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YiuCheung Shiu Purdue University

Shaheen Ahmad Purdue University

Richard P. Paul Purdue University

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# Mathematics for Visual Guidance of Robots

YiuCheung Shiu Shaheen Ahmad Richard P. Paul

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School of Electrical Engineering Purdue University West Lafayette, Indiana 47907

### Mathematics for Visual Guidance of Robots

YiuCheung Shiu Shaheen Ahmad Richard P. Paul

School of Electrical Engineering Purdue University West Lafayette, IN 47907

#### ABSTRACT

Vision can be used to position a robot relative to a known object or a known environment in 3D. If the object has enough feature points, one view is sufficient for determining the relative position between the object and the camera, otherwise, multiple views are required. We discuss the mathematics of viewpoint determination, using a combination of calibration matrix decomposition and space resection. The combined method has low noise sensitivity and does not require knowledge of camera parameters. If the object does not have enough features, multiple views are required to determine its position and orientation; an example of this is be given. The formulation of homogeneous transform equations to drive the manipulator to the goal position is also be given.

#### 1. Introduction

It is possible to find the position of an object using one view by identifying and finding the 2D locations of unobstructed visual features (such as points and lines). This set of image coordinates will be fed to a viewpoint determination algorithm to find the 3D position and orientation of the object. We will address only the viewpoint determination problem; the 2D locations of visual features are assumed to be provided by a computer vision system. In this report, we will only address point features.

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Viewpoints can be determined by the combination of calibration matrix decomposition [Gana83] and space resection [Wolf83]; the results of calibration matrix decomposition are used as an initial estimate for the iterative space resection method. The first method alone is noise sensitive (a technical report will be published to compare noise sensitivity of various viewpoint determination methods). The second method requires an initial estimate of the viewpoint because it uses the Newton-Raphson algorithm [Dode78] to solve for a non-linear system of equations Another disadvantage of the second method is that the solutions may not be unique [Fisc81]. These problems will be solved when the two methods are used together.

In some cases, there may not be enough feature points for one-view methods to work; we will show an example that does not require as many features but requires multiple views. Finally, we will show how the relative position between an object and the camera can be incorporated into a transform equation necessary for the manipulation of the object.

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#### 2. Finding Object Position with a Single Image

We want to find the 3-D position and orientation of an object using model-based vision. It is possible to find the 3-D position using only one view because of the knowledge of object dimensions. We will limit ourselves to methods that use image coordinates of local features such as corners and small holes instead of methods that uses extended features such as lines and curves. Let  $(u_i, v_i)^t$  be image coordinates of feature number i and  $(x_i, y_i, z_i)^t$  be the coordinates of the feature with respect to the object frame *OBJ*,  $\Omega$  be the set of 2D positions of image features and  $\Gamma$  be the set of corresponding 3D positions of the object features relative to the object. If there are n corresponding points,

$$\Omega = \left\{ (u_1, v_1), (u_2, v_2), \cdots (u_n, v_n) \right\}$$
(2.1)

$$\Gamma = \left\{ (\mathbf{x}_1, \, \mathbf{y}_1, \, \mathbf{z}_1) \,, \, (\mathbf{x}_2, \, \mathbf{y}_2, \, \mathbf{z}_2) \,, \, \cdots \, (\mathbf{x}_n, \, \mathbf{y}_n, \, \mathbf{z}_n) \right\}$$
(2.2)

We require a function F which takes the arguments  $\Omega$ ,  $\Gamma$ , n, and produce the homogeneous transform  $^{CAM}T_{OBJ}$  which specifies the position of the OBJ frame with respect to the CAM frame.

$$\mathbf{F}(\Omega,\Gamma,\mathbf{n})$$
. (2.3)

We will discuss calibration matrix decomposition [Gana84] and space resection [Wolf83]. Calibration matrix decomposition is a non-iterative method that solves for both the transform  $^{CAM}T_{OBJ}$  and the camera parameters uniquely. This method requires at least 6 feature points to be seen on the image. Space resection is an iterative method used in photogrammetry to locate a camera-equipped airplane with respect to some known ground control points. It requires a minimum of three feature points, camera parameters and an initial estimate. The space resection solution may not be unique if less than 6 feature points are used [Fisc81].

We have found from simulation that calibration matrix decomposition is much more noise sensitive than space resection. The noise sensitivity and the nonuniqueness problems can be solved by using space resection to find the final result, while the calibration matrix decomposition is used to find the initial estimate and the camera parameters.

#### 2.1. Camera Matrix Decomposition

In this section, we will find that the calibration matrix C can be solved when given a set of image coordinates and the corresponding set of 3-D feature coordinates with respect to the object frame OBJ. Then we can decompose C to find the position of the OBJ with respect to CAM and also the camera parameters.

Figure 2.1 shows the geometry of a camera viewing an object.  $^{CAM}T_{OBJ}$  is the homogeneous transform that relates the frames OBJ and CAM. The camera calibration matrix C transforms 3-D coordinates with respect to the object frame into 2-D image coordinates. In homogeneous transform notation, this is written as

$$\begin{bmatrix} u' \\ v' \\ w' \end{bmatrix} = \begin{bmatrix} C_{11} & C_{12} & C_{13} & C_{14} \\ C_{21} & C_{22} & C_{23} & C_{24} \\ C_{31} & C_{32} & C_{33} & C_{34} \end{bmatrix} \begin{bmatrix} x \\ y \\ z \\ 1 \end{bmatrix}$$
(2.4)

where.  $(x,y,z)^t$  is the feature position measured with respect to OBJ, and  $(u',v',w')^t$  is the feature position in homogeneous transform notation. Because of the nature of homogeneous transformation, Equation (2.4) still holds if C is scaled. In order to have a unique C, we will fix  $C_{34}$  to 1. The actual image position  $(u,v)^t$  in pixel units can be calculated by

$$\mathbf{u} = \frac{\mathbf{u}'}{\mathbf{w}'}; \quad \mathbf{v} = \frac{\mathbf{v}'}{\mathbf{w}'}.$$
 (2.5)

Given  $\Omega$  (set of image coordinates) and  $\Gamma$  (set of 3-D coordinates with respect to OBJ), we want to find the elements of the calibration matrix C. From the position ( $u_i, v_i$ ) of each image feature, we have from (2.5)

$$u'_i - u_i w'_i = 0;$$
  $v'_i - v_i w'_i = 0.$  (2.6)

But  $u'_i$ ,  $v'_i$ , and  $w'_i$  can be expressed in terms of elements of C as:

$$u'_{i} = C_{11} x_{i} + C_{12} y_{i} + C_{13}$$
(2.7a)

$$\mathbf{v}'_{i} = \mathbf{C}_{21} \, \mathbf{x}_{i} + \mathbf{C}_{22} \, \mathbf{y}_{i} + \mathbf{C}_{23} \tag{2.7b}$$

$$w'_i = C_{31} x_i + C_{32} y_i + C_{33}$$
 (2.7c)

Substitution (2.7) into (2.6) and using 6 points, we will arrive at the following matrix

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and can solve for the elements of C.

	11 AV.	$Q_{AA} = 0$							pp Solid	1	1 · · · ·	1
<b>x</b> <sub>1</sub>	y <sub>1</sub>	<b>z</b> 1	1	0	0	0	0	$-\mathbf{u}_1\mathbf{x}_1-\mathbf{u}_1\mathbf{y}_1-\mathbf{u}_1\mathbf{z}_1$	C <sub>11</sub>		u <sub>1</sub>	
x <sub>2</sub>	y <sub>2</sub>	<b>Z</b> 2	1	0	0	0	0	$-\mathbf{u}_2\mathbf{x}_2-\mathbf{u}_2\mathbf{y}_2-\mathbf{u}_2\mathbf{z}_2$	C <sub>12</sub>		u2	
<b>x</b> 3	y <sub>3</sub>	<b>z</b> 3	1	0	0	0	0	-u <sub>3</sub> x <sub>3</sub> -u <sub>3</sub> y <sub>3</sub> -u <sub>3</sub> z <sub>3</sub>	C <sub>13</sub>		u <sub>3</sub>	
x4	У4	Z4	1	0	0	0	0	$-\mathbf{u_4x_4} - \mathbf{u_4y_4} - \mathbf{u_4z_4}$	C <sub>14</sub>		u4	
<b>x</b> 5	У <sub>5</sub>	z <sub>5</sub>	1	0	0	0	. 0	-u <sub>5</sub> x <sub>5</sub> -u <sub>5</sub> y <sub>5</sub> -u <sub>5</sub> z <sub>5</sub>	C <sub>21</sub>		u <sub>5</sub>	
x <sub>8</sub>	Уß	Z <sub>6</sub>	1	0	0	0	0	-u <sub>6</sub> x <sub>6</sub> -u <sub>6</sub> y <sub>6</sub> -u <sub>6</sub> z <sub>6</sub>	C <sub>22</sub>	=	ug	(2.8)
0	0	0	0	<b>x</b> <sub>1</sub>	y <sub>1</sub> °	z <sub>1</sub>	1	$-\mathbf{v}_1\mathbf{x}_1-\mathbf{v}_1\mathbf{y}_1-\mathbf{v}_1\mathbf{z}_1$	C <sub>23</sub>		v <sub>1</sub>	
0	0	0	0	<b>x</b> <sub>2</sub>	У <sub>2</sub>	z <sub>2</sub>	1	$-v_2x_2-v_2y_2-v_2z_2$	C <sub>24</sub>		v <sub>2</sub>	
0	0	0	0	x <sub>3</sub>	y <sub>3</sub>	z <sub>3</sub>	1	v <sub>3</sub> x <sub>3</sub> v <sub>3</sub> y <sub>3</sub> v <sub>3</sub> z <sub>3</sub>	C <sub>31</sub>	Sugar .	v <sub>3</sub>	
0	0	0	0	x4	У₄	z4	1	-v <sub>4</sub> x <sub>4</sub> -v <sub>4</sub> y <sub>4</sub> -v <sub>4</sub> z <sub>4</sub>	C <sub>32</sub>		• • • •	
0	0	.0	0	$\mathbf{x}_{5}$	У5	z <sub>5</sub>	1	$-v_5x_5-v_5y_5-v_5z_5$	C <sub>33</sub>		$v_5$	

Let us abbreviate the Equation (2.8) to

$$\mathbf{X} \mathbf{C}' = \mathbf{U}. \tag{2.9}$$

C' can be solve as

$$C' = X^{-1} U.$$
 (2.10)

If there are more than 6 points, we will have redundant equations. In this case, we can minimize the mean square error of the image coordinates by

> $\mathbf{C'} = (\mathbf{X}^{\mathrm{T}} \mathbf{X})^{-1} \mathbf{X}^{\mathrm{T}} \mathbf{U}.$ (2.11)

Now we will express C in terms of the elements of the elements of  $CAM T_{OBJ}$  and the camera parameters. To do this, we need to understand the geometry of the system. Shown in Figure 2.1 are the coordinates  $(x_f, y_f, z_f)^t$  of a feature point with respect to OBJ, and the coordinates  $(x'_f, y'_f, z'_f)^t$  of the same feature point with respect to the CAM. The ray that emanates from the focal point to the feature point intersects the image plane at  $(x'_{u}, y'_{u})^{t}$ . The image coordinates read out from the vision system is not  $(x'_n, y'_n)^t$  because they are expressed in pixels instead of millimeters and the origin may not be at the center of the image. Thus we can view  $(u,v)^t$  as the results of scaling and translating  $(\mathbf{x}'_{u}, \mathbf{y}'_{u})^{t}$ . Let  $S_{u}$  and  $S_{v}$  be the scaling factors in the u and v

directions, and  $u_0$  and  $v_0$  be the translations. We have

$$u=S_u x'_u + u_0$$
, (2.12a)

$$v = S_v y'_u + v_0$$
. (2.12b)

Using similar triangles,

$$x'_{u} = F \frac{x'_{f}}{z'_{f}},$$
 (2.13a)

$$\mathbf{y'_u} = \mathbf{F} \ \frac{\mathbf{y'_f}}{\mathbf{z'_f}}.$$
 (2.13b)

where F is the focal length of the camera. Substituting (2.13) into (2.12) and rewritting in homogeneous notations,

$$\begin{bmatrix} u' \\ v' \\ w' \end{bmatrix} = \begin{bmatrix} S_{u}F & 0 & u_{0} & 0 \\ 0 & S_{v}F & v_{0} & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix} \begin{vmatrix} x'_{f} \\ y'_{f} \\ z'_{f} \\ 1 \end{vmatrix}$$
(2.14)

and  $u = \frac{u'}{w'}$ ,  $v = \frac{v'}{w'}$ .

We need to express the 3-D coordinates with respect to OBJ instead of CAM; this can be done with homogeneous transformations:

$$\begin{array}{c} CAM \\ \mathbf{x}_{f}' \\ \mathbf{y}_{f}' \\ \mathbf{z}_{f}' \\ 1 \end{array} \right| \begin{array}{c} CAM \\ CAM \\ = \begin{bmatrix} \mathbf{T} \end{bmatrix}_{OBJ} \\ \begin{bmatrix} \mathbf{y}_{f} \\ \mathbf{z}_{f} \\ 1 \end{bmatrix} \\ \mathbf{x}_{f} \\ \mathbf{x}_{f} \\ \mathbf{x}_{f} \end{bmatrix} , \qquad (2.15)$$

(2.16)

where 
$$CAM \begin{bmatrix} \mathbf{T} \end{bmatrix}_{OBJ} = \begin{bmatrix} n_{\mathbf{x}} & o_{\mathbf{x}} & a_{\mathbf{x}} & p_{\mathbf{x}} \\ n_{\mathbf{y}} & o_{\mathbf{y}} & a_{\mathbf{y}} & p_{\mathbf{y}} \\ n_{\mathbf{z}} & o_{\mathbf{z}} & a_{\mathbf{z}} & p_{\mathbf{z}} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Substituting (2.15) into (2.14) allows C to be expressed in terms of the components of  $^{CAM}\mathbf{T}_{OBJ}$  and the camera parameters (F, S<sub>u</sub>, S<sub>v</sub>, u<sub>0</sub>, v<sub>0</sub>). The C<sub>34</sub> element is p<sub>z</sub> so we need to divide all elements by p<sub>z</sub> to have C<sub>34</sub> = 1.

C <sub>11</sub>	C <sub>12</sub>	C <sub>13</sub>	C <sub>14</sub>
C <sub>21</sub>	C <sub>22</sub>	C <sub>23</sub>	C <sub>24</sub>
C <sub>31</sub>	C <sub>32</sub>	C <sub>33</sub>	C <sub>34</sub>

 $n_x S_u F + n_z u_0$	$\mathbf{o_x S_u F + o_z u_0}$	$a_x S_u F + a_z u_0$	$p_x S_u F + p_z u_0$
p <sub>z</sub>	p <sub>z</sub>	p <sub>z</sub>	Pz
$n_y S_v F + n_z v_0$	$o_y S_v F + o_z v_0$	$a_y S_v F + a_z v_0$	$p_y S_v F + p_z v_0$
pz	p <sub>z</sub>	$\mathbf{p}_{\mathbf{z}}$	$\mathbf{p}_{\mathbf{z}}$
$\underline{\mathbf{n}_{\mathbf{z}}}$	O <sub>Z</sub>	<u>a</u> z	, 1
Pz	Pz	Pz	• • • • • • • • • • • • • • • • • • •

The elements  $C_{11}$ ,  $C_{12}$ ,  $C_{13}$  etc. are known because they can be solved by (2.8). We will equate both sides of (2.16) to solve for the components of  $^{CAM}T_{OBJ}$  and the camera parameters. From (2.16), we can see that the parameters  $S_u$ ,  $S_v$ , and F occurs in either  $S_uF$  or  $S_vF$  and therefore cannot be solved for individually. We will solve for  $k_u$  and  $k_v$  instead, where

$$\mathbf{k}_{\mathbf{u}} = \mathbf{S}_{\mathbf{u}} \mathbf{F} \tag{2.17a}$$

$$\mathbf{k}_{\mathbf{v}} = \mathbf{S}_{\mathbf{v}} \mathbf{F} \tag{2.17b}$$

From the last row of (2.16),

$$C_{31}^{2} + C_{32}^{2} + C_{33}^{2} = \frac{n_{z}^{2}}{p_{z}^{2}} + \frac{o_{z}^{2}}{p_{z}^{2}} + \frac{a_{z}^{2}}{p_{z}^{2}} = \frac{1}{p_{z}^{2}}.$$
 (2.18)

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We will have two solutions for  $p_z$  from (2.18). However, if the z'-axis of the camera is pointing to the direction of sight and *OBJ*'s origin is within the object volume,  $p_z$  will be physically constrained to be positive. Thus,

$$p_{z} = \frac{1}{\sqrt{C_{31}^{2} + C_{32}^{2}}}$$
(2.19)

Once  $p_z$  is found,  $n_z$ ,  $o_z$ , and  $a_z$  can be found by equating the last row of equation (2.16).

$$n_z = p_z C_{31}$$
 (2.20)

$$o_z = p_z C_{32}$$
 (2.21)

$$a_{z} = p_{z} C_{33}$$
 (2.23)

To solve for  $k_v$ , we use the first and second rows of C:

$$C_{11} C_{32} - C_{31} C_{12} = \frac{k_u}{p_z^2} (n_x o_z - o_x n_z)$$
 (2.24a)

$$C_{11} C_{33} - C_{31} C_{13} = \frac{k_u}{p_z^2} (n_x a_z - n_z a_x)$$
 (2.24b)

$$C_{12} C_{33} - C_{32} C_{13} = \frac{k_u}{p_z^2} (o_x a_z - o_z a_x)$$
 (2.24c)

Taking sums of squares of (2.24a)-(2.24c), we obtain

$$(C_{11}C_{32}-C_{31}C_{12})^2 + (C_{11}C_{33}-C_{31}C_{13})^2 + (C_{12}C_{33}-C_{32}C_{13})^2 = \frac{k_u^2}{p_z^4} .$$
(2.25)

The sign of  $k_u$  is implementation dependent. In our system, we have assigned the coordinate frame to the camera such that u points to the same direction as x' and v points to the same direction as y'. In this case, both  $k_u$  and  $k_v$  are positive. Thus,

$$k_{u} = p_{z}^{2} \sqrt{(C_{11}C_{32} - C_{32}C_{12})^{2} + (C_{11}C_{33} - C_{31}C_{13})^{2} + (C_{12}C_{33} - C_{32}C_{13})^{2}}$$
(2.26)

To find  $u_0$ , we sum the squares of the elements of the first column.

$$C_{11}^{2}+C_{12}^{2}+C_{13}^{2} = \frac{1}{p_{z}^{2}}[k_{u}^{2}(n_{x}^{2}+o_{x}^{2}+a_{x}^{2}) + 2k_{u}u_{0}(n_{x}n_{z}+o_{x}o_{z}+a_{x}a_{z})+u_{0}^{2}(n_{z}^{2}+o_{z}^{2}+a_{z}^{2})].$$
(2.27)

Simplifying (2.27) using properties of n, o, and a, and choosing the correct sign, we can solve for  $u_0$ . From Equation (2.12), and from the assumption that  $k_u$  and  $k_v$  are positive, we can interpret a positive  $u_0$  to be the distance of the u-v origin left of the image center, and a positive  $v_0$  to be the distance of the origin below the image center. In our vision system, the origin of the coordinate axes is at the lower left hand corner of the image plane so our  $u_0$  and  $v_0$  are positive.

$$u_0 = \sqrt{p_z^2 (C_{11}^2 + C_{12}^2 + C_{13}^2) - k_u^2}$$
(2.28)

Finding  $k_v$  is similar to finding  $k_u$  except that we are working with the second and third rows of the C matrix. We will just state the results here.

$$k_{\tau} = p_{z}^{2} \sqrt{(C_{21}C_{32} - C_{31}C_{22})^{2} + (C_{21}C_{33} - C_{31}C_{23})^{2} + (C_{22}C_{33} - C_{32}C_{23})^{2}}.$$
 (2.29)

To find  $v_0$ , it is similar to the method for finding  $u_0$  except that we are working with the second row. We get

$$\mathbf{v}_{0} = \sqrt{\mathbf{p}_{z}^{2}(\mathbf{C}_{21}^{2} + \mathbf{C}_{22}^{2} + \mathbf{C}_{23}^{2}) - \mathbf{k}_{v}^{2}}$$
(2.30)

Now that  $n_z$ ,  $o_z$ ,  $a_z$ ,  $p_z$ ,  $k_u$ ,  $k_v$ ,  $u_0$ , and  $v_0$  are found, we can use equate the eight elements of both sides of (2.16) and solve for the eight remaining unknowns.

$$n_{x} = \frac{p_{z}}{k_{u}}(C_{11} - n_{z}u_{0}), \qquad (2.31)$$

$$o_x = \frac{p_z}{k_u} (C_{12} - o_z u_0),$$
 (2.32)

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$$a_{x} = \frac{p_{z}}{k_{u}}(C_{13}-a_{z}u_{0}),$$
 (2.33)

$$p_{x} = \frac{p_{z}}{k_{u}} (C_{14} - p_{z}u_{0}), \qquad (2.34)$$

$$n_{y} = \frac{p_{z}}{k_{y}} (C_{21} - n_{z} v_{0}), \qquad (2.35)$$

$$o_y = \frac{p_z}{k_v} (C_{22} - o_z v_0),$$
 (2.36)

$$a_{y} = \frac{p_{z}}{k_{y}}(C_{23}-a_{z}v_{0}),$$
 (2.37)

$$\mathbf{p}_{\mathbf{y}} = \frac{\mathbf{p}_{\mathbf{z}}}{\mathbf{k}_{\mathbf{y}}} (\mathbf{C}_{\mathbf{24}} - \mathbf{p}_{\mathbf{z}} \mathbf{v}_{\mathbf{0}}).$$

(2.38)

#### 2.2. Space Resection

This technique involves the formulation of nonlinear equations involving the position and orientation parameters, and then solving for the solution iteratively by the Newton-Raphson algorithm.

Figure 2.2 shows the relationship between the frames CAM and OBJ. We want to find  $^{CAM}T_{OBJ}$ ; this is equivalent to finding a sequence of transformations which takes a frame from CAM to OBJ:

$$^{CAM}T_{OBJ} = Rot(z, -\kappa)Rot(y, -\phi)Rot(x, -\omega)Trans(-x_{c}, -y_{c}, -z_{c}).$$
(2.39)

CAM is rotated about its z-axis by  $-\kappa$ , followed by a rotation about the y-axis of the rotated frame by  $-\phi$ , a rotation about the x-axis of the rotated frame by  $-\omega$ , followed by a translation of  $(-x_c, -y_c, -z_c)^t$  with respect to the resulting frame; the final frame will coincide with OBJ. Multiplying the matrices in (2.39) together we have the n, o, a, and p vectors of  $CAM_{TOBJ}$  as follows:

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			n an star Star an star		
a transformation National Antonio	0	0 0 1			
$CAM \begin{bmatrix} \mathbf{T} \end{bmatrix}_{OBJ}$	= n <sub>z</sub>	$o_z a_z p_z$			(2.40
	n <sub>y</sub>	$o_{\mathbf{x}} = \mathbf{x} + \mathbf{x}$ $o_{\mathbf{y}} = \mathbf{a}_{\mathbf{y}} + \mathbf{p}_{\mathbf{y}}$			
	n,	$o_{\mathbf{x}} \mathbf{a}_{\mathbf{x}} \mathbf{p}_{\mathbf{x}}$			

A set of collinearity equations are formed when we rotate CAM by the three rotations so that CAM and OBJ have the same orientation. Notice that we have not translated CAM at this point so it is still at a different position from OBJ, as shown in Figure 2.3. The OBJ frame has coordinate axes x-y-z;  $(x_f,y_f,z_f)^t$  and  $(x_c,y_c,z_c)^t$ are the coordinates of the feature point and the CAM origin with respect to OBJ. CAM has coordinate axes x'-y'-z' and  $(x'_u,y'_u,z'_u)^t$  is the point where the line that joins the feature point and the focal point intersects the image plane, with respect to CAM. After the rotation, as shown in Figure 2.3, the resulting frame is x''-y''-z'', and the intersection point expressed in this coordinate axes is  $(x''_u,y''_u,z''_u)^t$ . From similar triangles in Figure 2.3, we have

$$\left(\frac{\mathbf{x''_{u}}}{\mathbf{x_{f}}-\mathbf{x_{c}}}\right) = \left(\frac{\mathbf{y''_{u}}}{\mathbf{y_{f}}-\mathbf{y_{c}}}\right) = \left(\frac{\mathbf{z''_{u}}}{\mathbf{z_{f}}-\mathbf{z_{c}}}\right)$$
(2.41)

These equations can be rewritten as

$$\mathbf{x''}_{\mathbf{u}} = \left[\frac{\mathbf{x}_{\mathbf{f}} - \mathbf{x}_{\mathbf{c}}}{\mathbf{z}_{\mathbf{f}} - \mathbf{z}_{\mathbf{c}}} \mathbf{z''}_{\mathbf{u}}\right], \qquad (2.42a)$$

$$\mathbf{y''}_{\mathbf{u}} = \left[ \frac{\mathbf{y}_{\mathbf{f}} - \mathbf{y}_{\mathbf{c}}}{\mathbf{z}_{\mathbf{f}} - \mathbf{z}_{\mathbf{c}}} \mathbf{z''}_{\mathbf{u}} \right], \qquad (2.42b)$$

$$\mathbf{z''}_{\mathbf{u}} = \left[ \frac{\mathbf{z}_{\mathbf{f}} - \mathbf{z}_{\mathbf{c}}}{\mathbf{z}_{\mathbf{f}} - \mathbf{z}_{\mathbf{c}}} \mathbf{z''}_{\mathbf{u}} \right], \qquad (2.42c)$$

Since we have rotated *CAM* to the same orientation as *OBJ*, we can use the rotation vectors  $(n,o,a)^t$  of  ${}^{CAM}T_{OBJ}$  to relate  $(x''_u,y''_u,z''_u)^t$  and  $(x'_u,y'_u,z'_u)^t$ . We have

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$$\begin{bmatrix} x'_{u} \\ y'_{u} \\ z'_{u} \\ 1 \end{bmatrix} = \begin{bmatrix} n_{x} & o_{x} & a_{x} & 0 \\ n_{y} & o_{y} & a_{y} & 0 \\ n_{z} & o_{z} & a_{z} & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} x''_{u} \\ y''_{u} \\ z''_{u} \\ 1 \end{bmatrix}.$$
(2.43)

Multiplying out, we have

$$x'_{u} = n_{x}x''_{u} + o_{x}y''_{u} + a_{x}z''_{u}$$
(2.44a)

$$y'_{u} = n_{y}x''_{u} + o_{y}y''_{u} + a_{y}z''_{u}$$
 (2.44b)

$$z'_{u} = n_{z}x''_{u} + o_{z}y''_{u} + a_{z}z''_{u}$$
 (2.44c)

Substituting (2.43a, 2.43b, 2.43c, 2.44c) into (2.44a, 2.44b), and substituting  $z'_u$  by the focal length F, we have

$$\mathbf{x'_{u}} = \mathbf{F}\left[\frac{n_{\mathbf{x}}(\mathbf{x_{f}} - \mathbf{x_{c}}) + o_{\mathbf{x}}(\mathbf{y_{f}} - \mathbf{y_{c}}) + a_{\mathbf{x}}(\mathbf{z_{f}} - \mathbf{z_{c}})}{n_{\mathbf{z}}(\mathbf{x_{f}} - \mathbf{x_{c}}) + o_{\mathbf{z}}(\mathbf{y_{f}} - \mathbf{y_{c}}) + a_{\mathbf{z}}(\mathbf{z_{f}} - \mathbf{z_{c}})}\right]$$
(2.45a)

$$y'_{u} = F\left[\frac{n_{y}(x_{f}-x_{c})+o_{y}(y_{f}-y_{c})+a_{y}(z_{f}-z_{c})}{n_{z}(x_{f}-x_{c})+o_{z}(y_{f}-y_{c})+a_{z}(z_{f}-z_{c})}\right]$$
(2.45b)

In these two non-linear equations,  $(x_f, y_f, z_f)^t$  is known, and  $(x'_u, y'_u)^t$  can be calculated from  $(u, v)^t$  with (2.12) assuming the camera parameters are known. The unknowns we want to solve are the rotations  $\omega$ ,  $\phi$ , and  $\kappa$  (concealed in n, o, a), and the origin of  $CAM(x_{c,}y_{c,}z_c)^t$ . We will arrange these two equations in suitable form before applying the Newton-Raphson algorithm. Equations (2.45a,b) are rewritten as

$$G = qx'_{u} - rf = 0 \qquad (2.46a)$$

$$H = qy'_u - sf = 0 \tag{2.46b}$$

where

$$q = n_{z}(x_{f}-x_{c})+o_{z}(y_{f}-y_{c})+a_{z}(z_{f}-z_{c})$$

$$r = n_{x}(x_{f}-x_{c})+o_{x}(y_{f}-y_{c})+a_{x}(z_{f}-z_{c})$$

$$s = n_{y}(x_{f}-x_{c})+o_{y}(y_{f}-y_{c})+a_{y}(z_{f}-z_{c})$$

Equations (2.46a,b) are linearized using Taylor's theorem,

$$(G)_{0} + \left(\frac{\partial G}{\partial x'_{u}}\right)_{0} dx_{a} + \left(\frac{\partial G}{\partial \omega}\right)_{0} d\omega + \left(\frac{\partial G}{\partial \phi}\right)_{0} d\phi + \left(\frac{\partial G}{\partial \kappa}\right)_{0} d\kappa \qquad (2.47a)$$

$$+ \left(\frac{\partial G}{\partial x_{c}}\right)_{0} dx_{c} + \left(\frac{\partial G}{\partial y_{c}}\right)_{0} dy_{c} + \left(\frac{\partial G}{\partial z_{c}}\right)_{0} dz_{c} = 0$$

$$(H)_{0} + \left(\frac{\partial G}{\partial y'_{u}}\right)_{0} dx'_{u} + \left(\frac{\partial H}{\partial \omega}\right)_{0} d\omega + \left(\frac{\partial H}{\partial \phi}\right)_{0} d\phi + \left(\frac{\partial H}{\partial \kappa}\right)_{0} d\kappa \qquad (2.47b)$$

$$+ \left(\frac{\partial H}{\partial x_{c}}\right)_{0} dx_{c} + \left(\frac{\partial H}{\partial y_{c}}\right)_{0} dy_{c} + \left(\frac{\partial H}{\partial z_{c}}\right)_{0} dz_{c} = 0$$

(G)<sub>0</sub>, (H)<sub>0</sub>,  $(\partial G/\partial \omega)_0$ , etc., are the functions G, H and their partial derivatives evaluated at the initial approximations. The d $\omega$ , d $\phi$ , d $\kappa$ , d $\mathbf{x}_c$ , d $\mathbf{y}_c$  and d $\mathbf{z}_c$  are corrections to the initial approximations. From Equations (2.46a,b),

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$$\frac{\partial \mathbf{G}}{\partial \mathbf{x'_u}} = \frac{\partial \mathbf{H}}{\partial \mathbf{y'_u}} = \mathbf{q}$$
(2.48)

Performing the partial differentiations and simplifying, Equations (2.47a,b) can be written as follows:

$$dx'_{u} = b_{11}d\omega + b_{12}d\phi + b_{13}d\kappa - b_{14}dx_{c} - b_{15}dy_{c} - b_{16}dz_{c} + J$$
(2.49a)

$$dy'_{u} = b_{21}d\omega + b_{22}d\phi + b_{23}d\kappa - b_{24}dx_{c} - b_{25}dy_{c} - b_{26}dz_{c} + K$$
(2.49b)

where

$$\begin{split} \Delta \mathbf{x} = \mathbf{x}_{f} - \mathbf{x}_{c} \\ \Delta \mathbf{y} = \mathbf{y}_{f} - \mathbf{y}_{c} \\ \Delta \mathbf{z} = \mathbf{z}_{f} - \mathbf{z}_{c} \\ \mathbf{b}_{11} = \frac{\mathbf{x}'_{u}}{q} (\mathbf{o}_{z} \Delta \mathbf{z} - \mathbf{a}_{z} \Delta \mathbf{y}) + \frac{\mathbf{f}}{q} (\mathbf{a}_{x} \Delta \mathbf{y} - \mathbf{o}_{x} \Delta \mathbf{z}) \\ \mathbf{b}_{12} = \frac{\mathbf{x}'_{u}}{q} (\Delta \mathbf{x} \cos\phi + \Delta \mathbf{y} \sin\omega \sin\phi - \Delta \mathbf{z} \sin\phi \cos\omega) \\ + \frac{\mathbf{f}}{q} (\Delta \mathbf{x} \sin\phi \cos\kappa - \Delta \mathbf{y} \sin\omega \cos\phi \cos\kappa) \\ -\Delta \mathbf{z} \cos\omega \cos\phi \cos\kappa \\ \mathbf{b}_{13} = -\frac{\mathbf{f}}{q} (\mathbf{n}_{y} \Delta \mathbf{x} + \mathbf{o}_{y} \Delta \mathbf{y} + \mathbf{a}_{y} \Delta \mathbf{z}) \\ \mathbf{b}_{14} = \frac{\mathbf{x}'_{u}}{q} \mathbf{n}_{z} - \frac{\mathbf{f}}{q} \mathbf{n}_{x} \\ \mathbf{b}_{15} = \frac{\mathbf{x}'_{u}}{q} \mathbf{o}_{z} - \frac{\mathbf{f}}{q} \mathbf{o}_{x} \\ \mathbf{b}_{16} = \frac{\mathbf{x}'_{u}}{q} \mathbf{a}_{z} - \frac{\mathbf{f}}{q} \mathbf{a}_{x} \\ \mathbf{J} = \frac{\mathbf{q}\mathbf{x}'_{u} - \mathbf{r}\mathbf{f}}{q} \end{split}$$



 $+\Delta z \cos \omega \cos \phi \sin \kappa$ 



Equations (2.49a,b) can be used to solve for  $d\omega$ ,  $d\phi$ ,  $d\kappa$ ,  $dx_c$ ,  $dy_c$  and  $dz_c$ , the corrections for the orientation and position of the camera in order to improve the accuracy after each iteration. These changes are then added on to the previous estimate of  $\omega$ ,  $\phi$ ,  $\kappa$ ,  $x_c$ ,  $y_c$ , and  $z_c$  to get more accurate values. The iterations are terminated when the differential changes are smaller than the desired tolerance.

Three points are required to set up six equations in order to solve for the six unknowns. If there are more than three unknowns, mean square method can be used to minimize the sum of squares of the errors on the image positions  $(x'_{u,y}y'_{u,j})^t$ . For three different image features, Equations (2.49a,b) can be written in a matrix form.

$$\begin{bmatrix} J_{1} \\ K_{1} \\ J_{2} \\ K_{2} \\ J_{3} \\ K_{3} \end{bmatrix} = \begin{bmatrix} -b_{11_{1}} & -b_{12_{1}} & -b_{13_{1}} & b_{14_{1}} & b_{15_{1}} & b_{16_{1}} \\ -b_{21_{1}} & -b_{22_{1}} & -b_{23_{1}} & b_{24_{1}} & b_{25_{1}} & b_{26_{1}} \\ -b_{11_{2}} & -b_{12_{2}} & -b_{13_{2}} & b_{14_{2}} & b_{15_{2}} & b_{16_{2}} \\ -b_{21_{2}} & -b_{22_{2}} & -b_{23_{2}} & b_{24_{2}} & b_{25_{2}} & b_{26_{2}} \\ -b_{21_{2}} & -b_{22_{2}} & -b_{23_{2}} & b_{24_{2}} & b_{25_{2}} & b_{26_{2}} \\ -b_{11_{3}} & -b_{12_{3}} & -b_{13_{3}} & b_{14_{3}} & b_{15_{3}} & b_{16_{3}} \\ -b_{21_{3}} & -b_{22_{3}} & -b_{23_{3}} & b_{24_{3}} & b_{25_{3}} & b_{26_{3}} \end{bmatrix} \begin{bmatrix} d\omega \\ d\phi \\ d\kappa \\ d\kappa \\ dx_{c} \\ dy_{c} \\ dy_{c} \\ dz_{c} \end{bmatrix} + \begin{bmatrix} dx'_{u_{1}} \\ dy'_{u_{1}} \\ dx'_{u_{2}} \\ dy'_{u_{2}} \\ dx'_{u_{3}} \\ dy'_{u_{3}} \end{bmatrix}$$
 (2.50)

This equation is rewritten as

$$\mathbf{L} = \mathbf{A}\mathbf{X}_{c} + \mathbf{V} \tag{2.51}$$

where the error V is commonly known as residue. To minimize the residue with more than 3 points,  $X_c$  can be solved as follows.

$$\mathbf{X}_{\mathbf{c}} = (\mathbf{A}^{\mathrm{T}}\mathbf{A})^{-1}\mathbf{A}^{\mathrm{T}}\mathbf{L}$$
(2.52)

#### 2.3. Combining Space Resection with Camera Matrix Decomposition

Since space resection has inherently better behaviour in a noisy environment, it is used to calculate the position of an object. However, this method does require an initial estimate of the position and requires the camera parameters; this can be achieved using calibration matrix decomposition. Camera parameters only have to be found once as long as the same camera and the same lenses are used; a calibration object with abundant features should be used to find the parameters as accurately as possible. When camera calibration is used to find the initial estimate of the position of an object, the camera parameters are re-calculated as a by-product; these values can be ignored because they are not accurate as the one calculated initially.

In order to combine the two techniques, we need to be able to convert their different notations to one another. Calibration matrix used homogeneous transforms while space resection expresses positions and orientations in terms of  $(\mathbf{x}_c, \mathbf{y}_c, \mathbf{z}_c, \omega, \phi, \kappa)^t$ .

The results of space resection will be in terms of  $(x_c, y_c, z_c, \omega, \phi, \kappa)^t$ , we can convert them into a homogeneous transform using (2.40).

The initial estimate found by calibration matrix decomposition is a homogeneous transform. To convert it to  $(\mathbf{x}_c, \mathbf{y}_c, \mathbf{z}_c, \omega, \phi, \kappa)^t$ , we will use a method used by Paul, Renald, and Stevenson [Paul83]. We will first solve for the rotation part of the matrix. Let

$$\mathbf{M} = \begin{bmatrix} \mathbf{n}_{\mathbf{x}} & \mathbf{o}_{\mathbf{x}} & \mathbf{a}_{\mathbf{x}} \\ \mathbf{n}_{\mathbf{y}} & \mathbf{o}_{\mathbf{y}} & \mathbf{a}_{\mathbf{y}} \\ \mathbf{n}_{\mathbf{z}} & \mathbf{o}_{\mathbf{z}} & \mathbf{a}_{\mathbf{z}} \end{bmatrix}$$
(2.53)

Let us define U and V matrices as in [Paul83].

$$\mathbf{V}_0 = \mathbf{R}_1 \mathbf{R}_2 \mathbf{R}_3 = \mathbf{M} = \mathbf{U}_1 \tag{2.54}$$

$$V_1 = R_2 R_3 = R_1^{-1} M = U_2$$
 (2.55)

$$\mathbf{V}_2 = \mathbf{R}_3 = \mathbf{R}_2^{-1} \mathbf{V}_1 = \mathbf{U}_3.$$
 (2.56)

where  $\mathbf{R}_1$ ,  $\mathbf{R}_2$ , and  $\mathbf{R}_3$  are the rotational matrices about the z, y, and x axes by  $-\kappa$ ,  $-\phi$ , and  $-\omega$ , respectively. Let  $\mathbf{V}_{i_j}$  denote the jth column of  $\mathbf{V}_i$  and let  $\mathbf{M}_j = [\mathbf{s}_i, \mathbf{r}_i, \mathbf{t}_i]^T$  stands for the jth column of  $\mathbf{M}$ , i.e.,

$$\mathbf{M}_1 = [\mathbf{n}_{\mathbf{x}} \ \mathbf{n}_{\mathbf{y}} \ \mathbf{n}_{\mathbf{z}}]^{\mathrm{T}}, \mathbf{M}_2 = [\mathbf{o}_{\mathbf{x}} \ \mathbf{o}_{\mathbf{y}} \ \mathbf{o}_{\mathbf{z}}]^{\mathrm{T}}, \mathbf{M}_3 = [\mathbf{a}_{\mathbf{x}} \ \mathbf{a}_{\mathbf{y}} \ \mathbf{a}_{\mathbf{z}}]^{\mathrm{T}}.$$

From (2.55),

$$\mathbf{V}_{1_{j}} = \mathbf{R}_{1}^{-1} \mathbf{M}_{j} = \begin{bmatrix} \mathbf{C}_{\kappa} & -\mathbf{S}_{\kappa} & \mathbf{0} \\ \mathbf{S}_{\kappa} & \mathbf{C}_{\kappa} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & 1 \end{bmatrix} \begin{bmatrix} \mathbf{s}_{j} \\ \mathbf{r}_{j} \\ \mathbf{t}_{j} \end{bmatrix}$$
(2.57)

$$= \begin{bmatrix} \mathbf{C}_{\kappa} \mathbf{s}_{j} - \mathbf{S}_{\kappa} \mathbf{r}_{j} \\ \mathbf{S}_{\kappa} \mathbf{s}_{j} + \mathbf{C}_{\kappa} \mathbf{r}_{j} \\ \mathbf{t}_{j} \end{bmatrix} = \begin{bmatrix} \mathbf{v}_{11j} \\ \mathbf{v}_{12j} \\ \mathbf{t}_{j} \end{bmatrix}$$

where

$$\mathbf{v}_{11j} = \mathbf{C}_{\kappa} \mathbf{s}_j - \mathbf{S}_{\kappa} \mathbf{r}_j \tag{2.58}$$

$$\mathbf{v}_{12j} = \mathbf{S}_{\kappa} \mathbf{s}_{j} + \mathbf{C}_{\kappa} \mathbf{r}_{j} \tag{2.59}$$

From (2.56), to express  $V_{2_j}$  in terms of  $M_j$ ,

$$\mathbf{V}_{2_{j}} = \mathbf{R}_{2}^{-1} \mathbf{M}_{j} = \begin{bmatrix} C_{\phi} \mathbf{v}_{11} + S_{\phi} \mathbf{t}_{j} \\ \mathbf{v}_{12} \\ -S_{\phi} \mathbf{v}_{11} + C_{\phi} \mathbf{t}_{j} \end{bmatrix}$$
(2.60)

Now we can equate  $V_2$  to  $R_3$ ,

$$\begin{bmatrix} \mathbf{V}_{2_{1}}\mathbf{V}_{2_{2}}\mathbf{V}_{2_{3}} \end{bmatrix} \begin{bmatrix} C_{\phi}\mathbf{v}_{111} + S_{\phi}\mathbf{n}_{z} & C_{\phi}\mathbf{v}_{112} + S_{\phi}\mathbf{o}_{z} & C_{\phi}\mathbf{v}_{113} + S_{\phi}\mathbf{a}_{z} \\ \mathbf{v}_{121} & \mathbf{v}_{122} & \mathbf{v}_{123} \\ -S_{\phi}\mathbf{v}_{111} + C_{\phi}\mathbf{n}_{z} & -S_{\phi}\mathbf{v}_{112} + C_{\phi}\mathbf{o}_{z} & -S_{\phi}\mathbf{v}_{113} + C_{\phi}\mathbf{a}_{z} \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & C_{\omega} & S_{\omega} \\ 0 & -S_{\omega} & C_{\omega} \end{bmatrix} (2.61)$$

$$C_{\omega} = \mathbf{v}_{122} = S_{\kappa} \mathbf{o}_{\mathbf{x}} + C_{\kappa} \mathbf{o}_{\mathbf{y}}$$
(2.62)

$$S_{\omega} = S_{\phi} v_{112} - C_{\phi} o_{z} = S_{\phi} (C_{\kappa} o_{x} - S_{\kappa} o_{y}) - C_{\phi} o_{z}$$

$$(2.63)$$

A unique value of  $\omega$  can be found by the atan2 function using sine and cosine as arguments.

$$\omega = \tan^{-1} \frac{S_{\omega}}{C_{\omega}}$$
(2.64)

To solve for  $\phi$ , we equate  $V_1$  to  $U_2$ .

$$\begin{bmatrix} C_{\kappa} \mathbf{x} - S_{\kappa} \mathbf{y} \\ S_{\kappa} \mathbf{x} - C_{\kappa} \mathbf{y} \\ \mathbf{z} \end{bmatrix} = \mathbf{R}_{2} \mathbf{R}_{3}$$
(2.65)

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$$\begin{bmatrix} \mathbf{C}_{\phi} & \mathbf{S}_{\phi}\mathbf{S}_{\omega} & -\mathbf{S}_{\phi}\mathbf{C}_{\omega} \\ \mathbf{0} & \mathbf{C}_{\omega} & \mathbf{S}_{\omega} \\ \mathbf{S}_{\phi} & -\mathbf{C}_{\phi}\mathbf{S}_{\omega} & \mathbf{C}_{\phi}\mathbf{C}_{\omega} \end{bmatrix}$$

$$C_{\phi} = C_{\kappa} n_{\chi} - S_{\kappa} n_{\gamma}$$
(2.67)

$$S_{\phi} = n_{z}$$
(2.68)

$$\phi = \tan^{-1} \frac{S_{\phi}}{C_{\phi}} \tag{2.69}$$

Finally, to solve for  $\kappa$ , we equate  $V_0$  to  $U_1$ ,

$$\begin{bmatrix} \mathbf{n}_{\mathbf{x}} & \mathbf{o}_{\mathbf{x}} & \mathbf{a}_{\mathbf{x}} \\ \mathbf{n}_{\mathbf{y}} & \mathbf{o}_{\mathbf{y}} & \mathbf{a}_{\mathbf{y}} \\ \mathbf{n}_{\mathbf{z}} & \mathbf{o}_{\mathbf{z}} & \mathbf{a}_{\mathbf{z}} \end{bmatrix} = \begin{bmatrix} \mathbf{C}_{\kappa} \mathbf{C}_{\phi} & ? & ? \\ -\mathbf{S}_{\kappa} \mathbf{C}_{\phi} & ? & ? \\ \mathbf{S}_{\phi} & ? & ? \end{bmatrix}$$
(2.70)

where the terms with question marks are not used.

$$C_{\kappa} = \frac{n_{\chi}}{C_{\phi}}$$
(2.71)

$$S_{\kappa} = -\frac{n_{y}}{C_{\phi}}$$
(2.72)

It can be concluded that

$$\kappa = \tan^{-1} \frac{-n_{y}}{n_{x}} \quad \text{if } C_{\phi} > 0 \tag{2.73}$$

$$\kappa = \tan^{-1} \frac{n_{y}}{-n} \quad \text{if } C_{\phi} < 0$$

Note that  $\kappa$  is undefined when  $C_{\phi} = 0$ . There are multiple solutions to  $\kappa$ ,  $\phi$  and  $\omega$ . We only have to find one set of these solutions since we are only translating one set of notation to another and are not concerned about the mechanical configurations of an arm.

To find  $x_c$ ,  $y_c$  and  $z_c$  is straightforward once one realizes that they are the origin of the camera coordinate axes with respect to the object. The transform of the camera with respect to the object is just  $CAM T_{OBJ}^{-1}$ .

$$\begin{vmatrix} n_{x} & n_{y} & n_{z} & -n.p \\ o_{x} & o_{y} & o_{z} & -o.p \\ a_{x} & a_{y} & a_{z} & -a.p \\ 0 & 0 & 0 & 1 \end{vmatrix}$$
 (2.74)

Therefore,

$$x_{c} = -n.p$$
 (2.75)  
 $y_{c} = -o.p$  (2.76)  
 $z_{c} = -a.p$  (2.77)

#### 3. Finding Object Position with Two Views

We have discussed finding an object position with a single view in the last section. Ganapathy's method requires six points while space resection method requires three points. Fischler and Bolles [Fisc 81] showed that space resection with less than 6 points may have multiple solutions. To disambiguate the solutions, we can either check the consistencies of the solutions with the image, or we can use more than one view.

Multiple views are also useful when we deal with an object with very few local features, or when the viewpoint is degenerate (when the features and the focal point lie on the same circle), or when some of the features are occluded. An example of this kind of application is locating a wire or a thin peg; a wire has only two features.

we will discuss a method which uses two views to find the positions of individual feature points. Figure 3.1 shows a thin rod and its image on two cameras whose positions and orientations are known. CAM and CAM' are the coordinate frames of the two cameras. We can find the 3D coordinates of P1 and P2 by finding intersection of lines  $l_1$  and  $l'_1$  and intersection of lines  $l_2$  and  $l'_2$  respectively. For demonstration purposes, we will find P1 with respect to CAM whose coordinate frame is x-y-z. The parametric equation of  $l_1$  is

$$(\mathbf{x},\mathbf{y},\mathbf{z})^{t} = (0,0,-f)^{t} + t(\mathbf{x}_{1},\mathbf{y}_{1},f)^{t},$$
 (3.1)

where  $(x_1, y_1)^1$  are the image coordinates of the point P1 and f is the focal length. The equation of  $l'_1$  with respect to CAM' is

$$(\mathbf{x}',\mathbf{y}',\mathbf{z}')^{t} = (0,0,-f)^{t} + t'(\mathbf{x}'_{1},\mathbf{y}'_{1},f)^{t}.$$
(3.2)

We can specify this equation with respect to CAM by specifying the point  $(0,0,-f)^t$ and the vector  $(x'_{1},y'_{1},f)^t$  with respect to CAM. If

$$\mathbf{T} = \begin{bmatrix} n_{\mathbf{x}} & o_{\mathbf{x}} & a_{\mathbf{x}} & p_{\mathbf{x}} \\ n_{\mathbf{y}} & o_{\mathbf{y}} & a_{\mathbf{y}} & p_{\mathbf{y}} \\ n_{\mathbf{z}} & o_{\mathbf{z}} & a_{\mathbf{z}} & p_{\mathbf{z}} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$
(3.3)

is the transform matrix from CAM to CAM', then the point  $^{CAM'}(0,0,-f)^t$  is transformed too

 $^{CAM}(-a_xf+p_x,-a_yf+p_y,-a_zf+p_z)^t,$ 

and the vector  $CAM'(x'_1,y'_1,f)^t$  is transformed to

$$n_y x'_1 + o_y y'_1 + a_y f, n_z x'_1 + o_z y'_1 + a_z f)^t$$

Thus the equation of  $l'_1$  is

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$$(\mathbf{x},\mathbf{y},\mathbf{z})^{t} = (-\mathbf{a}_{\mathbf{x}}\mathbf{f} + \mathbf{p}_{\mathbf{x}}, -\mathbf{a}_{\mathbf{y}}\mathbf{f} + \mathbf{p}_{\mathbf{y}}, -\mathbf{a}_{\mathbf{z}}\mathbf{f} + \mathbf{p}_{\mathbf{z}})^{t} +$$

$$t'(\mathbf{n}_{\mathbf{x}}\mathbf{x}'_{1} + \mathbf{n}_{\mathbf{y}}\mathbf{y}'_{1} + \mathbf{n}_{\mathbf{z}}\mathbf{f}, \mathbf{n}_{\mathbf{y}}\mathbf{x}'_{1} + \mathbf{o}_{\mathbf{y}}\mathbf{y}'_{1} + \mathbf{a}_{\mathbf{y}}\mathbf{f}, \mathbf{n}_{\mathbf{z}}\mathbf{x}'_{1} + \mathbf{o}_{\mathbf{z}}\mathbf{y}'_{1} + \mathbf{a}_{\mathbf{z}}\mathbf{f})^{t}$$

$$(3.4)$$

The two lines generally may not intersect because of errors; we will find the mid-point of the shortest line segment joining  $l_1$  and  $l'_1$ . Let us rewrite the two lines as

$$l_1:(x,y,z)^t = (x_0,y_0,z_0)^t + t(a,b,c)^t,$$
(3.5)

$$l'_{1}:(\mathbf{x},\mathbf{y},\mathbf{z})^{t} = (\mathbf{x}'_{0},\mathbf{y}'_{0},\mathbf{z}'_{0})^{t} + t'(\mathbf{a}',\mathbf{b}',\mathbf{c}')^{t},$$
(3.6)

Let D be the distance form a point on  $l_1$  to  $l'_1$ .

$$D^{2} = (x_{0} + at - x'_{0} - a't')^{2} + (y_{0} + bt - y'_{0} - a't')^{2} + (z_{0} + ct - z'_{0} - c't')^{2}$$
(3.7)

Taking partial derivatives with respect to t and t', we will have two linear equations from which we can solve for t and t':

$$a'(x_0-x'_0)+b'(y_0-y'_0)+c'(z_0-z'_0)+t(aa'+bb'+cc')-t'(a'^2+b'^2+c'^2)=0.$$
 (3.8)

$$a(x_0-x'_0)+b(y_0-y'_0)+c(z_0-z'_0)-t'(aa'+bb'+cc')+t(a^2+b^2+c^2)=0.$$
 (3.9)

From the values of t and t', we can find points on the two lines that are closest to one another. We will take the mid-point as the estimate of the intersection of these two lines. Once P1 and P2 are found by this method, we can find the p and a vector of the homogeneous frame of the peg. There are infinite number of solutions for the n and o vector since the peg is symmetric about the z-axis. If P1 =  $(p_{1x}, p_{1y}, p_{1z})^{t}$  and P2 =  $(p_{2x}, p_{2y}, p_{2z})^{t}$ ,

$$(p_x, p_y, p_z)^t = (p2_x, p2_y, p2_z)^t,$$
 (3.10)

$$(\mathbf{a}_{x}, \mathbf{a}_{y}, \mathbf{a}_{z})^{t} = \frac{(p_{1x} - p_{2x}, p_{1y} - p_{2y}, p_{1z} - p_{2z})^{t}}{\sqrt{(p_{1x} - p_{2x})^{2} + (p_{1y} - p_{2y})^{2}(p_{1z} - p_{2z})^{2}}}$$
(3.11)

#### 4. Formulating The Manipulator Sequences in terms of Homogeneous Transform Equations

We will show two examples of formulating transform equations. In the first example, we assume the camera is mounted on the robot wrist and the task is to pick up an object in a two-move sequence. The second example shows an assembly task where the camera is located arbitrarily. We will also show the use of a time-variant  $\mathbf{R}(\gamma)$  transform which is servoed visually.

In the first example, the camera is fixed to the robot wrist, and the object to be grasped is assumed to be within the view of the camera The relative position of the object with respect to the camera can be calculated using techniques described in the last section, let us denote this transformed as  $^{CAM}T_{OBJ}$ . We also let T6(k) and T6(k+1) be the current position and the next position of the manipulator end, HAND be the gripper position with respect to manipulator wrist flange,  $^{T6}T_{CAM}$  be the camera position

relative to manipulator wrist flange, and APPR be the predefined "approach" position of the gripper with respect to the object. From Figure 4.1, we have

T6(k+1) can be solved as

 $\mathbf{T6}(\mathbf{k+1}) = \mathbf{T6}(\mathbf{k}) \quad {}^{\mathbf{T6}}\mathbf{T}_{CAM}$ 

After the move to the "approach" position, the robot will move on to the "grasp" position. The **T6** will be calculated using an equation similar to the previous one, except that **APPR** is replaced by **GRASP**.

Figure 4.2 shows two robots assembling two parts and the camera is at an arbitrary position viewing the part-mating operation; visual Servoing is used to overcome the mismatch of the two robot spaces (see next section). The camera position is not assumed to be known since the method described will be independent of it. Let OBJ1 and OBJ2 be the top object and the bottom object respectively. The relative position of OBJ1 with respect to OBJ2 ( $^{OBJ2}\mathbf{T}_{OBJ1}$ ) can be found by vision.

Assume Robot2 holding OBJ2 remains stationary and we want to move the Robot1 which manipulates OBJ1. We want to move Robot1 such that OBJ1 is at the desired "approach" position with respect to OBJ2, and let this transform be  $^{OBJ2}$ **TAPPR**\_{OBJ1}. Initially, due to coordinate mismatch, OBJ1 is at  $^{OBJ2}$ **T**(k)<sub>OBJ1</sub>, we want to move Robot1 such that OBJ1 is at the correct "approach" position. Let **T6**(k) and **T6**(k+1) be the position of the current position and next

position of Robot1 respectively, and GRASP1 and HAND1 be defined similar to the previous example. From Figure 4.2, we can see that

T6(k+1) = T6(k) HAND1 GRASP1<sup>-1</sup> GRASP1 HAND1<sup>-1</sup>

Once OBJ1 is at the "approach" position, we now can proceed to the "mate" position. We can just use an equation similar to the last one except substituting TAPPR by TMATE. However, if the resolution of the vision system is better than the robot accuracy, we should visually servo on all the intermediate positions from the "approach" position to "mate" position in order to acquire better accuracy. This can be accomplished by defining a variable transform  $D(\gamma)$  such that it changes from TAPPR to TMATE when  $\gamma$  changes from 0 to 1. For example, if we want Robot1 to move down from TAPPR to TMATE at a constant speed, and if

$${}^{OBJ}[\mathbf{TAPPR}]_{OBJ2} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & d1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$OBJ^2$$
 TMATE<sub>OBI1</sub> =

we can defined  $D(\gamma)$  as

$$\mathbf{D}(\gamma) = \begin{vmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & (1-\gamma)d1 + \gamma d2 \\ 0 & 0 & 0 & 1 \end{vmatrix}$$

where  $\gamma$  changes from 0 to 1. For general transitions from one transform to another, we can use the more general "drive" function described in Paul's book [Paul83].

#### 5. Conclusions

We have presented methods of calculating object positions from camera images. For objects with enough visible features, we used a combination of calibration matrix decomposition and space resection, and have achieved low noise sensitivity without requiring an initial estimate of the object position. For objects with very few features, we have presented a method which uses multiple views to find the 3D positions of feature points. We have also discussed the usage of the transforms to drive the manipulator during the visual servoeing.

# Appendix: Simulations of Noise Sensitivities

We simulated the noise sensitivities of camera calibration matrix decomposition and space resection by disturbing the 2D position of an feature point at pixel increments, assuming we have a 256 by 256 image. Figure A1 shows the viewpoint of the object and the feature to be disturbed. Figure A2 shows the comparative noise sensitivities.

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Figure 2.2. Viewpoint determination by space resection



Figure 2.3 Aligning the camera frame with the object frame in order to write the colinearity equations



Figure 3.1. Finding object position with two views







Figure 4.2. Transform equations for assembly



Figure A1 Simulated image of a cube. The feature to be perturbed is circled. The simulated image has a resolution of 256×256 pixels and the camera is 500 mm from the closest corner of the cube.



Figure A2. Rotational and translational errors resulting from perturbation of a feature position