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Motivation

Leverage the inter-satellite connectivity potential of constellations for precise orbit determination

Satellite Autonomous Navigation

Satellite autonomous navigation means performing orbit determination on-board the spacecraft without external intervention, which would:

- Reduce reliance on Earth-based resources (ground sensors, beacons, GNSS) for precise orbit determination and dissemination¹
- Enable on-board autonomy for location-based operations and data processing (i.e. reducing data volume to downlink)²
- Minimize operations cost and propellant utilization for satellite station-keeping and constellation maintenance³

On-board sensors used to estimate satellite position and velocity using timeseries measurements of relative range or bearing to known bodies/objects:

Sensor	Measurement	Refere
Rangefinder (e.g. altimeter)	Range	Object (e.g. Ea
Visible/IR camera (e.g. star-tracker)	Range, Bearing	Landm (e.g. st
Magnetometer	Range, Bearing	Magne
Beacon receiver (e.g. GNSS)	Range	Beacor (e.g. G
X-ray detector	Range	Pulsars

Inter-satellite Method

- Utilizes inter-satellite measurements of the relative position vector (range and bearing) between two satellites⁴
- Simultaneously estimates the orbital states of both spacecraft to meterlevel accuracy given precise inter-satellite measurements⁵
- Full satellite states observable in most orbit cases using J₂ Earth gravity model, except when satellites have equal a, e, θ at zero inclination⁵

Accuracy

The figure below illustrates the best orbit estimation error achieved using ground-based tracking and autonomous navigation techniques:

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					SLR	Satellite Laser Ranging (Zhao, G., et al., 2013)
	1-σ orbital e	rror (orders of mag	nitude, not to scale)	VLBI	Very-Long Baseline Interferometry (Ulvestad, J.S., 1992)
	mm	m	km		UHF	Ultra-High Frequency ranging (Foster, C., et al., 2015)
Tracking systems	SLR V	LBI	UHF		NORAD (TLEs)	North American Aerospace Defense Command Two-line Element Sets (Greene, M.R., et al., 2009)
(post-processed or	orbit solutions)	IODE	NORAD (TLEs)		DORIS	Doppler Orbitography and Radiopositioning Integrated by Satellite (Brunet, M., et al. 1995)
Navigation systems (real-time orbit solu	DORIS/D				DORIS/ DIODE	DORIS on-board OD software (Jayles, C., et al., 2015)
	DF-GNSS	SF-GNSS			SF-GNSS	Single-Frequency GNSS (Sun, X., et al., 2017)
	olutions)	Landmark	Pulsars		DF-GNSS	Dual-Frequency GNSS (Hauschild, A., et al., 2017)
					Landmarks	Earth Landmark Sensor (Markley, F.L., 1984)
		Iviag-S			Pulsars	X-Ray Pulsars (Sheikh, S., et al., 2006)
		EHS-S	ST		Mag-SS	Magnetometer & Sun-Sensors (Psiaki, M., 1999)
					EHS-ST	Earth Horizon Sensors & Star-Trackers (Hicks, K., Wiesel, W., 1992)

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Laser Communication Crosslinks for Satellite Autonomous Navigation

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Laser communication (lasercom) systems offer improved energy efficiency, data rates, and security over traditional radio-frequency (RF) communications systems.⁶ Lasercom crosslinks reduce latency in data and command routing in distributed constellations,⁷ and can obtain inter-satellite measurements for autonomous navigation.⁸

Notable Demonstration Missions



ESA's ARTEMIS geosynch. Past: satellite demonstrated the first one-way lasercom crosslink with SPOT-4 in 2001 (left), and first two-way link with OICETS in 2005 (right). Both SPOT-4 and OICETS operated from low Earth orbits.⁹



Future: The MIT STAR Lab and Univ. of Florida are co-developing Cubesat Laser Infrared the CrosslinK (CLICK) mission to demonstrate full duplex lasercom crosslinks between two identical 6U CubeSats with 2U transceivers.

Approach

In this work, a Cramer-Rao Lower Bound (CRLB) analysis is performed to compare the impact of using crosslink measurements from RF and lasercom systems. CRLB provides the theoretical lower limit of an estimator meansquare error primarily based on measurement uncertainty. The CRLB equations for an Extended Kalman Filter (EKF) estimator are:

$$J_{k} = \left(\overline{F}_{k-1}J_{k-1}^{-1}\overline{F}_{k-1}^{T}\right)^{-1} + \overline{H}_{k}^{T}R_{k}^{-1}\overline{H}_{k} \qquad \overline{F}_{k-1} = \left(\frac{\partial f}{\partial x}\right)_{x=x_{k-1}}$$

where
$$CRLB(x_{k}(j)) = J_{k-1}^{-1}(j,j) \qquad \overline{H}_{k} = \left(\frac{\partial h}{\partial x}\right)_{x=x_{k}}$$

Measurements were modeled using the following uncertainties:

	Crosslink Comms	Measurement	RMS Error Mode
	Radio-frequency (RF)	Range	3 m
		Bearing	N/A
	Free-space optical (lasercom)	Range	10 cm
		Bearing	2 arcsec

Three scenarios representing different orbit configurations selected based on existing or proposed satellite mission architectures:

- 2-satellite case GEO-LEO (existing, based on ARTEMIS-OICETS demo)
- Constellation cases SAR-Lupe (existing), 9/3/2 Walker (proposed) \bullet

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Laser Communication Crosslinks

Inter-satellite Measurements

Range – derive from time-encoded signal transfers between satellites

- Optical frequency = greater bandwidth vs. RF systems
- Time transfers on the order of picoseconds¹⁰ \rightarrow cm-level ranging • Multiple transfer methods: one-way, dual one-way, or two-way

Bearing – derive from on-board star-tracker and pointing offsets

- Higher carrier frequency vs. RF systems = narrower beamwidth
- Leverage accurate body-pointing knowledge from star-tracker, along
- with known, fixed offsets between star-tracker and transceiver
- Assumes fine-pointing control is achieved, crosslink is established
- Improve with filters/estimators, feedback from fine-pointing system

Equations adapted from [12]



Bearing not available for RF systems without additional hardware (e.g. camera, beacon).

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- Perform full EKF estimation using simulated measurements

MIT STAR Lab

MIT Space Systems Lab



MIT Lincoln Laboratory





Results

Expand EKF algorithm to estimate satellite clock biases/offsets and spacecraft attitude