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The Implants used for Intramedullary Fixation of Distal Fibula Fractures: A Review of Literature.

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Key words: Intramedullary, nail, fibula, lateral malleolus, fracture

1 **The Implants used for Intra-medullary Fixation of the Distal Fibula.**

2 **Abstract**

3 *Background*

4 Ankle fractures are amongst the most common surgically treated musculoskeletal injuries.

5 Intramedullary (IM) fixation of the lateral malleolus had been attempted as early as the
6 1990s. In recent years, dedicated implants have emerged. This review evaluates the design
7 characteristics of the technology used to perform IM fixation of distal fibular fractures.

8 *Materials and methods*

9 A search of electronic databases was performed. Medical subject headings (MeSH) and
10 free-text terms were used to optimise search sensitivity and specificity.

11 *Results*

12 We identified 10 different surgical technologies for IM fixation of lateral malleolar fractures
13 reported across 12 articles, including both improvised and custom-designed Orthopaedic
14 implants. Most implants were inserted through percutaneous surgical techniques.

15 *Conclusion*

16 Advances in technology have improved the feasibility of intramedullary fixation as a
17 treatment option for lateral malleolus fractures. The implants we reviewed had very diverse
18 morphological and mechanical properties. Intra-medullary fixation may outperform extra-
19 medullary fixation of the lateral malleolus, particularly in patients at high risk of soft tissue
20 complications. Robust scientific evidence is awaited.

21 Level of evidence Level IV evidence.

22 Key words: Intramedullary, nail, fibula, lateral malleolus, fracture

23 Introduction

24 The use of intramedullary (IM) devices has expanded in recent years to include the distal
25 fibula, in tandem with the move towards minimally invasive surgical approaches in other
26 areas of orthopaedic surgery. Ankle fractures are amongst the most common
27 musculoskeletal injuries treated with an operation.[1-3] Conventional surgical treatment is
28 open reduction followed by internal fixation using plates and screws as described by the AO
29 group[4]. However soft tissue fragility, swelling or compromise can pose significant
30 challenges for surgeons. Minimally invasive plate osteosynthesis (MIPO) has been
31 developed to address such cases although these techniques involve deep tissue
32 dissection.[5]

33 Intramedullary devices for ankle fractures are a continually evolving technology. Implants
34 range from screws and rod-like spikes to modern, bespoke IM fibular nails. Intramedullary
35 fixation may potentially reduce wound complications, symptomatic metalwork and
36 improved recovery times. The biomechanical advantages of IM over traditional plate
37 fixation have been extensively described. Nails are load-sharing implants, whereas plates
38 are load bearing implants. There is usually less stress shielding, reduced risk of peri-implant
39 fractures, and the injured limb can be loaded earlier. IM devices can be inserted through
40 minimal dissection. The weak evidence base and variety of implants does however create
41 dubiety over the effectiveness of this technology in clinical practice and may subsequently
42 hinder uptake.

43 The primary aims of this review are to evaluate the surgical devices that have been used to
44 treat distal fibular fractures with IM fixation. We provide discussion on the design and
45 biomechanical strengths and weaknesses.

46 **Methods**

47 A search of the following electronic databases was performed: Cochrane Central Register of
48 Controlled Clinical Trials (CENTRAL); MEDLINE (OvidSP); Embase (OvidSP) and WHO
49 international trial register. Medical subject headings (MeSH) and free-text terms were used
50 to optimise search sensitivity and specificity: unstable, ankle/fibula fracture, nail, pin, rod
51 and intramedullary fixation. Bibliographies of papers were hand searched for any additional
52 studies not obtained through electronic search. Images and user manuals were reviewed
53 where possible. Inclusion/Exclusion Criteria are listed in Table 1.

54 *Primary data extraction*

55 Technical descriptions of fracture fixation and descriptions of the technology used.

56 *Secondary data extraction*

57 Outcomes were extracted if standardised data was presented on union rates, complication
58 rates, functional scores and radiological scores were recorded.

59 **Results**

60 Our literature search identified 10 different surgical technologies for IM fixation of lateral
61 malleolar fractures reported across 12 articles. The number of patients described in the
62 articles ranged from 9 to 194. Only 3 techniques were evaluated by Randomised Controlled

63 Trial,[6-8] and 7 techniques in 9 case series alone.[9-18] Some techniques were reported
64 in multiple publications.

65 *Secondary outcome measures*

66 Functional Scoring was undertaken in 6 studies using the method devised by Olerud and
67 Molander[19] in 1984. Standardised radiological scoring of reduction was reported in 7
68 studies. A good reduction was defined as no fibular shortening, a posterior displacement of
69 less than 2mm and a 1mm increase in medial clear space. A fair reduction represented
70 fibular shortening of 2mm, posterior displacement of 2-4mm and a 1-3mm increase in
71 medial clear space. A poor reduction was defined as a fibular shortening in excess of 2mm,
72 posterior displacement of over 4mm and greater than 3 mm increase in medial clear space.

73 Study characteristics and secondary outcome data is presented in Table 2.

74 **Surgical Techniques & Implants**

75 Preparation and approach to the fibula

76 Patients were operated on in the supine position or lateral decubitus position depending on
77 surgeon preference. No tourniquet was used in the majority of cases. Generally, all authors
78 describe a *percutaneous* approach to the fibula.

79 Fluoroscopy was used in every case. Where present, medial malleolar fractures were
80 treated based on the fracture characteristics and surgeon preference. In most cases using
81 partially threaded lag screws or tension band wiring constructs were used. Less frequently a
82 small plate and screws.

83 Rush Rods (Berivon, Meridian, MS, USA)

84 Pritchett[7] described treatment of unstable ankle fractures using percutaneously inserted
85 3.2mm Rush Rods. Rush rods are steel rods with a chisel-like tip that can be inserted into
86 the intramedullary space without reaming. After pre-contouring, the Rush rods were
87 inserted through a drill hole made at the tip of the fibula. Patients were allowed to weight-
88 bear as tolerated with aids; the use of cast immobilisation was unclear from the authors'
89 technical description.

90 Knowles Pins (Zimmer, Warsaw, IL)

91 The Knowles pin was used to stabilise fibular fractures in a 45 patient cases series.[14,20]
92 Knowles pins are collared pins that are partially threaded from tip to midshaft, made from
93 stainless steel. The authors describe an extensile approach in their article, making an
94 incision from the tip of the fibula extended 1 cm proximal to the fracture to facilitate direct
95 fracture reduction using a bone holding forceps. The entry drill hole was made 2mm medial
96 to the tip of the fibula.

97 ANK Nail (manufacturer unspecified)

98 The ANK Nail was a steel rod with a curved anterior limb and distal loop for additional
99 fixation to the tibia conferring "stability" to the syndesmosis[10] (Figure 1). The device was
100 not fixed proximally. The authors approached the fibula using a linear incision placed along
101 the lateral malleolus, curved anteriorly (reverse 'J' incision) to expose the anterior tibio-
102 fibular junction. This incision facilitated fixation of the implant to the tibia distally. Fracture

103 reduction was achieved under direct vision and maintained with a bone-holding forceps.

104 The nail was inserted over a standard K-wire.

105 Inyo Nail (Richards Medial Company, Memphis, Tennessee, USA)

106 The Inyo Nail was trialled by McLennan et al.[9,21] This device relied on its wedge design for
107 improved bone contact within the metaphyseal bone. It was a 90mm v-shape, tapered nail
108 made from malleable stainless steel (ATSM F138), with holes present in the broadened
109 distal end to facilitate removal should this be required (Figure 2). To allow implantation the
110 distal ridge of the lateral malleolus was osteotomised via a linear 2-3cm incision. The
111 Intramedullary canal was then prepared with a 2.3mm dental burr prior to nail insertion
112 over a Steinmann Pin (Zimmer, Warsaw, Indiana).

113 Epiphysa fibular nail (manufacturer unspecified)

114 The Epiphysa fibular nail is described by Francois et al [15] for in a 39 patient case series.

115 The device is a smooth straight rod with a round profile and threaded head that was
116 available in three different lengths. The head engages the metaphysis but the device is not
117 fixed proximally. The exact surgical technique is unclear from the article.

118 Epifisa®Nail (FH Orthopaedics Inc, New York, USA)

119 Asloum et al[8] trialled a contemporary nail which combines a curved shaft with a self-
120 tapping threaded head (Figure 3). It is available in four lengths, ranging from 70 to 130mm.
121 The authors described a percutaneous approach but there is lack of clarity concerning the
122 techniques used to reduce the fracture, maintain alignment, and prepare the intramedullary
123 canal. All patients were immobilised in a cast post-operatively, but were permitted

124 progressive weight-bearing once the wound had healed.

125 Acumed Fibular Rod ((Hillsboro, Oregon, USA)

126 This nail is made of solid titanium and comes in two diameters (3mm and 3.6mm) and three
127 lengths (110mm, 145mm and 180mm). It was designed specifically for percutaneous fixation
128 of the lateral malleolus [6] (Figure 4). Insertion involves a number of stages. The tip of the
129 fibula is used as an entry point. A cannulated drill is passed over a 1.6mm guide wire to
130 prepare the distal metaphysis. The diaphysis can be further hand-reamed prior to nail
131 insertion. The device allows distal antero-posterior locking screws, and lateral to medial
132 trans-implant tibial / 'syndesmosis' screw. In initial reports it was recommended a proximal
133 blocking screw be inserted to prevent shortening but this practice has since been
134 discontinued[22]

135 XS Nail (Intraplant, Endocare, Germany)

136 The XS nail is a cylindrical implant with uniform diameters of 4.5mm or 3.5mm.[13] Lengths
137 range from 197mm to 272mm and it has between 4 to 11 locking holes that are 9mm apart.
138 Proximally, screws can be inserted across the fibula and into the tibia to provide additional
139 stability. This implant is cannulated and is inserted over a central guidewire pre-positioned
140 within the intramedullary canal. A radiolucent aiming device is used to facilitate cross-
141 locking screw insertion. Compression of the fracture can be achieved through one of two
142 oblong compression holes, either side of the implants centre-point.

143 SST® (Stainless Steel Taper) Nail (Biomet, Warsaw, IN, USA)

144 The SST Nail is a slender, tapered, cannulated rod made of stainless steel, with screw holes

145 that permit distal locking. It is described in two case series.[16,17] Both groups used the
146 interlocking feature of the implant and allowed progressive weight-bearing over a period of
147 4 to 6 weeks after the wound had healed.

148 Acutrak Plus Compression Screw (Acumed Inc., Beaverton, OR, USA)

149 The Acutrak plus compression screw is a fully-threaded, cannulated, tapered, headless
150 screw with a variable pitch measuring 5mm at its tip, and expanding to 6.5mm at its tail. The
151 screw is inserted over a guide pin. Fixation using this implant is described by Lee et al.[18] In
152 their study, the authors exposed both the tip of the fibula and the fracture site to permit
153 accurate fracture reduction with bone holding forceps while the screw was being inserted.

154 Percutaneous Screw Fixation

155 Fixation using stainless steel screws has been described in two papers, Ray et al[12] and
156 Smith et al.[11]

157 Smith et al used closed reduction of the fracture and direct digital pressure over the fracture
158 to maintain reduction. Through a 1cm inline incision made approximately 1.5cm distal to the
159 tip of the fibula, a 2.5mm drill was used to open the distal 1.5 cm of the fibula permitting
160 the insertion of a fully threaded 100mm long, 4mm cancellous screw. The authors aimed to
161 implant the screw such that the thread would engage the inner aspect of the diaphyseal
162 canal proximally. The tensile properties of the screw reduce the tendency for talar shift.
163 Ray et al[12] also used a 4.2mm fully threaded, self-tapping screw (Woodruff, Zimmer,
164 Warsaw, IN) measuring between 2.5 and 4 inches long, though the thread pitch is unclear.

165 Patients were not allowed to weight bear for 6 weeks post-operatively in either of the
166 studies.

167 **Discussion**

168 The increasing incidence of low-energy, unstable ankle fractures in elderly patients with
169 poor soft tissue and bone quality challenges contemporary trauma surgeons.[3,23] Demand
170 for safe and reliable fixation techniques has encouraged surgeon scientists and innovators
171 to advance minimally invasive techniques. Intramedullary fixation is a conceptually
172 straightforward technique relying on well-established principles, already applied in current
173 practice. It does not require substantial training or education.

174

175 The procedure can be unforgiving due to the limited 'inline' single axis the implant must
176 follow proximally into the diaphysis. Off-axis positioning of rigid implants and reamers in
177 'soft' bone can result in fracture malalignment, or iatrogenic fracture. Care should be taken
178 to achieve a good entry point, which ideally should be screened intra-operatively with both

179 antero-posterior and lateral views using image intensifier. Obese patients or particularly
180 swollen ankles add further complexity to the procedure. At the beginning of the learning
181 curve, patient selection is essential to avoid conversions, lengthy operating times and
182 further compromise to the soft tissue envelope. The reduced number of steps in IM nailing
183 should reduce operating time. However, achieving and maintaining closed reduction in
184 highly comminuted or displaced fractures can be technically challenging and consume more
185 time than expected initially.

186 The majority of authors describe closed reduction and a percutaneous approach to the
187 fibula for introduction of their specific implant. Generally, the rate of wound complications
188 reported was higher for the plate group in studies using a comparator.[7,8,14] This may
189 reflect the longer skin incisions for traditional ORIF, compared to the 1-2 cm incisions
190 required for nails. Modern implants do not require extensive dissection. Preventing
191 exposure of the fracture to the external environment and thus preserving fracture 'biology',
192 non-union and deep infection rates should be lower. Extensive dissection and direct
193 visualisation of the fracture negates the benefits of smaller incisions for nails, especially in
194 cases of swelling.

195 An additional benefit of intra-medullary implants is reduced potential for symptomatic
196 metalwork. Brown et al have reported that as much as 31% (n=126 patients) experienced
197 pain in the skin overlying hardware.[24] Where AP cross-locking screws options are available
198 the screws must not be too long, to prevent peroneal tendon injury.

199

200 The mechanical advantages of intramedullary devices are conferred by way of lying on the
201 central longitudinal bony axis and therefore implants are not subject to the same cantilever
202 forces as plates lying on one side of bone. Smith et al[25] studied the mechanics of the
203 fibular nail in fresh frozen cadaveric legs with oblique Weber[26,27] A fractures *but no*
204 *medial lesion*. The limbs were then mounted on a Zwick tensile biomechanical testing
205 apparatus and stressed to failure using an external rotation force. The study demonstrated a
206 higher load to failure for the limbs stabilised with a fibular nail compared to a standard AO
207 lag-screw and plate construct which sits “off-axis”.

208 There is much heterogeneity between implant designs. Intramedullary fixation of
209 metaphyseal bone is dissimilar to diaphyseal fixation due to reduced implant-bone contact
210 at the metaphysis. Compared to slender implants such as screws, Rush rods or Knowles pin,
211 tapered and or morphologically contoured devices should give improved reduction and
212 stability through greater load sharing and working length. However, an implant which is not
213 fixed to bone at two or more points creates an inherently unstable biomechanical construct
214 which will fail to resist shortening and rotation. Although tapered implants are certainly one
215 solution, metalwork migration may still be a problem. Ten percent of patients treated with
216 the Inyo nail required removal of the implant due to hardware prominence or proximal
217 migration. There was also a high rate of malunion with the wedge fit implant, presumably as
218 fracture were fixed with malalignment, or displacing during implantation or loading.
219 Exceptions may apply to devices with variable, cross-locking features. Cross locking
220 proximally through tapered, modern implants is often not possible due to the narrowness of
221 the fibula’s diaphysis. The XS nail does offer proximal locking but at the expense of width. A
222 uniform diameter may result in these implants being too large for the fibular diaphysis.

223 Bugler et al initially used a proximal “blocking” screw as the solution to shortening with the
224 Acumed Fibular Rod, although this practice was later discontinued due to the risk of
225 fracture. A relatively robust construct with Acumed nail can be achieved by routinely filling
226 the syndesmosis screw hole.

227

228 We are aware of one device, the Fibulock nail (Sonoma Orthopaedic Products Inc), which is
229 unpublished in medical literature that utilises expanding fins proximally to offer better
230 stability. Despite the design properties, such implants are again often wider than their
231 counterparts due to the internal mechanisms. Caution should be taken in using ‘wide’, non-
232 tapered implants as they pose high risk of iatrogenic fracture. Similarly, surgeons should
233 avoid over-dilating the intramedullary canal during the reaming process.

234 Screw fixation is a reasonable and inexpensive improvisation for intramedullary fixation.
235 Screws and nails have different mechanical properties. Bone purchase through the threads
236 of an adequately sized screw should prevent shortening. Such a feature also theoretically
237 allows a bridging type fixation of slightly comminuted bone. A well positioned screw should
238 also function as internal buttress, maintaining talar reduction by exerting medially directed
239 forces against the internal medial cortex through ‘elastic recoil’. Although all screws can be
240 applied in compression mode, the variable pitch on an Acturak is probably more effective in
241 doing so. Despite the absence of a cross-locking option with screws, Banskton et al[28] have
242 demonstrated rotational stability equal to plate and lag screw fixation in cadavers with
243 experimentally produced Weber B fractures (n=16). Specimens were placed under torsional
244 load to failure. This rotational stability presumably arises from the fracture ends

245 interlocking and opposing each other and would not apply to situations where there is a
246 high degree of comminution.

247 It is unclear from the literature whether the proposed advantages of intramedullary nails
248 are outweighed by implant costs. The reduced complications and early return to activity on
249 a weight-bearing construct may make the technique more cost-effective. Methods using
250 'improvised' intramedullary implants such as fixation with percutaneous screws are
251 inexpensive and viable alternatives to commercial products.

252 The poor level of evidence and range of implants can plunge one into a mire of uncertainty,
253 in selecting an intramedullary technique. It is important to focus on the physiological insult
254 the approach will deliver, and mechanical stability the implant offers. Based on past trends
255 it is likely future technology will remain morphologically contoured. This region of the
256 human body does not accommodate a 'one size fits all' implant. Although a range of sizes in
257 commercial products are available, a potential development may be patient-specific intra-
258 medullary nails. Such devices could be made intra-operatively using materials such as resin
259 or cement if a kit were available.

260 Limitations

261 Much of the current literature exists in the form of commentary and small case series.
262 Although reasonable attempts at systematic review and meta-analysis have been
263 made,[29,30] lack of standardised outcome measures and adequately powered randomised
264 controlled trials limits meaningful conclusions. Many of the early implants are no longer
265 commercially available. Then trend in both literature and technology would suggest that for

266 high-risk patients, intramedullary distal fibula fixation is becoming an accepted, 'emergency'
267 procedure within the surgical community. However, the individual studies do have potential
268 for selection bias because the primary aim of the authors is to present their technique or
269 implant, with subsequent favourable patient selection for cases in the experimental arm.
270 Authors used broadly similar inclusion criteria, elderly patients with unstable ankle fractures
271 avoiding cases in which there was a serious soft tissue insult. Our paper has focused on
272 techniques rather than reported outcomes.

273 Conclusion

274 Nails may outperform plate and screws for fixation of the lateral malleolus in elderly
275 patients at high risk of soft tissue complications. Robust scientific evidence is awaited. This
276 study evaluates and summarises the design aspects of implants used for intramedullary
277 fixation of the fibula. Future research must address cost effectiveness, scientifically assess
278 mechanical differences between implant designs and demonstrate superior health and
279 quality of life outcomes. The implants at the moment remain user dependant. Surgeons
280 should use an implant with characteristics that meet their individual case requirements.

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Inclusion Criteria	Exclusion Criteria
<ul style="list-style-type: none"> • All study designs • All studies in humans of any age • Original Studies, Biomechanical studies, case reports, review articles • All patients had been diagnosed preoperatively by imaging techniques including x-rays and CT. • Studies conducted on patients with unstable fracture of the distal fibula (lateral malleolus). 	<ul style="list-style-type: none"> • Experimental studies • Insufficient data to allow analysis • Studies with Duplicate Techniques by a single group of authors • Intramedullary devices described for use in the tibia • Intramedullary devices described for proximal fibula/diaphysis • Commentary • Letters

Table 1 – Inclusion/ Exclusion Criteria

Implant/ authors	Study type	Participants	Secondary outcomes	Current commercial availability
rush rod • Pritchett et al	RCT	n=25	Infection (n=0); non-union(n=25) “poor” radiological result (n=5)	Available
Knowles Pin • Lee et al	Case series	n=45	“Good” fracture reduction (95%); average operating time (22min); complications (n=0); symptomatic hardware (n=0)	Available
Inyo nail • McLennan et al	Case Series	n=75	non-union (0); infection (0); malunion (7%); removal metalwork (10%); Good radiological result (80%); good functional outcome (85%) (return to previous activity level with no pain or stiffness);	Not available
Fibular nail • Bugler et al	RCT	n=100	Infection (0); wound problems (0)	Available
Ank nail • Kara et al	Case series	n=139	Fibular shortening (11)	Not available. Customised implant
Accutrak Screw • Lee et al	Case Series	n=23	“Good” reduction (95.7%); mean operating time (25.3min); superficial wound infection (1); At long-term follow-up, 91.3% (21) patients reported good or excellent results	Not available
Cortical screw • Smith et al • Ray et al	Case series Case series	n=24	Infection (0); symptomatic hardware (1) – metalwork removed; “Good” reduction (21); “good/ excellent” function (16)	Available
Epiphysa nail • Francois et al	Case series	n=39		Not available
Epifisa Nail • Asloum et al	RCT	n=28	All patients rated their function as “excellent” despite there being a 7% post-operative complication rate.	Available
XS nail • Gehr et al	Case series	n=194	Superficial haematoma (2); superficial infection (1); metalwork migration (2); “good” or “excellent” outcomes (91.5%)	Available
SST Nail • Ramansay et al • Rajeev et al	Case Series Case Series	n=9 n=24	“Excellent/ good” outcome (88%); “poor” radiologic result (2) Complication (0); Olerud and Molander score at 1 year (58.125 +/- 6.00, fair outcome)	Available

Table 2: Study characteristics and secondary outcome data.

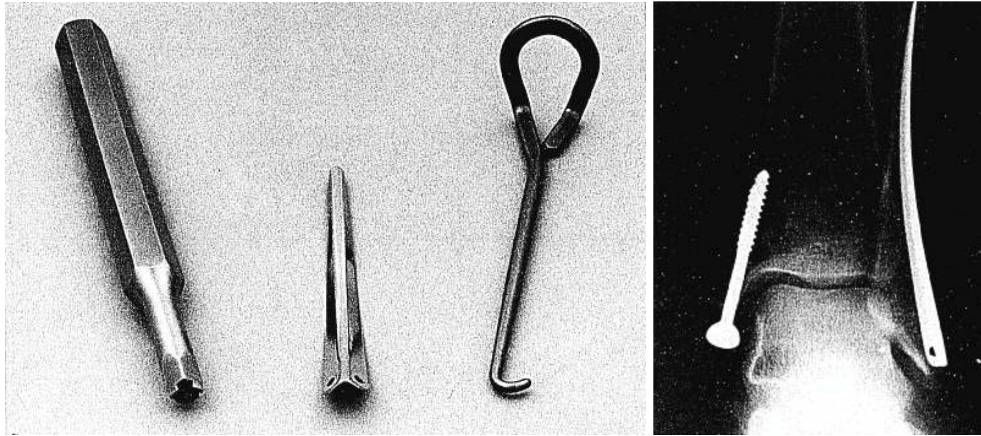


Figure 1 – Inyo Nail. Introducer, Nail and extractor (left to right).

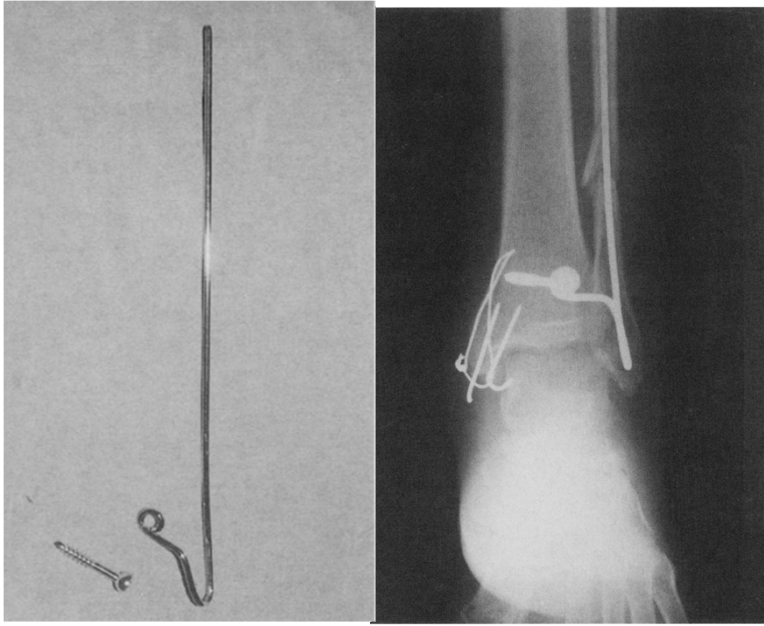


Figure 2 – ANK nail



Figure 3 – Epifisa Nail

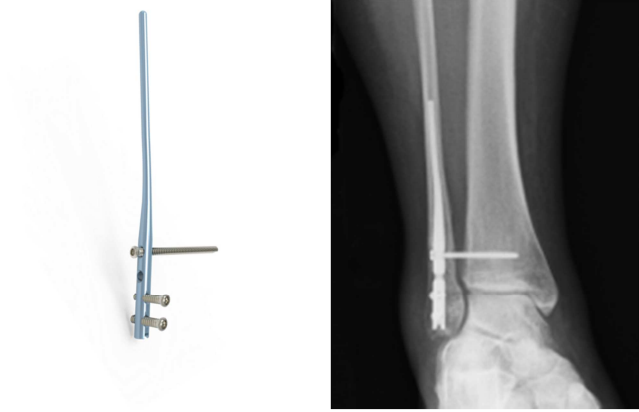


Figure 4 – Accumed Fibular rod

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- 1 • The design failure of some of the older devices has resulted in them being phased out
- 2 • Most devices can be inserted percutaneously
- 3 • Modern device control for rotation with cross locking screws or taper fit
- 4 • There is a need for adequately powered, scientific trials and biomechanical studies.

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