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THE ROLE OF INTEGRAL EXPERIMENTS AND
NUCLEAR CROSS SECTION EVALUATIONS IN
SPACE NUCLEAR REACTOR DESIGN

David L. Moses

Richard D. McKnight

Oak Ridge National Laboratory*

Argonne National Laboratory

P.O. Box X

9700 S. Cass Avenue

Oak Ridge, TN 37831

Argonne, IL 60430

Commercial 615/574-6103
FTS 624-6103

Commercial 312/972-6088
FTS 972-6088

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Author running head: D. L. Moses and R. D. McKnight

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Address correspondence to: D. L. Moses

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David L. Moses
Oak Ridge National Laboratory
P.O. Box X
Oak Ridge, TN 37831
Commercial 615/574-6103
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Richard D. McKnight
Argonne National Laboratory
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Argonne, IL 60430
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FTS 972-6088

At the previous symposia on Space Nuclear Power Systems, two papers^{1,2} were presented which acknowledged the importance of the nuclear and neutronic properties of candidate space reactor materials to the design process, and two other papers^{3,4} were presented which acknowledged the importance of using benchmark reactor physics experiments to verify and qualify analytical tools used in design, safety and performance evaluation. However, there are regulatory/legal precedents which make the case for using neutronic benchmark experiments somewhat stronger than merely that of good design practice.

With the single exception of "space-based reactors", the Department of Energy (DOE) implementing orders^{5,6} stipulate that the program requirements for new ground-based reactors and presumably for pre-launch handling of space reactor units are to comply with the applicable federal regulations, specifically, the Code of Federal Regulations, Title 10, Part 50 (including subpart 50.34) and Part 100. Further, for all new reactors except the "space-based reactors," the safety analysis reports are required to follow the Nuclear Regulatory Commission's (NRC's) guidelines on the Standard Format and Content of Safety Analysis Reports.⁷⁻⁹ Space-based reactors are to use "criteria consistent with space applications" (Ref. 5); however, the DOE policy statement¹⁰ on these criteria merely directs the reactor system contractor to use as appropriate those documents referenced in the DOE implementing order⁵ and to include a section on the nuclear design in the safety analysis report. As indicated above, the documents cited in the DOE order⁵ are the current NRC guidelines for safety analysis documentation. The NRC guidelines (specifically, Section 4.3 of Refs. 7, 8 and 9) are explicit with regard to documenting the use of reactor physics experimental data, including critical experiments, to establish the accuracy and uncertainty in the prediction of power distributions, reactivity coefficients, shutdown margins, control worths, and subcriticality during fuel handling. These reactor physics parameters plus core lifetime are also expected to be issues in establishing "criteria consistent with space applications," and so the existing quality assurance guidance for demonstrating and documenting the safety and nuclear design performance of ground-based reactors is expected to be equally applicable to space-based reactors.

Since June 1966, the Cross Section Evaluation Working Group (CSEWG) has acted as an interagency forum for the assessment and evaluation of nuclear

reaction data used in the nuclear design process.¹¹ Although CSEWG activities are not meant to support the specific safety analyses of particular reactor plants, CSEWG does direct a nuclear data testing program which quantifies the accuracy and uncertainty of nuclear data for those materials which are of most interest to the nuclear industry. Under project funding from the DOE, the CSEWG data testing has involved the specification¹² and calculation¹³ of benchmark experiments for fast reactor criticality and reaction rate data, thermal reactor criticality and reaction rate data, shielding and dosimetry. The calculations of the benchmark experiments have been made by participants from industry and the national laboratories employing the data processing methods and core analysis tools which are used widely for commercial reactor design and safety analysis. Therefore, the results of such testing can be used where appropriate in making the safety case as required by the regulations and NRC guidelines. The specification of the fast reactor benchmark experiments preceded the issuance of the industry standards^{14,15} for acceptance and use of "reference data", but the CSEWG benchmarks exceed the minimum acceptance criteria for such data.

The current set of CSEWG fast reactor benchmarks were developed to support the breeder reactor program. As such, the major constituent materials of the critical experiments are not the same as those anticipated for space reactor core application. There are minor constituents of molybdenum and carbon in a few of the critical experiments, and boron-10 has been extensively examined as a control poison. However, a number of the candidate structural materials for space reactors have been subjected to central worth measurements. The state of the art for predicting central worth for these materials is reflected in Table 1. The data presented in Table 1 represent a single set of calculations by Los Alamos National Laboratory using ENDF/B-V nuclear data.¹⁶ Problems experienced in accurately calculating the central worths have been addressed by studies at Argonne National Laboratory.^{17,18} These problems center on the inability of the analytical methods to simulate the precise configuration in which the experiment is performed. Some experiments, such as BIG TEN, have been found to employ techniques that minimize the calculation-to-experiment error observed in the worth of small, heavy metal samples; however, as shown in Table 1, this observation does not apply to lighter materials for which neutron scattering is the important effect.

Thus, although the current CSEWG benchmarks provide a place to start in assuring the accuracy and uncertainty of nuclear data important to space reactor applications, there need to be developed better benchmarks to quantify the accuracy and uncertainty of the differential and integral data. CSEWG is aware of the numerous critical experiments performed in support of space reactor programs during the 1960s and early 1970s, and the authors have compiled an extensive library of these data sources. Further effort will be required to develop from these a set of benchmarks consistent with the basis for the CSEWG benchmark specifications¹² and industry standards for reference data.^{14,15} The development of such benchmarks and the subsequent data testing will require interagency support and participation in order to be useful and effective. New experiments are most certainly required to meet the regulatory guidelines for the safety analysis of specific reactor concepts. CSEWG's role is to support industry in making the most effective use of existing and new data sources so as to minimize

the cost and time involved in the design effort and licensing-equivalent certification.

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Table 1. LANL ENDF/B-V Calculation-to-Experiment Ratios for Selected Central Worth Measurements in CSEWG Benchmarks

| CSEWG Fast Reactor Benchmark Number/Name | H-1 | Li | Li-6 | Li-7 | Be | B | B-10 | C | O-16 | Zr | Mn-55 | Mn | Ne | Ta-181 | V | U 235 | U 238 |
|---|--------|--------|---------------------|--------|--------|--------|---------------------|--------|--------|---------|---------------------|---------|--------|---------|--------|--------|--------|
| 1 JSZEBEL | 0.0621 | | | | 1.0133 | | 0.9968 | 1.1618 | 1.1134 | 0.7835 | 1.1791 ^a | 1.0840 | | 1.1080 | 1.0590 | 1.0712 | 0.9637 |
| 3 ZPR-3/48 | | | | | | | 1.0407 | 5.9277 | | | | 1.1664 | | 1.0373 | | 1.1533 | 1.1663 |
| 6 ZEBRA-3 | 1.5749 | 0.9062 | | | | 1.3755 | 0.9678 | | | | | | | -1.0755 | | 1.1466 | 1.0785 |
| 5 COOIVA | 0.9853 | | | | 0.9854 | | 0.8365 | 0.5273 | | | 0.9850 ^a | | | | | 0.9799 | 1.0028 |
| 4 VERA-18 | 1.0748 | | | | | | | | | | | | | | | 1.0076 | 1.5535 |
| 7 ZPR-3/6F | 0.6388 | | | | 1.0731 | | 0.9659 | 0.7466 | | 19.1516 | 1.1658 | -1.4212 | 1.4778 | 1.1330 | | 0.8800 | 2.9267 |
| 8 ZPR- | | | | | | | 0.9308 | 1.6832 | 1.2867 | | | 1.2699 | | 0.9754 | | 1.1101 | 1.0094 |
| 9 ZPR- | | | | | | | | 0.7582 | | | 1.1075 | 1.1661 | | 1.0178 | | 2.9885 | 0.9337 |
| 10 ZEBRA-7 | 1.0495 | 0.6435 | 0.8330 | | | 0.6027 | 0.8730 | 0.5967 | | | | | | 1.1778 | 1.7527 | 1.0927 | 1.0337 |
| 12 ZPR-2 | | | | | | | 0.9648 | 1.3331 | | | 1.2815 | 1.1275 | | 0.8715 | 1.4355 | | |
| 12 ZPR-6/7 | | | | | | | 1.2175 | 1.5505 | | | | 1.3167 | | 1.4653 | | 1.1157 | 1.0388 |
| 13 ZPR-1/5A | | | | | | | 0.8957 | 1.8523 | | | | | | 0.9738 | | 1.0587 | 1.1687 |
| 15 ZPR-4/6A | | | | | | | 0.9436 | 0.8116 | | | | | | 1.7377 | | 1.1191 | 1.1739 |
| 16 SREX-7A | | | | | | | 0.9024 | | | | | | | 0.6633 | | 1.0176 | 1.0898 |
| 17 SREX-7B | | | | | | | 0.8982 | | | | | | | 0.7967 | | 1.0185 | 1.0361 |
| 18 ZPR-9/31 | | | 1.1165 | | | | 1.0287 | 2.3430 | | | | | | | | 1.1413 | 1.0308 |
| 20 SIC T6W | 1.0933 | | 0.9186 | 1.3112 | 1.4409 | | 0.9099 | 1.3682 | 1.4830 | | | | | | | 1.0127 | 1.0191 |
| 20 SIC T6H | | | 0.8956 ^a | | | | 0.8643 ^a | | | | | | | | | | |

^a Central Section Rate Ratios Normalized to U-235 Fission.