
INGEN: A COBRA-NC Input Generator User's Manual

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ABSTRACT

The INGEN (INput GENERator) computer program has been developed as a preprocessor to simplify input generation for the COBRA-NC computer program. INGEN uses several empirical correlations and geometric assumptions to simplify the data input requirements for the COBRA-NC computer code. The simplified input scheme is obtained at the expense of much flexibility provided by COBRA-NC. For more complex problems requiring additional flexibility however, INGEN may be used to provide a skeletal input file to which the more detailed input may be added. This report describes the input requirements for INGEN and describes the algorithms and correlations used to generate the COBRA-NC input.

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SUMMARY

INGEN is a computer program that functions as an input generator for the **COBRA-NC** computer code. A relatively simple data input scheme is employed to describe a desired simulation. Several empirical correlations and geometric assumptions are then used to generate input for **COBRA-NC**.

The simplified data input scheme reduces the model flexibility provided by **COBRA-NC** and therefore **INGEN** is best suited to simple problems or when scoping calculations are required. **INGEN** may also be used to generate a skeletal **COBRA-NC** input deck which may be expanded using a text editor.

This report describes the input requirements for **INGEN** and presents the correlations and assumptions used in creating the **COBRA-NC** input. Also, several enhancements to the **COBRA-NC** code that were accomplished during the development of **INGEN** are described. Finally, a high energy line break analysis is presented as an example demonstrating the utility of **INGEN**,

1.0 INTRODUCTION

The COBRA-NC computer program is under development at PNL to provide a tool for modeling the time varying properties of mixtures of steam and noncondensable gases (Thurgood 1968). The program may be used to predict energy and species distribution in a compartment during large or small steam line break accidents. The code provides a two-fluid, three-field representation of two-phase flow, treating each field in three dimensions using compressible flow equations. The three fields are continuous gas, continuous liquid and entrained liquid. The continuous gas field is composed of steam vapor and up to 10 species of noncondensable gases.

COBRA-NC solves the conservation equations for continuous gas, continuous liquid, and entrained liquid fields using a semi-implicit finite-difference numerical technique on an Eulerian field. The same numerical technique is used to calculate heat transfer from and within the solid structures in contact with the fluid. This code features extremely flexible noding for both the hydrodynamic and transport solutions. This flexibility enables modeling of the wide variety of geometries encountered at nuclear reactor facilities. The high degree of flexibility and the diverse types of problems which can be analyzed, requires a very detailed model specification in the COBRA-NC input.

A simplified input scheme may be appropriate, especially for models which contain only a few rooms or for which upper-bound scoping calculations are desired. To aid the user in setting up scoping calculations, an input generator called INGEN was written. The input to INGEN consists of a simplified description of the desired geometry, selection of a few desired options, and the specification of initial and boundary conditions. The INGEN routine fleshes out this skeletal input using general assumptions about volume and area relationships, defaulted wall thicknesses, and various correlations. It then produces an output file which may be used as a COBRA-NC input file. The output file generated by INGEN can be used directly by COBRA-NC, or, for problems in which the defaulted values used by INGEN are insufficient, the file generated by INGEN can serve as a foundation to which the more specific COBRA-NC input can be incorporated.

2.0 GENERAL CONSIDERATIONS AND DEFINITIONS

The input required by INGEN is much simpler than that of COBRA-NC. However, this simplification was gained by reducing the flexibility which exists in COBRA-NC. In this section the rules and assumptions which govern the conversion of INGEN input to COBRA-NC input are discussed.

2.1 GEOMETRY

Two general types of geometry are required as input into COBRA-NC, the hydrodynamic geometry and the heat transfer geometry. The hydrodynamic input for a COBRA-NC computational cell consists of a vertical flow channel with flow area AN, a wetted perimeter PW, and an axial height DX. These cells are connected in the transverse plane by gaps having a width GAPN and a height DX. For momentum purposes, the length of the connection between transverse cells is LENGTH. In addition, areas for axial momentum calculations, defined as ABOT and ATOP, may be specified when the area connecting cells in the vertical direction is different from the continuity cell flow area.

The geometry input to INGEN includes the number of floors to be modeled, NFLOOR; the height of each floor, DX; the area or volume of each cell, A; the cell wall perimeters, P; and the flow areas between cells, AP. Table 1 shows the corresponding variable definitions used in COBRA-NC and INGEN.

TABLE 1. COBRA-NC and INGEN Variable Definitions

Variable Definition	COBRA-NC	INGEN
Vertical Flow Area	AN(I)	A(I)
Wetted Perimeter	PW(I)	P(I)
Axial Height	DX(I)	DX(I)
Axial Momentum Area (Upper)	ATOP(K,I)	AP(K,I) (a)
Axial Momentum Area (Lower)	ABOT(K,I)	AP(K,I) (b)
Gap Width	GAP(I)	AP(K,I) / DX(I)
Transverse Momentum Length	LENGTH(I)	(P(J)+P(K)) / 8.0 ^(c)

(a) Kth junction at top of cell ■

(b) Kth junction at bottom of cell ■

(c) For gap ■ connecting cells J and K

2.1.1 Loss Coefficient

Loss coefficients and friction multipliers are also required input for COBRA-NC. For intra-room junctions, INGEN sets the local loss coefficient to zero. For room-to-room connections the loss coefficient is estimated using a curve fit of the thick-walled orifice curve of Idel'chik^(a) (Idel'Chik, 1966). In making the estimation it is assumed that form losses dominate (i.e., friction losses may be ignored), that the walls between rooms are 2-ft thick, and that the hydraulic diameter may be approximated by

$$D_H = \left(\frac{4AP}{\pi}\right)^{1/2}$$

The correlating parameter used by Idel'chik to characterize the form loss coefficient is the ratio of orifice thickness to hydraulic diameter:

$$\zeta = f(L/D_H)$$

Idel'chik gives the local form loss coefficient in both tabular and graphical form. The analytical expression used in INGEN to approximate the tabular function is

$$\zeta = \alpha F1 (L/D_H) + (1-\alpha) F2 (L/D_H)$$

where

$$\alpha = \begin{cases} 0.5 & \leq 1.3 \\ 1.0 & \text{when } L/D_H > 1.3 \end{cases}$$

$$F1 = 2.204 - 0.44 \tan^{-1} (9.556((L/D_H) - 0.6656))$$

$$F2 = 2.826 - 0.943 L/D_H$$

Loss coefficients for both vertical and transverse junctions are calculated using this correlation. For connections in the transverse direction, a friction multiplier term, FWALL(K), may also be input to COBRA-NC. INGEN defaults this term to 2.0 for all room-to-room and intra-room connections. This value is most appropriate for rooms that are square in the transverse direction.

(a) Assumes rooms are square with no internal walls when estimating momentum length.

2.1.2 Wall Heat Transfer Model

COBRA-NC parameters pertinent to the wall heat transfer model are the wall thickness, the outside and inside perimeters, and a multiplication factor which can be used to modify the effective heat transfer surface area. The general assumptions used by INGEN are:

- The wall is adiabatic on the outside.
- There are two wall types per hydrodynamic cell. The first wall type represents concrete walls and has a thickness of 2 ft. The second represents steel components and has a thickness of 0.5 in.
- Each wall is homogeneous with respect to material type.

Since the outside surface is assumed to be adiabatic, the outside heated perimeter is set to zero. The inside heated perimeter is estimated by the following expression

$$HPERMI(I) = (2A(I) - \sum AP(I,K))/DX(L) + P(I)$$

The heated perimeter, therefore, is set equal to the cell wetted perimeter plus the floor and ceiling surfaces minus any flow passages. The properties assumed for the two wall types are given in Table 2.

TABLE 2. INGEN Default Wall Type

<u>Property</u>	<u>Type 1</u>	<u>Type 2</u>
Material	Concrete	Steel
Cp(Btu/lbm°F)	0.22	0.113
ρ (lbm/ft ³)	139	487
k(Btu/hr-ft-°F)	0.867	30
Thickness (ft)	2	0.0417

Multiplying factors are used to specify the fraction of the total wall area made up of each wall type. INGEN normally defaults the perimeter multiplying factor to 1.0 for the concrete walls and to 0.0 for steel walls. When the

multiplier is 0.0, COBRA-NC input for the wall is not generated as the wall is assumed to be nonexistent. The use of the multiplying factor to add or delete walls from the model is discussed further in the input description.

2.2 INITIAL AND BOUNDARY SPECIFICATIONS

Initial conditions specifying cell values for pressure, vapor and liquid enthalpy, vapor and liquid void fraction, and the partial pressure and enthalpy of the air initially in the building are required by COBRA-NC. The input to INGEN is limited to total pressure, atmospheric temperature, and atmospheric relative humidity. For initialization purposes, it is assumed that the pressure is uniform throughout the building and that the air and vapor are in thermal equilibrium. The saturation pressure at atmospheric temperature is calculated using the correlation from the ASME 1967 steam table (ASME Steam Tables, 1967):

$$\beta_K(\theta) = \exp \left[\frac{1}{\theta} \frac{\sum_{v=1}^5 k_v (1-\theta)^v}{1 + k_6(1-\theta) + k_7(1-\theta)^2} - \frac{(1-\theta)}{k_8(1-\theta)^2 + k_9} \right]$$

where $\beta = P_{\text{sat}}/3207.4$

P_{sat} = saturation pressure at T_{atm} (psia)

$\theta = T_{\text{atm}}(^{\circ}\text{K})/647.3$

$k_1 = -7.691234564$

$k_6 = 4.167117320$

$k_2 = -2.608023696\text{E}+1$

$k_7 = 2.097506760\text{E}+1$

$k_3 = -1.681706546\text{E}+2$

$k_8 = 1.\text{E}+9$

$k_4 = 6.423285504\text{E}+1$

$k_9 = 6.$

$k_5 = -1.189646225\text{E}+2$

The pressure of the vapor is calculated from:

$$P_v = \max(0.11, P_{\text{sat}} * \Psi)$$

where Ψ = relative humidity of the atmosphere.

The initial liquid volume fraction in the building is assumed to be negligible, and is therefore set to

$$\alpha_L = 0.000001$$

The vapor and gas volume fraction are calculated using Amagat's law of additive volumes for an ideal gas and the definition of relative humidity. INGEN calculates these volume fractions from

$$a_v = \text{vapor volume fraction} = P_v / P_{\text{atm}}$$

$$a_g = \text{air volume fraction} = 1 - a_v - a_L$$

Steam enthalpy, compatible with the values of relative humidity and temperature, is calculated using the correlation given by Keenan and Keyes (Keenan and Keyes 1936)

$$h = f(P, T)$$

$$= F_0(14.696P) + \frac{F_1}{2} (14.696P)^2 + \frac{F_3}{4} (14.696P)^4 + \frac{F_{12}}{13} (14.696P)^{13} + F'$$

F_0 , F_1 , F_3 and F_{12} are defined as follows.

$$F_k = \frac{\partial}{\partial \tau} (B_k \tau) , k = 0, 1, 3, 12$$

where:

$$\tau = 1.8/T$$

$$B_0 = 1.89 - 2641.62 \tau - 10^{80870} \tau^2$$

$$B_1 = B_0^2 (82.546 \tau^2 - 1.6246(10)^5 \tau^3)$$

$$B_3 = B_0^4 (0.21828 \tau^3 - 1.2697(10)^5 \tau^5)$$

$$B_{12} = -B_0^{13} (3.635(10)^{-4} \tau^{12} - 6.768(10)^{64} \tau^{36})$$

The function F' is given by

$$F' = \int_{491.69}^T C_{p_o} dT + 1075.90$$

with

$$C_{p_o} = 0.3516 + 1.0028(10)^{-4}T + 11.427\tau$$

T is in $^{\circ}R$, P is in psia, h is in Btu/lbm, and C_{p_o} is in Btu/lbm $^{\circ}R$

Values for superheated vapor temperature are computed as functions of pressure and enthalpy using an iterative method described by McClintock and Silvestri (McClintock and Silvestri 1968). First, estimates for T and C_p are estimated using

$$T = A_1 + A_2h + A_3h^2 + A_4h^3 + A_5P + A_6P^2$$

$$+ A_7P^3 + P(A_8h + A_9h^2 + A_{10}h^3)$$

$$1/C_p = B_1 + B_2h + B_3h^2 + B_4h^3 + B_5 \ln P + B_6(\ln P)^2$$

$$+ B_7(\ln P)^3 + (\ln P) (B_8h + B_9h^2 + B_{10}h^3)$$

where T is in $^{\circ}F$, P is in psia, h is in Btu/lbm, and C_p is in Btu/lbm- $^{\circ}F$.
When $P \leq 1000$ psia, or $P > 1000$ psia and $h \geq 1280$ Btu/lbm, the constants are

$A_1 = -1.0659659E+4$	$A_6 = -7.7618225E-6$
$A_2 = 2.0110905E+1$	$A_7 = 2.4391612E-10$
$A_3 = -1.250954E-2$	$A_8 = -9.8147341E-3$
$A_4 = 2.8274992E-6$	$A_9 = 6.5824890E-6$
$A_5 = 4.9815820$	$A_{10} = -1.4749938E-9$

$$\begin{array}{ll}
B_1 = -2.8557816 & B_6 = -3.6261637E-2 \\
B_2 = 1.3250230E-2 & B_7 = 7.3529479E-4 \\
B_3 = -1.0521514E-5 & B_8 = 5.7703098E-3 \\
B_4 = 2.5007955E-9 & B_9 = -2.9972073E-6 \\
B_5 = -3.4620214 & B_{10} = 5.2037300E-10
\end{array}$$

When $P > 1000$ psia and $h < 1280$ Btu/lbm, the constants are given by

$$\begin{array}{ll}
A_1 = -4.5298646E+3 & A_6 = -9.1654905E-6 \\
A_2 = 1.5358850E+1 & A_7 = 2.7549766E-10 \\
A_3 = -1.5655537E-2 & A_8 = -1.1541553E-3 \\
A_4 = 5.2687849E-6 & A_9 = 1.2384560E-6 \\
A_5 = 4.4185386E-10 & A_{10} = -4.1724604E-10 \\
B_1 = 1.2659960E+2 & B_6 = 1.3424036 \\
B_2 = -2.5611614E-1 & B_7 = -4.9110372E-2 \\
B_3 = 2.2270593E-4 & B_8 = 2.7966370E-2 \\
B_4 = -5.9928922E-8 & B_9 = -2.4665012E-5 \\
B_5 = -2.1818030E+1 & B_{10} = 6.7723080E-9
\end{array}$$

The estimated temperature is then used to compute an approximate enthalpy from

$$h' = f(P, T)$$

where the function $f(P, T)$ is that of Keenan and Keyes given above. Next, a temperature correction, AT , is computed from

$$AT = (1/C_p) (h - h')$$

and the new estimated temperature becomes

$$T' = T + \Delta T$$

A new approximate enthalpy, h'' , is computed using this temperature in the function $h = f(P, T)$ and the iteration is continued until $(h - h'') < 0.5$ Btu/lbm. Iteration is not used in the specific heat calculation. The C_p value given previously is taken as the final value. Liquid and vapor specific volumes as functions of pressure and enthalpy are computed using equations from Agee (1977). For the vapor

$$v = E_1 + E_2 P + E_3/P + E_4 h + E_5 P h + E_6 h/P$$

and for the liquid

$$v = \exp \left\{ \sum_{k=0}^4 \sum_{n=0}^2 C_{k,n} P^n h^k \right\}$$

where P is in psia, h is in Btu/lbm, and v is in ft^3/lbm . The constants for these equations are

$$\begin{array}{ll} E_1 = -0.81735849E-3 & E_4 = -0.62941689E-5 \\ E_2 = 0.12378514E-4 & E_5 = -0.87292160E-8 \\ E_3 = -0.10339904E+4 & E_6 = 0.12460225E+1 \end{array}$$

$$\begin{array}{lll} C_{0,0} = -0.41345E+1 & C_{0,1} = -0.59428E-5 & C_{0,2} = 0.15681E-8 \\ C_{1,0} = 0.13252E-4 & C_{1,1} = 0.63377E-7 & C_{1,2} = -0.40711E-10 \\ C_{2,0} = 0.15812E-5 & C_{2,1} = -0.39974E-9 & C_{2,2} = 0.25401E-12 \\ C_{3,0} = -0.21959E-8 & C_{3,1} = 0.69391E-12 & C_{3,2} = -0.52372E-15 \\ C_{4,0} = 0.21683E-11 & C_{4,1} = -0.36159E-15 & C_{4,2} = 0.32503E-18 \end{array}$$

Saturation enthalpies are calculated using EPRI curve fits (McFadden et al. 1980) defined by the following function:

$$h_f = \begin{cases} \sum_{i=0}^8 a_1 (\ln(P))^i & \text{if } 0.1 < P \leq 950 \text{ psia} \\ \sum_{i=0}^8 a_2 (\ln(P))^i & \text{if } 950 < P \leq 2550 \\ \sum_{i=0}^8 a_3 ((P_{\text{crit}} - P)^{.41})^i & \text{if } 2550 < P \leq P_{\text{crit}} \end{cases}$$

and

$$h_g = \begin{cases} \sum_{i=0}^{11} b_1 (\ln(P))^i & \text{if } 0.1 < P \leq 1500 \text{ psia} \\ \sum_{i=0}^8 b_2 (\ln(P))^i & \text{if } 1500 < P \leq 2650 \\ \sum_{i=0}^6 b_3 ((P_{\text{crit}} - P)^{.41})^i & \text{if } 2650 < P \leq P_{\text{crit}} \end{cases}$$

The coefficients for the saturation enthalpy equations are:

<u>i</u>	<u>a₁</u>	<u>a₂</u>	<u>a₃</u>
0	.6970887859 E+2	.8408618802 E+6	.9070030436 E+3
1	.3337529994 E+2	.3637413208 E+6	-.1426813520 E+2
2	.2318240735 E+1	-.4634506669 E+6	.1522233257 E+1
3	.1840599513 E+0	.1130306339 E+6	-.6973992961 E+0
4	-.5245502284 E-2	-.4350217298 E+3	.1743091663 E+0
5	.2878007027 E-2	-.3898988188 E+4	-.2319717696 E-1
6	.1753652324 E-2	.6697399434 E+3	.1694019149 E-2
7	-.4334859629 E-3	-.4730726377 E+2	-.6454771710 E-4
8	.3325699282 E-4	.1265125057 E+1	.1003003098 E-5

<u>i</u>	<u>b₁</u>	<u>b₂</u>	<u>b₃</u>
0	.1105836875 E+4	-.2234264997 E+7	.9059978254 E+3
1	.1436943768 E+2	.1231247634 E+7	.5561957539 E+1
2	.8018288621 E+0	-.1978847871 E+6	.3434189609 E+1
3	.1617232913 E-1	.1859988044 E+2	-.6406390628 E+0
4	-.1501147505 E-2	-.2765701318 E+1	.5918579484 E-1
5	.0000000000 E+0	.1036033878 E+4	-.2725378570 E-2
6	.0000000000 E+0	-.2143423131 E+3	.5006336938 E-4
7	.0000000000 E+0	.1690507762 E+2	
8	.0000000000 E+0	-.4864322134 E+0	
9	-.1237675562 E-4		
10	.3004773304 E-5		
11	-.2062390734 E-6		

Air enthalpy is calculated assuming constant specific heat, from

$$h_{air} = 126.66 + 24 * (T_{atm} - 70.3) \text{ [Btu/lbm]}$$

COBRA-NC requires a reference pressure for the top cell of the model. A gravitational head based on the total height of the system being modeled is calculated by INGEN. This pressure head is subtracted from the initial pressure specified for INGEN to give the desired COBRA-NC reference pressure. This calculation affects only the value of the reference pressure as input to COBRA and is transparent to the user when he specifies the desired initial pressure in the INGEN input.

3.0 INGEN INPUT INSTRUCTIONS

This section describes the format and content of the INGEN input. An asterisk, "*", following the format specification indicates the card is required in the input stream and a double asterisk, "**", indicates the card is required but may be blank. If there is no asterisk following the format specification the card may be omitted.

1. Title Card: Format (17A4)**

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-64	TITLE	Alphanumeric job title

2. Operation Parameter Card: Format (2110, F10.3)

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-10	NBOUND	Number of boundary specifications to be supplied. Each boundary specification defines a location where flow enters or leaves the calculation domain. Inflow from pipe breaks and vents to the atmosphere require boundary specifications.
11-20	MCRIT	Critical flow parameter. Valid entries are: Blank = no critical flow calculation 1 = Moody critical flow model 2 = Henry-Fauske subcooled (extended) model 3 = Henry-Fauske (original) model
21-30	TOTTRN	Total simulation time for transient (sec)

3. Restart Data: Format (110, F10.3)**

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-10	IDSTEP	Time step number of dump to be used for restarting.
10-20	TIMET	Restart time for problem (seconds).

For normal runs (no restart) Card 3 is input as a blank card.

4. Containment Initialization Card: Format (3F10.2)**

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
0-10	PATM	Initial pressure in containment building (psia) .
11-20	TATM	Initial temperature in containment building (°F)
21-30	RHUMID	Initial relative humidity

The above variables will take on default values of 14.696 psia, 92°F, and 0.5 respectively if their field is left blank. A blank card must be supplied if default values are desired.

5. Geometry Input Group

5a. Format (3I10)*

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-10	NFLOOR	Number of floors to be modeled.
11-20	NCRITC	Number of axial junctions to be checked for critical flow
21-30	NCRITK	Number of transverse junctions to be checked for critical flow

Cards 5b and 5c are read in sets. Card 5b is read NFLOOR times (where NFLOOR is specified on card 5a) and each card 5b is immediately followed by NCELL(L) of card 5c (where NCELL(L) is specified on card 5b).

5b. Format (110, F10.3, 2I10)*

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-10	NCELL(L)	Number of cells on Lth floor.
11-20	DX(L)	Height of Lth floor (ft).
21-30	NODESF(L)	Number of axial nodes on the Lth floor
31-40	IAORV	Flag to select volume or input to variable A(I) of card 5c. If IAORV is not blank (or zero) then when reading card 5c the cell area will be set to A(I)/DX.

5c. Format (I5,2F5.0,6(I5,F5.0))*

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-5	I	Cell designation number
6-10	A(I)	Floor area of cell (ft ²), or cell volume (ft ³), if depending on flag IORV of card 5b.
11-15	P(I)	Perimeter of cell wall (ft) will default to 4* $\sqrt{\text{cell floor area}}$ if blank.
16-20	JC(K,I)	Designation number of cell connected to cell I. Only cells having designation numbers greater than I are input. A negative JC(K,I) indicates that local loss coefficients should not be computed for the connection defined by JC(K,I). This would be used typically when the connection is an intra-room connection. The number of connections is limited to six.
21-25	AP(K,I)	Flow area of junction connecting cells I and JC(K,I) (ft ²).

If NCRITC >0 then card 5d is read NCRITC times (where NCRITC is specified on card 5a), otherwise card 5d is omitted from the input stream.

5d. Format (215)

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-5	ICRIT(1,L)	Enter the cell number of either cell connected by the Lth axial junction.
6-10	TORB	Enter a zero (or blank) if the junction is at the bottom of the cell. Enter a 1 if it is at the top of the cell.

If NCRITK >0 then card 5e is read NCRITK times (where NCRITK is specified on card 5a), otherwise it is omitted from the input stream.

5e. Format (215)

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-5	KCRIT(1,L)	Enter the cell number of the lower-numbered cell connected by the Lth transverse junction.
6-10	KCRIT(2,L)	Enter the cell number of the higher-numbered cell connected by the Lth transverse junction.

6. Wall Conduction Input

NGEN generates a wall heat transfer surface area for each cell (I) which is defined by

$$AS(I) = P(I)*DX(L) + 2 A(I) - \sum_{k=1}^{Np} AP(K,I)$$

where

AS(I) is the wall surface area (ft²)

P(I), A(I), and AP(K,I) are defined by card 5c

DX(L) is defined by card 5b

Np is the number of junctions in cell I.

The heated perimeter of each cell is defined as

$$HPERIMI(I) = AS(I)/DX(L) \text{ (ft)}$$

Two walls, each having the heated perimeter as defined above, are generated for each cell. The first is assigned properties and dimensions which are representative of concrete walls. The default properties for concrete walls are:

Density	= 139 lbm/ft ³
Specific heat	= 0.22 Btu/lbm °F
Thermal conductivity	= 0.867 Btu/hr-ft °F
Wall thickness	= 2 ft

The second is assigned properties representative of steel panels. The default properties for steel walls are:

Density	= 487 lbm/ft ³
Specific heat	= 0.113 Btu/lbm-°F
Thermal conductivity	= 30 Btu/hr-ft-°F
Wall thickness	= 0.5 in.

The concrete wall is assigned a wall number designation equal to the cell number and the steel wall is assigned a wall number equal to the cell number plus the total number of cells. The fraction of each wall allowed to interact with the cell is specified by RMULS(I). RMULS for the concrete wall is defaulted to 1, while RMULS for the steel wall is defaulted to 0.

This assignment is valid only at the time of input. If walls are deleted or added in the wall conduction input card group, then the wall numbers are automatically reassigned such that the wall numbers run sequentially from 1 to the total number of walls.

The input in the following section consists of information which modifies the default values discussed above.

6a. Format (I10)**

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-10	NMOD	Number of walls for which the heated perimeter, interaction fraction, or thickness is to be modified. If no modifications are desired a blank card must be supplied.

6b. Format (I10,3F10.3)

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-10	N	Wall designatipn number of cell which is to have its heated perimeter, multiplier, or thickness modified.
11-20	HPERIMI(N)	New heated perimeter (ft). If HPERIMI(N) is input as zero then it is set to the default value as calculated above.
21-30	RMULS(N)	Fraction of wall surface which is allowed to interact with the cell adjacent to it. RMULS(N) must be defined; a value of zero would be specified to remove a defaulted wall from the COBRA-NC input.
31-40	DIN(N)	Thickness of the modified wall in feet, If no value is specified, DIN(N) defaults to 2 ft for the concrete wall and 0.5 in, (0.0417 ft) for the steel wall.

If NMOD is greater then 0 then NMOD cards of the type 6b must be supplied.

7. Boundary Specification Group

NBOUND card sets are required. NBOUND was previously specified on the operation parameter card.

7a. Format (2I10,4F10.0)*

Columns	Variable	Description
1-10	IBOUND(J)	The cell number to which this boundary is applied.
11-20	ISPEC(J)	Boundary specification type. Valid options are: 1 = pressure and enthalpy 2 = flow and enthalpy 3 = flow only 4 = mass source 5 = pressure sink and enthalpy See COBRA input instructions for complete discussion of these options.
21-30	XVALUE(J)	Boundary pressure (psia)
31-40	ASINK(J)	The flow area through which the flow defined by the boundary specification enters the cell (ft ²). This value is required for all pressure boundary specifications. It is also required if the local loss coefficient is to be defaulted.
41-50	SSINK(J)	Local flow loss coefficient (dimensionless) at the boundary. If blank, the code calculates a value using Idel'Chik (Idel'Chik, 1966) and the specified cell flow area (ASINK).
51-60	DXSINK	Length of the momentum control volume for the sink. This variable is needed for a type 5 specification; however, if blank a value equal to $\sqrt{(A(I))}$ will be supplied.

7b. Format (3I10)**

This card specifies the number of points to be supplied for the time-varying boundary specification table and the wall condensation heat transfer time-varying multiplication factor. Three values are supplied. If the boundary type is either 1 or 5, the first value is the number of pressure-time coordinates specified in the table. If the boundary type is 2, 3, or 4, this first value is the number of flow rate-time coordinates specified in the table. The second value is the number of enthalpy-time coordinates to be supplied. If either or both of these values is zero, then that particular boundary specification will remain constant in time. The third value specifies the number of points (pairs of values) to be applied as a time-varying multiplicative factor for modeling the wall condensation heat transfer coefficient.

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-10	NPTS1	Number of points (pairs of values) in the pressure or flow forcing function table.
11-20	NPTS2	Number of points (pairs of values) in the enthalpy forcing function table.
21-30	NPHTCF	Number of points (pairs of values) in the condensation heat transfer coefficient modifier table. A maximum of 40 points may be specified. The wall condensation heat transfer coefficient is calculated using the Uchida correlation (Second Australian Heat Conference, 1977)

The card (7b) must be included as a blank card if no tables are to be input.

7c. Flow or Pressure Specifications Table

Two options are available in this group. If NPTS1 is zero or blank then only a single value of flow or pressure is input.

Format (F10.2)**

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-10	PVALUE(J)	Either boundary pressure (psia) or flow rate (lbm/sec), whichever is called for by 7a.

If NPTS1 is not zero or blank, then a tabular forcing function containing NPTS1 pairs of points is supplied.

Format (5(F5.0,F10.0))**

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-5,16-20 etc.	ABSCIS(K,J)	Enter the time, in seconds, at which to apply the factor.
6-15,21-30 etc.	ORDINT(K,J)	Enter the forcing pressure or flow rate to be applied at time ABSCIS(K,J) (psia or lbm/sec).

7d. Enthalpy Specification

As above, two options are available. If NPTS2 is 0 or blank, only a single value of boundary enthalpy is input.

Format (F10.2)**

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-10	HVALUE(J)	Constant boundary cell enthalpy Btu/lbm.

If NPTS2 is greater than 0, then a tabular forcing function containing NPTS2 pair of points is supplied.

Format (5(F5.0,F10.0))**

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-5,16-20 etc.	ABSCIS(K,J)	Enter the time, in seconds, at which to apply the enthalpy.
6-15,21-30 etc.	ORDINT(K,J)	Enter the forcing enthalpy to be applied at time ABSCIS(K,J) (Btu/lb).

Cards 7a, 7b, 7c, and 7d are required for each boundary from which flow enters or leaves the computational region. Each boundary is completely specified before information concerning other boundaries is input. When the boundary is a pressure type boundary and the pressure is specified by XVALUE on card 7a, card 7c may be left blank for the constant pressure option. In addition, if the flow is always out of the system then 7d may also be left blank. The boundary specification is limited to two specifications per cell. If more boundary conditions are required to define the physical problems, then the cell may be divided into more than one cell.

7e. Wall Heat Transfer Specification Table

If NPHTCF is blank or zero card group 7e is omitted from the input stream. If NPHTCF is nonzero then a tabular forcing function is supplied. This card is supplied after all boundary specifications have been input.

Format (5(F5.0,F10.0)).

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-5,16-20 etc.	ABSCIS(K,J)	Enter the time, in seconds, at which to apply the wall heat transfer multiplier.
6-15,21-30 etc.	ORDINT(K,J)	Enter the wall heat transfer multiplier to be applied at time ABSCIS(K,J) (dimensionless).

8. Output Information

This card is required, but if the standard printed output of all cells is desired, then it may be blank. The standard output consists of a description of the input and the calculated cell pressure, temperature, relative humidity, and liquid volume fraction as functions of time. This information is printed for all output options.

8a. Format (5I10)**

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-10	N1	Enter the general vessel output option. Valid entries are: 1 = print cells only 2 = print cells and junctions only 3 = print walls only 4 = print walls and cells only 5 = print cells, junctions, and walls (This entry applies to the microfiche COBRA output only)
11-20	NOUT1	Enter the number of cells to be printed (used if N1=1, 2, or 5). If NOUT1 = 0, all channel will be printed. If NOUT1 > 0, an array of channels numbers will be entered on card 8b.
21-30	NOUT4	Enter number of walls to be printed (used if N1 ≥ 3). If NOUT4 = 0, all walls will be printed. If NOUT4 > 0, an array of wall numbers to be printed will be entered on card 8c.
31-40	NCGRAF	Graphics dump option. If NCGRAF is zero then no plot file will be generated. If NCGRAF is > 0 then the standard COBRA-NC files for generating graphs of pressure, relative humidity, and temperature will be produced for the cells specified by the NOUT1 option.

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
41-50	MFICHE	Option for printing complete COBRA output to microfiche. If MFICHE > 0 then the complete output is printed on microfiche. This includes all of the output described in the COBRA User's Manual (Thurgood 1986).

8b. Format (1215)

Omit card 8b if NOUT1=0

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-5, ..	PRINTC(I)	Enter the index numbers of channels to be printed. Twelve (12) values are entered per card, Repeat this card until NOUT1 values have been entered.

8c. Format (1215)

Omit Card 8c if NOUT4 = 0.

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-5, ...	PRINTS (I)	Enter the index numbers of walls to be printed. Twelve (12) values are entered per card. Repeat this card until NOUT4 values have been entered.

4.0 COBRA MODIFICATIONS

The COBRA-NC code has been modified to provide more useful output as requested by the Nuclear Regulatory Commission's Auxiliary Systems Branch (NRC/ASB). An interim version of the code was created, designated COBRA-NC/ASB, which included the modifications described in this section. These changes have since been incorporated into Cycle 15 of COBRA-NC. In the following discussion it is assumed that the reader is familiar with COBRA-NC input definitions (Thurgood 1986).

4.1 GENERAL DESCRIPTION OF COBRA-NC MODIFICATIONS

The following modifications to the COBRA-NC code were made to meet specific needs of the NRC/ASB:

If English units are to be used in the input, feet, rather than inches, may be selected for the basic length unit.

- The output edit option definitions were changed such that the complete COBRA-NC output which was printed may now be output to a computer file every EDINT seconds.
- A new printed output option was added which prints cell values of pressure, vapor temperature, relative humidity, and cell liquid volume fraction at user-specified intervals.
- A choked flow option was added which limits flow rate at pressure boundaries and internal junctions.

Each of the above modifications is discussed further in the following sections.

The edit options generated by INGEN are prescribed, and except for the total running time and the option of outputting microfiche, the user has no control over the generated edit options. However, should these hardwired options be unacceptable then the user may edit the INGEN output file before submitting it as COBRA-NC input.

The generated edit and time domain output consists of four time domains. The first is an initialization regime extending 0.1 sec into the simulation. During this regime the maximum time step is set to 0.001 sec and the print interval is set to 0.02 sec. The second time regime extends through the first second of the simulation. This domain sets a maximum time step of 0.05 sec and a print interval of 0.1 sec. The third regime extends 100 sec into the simulation or to the end of the simulation, whichever comes first. The maximum time step in this regime is 1.0 sec and the print interval is 1.0 sec. The final regime extends to the end of the simulation with a maximum time step of 1.0 sec and a print interval of 10.0 sec.

When microfiche output is desired, MFCHE is input with a value greater than 0. The dump interval to the microfiche file is then set to 1.0 sec by INGEN. Likewise, when NCGRAF is greater than zero, all pressure, temperature, relative humidity, and liquid volume fractions are saved on file 'tape11' at each dump interval. Since plots are not drawn as part of the COBRA-NC run, tape11 must be saved after the completion of COBRA-NC execution. Plots can then be generated by running a separate plotting routine.

Another major change to COBRA-NC is the modification of the wall condensation heat transfer package. The existing correlations were removed and replaced with the Uchida (Second Australian Heat Conference, 1977) correlation in the following form,

$$H = MN(280,79.33*(\rho_{vap}/\rho_{air})^{.8}*f_1)$$

where H = condensation heat transfer coefficient (Btu/hr-ft²-°F)
 ρ_{vap} = steam density (lbm/ft³)
 ρ_{air} = air density (lbm/ft³)
 f_1 = user input time varying multiplication factor

At the present time there is a large uncertainty in estimating condensation heat transfer. The above expression is known to be incomplete in that the heat transfer coefficient should also contain local temperature and velocity effects. However, since work is currently underway at PNL and other institutions throughout the world to develop universal condensation heat transfer coefficients, it is recommended that for the interim the multiplication factor f_1 be set in the range 1-3 for small breaks, and 3-6 for large breaks during blowdown, and set to 1 after blowdown for both large and small breaks. To perform a conservative analysis, f_1 should be set equal to 1.

The final modification to COBRA-NC is the addition of a choked flow model. The approach taken is the historic approach where correlations are used to calculate limiting flow rates. Three different correlations are available in tabular form; they are Moody, Henry-Fauske and Henry-Fauske subcooled. The tabular form of these correlations were taken from a code listing of RELAP 4 (Moore and Rettig 1975). Once a model is chosen it must be used until the problem is finished or until it is dumped and then restarted. The calculation is implemented by checking the flow calculated by COBRA-NC against that calculated with the chosen model.

When making the critical flow calculation it is assumed that the enthalpy of the upstream continuity cell is the stagnation enthalpy. This assumption is valid for containment geometries where rooms are large compared to connecting flow areas. If the calculated critical flow is less than the tentative flow, then the tentative flow is set to the critical value and the local derivatives of flow with respect to pressure are set to zero. The relative distributions of vapor and liquid flows will not necessarily be the same for the tentative

and critical flow calculations. The most consistent approach is to define the vapor-liquid distribution consistently with the assumption used in development of the critical flow model. Therefore, when the critical flow rate is used, it is assumed that the continuous liquid and droplet fields have the same velocity and that the slip ratio between vapor and liquid is defined to be:

$$S = (p / \rho_g)^{1/3} \quad \text{for Moody model}$$

$$S = 1.6 \quad \text{for Henry-Fauske model (original and subcooled)}$$

where $S = V_g/V_f$

V_g = vapor velocity

V_f = liquid velocity

ρ_f = liquid density

ρ_g = density of vapor and gas combined.

The expanded capabilities of cycle 15 of COBRA-NC have resulted in some modification to the COBRA-NC input instructions (Thurgood 1986). The input cards that have been added or modified are listed in Table 3.

TABLE 3. COBRA-NC Input Cards that Require Modification to Input Instructions

<u>Card</u>	<u>Disposition</u>
INPUT. 1	Modify input instructions
CARD1.I	Modify input instructions
CARD13.1	Modify input instructions
CARD13.10	Add to input instructions
CARD13.11	Add to input instructions
CARD14.1	Modify input instructions
TIME. 1B	Add to input instructions

The input instructions for card INPUT.I is replaced by:

INPUT.I: ICOBRA, IAPENK, ENGUNI FORMAT (3114)

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-14	ICOBRA	Enter input units option: 0 = use English units (default) 1 = use metric units; code will convert the data to English units.
15-28	IAPENK	Leave blank.
29-42	ENGUNI	For English units only, enter the number of inches to use for the basic length unit, i.e., enter 12 if input data is to have feet as the basic unit of length. The default value of ENGUNI is 1.

The input instructions for card CARD1.I is replaced by:

CARD1.I: NGROUP, NGAS, IREF, NTGAS, NAL, NHF, NLE, NZS, MCRIT FORMAT (915)

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-5	NGROUP	Enter one (1).
6-10	NGAS	Enter the total number of noncondensable gas species to be used in the calculation.
11-15	IREF	Flag to specify if a uniform initial gas or if a uniform initial steam pressure is to be assumed. Enter 0 if a uniform initial steam pressure is desired. Enter 1 if a uniform initial gas pressure is desired.
16-20	NTGAS	Enter the number of initial gas temperature tables to be read.
21-25	NAL	Enter the number of initial liquid volume fraction tables to be read.
26-30	NHF	Enter the number of fluid heat flux tables to be read.
31-35	NLE	Enter the number of initial liquid enthalpy tables to be read.

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
36-40	NZS	Enter the number of slab zero heat flux tables to be read.
41-45	MCRIT	If critical flow calculations are to be performed input a 1. Otherwise enter a 0, or leave blank.

The input instructions for card CARD13.1 is replaced by:

CARD13.1 NGROUP,NIBND,NKBND,NFUNCT,NGEND,ICONVB,NCRITC I T FORMAT(8I5)

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-5	NGROUP	Enter thirteen (13) .
6-10	NIBND	Enter the total number of vertical mesh cell boundary conditions.
11-15	NKBND	Enter the total number of transverse momentum cells for which crossflow will be set to zero.
16-20	NFUNCT	Enter the number of forcing functions for the boundary conditions,
21-25	NGEND	Enter the number of groups of contiguous transverse momentum tells for which crossflows will be set to zero.
26-30	ICONVB	Momentum convection flag for type 1 boundary conditions specified on <u>CARD13.4</u> . If INCONVB=0 convect zero momentum into mesh. If INCONVB>0 convect downstream momentum into mesh.
31-35	NCRITC	Enter the number of axial junctions to be checked for critical flow.
36-40	NCRITK	Enter the number of transverse junctions to be checked for critical flow.

Add new card to input instructions as follows:

CARD13.10 is read NCRITC times.

CARD13.10 ICRIT(1,L),ICRIT(2,L) FORMAT(2I5)

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-5	ICRIT(1,L)	Enter the channel number of channel with axial junction to be checked for critical flow.

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
6-10	ICRIT(2,L)	Enter the vertical node with the axial junction to be checked for critical flow. (Note: if the junction is at the bottom of the channel enter a 1, if it is at the top of the channel enter 1 plus the number of vertical levels in the section containing channel ICRIT(1,L).

Add new card to input instructions as follows:

CARD13.11 is read NCRITK times.

CARD13.11 KCRIT(1,L),KCRIT(2,L) FORMAT(2I5)

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-5	KCRIT(1,L)	Enter the identification number of the lower-numbered channel of the pair connected by the transverse junction to be checked for critical flow.
6-10	KCRIT(2,L)	Enter the identification number of the higher-numbered channel of the pair connected by the transverse junction to be checked for critical flow.

The input instructions for CARD14.1 is replaced by:

CARD14.1 NGROUP,N1,NOUT1,NOUT2,NOUT3,NOUT4,IPROPP, IOPT,ASBINT FORMAT(9I5)

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-5	NGROUP	Enter fourteen (14).
6-10	N1	Enter the general output option. Valid entries are: 1 = print channels only 2 = print channels and gaps only 3 = print thermal conductors only 4 = print thermal conductors and channels only 5 = print channels, gaps, and thermal conductors

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
11-15	NOUT1	Enter the number of channels to be printed (used if N1 = 1, 2, 4, or 5) If NOUT1 = 0, all channels will be printed. If NOUT1 > 0, an array of NOUT1 channel numbers must be entered on CARD14.2.
16-20	NOUT2	Leave blank.
21-25	NOUT3	Enter the number of gaps to be printed (used if N1 = 2 or 5). If NOUT3 = 0, all gaps will be printed. If NOUT3 > 0, an array of NOUT3 gap numbers must be entered on CARD14.3.
26-30	NOUT4	Enter the number of thermal conductor to be printed (used if N1 > 2). If NOUT4 = 0, all unheated conductors will be printed. If NOUT4 > 0, an array of NOUT4 thermal conductor numbers must be entered on CARD14.5.
31-35	IPROPP	Enter the property table print option. Valid entries: 0 = do not print the property table 1 = print the property table
36-40	IOPT	Enter the debug print option, Valid entries are: 0 = normal printout only 1 = debug printout (print extra data for channels, conductors, and gaps)
41-45	ASBINT	Flag to specify abbreviated output option. IF ASBINT > 0 abbreviated output selected.

Add new card to input instructions as follows:

Card TIME.1B is read only if ASBINT > 0 on card CARD14.1.

TIME. 1B ASBINT FORMAT(F14.6)

<u>Columns</u>	<u>Variable</u>	<u>Description</u>
1-14	ASBINT	Enter the print interval for abbreviated output (sec).

5.0 SAMPLE PROBLEM

The INGEN input generator was used to create COBRA-NC input for an analysis of a high energy steam line break (HELB) at a typical nuclear generator station. The steam line break that was modeled and the resulting INGEN input and output are described below.

5.1 STEAM LINE BREAK MODEL

The HELB scenario modeled involves the rupture of a high pressure pipe carrying saturated steam. The postulated pipe rupture occurs in the high pressure injection (HPI) pump room (Room 053) which has the following initial conditions:

Initial Pressure	14.7 psia
Initial Temperature	90°F
Initial Relative Humidity	50%

The steam escaping from the pipe has a temperature of 590°F and a pressure of 925 psia. The mass flow rate and enthalpy content of the escaping steam were defined to be as shown in Table 4.

The dimensional data for the rooms connected to the HPI pump room, including a description of the junctions between rooms is typical. A noding diagram for this model is shown in Figure 1.

This model consists of 18 computational cells with 12 lateral and 6 vertical junctions. The cell volumes are given in Table 5 and the junction flow areas are given in Table 6.

INGEN Input

A copy of the INGEN input for this model is shown in Figure 2. Note that the line numbers to the left of the input data are not part of this input. They will be used here to reference specific lines of input. Lines 1 through 4 are the Title Card, Operation Parameter Card, Restart Data Card, and Containment Initialization Card, respectively. These cards identify the input deck and provide some initialization data.

Lines 5 through 26 are the Geometry Input Group. Line 5 specifies that there are 3 floors; Lines 6, 19 and 25 specify the number and height of the cells on each floor. The remaining lines specify the volume of each cell and define the junctions between cells.

Line 27 is the Wall Conduction Input. In this case a blank card was used to select the INGEN default wall parameters.

TABLE 4. Mass Flow Rate and Specific Enthalpy of Steam Flow into Pump Room

<u>Time From Pipe Rupture (sec)</u>	<u>Mass Flow Rate (lbm/sec)</u>	<u>Enthalpy (Btu/lbm)</u>
0.00 - 0.85	142.0	1249.4
0.85 - 5.0	71.0	1249.4
5.0 - 6.0	68.8	1249.4
6.0 - 7.5	67.8	1249.4
7.5 - 10.0	64.9	1249.4
10.0 - 12.5	62.8	1249.4
12.4 - 15.0	61.0	1249.4
15.0 - 17.5	58.0	1249.4
17.5 - 20.0	54.5	1249.4
20.0 - 22.5	49.5	1249.4
22.5 - 25.0	46.2	1249.4
25.0 - 27.5	39.3	1249.4
27.5 - 30.0	27.7	1249.4
30.0 - 32.5	15.2	1249.4
35.0 - +	0	1249.4

TABLE 5. Cell Volumes Used in COBREE Analysis

<u>Cell</u>	<u>Volume (ft³)</u>
1	25,498
2	4,493
3	29,395
4	7,286
5	8,163
6	25,661
7	3,525
8	95,910
9	567
10	11,703
12	6,683
13	12,830
14	1,763
15	283
16	5,851
17	7,664
<u>18</u>	<u>3,525</u>
Total volume:	266,127

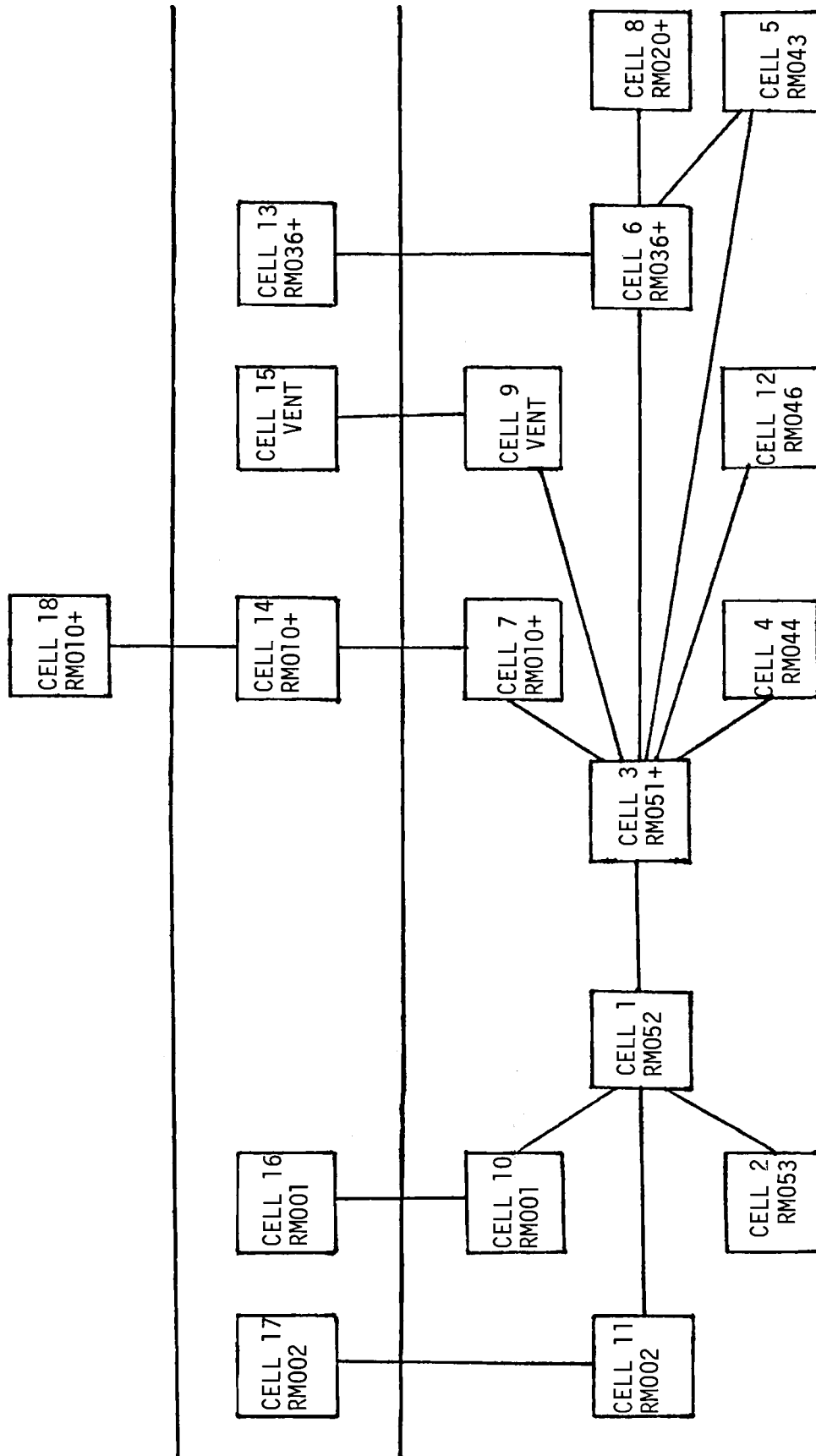


FIGURE 1. COBREE Noding Diagram

TABLE 6. Junction Flow Areas Used in COBREE Analysis

<u>Connecting Cells</u>	<u>Flow Area (ft²)</u>
1-2	21.0
1-3	57.5
1-10	12.0
1-11	12.0
3-4	23.8
3-5	4.9
3-6	96.0
3-7	23.3
3-9	17.5
3-12	20.0
5-6	22.0
6-8	206.0
6-13	1425.0
7-14	195.0
9-15	31.0
10-16	650.0
11-17	850.0
14-18	195.0
15-atm	19.5

Lines 28 through 40 are the Boundary Specification Group. The steam line break boundary condition is described in lines 28 through 36. An atmospheric vent boundary is specified for cell 15 in lines 37 through 40.

Finally, line 41, which is blank, specifies INGEN default output selection.

INGEN Output

A copy of the output generated by INGEN for this analysis is given in Figure 3. Note that INGEN annotates the input file with comments to the right of the data at the beginning of the major input data groups. For a complete description of the COBRA-NC input data refer to Reference 1.

The input file generated by INGEN may now be submitted as input for COBRA-NC or modified to meet the requirements of the particular analysis being performed.

In this example we see the significant reduction in input requirements between INGEN and COBRA-NC. The 41 lines of input to INGEN is used to generate a 213 line input deck for COBRA-NC.

COBRA-NC Output

A copy of the output generated by COBRA-NC for this analysis is given in Appendix C.

```

1 1 helb model 3-21-85
2           2           1000.
3
4      14.7      90.      0.5
5           3
6           12      18.0      1      1
7 125498      2 21.0      3 57.5      10 12.0      11 12.0
8 24493.
9 329395      4 23.8      5 4.9      6 96.0      7 23.3      9 17.5      12 20.0
10 47286.
11 58163.      6 22.0
12 625661      8206.0      -131425.
13 73525.      -14 195.
14 895910
15 9 567.      -15 31.0
16 1011703      -16 650.
17 1115327      -17 850.
18 126683.
19           5      9.00      1      1
20 1312830
21 141763.      -18 195.
22 15283.
23 165851.
24 177664.
25           1      18.0      1      1
26 183525.
27
28           2      2      925.
29           30      0
30 0.0      142.0 0.85      142.00.851      71.0 5.0      71.0 5.01      68.8
31 6.0      68.6 6.01      67.8 7.5      67.8 7.51      64.9 10.0      64.9
32 10.01      62.8 12.5      62.812.51      61.0 15.0      61.015.01      58.0
33 17.5      58.017.51      54.5 20.0      54.520.01      49.5 22.5      49.5
34 22.51      46.2 25.0      46.225.01      39.3 27.5      39.327.51      27.7
35 30.0      27.730.01      15.2 32.5      15.2 35.0      0.01500.
0.0
36 1249.4
37           15      1      14.7
38           0      0
39 14.7
40 145.3
41

```

FIGURE 2. HELB INGEN input. (Line numbers to the left are for reference only)

```

0.100000e-02 0 0.000000e+00 12 set units and linear conv.
1 helb model 3-21-85 40 restart data
1 1 278.00 278.00 27.80 278.00 0 vessel 1.1
14.691 1101.108 131.388 0.0000010 0.0237449
air 0.9762541 vessel 2.1
2 18 18
11417.150.5
2249.663.20249.6
31633.161.6
4404.880.48
5453.585.18
61426.151 .0 1425.
7195.855.98 195.0
85328.292.0
931.5022.45 31.00
10650.2102.0 650.0
11851.5116.7 850.0
12371.377.07
131426.151.01425.
14195.955.98195.0195.0
1531.4422.4331.0031.44
16650.1102.0650.0
17851.6116.7850.0
18195.855.98195.0
1 -1 0
2 -2 0
3 -3 0
4 -4 0
5 -5 0
6 -6 0
7 -7 0
8 -8 0
9 -9 0
10 -10 0
11 -11 0
12 -12 0
13 -13 0
14 -14 0
15 -15 0
16 -16 0
17 -17 0
18 -18 0

```

FIGURE 3. HELB COBRA-NC input.

3	12	
1	1	21.1679.1652.5992.000
1.		
2	1	33.19415.172.6982.000
1.		
3	1	10.66676.9282.4882.000
1.		
4	1	11.66676.9282.4882.000
1.		
5	3	41.3229.7572.6162.000
1.		
6	3	5.27224.4271.9372.000
1.		
7	3	65.33319.602.7292.000
1.		
8	3	71.2949.6542.6132.000
1.		
9	3	9.97228.3672.5712.000
1.		
10	3	121.1118.9442.5922.000
1.		
11	5	61.2229.3812.6062.000
1.		
12	6	811.4428.712.7602.000
1.		

vessel 3.1

4	3	1	
1	12	1	18.00
1	1		
2	2		
3	3		
4	4		
5	5		
6	13		
7	14		
8	8		
9	15		
10	16		
11	17		
12	12		
2	5	1	9.00
13	13		
14	18		
15	15		
16	16		

blank 3.4
vessel 4.1

1
2
3
4
5
6
7
8
9
10
11
12
6
7
9
10

FIGURE 3. (contd)

8 wall	884.	2.00	4	1					
5 10.008		5	10.042	5	1 0.65		5	1 1.30	
9 wall	24.	2.00	4	1					
5 10.008		5	10.042	5	1 0.65		5	1 1.30	
10 wall	138.	2.00	4	1					
5 10.008		5	10.042	5	1 0.65		5	1 1.30	
11 wall	164.	2.00	4	1					
5 10.008		5	10.042	5	1 0.65		5	1 1.30	
12 wall	118.	2.00	4	1					
5 10.008		5	10.042	5	1 0.65		5	1 1.30	
13 wall	309.	2.00	4	1					
5 10.008		5	10.042	5	1 0.65		5	1 1.30	
14 wall	56.	2.00	4	1					
5 10.008		5	10.042	5	1 0.65		5	1 1.30	
15 wall	26.	2.00	4	1					
5 10.008		5	10.042	5	1 0.65		5	1 1.30	
16 wall	174.	2.00	4	1					
5 10.008		5	10.042	5	1 0.65		5	1 1.30	
17 wall	212.	2.00	4	1					
5 10.008		5	10.042	5	1 0.65		5	1 1.30	
18 wall	67.	2.00	4	1					
5 10.008		5	10.042	5	1 0.65		5	1 1.30	
10 1								vessel 10.1	
1 2	139.00								
50.000	0.220	0.867	1000.000	0.220	0.867				
13 24	0 1	0 0	0 0					vessel 13.1	
30									
	142.00.8500	142.00.8510	71.005.000	71.005.010	68.80				
6.000	68.606.010	67.807.500	67.807.510	64.9010.00	64.90				
10.01	62.8012.50	62.8012.51	61.0015.00	61.0015.01	58.00				
17.50	58.0017.51	54.5020.00	54.5020.01	49.5022.50	49.50				
22.51	46.2025.00	46.2025.01	39.3027.50	39.3027.51	27.70				
30.00	27.7030.01	15.2032.50	15.2035.00	0.001500.	0.00				
2 1	2 1	0 1.000	1249.400	925.000					
251.5.0001	1.9999.0001							blank 13.4b	
15 3	1 0	0 14.700	145.300	14.700					
152.3.9999	1.9999.0001							blank 13.4b	
1 1	3								
3 1	3								
4 1	3								
5 1	3								
6 1	3								
7 1	3								

FIGURE 3. (contd)

```

8  1  3
9  1  3
10 1  3  11  1  3
12 1  3
1  2  3
2  2  3
3  2  3
4  2  3
5  2  3
8  2  3
12 2  3
13 2  3
16 2  3
17 2  3
18 2  3
14 1  0          0          1          vessel 14.1
                                     end set 1
                                     blank graf.1
                                     graf.2
0  -1
0.000100  0.001000  0.100000  1.000000  300.000000
1000000.0000001000000.000000  500.0000001000000.000000
0.020000
0.000100  0.050000  1.000000  1.000000  300.000000
1000000.0000001000000.000000  500.0000001000000.000000
0.100000
0.000100  0.010000  36.000000  1.000000  300.000000
1000000.0000001000000.000000  500.0000001000000.000000
1.000000
0.000100  0.200000  36.000000  1.000000  300.000000
1000000.0000001000000.000000  500.0000001000000.000000
10.000000
-1.000000

```

FIGURE 3. (contd)

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APPENDIX A
INGEN PROGRAM LISTING

APPENDIX A

INGEN PROGRAM LISTING

```

program ingen (input ,output ,tape6=input ,tty,tape9)
common /forms/ ka(80)
common scommon,
    title (17) ,ck(12),nrpc(2,50),
    a(50),ncell(10),dx(10),ncstart(10),nclast(10),
*   p(50),jc(6,50),ap(6,50),npts(9),irdint(9,50),
    ik(100),jk(100),gapn(100),length(100),fwall(100),
    wkr(100),abot(50),atop(50),kchana(50,6),kchanb(50,6),
*   icy(50,10),cdl(50),izdum(50),jzdum(50),
*   hperimi(100),rmuls(100),ir(50),dir(100),nwhtcf,
*   abscis(50,9),ordint(50,9),lbot(50),ltop(50),
    ibound(9),isped(9),xvalue(9),asin(9),ssin(9),dxsin(9),
    hvalue(9),pvalue(9),npfn(9),nhfn(9),lcb(9),nbcs(50),
    xarg,zarg,nodes(50),nodesf(10),
    kcrit(2,50),icrit(2,50),
    nll(50),
    ecommon
real length
dimension icomn(1)
dimension jwarn(30)
equivalence (i comn,scommon)
c
    data pi,feet,sqft,nconv/3.14159,1.,1.,12/
    data scvl,shvl,sc11,sh11/278.,278.,27.8,278./
    data humax,humin/280.,2.0/
cc**** zero common
    is=locf(ecommon) - locf(scommon)
c
    do 10 i=1,is
    icomn(i)=0
10 continue
c
    warning=0.
    nwarn=0
    do 20 j=1,5
    pvalue(j)=1.0
20 hvalue(j)=1.0
    read (6,550) title
    read (6,540) nbound,mcrit,tottrn
    read (6,530) idstep,timet
    read (6,560) patm,tatm,rhumid
    if (patm.eq.0) patm=14.696

```

```

        if (tatm.eq.0.0) tatm=92.0
        if (rhumid.eq.0) rhumid=.5
cc*** default wall thickness to 2ft.
cc*** default steel material thickness to 1/2 inch.
        wt=2.*feet
        swt=.5/12.
        read (6,580) nfloor,ncritc,ncritk
        nctot=0
        nntot=0
        do 40 l=1,nfloor
        read (6,533) ncell(l),dx(l),nnode,iaorv
        if(nnode.le.0) nnode=1
        nodesf(l)=nnode
        dx(l)=dx(l)*feet
        nc=ncell(l)
        do 30 ic=1,nc
        nctot=nctot+1
        if (ic.eq.1) ncstart(l)=nctot
        if (ic.eq.nc) nclast(l)=nctot
        read (6,570) i,a(i),p(i),(jc(k,i),ap(k,i),k=1,6)
        icy(ic,l)=i
        lbot(i)=0
        nntot=nntot+nnode
        nodes(i)=nnode
        if(iaorv.gt.0) a(i)=a(i)/dx(l)
        if(p(i).le.0.) p(i)=4.*sqrt(a(i))
        ltop(i)=0
30 continue
40 continue
        do 45 nncritc=1,ncritc
        read(6,660) icrit(1,nncritc),torb
        if(torb.eq.0) then
            icrit(2,nncritc)=1
        else
            icrit(2,nncritc)=nodes(i crit(1,nncritc))+1
        end if
45 continue
        do 47 nncritk=1,ncritk
        read(6,660)(kcrit(kk,nncritk),kk=1,2)
47 continue
        nk=0
        l=1
        iwide=0
        ncdt=0
        ncd=0
        do 50 i=1,nctot
        lbot(i)=0
50 ltop(i)=0

```

```

do 90 i=1,nctot
a(i)=a(i)*sqft
p(i)=p(i)*feet
if (i.gt.nclast(1)) l=l+1
do 80 k=1,6
j=iabs(jc(k,i))
ap(k,i)=ap(k,i)*sqft
if (j.eq.0) go to 90
cc*** room to room-define port loss coefficient
cc*** assumes circular port here
f1=0.
f2=0.
if (jc(k,i).lt.0) go to 60
cc*** room to room - define port loss coefficient
cc r port here
d0 = (4.*ap(k,i)/pi) **.5
xarg= wt/d0
zarg=.5
if (xarg.gt.1.3) zarg=1.
f1=2.204-.44*atan(9.556*xarg-.6656)
f2=2.826-.943*xarg
60 continue
if (j.gt.nclast(1)) go to 70
cc** transverse port ****
nk=nk+1
gapn(nk)=ap(k,i)/dx(1)
ik(nk)=i
jk(nk)=j
iwide=max0(iwide,iabs(j-i))
length(nk)=amin1(0.125*(p(i)+p(j)),2.*sqrt(ap(k,i)))
wkr(nk)=zarg*f1+(1.-zarg)*f2
cc*** assume all cells are rooms for friction calculatio@
fwal(n,k)=2.
go to 80
70 continue
cc*** come here if port connects different floors
abot(j)=ap(k,i)
lbot(j)=lbot(j)+1
ltop(i)=ltop(i)+1
lb=lbot(j)
lt=ltop(i)
kchanb(j,lb)=i
atop(i)=ap(k,i)
kchandi(lt)=j
ncdt=ncdt+1
if (abs(f1).le.0.) go to 80
ncd=ncd+1
cdl(ncd)=zarg*f1+(1.-zarg)*f2

```

```

      izdum(ncd)=i
      jzdum(ncd)=nodes(i )+1
80  continue
90  continue
      do 110 i=1,nctot
      if (lbot(i).ne.0) go to 100
      lbot(i)=1
      kchan(i,1)=i
100  if (ltop(i).ne.0) go to 110
      ltop(i)=1
      kchan(i,1)=i
110  continue
      read(6,580) nmod
cc*** r=1 set up concrete walls
cc*** k=2 set up steel ( defaulted to zero surface area
      l=1
      do 140 i=1,nctot
      if (i .gt.nclast(1)) l=l+1
      hperim(i) =2*di) -abot(i) -atop(i)
      do 120 k=1,6
      if (jc(k,i).eq.0) go to 130
      if (iabs(jc(k,i)).gt.nclast(1)) go to 120
      hperim(i)=hperim(i)-ap(k,i)
120  continue
130  continue
      hperim(i)=hperim(i)/dx(1)+p(i)
      n=i+nctot
      hperim(n) =hperim(i)
      rmuls(i)=1.
      if(hperim(i).le.0) rmuls(i)=0.
      rmuls(n) =0.
      dini) =wt
      din(n) =swt
140  continue
      if (nmod.le.0) go to 160
      do 150 k=1,nmod
      read(6,530) n,hper,rmuls(n),dini
      if (hper.ne.0.) hperim(n) =hper
      if (dini .ne.0.) din(n)=dini
      if(hper+dini.gt.0.and.rmuls(n).le.0) rmuls(n)=1.
150  continue
160  continue
      do 170 i=1,nctot
      nrpc(1,i)=0
170  nrpc(2,i)=0
      itot=0
      nrtot=0
      do 180 i=1,nctot

```

```

    if (rmuls(i).eq.0) go to 180
    nrtot=nrtot+1
    nrpc(1,i)=nrtot
    itot=itot+1
    ir(nrtot)=i
180 continue
    nexcon = 0.
    do 190 i=1,nctot
    if(ltop(i).gt.1) nexcon = nexcon+ltop(i)-1
    if(lbot(i).gt.1) nexcon = nexcon+lbot(i)-1
    ip=nctot+i
    if (rmuls(ip).eq.0) go to 190
    nrtot=nrtot+1
    nrpc(2,i)=nrtot
    if (nrpc(1,i).eq.0) itot=itot+1
    ir(nrtot)=ip
190 continue
    nbc=2*(nctot-ncdt)+nbound
    nbc = nbc+ nexcon
    npt=0
    do 240 j=1,nbound
    read (6,590) ibound(j),ispec(j),xvalue(j),asink(j),ssink(j),dxsink
1(j)
    jbound=ibound(j)
    if(asink(j).le.0.) asink(j)=a(jbound)
    nbcs(jbound)=nbcs(jbound)+1
    lcb(j)=1
    if(abot(jbound).gt.0.or.nbcs(jbound).eq.2) lcb(j)=1+nodes(jbound)
    if(abot(jbound).le.0..or.atop(jbound).le.0.) go to 195
    warning=1.
    nwarn = nwarn+1
    jwarn(nwarn)=jbound
195 continue
    if (ispec(j).lt.4) nbc=nbc-1
    if(abot(jbound).le.0.) go to 198
    if(atop(jbound).le.0.) atop(jbound) = asink(j)
    go to 199
198 abot(jbound) = asink(j)
199 continue
    if (ispec(j).ne.1) go to 200
    if (ssink(j).lt.0.) go to 200
    if (asink(j).le.0.0) go to 200
    d0=(4.*asink(j)/pi)**.5
    xarg= wt/d0
    zarg=.5
    if (xarg.gt.1.3) zarg=1.
    f1=2.204-.44*atan(9.556*(xarg-.6656))
    f2=2.826-.943*xarg

```

```

ncd=ncd+1
cdl(ncd) =zarg*f1+(1.-zarg)*f2
if (ssink(j).gt.0.) cdl(ncd)=ssink(j)
izdum(ncd)=jbound
jzdum(ncd)=lcb(j)
200 continue
asink(j)=asink(j)*sqft
dxsink(j)=dxsink(j)*feet
npfn(j) =0
nhfn(j) =0
read(6,580) npts1,npts2,nphtcf
if (npts1.eq.0) go to 210
pvalue(j)=1.
npfn(j)=1
npt=npt+1
npts(npt)=npts1
read(6,600) (abscl s(k,npt),ordint(k,npt),k=1,npts1)
go to 220
210 read(6,560) pvalue(j)
220 if (npts2.eq.0) go to 230
nhfn(j) =npfn(j)+1
hvalue(j) =1.
npt=npt+1
npts(npt) =npts2
read(6,600) (abscl s(k,npt),ordint(k,npt),k=1,npts2)
go to 240
230 read(6,560) hvalue(j)
240 continue
if (nphtcf.le.0) go to 250
npt=npt+1
npts(npt) =nphtcf
read(6,600) (abscis (k,npt),ordint(k,npt),k=1,nphtcf)
nwhhtcf=npt
250 continue
cc*** start making output
cc*** default english units(12.0 for feet)
write(9,610) nconv
write(9,620) idstep,timet
epso=.001
itmax=5
iitmax=40
write(9,630) epso,itmax,iitmax
init=1
if (idstep.ne.0) init=4
write(9,640) init,title
cc*** group 1
ig=1
write(9,650) ig,ig,mcrit

```

```

write (9,655) scvl,shvl,scl1,shl1
cc*** find psat of vapor in room
ck(1) = -7.691234564
ck(2) = -2.608023696e+1
ck(3) = -1.681706546e+2
ck(4) = 6.423285504e+1
ck(5) = -1.189646225e+2
ck(6) = 4.167117320
ck(7) = 2.097506760e+1
ck(8) = 1.e9
ck(9) = 6.
theta = (tatm + 459.67) / 1.8 / 647.3
sum = 0.
onemt = 1. - theta
onemt2 = onemt * onemt
pionemt = 1.
do 260 i = 1, 5
pionemt = pionemt * onemt
sum = sum + ck(i) * pionemt
260 continue
sum = sum / theta
sum = sum / (1. + ck(6) * onemt + ck(7) * onemt2)
sum = sum - onemt / (ck(8) * onemt2 + ck(9))
beta = exp(sum)
pg = beta * 3208.11
pv = amax1(.11, rhumid * pg)
cc*** default liquid volume fraction to .000001
vfl = .000001
vfls = vfl
vfv = pv / patm
vfa = 1. - vfv - vfl
cc*** approximate vapor enthalpy by hsat at pg
hs = hg(pg)
do 265 m = 1, 1000
ts = tv(pv, hs, fp)
delh = (tatm - ts) / fp
hs = hs + delh
if(abs(delh/hs) .lt. 1.0e-6) go to 266
265 continue
266 continue
ha = 126.66 + .24 * (tatm - 70.3)
has = ha
c** correct pressure so p at top of room is ref. pressure
rhoa = 144.0 * (patm - pv) / (tatm + 459.67) / 53.342
rhov = 1.0 / vog(pv, hs)
rhom = rhoa + rhov
delpres = rhom * dx(nfloor) / 144.0
pcor = patm - delpres

```

```

        write(9,670) pcor,hs,ha,vf1,vfv
        write(9,680) vfa
cc*** group 2
        ig=2
        write(9,690) ig,nctot,itot
        do 270 i=1,nctot
        call blankit
        call form(a(i),1)
        call form(p(i),6)
        call form(abot(i),11)
        call form(atop(i),16)
270 write(9,700) i,(ka(k),k=1,20)
        do 280 i=1,nctot
        if (nrpc(1,i)+nrpc(2,i).eq.0.) go to 280
        n1=-nrpc(1,i)
        n2=-nrpc(2,i)
        write(9,710) i,n1,n2
280 continue
cc*** group 3
        if (nk.le.0) go to 300
        ig=3
        g1=1.
        write(9,720) ig,nk
        do 290 k=1,nk
        call blankit
        call form(gapr(k),1)
        call form(length(k),6)
        call form(wkr(k),11)
        call form(fwall(k),16)
        write(9,731) k,ik(k),jk(k),(ka(m),m=1,20)
        write(9,740) g1
290 continue
cc*** zero transverse momentum cards
        write(9,750)
cc*** group 4
cc***
300 ig=4
        ig1=1
        write(9,760) ig,nfloor,ig1
        htotal=0.
        do 330 l=1,nfloor
        htotal=htotal+dx(l)
        ig1=nodesf(l)
        dxo=dx(l)/nodesf(l)
        write(9,770) l,ncell(l),ig1,dxo
        nc=ncell(l)
        do 320 ic=1,nc
        i=icy(ic,l)

```



```

    llb=lbot(i)
    llt=ltop(i)
    if (llt.eq.1)
      . write(9,780) i, (kchana(i,ll),ll=1,llt), (kchanb(i,ll),ll=1,llb)
    if.(llt.eq.2)
      . write(9,790) i, (kchana(i,ll),ll=1,llt), (kchanb(i,ll),ll=1,llb)
    if (llt.eq.3)
      . write(9,800) i, (kchana(i,ll),ll=1,llt), (kchanb(i,ll),ll=1,llb)
    if (llt.eq.4)
      . write(9,810) i, (kchana(i,ll),ll=1,llt), (kchanb(i,ll),ll=1,llb)
    if (llt.eq.5)
      . write(9,820) i, (kchana(i,ll),ll=1,llt), (kchanb(i,ll),ll=1,llb)
    if (llt.eq.6)
      . write(9,830) i, (kchana(i,ll),ll=1,llt), (kchanb(i,ll),ll=1,llb)
    do 310 ll=1,llt
310 iwide=max0(iwide,kchana(i,llt)-i,1)
320 continue
330 continue
    write(9,780) nntot
cc*** group 7
cc***
    do 333 i=1,nc
333 nlll(i)=0
    if (ncd.le.0) go to 350
    ig1=7
    jc1=1
    write(9,840) ig1,ncd
    do 340 j=1,ncd
      i=izdum(j)
      if(ltop(i).le.1) go to 339
      jzdum(j)=1
      nlll(i)=nlll(i)+1
      nll=nlll(i)
      izdum(j)=kchana(i,nll)
339 continue
    write(9,850) cdl(j),jzdum(j),izdum(j)
340 continue
350 continue
cc*** group 8
cc***
    ig1=8
    jc1=1
    jc0=0
    write(9,860) ig1,jc0,nrtot,jc1,jc1
    write(9,865) humax,humin
    do 360 i=1,nrtot
      j=ir(i)
      write(9,870) i,i,hperimi(j),rmuls(j)

```

```

360 continue
cc*** card 8.4 and 8.5
    ig=1
    igt=0
    ig2=2
    write(9,880) ig,igt,nrtot,ig2
    write(9,890) (i,i=1,nrtot)
cc*** card 8.6
    gig=0.
    write(9,900) gig,tatm,htotal,tatm
cc*** group9
cc***
    ig=9
    ig4=4
    write(9,910) ig,nrtot,nwhctf
    iwalls=1
    do 370 j=1,nrtot
    i=ir(j)
    iwall=1
    t1=amin1(.1,.1*din(i)*12.)/12.
    t2=amin1(.5,.2*din(i)*12.)/12.
    t3=(din(i)-t1-t2)/3.
    t4=din(i) -t1-t2-t3
    if(i r(j).gt.nctot) iwall=2
    if(iwall .eq.2) iwalls=2
    write(9,920) j,hperimi(i),din(i),ig4,iwall
    ig5=5
    * write(9,930) ig5,iwall,t1,ig5,iwall,t2,ig5,iwall,t3,ig5,iwall,
      t4
370 continue
cc*** group 10
cc***
cc*** default concrete for type 1 and steel for type 2
    ig=10
    ig2=2
    write(9,940) ig,iwalls
    rc=139.
    rs=487.
    cpc=.22
    cps=.113
    tkc=.867
    tks=30.
    tp1=50.
    tpm=1000.
    ig=1
    write(9,950) ig,ig2,rc
    write(9,960) tp1,cpc,tkc,tpm,cpc,tkc
    if (iwalls.eq.1) go to 380

```

```

        ig=2
        write (9,950)  ig,ig2,rs
        write (9,960)  tp1,cps,tk,tpm,cps,tk
380    continue
cc***  group 13
cc***
        ig=13
        nkbnd=0
        nfunct=npt
        ngbnd=0
        iconvb=0
        write (9,970)  ig,nbc,nkbnd,nfunct,ngbnd,iconvb,ncritc,ncritk
        if (nfunct.eq.0) go to 400
        write (9,660)  (npts(i) ,i=1,npt)
        do 390 l=1,nfunct
        np=npts(l)
        do 387 k=1,np
        call blankit
        call form(abscis(k,l),1)
        do 385 j=1,5
385    irdint(j,k)=ka(j)
387    continue
        write(9,980) ((irdint(j,k),j=1,5),ordint(k,l),k=1,np)
390    continue
400    continue
        do 470 j=1,nbound
        jump=0
        jbound=ibound(j)
        if (i spec(j) .eq. 1) pvalue(j) =amax1(pvalue(j) ,xvalue(j) )
        if (i spec(j) .eq. 1) xvalue(j) =pvalue(j)
        if (pvalue(j).eq.0..and.npfn(j).eq.0) pvalue(j)=xvalue(j)
        if (hvalue(j)+nhfn(j).ne.0.) go to 410
cc***  default boundry pressure and vol fract to that in c@
        hvalue(j) =hs
        g9=vfv
        g1=vfa
        ha=has
        vfl=vfls
        head=0.
        if(lcb(j).eq.1) head=rhom*htotal*1.25/144.
        jump=1
        xvalue(j) =patm+head
        pvalue(j) =patm+head
410    continue
        if(lcb(j).gt.1.and.ispec(j),eq.1) lcb(j)=lcb(j)+1
        write (9,990)  ibound(j),lcb(j),ispec(j),npfn(j),nhfn(j),pvalue(j)
        $,hvalue(j),xvalue(j)
        if (jump.eq.1) go to 460

```

```

h=hvalue(j)
if (nhfn(j) .ne.0.) h=ordint(1,nhfn(j))
hl=hf(xvalue(j))
hv=hg(xvalue(j))
x=(h-hl)/(hv-hl)
if (x) 420,420,430
420 t=t1(xvalue(j),h)
    alfa=.0001
    go to 450
430 if (x.ge.1.) go to 440
    t=t1(xvalue(j),h)
    alfa=x/(x+vol(xvalue(j),h)/vog(xvalue(j),h)*(1.-x))
    alfa=amin1(alfa,,9999)
    alfa=amax1(alfa,.0001)
    go to 450
440 t=tv(xvalue(j),h,fp)
    alfa=.9999
450 ha=126.66 + 0.24 * (t - 70.3)
    vfl=1.-alfa
cc* default vol fraction of air upstream of break to .0001
    g9=.9999
    g1=.0001
460 write (9,1020) ha,vfl,g9,g1
    write (9,1000)
470 continue
    do 475 i=1,nbound
        if (ispec(j).eq.4) then
            write (9,1010) asink(j)
        else if (ispec(j).eq.5) then
            if(dxsink(j).eq.0.) dxsink(j)=a(jbound)**.5
            write (9,1010) asink(j),ssink(j),dxsink(j)
        end if
475 continue

    ig3=3
    do 500 k=1,2
    do 490 i=1,nctot
        kb=0
        kt=0
        do 480 j=1,nbound
            if (i.ne.ibound(j)) go to 480
            if (ispec(j).ge.4) go to 480
            if(lcb(j).ge.2) kt=1
            if (lcb(j).eq.1) kb=1
480 continue
            if(kb.eq.0.and.k.eq.1.and.abot(i).le.0.) write(9,990) i,k,ig3
            if(k.eq.2.and.kt.eq.0.and.atop(i).le.0.) write(9,990)i,k,ig3
490 continue

```

```

500 continue
    if (ncritc.eq.0) go to 504
    do 503 j=1,ncritc
        write(9,950) (icrit(ii,j),ii=1,2)
503 continue
504 continue
    if (ncritk.eq.0) go to 507
    do 506 j=1,ncritk
        write(9,950) (kcrit(ii,j),ii=1,2)
506 continue
507 continue
cc**** group 14
cc****
    ig=14
    read(6,580) n1,nout1,nout4,ncgraf,mfiche
    if (n1.eq.0) n1=1
    write(9,1030) ig,n1,nout1,nout4,1
    if (nout1.eq.0) go to 510
    read(6,1040) (izdum(i),i=1,nout1)
    write(9,1040) (izdum(i),i=1,nout1)
510 if (nout4.eq.0) go to 520
    read(6,1040) (izdum(i),i=1,nout4)
    write(9,1040) (izdum(i),i=1,nout4)
520 write(9,1050)
    write(9,1070)
    ig2=-1
    write(9,1080) ncgraf,ig2
cc **** default time domain data
cc *** start of run
    dtmin=.0001
    dtmax=.001
    tend=.1
    rtwfp = 1.
    tmax=300.
    write(9,1090) dtmin,dtmax,tend,rtwfp,tmax
    edint=1.e6
    if(mfiche.gt.0) edint= 1.
    gfint=1.e6
    if(ncgraf .gt.0) gfint=1.
    dumpint=500.
    sedint=1.e6
    asbint=0.02
    write(9,1090) edint,gfint,dumpint,sedint
    write(9,1095) asbint
cc *** intermediate zone
    dtmin=.0001
    dtmax=.05
    tend=1.

```

```

rtwfp=1.
tmax=300.
write (9,1090) dtmin,dtmax,tend,rtwfp,tmax
edint=1.e6
if(mfiche.gt.0) edint= 1.
gfint=1.e6
if(ncgraf .gt.0) gfint=.1
dumpint=500.
asbint=0.1
write (9,1090) edint,gfint,dumpint,sedint
write (9,1095) asbint
cc **** duration of run
dtmin=.0001
dtmax=1.0
*
tend=amin1(tottrn, 100.0)
rtwfp = 1.
tmax=300.
write (9,1090) dtmin,dtmax,tend,rtwfp,tmax
edint=1.e6
if(mfiche.gt.0) edint= 1.
gfint=1.e6
if(ncgraf .gt.0) gfint=.1.
dumpint=500.
asbint=1.0
write (9,1090) edint,gfint,dumpint,sedint
write (9,1095) asbint
tend=tottrn
asbint=10.0
write (9,1090) dtmin,dtmax,tend,rtwfp,tmax
write (9,1090) edint,gfint,dumpint,sedint
write (9,1095) asbint
dtmin=-1.
write (9,1090) dtmin
if (warning.gt.0.) write (9,1100) (jwarn (i,j)=1,nwarn)
530 format (i10,3f10.3)
533 format(i 10,f10.5,2i10)
540 format (2i10,f10.3)
550 format (17a4)
560 format (8f10.2)
570 format (i5,2f5.0,6(i5,f5.0))
580 format (8i10)
590 format (2i10,4f10.0)
600 format (5(f5.0,f10.0))
610 format (28x,i14,8x,26hset units and linear conv.)
620 format (i 14,e14.6,40x,12hrestart data)
630 format (e14.6,2i14,20x,18hiteration control)
640 format (5x,i5,17a4)

```

655 format (4f10.2)
650 format (2i5,30x,i5,24x,1lhvessel 1.1)
660 format (8i5)
670 format (2f10.3,20x,1f10.3,2f10.7)
680 format (8hair ,f10.7)
690 format (3i5,54x,1lhvessel 2.1)
700 format (i5,20a1)
710 format (i5,30x,2i5)
720 format (2i5,59x,1lhvessel 3.1)
730 format (3i5,2f5.0,2f5.2)
731 format (3i5,20a1)
740 format (f5.0)
750 format (69x,11h blank 3.4)
760 format (3i5,54x,1lhvessel 4.1)
770 format (3i5,f10.2)
780 format (2i5,25x,6i5)
790 format (3i5,20x,6i5)
800 format (4i5,15x,6i5)
810 format (5i5,10x,6i5)
820 format (6i5,5x,6i5)
830 format (13i5)
840 format (2i5,59x,1lhvessel 7.1)
850 format (f5.1,13i5)
860 format (5i5,44x,1lhvessel 8.1)
865 format (2f10.2)
870 format (2i5,10x,2f10.1)
880 format (4i5,49x,1lhvessel 8.4)
*/fix error in assigning wall desegnators
890 format (12i5)
900 format (4f10.1)
910 format (2i5,15x,i5,39x,1lhvessel 9.1)
920 format (i5,5h wall,f10.0,f10.2,i5,i10)
930 format (2(2i5,f5.3,5x),2(2i5,f5.2,5x))
940 format (2i5,59x,1lhvessel 10.1)
950 format (2i5,f10.2)
960 format (6f10.3)
970 format (8i5,29x,1lhvessel 13.1)
980 format (5(5a1,f10.2))
990 format (5i5,3f10.3)
1000 format (69x,11hblank 13.4b)
1010 format (8f5.1)
1020 format (f5.1,3f5.4)
1030 format (3i5,10x,i5,10x,i5,24x,1lhvessel 14.1)
1040 format (12i5)
1050 format (71x,9hend set 1)
1060 format (70x,10hblank 15.1)
1070 format (68x,12hblank graf. 1)
1080 format (2i5,59x,10h graf.2)

```

1090 format (5f14.6)
1095 format (f14.6)
1100 format (40h **** too many boundaries in cells *** ,30i3)
end

```

```

function hg (p)
dimension ag(3,12)
cc constants for saturated vapor enthalpy equations
data ag/ +.1105836875e+4, -.2234264997e+7, +.9059978254e+3,
1 +.1436943768e+2, +.1231247634e+7, +.5561957539e+1,
2 +.8018288621e+0, -.1978847871e+6, +.3434189609e+1,
3 +.1617232913e-1, +.1859988044e+2, -.6406390628e+0,
4 -.1501147505e-2, -.2765701318e+1, +.5918579484e-1,
5 0., +.1036033878e+4, -.2725378570e-2,
6 0., -.2143423131e+3, +.5006336938e-4,
7 0., +.1690507762e+2, 0.,
8 0., -.4864322134e+0, 0.,
9 -.1237675562e-4, 0., 0.,
1 +.3004773304e-5, 0., 0.,
2 -.2062390734e-6, 0., 0./

```

```

cc p = psi
cc hg=btu/lbm
l=1
ls=12
x=a*log(p)
if (p.le.950.) go to 10
l=2
ls=9
if (p.le.2650.) go to 10
l=3
ls=7
x=(3208.2-p)**.41
10 continue
lsm=ls-1
hg=ag(l,ls)
do 20 n=1,lsm
20 hg=hg*x+ag(l,ls-n)
return
end

```

```

function hf (p)
dimension af(3,9)
cc constants for saturated liquid enthalpy (revised eq@
data af/ +.6970887859e+2, +.8408618802e+6, +.9060030436e+3,
1 +.3337529994e+2, +.3637413208e+6, -.1426813520e+2,
2 +.2318240735e+1, -.4634506669e+6, +.1522233257e+1,

```



```

3          +.1840599513e+0, +.1130306339e+6, -.6973992961e+0,
4          -.5245502284e-2, -.4350217298e+3, +.1743091663e+0,
5          +.2878007027e-2, -.3898988188e+4, -.2319717696e-1,
6          +.1753652324e-2, +.6697399434e+3, +.1694019149e-2,
7          -.4334859629e-3, -.4730726377e+2, -.6454771710e-4,
8          +.3325699282e-4, +.1265125057e+1, +.1003003098e-5/
cc      p(psi), hf(btu/lbm)
        ls=9
        k=1
        x=log(p)
        if (p.lt.950) go to 10
        k=2
        if (p.lt.2550.) go to 10
        k=3
        x=(3208.2-p) **.41
10      lsm=ls-1
        hf=af(k, ls)
        do 20 n=1, lsm
20      hf=hf*x+af(k, ls-n)
        return
        end

        function tl (p,h)
        dimension al(2,4), ac(5,5)
cc      constants for liquid temperature equation
        data al/ +.3276275552e+2, +.3360880214e-2, +.9763617000e+0,
1          -.5595281760e-4, +.1857226027e-3, +.1618595991e-6,
2          -.4682674330e-6, -.1180204381e-9/
cc      above critical pressure
        data ac/ +.6390801208e+3, -.4302857237e+0, +.1174524584e-3,
1          -.1473977290e-7, +.7104327342e-12, -.3055217235e+1,
2          +.2673303422e-2, -.6839200986e-6, +.8018858166e-10,
3          -.3649500626e-14, +.8713231868e-2, -.5198380474e-5,
4          +.1168011772e-8, -.1164901355e-12, +.4457387575e-17,
5          -.6269403683e-5, +.3037825558e-8, -.4260074181e-12,
6          +.4559400289e-17, +.1678398723e-20, -.9844700000e-17,
7          +.3309704045e-12, -.2732081763e-15, +.5825511142e-19,
8          -.37568004091e-23/
        if (p.gt.3208.2) go to 20
        tl=al(1,4)+p*al(2,4)
        do 10 j=1,3
            k=4-j
10      tl=tl*h+al(1,k)+p*al(2,k)
        return
20      tl=poly5(ac,p,h)
        return
        end

```

```

function tv(p,h,cpi)
dimension a1(6),a2(6),b1(6),b2(6)
dimension a11(4),a22(4),b11(4),b22(4)
data a1/2.0110905e1,-1.250954e-2,2.8274992e-6,-9.8147341e-3,
+ 6.582489e-6,-1.4749938e-9/
data a2/15.35885,-1.5655537e-2,5.2687849e-6,-1.1541553e-3,
+ 1.238456e-6,-4.1724604e-10/
data b1/1.325023e-2,-1.0521514e-5,2.5007955e-9,5.7703098e-3,
+ -2.9972073e-6,5.20373e-10/
data b2/-2.5611614e-1,2.2270593e-4,-5.9928922e-8,2.796637e-2,
+ -2.4665012e-5,6.772308e-9/
data a11/-1.0659659e4,4.981582,-7.7618225e-6,2.4391612e-10/
data a22/-4.5298646e3,4.4185386e-1,-9.1654905e-6,2.7549766e-10/
data b11/-2.8557816,-3.4620214,-3.6261637e-2,7.3529479e-4/
data b22/126.5996,-21.81803,1.3424036,-4.9110372e-2/
h2 = h*h
h3 = h2*h
plog = alog(p)
tgaspl = a11(1)+p*(a11(2)+p*(a11(3)+p*a11(4)))
tgaspl = a22(1)+p*(a22(2) +p*(a22(3) +p*a22(4) ))
cpgas1 = b11(1)+plog*(b11(2)+plog*(b11(3)+plog*b11(4)))
cpgas2 = b22(1)+plog*(b22(2) +plog*(b22(3) +plog*b22(4) ))
patm = p/14.6959
patm2 = patm*patm
patm4 = patm2*patm2
if (p.gt.1000..and.h.lt.1280.) go to 5
t = tgaspl+a1(1)*h+a1(2)*h2+a1(3)*h3+p*(a1(4) *h+a1(5)*h2+a1(6)*h3)
cpi = cpgas1+b1(1)*h+b1(2)*h2+b1(3)*h3+plog*(b1(4) *h+b1(5)*h2+
+ b1(6)*h3)
c = 1.0/cpi
go to 10
5 t = tgaspl+a2(1)*h+a2(2) *h2+a2(3) *h3+p*(a2(4) *h+a2(5) *h2+a2(6) *h3)
cpi = cpgas2+b2(1)*h+b2(2) *h2+b2(3) *h3+plog*(b2(4) *h+b2(5) *h2+
+ b2(6)*h3)
c = 1.0/cpi
10 continue
c
c start iteration loop
c
do 20 n=1,10
if(t.ge.-459.6) go to 13
write(9,12) p,h
12 format(/3x,"tgas failed -- negative temperature"/18x,
. "pressure =",e15.6," enthalpy =",e15.6)
call exit
13 told = t
tdc = (t-32.)/1.8

```

```

tdk = tdc + 273.16
tml = 1./tdk
tm2 = tml*tml
tm3 = tml**3
tm5 = tml**5
tm6 = tml**6
tm23 = tml**23
tm24 = tm23*tml
ex = 80870.*tm2
bo = 1.89-2641.62*tml*10.**ex
bt = bo*tml
bt2 = bt*bt
bt3 = bt2*bt
bt4 = bt3 * bt
bt12=bt4*bt4*bt4
bt13=bt12*bt
g1=82.546*tml-1.6246*tm2*1.0e+5
g2 = .21828-1.2697e5*tm2
g3=3.635e-4*(1.1613e16*tm6)**4
dg1dt=82.546-1.6246e5*2.*tml
dg2dt=-2.*1.2697e5*tml
dg3dt=-24.0*(1.1613e16*tm5)**4*tm3
dbtdt=1.89-2.*2641.62*10.**ex*(1.0+ex*log(10.))*tml
f1=2.*g1*bt*dbtdt+bt2*dg1dt
f3=4.*bt3*g2*dbtdt+bt4*dg2dt
f12 = -13.*bt12*g3*dbtdt-bt13*dg3dt
fp1=1.472*tdk
fp2=7.5566e-4/2.*tdk**2.
fp3=47.8365*log(tdk)
fp=fp1+fp2+fp3+1803.68
hp1=patm*dbtdt
hp2=f1*patm2/2.
hp3=f3*patm4/4.
patm13=patm ** 13
hp4 = f12*patm13/13.0
hh = (hp1+hp2+hp3+hp4)*.101295+fp
hh = 0.43*hh
if (abs(hh-h) .lt. 0.5) go to 30
c
c adjust temperature
c
t = told + (h-hh)/c
t = 0.2*told+0.8*t
if (abs(t-told) .lt.1.0) go to 30
20 continue
30 continue
tv=amax1(35.,t)
return

```

```

function poly5 (a,p,h)
dimension a(5,5)
f=a(1,5)+p*(a(2,5)+p*(a(3,5)+p*(a(4,5)+p*a(5,5))))
do 10 j=1,4
k=5-j
10 f=f*h+a(1,k)+p*(a(2,k)+p*(a(3,k)+p*(a(4,k)+p*a(5,k))))
poly5=f
return
end

```

```

function vol (p, h)
dimension c(3,5)
cc constants for liquid specific volume equation
data c/ -.4117961750e+1, -.4816067020e-5, -.1820625039e-8,
1 -.3811294543e-3, +.7744786733e-7, +.1440785930e-10,
2 +.4308265942e-5, -.6988467605e-9, -.2082170753e-13,
3 -.9160120130e-8, +.1916720525e-11, -.3603625114e-16,
4 +.8017924673e-11, -.1760288590e-14, +.7407124321e-19/
f=c(1,5)+p*(c(2,5)+c(3,5)*p)
do 10 j=2,4
k=5-j
10 f=f*h+c(1,k)+p*(c(2,k)+c(3,k)*p)
vol=exp(f)
return
end

```

```

function vog (p,h)
dimension c(4,3)
cc constants for vapor specific volume equation
data c/ -.1403086182e+4, +.3817195017e+0, -.6449501159e-4,
1 +.7823817858e-8, +.1802594763e+1, -.5394444747e-3,
2 +.8437637660e-7, -.1053834646e-10, -.2097979215e-3,
3 +.1855203702e-6, -.2713755001e-10, +.3629590764e-14/
f=c(1,3)/p+c(2,3)+p*(c(3,3)+c(4,3)*p)
do 10 k=1,2
10 f=f*h+c(1,k)/p+c(2,k)+p*(c(3,k)+c(4,k)*p)
vog=f
return
end

```

```

subroutine form (a,ns)
common /forms/ ka(80)
dimension num(15),j(5)

```

```

data num /1h0,1h1,1h2,1h3,1h4,1h5,1h6,1h7,1h8,1h9,1h.,1he,1h-,1h*,
1 lh /
nset=ns-1
b=a
if.(b.eq.0.) return
if (a.lt.0.0001) go to 60
if (a.gt.9999.) go to 110
ccc come here for non-exponential format.
if (a.ge.1.) go to 10
id=1
go to 30
10 id=2
do 20 k=1,11
b=b/10.
if (b.lt.1.) go to 30
id=id+1
20 continue
30 b=a*10.**(5-id)+.5
do 40 i=1,4
j(i)=ifix(b/10**(4-i))+1
b=b-(j(i)-1)*10**(4-i)
40 continue
do 50 l=1,4
iadd=0
if (l.ge.id) iadd=1
i=j(l)
ka(1+iadd+nset)=num(i)
50 continue
ka(i d+nset)=num(11)
go to 140
ccc come here for negative exponential format.
60 nexp=ifix(alog10(a))-1
front=a/10.**nexp
if (front.lt.10.) go to 70
nexp=nexp+1
front=1.0
70 continue
if (nexp.ge.-9) go to 90
ccc set field to *'s if >=1e-10
do 80 l=1,5
80 ka(1+nset)=num(14)
go to 140
90 iz=ifix(front+.5)
if (iz.le.9) go to 100
iz=1
nexp=nexp+1
100 ka(1+nset)=num(iz+1)
ka(2+nset)=num(11)

```

```

ka(3+nset)=num(12)
ka(4+nset)=num(13)
ka(5+nset)=num(abs(nexp) +1)
go to 140
ccc come here for positive exponential format.
110 nexp=ifix(a*log10(a))
front=a/(1.*10.**nexp-1)
iz2=ifix((front-ifix(front))*10+.5)
if (iz2.le.9) go to 120
iz2=0
front=front+.5
120 iz1=ifix(front+.5)
if (iz1.le.9) go to 130
iz1=1
nexp=nexp+1
130 ka(1+nset)=num(iz1+1)
ka(2+nset)=num(11)
ka(3+nset)=num(iz2+1)
ka(4+nset)=num(12)
ka(5+nset)=num(nexp+1)
if (nexp.le.9) go to 140
ka(3+nset)=num(12)
ka(4+nset)=num(nexp/10+1)
ka(5+nset)=num(nexp-(nexp/10)*10+1)
140 continue
return
entry blankit
do 150 i=1,80
150 ka(i)=num(15)
return
end

```

APPENDIX B

COBRA-NC MODIFICATION CARD LISTING

APPENDIX B
COBRA-NC MODIFICATION CARD LISTING

```
1 *id asb
2 */
3 */ start asb updates
4 */ use feet and not inches as geometry input
5 *i input.9
6 common/unite/ enguni
7 *d upd13.723
8 read(in, 10050) icobra,iapenk,inguni
9 enguni=float(i nguni)
10 if(enguni.le.0.) enguni=1.
11 *i setin.38
12 common/unite/ enguni
13 *d setin.41
14 data feets,sqfts,btu /12.,144.,3412./
15 *i setin.43
16 feet=feets/enguni
17 sqft=sqfts/enguni**2
18 *d setin.51
19 read(i2,10000)ngroup,n1,n2,n3,n4,n5,n6,n7,n8
20 *d setin.53
21 write(i3,10000)ngroup,n1,n2,n3,n4,n5,n6,n7,n8
22 */ adds multiplier on wall heat transfer correlation
23 */ whtcf and nwhtcf must be added to comdeck xtradat
24 *i prep3d.373
25 c
26 c find time varying multiplier on wall heat transfer coefficient.
27 if(nwhtcf .gt.0) call curvel(whtcf,etime,nwhtcf)
28 *i setin.797
29 nwhtcf=n5
30 whtcf=1.
31 */
32 */ these changes add the critical flow model to xschem
33 */ mcrit, ncritc, and ncritk must be added to comdeck xtradat
34 *i setin.63
35 mcrit=n8
36 */ add input of locations to check for critical flow
37 */ add icrit and kcrit to common snkdat
38 *i setin.1417
39 ncritc=n5
40 ncritk=n6
41 *d setin.1503
```

```

42     if(ngbnd.lt.1) go to 1377
43 *i setin.1526
44 1377 if(ncritc.lt.1) go to 1395
45     do 1380 l=1,ncritc
46     read (12,10130) (icri t(n, l),n=1,2)
47     icrit(3,l)=0.0
48     msk=0
49     do 1379 n=1,nibnd
50     ifi spec(n) .ne.5) go to 1379
51     msk=msk+l
52     if(ibound(1,n).ne.icrit(1,l)) go to 1379
53     if(ibound(2,n).ne.icrit(2,l)) go to 1379
54     icrit(3,l)=msk
55     go to 1380
56 1379 continue
57 1380 continue
58     if(ncri tc.le.mudim) go to 1395
59     write(i3,20251) ncritc,mudim
60 20251 format(10x,"in card group 13, ncritc exceeds allowed dimensions"/
61     1 10x,"ncritc="i5," mu="i5//)
62     istop=1
63 1395 if(ncri tk.lt.1) go to 1397
64     do 1396 l=1,ncritk
65 1396 read (i 2,10130) (kcri t(n, l),n=1,2)
66     if(ncritk.le.mudim) go to 1397
67     write(i3,20252) ncritk,mudim
68 20252 format(10x,"in card group 13, ncritk exceeds allowed dimensions"/
69     1 10x,"ncritk="i5," mu="i5//)
70     istop=1
71 1397 continue
72 *i prep3d.36
73 c
74 c     re initialize iaspec when critical flow model used
75     if(mcrit.eq.0) go to 3
76     do 2 ic=1,nchanl
77     i=idchar(i c)
78     isec=lchar(i)
79     jnodes=isect$ i sec,1)+2
80     do 2 j=1,jnodes
81     iaspec(i,j) =10
82     2 continue
83     3 continue
84 *i xschem.1258
85 c     check for critical flow calculation
86 c
87     if(mcri t) 1824,1824,1801
88 1801 msk=0
89     if(ncri tc) 1817,1817,1802

```

```

90 1802 do 1815 l=1,ncritc
91     i=icrit(1,l)
92     j=icrit(2,l)
93     isp=iaspec(i,j)
94     if((isp-10)*(isp-1)) 1809,1803,1809
95 1803 sumf = fem(i,j) + fgm(i,j) + flm(i,j)
96     jstar = j
97     if(sumf) 1806,1815,1807
98 1806 jstar=jp1
99 1807 rll=rl(i,jstar)
100     alrlst = aliq(i,jstar)*rll
101     alrv=0.5*(al(i,j)*(rv(i,j)+rmgas(i,j))+al(i,jp1)*(rv(i,jp1)+rmgas
102     1(i,jp1)))
103     alrl=0.5*(aliq(i,j)*rll( i,j)+aliq(i,jp1)*rll(i,jp1))
104     aerl=0.5*(ae(i,j)*rll(i,j)+ae(i,jp1)*rll(i,jp1))
105     flc=flm(i,j)*alrlst/alrl
106     aerlst=ae(i,jstar)*rll
107     fec=fem(i,j)*aerlst/aerl
108     rvapm=(rv(i,jstar)+rmgas(i,jstar))
109     agrgst=al(i,jstar)*rvapm
110     fgc=fgm(i,j)*agrgst/avr
111     sumf=fgc+fec+flc
112     c1=alrlst+aerlst
113     hvgas=rv(i,jstar)*hv(i,jstar)+rmgas(i,jstar)*hmgas(i,jstar)
114     sumh=(c1*hl(i,jstar)+al( i,jstar)*hvgas)/(c1+agrgst)
115     call gcritf(p(i,jstar)*ri144+pref,sumh,mcrit,gcrit,s,
116     rvapm,rll)
117     fcrit = gcrit*amom(i,j)
118     if(fcrit .gt. sumf) go to 1815
119     sumf =fcrit/(c1+s*agrgst)*sign(1.,sumf)
120     fem(i,j) = sumf*aerl
121     fgm(i,j) = sumf*avr*s
122     flm(i,j) = sumf*alrl
123     dfemdp(i,j) = 0.
124     dfgmdp(i,j) = 0.
125     dflmdp(i,j) = 0.
126 c   treat as forced flow boundry
127     iaspec(i,j)=2
128     go to 1815
129 1809 if(isp-5) 1815,1810,1815
130 1810 msk=icrit(3,l)
131 1811 sumw = wesink(msk) + wgsink(msk)+wlsink(msk)
132     if(sumw) 1812,1815,1813
133 1812 pstar = p(i,j)*ri144 + pref
134     c1 = rl(i,jp1)*(aliq(i,jp1)+ae(i,jp1))
135     c2 = (rv(i,jp1) + rmgas(i,jp1))*al(i,jp1)
136     rll=rl(i,jp1)
137     rvv= rv(i,jp1)+rmgas(i,jp1)

```

```

138     sumh = (c1*h1(i ,jp1) +(rv(i,jp1)*hv(i,jp1)+
139 $rmgas(i,jp1)*hmgas(i,jp1))*asink(msk))/(c1+c2)
140     go to 1814
141 1813 c1 = rlsink(msk)*(aliqs(msk) + aesink(msk))
142     c2 = (rvsink(msk) + rmgsink(msk)) * alsink(msk)
143     rll=rlsink(msk)
144     rvv=rvsink(msk)+rmgsink(msk)
145     sumh = (c1*hlsink(msk)+alsink(msk)*(rmgsink(msk)
146 $*hgsink(msk)+rvsink(msk)*hvsink(msk)))/(c1+c2)
147     pstar = psink(msk)*ri144 + pref
148 1814 call gcritf(pstar, sumh,mcrit,gcrit,s,rvv,rll)
149     fcrit = gcrit * asink(msk)*sign(1.,sumw)
150     sumf = abs(sumw)
151     if (fcrit .gt. sumf) go to 1815
152     sumf = fcrit/(c1+c2*s)*sign(1., sumw)
153 c     assume alfal = alfae
154     wesink(msk) =sumf*.5*c1
155     wgsink(msk) =sumf*s*c2
156     wlsink(msk) =sumf*.5*c1
157     dwesink(msk) = 0.
158     dwgsink(ms k)=0.
159     dwlsink(msk)=0.
160 1815 continue
161 c
162 c check for gap critical flow
163 1817 if(ncritk) 1824,1824,1818
164 1818 do 1823 l=1,ncritk
165     k=kcrit(1,l)
166     j=kcrit(2,l)
167     ii=ik(k)
168     jj=jk(k)
169     sumw = wem(k,j) + wgm(k,j)+wlm(k,j)
170     istar = ii
171     if(sumw) 1821,1823,1822
172 1821 istar=jj
173 1822 rll=rll(istar,j)
174     alrls=aliq(istar,j)*rll
175     alrlisx=alrl/sdx
176     aerls=aliq(istar,j)*rll
177     alerisx=alre/sdx
178     alrvs=al(istar,j)*(rv(istar,j)+rmgas(istar,j))
179     alrvsdx=alrv/sdx
180     wlc=wlm(k,j)*alrls/alrlisx
181     wec=wem(k,j)*aerls/alreix
182     wgc=wgm(k,j)*alrvs/alrvsdx
183     rvapm=rv(istar,j)+rmgas(istar,j)
184     sumf=wlc+wec+wgc
185     c1=aerls+alrls

```

```

186     hvgas=rv(istar,j)*hv(istar,j)+rmgas(istar,j)*hmgas(istar,j)
187     sumh=(c1*hl(istar,j)+al(istar,j)*hvgas)/(c1+alrvs)
188     call gcritf(p(i,j)*ri144+pref,sumh,mcrit,gcrit,s,rvamp,rll)
189     wcrit = gcrit*sdx
190     if(wcrit .gt. abs(sumf)) go to 1823
191     sumw = wcrit/(c1+s*alrvs)*sign(1., sumf)
192     wem(k,j) = sumw*alreix
193     wgm(k,j) = sumw*s*alrvix
194     wlm(k,j) = sumw*alrlisx
195     dwemdp(k,j) = 0.
196     dwgmdp(k,j) = 0.
197     dwlmdp(k,j) = 0.
198 1823 continue
199 1824 continue
200 *d xschem.2069
201     if(dwgmdp(k,j).eq.0.) go to 3655
202 *i xschem.2083
203     go to 3670
204 3655 dumgx=1.
205     dumvx=1.
206     dumlx=1.
207     dumex=1.
208 3670 continue
209 */ add critical flow tables to common
210 *i cobratf.25
211     common /leakc / g01(735) ,ng,np1
212     common /leakhe / pe01(368),nhhe,nphe
213     common / leakh / pm(1062),nhh,nph
214 *i blkdat.448
215     call datm
216     call datz
217     call dath
218 */ the following make changes to cobra-nc
219 */ specifically for asb by changing the way in which
220 */ the output is formatted.
221 *d cobratf.4
222     $      tape10,tape59,fiche,tape4=fiche)
223 *i cobratf.11
224 *call ocommn
225     common /outasb/ asbint,iedit,asbedit
226 *i edit.7
227     common /outasb/ asbint,iedit,asbedit
228 *i setin.38
229     common /outasb/ asbint,iedit,asbedit
230 *i setin.1538
231     asbint = float(n8)
232 *i trans.15
233     common /outasb/ asbint,iedit,asbedit

```

```

234 *i timstp.17
235     common /outasb/ asbint,iedit,asbedit
236 *i timstp.34
237     if(asbint.gt.0) read (in,402) asbint
238 *i timstp.56
239     if(asbint.le.0) go to 150
240     write(iout,3201) asbint
241     write(imout ,3201) asbint
242     write(itty,3201) asbint
243 3201 format(lx, " interval for a.s.b. output is ",f10.5," seconds.")
244 150 continue
245 *i timstp.67
246     asbedit=timet+asbint
247 *d trans.179
248     iedit=0
249     if(timet.lt.(tedit-eps)) go to 325
250     iedit =iedit+1
251 325 if(asbint.le.0) go to 328
252     if(timet.lt.(asbedit-eps)) go to 328
253     iedit=iedit+2
254 328 if(iedit.eq.0) go to 330
255 *i trans.205
256     iedit=1
257     if(asbint.gt.0,) iedit=2+iedit
258     idon=1
259 *i blkdat.2
260 *call ocommn
261 *b blkdat.420
262     data iprcnt/0/,idon/0/
263 *i edit.2
264 *call mcmx
265 *call spltdat
266 *call twophas
267 *call xtrdat
268 *call propmat
269 *call ocommn
270 *call mfrac
271 *call gasvar
272 *b edit.10
273     dimension ck(9)
274     data ck/ -7.691234564, -2.608023696e+1, -1.681706546e+2,
275             6.423285504e+1, -1.189646225e+2, 4.167117320,
276             ., 2.097506760e+1, 1.e9, 6./
277 *i edit.21
278 c   if asb output is required
279 c   i3 is set to 4 so that all the data from
280 c   subroutine result goes to lun 4. i3 will be set
281 c   back to 6 before returning.

```

```

282 c
283     if(asbint.gt.0.)   i3=4
284     if(iedit.eq.2) go to 60
285 *i edit.24
286     60 i3=6
287     if(iedit.eq.1) go to 100
288 c     setup asb output
289     asbedit=asbedit+asbint
290 c
291 c     store results in arrays until 50 entries
292 c     have been accumulated. if 50 entries have
293 c     been accumulated, call "prnter" to report
294 c     them.
295 c
296     istop=iprcnt
297     iprcnt=iprcnt + 1
298     if(iprcnt.gt.50) call prnter(istop)
299     if(iprcnt.gt.50) iprcnt=1
300     strtim(iprcnt)=etime
301 c
302     if(nout1.le.0) go to 90
303 c
304     iknt=0
305 c
306     do 85 indx=1,nout1
307     i=prntc(indx)
308     jnode=isects(lchan(i),1) + 1
309     iknt=iknt + 1
310 c
311 c     store pressure
312 c
313     storep(iknt,iprcnt)=P(i,jnode) / 144.0 + pref
314 c
315 c     store liquid fraction
316 c
317     storali(iknt,iprcnt)=aliq(i,jnode )
318 c
319 c     store temperature
320 c
321     rhomix=rmgas(i,jnode)+rv(i,jnode)
322     vap=rv(i,jnode)/rhomix
323     sum=vap/18.105
324     do 65 nga=1,ngas
325     frctnga=rgas(nga,i,jnode)/rhomix
326     sum=sum+frctnga/mw(nga)
327 65 continue
328     ppvap=vap/18.105/sum
329     pps=ppvap * (p(i,jnode) / 144.0 + pref)

```

```

330      ppss=pps
331      hvij=hv(i,jnode)
332      ssat=tv(pps, hvij)
333      theta=(ssat+459.67)/1.8/647.3
334      sums=0.
335      onemt=1.-theta
336      onemt2=onemt*onemt
337      pionemt=1.
338      do 70 i=1,5
339      pionemt=pionemt*onemt
340      sums=sums+ck(i)*pionemt
341 70 continue
342      sums=sums/theta
343      sums=sums/(1.+ck(6)*onemt+ck(7) *onemt2)
344      sums=sums-onemt/(ck(8) *onemt2+ck(9) )
345      beta=exp(sums)
346      pssat=beta*2984.907486
347 75 continue
348 c
349 80 continue
350 c
351      storet(i knt,iprcnt)=ssat
352 c
353 c store relative humidity
354 c
355      storrrh(i knt,iprcnt)=ppss/pssat
356 c
357 c
358 85 continue
359      if(idon.eq.1) call prntr(istop+1)
360 c
361 90 continue
362 *i error.5
363 *call ocommn
364 *i error.22
365      idon=1
366 *i trans.2
367 *call ocommn
368 c
369 *af ,momntd2
370 *comdeck ocommn
371 c
372 c this is common block is used to save containment
373 c data for printing later. the dimensions are:
374 c
375 c no. of rooms (max. to be printed) x 50
376 c
377      common/ocomn/ iprcnt,idon,storl(30 ,50) ,storep(30 ,50) ,

```



```

378      1   storet(30,50),storrh(30,50),strtim(50)
379 *af ,cwvssl
380 *deck prnter
381      subroutine prnter(istop)
382 c
383 *call xtradat
384 *call ocommn
385 c   this subroutine prints results
386 c   for the containment version of
387 c   cobra-tf
388 c
389 c   this is a much simpler routine than
390 c   "result".
391 c
392 c   only pressure, temperature, relative humidity,
393 c   and liquid fraction are reported. only one
394 c   node per "room" (channel) is reported as a function
395 c   of time.
396 c
397 c   first, pressure.
398 c
399      ibeg=0
400 c
401 100  continue
402 c
403      ibeg=ibeg + 1
404      if(ibeg.gt.nout1) go to 175
405      ifin=min0 (ibeg+9,nout1)
406 c
407      write(i3,10001) (printc(i),i=ibeg,ifin)
408 10001 format(1h1,59x,"pressure (psia)"/2x,"time",
409      1   10(4x,"room",i4)/2x,"(sec)"/)
410 c
411      do 150 ii=1,istop
412      write(i3,10002) strtim(ii),(storep(iknt,ii),iknt=ibeg,ifin)
413 10002 format(1x,f8.2,10(1x,lpell.4))
414 150  continue
415 c
416      ibeg=ifin
417      go to 100
418 c
419 175  continue
420 c
421      ibeg=0
422 c
423 200  continue
424 c
425      ibeg=ibeg + 1

```

```

426     ifi beg.gt.nout1) go to 275
427     ifin=min0(ibeg + 9,nout1)
428 c
429     write(i3,10003) (printc(i),i=ibeg,ifin)
430 10003 format(lh1, 53x,"temperature (degrees f.) "//2x,
431     1 "time",10(4x,"room",i4)/2x,"(sec)"/)
432 c
433     do 250 ii=1,istop
434     write(i3,10002) strtim(ii),(storet(iknt,ii),
435     1 iknt=ibeg,ifin)
436 250 continue
437 c
438     ibeg=ifin
439     go to 200
440 c
441 275 continue
442 c
443     ibeg=0
444 c
445 300 continue
446 c
447     ibeg=ibeg + 1
448     if(ibeg.gt.nout1) go to 375
449     ifin=min0(ibeg + 9,nout1)
450 c
451     write(i3,10004) (printc(i),i=ibeg,ifin)
452 10004 format(lh1,57x,"relative humidity"//2x,"time",
453     1 10(4x,"room",i4)/2x,"(sec)"/)
454 c
455     do 350 ii=1,istop
456     write(i3,10002) strtim(ii),(storrh(iknt,ii),
457     1 iknt=ibeg,ifin)
458 350 continue
459 c
460     ibeg=ifin
461     go to 300
462 c
463 375 continue
464 c
465     ibeg=0
466 c
467 400 continue
468 c
469     ibeg=ibeg + 1
470     ifi beg.gt.nout1) go to 475
471     ifin=min0i beg + 9,nout1)
472 c
473     write(i3,10005) (printc(i),i=ibeg,ifin)

```

```

474 10005 format(1h1,59x,"liquid fraction"//2x,"time",
475      1      10(4x,"room",i4)/2x,"(sec)"//)
476 c
477      do 450 ii=1,istop
478          write(i3,10006) strtim(ii),(storal (knt,ii),
479      1      iknt=ibeg,ifin)
480 10006 format(1x,f8.2,3x,f7.5,9(5x,f7.5))
481 450      continue
482 c
483          ibeg=ifin
484          go to 400
485 c
486 475      continue
487 c
488          return
489          end
490 *af ,tods
491 *deck tvofph
492      function tv(p,h)
493 c          p(psi),h(btu/lbm)
494          dimension av(5,5), ac(5,5)
495 c          constants for vapor temperature equation
496          data av/  -.1179100862e+5, +.1256160907e+3, -.1083713369e+0,
497      1          +.3278071846e-4, -.3425564927e-8, +.2829274345e+2,
498      2          -.3333448495e+0, +.2928177730e-3, -.8970959364e-7,
499      3          +.9527692453e-11,-.2678181564e-1,+ .3326901268e-3,
500      4          -.2972436458e-6, +.9246248312e-10,-.1001409043e-13,
501      5          +.1218742752e-4, -.1477890326e-6, +.1342639113e-9,
502      6          -.4249155515e-13,+ .4703914404e-17,-.2092033147e-8,
503      7          +.2463258371e-10,-.2275585718e-13,+ .7338316751e-17,
504      8          -.8315044742e-21/
505 c          above critical pressure
506          data ac/ +.3795256853e+4, -.3910086240e+1, +.3410500159e-4,
507      1          +.1527377542e-6, -.1437179752e-10,-.6347031007e+1,
508      2          +.1222747819e-1, +.7010900113e-9, -.5356866315e-9,
509      3          +.5006731336e-13,+ .2867228326e-2, -.1404664699e-4,
510      4          -.1030201866e-9,+ .96823225984e-12,-.6365519546e-16,
511      5          +.5953599813e-8, +.7505679464e-8, +.5731099333e-14,
512      6          -.3668096142e-15,+ .3473711350e-19,+ .4798207438e-10,
513      7          -.1608693653e-11,+ .3720795449e-16,+ .6946004624e-19,
514      8          -.6842306083e-23/
515          if(p.gt.3208.2) go to 100
516          tv=poly5(av,p,h)
517          return
518      100 tv=poly5(ac,p,h)
519          return
520          end
521          function poly5(a,p,h)

```

```

522     dimension  a(5,5)
523     f= a(1,5) +p*(a(2,5)+p*(a(3,5)+p*(a(4,5)+p*a(5,5))))
524     do 10 j=1,4
525         k=5-j
526     10 f= f*h +a(1,k)+p*(a(2,k) +p*(a(3,k)+p*(a(4,k)+p*a(5,k))))
527     poly5=f
528     return
529     end
530 *deck datm
531     subroutine datm
532 c
533     common / leakc / g01(35), g02(35), g03(35), g04(35), g05(35),
534     1     g06(35), g07(35), g08(35), g09(35), g10(35), g11(35),
535     2     g12(35), g13(35), g14(35), g15(35), g16(35), g17(35),
536     3     g18(35), g19(35), g20(35), g21(35), ng, npi
537 c
538 c     critical flow tables
539 c
540 c     gxx(1)      = stagnation pressure (psia)
541 c     gxx(even)  = maximum flow rate (lbm/ft**2-sec)
542 c     gxx(odd)   = stagnation enthalpy (btu/lb)
543 c
544 c     ng         = number of pairs of flow and enthalpy values per pressure
545 c     npi        = number of pressure values
546 c
547     data ng, npi / 17, 21 /
548 c
549     data g01 /      1.0e0, 214.71e0, 69.733e0, 20.11e0, 173.340e0,
550     1 10.95e0, 276.948e0, 7.54e0, 380.555e0, 5.76e0, 484.163e0,
551     2 4.65e0, 587.771e0, 3.91e0, 691.378e0, 3.37e0, 794.986e0,
552     3 2.96e0, 898.593e0, 2.64e0,1002.201e0, 2.38e0,1105.809e0,
553     4 2.50e0,1112.678e0, 2.00e0,1238.828e0, 1.80e0,1369.999e0,
554     5 1.60e0,1507.606e0, 1.40e0,1652.162e0, 1.30e0,1803.545e0/
555     data g02 /      5.0e0, 527.49e0, 130.196e0, 90.72e0, 230.286e0,
556     1 50.86e0, 330.376e0, 35.44e0, 430.465e0, 27.21e0, 530.555e0,
557     2 22.09e0, 630.645e0, 18.60e0, 730.734e0, 16.06e0, 830.824e0,
558     3 14.13e0, 930.913e0, 12.62e0,1031.003e0, 11.39e0,1131.093e0,
559     4 11.70e0,1142.565e0, 9.80e0,1264.479e0, 8.60e0,1390.263e0,
560     5 7.70e0,1521.800e0, 7.10e0,1659.584e0, 6.60e0,1803.492e0/
561     data g03 /     10.0e0, 767.75e0, 161.261e0, 171.18e0, 259.470e0,
562     1 97.76e0, 357.678e0, 68.64e0, 455.887e0, 52.93e0, 554.096e0,
563     2 43.09e0, 652.305e0, 36.34e0,750.513e0, 31.42e0, 848.722e0,
564     3 27.67e0, 946.931e0, 24.73e0,1045.140e0, 22.35e0,1143.348e0,
565     4 22.90e0,1157.466e0, 19.30e0,1277.542e0, 17.10e0,1400.619e0,
566     5 15.40e0,1529.045e0, 14.20e0,1663.351e0, 13.10e0,1803.425e0/
567     data g04 /     14.7e0, 943.01e0, 180.179e0, 242.34e0, 277.210e0,
568     1 140.17e0, 374.240e0, 98.93e0, 471.270e0, 76.51e0, 568.300e0,
569     2 62.40e0, 665.331e0, 52.69e0, 762.361e0, 45.60e0, 859.391e0,

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570      3  40.19e0, 956.421e0, 35.93e0, 1053.452e0, 32.49e0, 1150.482e0,
571      4  33.10e0, 1166.3770e0, 28.20e0, 1258.449e0, 24.90e0, 1406.903e0,
572      5  22.60e0, 1533.437e0, 20.80e0, 1665.624e0, 19.30e0, 1803.363e0/
573      data g05 / 50.0e0, 1787.76e0, 250.212e0, 706.24e0, 342.600e0,
574      1  432.14e0, 434.988e0, 312.25e0, 527.376e0, 244.68e0, 619.764e0,
575      2  201.24e0, 712.153e0, 170.93e0, 804.541e0, 148.58e0, 896.929e0,
576      3  131.40e0, 989.317e0, 117.79e0, 1081.705e0, 106.74e0, 1174.093e0,
577      4  107.50e0, 1196.581e0, 92.90e0, 1312.998e0, 83.20e0, 1428.913e0,
578      5  76.00e0, 1548.789e0, 70.40e0, 1673.458e0, 65.80e0, 1802.893e0/
579      data g06 / 100.0e0, 2546.50e0, 298.538e0, 1252.95e0, 387.401e0,
580      1  802.83e0, 476.264e0, 591.90e0, 565.127e0, 469.15e0, 653.989e0,
581      2  388.73e0, 742.852e0, 331.92e0, 831.715e0, 289.63e0, 920.578e0,
582      3  256.92e0, 1009.440e0, 230.86e0, 1098.303e0, 209.60e0, 1187.166e0,
583      4  209.20e0, 1214.890e0, 182.30e0, 1330.371e0, 164.50e0, 1442.897e0,
584      5  151.10e0, 1558.489e0, 140.30e0, 1678.248e0, 131.60e0, 1802.229e0/
585      data g07 / 200.0e0, 3608.16e0, 355.506e0, 2153.39e0, 439.789e0,
586      1  1463.65e0, 524.071e0, 1108.91e0, 608.354e0, 893.05e0, 692.637e0,
587      2  747.78e0, 776.920e0, 643.27e0, 861.202e0, 564.45e0, 945.485e0,
588      3  502.88e0, 1029.768e0, 453.44e0, 1114.051e0, 412.87e0, 1198.334e0,
589      4  407.00e0, 1234.101e0, 357.60e0, 1349.174e0, 325.00e0, 1458.103e0,
590      5  300.00e0, 1568.929e0, 279.90e0, 1683.135e0, 263.30e0, 1800.900e0/
591      data g08 / 400.0e0, 5084.55e0, 424.167e0, 3560.62e0, 502.210e0,
592      1  2601.91e0, 580.252e0, 2044.87e0, 658.294e0, 1683.97e0, 736.337e0,
593      2  1413.45e0, 814.379e0, 1244.89e0, 892.421e0, 1101.42e0, 970.464e0,
594      3  987.66e0, 1048.506e0, 895.23e0, 1126.548e0, 818.64e0, 1204.591e0,
595      4  792.40e0, 1253.154e0, 701.20e0, 1368.603e0, 641.80e0, 1473.887e0,
596      5  595.90e0, 1579.509e0, 558.50e0, 1687.509e0, 527.30e0, 1798.245e0/
597      data g09 / 600.0e0, 6192.24e0, 471.697e0, 4682.13e0, 544.893e0,
598      1  3588.84e0, 618.089e0, 2897.01e0, 691.285e0, 2426.85e0, 764.481e0,
599      2  2087.61e0, 837.677e0, 1831.53e0, 910.873e0, 1631.43e0, 984.069e0,
600      3  1470.77e0, 1057.265e0, 1338.95e0, 1130.461e0, 1228.83e0, 1203.657e0,
601      4  1172.40e0, 1262.896e0, 1040.80e0, 1379.241e0, 956.20e0, 1482.588e0,
602      5  890.60e0, 1585.098e0, 837.00e0, 1689.262e0, 792.00e0, 1795.591e0/
603      data g10 / 800.0e0, 7103.30e0, 509.811e0, 5630.54e0, 578.769e0,
604      1  4472.42e0, 647.726e0, 3689.49e0, 716.684e0, 3135.77e0, 785.641e0,
605      2  2725.47e0, 854.599e0, 2409.78e0, 923.557e0, 2159.53e0, 992.514e0,
606      3  1956.33e0, 1061.472e0, 1788.08e0, 1130.429e0, 1646.48e0, 1199.387e0,
607      4  1550.10e0, 1268.822e0, 1378.50e0, 1386.128e0, 1269.40e0, 1488.245e0,
608      5  1184.90e0, 1588.533e0, 1115.70e0, 1689.882e0, 1057.40e0, 1792.940e0/
609      data g11 / 1000.0e0, 7883.70e0, 542.551e0, 6458.25e0, 607.589e0,
610      1  5277.33e0, 672.628e0, 4434.96e0, 737.666e0, 3818.11e0, 802.705e0,
611      2  3349.91e0, 867.743e0, 2983.26e0, 932.782e0, 2688.66e0, 997.820e0,
612      3  2446.89e0, 1062.859e0, 2244.95e0, 1127.898e0, 2073.79e0, 1192.936e0,
613      4  1928.00e0, 1272.169e0, 1715.80e0, 1390.601e0, 1582.30e0, 1491.960e0,
614      5  1479.30e0, 1590.602e0, 1394.80e0, 1689.784e0, 1323.60e0, 1790.290e0/
615      data g12 / 1200.0e0, 8566.61e0, 571.853e0, 7194.59e0, 633.149e0,
616      1  6018.53e0, 694.445e0, 5141.21e0, 755.741e0, 4478.45e0, 817.037e0,
617      2  3964.05e0, 878.333e0, 3554.43e0, 939.629e0, 3221.01e0, 1000.925e0,

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618 3 2944.51e0,1062.221e0, 2711.61e0,1123.517e0, 2512.78e0,1184.813e0,
619 4 2306.00e0,1274.362e0, 2052.90e0,1393.811e0, 1895.20e0,1494.624e0,
620 5 1773.90e0,1591.920e0, 1674.40e0,1689.289e0, 1590.60e0,1787.642e0/
621 data g13 / 1400.0e0, 9171.02e0, 598.830e0, 7857.52e0, 656.477e0,
622 1 6705.77e0, 714.125e0, 5813.30e0, 771.773e0, 5119.72e0, 829.420e0,
623 2 4569.95e0, 887.068e0, 4125.04e0, 944.716e0, 3758.28e0,1002.364e0,
624 3 3450.98e0,1060.011e0, 3189.90e0,1117.659e0, 2965.42e0,1175.307e0,
625 4 2684.80e0,1275.682e0, 2390.20e0,1396.083e0, 2208.30e0,1496.504e0,
626 5 2068.80e0,1592.681e0, 1954.50e0,1688.499e0, 1858.30e0,1784.994e0/
627 data g14 / 1600.0e0, 9708.52e0, 624.202e0, 8458.62e0, 678.235e0,
628 1 7345.72e0, 732.268e0, 6454.71e0, 786.300e0, 5743.98e0, 840.333e0,
629 2 5169.19e0, 894.366e0, 4696.66e0, 948.399e0, 4302.13e0,1002.431e0,
630 3 3968.12e0,1056.464e0, 3681.89e0,1110.497e0, 3433.97e0,1164.530e0,
631 4 3067.10e0,1275.712e0, 2729.00e0,1397.285e0, 2522.30e0,1497.542e0,
632 5 2364.50e0,1592.855e0, 2235.40e0,1687.403e0, 2126.80e0,1782.347e0/
633 data g15 / 1800.0e0,10186.24e0, 648.490e0, 9005.71e0, 698.875e0,
634 1 7943.45e0, 749.258e0, 7068.47e0, 799.642e0, 6353.40e0, 850.027e0,
635 2 5763.77e0, 900.411e0, 5271.40e0, 950.795e0, 4855.02e0,1001.179e0,
636 3 4498.77e0,1051.564e0, 4190.73e0,1101.948e0, 3921.87e0,1152.332e0,
637 4 3448.60e0,1275.998e0, 3067.70e0,1398.372e0, 2836.40e0,1498.413e0,
638 5 2660.50e0,1592.891e0, 2516.90e0,1686.228e0, 2396.00e0,1779.701e0/
639 data g16 / 2000.0e0,10608.22e0, 672.111e0, 9504.17e0, 718.734e0,
640 1 8503.14e0, 765.356e0, 7657.68e0, 811.979e0, 6950.77e0, 858.601e0,
641 2 6356.68e0, 905.224e0, 5852.74e0, 951.846e0, 5420.97e0, 998.468e0,
642 3 5047.45e0,1045.091e0, 4721.42e0,1091.713e0, 4434.55e0,1138.336e0,
643 4 3833.80e0,1257.411e0, 3408.30e0,1398.751e0, 3151.70e0,1498.725e0,
644 5 2957.50e0,1592.538e0, 2799.20e0,1684.851e0, 2666.10e0,1777.056e0/
645 data g17 / 2200.0e0,10975.67e0, 695.462e0, 9956.80e0, 738.132e0,
646 1 9027.41e0, 780.802e0, 8224.65e0, 823.471e0, 7538.67e0, 866.141e0,
647 2 6951.18e0, 908.811e0, 6444.80e0, 951.481e0, 6004.98e0, 994.150e0,
648 3 5620.04e0,1036.820e0, 5280.64e0,1079.490e0, 4979.37e0,1122.159e0,
649 4 4220.10e0,1274.756e0, 3749.80e0,1398.911e0, 3467.80e0,1498.821e0,
650 5 3255.10e0,1592.023e0, 3082.30e0,1683.386e0, 2937.10e0,1774.411e0/
651 data g18 / 2400.0e0,11209.60e0, 718.953e0,10316.18e0, 757.431e0,
652 1 9486.43e0, 795.909e0, 8750.33e0, 834.387e0, 8105.54e0, 872.866e0,
653 2 7541.38e0, 911.344e0, 7046.15e0, 949.822e0, 6609.24e0, 988.300e0,
654 3 6221.66e0,1026.779e0, 5875.90e0,1065.257e0, 5565.81e0,1103.735e0,
655 4 4619.20e0,1271.798e0, 4096.70e0,1397.651e0, 3787.00e0,1497.913e0,
656 5 3554.70e0,1590.843e0, 3366.60e0,1681.584e0, 3208.80e0,1771.765e0/
657 data g19 / 2600.0e0,11428.29e0, 744.475e0,10644.57e0, 778.232e0,
658 1 9914.50e0, 811.988e0, 9254.60e0, 845.745e0, 8664.25e0, 879.502e0,
659 2 8137.27e0, 913.259e0, 7666.18e0, 947.016e0, 7243.77e0, 980.772e0,
660 3 6863.58e0,1014.529e0, 6520.03e0,1048.286e0, 6208.34e0,1082.043e0,
661 4 5012.40e0,1270.621e0, 4441.80e0,1397.239e0, 4105.40e0,1497.515e0,
662 5 3854.20e0,1589.972e0, 3651.40e0,1679.930e0, 3481.50e0,1769.120e0/
663 data g20 / 2800.0e0,11589.07e0, 770.686e0,10931.29e0, 799.200e0,
664 110314.45e0, 827.715e0, 9746.45e0, 856.230e0, 9227.42e0, 884.745e0,
665 2 8754.35e0, 913.260e0, 8323.15e0, 941.774e0, 7929.53e0, 970.289e0,

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666      3 7569.46e0, 998.804e0, 7239.24e0,1027.319e0, 6935.60e0,1055.834e0,
667      4 5411.00e0,1269.067e0, 4789.20e0,1396.501e0, 4425.40e0,1496.853e0,
668      5 4154.90e0,1588.914e0, 3937.10e0,1678.177e0, 3755.00e0,1766.475e0/
669      data g21 / 3000.0e0,11604.42e0, 801.845e0,11109.66e0, 823.687e0,
670      110640.97e0, 845.529e0,10200.60e0, 867.371e0, 9788.61e0, 889.213e0,
671      2 9403.93e0, 911.055e0, 9044.98e0, 932.898e0, 8709.95e0, 954.740e0,
672      3 8397.01e0, 976.582e0, 8104.38e0, 998.424e0, 7830.38e0,1020.266e0,
673      4 5816.40e0,1267.043e0, 5139.50e0,1395.404e0, 4747.10e0,1495.908e0,
674      5 4456.80e0,1587.660e0, 4223.80e0,1676.323e0, 4029.40e0,1763.830e0/
675 c
676      end
677 *deck date
678      subroutine datz
679 c
680      common / leakhe / pe01(23), pe02(23), pe03(23), pe04(23),
681      1 pe05(23), pe06(23), pe07(23), pe08(23), pe09(23),
682      2 pe10(23), pe11(23), pe12(23), pe13(23), pe14(23),
683      3 pe15(23), pe16(23),nhhe,nphe
684 c
685 c      henry model critical flow tables extend to subcooled region
686 c
687 c      pe( 1,i) = stagnation pressure (psia)
688 c      pe(even,i) = maximum flow rate (lb/ft**2-sec)
689 c      pe( odd,i) = stagnation enthalpy (btu/lb)
690 c
691 c      nphe = number of pressure values
692 c      nhhe = number of pairs of enthalpy and flow values per pressure
693 c
694      data nhhe,nphe / 11,16 /
695 c
696      data pe01 / 10.0e0, 2293.0e0, 64.630e0, 2255.0e0, 74.271e0,
697      1 2204.0e0, 83.914e0, 2140.0e0, 93.560e0, 2059.0e0, 103.210e0,
698      2 1955.0e0, 112.866e0, 1820.0e0, 122.527e0, 1647.0e0, 132.195e0,
699      3 1415.0e0, 141.871e0, 1108.0e0, 151.556e0, 768.0e0, 161.261e0/
700 c
701      data pe02 / 14.7e0, 2788.0e0, 74.023e0, 2744.0e0, 84.605e0,
702      1 2684.0e0, 95.190e0, 2609.0e0, 105.780e0, 2512.0e0, 116.377e0,
703      2 2388.0e0, 126.981e0, 2227.0e0, 137.594e0, 2014.0e0, 148.217e0,
704      3 1735.0e0, 158.852e0, 1369.0e0, 169.501e0, 943.0e0, 180.179e0/
705 c
706      data pe03 / 50.0e0, 5174.0e0, 108.576e0, 5094.0e0, 122.624e0,
707      1 4989.0e0, 136.686e0, 4853.0e0, 150.766e0, 4679.0e0, 164.868e0,
708      2 4449.0e0, 178.996e0, 4156.0e0, 193.154e0, 3771.0e0, 207.349e0,
709      3 3273.0e0, 221.585e0, 2646.0e0, 235.869e0, 1787.8e0, 250.212e0/
710 c
711      data pe04 / 100.0e0, 7314.0e0, 131.690e0, 7203.0e0, 148.066e0,
712      1 7059.0e0, 164.470e0, 6870.0e0, 180.909e0, 6624.0e0, 197.390e0,
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721		data pe06 /	400.0e0,	14530.0e0,	191.387e0,	14278.0e0,	213.823e0,
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725	c						
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727		117020.0e0,	262.216e0,	16499.0e0,	287.192e0,	15845.0e0,	312.394e0,
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730	c						
731		data pe08 /	800.0e0,	20397.0e0,	229.413e0,	20026.0e0,	255.753e0,
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736		data pe09 /	1000.0e0,	22751.0e0,	243.188e0,	22316.0e0,	270.943e0,
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759		318388.0e0,	559.264e0,	15234.0e0,	601.066e0,	10186.3e0,	648.990e0/
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765 c
766      data pe15 /2200.0e0,  33369.0e0,  298.970e0,  32664.0e0,  332.498e0,
767      131782.0e0,  366.495e0,  30655.0e0,  401.079e0,  29295.0e0,  436.411e0,
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774      320862.0e0,  606.736e0,  16975.0e0,  656.028e0,  11209.6e0,  718.953e0/
775 c
776      end
777 *deck dath
778      subroutine dath
779 c
780      common /leakh/ pm(59,18),nhh,nph
781 c
782 c      henry model critical flow tables
783 c
784 c      pm( 1,i) = stagnation pressure (psia)
785 c      pm(even,i) = maximum flow rate (lb/ft**2-sec)
786 c      pm( odd,i) = stagnation enthalpy (btu/lb)
787 c
788 c      nph = number of pressure values
789 c      nhh = number of pairs of enthalpy and flow values per pressure
790 c
791      data nhh,nph / 29,18 /
792      data pm( 1, 1),pm( 2, 1),pm( 3, 1),pm( 4, 1),pm( 5, 1),pm( 6, 1),
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810 8 0.17334014e 03, 0.54843542e 01, 0.27694776e 03, 0.45099980e 01,
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814 2 0.58777062e 03, 0.32189742e 01, 0.69137824e 03, 0.29827733e 01,
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816 4 0.10022011e 04, 0.25055368e 01, 0.11047726e 04/
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841 4 0.10310031e 04, 0.11931808e 02, 0.11300918e 04/
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860 8 0.25946963e 03, 0.50774594e 02, 0.35767836e 03, 0.41893032e 02,
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866 4 0.10451395e 04, 0.23315677e 02, 0.11423661e 04/
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1135 8 0.60758921e 03, 0.43117547e 04, 0.67262775e 03, 0.37069297e 04,
1136 9 0.73766630e 03, 0.32785492e 04, 0.80270485e 03, 0.29640857e 04/
1137 data pm(49,14),pm(50,14),pm(51,14),pm(52,14),pm(53,14),pm(54,14),
1138 1 pm(55,14),pm(56,14),pm(57,14),pm(58,14),pm(59,14)/
1139 2 0.86774340e 03, 0.27184155e 04, 0.93278195e 03, 0.25268527e 04,
1140 3 0.99782049e 03, 0.23699277e 04, 0.10628590e 04, 0.22380367e 04,
1141 4 0.11278976e 04, 0.21249484e 04, 0.11922857e 04/
1142 data pm( 1,15),pm( 2,15),pm( 3,15),pm( 4,15),pm( 5,15),pm( 6,15),
1143 1 pm( 7,15),pm( 8,15),pm( 9,15),pm(10,15),pm(11,15),pm(12,15),
1144 2 pm(13,15),pm(14,15),pm(15,15),pm(16,15),pm(17,15),pm(18,15),
1145 3 pm(19,15),pm(20,15),pm(21,15),pm(22,15),pm(23,15),pm(24,15)/

```



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1146 4 0.14000000e 04, 0.11153878e 05, 0.59882953e 03, 0.11114695e 05,
1147 5 0.59940601e 03, 0.11023777e 05, 0.59998248e 03, 0.10935160e 05,
1148 6 0.60055896e 03, 0.10824250e 05, 0.60113544e 03, 0.10740498e 05,
1149 7 0.60171192e 03, 0.10658759e 05, 0.60228839e 03, 0.10578952e 05,
1150 8 0.60286487e 03, 0.10501005e 05, 0.60344135e 03, 0.10402988e 05,
1151 9 0.60401782e 03, 0.10328995e 05, 0.60459430e 03, 0.96529195e 04/
1152 data pm(25,15),pm(26,15),pm(27,15),pm(28,15),pm(29,15),pm(30,15),
1153 1 pm(31,15),pm(32,15),pm(33,15),pm(34,15),pm(35,15),pm(36,15),
1154 2 pm(37,15),pm(38,15),pm(39,15),pm(40,15),pm(41,15),pm(42,15),
1155 3 pm(43,15),pm(44,15),pm(45,15),pm(46,15),pm(47,15),pm(48,15)/
1156 4 0.61035907e 03, 0.90851395e 04, 0.61612385e 03, 0.86244273e 04,
1157 5 0.62188862e 03, 0.82315907e 04, 0.62765339e 03, 0.78916747e 04,
1158 6 0.63341817e 03, 0.75939611e 04, 0.63918294e 03, 0.73305411e 04,
1159 7 0.64494771e 03, 0.72131545e 04, 0.65071249e 03, 0.70524429e 04,
1160 8 0.65647726e 03, 0.60582937e 04, 0.71412499e 03, 0.52735113e 04,
1161 9 0.77177272e 03, 0.46694008e 04, 0.82942045e 03, 0.42278200e 04/
1162 data pm(49,15),pm(50,15),pm(51,15),pm(52,15),pm(53,15),pm(54,15),
1163 1 pm(55,15),pm(56,15),pm(57,15),pm(58,15),pm(59,15)/
1164 2 0.88706818e 03, 0.38845710e 04, 0.94471591e 03, 0.36116173e 04,
1165 3 0.10023636e 04, 0.33915424e 04, 0.10600114e 04, 0.32023508e 04,
1166 4 0.11176591e 04, 0.30463219e 04, 0.11747303e 04/
1167 data pm( 1,16),pm( 2,16),pm( 3,16),pm( 4,16),pm( 5,16),pm( 6,16),
1168 1 pm( 7,16),pm( 8,16),pm( 9,16),pm(10,16),pm(11,16),pm(12,16),
1169 2 pm(13,16),pm(14,16),pm(15,16),pm(16,16),pm(17,16),pm(18,16),
1170 3 pm(19,16),pm(20,16),pm(21,16),pm(22,16),pm(23,16),pm(24,16)/
1171 4 0.18000000e 04, 0.12092534e 05, 0.64848967e 03, 0.12060637e 05,
1172 5 0.64899351e 03, 0.11997142e 05, 0.64949736e 03, 0.11934703e 05,
1173 6 0.65000120e 03, 0.11873291e 05, 0.65050504e 03, 0.11812880e 05,
1174 7 0.65100889e 03, 0.11753444e 05, 0.65151273e 03, 0.11694956e 05,
1175 8 0.65201657e 03, 0.11637392e 05, 0.65252041e 03, 0.11580728e 05,
1176 9 0.65302426e 03, 0.11524943e 05, 0.65352810e 03, 0.10990746e 05/
1177 data pm(25,16),pm(26,16),pm(27,16),pm(28,16),pm(29,16),pm(30,16),
1178 1 pm(31,16),pm(32,16),pm(33,16),pm(34,16),pm(35,16),pm(36,16),
1179 2 pm(37,16),pm(38,16),pm(39,16),pm(40,16),pm(41,16),pm(42,16),
1180 3 pm(43,16),pm(44,16),pm(45,16),pm(46,16),pm(47,16),pm(48,16)/
1181 4 0.65856652e 03, 0.10529341e 05, 0.66360495e 03, 0.10125821e 05,
1182 5 0.66864337e 03, 0.97692276e 04, 0.67368180e 03, 0.94513008e 04,
1183 6 0.67872022e 03, 0.92456831e 04, 0.68375865e 03, 0.91922360e 04,
1184 7 0.68879708e 03, 0.90603008e 04, 0.69383550e 03, 0.89992705e 04,
1185 8 0.69887393e 03, 0.79242901e 04, 0.74925818e 03, 0.69285961e 04,
1186 9 0.79964243e 03, 0.61446165e 04, 0.85002669e 03, 0.55627091e 04/
1187 data pm(49,16),pm(50,16),pm(51,16),pm(52,16),pm(53,16),pm(54,16),
1188 1 pm(55,16),pm(56,16),pm(57,16),pm(58,16),pm(59,16)/
1189 2 0.90041094e 03, 0.51168594e 04, 0.95079519e 03, 0.47668412e 04,
1190 3 0.10011794e 04, 0.44867060e 04, 0.10515637e 04, 0.42427561e 04,
1191 4 0.11019480e 04, 0.40393917e 04, 0.11518283e 04/
1192 data pm( 1,17),pm( 2,17),pm( 3,17),pm( 4,17),pm( 5,17),pm( 6,17),
1193 1 pm( 7,17),pm( 8,17),pm( 9,17),pm(10,17),pm(11,17),pm(12,17),

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1194      2      pm(13,17),pm(14,17),pm(15,17),pm(16,17),pm(17,17),pm(18,17),
1195      3      pm(19,17),pm(20,17),pm(21,17),pm(22,17),pm(23,17),pm(24,17)/
1196      4      0.20000000e 04, 0.12548625e 05, 0.67211135e 03, 0.12527433e 05,
1197      5      0.67257758e 03, 0.12477584e 05, 0.67304380e 03, 0.12428359e 05,
1198      6      0.67351002e 03, 0.12354095e 05, 0.67397625e 03, 0.12306429e 05,
1199      7      0.67444247e 03, 0.12259343e 05, 0.67490870e 03, 0.12212826e 05,
1200      8      0.67537492e 03, 0.12166866e 05, 0.67584115e 03, 0.12097623e 05,
1201      9      0.67630737e 03, 0.12053056e 05, 0.67677360e 03, 0.11593333e 05/
1202      data pm(25,17),pm(26,17),pm(27,17),pm(28,17),pm(29,17),pm(30,17),
1203      1      pm(31,17),pm(32,17),pm(33,17),pm(34,17),pm(35,17),pm(36,17),
1204      2      pm(37,17),pm(38,17),pm(39,17),pm(40,17),pm(41,17),pm(42,17),
1205      3      pm(43,17),pm(44,17),pm(45,17),pm(46,17),pm(47,17),pm(48,17)/
1206      4      0.68143584e 03, 0.11157809e 05, 0.68609809e 03, 0.10765562e 05,
1207      5      0.69076033e 03, 0.10467344e 05, 0.69542258e 03, 0.10284563e 05,
1208      6      0.70008482e 03, 0.10275959e 05, 0.70474707e 03, 0.10180133e 05,
1209      7      0.70940931e 03, 0.10112706e 05, 0.71407156e 03, 0.10047270e 05,
1210      8      0.71873380e 03, 0.89878104e 04, 0.76535625e 03, 0.78172752e 04,
1211      9      0.81197870e 03, 0.69030697e 04, 0.85860115e 03, 0.62502254e 041
1212      data pm(49,17),pm(50,17),pm(51,17),pm(52,17),pm(53,17),pm(54,17),
1213      1      pm(55,17),pm(56,17),pm(57,17),pm(58,17),pm(59,17)/
1214      2      0.90522360e 03, 0.57611957e 04, 0.95184605e 03, 0.53897722e 04,
1215      3      0.99846850e 03, 0.50810573e 04, 0.10450909e 04, 0.48154370e 04,
1216      4      0.10917134e 04, 0.45892802e 04, 0.11378696e 04/
1217      data pm( 1,18),pm( 2,18),pm( 3,18),pm( 4,18),pm( 5,18),pm( 6,18),
1218      1      pm( 7,18),pm( 8,18),pm( 9,18),pm(10,18),pm(11,18),pm(12,18),
1219      2      pm(13,18),pm(14,18),pm(15,18),pm(16,18),pm(17,18),pm(18,18),
1220      3      pm(19,18),pm(20,18),pm(21,18),pm(22,18),pm(23,18),pm(24,18)/
1221      4      0.22000000e 04, 0.12813458e 05, 0.69546232e 03, 0.12797706e 05,
1222      5      0.69588902e 03, 0.12737513e 05, 0.69631572e 03, 0.12703856e 05,
1223      6      0.69674241e 03, 0.12670456e 05, 0.69716911e 03, 0.12612354e 05,
1224      7      0.69759581e 03, 0.12579734e 05, 0.69802250e 03, 0.12547358e 05,
1225      8      0.69844920e 03, 0.12515223e 05, 0.69887590e 03, 0.12459599e 05,
1226      9      0.69930260e 03, 0.12428195e 05, 0.69972929e 03, 0.12063798e 05/
1227      data pm(25,18),pm(26,18),pm(27,18),pm(28,18),pm(29,18),pm(30,18),
1228      1      pm(31,18),pm(32,18),pm(33,18),pm(34,18),pm(35,18),pm(36,18),
1229      2      pm(37,18),pm(38,18),pm(39,18),pm(40,18),pm(41,18),pm(42,18),
1230      3      pm(43,18),pm(44,18),pm(45,18),pm(46,18),pm(47,18),pm(48,18)/
1231      4      0.70399626e 03, 0.11751453e 05, 0.70826323e 03, 0.11464110e 05,
1232      5      0.71253020e 03, 0.11375772e 05, 0.71679717e 03, 0.11364155e 05,
1233      6      0.72106414e 03, 0.11429088e 05, 0.72533111e 03, 0.11397517e 05,
1234      7      0.72959808e 03, 0.11351836e 05, 0.73386505e 03, 0.11291398e 05,
1235      8      0.73813202e 03, 0.10144490e 05, 0.78080172e 03, 0.84951054e 04,
1236      9      0.82347142e 03, 0.74811964e 04, 0.86614112e 03, 0.68680311e 04/
1237      data pm(49,18),pm(50,18),pm(51,18),pm(52,18),pm(53,18),pm(54,18),
1238      1      pm(55,18),pm(56,18),pm(57,18),pm(58,18),pm(59,18)/
1239      2      0.90881083e 03, 0.64129876e 04, 0.95148053e 03, 0.60360975e 04,
1240      3      0.99415023e 03, 0.57181600e 04, 0.10368199e 04, 0.54250196e 04,
1241      4      0.10794896e 04, 0.51763832e 04, 0.11217326e 041

```

```

1242      end
1243 c
1244 *deck gcrit
1245      subroutine gcritf(p,h,m,g,s,rhov,rhol)
1246 c
1247 c          m=1      moody
1248 c          m=2      henry fauske
1249 c          m=3      subcoold henry
1250 c
1251      common /leakc / g01(735),ng,npi
1252      common /leakhe / pe01(368),nhhe,nphe
1253      common / leakh / pm(1062),nhh,nph
1254      dimension tm(1),thfs(1),thf(1)
1255      equivalence (g01(1),tm(1)),(pe01(1),thfs(1)),(pm(1),thf(1))
1256      go to (10,20,30),m
1257 10 call dterp(p,h,g,tm,ng,npi)
1258      s=(rhol/rhov)**.333333334
1259      return
1260 20 call dterp(p,h,g,thfs,nhhe,nphe)
1261      s=1.
1262      return
1263 30 call dterp(p,h,g,thf,nhh,nph)
1264      s=1.
1265      return
1266      end
1267      subroutine dterp(p,h,g,table,ng,npi)
1268      dimension table(1)
1269      data lm1/10/
1270      lm1 = min0(npi-1,max0(lm1,1))
1271      inc = (2*ng + 1)
1272      l = lm1 + 1
1273      j = (lm1-1)*inc+1
1274      if(p.ge.table(j)) go to 25
1275      go to 55
1276 25 do 50 i=1,npi
1277      j = j + inc
1278      if(p.gt.table(j)) go to 50
1279      f = (p - table(j))/(table(j+inc) - table(j))
1280      l = j
1281      go to 70
1282 50 lm1 = lm1 + 1
1283 55 lm2 = lm1 - 1
1284      do 60 k=1,lm2
1285      j = j-inc
1286      if(p.lt.table(j)) go to 60
1287      lm1 = lm2 - k + 1
1288      l = j
1289      f = (p - table(j)) / (table(j+inc) - table(j))

```

```

1290          go to 70
1291 60        continue
1292 70        l1 = l + 2
1293          do 100 i =2,ng
1294          l1 = l1 + 2
1295          if (h.ge.table(l1)) go to 100
1296          lb = l1-2
1297          fm= (h-table(lb))/(table(l1)-table(lb))
1298          gm=table(lb-1)+fm *(table(l1-1)-table(lb-1))
1299          go to 150
1300 100       continue
1301 150       if(h.ge.table(lb+inc)) go to 175
1302          go to 250
1303 175       l1 = lb + inc
1304          do 200 m=i,ng
1305          l1 = l1+2
1306          if(h.ge.table(l1)) go to 200
1307          fp=(h-table(l1-2))/(table(l1)-table(l1-2))
1308          gp = table(l1-3)+fp*(table(l1-1)-table(l1-3))
1309          go to 300
1310 200       continue
1311 250       l1 = lb + inc
1312          do 252 m=1,i
1313          l1=l1 - 2
1314          if(h.lt.table(l1)) go to 252
1315          fp= (h-table(l1))/(table(l1+2)-table(l1))
1316          gp = table(l1-1) +fp*(table(l1+1)-table(l1-1))
1317          go to 300
1318 252       continue
1319 300       g = gm + f *(gp-gm)
1320          return
1321          end

```

APPENDIX C

COBRA-NC SAMPLE ASB OUTPUT


```

          xxxxxxxx
        xx      xxxxx
      xx      xxxxx
    xx      xxxxxx
  xx      xxxxxxx
xx      xxxxxxx

```

```

xxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxx
xx      xxx
xx      xxxx
  xx      xxxx
    xx      xxxxxx
      xx      xxxxxx

```

```

cccc  oooo  bbbbbb  rrrrrr  aaaa  //
ccc  c  ooo  o  bbb  b  rrr  r  aaa  a  //
ccc  c  ooo  o  bbb  b  rrr  r  aaa  a  //
ccc  ooo  o  bbb  b  rrr  r  aaa  a  //
ccc  ooo  o  bbbbbb  rrrrrr  aaaaaaaa  //
ccc  ooo  o  bbbbbb  rrrrrr  aaaaaaaa  //
ccc  c  ooo  o  bbb  b  rrr  r  aaa  a  //
ccc  c  ooo  o  bbb  b  rrr  r  aaa  a  //
cccc  oooo  bbbbbb  rrr  r  aaa  a  //

```

```

nnn  n  ccccc
nnn  n  ccc  c
nn  n  n  ccc
nn  n  n  ccc
nn  n  n  ccc
nn  n  n  ccc
nn  n  n  ccc  c
nn  nn  ccc  c
nn  nn  ccccc

```

```

  xx      xxxxxxxx
  xx      xxxxxxxx
  xx      xxxxxxxx
  xx      xxxxxxxx
  xx      xxxxxxxx

```

```

  xx      xxxxxx
  xx      xxxxxx
  xx      xxxxxx
  xx      xxxxxx
  xx      xxxxx

```

C.1

xxxxxxxxxxxxxxxxdonxxxmarvxxxjoexxtixxxxtomxxxrickxxxjudixxxgaryxxxchr isxxxannettexxxshawxxxpeggyxxxke ithxxcathy-
xxxxxxxxxxxxxxxx

```

PPPPPP  nnn  n  |||
PPP  P  nnn  n  |||
PPP  P  nnnn  n  |||
PPP  P  nnnnn  n  |||
PPPPPP  nnn  nn  n  |||
PPPPPP  nnn  nn  n  |||
PPP  nnn  nn  |||
PPP  nnn  nn  |||
PPP  nnn  nn  |||
PPP  nnn  n  |||
PPP  nnn  n  |||

```

bbbb aa ttt ttt eeee l l eeee	pppp aa cc i ffff i cc
b b a a t t e l l e	p p a a c c i f i c c
bbb aaaa t t eee l l eee	pppp aaaa c i fff i c
b b a a t t e l l e	p a a c c i f i c c
bbbb a a t t eeee llll llll eeee	p a a c c i f i cc

n n oo rrr ttt h h w w eeee ssss ttt	l aa bbbb oo rrr aa ttt oo rrrr y y
nnno o r r t h h w w e s t	l a a b b o o r r a a t o o r r y y
n nn o o rrrr t hhhh w w eee ssss t	l aaaa bbb o o rrrr aaaa t o o rrrr y
nnno o r r t h h www e s t	l a a b b o o r r a a t o o r r y
n n oo r r t h h w w eeee ssss t	llll a abbbb oo r r a a t oo r r y

p. o. box **999**, richland, washington **99352**

this is cycle **15** of cobranc - **-09/19/85**

in case of questions or **problems**, call

fluid and thermal engineering section of
 pn| -- battelle pacific northwest laboratory
 richland, washington

phone number -- (509) 375-2069

1***** input file listing *****

```
1234567890123456789012345678901234567890123456789012345678901234567890
1      12      set units and linear conv.
2      0 0.000000e+00      restart data
3 0.100000e-02      5      40      iteration control
4      1 model 3-21-85
5      1 1      0      vessel 1.1
6      278.00 278.00 27.80 278.00
7      14.691 1101.108      131.388 0.0000010 0.0237449
8 air 0.9762541
9      2 18 18      vessel 2.1
10     11417.150.5
11     2249.663.20249.6
12     31633.161.6
13     4404.880.48
14     5453.585.18
15     61426.151.0 1425.
16     7195.855.98 195.0
17     85328.292.0
18     931.5022.45 31.00
19     10650.2102.0 650.0
20     11851.5116.7 850.0
21     12371.377.07
22     131426.151.01425.
23     14195.955.98195.0195.0
24     1531.4422.4331.0031.44
25     16650.1102.0650.0
26     17851.6116.7850.0
27     18195.855.98195.0
28     1      -1 0
29     2      -2 0
30     3      -3 0
1234567890123456789012345678901234567890123456789012345678901234567890
31     4      -4 0
32     5      -5 0
33     6      -6 0
34     7      -7 0
35     8      -8 0
36     9      -9 0
37    10     -10 0
```

38	11			-11	0
39	12			-12	0
40	13			-13	0
41	14			-14	0
42	15			-15	0
43	16			-16	0
44	17			-17	0
45	18			-18	0
46	3	12			
47	1	1	21.1679.1652.5992.000		vessel 3.1
48	1.				
49	2	1	33.19415.172.6982.000		
50	1.				
51	3	1	10.66676.9282.4882.000		
52	1.				
53	4	1	11.66676.9282.4882.000		
54	1.				
55	5	3	41.3229.7572.6162.000		
56	1.				
57	6	3	5.27224.4271.9372.000		
58	1.				
59	7	3	65.33319.602.7292.000		
60	1.				
12345678901234567890123456789012345678901234567890123456789012345678901234567890					
61	8	3	71.2949.6542.6132.000		
62	1.				
63	9	3	9.97228.3672.5712.000		
64	1.				
65	10	3	121.1118.9442.5922.000		
66	1.				
67	11	5	61.2229.3812.6062.000		
68	1.				
69	12	6	811.4428.712.7602.000		
70	1.				
71					blank 3.4
72	4	3	1		vessel 4.1
73	1	12	1	18.00	
74	1	1			1
75	2	2			2
76	3	3			3
77	4	4			4

78	5	5							5
79	6	13							6
80	7	14							7
81	8	8							8
82	9	15							9
83	10	16							10
84	11	17							11
85	12	12							12
86	2	5	1		9.00				
87	13	13							6
88	14	18							7
89	15	15							9
90	16	16							10
1234567890123456789012345678901234567890123456789012345678901234567890									
91	17	17							11
92	3	1	1		18.00				
93	18	18							14
94	18								
95	7	1						vessel	7.1
96	2.6	2	15						
97	8	0	18	1	1			vessel	8.1
98	280.00		2.00						
99	1	1			302.2				1.0
100	2	2			90.9				1.0
101	3	3			332.8				1.0
102	4	4			125.5				1.0
103	5	5			134.3				1.0
104	6	6			218.8				1.0
105	7	7			66.9				1.0
106	8	8			884.0				1.0
107	9	9			24.2				1.0
108	10	10			138.1				1.0
109	11	11			164.1				1.0
110	12	12			118.3				1.0
111	13	13			309.5				1.0
112	14	14			56.2				1.0
113	15	15			26.0				1.0
114	16	16			174.2				1.0
115	17	17			211.5				1.0
116	18	18			66.9				1.0
117	1	0	18	2				vessel	8.4

118	1	2	3	4	5	6	7	8	9	10	11	12
119	13	14	15	16	17	18						
120		0.0	90.0		45.0	90.0						
1234567890123456789012345678901234567890123456789012345678901234567890												
121	9	18				0					vessel	9.1
122	1	wall	302.		2.00	4		1				
123	5	10.008		5	10.042		5	1 0.65	5	1 1.30		
124	2	wall	91.		2.00	4		1				
125	5	10.008		5	10.042		5	1 0.65	5	1 1.30		
126	3	wall	333.		2.00	4		1				
127	5	10.008		5	10.042		5	1 0.65	5	1 1.30		
128	4	wall	125.		2.00	4		1				
129	5	10.008		5	10.042		5	1 0.65	5	1 1.30		
130	5	wall	134.		2.00	4		1				
131	5	10.008		5	10.042		5	1 0.65	5	1 1.30		
132	6	wall	219.		2.00	4		1				
133	5	10.008		5	10.042		5	1 0.65	5	1 1.30		
134	7	wall	67.		2.00	4		1				
135	5	10.008		5	10.042		5	1 0.65	5	1 1.30		
136	8	wall	884.		2.00	4		1				
137	5	10.008		5	10.042		5	1 0.65	5	1 1.30		
138	9	wall	24.		2.00	4		1				
139	5	10.008		5	10.042		5	1 0.65	5	1 1.30		
140	10	wall	138.		2.00	4		1				
141	5	10.008		5	10.042		5	1 0.65	5	1 1.30		
142	11	wall	164.		2.00	4		1				
143	5	10.008		5	10.042		5	1 0.65	5	1 1.30		
144	12	wall	118.		2.00	4		1				
145	5	10.008		5	10.042		5	1 0.65	5	1 1.30		
146	13	wall	309.		2.00	4		1				
147	5	10.008		5	10.042		5	1 0.65	5	1 1.30		
148	14	wall	56.		2.00	4		1				
149	5	10.008		5	10.042		5	1 0.65	5	1 1.30		
150	15	wall	26.		2.00	4		1				
1234567890123456789012345678901234567890123456789012345678901234567890												
151	5	10.008		5	10.042		5	1 0.65	5	1 1.30		
152	16	wall	174.		2.00	4		1				
153	5	10.008		5	10.042		5	1 0.65	5	1 1.30		
154	17	wall	212.		2.00	4		1				
155	5	10.008		5	10.042		5	1 0.65	5	1 1.30		
156	18	wall	67.		2.00	4		1				

157	5	10.008		5	10.042		5	1 0.65	5	1 1.30	
158	10	1								vessel 10.1	
159	1	2	139.00								
160	50.000	0.220		0.867	1000.000		0.220	0.867			
161	13	24	0 1	0 0 0 0						vessel 13.1	
162	30										
163		142.00.8500		142.00.8510		71.005.000		71.005.010		68.80	
164	6.000	68.606.010		67.807.500		67.807.510		64.9010.00		64.90	
165	10.01	62.8012.50		62.8012.51		61.0015.00		61.0015.01		58.08	
166	17.50	58.0017.51		54.5020.00		54.5020.01		49.5022.50		49.50	
167	22.51	46.2025.00		46.2025.01		39.3027.50		39.3027.51		27.70	
168	30.00	27.7030.01		15.2032.50		15.2035.00		0.001500.		0.00	
169	2	1	2 1	0	1.000	1249.400		925.000			
170	251.5.0001.9999.0001										
171										blank 13.4b	
172	15	3	1 0	0	14.700	145.300		14.700			
173	152.3.9999.9999.0001										
174										blank 13.4b	
175	1	1	3								
176	3	1	3								
177	4	1	3								
178	5	1	3								
179	6	1	3								
180	7	1	3								
1234567890123456789012345678901234567890123456789012345678901234567890											
181	8	1	3								
182	9	1	3								
183	10	1	3								
184	11	1	3								
185	12	1	3								
186	1	2	3								
187	2	2	3								
188	3	2	3								
189	4	2	3								
190	5	2	3								
191	8	2	3								
192	12	2	3								
193	13	2	3								
194	16	2	3								
195	17	2	3								
196	18	2	3								

rancho seco unit no 1 helb (50-312) model 3-21-85

date 86/09/23 time 18:46:55

general information

0 initial system operating pressure (psi) 14.69100
 initial system ~~steam/water~~ enthalpy~~1101.10800~~
 initial noncondensable gas enthalpy 131.38800
 initial liquid volume fraction 0.00000
 mass flux for initialization (lb/ft**2-sec) . . . 0.00000
 average linear heat rate (kw/ft) 0.00000
 total axial length (inches). 540.00000
 total no. of axial nodes 3

1

initial volume fractions of vapor and noncondensa gases

1

99.99990 percent of the total system volume is initially filled with vapor and/or noncondensable gases. the fraction

of this gas volume occupied by water vapor and each noncondensable gas is as follows:

steam	0.0237	air	0.97625
--------------	--------	-----	---------

1

subchannel data

		nominal	wetted	momentum	momentum	axial variation
tables	subchannel	channel area	perimeter	area	area	continuity momentum
wetted	id. no.	(in**2)	(in.)	(bottom)	(top)	area area
perimeter						

C.9

0	1	204048.0000	1806.000	204048.0000	204048.0000	0	0
0	2	35942.4000	758.400	35942.4000	35942.4000	0	0
0	3	235152.0000	1939.200	235152.0000	235152.0000	0	0
0	4	58291.2000	965.760	58291.2000	58291.2000	0	0
0	5	65304.0000	1022.160	65304.0000	65304.0000	0	0
0	6	205344.0000	1812.000	205344.0000	205200.0000	0	0
0	7	28195.2000	671.760	28195.2000	28080.0000	0	0
0	8	767232.0000	3504.000	767232.0000	767232.0000	0	0
0	9	4536.0000	269.400	4536.0000	4464.0000	0	0
0	10	93628.8000	1224.000	93628.8000	93600.0000	0	0
0	11	122616.0000	1400.400	122616.0000	122400.0000	0	0
0	12	53467.2000	924.840	53467.2000	53467.2000	0	0
0	13	205344.0000	1812.000	205200.0000	205344.0000	0	0
0	14	28209.6000	671.760	28080.0000	28080.0000	0	0
0	15	4527.3600	269.160	4464.0000	4527.3600	0	0
0	16	93614.4000	1224.000	93600.0000	93614.4000	0	0
0	17	122630.4000	1400.400	122400.0000	122630.4000	0	0
0	18	28195.2000	671.760	28080.0000	28195.2000	0	0

axial loss coefficients

node

channel 1 2

15 * 0.000 2.600

Ø

data for lateral momentum convected by axial velocities at section boundaries

channel	node	gap	gap	area	node	gap	gap	area	node	gap	gap	area	node	gap	
gap	area														
no.	no.	below	above			no.	below	above			no.	below	above	no.	below

Ø

channel thermal connection input data

channel no.

1

fuel rod indices

Ø Ø Ø Ø Ø Ø

heat slab indices

-1 Ø Ø Ø Ø Ø Ø

14	18	0	0	0	0	0	7	0	0	0	0	0
15	15	0	0	0	0	0	9	0	0	0	0	0
16	16	0	0	0	0	0	10	0	0	0	0	0
17	17	0	0	0	0	0	11	0	0	0	0	0

1

channel splitting data - axial level 3 of 3

number of channels	no. of nodes
1	1

channel	channels above						channels below						
18	18	0	0	0	0	0	1	4	0	0	0	0	0

simultaneous solution group information

no. of groups	last cell number in each group
1	18

1

fuel rod and heat slab model input

no. of fuel rods = 0
no. of heat slabs = 18

heat slab model input

heat slab index	channel connection - inside	heated perimeter outside	geometry type	conductor type	slab multiplier
-----	-----	-----	-----	-----	-----
1	1 - 3626.40	0 - 0.00	wal l	1	1.000
2	2 - 1090.80	0 - 0.00	wal l	2	1.000
3	3 - 3993.60	0 - 0.00	wal l	3	1.000
4	4 - 1506.00	0 - 0.00	wal l	4	1.000
5	5 - 1611.60	0 - 0.00	wal l	5	1.000
6	6 - 2625.60	0 - 0.00	wal l	6	1.000
7	7 - 802.80	0 - 0.00	wal l	7	1.000
8	8 - 10608.00	0 - 0.00	wal l	8	1.000
9	9 - 290.40	0 - 0.00	wal l	9	1.000
10	10 - 1657.20	0 - 0.00	wal l	10	1.000
11	11 - 1969.20	0 - 0.00	wal l	11	1.000
12	12 - 1419.60	0 - 0.00	wal l	12	1.000
13	13 - 3714.00	0 - 0.00	wal l	13	1.000
14	14 - 674.40	0 - 0.00	wal l	14	1.000
15	15 - 312.00	0 - 0.00	wal l	15	1.000
16	16 - 2090.40	0 - 0.00	wal l	16	1.000
17	17 - 2538.00	0 - 0.00	wal l	17	1.000
18	18 - 802.80	0 - 0.00	wal l	18	1.000

conductor geometry description
 no. of geometry types = 18

 type 1 - wall ftat plate conductor geometry

wall perimeter 3624.000 (in.)
 wall thickness 24.0000 (in.)
 no. of nodes (total) 20
 material index (inside) 1
 material index(outside) 0

radial noding information

node no.	material index	radial location	node boundaries (inside) (outside)		power fraction
----	-----	-----	-----	-----	-----
1	1	0.0000	0.0000	0.0107	0.00000
2	1	0.0213	0.0107	0.0320	0.00000
3	1	0.0427	0.0320	0.0533	0.00000
4	1	0.0640	0.0533	0.0747	0.00000
5	1	0.0853	0.0747	0.0960	0.00000
6	1	0.1464	0.0960	0.1968	0.00000
7	1	0.2472	0.1968	0.2976	0.00000
8	1	0.3480	0.2976	0.3984	0.00000
9	1	0.4488	0.3984	0.4992	0.00000
10	1	0.5496	0.4992	0.6000	0.00000
11	1	1.3800	0.6000	2.1600	0.00000
12	1	2.9400	2.1600	3.7200	0.00000
13	1	4.5000	3.7200	5.2800	0.00000
14	1	6.0600	5.2800	6.8400	0.00000
15	1	7.6200	6.8400	8.4000	0.00000
16	1	10.1333	8.4000	11.8667	0.00000
17	1	13.6000	11.8667	15.3333	0.00000
18	1	17.0667	15.3333	18.8000	0.00000
19	1	20.5333	18.8000	22.2667	0.00000

20 1 24.0000 22.2667 24.0000 0.00000

type 2 - wall flat plate conductor geometry

 wall perimeter 1092.000 (in.)
 wall thickness 24.0000 (in.)
 no. of nodes (total) 20
 material index (inside) 1
 material index(outside) 0

radial noding information

node no.	material index	radial location	node boundaries (inside)	node boundaries (outside)	power fraction
1	1	0.0000	0.0000	0.0107	0.00000
2	1	0.0213	0.0107	0.0320	0.00000
3	1	0.0427	0.0320	0.0533	0.00000
4	1	0.0640	0.0533	0.0747	0.00000
5	1	0.0853	0.0747	0.0960	0.00000
6	1	0.1464	0.0960	0.1968	0.00000
7	1	0.2472	0.1968	0.2976	0.00000
8	1	0.3480	0.2976	0.3984	0.00000
9	1	0.4488	0.3984	0.4992	0.00000
10	1	0.5496	0.4992	0.6000	0.00000
11	1	1.3800	0.6000	2.1600	0.00000
12	1	2.9400	2.1600	3.7200	0.00000
13	1	4.5000	3.7200	5.2800	0.00000
14	1	6.0600	5.2800	6.8400	0.00000
15	1	7.6200	6.8400	8.4000	0.00000
16	1	10.1333	8.4000	11.8667	0.00000
17	1	13.6000	11.8667	15.3333	0.00000
18	1	17.0667	15.3333	18.8000	0.00000
19	1	20.5333	18.8000	22.2667	0.00000
20	1	24.0000	22.2667	24.0000	0.00000

type 3 - wall flat plate conductor geometry

wall perimeter 3996.000 (in.)
 wall thickness 24.0000 (in.)
 no. of nodes (total) 20
 material index (inside) 1
 material index(outside) 0

radial noding information

node no.	material index	radial location	node boundaries		power fraction
			(inside)	(outside)	
1	1	0.0000	0.0000	0.0107	0.00000
2	1	0.0213	0.0107	0.0320	0.00000
3	1	0.0427	0.0320	0.0533	0.00000
4	1	0.0640	0.0533	0.0747	0.00000
5	1	0.0853	0.0747	0.0960	0.00000
6	1	0.1464	0.0960	0.1968	0.00000
7	1	0.2472	0.1968	0.2976	0.00000
8	1	0.3480	0.2976	0.3984	0.00000
9	1	0.4488	8.3984	0.4992	0.00000
10	1	0.5496	0.4992	0.6000	0.00000
11	1	1.3800	0.6000	2.1600	0.00000
12	1	2.9400	2.1600	3.7200	0.00000
13	1	4.5000	3.7200	5.2800	0.00000
14	1	6.0600	5.2800	6.8400	0.00000
15	1	7.6200	6.8400	8.4000	0.00000
16	1	10.1333	8.4000	11.8667	0.00000
17	1	13.6000	11.8667	15.3333	0.00000
18	1	17.0667	15.3333	18.8000	0.00000
19	1	20.5333	18.8000	22.2667	0.00000
20	1	24.0000	22.2667	24.0000	0.00000

type 4 - wall flat plate conductor geometry

wall perimeter 1500.000 (in.)
 wall thickness 24.0000 (in.)
 no. of nodes (total) 20
 material index (inside) 1

material index(outside) 0

radial noding information

node no.	material index	radial location	node boundaries		power fraction
			(inside)	(outside)	
1	1	0.0000	0.0000	0.0107	0.00000
2	1	0.0213	0.0107	0.0320	0.00000
3	1	0.0427	0.0320	0.0533	0.00000
4	1	0.0640	0.0533	0.0747	0.00000
5	1	0.0853	0.0747	0.0960	0.00000
6	1	0.1464	0.0960	0.1968	0.00000
7	1	0.2472	0.1968	0.2976	0.00000
8	1	0.3480	0.2976	0.3984	0.00000
9	1	0.4488	0.3984	0.4992	0.00000
10	1	0.5496	0.4992	0.6000	0.00000
11	1	1.3800	0.6800	2.1600	0.00000
12	1	2.9400	2.1600	3.7200	0.00000
13	1	4.5000	3.7200	5.2800	0.00000
14	1	6.0600	5.2800	6.8408	0.00000
15	1	7.6200	6.8400	8.4000	0.00000
16	1	10.1333	8.4000	11.8667	0.00000
17	1	13.6000	11.8667	15.3333	0.00000
18	1	17.0667	15.3333	18.8000	0.00000
19	1	20.5333	18.8000	22.2667	0.00000
20	1	24.0000	22.2667	24.0000	0.00000

type 5 - wall flat plate conductor geometry

.....

wall perimeter	1608.000 (in.)
wall thickness	24.0000 (in.)
no. of nodes (total)	20
material index (inside)	1
material index(outside)	0

radial noding information

node	material	radial	node boundaries	power
------	----------	--------	-----------------	-------

no.	index	location	(inside)	(outside)	fraction
----	-----	-----	-----	-----	-----
1	1	0.0000	0.0000	0.0107	0.00000
2	1	0.0213	0.0107	0.0320	0.00000
3	1	0.0427	0.0320	0.0533	0.00000
4	1	0.0640	0.0533	0.0747	0.00000
5	1	0.0853	0.0747	0.0960	0.00000
6	1	0.1464	0.0960	0.1968	0.00000
7	1	0.2472	0.1968	0.2976	0.00000
8	1	0.3480	0.2976	0.3984	0.00000
9	1	0.4488	0.3984	0.4992	0.00000
10	1	0.5496	0.4992	0.6000	0.00000
11	1	1.3800	0.6000	2.1600	0.00000
12	1	2.9400	2.1600	3.7200	0.00000
13	1	4.5000	3.7200	5.2800	0.00000
14	1	6.0600	5.2800	6.8400	0.00000
15	1	7.6200	6.8400	8.4000	0.00000
16	1	10.1333	8.4000	11.8667	0.00000
17	1	13.6000	11.8667	15.3333	0.00000
18	1	17.0667	15.3333	18.8000	8.00000
19	1	20.5333	18.8000	22.2667	8.00000
20	1	24.0000	22.2667	24.0000	0.00000

type 6 - wall flat plate conductor geometry

wall perimeter 2628.000 (in.)
wall thickness 24.0000 (in.)
no. of nodes (total) 20
material index (inside) 1
material index(outside) 0

radial noding information

node	material	radial	node boundaries		power
no.	index	location	(inside)	(outside)	fraction
----	-----	-----	-----	-----	-----
1	1	0.0000	0.0000	0.0107	0.00000
2	1	0.0213	0.0107	0.0320	0.00000
3	1	0.0427	0.0320	0.0533	0.00000

4	1	0.0640	0.0533	0.0747	0.00000
5	1	0.0853	0.0747	0.0960	0.00000
6	1	0.1464	0.0960	0.1968	0.00000
7	1	0.2472	0.1968	0.2976	0.00000
8	1	0.3480	0.2976	0.3984	0.00000
9	1	0.4488	0.3984	0.4992	0.00000
10	1	0.5496	0.4992	0.6000	0.00000
11	1	1.3800	0.6000	2.1600	0.00000
12	1	2.9400	2.1600	3.7200	0.00000
13	1	4.5000	3.7200	5.2800	0.00000
14	1	6.0600	5.2800	6.8400	0.00000
15	1	7.6200	6.8400	8.4000	0.00000
16	1	10.1333	8.4000	11.8667	0.00000
17	1	13.6000	11.8667	15.3333	0.00000
18	1	17.0667	15.3333	18.8000	0.00000
19	1	20.5333	18.8000	22.2667	0.00000
20	1	24.0000	22.2667	24.0000	0.00000

type 7 - wall flat plate conductor geometry

.....

wall perimeter	804.000 (in.)
wall thickness	24.0000 (in.)
no. of nodes (total)	20
material index (inside)	1
material index(outside)	0

radial noding information

node no.	material index	radial location	node boundaries		power fraction
			(inside)	(outside)	
1	1	0.0000	0.0000	0.0107	0.00000
2	1	0.0213	0.0107	0.0320	0.00000
3	1	0.0427	0.0320	0.0533	0.00000
4	1	0.0640	0.0533	0.0747	0.00000
5	1	0.0853	0.0747	0.0960	0.00000
6	1	0.1464	0.0960	0.1968	0.00000
7	1	0.2472	0.1968	0.2976	0.00000
8	1	0.3480	0.2976	0.3984	0.00000

9	1	0.4488	0.3984	0.4992	0.00000
10	1	0.5496	0.4992	0.6000	0.00000
11	1	1.3800	0.6000	2.1600	0.00000
12	1	2.9400	2.1600	3.7200	0.00000
13	1	4.5000	3.7200	5.2800	0.00000
14	1	6.0600	5.2800	6.8400	0.00000
15	1	7.6200	6.8400	8.4000	0.00000
16	1	10.1333	8.4000	11.8667	0.00000
17	1	13.6000	11.8667	15.3333	0.00000
18	1	17.0667	15.3333	18.8000	0.00000
19	1	20.5333	18.8000	22.2667	0.00000
20	1	24.0000	22.2667	24.0000	0.00000

type 8 - wall flat plate conductor geometry

.....

wall perimeter 10608.000 (in.)
wall thickness 24.0000 (in.)
no. of nodes (total) 20
material index (inside) 1
material index(outside) 0

radial noding information

node no.	material index	radial location	node boundaries (inside)	node boundaries (outside)	power fraction
----	-----	-----	-----	-----	-----
1	1	0.0000	0.0000	0.0107	0.00000
2	1	0.0213	0.0107	0.0320	0.00000
3	1	0.0427	0.0320	0.0533	0.00000
4	1	0.0640	0.0533	0.0747	0.00000
5	1	0.0853	0.0747	0.0960	0.00000
6	1	0.1464	0.0960	0.1968	0.00000
7	1	0.2472	0.1968	0.2976	0.00000
8	1	0.3480	0.2976	0.3984	0.00000
9	1	0.4488	0.3984	0.4992	0.00000
10	1	0.5496	0.4992	0.6000	0.00000
11	1	1.3800	0.6000	2.1600	0.00000
12	1	2.9400	2.1600	3.7200	0.00000
13	1	4.5000	3.7200	5.2800	0.00000

14	1	6.0600	5.2800	6.8400	0.00000
15	1	7.6200	6.8400	8.4000	0.00000
16	1	10.1333	8.4000	11.8667	0.00000
17	1	13.6000	11.8667	15.3333	0.00000
18	1	17.0667	15.3333	18.8000	0.00000
19	1	20.5333	18.8000	22.2667	0.00000
20	1	24.0000	22.2667	24.0000	0.00000

type 9 - wall flat plate conductor geometry

.....

wall perimeter	288.000 (in.)
wall thickness	24.0000 (in.)
no. of nodes (total)	20
material index (inside)	1
material index(outside)	0

radial noding information

node no.	material index	radial location	node boundaries (inside) (outside)		power fraction
----	-----	-----	-----	-----	-----
1	1	0.0000	0.0000	0.0107	0.00000
2	1	0.0213	0.0107	0.0320	0.00000
3	1	0.0427	0.0320	0.0533	0.00000
4	1	0.0640	0.0533	0.0747	0.00000
5	1	0.0853	0.0747	0.0960	0.00000
6	1	0.1464	0.0960	0.1968	0.00000
7	1	0.2472	0.1968	0.2976	8.00000
8	1	0.3480	0.2976	0.3984	0.00000
9	1	0.4488	0.3984	0.4992	0.00000
10	1	0.5496	0.4992	0.6000	0.00000
11	1	1.3800	0.6000	2.1600	0.00000
12	1	2.9400	2.1600	3.7200	0.00000
13	1	4.5000	3.7200	5.2800	0.00000
14	1	6.0600	5.2800	6.8400	0.00000
15	1	7.6200	6.8400	8.4000	0.00000
16	1	10.1333	8.4000	11.8667	0.00000
17	1	13.6000	11.8667	15.3333	0.00000
18	1	17.0667	15.3333	18.8000	0.00000

19	1	20.5333	18.8000	22.2667	0.00000
20	1	24.0000	22.2667	24.0000	0.00000

type 10 - wall flat plate conductor geometry

.....

wall perimeter **1656.000** (in.)
wall thickness **24.0000** (in.)
no. of nodes (total) **20**
material index (inside) **1**
material index(outside) **0**

radial **noding** information

node no.	material index	radial location	node boundaries (inside) (outside)		power fraction
----	-----	-----	-----	-----	-----
1	1	0.0000	0.0000	0.0107	0.00000
2	1	0.0213	0.0107	0.0320	0.00000
3	1	0.0427	0.0320	0.0533	0.00000
4	1	0.0640	0.0533	0.0747	0.00000
5	1	0.0853	0.0747	0.0960	0.00000
6	1	0.1464	0.0960	0.1968	0.00000
7	1	0.2472	0.1968	0.2976	0.00000
8	1	0.3480	0.2976	0.3984	0.00000
9	1	0.4488	0.3984	0.4992	0.00000
10	1	0.5496	0.4992	0.6000	0.00000
11	1	1.3800	0.6000	2.1600	0.00000
12	1	2.9400	2.1600	3.7200	0.00000
13	1	4.5000	3.7200	5.2800	0.00000
14	1	6.0600	5.2800	6.8400	0.00000
15	1	7.6200	6.8400	8.4000	0.00000
16	1	10.1333	8.4000	11.8667	0.00000
17	1	13.6000	11.8667	15.3333	0.00000
18	1	17.0667	15.3333	18.8000	0.00000
19	1	20.5333	18.8000	22.2667	0.00000
20	1	24.0000	22.2667	24.0000	0.00000

type 11 - wall \$1% plate conductor geometry

wall perimeter 1968,000 (in.)
 wall thickness 24,0000 (in.)
 no. of nodes (total) 20
 material index (inside) 1
 material index (outside) 0

radial nodding information

node	material	location	node boundaries	power
no.	index	radial	(inside) (outside)	fraction

1	1	0.0000	0.0107	0.00000
2	1	0.0213	0.0107	0.00000
3	1	0.0427	0.0320	0.00000
4	1	0.0640	0.0533	0.00000
5	1	0.0853	0.0747	0.00000
6	1	0.1464	0.0960	0.00000
7	1	0.2472	0.1968	0.00000
8	1	0.3480	0.2976	0.00000
9	1	0.4488	0.3984	0.00000
10	1	0.5496	0.4992	0.00000
11	1	1.3800	2.1600	0.00000
12	1	2.9400	3.7200	0.00000
13	1	4.5000	6.2800	0.00000
14	1	6.0600	8.8400	0.00000
15	1	7.6200	11.4000	0.00000
16	1	10.1333	15.8667	0.00000
17	1	13.6000	21.8000	0.00000
18	1	17.0667	29.7333	0.00000
19	1	20.5333	38.6667	0.00000
20	1	24.0000	48.6000	0.00000

type 12 - wall flat plate conductor geometry

wall perimeter 1416,000 (in.)
 wall thickness 24,0000 (in.)

no. of nodes (total) **20**
 material index (inside) **1**
 material index(outside) **0**

radial **nod**ing information

node no.	material index	radial location	node boundaries		power fraction
-----	-----	-----	(inside)	(outside)	-----
1	1	0.0000	0.0000	0.0107	0.00000
2	1	0.0213	0.0107	0.0320	0.00000
3	1	0.0427	0.0320	0.0533	0.00000
4	1	0.0640	0.0533	0.0747	0.00000
5	1	0.0853	0.0747	0.0960	0.00000
6	1	0.1464	0.0960	0.1968	0.00000
7	1	0.2472	0.1968	0.2976	0.00000
8	1	0.3480	0.2976	0.3984	0.00000
9	1	0.4488	0.3984	0.4992	0.00000
10	1	0.5496	0.4992	0.6000	0.00000
11	1	1.3800	0.6000	2.1600	0.00000
12	1	2.9400	2.1600	3.7200	0.00000
13	1	4.5000	3.7200	5.2800	0.00000
14	1	6.0600	5.2800	6.8400	0.00000
15	1	7.6200	6.8400	8.4000	0.00000
16	1	10.1333	8.4000	11.8667	0.00000
17	1	13.6000	11.8667	15.3333	0.00000
18	1	17.0667	15.3333	18.8000	0.00000
19	1	20.5333	18.8000	22.2667	0.00000
20	1	24.0000	22.2667	24.0000	0.00000

type 13 - wall flat plate conductor geometry

 wall perimeter **3708.000** (in.)
 wall thickness **24.0000** (in.)
 no. of nodes (total) **20**
 material index (inside) **1**
 material index(outside) **0**

```

radial nodding information
node material
no. index
-----
1
1
-----
material index(inside)
material index(outside)
0
I
no. of nodes (total)
20
wall thickness
24.0000 (in.)
wall perimeter
672.000 (in.)
-----
radial
location
-----
0.0000
0.0000
node boundaries
0.0000
0.0107
-----
power
fraction
0.00000

```

type 14 - wall flat plate conductor geometry

```

radial nodding information
node material
no. index
-----
1
1
-----
material index(inside)
material index(outside)
0
I
no. of nodes (total)
20
wall thickness
24.0000 (in.)
wall perimeter
672.000 (in.)
-----
radial
location
-----
0.0000
0.0000
node boundaries
0.0000
0.0107
-----
power
fraction
0.00000

```

20	1	ZD.0008	22.2667	22.2667	0.00000
19	1	20.5333	18.8000	22.2667	0.00000
18	1	17.0667	15.3333	18.8000	0.00000
17	1	13.6000	11.8667	15.3333	0.00000
16	1	10.1333	8.4000	11.8667	0.00000
15	1	7.6200	6.8400	8.4000	0.00000
14	1	6.8688	5.2800	6.8400	0.00000
13	1	4.5000	3.7200	5.2800	0.00000
12	1	2.9400	2.1688	3.7200	0.00000
11	1	1.3800	8.6008	2.1600	0.00000
10	1	0.5496	0.4992	8.6888	0.00000
9	1	0.4488	0.3984	0.4992	0.00000
8	1	0.3480	0.2976	0.3984	0.00000
7	1	0.2472	8.1968	0.2976	0.00000
6	1	0.1464	0.8960	8.1968	0.00000
5	1	0.0853	0.0747	8.0968	0.00000
4	1	0.0640	8.0533	0.0747	0.00000
3	1	0.0427	0.0320	0.0533	0.00000
2	1	0.0213	0.0107	0.0320	0.00000
1	1	8.8808	8.0000	0.0107	0.00000

2	1	0.0213	0.0107	0.0320	0.00000
3	1	0.0427	0.0320	0.0533	0.00000
4	1	0.0640	0.0533	0.0747	0.00000
5	1	0.0853	0.0747	0.0960	0.00000
6	1	0.1464	0.0960	0.1968	0.00000
7	1	0.2472	0.1968	0.2976	0.00000
8	1	0.3480	0.2976	0.3984	0.00000
9	1	0.4488	0.3984	0.4992	0.00000
10	1	0.5496	0.4992	0.6000	0.00000
11	1	1.3800	0.6000	2.1600	0.00000
12	1	2.9400	2.1600	3.7200	0.00000
13	1	4.5000	3.7200	5.2800	0.00000
14	1	6.0600	5.2800	6.8400	0.00000
15	1	7.6200	6.8400	8.4000	0.00000
16	1	10.1333	8.4000	11.8667	0.00000
17	1	13.6000	11.8667	15.3333	0.00000
18	1	17.0667	15.3333	18.8000	0.00000
19	1	20.5333	18.8000	22.2667	0.00000
20	1	24.0000	22.2667	24.0000	0.00000

type 15 - wall flat plate conductor geometry

wall perimeter 312.000 (in.)
wall thickness 24.0000 (in.)
no. of nodes (total) 20
material index (inside) 1
material index(outside) 0

radial noding information

node no.	material index	radial location	node boundaries		power fraction
-----	-----	-----	(inside)	(outside)	-----
1	1	0.0000	0.0000	0.0107	0.00000
2	1	0.0213	0.0107	0.0320	0.00000
3	1	0.0427	0.0320	0.0533	0.00000
4	1	0.0640	0.0533	0.0747	0.00000
5	1	0.0853	0.0747	0.0960	0.00000
6	1	0.1464	0.0960	0.1968	0.00000

7	1	0.2472	0.1968	0.2976	0.00000
8	1	0.3480	0.2976	0.3984	0.00000
9	1	0.4488	0.3984	0.4992	0.00000
10	1	0.5496	0.4992	0.6000	0.00000
11	1	1.3800	0.6000	2.1600	0.00000
12	1	2.9400	2.1600	3.7200	0.00000
13	1	4.5000	3.7200	5.2800	0.00000
14	1	6.0600	5.2800	6.8400	0.00000
15	1	7.6200	6.8400	8.4000	0.00000
16	1	10.1333	8.4000	11.8667	0.00000
17	1	13.6000	11.8667	15.3333	0.00000
18	1	17.0667	15.3333	18.8000	0.00000
19	1	20.5333	18.8000	22.2667	0.00000
20	1	24.0000	22.2667	24.0000	0.00000

type 16 - wall flat plate conductor geometry

.....

wall perimeter	2088.000 (in.)
wall thickness	24.0000 (in.)
no. of nodes (total)	20
material index (inside)	1
material index(outside)	0

radial noding information

node no.	material index	radial location	node boundaries (inside) (outside)		power fraction
1	1	0.0000	0.0000	0.0107	0.00000
2	1	0.0213	0.0107	0.0320	0.00000
3	1	0.0427	0.0320	0.0533	0.00000
4	1	0.0640	0.0533	0.0747	0.00000
5	1	0.0853	0.0747	0.0960	0.00000
6	1	0.1464	0.0960	0.1968	0.00000
7	1	0.2472	0.1968	0.2976	0.00000
8	1	0.3480	0.2976	0.3984	0.00000
9	1	0.4488	0.3984	0.4992	0.00000
10	1	0.5496	0.4992	0.6000	0.00000
11	1	1.3800	0.6000	2.1600	0.00000

12	1	2.9400	2.1600	3.7200	0.00000
13	1	4.5000	3.7200	5.2800	0.00000
14	1	6.0600	5.2800	6.8400	0.00000
15	1	7.6200	6.8400	8.4000	0.00000
16	1	10.1333	8.4000	11.8667	0.00000
17	1	13.6000	11.8667	15.3333	0.00000
18	1	17.0667	15.3333	18.8000	0.00000
19	1	20.5333	18.8000	22.2667	0.00000
20	1	24.0000	22.2667	24.0000	0.00000

type 17 - wall flat plate conductor geometry

wall perimeter 2544.000 (in.)
wall thickness 24.0000 (in.)
no. of nodes (total) 20
material index (inside) 1
material index(outside) 0

radial noding information

node no.	material index	radial location	node boundaries (inside)	node boundaries (outside)	power fraction
-----	-----	-----	-----	-----	-----
1	1	0.0000	0.0000	0.0107	0.00000
2	1	0.0213	0.0107	0.0320	0.00000
3	1	0.0427	0.0320	0.0533	0.00000
4	1	0.0640	0.0533	0.0747	0.00000
5	1	0.0853	0.0747	0.0960	0.00000
6	1	0.1464	0.0960	0.1968	0.00000
7	1	0.2472	0.1968	0.2976	0.00000
8	1	0.3480	0.2976	0.3984	0.00000
9	1	0.4488	0.3984	0.4992	0.00000
10	1	0.5496	0.4992	0.6000	0.00000
11	1	1.3800	0.6000	2.1600	0.00000
12	1	2.9400	2.1600	3.7200	0.00000
13	1	4.5000	3.7200	5.2800	0.00000
14	1	6.0600	5.2800	6.8400	0.00000
15	1	7.6200	6.8400	8.4000	0.00000
16	1	10.1333	8.4000	11.8667	0.00000

17	1	13.6000	11.8667	15.3333	0.00000
18	1	17.0667	15.3333	18.8000	0.00000
19	1	20.5333	18.8000	22.2667	0.00000
20	1	24.0000	22.2667	24.0000	0.00000

type 18 - wall flat plate conductor geometry

wall perimeter 804.000 (in.)
 wall thickness 24.0000 (in.)
 no. of nodes (total) 20
 material index (inside) 1
 material index (outside) 0

radial nodding information

node no.	material index	radial location	node boundaries (ins~ a)	power fraction
1	1	0.0000	0.0088	0.00000
2	1	0.0213	0.0107	0.00000
3	1	0.0427	0.0320	0.00000
4	1	0.0640	0.0533	0.00000
5	1	0.0853	0.0747	0.00000
6	1	0.1064	0.0960	0.00000
7	1	0.1277	0.1168	0.00000
8	1	0.1480	0.1376	0.00000
9	1	0.1688	0.1584	0.00000
10	1	0.1896	0.1792	0.00000
11	1	0.2100	0.1992	0.00000
12	1	0.2300	0.2192	0.00000
13	1	0.2500	0.2392	0.00000
14	1	0.2700	0.2592	0.00000
15	1	0.2900	0.2792	0.00000
16	1	0.3100	0.2992	0.00000
17	1	0.3300	0.3192	0.00000
18	1	0.3500	0.3392	0.00000
19	1	0.3700	0.3592	0.00000
20	1	0.3900	0.3792	0.00000

6.000 68.600 12.500 62.800 20.000 54.500 27.500 39.300 1500.000
 0.000

1

axial and/or injection boundary conditions

boundary type property specification

- 1= pressure and enthalpy (axial) pressure
- 2= flow and enthalpy (axial) mass flow
- 3= zero axial flow zero
- 4= injected flow and enthalpy injected flow
- 5= pressure sink and enthalpy sink pressure

channel index	axial node	boundary type (see above)	specified property (see above)	enthalpy
2	1	2	1.00	1249.40
15	3	1	14.70	145.30
1	1	3	0.00	0.00
3	1	3	0.00	0.00
4	1	3	0.00	0.00
5	1	3	0.00	0.00
6	1	3	0.00	0.00
7	1	3	0.00	0.00
8	1	3	0.00	0.00
9	1	3	0.00	0.00
10	1	3	0.00	0.00
11	1	3	0.00	0.00
12	1	3	0.00	0.00
1	2	3	0.00	0.00
2	2	3	0.00	0.00
3	2	3	0.00	0.00
4	2	3	0.00	0.00
5	2	3	0.00	0.00
8	2	3	0.00	0.00
12	2	3	0.00	0.00

13	2	3	0.00	0.00
16	2	3	0.00	0.00
17	2	3	0.00	0.00
18	2	3	0.00	0.00

0

zero crossflow boundary conditions

gap	axial
index	node

18 channelswillbeprinted

1	2	3	4	5	6	7	8	9	1	0
11	12	13	14	15	16	17	18			

0 0 rods will be printed

0 0 gapswillbeprinted

1 trac major edit

time = 0.000e+00 seconds delt = 0.000e+00 seconds time steps + 0 oitno= 0

average outer iteration count over the last 0 time steps was 0.00e+00

the last minimum number of outer iterations was 0 at step 8

the last maximum number of outer iterations was 0 at step 0

last minimum number of inner iterations was 0 at step 0

current convergence limits and limitation counts

delamx	delamx	delmx	delvmx	delprx
0.000e+00	0.000e+00	0.000e+00	0.000e+00	0.000e+00
0	0	0	0	0

cptime = 5.640e-01

```

*****
*          neu time domain reached
* minimum maximum time long short graphics dump
* time time domain edit interval interval
* step step and interval interval interval
*
* 1.000e-04 1.000e-03 1.000e-01 1.000e+06 1.000e+06 5.000e+02
*****

```

```

interval for a.s.b. oupbub is 0.02000 seconds.
time step ratio = 1.000e+00

```

```

1 trac major edit
1 trac major edit
1 trac major edit
1 trac major edit
1 trac major edit

```

```

*****
*          neu time domain reached
* minimum maximum time long short graphics dump
* time time domain edit interval interval
* step step and interval interval interval
*
* 1.000e-04 5.000e-02 1.000e+00 1.000e+06 1.000e+06 5.000e+02
*****

```

```

interval for a.s.b. oupbub is 0.10000 seconds.
time sbap ratio = 1.000e+00

```

```

1 trac major edit
1 trac major edit
1 trac major edit
1 trac major edit
1 trac major edit
1 trac major edit
1 trac major edit

```


30.03	2.0724e+01	2.0702e+01	2.0625e+01	2.0625e+01	2.0601e+01	2.0601e+01	2.0627e+01	2.0601e+01	2.3936e+01
2.0726e+01									
31.03	2.0673e+01	2.0677e+01	2.0639e+01	2.0650e+01	2.0639e+01	2.0640e+01	2.0655e+01	2.0640e+01	2.3936e+01
2.0674e+01									
32.03	2.0679e+01	2.0682e+01	2.0675e+01	2.0656e+01	2.0671e+01	2.0671e+01	2.0649e+01	2.0671e+01	2.3954e+01
2.0678e+01									
33.03	2.0715e+01	2.0716e+01	2.0712e+01	2.0733e+01	2.0701e+01	2.0701e+01	2.0729e+01	2.0701e+01	2.3967e+01
2.0715e+01									
34.03	2.0715e+01	2.0715e+01	2.0737e+01	2.0737e+01	2.0735e+01	2.0735e+01	2.0748e+01	2.0735e+01	2.3973e+01
2.0715e+01									
35.03	2.0682e+01	2.0681e+01	2.0736e+01	2.0736e+01	2.0760e+01	2.0760e+01	2.0728e+01	2.0761e+01	2.3971e+01
2.0682e+01									
36.00	2.0640e+01	2.0640e+01	2.0714e+01	2.0720e+01	2.0744e+01	2.0745e+01	2.0723e+01	2.0745e+01	2.3959e+01
2.0640e+01									

1

pressure (psia)

time	room 11	room 12	room 13	room 14	room 15	room 16	room 17	room 18	room
0.00	1.4713e+01	1.4713e+01	1.4707e+01	1.4707e+01	1.4707e+01	1.4707e+01	1.4707e+01	1.4700e+01	
0.02	1.4713e+01	1.4713e+01	1.4707e+01	1.4707e+01	1.4742e+01	1.4707e+01	1.4707e+01	1.4700e+01	
0.04	1.4714e+01	1.4713e+01	1.4707e+01	1.4707e+01	1.4769e+01	1.4707e+01	1.4707e+01	1.4700e+01	
0.06	1.4716e+01	1.4714e+01	1.4707e+01	1.4707e+01	1.4742e+01	1.4709e+01	1.4708e+01	1.4700e+01	
0.08	1.4720e+01	1.4715e+01	1.4707e+01	1.4708e+01	1.4695e+01	1.4714e+01	1.4713e+01	1.4700e+01	
0.10	1.4729e+01	1.4719e+01	1.4708e+01	1.4710e+01	1.4665e+01	1.4726e+01	1.4721e+01	1.4702e+01	
0.20	1.4818e+01	1.4812e+01	1.4748e+01	1.4793e+01	1.4932e+01	1.4839e+01	1.4812e+01	1.4786e+01	
0.28	1.4885e+01	1.4875e+01	1.4789e+01	1.4873e+01	1.4971e+01	1.4914e+01	1.4879e+01	1.4868e+01	
0.40	1.4955e+01	1.4875e+01	1.4836e+01	1.4876e+01	1.4949e+01	1.4976e+01	1.4949e+01	1.4869e+01	
0.46	1.4988e+01	1.4893e+01	1.4871e+01	1.4880e+01	1.5118e+01	1.5001e+01	1.4981e+01	1.4873e+01	
0.59	1.5040e+01	1.4949e+01	1.4939e+01	1.4939e+01	1.6471e+01	1.5042e+01	1.5033e+01	1.4931e+01	
0.69	1.5075e+01	1.5002e+01	1.4986e+01	1.4996e+01	1.7641e+01	1.5075e+01	1.5068e+01	1.4989e+01	
0.79	1.5113e+01	1.5056e+01	1.5031e+01	1.5050e+01	1.8092e+01	1.5113e+01	1.5106e+01	1.5043e+01	
0.89	1.5151e+01	1.5110e+01	1.5078e+01	1.5102e+01	1.7582e+01	1.5153e+01	1.5144e+01	1.5096e+01	
0.99	1.5171e+01	1.5154e+01	1.5123e+01	1.5147e+01	1.6469e+01	1.5169e+01	1.5165e+01	1.5141e+01	
2.03	1.5352e+01	1.5825e+01	1.5563e+01	1.5721e+01	1.4681e+01	1.5338e+01	1.5343e+01	1.5709e+01	
3.03	1.6389e+01	1.6434e+01	1.6370e+01	1.6412e+01	1.7473e+01	1.6416e+01	1.6382e+01	1.6405e+01	
4.03	1.6836e+01	1.6844e+01	1.6824e+01	1.6837e+01	1.7322e+01	1.6835e+01	1.6828e+01	1.6829e+01	
5.03	1.7173e+01	1.7159e+01	1.7151e+01	1.7164e+01	1.7488e+01	1.7167e+01	1.7166e+01	1.7158e+01	
6.03	1.7534e+01	1.7618e+01	1.7506e+01	1.7533e+01	1.7626e+01	1.7530e+01	1.7526e+01	1.7525e+01	
7.03	1.7816e+01	1.7822e+01	1.7804e+01	1.7809e+01	1.7771e+01	1.7812e+01	1.7809e+01	1.7801e+01	
8.03	1.8062e+01	1.8061e+01	1.8045e+01	1.8053e+01	1.7850e+01	1.8057e+01	1.8055e+01	1.8045e+01	
9.03	1.8278e+01	1.8275e+01	1.8258e+01	1.8268e+01	1.7920e+01	1.8272e+01	1.8270e+01	1.8260e+01	
10.03	1.8478e+01	1.8474e+01	1.8457e+01	1.8467e+01	1.7983e+01	1.8472e+01	1.8470e+01	1.8459e+01	

11.03	1.8670e+01	1.8667e+01	1.8648e+01	1.8659e+01	1.8044e+01	1.8664e+01	1.8662e+01	1.8651e+01		
12.03	1.8857e+01	1.8853e+01	1.8833e+01	1.8845e+01	1.8102e+01	1.8850e+01	1.8849e+01	1.8837e+01		
13.03	1.9032e+01	1.9026e+01	1.9010e+01	1.9020e+01	1.8157e+01	1.9025e+01	1.9024e+01	1.9012e+01		
14.03	1.9200e+01	1.9195e+01	1.9178e+01	1.9188e+01	1.8210e+01	1.9193e+01	1.9192e+01	1.9180e+01		
15.03	1.9360e+01	1.9356e+01	1.9337e+01	1.9348e+01	1.8260e+01	1.9353e+01	1.9352e+01	1.9340e+01		
16.03	1.9504e+01	1.9500e+01	1.9481e+01	1.9492e+01	1.8305e+01	1.9496e+01	1.9496e+01	1.9484e+01		
17.03	1.9641e+01	1.9637e+01	1.9618e+01	1.9629e+01	1.8348e+01	1.9634e+01	1.9633e+01	1.9621e+01		
18.03	1.9766e+01	1.9762e+01	1.9746e+01	1.9754e+01	1.8387e+01	1.9758e+01	1.9758e+01	1.9746e+01		
19.03	1.9883e+01	1.9879e+01	1.9863e+01	1.9871e+01	1.8424e+01	1.9875e+01	1.9875e+01	1.9863e+01		
20.03	1.9993e+01	1.9990e+01	1.9973e+01	1.9982e+01	1.8458e+01	1.9986e+01	1.9985e+01	1.9973e+01		
21.03	2.0086e+01	2.0083e+01	2.0069e+01	2.0075e+01	1.8487e+01	2.0078e+01	2.0078e+01	2.0067e+01		
22.03	2.0176e+01	2.0173e+01	2.0159e+01	2.0165e+01	1.8515e+01	2.0168e+01	2.0168e+01	2.0156e+01		
23.03	2.0258e+01	2.0255e+01	2.0243e+01	2.0247e+01	1.8541e+01	2.0250e+01	2.0250e+01	2.0238e+01		
24.03	2.0334e+01	2.0331e+01	2.0319e+01	2.0323e+01	1.8565e+01	2.0326e+01	2.0326e+01	2.0314e+01		
25.03	2.0407e+01	2.0404e+01	2.0392e+01	2.0396e+01	1.8587e+01	2.0399e+01	2.0399e+01	2.0387e+01		
26.03	2.0461e+01	2.0459e+01	2.0449e+01	2.0451e+01	1.8604e+01	2.0452e+01	2.0452e+01	2.0443e+01		
27.03	2.0540e+01	2.0506e+01	2.0499e+01	2.0498e+01	1.8618e+01	2.0533e+01	2.0531e+01	2.0489e+01		
28.03	2.0651e+01	2.0537e+01	2.0529e+01	2.0531e+01	1.8628e+01	2.0642e+01	2.0643e+01	2.0522e+01		
29.03	2.0686e+01	2.0573e+01	2.0565e+01	2.0565e+01	1.8640e+01	2.0677e+01	2.0677e+01	2.0557e+01		
30.03	2.0726e+01	2.0630e+01	2.0593e+01	2.0618e+01	1.8655e+01	2.0718e+01	2.0718e+01	2.0610e+01		
31.03	2.0674e+01	2.0648e+01	2.0632e+01	2.0647e+01	1.8659e+01	2.0665e+01	2.0665e+01	2.0638e+01		
32.03	2.0678e+01	2.0655e+01	2.0663e+01	2.0641e+01	1.8670e+01	2.0670e+01	2.0670e+01	2.0633e+01		
33.03	2.0715e+01	2.0733e+01	2.0693e+01	2.0721e+01	1.8681e+01	2.0707e+01	2.0707e+01	2.0713e+01		
34.03	2.0715e+01	2.0736e+01	2.0727e+01	2.0739e+01	1.8689e+01	2.0707e+01	2.0707e+01	2.0731e+01		
35.03	2.0682e+01	2.0737e+01	2.0752e+01	2.0719e+01	1.8688e+01	2.0674e+01	2.0674e+01	2.0711e+01		
36.00	2.0640e+01	2.0720e+01	2.0737e+01	2.0715e+01	1.8680e+01	2.0632e+01	2.0632e+01	2.0707e+01		

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temperature (degrees f.)

time	room 1	room 2	room 3	room 4	room 5	room 6	room 7	room 8	room 9
0.00	8.6556e+01	8.6556e+01	8.6556e+01	8.6556e+01	8.6556e+01	8.6556e+01	8.6556e+01	8.6556e+01	8.6556e+01
0.02	8.6613e+01	9.8033e+01	8.6556e+01	8.6556e+01	8.6556e+01	8.6556e+01	8.6556e+01	8.6556e+01	8.6621e+01
0.04	8.6927e+01	1.0731e+02	8.6567e+01	8.6556e+01	8.6556e+01	8.6556e+01	8.6556e+01	8.6556e+01	8.7073e+01
0.06	8.7514e+01	1.1476e+02	8.6617e+01	8.6559e+01	8.6557e+01	8.6557e+01	8.6561e+01	8.6556e+01	8.6995e+01

0.08	8.8201e+01	1.2105e+02	8.6719e+01	8.6573e+01	8.6563e+01	8.6563e+01	8.6580e+01	8.6556e+01	8.6390e+01	8.6658e+01
0.10	8.8818e+01	1.2679e+02	8.6860e+01	8.6615e+01	8.6581e+01	8.6579e+01	8.6623e+01	8.6556e+01	8.6357e+01	8.6788e+01
0.20	9.0299e+01	1.5456e+02	8.7747e+01	8.7680e+01	8.7060e+01	8.7030e+01	8.7542e+01	8.6638e+01	8.8513e+01	8.8066e+01
0.28	9.1697e+01	1.7569e+02	8.8159e+01	8.8391e+01	8.7579e+01	8.7488e+01	8.8400e+01	8.7050e+01	8.9412e+01	8.8916e+01
0.40	9.4552e+01	2.0339e+02	8.8615e+01	8.8374e+01	8.7974e+01	8.8042e+01	8.8464e+01	8.8009e+01	9.2850e+01	8.9628e+01
0.46	9.6259e+01	2.1779e+02	8.8852e+01	8.8573e+01	8.8315e+01	8.8439e+01	8.8524e+01	8.8505e+01	9.3408e+01	8.9922e+01
0.59	9.9839e+01	2.4324e+02	8.9633e+01	8.9210e+01	8.9145e+01	8.9200e+01	8.9174e+01	8.9250e+01	9.0620e+01	9.0403e+01
0.69	1.0280e+02	2.6027e+02	9.0369e+01	8.9800e+01	8.9707e+01	8.9732e+01	8.9808e+01	8.9704e+01	9.4984e+01	9.0787e+01
0.79	1.0598e+02	2.7598e+02	9.1138e+01	9.0402e+01	9.0224e+01	9.0244e+01	9.0412e+01	9.0156e+01	1.0340e+02	9.1252e+01
0.89	1.0883e+02	2.8234e+02	9.1980e+01	9.1001e+01	9.0740e+01	9.0772e+01	9.1004e+01	9.0644e+01	1.2718e+02	9.1738e+01
0.99	1.1038e+02	2.8684e+02	9.2779e+01	9.1489e+01	9.1236e+01	9.1290e+01	9.1502e+01	9.1170e+01	1.5563e+02	9.1923e+01
2.03	1.3066e+02	3.4556e+02	1.1168e+02	9.9139e+01	9.5397e+01	9.6351e+01	9.8131e+01	9.3260e+01	1.7662e+02	9.4195e+01
3.03	1.5409e+02	3.8510e+02	1.5324e+02	1.0689e+02	1.0565e+02	1.1277e+02	1.0934e+02	1.0480e+02	1.7706e+02	1.0846e+02
4.03	1.7408e+02	4.0423e+02	1.6232e+02	1.1192e+02	1.1164e+02	1.2301e+02	1.1575e+02	1.0963e+02	1.7720e+02	1.1409e+02
5.03	1.9270e+02	4.1491e+02	1.6634e+02	1.1586e+02	1.0538e+02	1.2898e+02	1.2059e+02	1.1319e+02	1.7729e+02	1.1871e+02
6.03	2.1053e+02	4.2161e+02	1.6881e+02	1.2027e+02	1.3569e+02	1.2696e+02	1.2598e+02	1.1690e+02	1.7715e+02	1.2393e+02
7.03	2.2654e+02	4.2508e+02	1.7039e+02	1.2335e+02	1.4419e+02	1.3218e+02	1.2984e+02	1.1980e+02	1.7839e+02	1.2807e+02
8.03	2.4103e+02	4.2685e+02	1.7153e+02	1.2511e+02	1.4973e+02	1.3583e+02	1.3310e+02	1.2218e+02	1.7900e+02	1.3176e+02
9.03	2.5420e+02	4.2779e+02	1.7239e+02	1.2660e+02	1.5328e+02	1.3913e+02	1.3590e+02	1.2429e+02	1.7954e+02	1.3506e+02
10.03	2.6645e+02	4.2821e+02	1.7312e+02	1.2784e+02	1.5592e+02	1.4210e+02	1.3834e+02	1.2624e+02	1.8002e+02	1.3818e+02

31.03	3.6866e+02	4.2180e+02	1.7936e+02	1.3996e+02	1.6381e+02	1.6701e+02	1.5319e+02	1.4550e+02	1.8483e+02
1.7445e+02									
32.03	3.6860e+02	4.2080e+02	1.7907e+02	1.3993e+02	1.6391e+02	1.6729e+02	1.5308e+02	1.4565e+02	1.8493e+02
1.7446e+02									
33.03	3.6880e+02	4.2013e+02	1.7907e+02	1.4058e+02	1.6397e+02	1.6757e+02	1.5381e+02	1.4579e+02	1.8500e+02
1.7504e+02									
34.03	3.6826e+02	4.1891e+02	1.7897e+02	1.4053e+02	1.6406e+02	1.6791e+02	1.5390e+02	1.4597e+02	1.8503e+02
1.7496e+02									
35.03	3.6628e+02	4.1704e+02	1.7878e+02	1.4044e+02	1.6403e+02	1.6815e+02	1.5367e+02	1.4606e+02	1.8502e+02
1.7444e+02									
36.00	3.6234e+02	4.1462e+02	1.7835e+02	1.4022e+02	1.6368e+02	1.6799e+02	1.5357e+02	1.4578e+02	1.8496e+02
1.7384e+02									

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temperature (degrees f.)

time	room 11	room 12	room 13	room 14	room 15	room 16	room 17	room 18	room
0.00	8.6556e+01	8.6556e+01	8.6556e+01	8.6556e+01	8.6556e+01	8.6556e+01	8.6556e+01	8.6556e+01	8.6556e+01
0.02	8.6556e+01	8.6556e+01	8.6556e+01	8.6556e+01	8.6936e+01	8.6556e+01	8.6556e+01	8.6556e+01	8.6556e+01
0.04	8.6560e+01	8.6556e+01	8.6556e+01	8.6556e+01	8.7195e+01	8.6558e+01	8.6558e+01	8.6556e+01	8.6556e+01
0.06	8.6581e+01	8.6559e+01	8.6557e+01	8.6558e+01	8.6866e+01	8.6578e+01	8.6573e+01	8.6556e+01	8.6556e+01
0.08	8.6635e+01	8.6573e+01	8.6561e+01	8.6568e+01	8.6329e+01	8.6643e+01	8.6623e+01	8.6561e+01	8.6561e+01
0.10	8.6735e+01	8.6614e+01	8.6576e+01	8.6599e+01	8.5989e+01	8.6771e+01	8.6721e+01	8.6583e+01	8.6583e+01
0.20	8.7760e+01	8.7669e+01	8.7026e+01	8.7530e+01	9.4485e+01	8.8049e+01	8.7744e+01	8.7524e+01	8.7524e+01
0.28	8.8527e+01	8.8381e+01	8.7481e+01	8.8430e+01	1.1703e+02	8.8885e+01	8.8497e+01	8.8453e+01	8.8453e+01
0.40	8.9330e+01	8.8381e+01	8.8019e+01	8.8460e+01	1.3658e+02	8.9579e+01	8.9279e+01	8.8460e+01	8.8460e+01
0.46	8.9706e+01	8.8574e+01	8.8411e+01	8.8510e+01	1.4735e+02	8.9862e+01	8.9641e+01	8.8501e+01	8.8501e+01
0.59	9.0314e+01	8.9206e+01	8.9166e+01	8.9164e+01	1.6120e+02	9.0319e+01	9.0219e+01	8.9160e+01	8.9160e+01
0.69	9.0731e+01	8.9797e+01	8.9692e+01	8.9800e+01	1.6730e+02	9.0678e+01	9.0609e+01	8.9799e+01	8.9799e+01
0.79	9.1182e+01	9.0399e+01	9.0196e+01	9.0401e+01	1.6973e+02	9.1106e+01	9.1024e+01	9.0401e+01	9.0401e+01
0.89	9.1648e+01	9.0998e+01	9.0713e+01	9.0987e+01	1.7100e+02	9.1549e+01	9.1448e+01	9.0986e+01	9.0986e+01
0.99	9.1897e+01	9.1487e+01	9.1216e+01	9.1485e+01	1.7225e+02	9.1717e+01	9.1673e+01	9.1486e+01	9.1486e+01
2.03	9.4241e+01	9.8874e+01	9.6027e+01	9.7750e+01	1.7692e+02	9.3565e+01	9.3619e+01	9.7675e+01	9.7675e+01
3.03	1.0803e+02	1.0690e+02	1.0471e+02	1.0535e+02	1.7721e+02	1.0511e+02	1.0476e+02	1.0499e+02	1.0499e+02
4.03	1.1403e+02	1.1190e+02	1.0956e+02	1.0993e+02	1.7846e+02	1.0942e+02	1.0937e+02	1.0927e+02	1.0927e+02
5.03	1.1874e+02	1.1567e+02	1.1301e+02	1.1344e+02	1.7950e+02	1.1277e+02	1.1278e+02	1.1250e+02	1.1250e+02
6.03	1.2393e+02	1.2022e+02	1.1667e+02	1.1741e+02	1.8035e+02	1.1638e+02	1.1637e+02	1.1605e+02	1.1605e+02
7.03	1.2810e+02	1.2139e+02	1.1967e+02	1.2035e+02	1.8122e+02	1.1914e+02	1.1914e+02	1.1864e+02	1.1864e+02
8.03	1.3181e+02	1.2275e+02	1.2206e+02	1.2290e+02	1.8169e+02	1.2149e+02	1.2151e+02	1.2087e+02	1.2087e+02
9.03	1.3512e+02	1.2381e+02	1.2415e+02	1.2513e+02	1.8210e+02	1.2353e+02	1.2356e+02	1.2281e+02	1.2281e+02
10.03	1.3825e+02	1.2478e+02	1.2608e+02	1.2717e+02	1.8247e+02	1.2540e+02	1.2545e+02	1.2456e+02	1.2456e+02
11.03	1.4130e+02	1.2577e+02	1.2791e+02	1.2911e+02	1.8282e+02	1.2718e+02	1.2723e+02	1.2622e+02	1.2622e+02
12.03	1.4431e+02	1.2679e+02	1.2968e+02	1.3097e+02	1.8316e+02	1.2889e+02	1.2896e+02	1.2782e+02	1.2782e+02

13.03	1.4716e+02	1.2780e+02	1.3134e+02	1.3269e+02	1.8348e+02	1.3048e+02	1.3056e+02	1.2929e+02		
14.03	1.4992e+02	1.2881e+02	1.3291e+02	1.3430e+02	1.8378e+02	1.3199e+02	1.3209e+02	1.3067e+02		
15.03	1.5257e+02	1.2977e+02	1.3437e+02	1.3581e+02	1.8407e+02	1.3342e+02	1.3353e+02	1.3198e+02		
16.03	1.5495e+02	1.3062e+02	1.3568e+02	1.3712e+02	1.8432e+02	1.3468e+02	1.3480e+02	1.3312e+02		
17.03	1.5724e+02	1.3148e+02	1.3691e+02	1.3835e+02	1.8456e+02	1.3587e+02	1.3600e+02	1.3418e+02		
18.03	1.5933e+02	1.3228e+02	1.3805e+02	1.3944e+02	1.8478e+02	1.3693e+02	1.3707e+02	1.3513e+02		
19.03	1.6129e+02	1.3305e+02	1.3907e+02	1.4044e+02	1.8499e+02	1.3792e+02	1.3807e+02	1.3599e+02		
20.03	1.6315e+02	1.3381e+02	1.4002e+02	1.4136e+02	1.8518e+02	1.3883e+02	1.3900e+02	1.3679e+02		
21.03	1.6470e+02	1.3444e+02	1.4082e+02	1.4211e+02	1.8534e+02	1.3957e+02	1.3975e+02	1.3743e+02		
22.03	1.6622e+02	1.3506e+02	1.4156e+02	1.4282e+02	1.8549e+02	1.4029e+02	1.4048e+02	1.3803e+02		
23.03	1.6758e+02	1.3564e+02	1.4224e+02	1.4344e+02	1.8563e+02	1.4091e+02	1.4112e+02	1.3856e+02		
24.03	1.6885e+02	1.3618e+02	1.4284e+02	1.4401e+02	1.8576e+02	1.4149e+02	1.4170e+02	1.3904e+02		
25.03	1.7007e+02	1.3670e+02	1.4340e+02	1.4454e+02	1.8589e+02	1.4203e+02	1.4225e+02	1.3948e+02		
26.03	1.7095e+02	1.3708e+02	1.4382e+02	1.4490e+02	1.8598e+02	1.4238e+02	1.4262e+02	1.3976e+02		
27.03	1.7228e+02	1.3738e+02	1.4416e+02	1.4517e+02	1.8606e+02	1.4299e+02	1.4323e+02	1.3996e+02		
28.03	1.7420e+02	1.3758e+02	1.4431e+02	1.4531e+02	1.8611e+02	1.4389e+02	1.4416e+02	1.4004e+02		
29.03	1.7473e+02	1.3784e+02	1.4451e+02	1.4547e+02	1.8617e+02	1.4405e+02	1.4433e+02	1.4013e+02		
30.03	1.7537e+02	1.3830e+02	1.4464e+02	1.4581e+02	1.8626e+02	1.4428e+02	1.4456e+02	1.4039e+02		
31.03	1.7470e+02	1.3839e+02	1.4487e+02	1.4590e+02	1.8628e+02	1.4365e+02	1.4394e+02	1.4043e+02		
32.03	1.7471e+02	1.3839e+02	1.4504e+02	1.4567e+02	1.8634e+02	1.4352e+02	1.4383e+02	1.4017e+02		
33.03	1.7529e+02	1.3907e+02	1.4518e+02	1.4627e+02	1.8640e+02	1.4371e+02	1.4403e+02	1.4067e+02		
34.03	1.7523e+02	1.3901e+02	1.4537e+02	1.4627e+02	1.8644e+02	1.4354e+02	1.4387e+02	1.4062e+02		
35.03	1.7472e+02	1.3895e+02	1.4547e+02	1.4590e+02	1.8644e+02	1.4308e+02	1.4342e+02	1.4023e+02		
36.00	1.7414e+02	1.3874e+02	1.4520e+02	1.4569e+02	1.8640e+02	1.4255e+02	1.4290e+02	1.3999e+02		

1

relative humidity

time	room 1	room 2	room 3	room 4	room 5	room 6	room 7	room 8	room 9	room 10
(sec)										
0.00	5.7746e-01	5.7746e-01	5.7746e-01	5.7746e-01	5.7746e-01	5.7746e-01	5.7746e-01	5.7746e-01	5.7746e-01	5.7746e-01
0.02	5.7665e-01	6.7485e-01	5.7745e-01	5.7746e-01	5.7746e-01	5.7746e-01	5.7746e-01	5.7746e-01	5.7649e-01	5.7745e-01
0.04	5.7262e-01	7.0945e-01	5.7730e-01	5.7745e-01	5.7745e-01	5.7745e-01	5.7745e-01	5.7746e-01	5.7013e-01	5.7737e-01
0.06	5.6588e-01	7.2969e-01	5.7655e-01	5.7741e-01	5.7744e-01	5.7743e-01	5.7738e-01	5.7746e-01	5.7226e-01	5.7697e-01
0.08	5.5926e-01	7.4072e-01	5.7504e-01	5.7720e-01	5.7735e-01	5.7735e-01	5.7710e-01	5.7745e-01	5.8257e-01	5.7594e-01

32.03 9.2653e-02 7.1024e-02 1.0603e+00 8.4686e-01 1.0511e+00 1.0507e+00 9.4848e-01 3.0145e-01 1.0598e+00
 3.3535e-01
 33.03 9.2793e-02 7.1665e-02 1.0603e+00 8.4343e-01 1.0487e+00 1.0522e+00 9.4759e-01 3.0265e-01 1.0598e+00
 3.3475e-01
 34.03 9.3420e-02 7.2608e-02 1.0603e+00 8.4918e-01 1.0461e+00 1.0524e+00 9.5619e-01 3.0387e-01 1.0598e+00
 3.3550e-01
 35.03 9.5134e-02 7.3943e-02 1.0603e+00 8.5325e-01 1.0455e+00 1.0539e+00 9.6656e-01 3.0518e-01 1.0598e+00
 3.3795e-01
 36.00 9.8948e-02 7.5562e-02 1.0603e+00 8.5762e-01 1.0511e+00 1.0600e+00 9.7260e-01 3.0352e-01 1.0598e+00
 3.4079e-01

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relative humidity

time	room 11	room 12	room 13	room 14	room 15	room 16	room 17	room 18	room
0.00	5.7746e-01	5.7746e-01	5.7746e-01	5.7746e-01	5.7746e-01	5.7746e-01	5.7746e-01	5.7746e-01	5.7746e-01
0.02	5.7745e-01	5.7746e-01	5.7746e-01	5.7746e-01	6.0964e-01	5.7746e-01	5.7746e-01	5.7746e-01	5.7746e-01
0.04	5.7739e-01	5.7745e-01	5.7746e-01	5.7745e-01	7.2911e-01	5.7742e-01	5.7743e-01	5.7746e-01	5.7746e-01
0.06	5.7708e-01	5.7741e-01	5.7745e-01	5.7743e-01	8.3785e-01	5.7712e-01	5.7720e-01	5.7745e-01	5.7745e-01
0.08	5.7629e-01	5.7720e-01	5.7738e-01	5.7728e-01	8.9599e-01	5.7616e-01	5.7646e-01	5.7738e-01	5.7738e-01
0.10	5.7480e-01	5.7658e-01	5.7716e-01	5.7681e-01	9.2532e-01	5.7427e-01	5.7500e-01	5.7706e-01	5.7706e-01
0.20	5.6001e-01	5.6114e-01	5.7050e-01	5.6316e-01	1.3052e+00	5.5572e-01	5.6008e-01	5.6325e-01	5.6325e-01
0.28	5.4946e-01	5.5102e-01	5.6387e-01	5.5031e-01	1.1570e+00	5.4396e-01	5.4938e-01	5.5000e-01	5.5000e-01
0.40	5.3903e-01	5.5102e-01	5.5615e-01	5.4989e-01	1.1213e+00	5.3445e-01	5.3854e-01	5.4991e-01	5.4991e-01
0.46	5.3442e-01	5.4831e-01	5.5059e-01	5.4920e-01	1.0526e+00	5.3062e-01	5.3360e-01	5.4933e-01	5.4933e-01
0.59	5.2743e-01	5.3956e-01	5.4008e-01	5.4012e-01	1.0324e+00	5.2451e-01	5.2584e-01	5.4018e-01	5.4018e-01
0.69	5.2300e-01	5.3155e-01	5.3290e-01	5.3145e-01	1.0397e+00	5.1977e-01	5.2068e-01	5.3146e-01	5.3146e-01
0.79	5.1855e-01	5.2356e-01	5.2613e-01	5.2341e-01	1.0603e+00	5.1419e-01	5.1526e-01	5.2341e-01	5.2341e-01
0.89	5.1432e-01	5.1577e-01	5.1930e-01	5.1571e-01	1.0654e+00	5.0850e-01	5.0980e-01	5.1574e-01	5.1574e-01
0.99	5.1223e-01	5.0954e-01	5.1275e-01	5.0929e-01	1.0648e+00	5.0637e-01	5.0692e-01	5.0928e-01	5.0928e-01
2.03	4.9914e-01	4.4537e-01	4.5502e-01	4.3740e-01	1.0621e+00	4.8367e-01	4.8301e-01	4.3679e-01	4.3679e-01
3.03	4.3793e-01	4.6232e-01	3.7654e-01	3.8483e-01	1.0612e+00	3.6784e-01	3.7067e-01	3.6634e-01	3.6634e-01
4.03	4.2061e-01	4.6249e-01	3.4754e-01	3.6154e-01	1.0512e+00	3.3471e-01	3.3506e-01	3.3202e-01	3.3202e-01
5.03	4.1104e-01	4.6406e-01	3.3231e-01	3.4870e-01	1.0511e+00	3.1208e-01	3.1198e-01	3.0900e-01	3.0900e-01
6.03	4.0249e-01	5.8370e-01	3.2115e-01	3.3856e-01	1.0610e+00	2.9029e-01	2.9028e-01	2.8617e-01	2.8617e-01
7.03	3.9654e-01	6.6329e-01	3.1422e-01	3.3353e-01	1.0610e+00	2.7546e-01	2.7534e-01	2.7109e-01	2.7109e-01
8.03	3.9176e-01	6.9928e-01	3.0946e-01	3.2981e-01	1.0609e+00	2.6387e-01	2.6365e-01	2.5905e-01	2.5905e-01
9.03	3.8777e-01	7.3176e-01	3.0606e-01	3.2734e-01	1.0609e+00	2.5464e-01	2.5435e-01	2.4931e-01	2.4931e-01
10.03	3.8406e-01	7.6170e-01	3.0345e-01	3.2564e-01	1.0609e+00	2.4678e-01	2.4642e-01	2.4103e-01	2.4103e-01
11.03	3.8031e-01	7.8775e-01	3.0143e-01	3.2477e-01	1.0609e+00	2.3980e-01	2.3939e-01	2.3357e-01	2.3357e-01
12.03	3.7641e-01	8.1006e-01	2.9988e-01	3.2491e-01	1.0609e+00	2.3351e-01	2.3304e-01	2.2684e-01	2.2684e-01
13.03	3.7252e-01	8.2625e-01	2.9874e-01	3.2586e-01	1.0609e+00	2.2806e-01	2.2753e-01	2.2095e-01	2.2095e-01
14.03	3.6856e-01	8.2929e-01	2.9796e-01	3.2737e-01	1.0609e+00	2.2320e-01	2.2260e-01	2.1570e-01	2.1570e-01

17.03	0.00000	0.00109	0.00000	0.00000	0.00000	1.00000	0.00000	0.00000	0.00000
18.03	0.00000	0.00121	0.00000	0.00000	0.00000	1.00000	0.00000	0.00000	0.00000
19.03	0.00000	0.00133	0.00000	0.00000	0.00000	1.00000	0.00000	0.00000	0.00000
20.03	0.00000	0.00146	0.00000	0.00000	0.00000	1.00000	0.00000	0.00000	0.00000
21.03	0.00000	0.00160	0.00000	0.00000	0.00000	1.00000	0.00000	0.00000	0.00000
22.03	0.00000	0.00173	0.00000	0.00000	0.00000	1.00000	0.00000	0.00000	0.00000
23.03	0.00000	0.00187	0.00000	0.00000	0.00000	1.00000	0.00000	0.00000	0.00000
24.03	0.00000	0.00201	0.00000	0.00000	0.00000	1.00000	0.00000	0.00000	0.00000
25.03	0.00000	0.00215	0.00000	0.00000	0.00000	1.00000	0.00000	0.00000	0.00000
26.03	0.00000	0.00229	0.00000	0.00000	0.00000	1.00000	0.00000	0.00000	0.00000
27.03	0.00000	0.00243	0.00000	0.00000	0.00000	1.00000	0.00000	0.00000	0.00000
28.03	0.00000	0.00254	0.00000	0.00000	0.00000	1.00000	0.00000	0.00000	0.00000
29.03	0.00000	0.00269	0.00000	0.00000	0.00000	1.00000	0.00000	0.00000	0.00000
30.03	0.00000	0.00285	0.00000	0.00000	0.00000	1.00000	0.00000	0.00000	0.00000
31.03	0.00000	0.00292	0.00000	0.00000	0.00000	1.00000	0.00000	0.00000	0.00000
32.03	0.00000	0.00303	0.00000	0.00000	0.00000	1.00000	0.00000	0.00000	0.00000
33.03	0.00001	0.00322	0.00000	0.00000	0.00000	1.00000	0.00000	0.00000	0.00000
34.03	0.00001	0.00328	0.00000	0.00000	0.00000	1.00000	0.00000	0.00000	0.00000
35.03	0.00001	0.00334	0.00000	0.00000	0.00000	1.00000	0.00000	0.00000	0.00000
36.00	0.00001	0.00339	0.00000	0.00000	0.00000	1.00000	0.00000	0.00000	0.00000

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<p>The INGEN (INput GENerator) computer program has been developed as a preprocessor to simplify input generation for the COBRA-NC computer program. INGEN uses several empirical correlations and geometric assumptions to simplify the data input requirements for the COBRA-NC computer code. The simplified input scheme is obtained at the expense of much flexibility provided by COBRA-NC. For more complex problems requiring additional flexibility however, INGEN may be used to provide a skeletal input file to which the more detailed input may be added. This report describes the input requirements for INGEN and describes the algorithms and correlations used to generate the COBRA-NC input</p>		
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