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# THORS - A HIGH-TEMPERATURE SODIUM TEST FACILITY RATED AT 2.0 MW

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### ABSTRACT

The Thermal-Hydraulic Out-of-Reactor Safety (THORS) facility at Oak Ridge National Laboratory (ORNL) is a high-temperature sodium test facility operated for the United States Breeder Reactor Safety Program. The facility is primarily used for testing large simulated Liquid-Metal Fast Breeder Reactor (LMFBR) fuel subassemblies. The facility has recently been upgraded to provide a 2.0-MW test bundle power input and heat removal capability. A new test section, which will be capable of operating at 980°C and which will accommodate a 217-pin bundle, has also been added. A 61-pin bundle is currently under test in the facility. A description of the test facility is presented, along with a brief summary of the 8-year operating history of this safety-related test facility.

### INTRODUCTION

The breeder reactor programs in the United States and abroad have generated a strong need for improved understanding of core thermal-hydraulic phenomena in sodium-cooled reactors and for detailed investigations of safety-related occurrences in the core. The requirements for information on local flow and temperature patterns in unperturbed fuel subassemblies have been identified by the Fast Test Reactor core designers. The evaluation of the damage potential of flow coastdowns, partial inlet blockages, heated zone blockages, and blockages arising from fuel failure because of loss of flow is necessary for assurance of Liquid-Metal Fast Breeder Reactor (LMFBR) safety. It is also important that the reactor designers have experimental data to validate and develop practical analytical models by which data obtained from (relatively) small experiments can be applied to a full-size reactor.

A large-scale sodium flow facility, originally called the Fuel Failure Mockup Facility [1], was built in 1970 for testing 19-pin, simulated LMFBR fuel subassemblies. In 1976, the name of the facility was changed to the Thermal-Hydraulic Out-of-Reactor Safety (THORS) Facility.

### FACILITY DESCRIPTION

The THORS Facility is a large, high-temperature sodium system in which test assemblies designed specifically to simulate LMFBR core segments are subjected to thermal and hydraulic testing at normal and off-normal Fast Test Reactor operating conditions. The test assemblies are composed of bundles of electrically heated pins having the same axial power density and external configuration as the LMFBR fuel pins; the reactor fuel is thus simulated by special purpose cartridge electric heaters [fuel pin simulators (FPSs)].

The test facility shown in Fig. 1 includes a 40-liter per sec centrifugal pump, a 40-liter per sec electromagnetic (EM) pump, two test section housings into which the test bundles are inserted, a 2.0-MW test bundle power supply, a 2.0-MW heat dump system, a 0.5-MW heat dump system that can be used for lower power testing, an expansion tank at the test section outlet to simulate the free liquid surface of the reactor, a sodium purification system, a bypass line in parallel with the larger test section housing to simulate the flow passages among the many other reactor fuel elements, and instrumentation needed to monitor the facility parameters. An isometric view of the THORS facility is shown in Fig. 2, and Table I presents the principal capabilities of the facility.

The new test section housing is fabricated from Hastelloy X material and is rated for operation at 980°C and 690 kPa. It is long enough to accommodate simulated full-length Clinch River Breeder Reactor (CRBR) fuel pins and large enough in diameter to accommodate a 217-pin bundle. The original 19-pin test section housing is still installed and can be operated in parallel with the new one. Figure 3 is a photograph of the new housing and a 61-pin test bundle, which is ready for installation. Figure 4 shows the bundle and housing installed in the facility; the 2.0-MW heat exchanger



Fig. 1. THORS facility flow diagram.





	TABLE 1						
Principal	Design	Characteristics	of	the	THORS	Facility	

Test Section Housing Design Pressure	690 kPa 980°C
Test Section Housing Operating Temperature	300-980°C for 1000 hr
Test Section FPS Power Heat Removal Capability	2500 kW @ 540°C
Facility Piping System Design Pressure Facility Piping System Design Temperature	690 kPa 700°C

is also shown. In the 2-MW sodium-to-air heat exchanger, sodium at temperatures of up to 700°C flows in parallel through forty 22-mm serpentine stainless steel tubes.

The FPSs are connected to a variable voltage power supply with a voltage range from 40 to 400 V and a total load capacity of 2.0 MW. A pair of silicon-controlled rectifiers (SCRs) are provided for each of 37 circuits. (For the 61-pin bundle, two FPSs are connected in parallel.) The SCRs act as switches that are electronically controlled to provide power control from 0 to 100% in 1% increments [2]. The individual FPSs are electronically



Fig. 3. THORS facility photograph showing test section housing and 61-pin bundle.



Fig. 4. THORS facility photograph showing 61-pin test bundle housing and 2.0-MW heat exchanger.

protected to prevent electrical damage in the event of a short circuit [3]. Figure 5 is a schematic diagram of the electrical supply system for the test bundles.

The flow diagram of the THORS facility (Fig. 1) shows the relevant loop instrumentation. Table II gives the type, range, and accuracy of the instrumentation [4-7].

Facility piping is trace-heated with  $\sim 350$  tubular cartridge heaters. The preheat temperatures are monitored by  $\sim 700$  sheath-type thermocouples, which are connected to multipoint recorders.



Fig. 5. Sixty-one pin-bundle connections to 2.0-MW power supply. (Power is limited to 1.3 MW in this configuration.)

### TABLE II

#### Accuracy Range Measurement Туре 0-1030 kPa +1% Diaphragm NaK Pressure 0-690 kPa +1% Pressure Sensor Differential Diaphragm NaK 0-5080 mm W.C. +1% Differential Pressure Pressure Sensor 0-1090°C Chromel-Alume1 +1% Temperature Thermocouple 190-6050 liter per min +1% Flow Magnetic 0-190 liter per min +1% Flowmeter Single & Twin 0-1220 mm +1% Level I-tube Probes Thermal Watt 0-30 mV Power +1% Converters Hydrophone 0.1-120,000 Hz 0.3 V/psi Boiling Accoustic Sensors

### THORS Loop Instrumentation

Data are recorded during actual bundle testing using a 512-channel data acquisition system (DAS) controlled by a PDP-8E computer. Data are logged at the rate of up to 10,000 points per sec and stored on magnetic tape for subsequent processing and display. At the THORS DAS operating console, data may be displayed on a high-speed lineprinter or on two cathode-ray-tube (CRT) terminals. A data management system [8] has been developed to provide operating and data logging programs and the capability of translating DAS-generated data into a tape format that can be used in IBM computers.

# TEST BUNDLES

An elevation view of a test bundle (bundle 9A) installed in the test section housing is shown in Fig. 6. It consists of 61 electrically heated 5.84-mm-diam pins spaced by 1.42-mm-diam helical wire wrap spacers on a 305-mm pitch. This bundle has a heated length of 914 mm with an axial chopped-cosine heat flux distribution. The unheated simulated fission gas plena, located downstream of the heated section in a portion of the dummy rod length, are 1537 mm long.

Figure 7a is a photograph of the partially assembled bundle, Fig. 7b is a close-up photograph of the 6l FPSs installed in the tubesheet, and Fig. 7c is a photograph of the duct at the end of the FPS assembly.

A typical FPS used in the test bundles is shown in Fig. 8. Voltage is applied to the heating element through the copper lead at the open end of the FPS, and the electric circuit is completed at the opposite end, where the element is grounded through the end plug to the sodium. This particular FPS is rated at 51.8 kW/m. The FPSs are described in Refs. 9 and 10.



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Fig. 6. Typical THORS bundle (9A) test section assembly.



(c)

Fig. 7. THORS bundle 9A. (a) 61 pin bundle in partial assembly; (b) 61 FPSs installed in bundle 9 tubesheet; (c) duct end of FPS assembly.



(b)

# FACILITY OPERATION

Seven test bundles have been built since testing was initiated in 1970, and they have been operated in 12 different configurations. Table III shows the operating history of these bundles. Bundles 1A and 1B were unblocked bundles in a scalloped duct [11]. Bundle 2, which was enclosed in a hexagonal duct, was originally designed to obtain thermal-hydraulic data; in this configuration it was referred to as bundle 2A [12]. After completion of the test program with this configuration, the bundle was still viable and was inverted in the test section and operated with blockage plates of various sizes installed at the inlet of the bundle. In this latter configuration, it was referred to as bundle 2B [13]. Bundle 3A [14], which was in a scalloped duct with dummy wire-wrap segments on dummy edge rods and which contained a six-channel central blockage in the heated zone, was used for single-phase experiments. Bundle 3B [15,16] was identical to bundle 3A, but its test program (which followed the bundle 5 tests) included quasi-steadystate sodium boiling and inert gas injection. Bundle 5, which was enclosed in a hexagonal duct with half-size (0.17-mm) wire spacers between the FPSs and the duct wall, was designed for operation in four configurations. Bundles 5A [17] and 5B [18] contained a blockage along one of the hexagonal sides that blocked one-third of the flow area. Tests for bundles 5C [18] and 5D [19] were run with the blockage plate removed. Bundle 5D was the first

### Table III

THORS Facility Operating Experie	ence
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Bundle dentification	Number of Pins	Blockage Configuration	Reactor Simulation	Operating Time (hr)	
1A	19	None	Thermodynamic Simulation Only	1,300	
2A	19	None	Thermodynamic Simulation Only	)	
2B	19	13- and 14-Channel Inlet	Thermodynamic Simulation Only	3,010	
18	19	None	Thermodynamic Simulation Only	894	
3A	19	6-Channel in Heated Zone	Thermodynamic Simulation Only	3,039	
3B <sup><i>a</i>, <sup><i>b</i></sup></sup>	19	6-Channel in Heated Zone	Thermodynamic Simulation Only	537	
5A,5B,5C	19	12-Channel Edge Gap	Thermodynamic Simulation Only	3,252	
50 <sup><i>a</i>, <sup><i>b</i></sup></sup>	19	None	Thermodynamic Simulation Only	2,827	
6A	19	None	FFTF Simulation	7,864	
3C	31 <sup>°</sup>	6-Channel in Heated Zone	FFTF Simulation	3,666	
9	61	None	CRBR Simulation	d	
			Total	26,389 <sup>d</sup>	

<sup>a</sup>Boiling tests.

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 $^{b}$ Boiling tests with gas injection.

<sup>C</sup>Nineteen central pins, 12 guard heat pins.

<sup>d</sup>Bundle 9 testing in progress.

THORS bundle taken to temperatures high enough to produce steady-state sodium boiling; these tests were run in October 1974. Bundle 6A was designed with a low thermal capacity duct surrounding the bundle. The main objectives for this bundle were to establish steady-state temperature distributions at various flow-power ratios for comparison with data from previous bundles [20]. The bundle was also used for transient free convection tests [21] and for transient sodium boiling tests (including several partial dryout) [22-24]. The objective of bundle 3C tests was to investigate axial and radial boiling propagation behind a blockage. A six-channel blockage plate was attached to the central pin in the heated zone, as in bundles 3A and 3B. An unheated section was added downstream of the FPSs to give a simulation of the fission gas region in the reactor. The test program for bundle 9, the 61-pin bundle now installed in the facility, will incorporate all tests that have been run with the smaller unblocked bundles. Hence, a comparison of results can be made for 19- and 61-pin bundles. This comparison should give an insight into the effect of size on test bundle performance.

Sodium has been circulated in the THORS facility at temperatures as high as  $700^{\circ}$ C; sodium temperatures in the test section, however, have reached  $1010^{\circ}$ C. Power levels have been as high as 36.0 kW/m in each pin.

Plans are being made for fabricating and testing additional bundles. Under consideration at the present time are (1) a bundle to investigate the effects of duct heat capacity on bundle internal temperatures, (2) test bundles for advanced fuels, and (3) a bundle to measure the effects of pin bowing.

### SUMMARY AND CONCLUSION

The THORS Facility has been in use since 1970 to obtain data for fast reactor safety technology from simulated LMFBR fuel subassemblies. The system has recently been upgraded to 2.0-MW test bundle power input and heat rejection capability. Seven different bundles have been built and operated in 12 different configurations. The facility has logged over 27,000 hr at sodium temperatures ranging up to  $1010^{\circ}$ C. Sodium boiling tests have been run to investigate axial and radial boiling propagation in simulated reactor subassemblies. Experiments with inlet blockages and heated zone blockages have produced data to provide an insight into the problems associated with fast reactor safety. Thermal-hydraulic data obtained from tests in bundles of 19-, 31-, and 61-pin sizes can be used to provide core designers with experimental data to verify and/or develop computer models.

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### REFERENCES

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- 1. A. G. GRINDELL and R. E. MacPHERSON, "Final Systems Design Description of the Failed Fuel Mockup (FFM) of the Liquid Metal Fast Breeder Reactor," ORNL/TM-3656 (September 1972).
- M. M. YAROSH and P. A. GNADT, "The Intermediate Potassium System A Rankine Cycle Test 2. Facility," ORNL-4025, pp. 151-156 (October 1968).
- 3. R. D. STULTING, "Electronic Circuit for the Protection of Cartridge Heaters Simulating Fast Reactor Fuel Pins," ORNL/TM-3693 (July 1972).
- W. R. MILLER, "High Temperature Pressure Transmitter Evaluation," ORNL-2483 (May 1958). 4.
- R. G. AFFEL, G. H. BURGER, and C. L. PEARCE, "Calibration and Testing of 2 and 3 1/2 inch 5. Magnetic Flowmeters for High Temperature NaK Service," ORNL-2793 (March 1960). M. M. YAROSH and P. A. GNADT, "The Intermediate Potassium System - A Rankine Cycle Test
- 6. Facility," ORNL-4025, pp. 39-45 (October 1968).
- 7. W. H. SIDES, W. H. LEAVELL, and R. F. SAXE, "Detection of Sodium Boiling in Fuel Failure Mockup," ORNL/TM-5355 (July 1976).
- 8. N. E. CLAPP, "The Data Management System for the Thermal-Hydraulic Out-of-Reactor Safety Facility Computor Controlled Data Acquisition System Configuration for Bundle 3C Operation," ORNL/TM-6745 (1979).
- R. E. MacPHERSON, D. L. CLARK, and R. G. DONNELLY, "High Performance Heater for LMFBR Fuel Rod Simulation Status Report," ORNL/TM-4234 (May 1973). 9.
- W. E. BAUCUM et al., "State of the Art of Fuel Pin Simulators for LMFBR Out-of-Reactor Safety Tests Status Report," ORNL/TM-5889 (September 1977). 10.
- 11. M. H. FONTANA et al., "Temperature Distribution in a 19-Rod Simulated LMFBR Fuel Assembly in a Scalloped Duct Data," ORNL/TM-4939 (November 1975). M. H. FONTANA et al., "Temperature Distribution in a 19-Rod Simulated LMFBR Fuel Assembly
- 12. M. H. FONTANA et al., in a Hexagonal Duct (Fuel Failure Mockup Bundle 2A) - Record of Experimental Data, ORNL/TM-4113 (September 1973).
- 13. M. H. FONTANA et al., "Temperature Distribution in a 19-Rod Simulated LMFBR Fuel Rod Bundle with Inlet Blockages (FFM bundle 2B)," ORNL/TM-4367 (January 1974).
- 14. M. H. FONTANA et al., "Temperature Distribution in a 19-Rod Simulated LMFBR Fuel Assembly with a Six-Channel Internal Blockage (Fuel Failure Mockup Bundle 3A) - Record of Experimental Data," ORNL/TM-5101 (March 1976).
- 15. J. L. WANTLAND et al., "Sodium Boiling Tests in a 19-Rod Bundle with a Central Blockage --Record of Experimental Data for Fuel Failure Mockup Bundle 3B," ORNL/TM-5458 (October 1976).
- 16. N. HANUS et al., "Local Sodium Boiling in a Partially Blocked Simulated Subassembly (THORS Bundle 3B), " ORNL/TM-5862 (June 1977).
- 17. M. H. FONTANA et al., "Temperature Distribution in a 19-Rod Simulated LMFBR Fuel Assembly with an Edge Blockage (Out-of-Reactor Test for ANL FEFP Pl Experiment) — Record of Experimental Data for Fuel Failure Mockup Bundle 5A," ORNL/TM-4633 (November 1974).
- M. H. FONTANA et al., "Temperature Distribution in a 19-Rod Simulated LMFBR Fuel Assembly 18. With and Without an Edge Blockage (Out-of-Reactor Tests for ANL SLSP Pl Experiment) -Record of Experimental Data for Fuel Failure Mockup Bundles 5B and 5C," ORNL/TM-5003 (January 1976).
- 19. J. L. WANTLAND et al., "Transient Temperature Distribution in a 19-Rod Bundle During Operation to Sodium Boiling - Record of Experimental Data for Fuel Failure Mockup Bundle 5D. ORNL/TM-5580 (February 1977).
- 20. J. L. WANTLAND et al., "Steady State Tests in a 19-Pin Full Length Simulated LMFBR Fuel Assembly - Record of Steady State ExperimentalData for THORS Bundle 6A," ORNL/TM-6106 (March 1978).
- 21.
- R. J. RIBANDO, "Free Convection Tests in Bundle 6A," ORNL/TM-6778 (June 1979). THORS Staff, "Sodium Boiling in a Full Length Simulated Fuel Assembly (THORS Bundle 6A) Record of Experimental Data," ORNL/TM-6553 (January 1979). 22.
- J. T. HAN and C. T. TOMLINSON, "SAS3A Simulation for a 19-Pin Dryout Experiment," Trans. 23. Am. Nucl. Soc., 28, 438 (1978). P. W. GARRISON, "A Simple Transient Analysis of The THORS Bundle 6A Boiling Test Results,"
- 24. Trans. Am. Nucl. Soc., 28, 440 (1978).
- 25. THORS Staff, "Steady State Sodium Tests in a 19-Pin Internally Guard Heated Simulated LMFBR Fuel Assembly with a Six Channel InternalBlockage - Record of Experimental Data for THORS Bundle 3C," ORNL/TM-6498 (February 1979).
- THORS Staff, "Boiling and Transient Tests in a 19-Pin Internally Guard Heated Simulated 26. LMFBR Fuel Assembly with a Six Channel Internal Blockage - Record of Experimental Data for THORS Bundle 3C," ORNL/TM-6792 (May 1979).