  $\beta \le 1$ . Hence Eqs. (12) and (13) are reduced to:

$$\frac{\mathrm{d}^2 \bar{c}_{H^+}}{\mathrm{d} \bar{X}^2} + \alpha \,\xi_1 c_i [\bar{G}] = 0 \tag{37}$$

$$\frac{\mathrm{d}^2[\overline{G}]}{\mathrm{d}\overline{X}^2} - \alpha[\overline{G}] = 0 \tag{38}$$

Hence, the nonlinear Eqs. (12) and (13) have been reduced to one equation which is linear. By solving the Eq. (37) and Eq. (38) using boundary conditions (Eqs. (15) - (20)), we can obtain the concentration of glucose and hydrogen ions inside the enzyme layer ( $0 < \overline{X} < L/d$ ) as follows;

$$[\overline{G}](\overline{X}) = \cosh\left(\sqrt{\alpha}\,\overline{X}\right) - \left(\frac{\sqrt{\alpha}\,L}{2dz}\right) \left(\sinh\left(\sqrt{\alpha}\,\overline{X}\right)\right) \tag{39}$$

$$\overline{c}_{H^+}(\overline{X}) = 1 + \frac{1}{\mu_2} \left[ \mu_3 + \mu_4 \left( 1 - \frac{L}{d} \right) \right] \overline{X} + \xi_1 c_i \left[ 1 - \cosh\left(\sqrt{\alpha} \,\overline{X}\right) + \left(\frac{\sqrt{\alpha} L}{2dz}\right) \sinh\left(\sqrt{\alpha} \,\overline{X}\right) \right]$$
(40)

Solving the Eq. (14) using boundary conditions (Eqs. (15) - (20)) we can obtain the concentration of hydrogen ions outside the enzyme layer  $(L/d < \overline{X} < 1)$  as follows;

$$\overline{c}_{H^+}(\overline{X}) = \frac{1}{\mu_2} \left( \xi_2 \mu_3 - \left(\frac{L}{d}\right) \mu_4 \right) \left(\overline{X} - 1\right) + \frac{c_d}{c_0}$$

$$\tag{41}$$

In this case current density becomes represented by the following Eq. (42):

$$I = \frac{jd}{zFD_{H^+}c_0} = \left(\frac{d\overline{c}_{H^+}}{d\overline{X}}\right)_{\overline{X}=0} = \frac{1}{\mu_2} \left[\mu_3 + \mu_4 \left(1 - \frac{L}{d}\right)\right] + \xi_1 c_i \left(\frac{\sqrt{\alpha}L}{2dz}\right)$$
(42)

where  $\mu_2$  is defined in Eq. (28) and  $\mu_3$  and  $\mu_4$  are described by Eqs. (43) and (44) as follows:

$$\mu_{3} = \frac{c_{d}}{c_{0}} - \xi_{1}c_{i} \left[ 1 - \cosh\left(\sqrt{\alpha} \frac{L}{d}\right) + \sqrt{\alpha}\left(\frac{L}{2dz}\right) \sinh\left(\sqrt{\alpha} \frac{L}{d}\right) \right] - 1$$
(43)

$$\mu_4 = \xi_2 \left[ \xi_1 c_i \sqrt{\alpha} \sinh\left(\sqrt{\alpha} \frac{L}{d}\right) - \left(\alpha \xi_1 c_i\right) \left(\frac{L}{2dz}\right) \cosh\left(\sqrt{\alpha} \frac{L}{d}\right) \right]$$
(44)

Therefore, by re-organising those equations, the electrical power becomes as:

$$p = \frac{\overline{P}d^2}{RT[G_0]D_GL} = \frac{\alpha z[\overline{G}]\left(\ln\frac{c_L}{c_d}\right)}{2}$$
(45)

#### 6. Results and discussion

Here Eqs. (22) – (24) are the analytical expressions of concentration of glucose, hydrogen ions inside of the enzyme layer  $(0 < \overline{X} < L/d)$  and hydrogen ions outside of the enzyme layer  $(L/d < \overline{X} < 1)$ . For an enzymatic fuel cell to be analytically useful, its response must be quantitatively related to the substrate concentration. Based on this principle,  $\beta > 1$  is not the proper case for an enzymatic fuel cell, because in the zero order reaction, hydrogen ions concentration is independent of the glucose concentration. Eq. (22) represents the most general approximate new analytical expression for the glucose concentration profiles for all values of parameter  $\alpha$  (or distance between electrodes) and  $\beta$  (or initial concentration of glucose).

Dimensionless concentration of hydrogen ions  $(\overline{c}_{H^+})$  inside the enzyme layer  $(0 < \overline{X} < L/d)$ and outside the enzyme layer  $(L/d < \overline{X} < 1)$  versus dimensionless distance from the anode  $\overline{X}$ using Eq. (23) and Eq. (24) is plotted in Fig. 2. From this figure it is inferred that the concentration of Hydrogen ion increases absurdly from the anode surface and reaches the maximum near the boundary of the enzyme layer  $(\overline{X} = L/d)$  and then decreases slowly to  $c_d / c_0$ in the bulk solution. Because the hydrogen ions are generating on the anode, moving towards the cathode and consumed on the cathode. Also this is due to the effect of  $c_d / c_0$  as an individual term in the equations (23) and (24).

Dimensionless concentration of hydrogen ions  $\bar{c}_{H^+}$  in the inside the enzyme layer as a function of distance from the anode  $\bar{X}$  are plotted in Figs. 3(a)-3(e) for various values of  $\alpha, \beta, c_i, \xi_1$  and  $\xi_2$  and some fixed values of other parameters using Eq. (23) and Eq. (40). From Figs. 3(a)-3(e), it is inferred that the concentration of hydrogen ions in the interface between

inside the enzyme layer and outside the enzyme layer  $(\overline{X} = L/d)$  is high because generation of hydrogen ions.

Figs. 4(a)-4(b) represent dimensionless concentration profiles of the concentration of hydrogen ions  $\overline{c}_{H^+}$  ( $L/d < \overline{X} < 1$ ) versus distance from the anode surface  $\overline{X}$  for various values of parameters using Eq. (24) and Eq. (41). From this figures, it is observed that the concentration of the hydrogen ions decreases in outside the enzyme layer due to consumption of the hydrogen ions in this layer.

Eq. (25) represents the simple closed form of analytical expression of current density. Figs. 5(a)-5(d) represent the dimensionless current density *I* versus dimensionless parameter  $\alpha$  for various values of other parameters. From this figures it is observed that the current density is directly proportional to enzyme concentration or square of the distance between electrodes. Also current density is linear with respect to dimensionless thickness of enzyme layer and ratio between diffusion coefficient of glucose and hydrogen ions ( $\xi_1$ ) (Fig. 6(a)-6(c)).

Figs. 7(a)-7(c) to 9(a)-9(c) represent dimensionless power versus dimensionless glucose concentration [ $\overline{G}$ ], dimensionless parameter  $\alpha$  and  $\beta$  for various values of parameters using Eq. (29). From this figures it is observed that the power density increases when concentration of glucose, enzyme, initial concentration of glucose and  $c_L/c_d$ . Also from this figures it is also observe that power density p attains the maximum value and then remains constant because of external resistance and consequence of a current reduction. Increasing the enzyme concentration or distance between electrodes has an important effect on the fuel cell (Fig. 7(a)). Power does not differ significantly give to due to increase of glucose concentration.

#### 7. Conclusions

The time independent nonlinear reaction-diffusion equations have been formulated and solved analytically for the first time. The analytical expressions for glucose, hydrogen ions inside and outside the enzyme layer, current density and power are derived for all parameters using a new approach of Homotopy perturbation method. In addition, these analytical solutions are compared with zero order analytical solutions. This analytical result is useful to investigate the effects of various parameters of the fuel cell on power. A good agreement with limiting case results for the experimental values of the all parameters is also noted.

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#### 9. Appendixes

## Appendix A: Approximate analytical solution of nonlinear Eq. (13) using a new approach to the Homotopy perturbation method (NHPM)

In this appendix, we have indicated how to determine the solution of Eq. (13). To solve Eq. (13), we first construct the Homotopy for the equation as follows:

$$\left(1-p\right)\left[\frac{d^{2}[\overline{G}]}{d\overline{X}^{2}}-\frac{\alpha[\overline{G}]}{1+\beta([\overline{G}](\overline{X}=0))}\right]+p\left[\frac{d^{2}[\overline{G}]}{d\overline{X}^{2}}-\frac{\alpha[\overline{G}]}{1+\beta[\overline{G}]}\right]=0$$
(A1)

$$\left(1-p\right)\left[\frac{d^{2}[\overline{G}]}{d\overline{X}^{2}}-\frac{\alpha[\overline{G}]}{1+\beta}\right]+p\left[\frac{d^{2}[\overline{G}]}{d\overline{X}^{2}}-\frac{\alpha[\overline{G}]}{1+\beta[\overline{G}]}\right]=0$$
(A2)

The approximate solution of (A2) is given by

$$[\overline{G}] = [\overline{G}_0] + p[\overline{G}_1] + p^2[\overline{G}_2] + \dots$$
(A3)

Substituting Eq. (A3) comparing the coefficient of  $p^0$  we obtain the following differential equation:

$$p^{0}:\frac{d^{2}[\overline{G}_{0}]}{d\overline{X}^{2}} - \frac{\alpha[\overline{G}_{0}]}{1+\beta} = 0$$
(A4)

Solving Eq. (A4) by using boundary conditions Eq. (17) and Eq. (18), we obtain the following equation:

$$[G_0] = \cosh\left(\sqrt{\frac{\alpha}{1+\beta}}\overline{X}\right) - \left(\frac{L}{2dz}\sqrt{\frac{\alpha}{1+\beta}}\right) \left(\sinh\left(\sqrt{\frac{\alpha}{1+\beta}}\overline{X}\right)\right)$$
(A5)

Similarly, we can obtain the Eq. (23) and Eq. (24).

#### Appendix B. Nomenclature and units

Symbols	Definitions	Units and Experimental
		values
[G]	Glucose concentration	0.1M, 0.01M, 0.001M
$c_{H^+}$	Hydrogen ions concentration	М
x	Distance	m
k <sub>cat</sub>	Kinetic enzyme reaction rate	10^3 Sec <sup>-1</sup>
K <sub>M</sub>	Kinetic enzyme reaction rate	0.019M
$[E_T]$	Volume enzyme concentration	0.7x10 <sup>-5</sup> M, 0.5x10 <sup>-5</sup> M,
		0.3x10 <sup>-5</sup> M, 0.1x10 <sup>-5</sup> M
L	Thickness of an enzyme layer	0.001-0.0005m
d	Distance between electrodes	0.003-0.004m
$D_G$	Diffusion coefficients of glucose	$10^{-5} \text{m}^2 \text{ s}^{-1}$
$D_{H^+}$	Diffusion coefficients of	$10^{-5} \text{ m}^2 \text{ s}^{-1}$
	hydrogen ions	
$D_{bH^+}$	Diffusion coefficients of	$10^{-5} \text{ m}^2 \text{ s}^{-1}$
	hydrogen ions in bulk	
<i>C</i> <sub>0</sub>	Hydrogen ions concentration	0.002M
-	between the glucose reservoir	
	and an anode	
$[G_0]$	Glucose concentration in the	0.001, 0.01, 0.1, 0.19, 1.9 mol
	glucose reservoir	m <sup>-3</sup>
<u>C</u>	Ratio between initial	5x10 <sup>3</sup> , 50
C <sub>d</sub>	concentration of hydrogen ions	
	at $x = L$ and $x = d$ .	
<u><i>c</i></u> <i>d</i>	Ratio between initial	1
<i>c</i> <sub>0</sub>	concentration of hydrogen ions	
	at $x = d$ and $x = 0$ .	

$P = I^2 R_L$	Power	Watt(W)
$\overline{P}$	Power density	W/cm <sup>2</sup>
		(or)
		Watt = $J/s=kg*m^2/s^3$
R <sub>L</sub>	Resistance	$0.01 \Omega - 1 \Omega$
		$(\Omega = V / A = kg * m^2 A^2 s^3)$
$\alpha = \frac{2d^2 k_{cat}[E_T]}{D_G K_M}$	Reaction diffusion parameter	16,50,84,117
$\beta = \frac{[G_0]}{K_M}$	Saturation parameter	0.05, 0.5, 5.2, 10, 100
$[G_0]$	Ratio between initial	0.5, 5, 50, 95, 950
$c_i = \frac{c_0}{c_0}$	concentration of glucose and	
	hydrogen ions	
$\xi_1 = \frac{D_G}{D_{H^+}}$	Ratio between diffusion coefficients	1
$\xi_2 = \frac{D_{H^+}}{D_{bH^+}}$	Ratio between diffusion coefficients	0.5,0.8,1
$[\overline{G}]$	Dimensionless concentration of Glucose	
$\overline{c}_{H^+}$	Dimensionless concentration of Hydrogen ions	
$\overline{X}$	Dimensionless distance	
L/d	Dimensionless thickness of an enzyme layer	



**Figure1.** Boundary conditions employed in the enzymatic glucose fuel cell for the substrate[G] and product  $c_{H^+}$ .



**Figure 2.** Combined plot of dimensionless concentration of hydrogen ions  $(\bar{c}_{H^+})$  inside the enzyme layer  $(0 < \bar{X} < L/d)$  and dimensionless concentration of hydrogen ions  $(\bar{c}_{H^+})$  outside the enzyme layer  $(L/d < \bar{X} < 1)$  versus dimensionless distance  $\bar{X}$  using Eq. (23) and Eq. (24). Where L/d is the interface between inside the enzyme layer and outside the enzyme layer.



**Figure 3(a)-3(e).** Comparison of dimensionless concentration profiles of the product  $\overline{c}_{H^+}$  versus dimensionless distance  $\overline{X}$  for various values of  $\alpha, \beta, c_i, L/d, \xi_i$  and  $\xi_2$  and some fixed values of other parameters using Eq. (23) and Eq. (40). The key to the graph: (\_) represents the Eq. (23) and (...) represent the Eq. (40).



**Figure 4(a)-4(e).**Comparison of dimensionless concentration profiles of the product  $\overline{c}_{H^+}$  versus dimensionless distance  $\overline{X}$  for various values of  $\alpha, \beta, c_i, L/d, \xi_1$  and  $\xi_2$  and some fixed values of other parameters using Eq. (24) and Eq. (41). The key to the graph: ( \_ ) represents the Eq. (24) and (...) represent the Eq. (41).



**Figure 5.**Plot of dimensionless current density *I* versus dimensionless parameter  $\alpha$  for various values of  $\beta_{,c_i,L/d,\xi_1}$  and  $\xi_2$  and some fixed values of other parameters using Eq. (28).



**Figure 6(a)-6(c).** Plot of dimensionless current density *I* versus  $L/d, \xi_1$  and  $\xi_2$  for various values of  $\alpha$  and some fixed values of other parameters using Eq. (28).



Figure 7(a)-7(c). Plot of dimensionless power versus p dimensionless concentration  $[\overline{G}]$  for various values of  $\alpha$ ,  $\beta$  and  $c_L/c_d$  and some fixed values of other parameters using Eq. (29).



Figure 8(a)-8(c). Plot of dimensionless power p versus dimensionless parameter  $\alpha$  for various values of  $\beta$ ,  $[\overline{G}]$  and  $c_L/c_d$  and some fixed values of other parameters using Eq. (29).



Figure 9(a)-9(c). Plot of dimensionless power p versus dimensionless parameter  $\beta$  for various values of  $\alpha$ ,  $[\overline{G}]$  and  $c_L/c_d$  and some fixed values of other parameters using Eq. (29).