

CFD Simulations of a Passively Controlled Point Absorber

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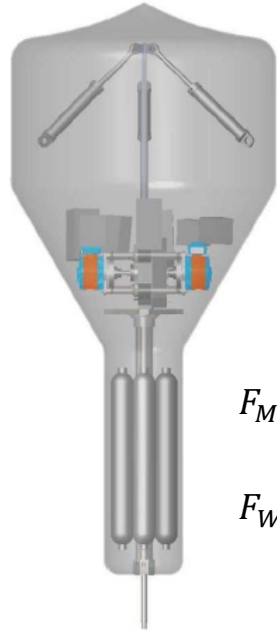
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Research Objectives

- ⚙ Point absorber WEC – designed by CorPower
- ⚙ CFD simulation – motion in regular waves
- ⚙ PTO
- ⚙ Passive control system



Passive control system – WaveSpring



$$F_{WS,z} = N_c p(z) A_c \cdot \frac{z}{\sqrt{l_0^2 + z^2}}$$

$$F_M + F_{PTO} = (-k \cdot \Delta l - F_{pre} - C_{PTO} \cdot u_1) \cdot \mathbf{n}_1$$

$$F_{WS} = F_{WS,z} \cdot \mathbf{n}_1$$

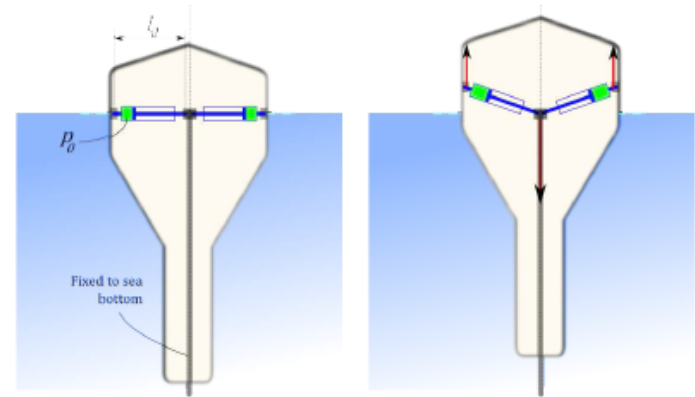


Fig. 5. Illustration of how the buoy displacement induces a vertical spring force with negative stiffness. Buoy in mean vertical position (left) and displaced upwards (right).

Hals et al (EWTEC 2015)

Hydrodynamics Modellings

BEM

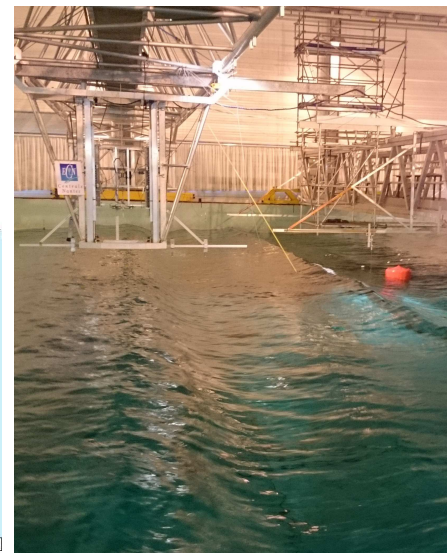
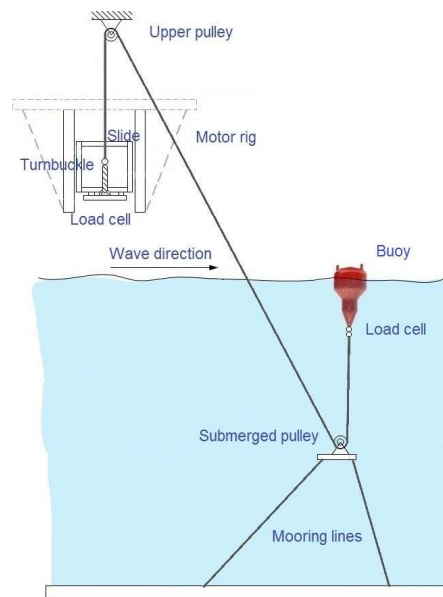
- ⊗ **Small** amplitude assumption
- ⊗ **Small** motion assumption
- ⊗ Viscous term simplified
- ⊗ Overtopping not captured
- ⊗ Some 2nd order effects included (eg. drift, QTF etc)
- ⊗ Nonlinear source term included in time-domain simulation
- ⊗ **FAST** computation

CFD

- ⊗ Nonlinear effects '**All-inclusive**'
- ⊗ Single fluid approximation
- ⊗ Multiphase through (often) VOF
- ⊗ Turbulence models
- ⊗ **SLOW COMPUTATIONS**

Physical Experiments

- ⊗ Hals et al (EWTEC 2015)
- ⊗ Wave basin in Nantes
- ⊗ 1:16 scale buoy
- ⊗ PTO Linear damper
- ⊗ No mooring – linear spring
- ⊗ WaveSpring



Hals et al (EWTEC 2015)

Numerical modellings

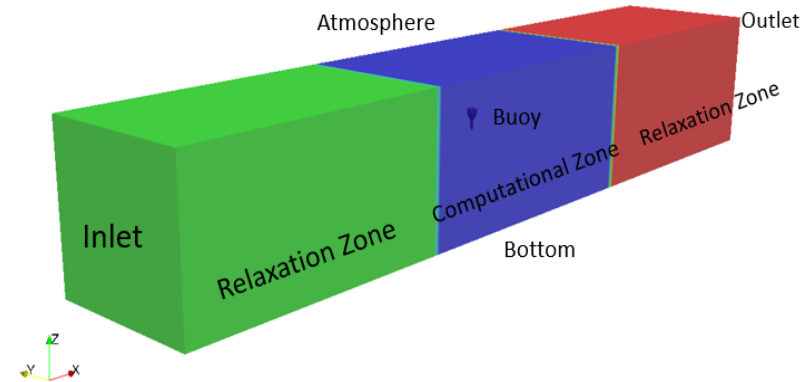
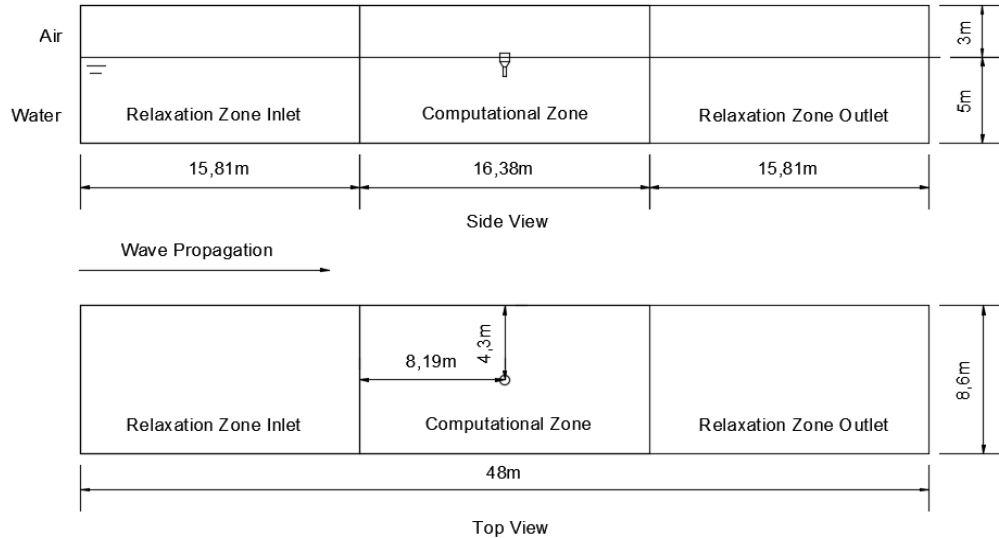
Method

- ⊗ URANS
- ⊗ VOF
- ⊗ NWT
- ⊗ Fluid to floating-body interaction

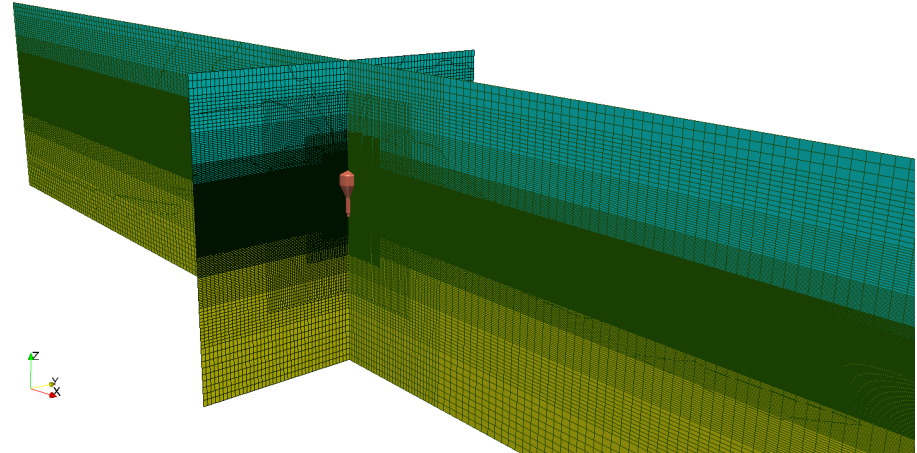
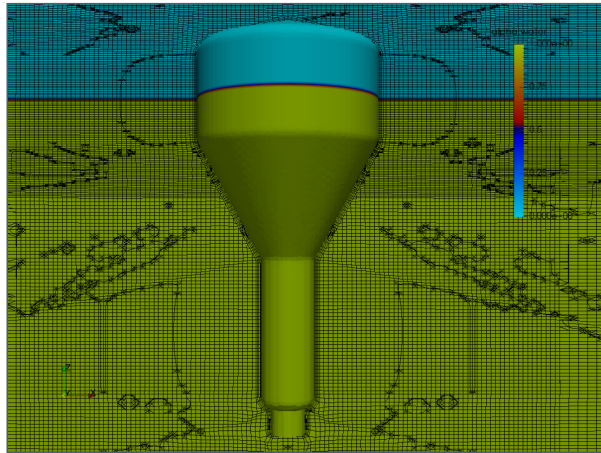
Solver

- ⊗ OpenFOAM package
- ⊗ Fluid domain – *interDyMFoam*
- ⊗ 6DOF - *sixDoFRigidBodyMotion*
- ⊗ Pre-tension mooring , PTO, WaveSpring – **in-house coding**
- ⊗ Wave generation – *waves2Foam*

Numerical settings - domain

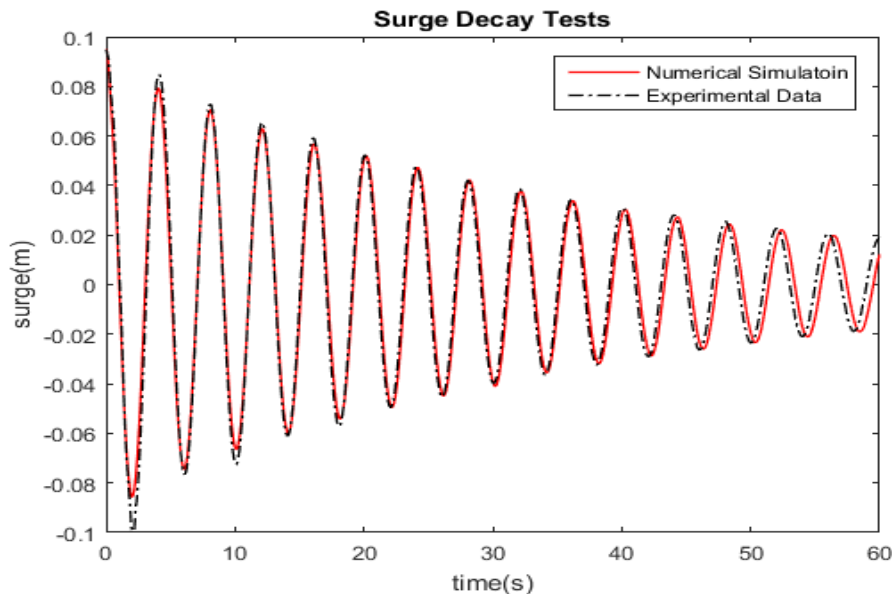


Numerical settings - grids



Surge Decay

- ⊗ 10M cells
- ⊗ Initial horizontal offset 0.1m
- ⊗ Linearized damping ratio
- ⊗ Average periods

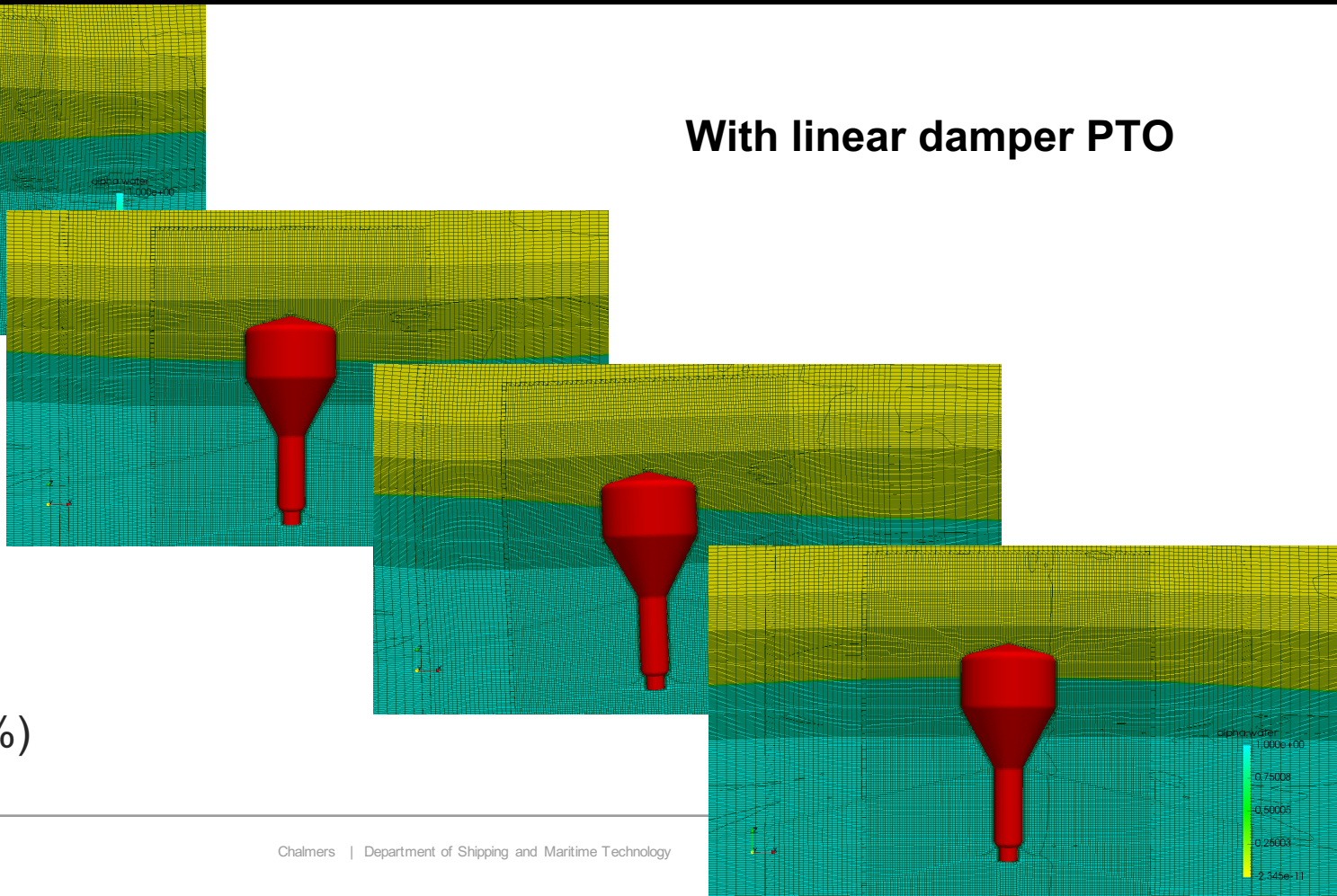


Results	Exp	CFD	Rel. error
Average period, T (s)	3.98	4.03	1.26%
Damping ratio	0.00955	0.0875	-8.32%

$$\delta = \frac{1}{N} \sum_{i=1}^N \frac{1}{t_{Trough,i} - t_{Peak,i}} \ln \frac{a_{Trough,i}}{a_{Peak,i}}$$

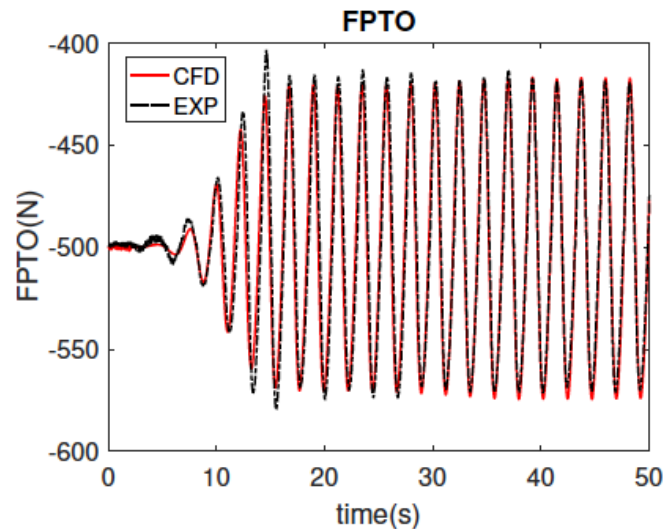
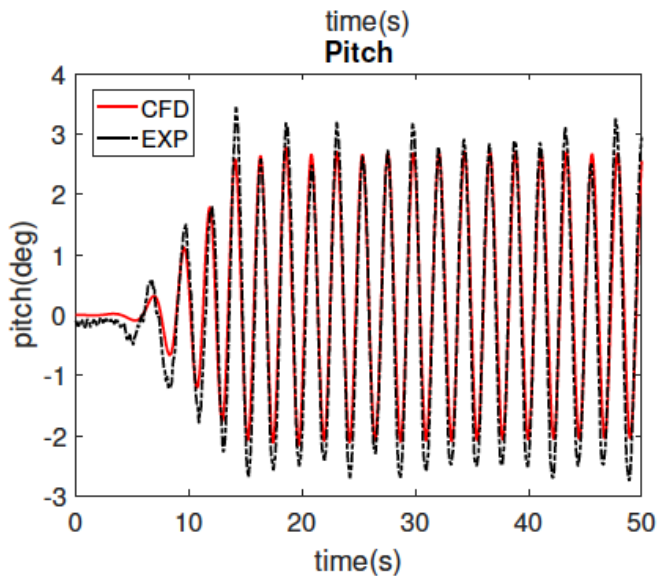
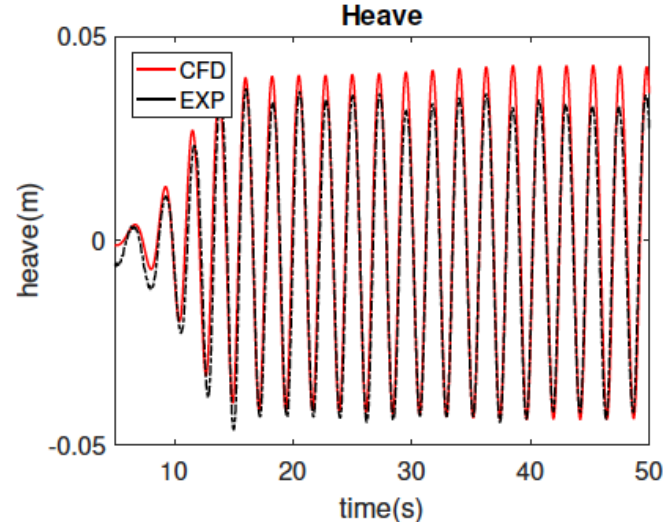
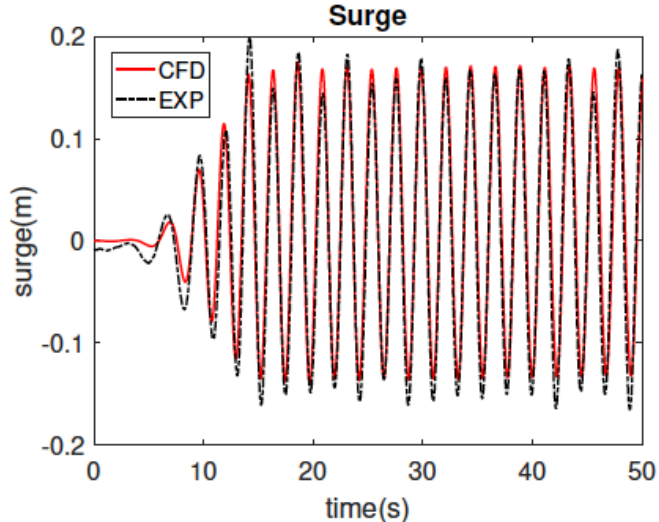
With linear damper PTO

- ⊗ 10M cells
- ⊗ Regular waves
 $T=2.25s$
 $H=15.6cm$
 $H/L=0.02$
- ⊗ Sensitive to pre-tension (3%)



PTO only

- 10M cells
- Regular waves
T=2.25s
H=15.6cm
H/L=0.02
- Sensitive to pre-tension (3%)



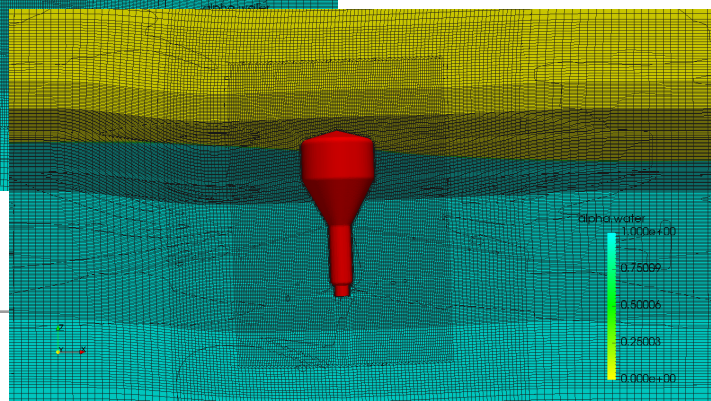
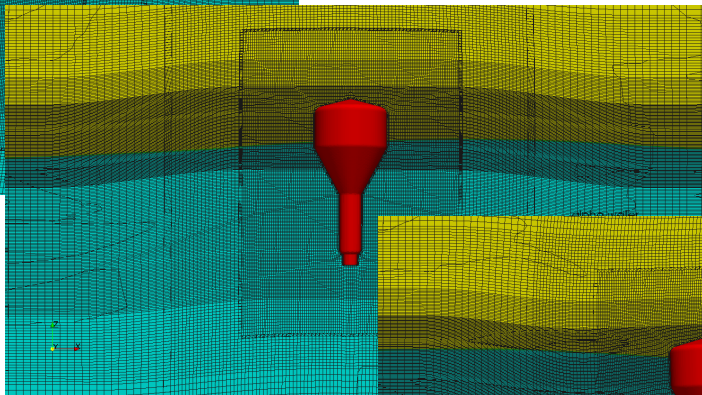
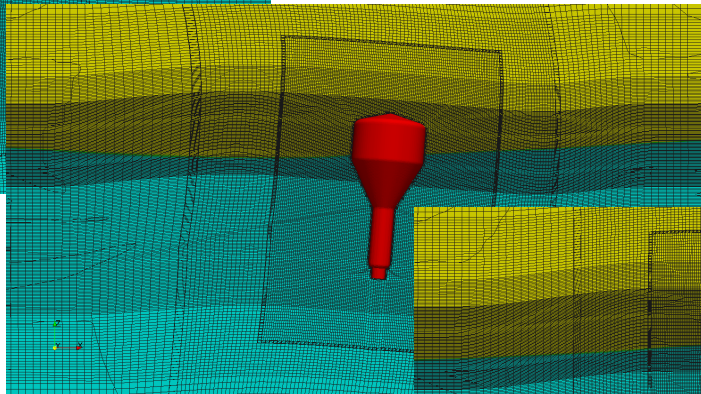
PTO only

Results (Average double amplitude)	Exp	CFD	Rel. error
Surge (m)	0.3206	0.3037	-5.271%
Heave (m)	0.0771	0.0850	10.246%
Pitch (deg)	5.4426	4.7536	-12.659%
PTO-mooring system force (N)	153.64	154.41	0.503%

Hals et al (EWTEC 2015)

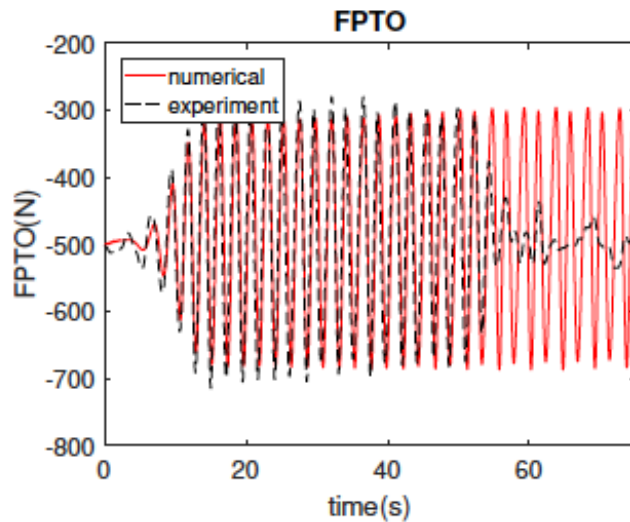
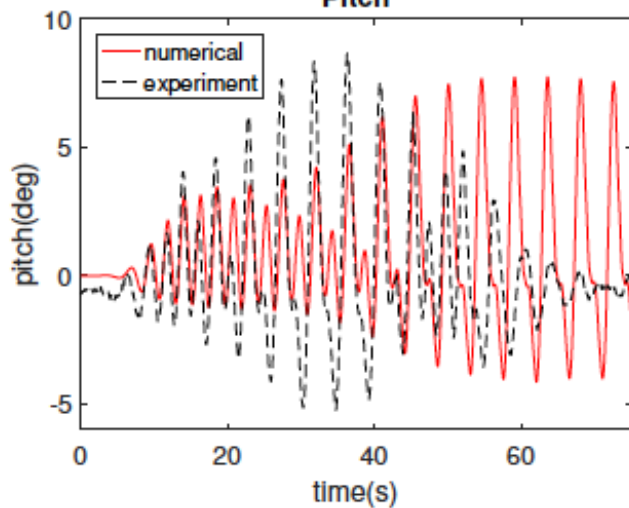
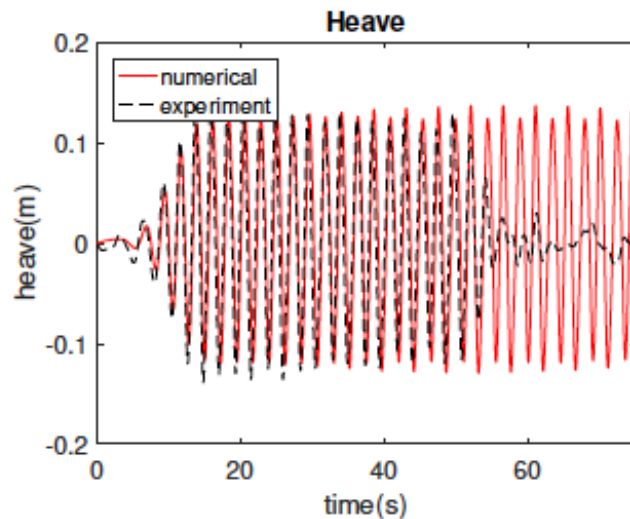
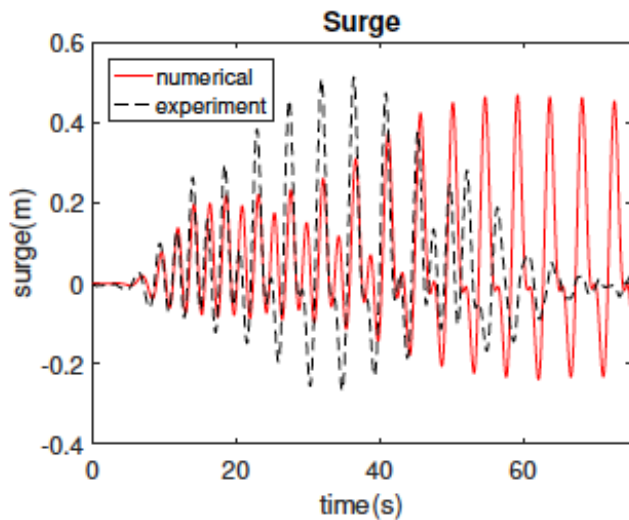
With WaveSpring and linear damper PTO

- ⊗ 10M cells
- ⊗ Regular waves
 $T=2.25s$
 $H=15.6cm$
 $H/L=0.02$
- ⊗ Sensitive to pre-tension (3%)

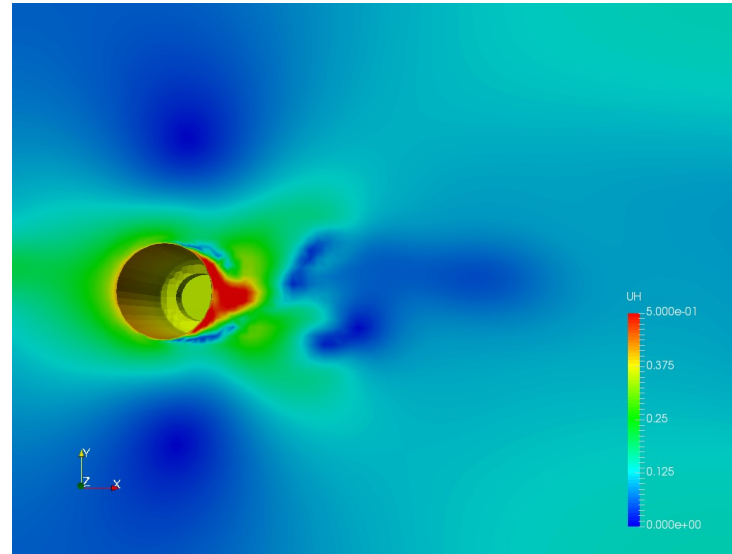
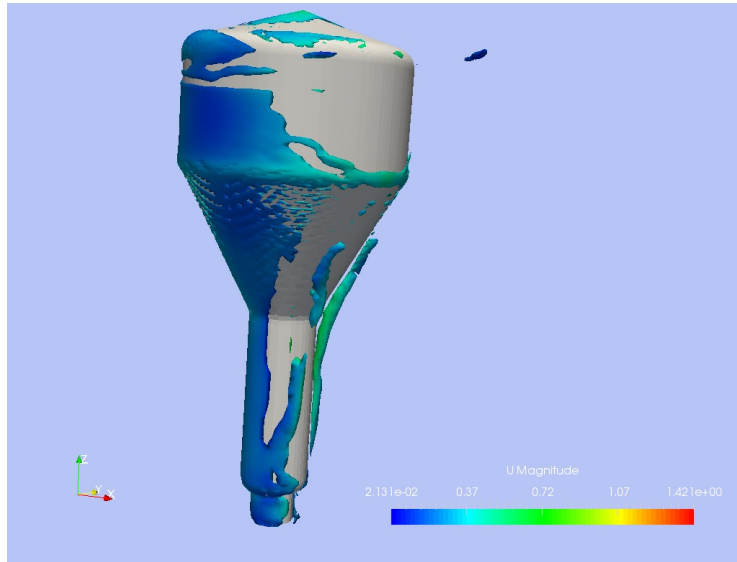


PTO+ WaveSpring

- ⊗ 10M cells
- ⊗ Regular waves
T=2.25s
H=15.6cm
H/L=0.02
- ⊗ Sensitive to
pre-tension (3%)



PTO+WaveSpring



PTO + WaveSpring

Results	Experimental	Numerical	Rel. error
Maximum amplitude			
Surge (m)	0.7800	0.7068	-9.385%
Pitch (deg)	13.88	11.88	-14.45%
Averaged double amplitude			
Heave (m)	0.2541	0.2486	-2.165%
PTO-mooring system force (N)	399.96	370.77	-7.298%
WaveSpring force, F_{WS} (N)	383.19	365.14	-4.710%

Hals et al (EWTEC 2015)

Verification & Validation

- ⊗ Numerical uncertainty (Eça & Hoekstra, JCP 2014)
 - ⊗ **Discretization error**
 - ⊗ **Iteration error**
- ⊗ Modelling error (turbulence - ongoing)
- ⊗ Geometry error (not performed)
- ⊗ Domain error (done - no influence of width)

Verification & Validation procedure

Case name	1M	3M	10M	20M
Level 0 cell size x, y (m)	0.48	0.33	0.215	0.175
Level 0 cell size z (m)	0.33	0.25	0.167	0.136
Grid number	1075404	3082530	10886096	19934406
Grid within wave height	15	20	30	37
Max. y+ from simulation	208	131	49.2	99.7

$$\varepsilon = \delta_{RE} = \phi_i - \phi_0 = ah^p$$

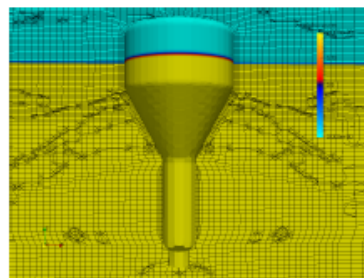
$$U_\phi = F_S |\varepsilon|$$

$$x_{bND} = x_b / H_0$$

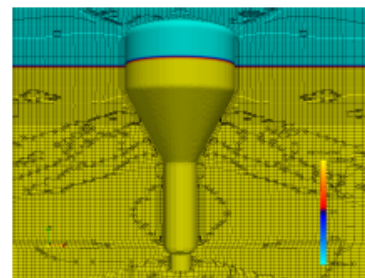
$$z_{bND} = z_b / H_0$$

$$\theta_{ND} = \theta / kH_0$$

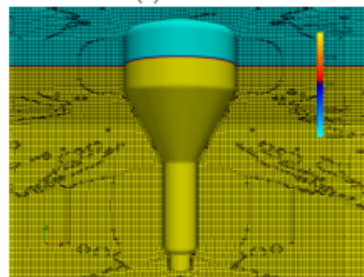
$$RF_{ND} = RF / \rho g H_0 S_w$$



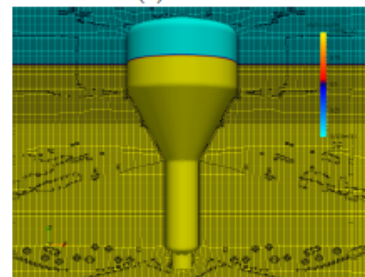
(a) 1M mesh



(b) 3M mesh



(c) 10M mesh

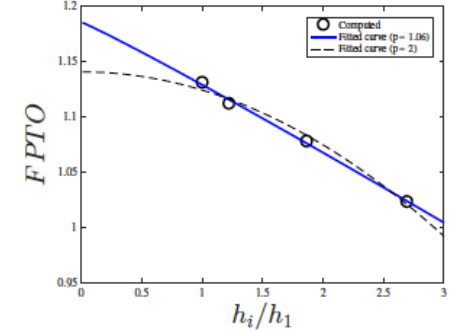
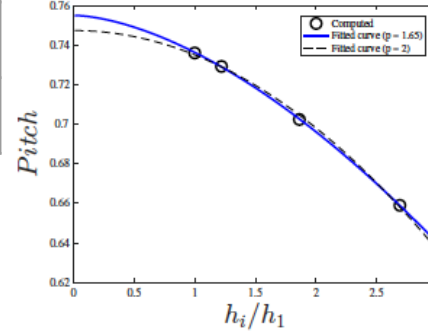
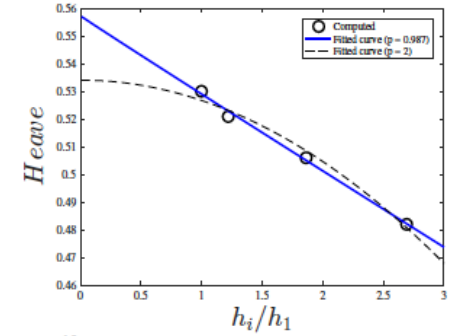
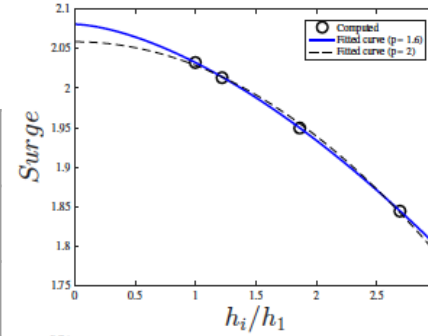


(d) 20M mesh

Figure 6: Different mesh configuration near the buoy

Discretization error

Uncertainty	Surge	Heave	Pitch	Res.Force
20M	6.14%	3.77%	2.37%	7.53%
10M	8.45%	4.54%	3.29%	9.21%
3M	16.49%	6.76%	6.56%	14.31%
1M	29.61%	9.61%	12.02%	20.65%



Iterative error

Uncertainty	Surge	Heave	Pitch	Res.Force
5 iterations	0.907%	0.425%	1.354%	0.661%
10 iterations	0.095%	0.023%	0.090%	0.043%

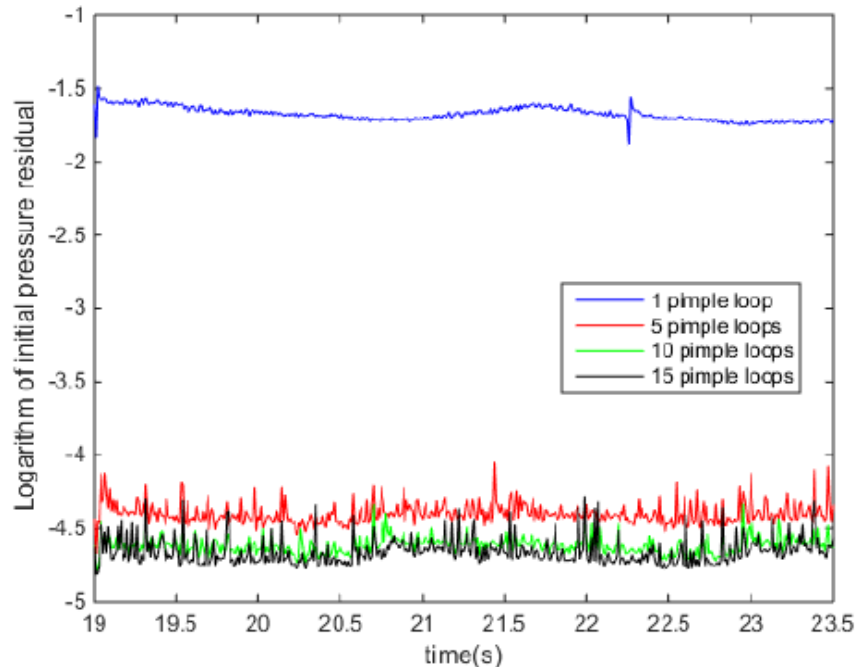


Figure 20: Initial pressure residual in the two periods

- ⊗ Should use 10 in order to keep iteration error two orders of magnitude lower than disc. error

Concluding remarks

- 1 The innovative design of CorPower is validated with CFD
- 2 The WaveSpring system is well represented in CFD simulation
- 3 The numerical study shows 5-10% uncertainty

Thanks for your attention!