

27
9-11-81
24 Sept 81
715

(11)

B7008

LBL-12987



Lawrence Berkeley Laboratory

UNIVERSITY OF CALIFORNIA

EARTH SCIENCES DIVISION

MASTER

PROGRAM ROCMAS: INTRODUCTION AND USER'S GUIDE

J. Noorishad and M.S. Ayatollahi

September 1980



LEGAL NOTICE

This book was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor any agency thereof, nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof.

Printed in the United States of America
Available from
National Technical Information Service
U.S. Department of Commerce
5285 Port Royal Road
Springfield, VA 22161
Price Code A05

PROGRAM ROCMAS: INTRODUCTION AND USER'S GUIDE

J. Noorishad and M. S. Ayatollahi

Earth Sciences Division
Lawrence Berkeley Laboratory
University of California
Berkeley, California 94720



September 1980

This work was supported by the Assistant Secretary for Nuclear Energy, Office of Waste Isolation of the U. S. Department of Energy under contract W-7405-ENG-48. Funding for this project is administered by the Office of Nuclear Waste Isolation at Battelle Memorial Institute.



TABLE OF CONTENTS

	<u>Page</u>
INTRODUCTION	1
I. GOVERNING EQUATIONS	1
Pressure-Strain Equation	2
Stress-Strain Relation	2
Load Balance	3
II. NUMERICAL METHOD	4
Solution Scheme	6
III. COMPUTER CODE	7
Documentation and Availability	7
Spatial Grid	7
Material Properties	7
Fluid Properties	8
Initial Conditions	8
Boundary Conditions	8
Time Stepping and Solution Control	8
Output	8
IV. VALIDATION	9
V. APPLICATION	11
VI. SUMMARY	17
VII. REFERENCES	13
VIII. USER'S GUIDE	16
APPENDIX I. SAMPLE PROBLEM WITH SAMPLE INPUT OUTPUT	27
Sample Problem	29
Sample Input Data Preparation for Coupled Problems	33
Sample Output for Uncoupled Problem	37
I. General parameters and material properties	37
II. Displacement and pressure results	38
III. Stress and flow results	39
APPENDIX II. LISTING OF FORTRAN IV SOURCE PROGRAM	41

INTRODUCTION

ROCMAS (ROCK MASS) is a finite-element program for coupled flow and stress in deformable, saturated, fractured rock medium. The two-dimensional code combines the capability of isothermal transient pressure analysis and stress-strain analysis in formations with discrete fractures and porous blocks. Coupling of the pressure field and the mechanical deformation is founded on the extension of Biot's consolidation theory for porous elastic medium to nonlinear fracture behavior. The current version of the model is described by Noorishad [18]. Summary of early developments and related information are in Ayatollahi [1]. The early version of this code is known as PORFRC.

I. GOVERNING EQUATIONS

In this model, the fluid movement and the solid deformation are coupled. Each point in space, either inside a discrete fracture or within a rock block, has a pressure variable P and a solid displacement vector \bar{u} . The pressure field determines the fluid flow. The coupling between P and \bar{u} can be described in the following loop. As the pressure changes, the effective stress acting on the rock solid changes accordingly and affects the displacement or strain of the solid. The displacement of solid changes the flow path of fluid and results in changes in the pressure field. The last coupling step is especially important for fractures. The fracture flow is very sensitive to the aperture $2b$. The fracture-specific permeability $k^f = (2b)^2/12$ for parallel-plate laminar flow is used in this model.

Pressure-Strain Equation

The mathematical form of the coupling between the fluid flow and solid displacement can be written down as a set of three equations for the pressure-strain, strain-stress, and stress-load balance relations. The first fluid flow equation is

$$\frac{1}{M^i} \frac{\partial P}{\partial t} - \alpha^i \frac{\partial \epsilon}{\partial t} = \nabla \cdot \frac{k^i}{\mu} \nabla P$$

where α^i and M^i ($i =$ fractures or rock medium blocks) are material properties (Biot constants) representing the responses of fluid mass content to changes in pressure and changes in volumetric strain ϵ . Depending on the boundary conditions, the derivative $\partial \epsilon / \partial t$ in some cases can be approximated in terms of the pressure derivative $\partial P / \partial t$. The fluid flow equation will be reduced to a simple transient pressure equation with the storage coefficient in front of $\partial P / \partial t$ determined by the porosity and compressibilities of fluid and void structures.

Stress-Strain Relation

In more general cases, the volumetric strain $\epsilon = \epsilon_{xx} + \epsilon_{zz}$ depends on the effective stress field. The pressure counteracts normal to the fluid-solid interfaces. The effective stress-strain relation can be formally written in the form of Hook's Law [2-5]:

$$\tau = \alpha^i P \bar{1} = \bar{C}^i : \epsilon$$

For isotropic elastic porous rock medium, the components of the tensor \bar{C}^i can

be expressed in terms of two elastic constants, e.g., Young's modulus and Poisson's ratio. For anisotropic, inelastic deformable fractures, the stress-strain-strain relation is very nonlinear. In this model, a nonlinear normal stress-normal displacement relation and a nonlinear shear stress-shear displacement relation are used [12]. The normal and shear stiffness (change of stress per unit change of displacement) as functions of stresses characterize the fracture behavior. The displacement \bar{u} is simply related to the strain $\bar{\epsilon}$ by the component definition:

$$\epsilon_{i,j} = 0.5 \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right)$$

Load Balance

The third equation for the unknowns P , $\bar{\tau}$ and $\bar{\epsilon}$ is Newton's first law of static equilibrium applied to an infinitesimal volume element of the fluid-filled medium

$$\nabla \cdot \bar{\tau} + \rho_s \bar{f} = 0$$

where ρ_s is the bulk mass density and \bar{f} is the body force. One body force or volumetric force is the gravity. Both the gravity effects on the fluid and rock can be taken into account. Gravitational drainage of fluid can be modeled.

II. NUMERICAL METHOD

Having established the governing and constitutive relations for fractures and solids from structural and fluid flow analysis points of view, the media under consideration could be thought to be composed of two materials with known behaviors. Analysis of such media for coupled stress and fluid flow behavior is made feasible by application of a numerical method. The method starts with adoption of a variational principle [8,9]. The variational form, written for general initial and boundary conditions, includes all the terms of the static-structural analysis variational and those of the transient fluid flow analysis in porous media. A coupling term links the two functions [1,18]. A finite-element discretization is used to discretize the space domain. The two-dimensional space is decomposed into finite element quadrilateral domains with four-corner nodes[22]. Each node has the values of three variables: the pressure P and the two components of solid displacement \bar{u} . Isoparametric bilinear polynomial basis functions are used to interpolate from the nodal values to the space within an element representing the porous rock medium. For a fracture, it is assumed that the aperture is small and fluid flow is along the fracture surfaces. The pressure difference between adjacent nodes across the aperture is negligible and a one-dimensional element can be used for interpolating between two end point pressures [21]. For the fracture displacements, it is convenient to take the same spatial (global) coordinates for each pair of points across the small aperture for the four-corner element. However, the relative movements of the surfaces in the direction vertical to the fracture plane and along the fracture are important for

the structure analysis. The fracture element in terms of these relative displacements is used [12].

Taking variation of the discretized variational principle with respect to u and p results in the following matrix equations:

$$[K] \{\bar{u}\} + [C] \{p\} = \{F\}$$

$$[C]^T \{\bar{u}\} + ([E] + I * [H]) \{p\} = I * \{Q\}$$

where the matrix $[K]$ contains the coefficients of the stiffness of stress displacement of both inelastic fractures and elastic medium, $[C]$ the Biot coupling coefficients, $[E]$ fluid storage coefficients, $[H]$ fluid hydraulic conductivities, and $\{Q\}$ the fluid boundary fluxes. The column vector $\{\bar{u}\}$ contains the $2N$ nodal values of \bar{u} for the m porous nodes and $N - m$ fracture nodes, $\{p\}$ the N values of p , and $\{F\}$ the body force and boundary loads.

Time Discretization: The notation $I *$ in the matrix equation represents the time integration from 0 to t . To step from t to $t + \Delta t$, this model uses a predictor-corrector scheme. The solution is first predicted at $t + \Delta t$ with

$2 \times 2 \times 1$

$$I * p_{\hat{t}} = A(t + \Delta t) = \int_0^{t + \Delta t} P(\tau) d\tau = A(t) + \frac{1}{2} \Delta t (P_t + P_{t + \Delta t})$$

and then it is corrected by linear interpolation

$$I * p_t = A(t + \Delta t) = A(t) + \frac{1}{2} \Delta t (P_t + P_{t + \Delta t})$$

the unknown at $t+\Delta t$ is given by

$$P_{t+\Delta t} = P_t + \frac{1}{\theta} (P_{t+\theta\Delta t} + P_t)$$

It is noted that $\theta = 1$ is the central differencing Crank-Nicholson scheme. The coefficient $\theta > 1$ is used to damp out the numerical oscillation while slightly slowing down the convergence rate [20].

Solution Scheme

The nonlinear behavior of fracture stress-displacement is dealt with by the stiffness perturbation technique [12] during each time step. The stiffness matrix depends on the displacement when the displacement are out of the linear range. Iterations proceed until the stiffness matrix stabilizes within convergent criteria.

Within one iteration the matrix equation of $\{u\}$ and $\{P\}$ is solved by a direct procedure. The matrix is decomposed into lower and upper triangular matrices by the Gaussian LU decomposition method [2]. This reduces the matrix equation into two triangular systems which can be solved by backward and forward substitution procedures.

III. COMPUTER CODE

Documentation and Availability

The code is written in FORTRAN IV and presently being used on the CDC 7600 at LBL. Set-up of the data follows the organization of other finite-element programs at the University of California, Berkeley. Familiar options of two-dimensional finite-element (2-D FE) stress and strain analysis codes and two-dimensional finite-element (2-D FE) fluid flow codes are included in this code.

Spatial Grid

The two-dimensional grid consists of four-corner quadrilateral elements for the porous rock medium and two-node elements for the discrete fractures. The fractures can extend from one boundary to another, intersect each other, or can be isolated in the porous rock medium. An axisymmetric grid is also used.

Material Properties

The constant permeability of the porous rock medium and the initial aperture of the fracture are input parameters. For coupled calculations, the pressure- and stress-induced changes in displacement will be used to update the aperture and the fracture permeability.

The parameters α^i in the fluid flow equation for the porous rock medium and fracture can be estimated in general from the porosity and the compressibility of fluid as $1/(\alpha C_f)$. The coupling constants α^i are dimensionless.

$\alpha^i = 0$ decouples the pressure calculations from the stress-strain analysis.

For material with highly incompressible solid grains, $\alpha \approx 1$.

The mechanical properties required are Young's modulus and Poisson's ratio for the elastic porous rock medium and the initial normal stiffness, tangential stiffness, cohesion, and angle of friction for the fracture.

Fluid Properties

The fluid density and viscosity are input parameters.

Initial Conditions

Distribution of stresses, pressure and displacement can be specified at initial or program restarting time.

Boundary Conditions

Pressure and flux boundary conditions can be specified for the fluid flow. Static load and displacement boundary conditions can be specified for the stress-strain analysis.

Time Stepping and Solution Control

The time step can be increased logarithmically. A convergent criterion is specified on the stiffness difference in the iteration-perturbation procedure to handle the nonlinear fracture behavior.

Output

At the end of each time step, the pressure, displacement and the flow flux and the stress components on the elements can be printed. Graphic output of the mesh with the plot of the principal components of stress, and displacement are generated in the program.

IV. VALIDATION

The code is developed from an early iterative finite element program with steady state flow and static force-displacement analysis in jointed formation with impermeable rock [17]. Most of the efforts to validate this code are on the transient fluid flow behavior in fractures embedded in porous rock medium. Validation of the capability to handle coupling between transient fluid flow and stress-strain analysis is limited due to absence of both the analytic solutions and other numerical results. The documented tests [1] on the transient fluid flow in porous media and in fractures will be listed below.

1. Continuous Finite-Radius Well Source: The early time transient pressure responses of an axisymmetric flow to a producing well are compared with the analytic solution of Mueller and Witherspoon [15].
2. Finite Axisymmetric Aquifer: The late time pressure responses with no flow as well as constant outer boundaries are compared with the analytic solutions of Muskat [16].
3. Vertical Fractures: The pressure responses for a single vertical fracture and two perpendicular vertical fractures intersecting a well at the center of a rectangular porous medium are compared with the analytic solutions of Raghavan [19]. Geometry, mesh, input data, and the results for the latter problem are given at the end.
4. Vertical Fracture Near a Well: The pressure responses for an observation well in a system with a fracture not intersecting, but aligned with a producing

and an observation well, are compared with the analytic solution of Heber-Cinco et al. [13].

5. Horizontal Fracture: The pressure responses for a horizontal fracture located at the center of an aquifer and intersecting a well in an axisymmetric region are compared with the analytic solution of Gringarten and Ramey [11].

V. APPLICATION

The importance of the coupling between the fluid flow and the mechanical deformation in fractures has been analyzed by the iterative steady state version of this code. The flow through a jointed dam foundation has been simulated [17]. It is noted that a deformable fracture system has lower flow through the foundation and higher uplift pressure than a rigid network of fractures. The code has also been used in the analyses of laboratory experiments of large rock samples with tension fractures and of field tests in shallow fractured formations [7]. It is well known that high pressure at a wellbore can open up the fractures and will result in a high injection rate while low pressure at a wellbore during withdrawal can close the fracture and decrease the hydraulic conductivity of flow.

This recently developed transient code is well suited for a thorough study of the mentioned effects due to the fact that it can provide additional insight to the very important transient processes of the coupling phenomena.

VI. SUMMARY

This model is for the study of coupled fluid flow and stress in deformable fractured rock masses. The effective mass theory of Biot is used to relate the pressure changes with the displacements of the rock matrix. The deformation of the fracture surfaces in turn affects the fracture flow through the sensitive dependence of permeability on aperture.

The code combines techniques of fluid flow modeling and stress-strain analysis. The two-dimensional finite-element code incorporates the flow element of Wilson and Witherspoon [21] for the fracture flow, the joint element of Goodman et al. [12] for the representation of mechanical behavior, and a predictor-corrector scheme to damp out numerical oscillation.

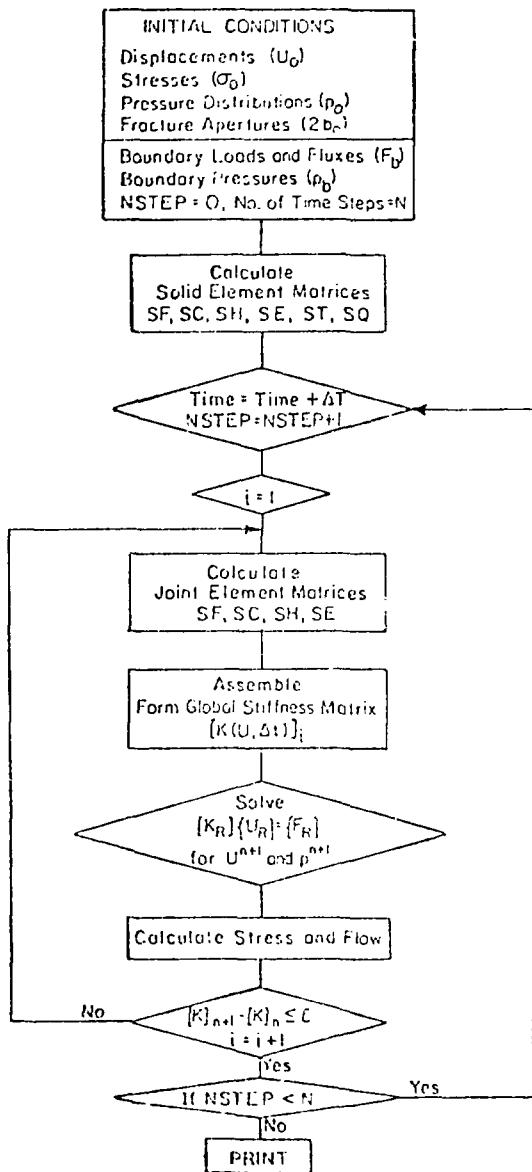
The model is based on general theory which is of fundamental interest and practical importance. The code has the capability of handling a range of complex problems in fluid flow, induced rock mass deformation and soil consolidation [8]. Further developments to couple the fluid flow with heat transfer, or to incorporate dynamic stress analysis, can increase the range of applicability. More extensive application of the code is called for.

VII. REFERENCES

1. Ayatollahi, M. S., Noorishad, J., Witherspoon, P. A., "A finite element method for stress and flow analysis in fractured rock masses." submitted for publication in J. of Engineering Mechanics Division, Proceedings ASCE 1981.
2. Bathe, K. J. and Wilson, E. L. Numerical Methods in Finite Element Analysis. Prentice Hall, Englewood Cliff, New Jersey, 1976.
3. Biot, M. A. "General theory of three-dimensional consolidation." J. Applied Physics, V. 12, pp. 155-164, 1941.
4. Biot, M. A. "Theory of elasticity and consolidation for a porous anisotropic media." J. Applied Physics, V. 26, pp. 182-185, 1955.
5. Biot, M. A. "Theory of deformation of a porous viscoelastic anisotropic solid." J. Applied Physics, V. 27, 1956.
6. Biot, M. A. "Mechanics of deformation and acoustic propagation in porous media." J. Applied Physics, V. 34-A, pp. 1483-1498, 1961.
7. Gale, J. E. A Numerical, Field and Laboratory Study of Flow in Rocks with Deformable Fractures. Ph.D. thesis, University of California, Berkeley, 1975.
8. Ghaboussi, J. and Wilson, E. L. "Flow of compressible fluids in porous media." SESM Report No. 72-12, University of California, Berkeley, 1971.
9. Ghaboussi, J. Dynamic Stress Analysis of Porous Elastic Solids Saturated with Compressible Fluids. Ph.D. thesis, University of California, Berkeley, 1971.
10. Ghaboussi, J. and Wilson, E. L. "Liquefaction analysis of saturated granular soils." 5th World Conference on Earthquake Engineering, Rome, 1973.
11. Gringarten, A. C. and Ramey, H. J. "Unsteady state pressure distribution created by a well with a single horizontal fracture." SPE Journal, n. 413, August 1974.
12. Goodman, R. E., Taylor, R. L. and Brekke, T. L. "A model for the mechanics of jointed rocks." J. Soil Mech. and Found. Div., ASCE, V. 94, N.S.N., 3 May 1968.
13. Heber-Cinco, L., Samaniego-V., E., and Dominguez-A., M. "Transient pressure behavior for a well with a finite conductivity vertical fracture." 51st Conference Soc. Pet. Eng., October 1976.

14. Hilber, H. and Taylor, R. L. "A finite element model of fluid flow in systems of deformable fractured rock." Report No. UC-SESM 76-5, Department of Civil Engineering, University of California, Berkeley, 1976.
15. Mueller, T. D. and Witherspoon, P. A. "Pressure Interface Effects Within Reservoirs and Aquifers" Trans. AIME, V. 234, p. 471, 1965.
16. Muskat, M. "The Flow of Homogeneous Fluids Through Porous Media". J. W. Edwards, Inc., An Arbor, 1946.
17. Noorishad, J. Finite-Element Analysis of Rock Mass Behavior Under Coupled Action of Body Forces, Flow Forces, and External Loads. Ph.D. dissertation, University of California, Berkeley, 1971.
18. Noorishad, J., Ayatollahi, M. S. and Witherspoon, P. A. Coupled stress and fluid flow analysis of fractured rocks, submitted to International Journal of Rock Mechanics and Mining Sciences, 1981.
19. Raghavan, R., Uraiet, A., and Thomas, G. W. "Vertical fracture height effect on transient flow behavior." 51st Conf. Soc. Pet. Eng., Oct. 1976.
20. Taylor, R. L. "Analysis of flow of compressible or incompressible fluids in porous elastic solids." Consulting Report to the Naval Civil Engineering Lab., Port Hueneme, California, 1974.
21. Wilson, C. and Witherspoon, P. A. An Investigation of Laminar Flow in Fractured Porous Rocks. Ph.D. thesis, University of California, Berkeley, California, 1970.
22. Zienkiewicz, O. C. The Finite Element Method in Engineering Science. McGraw-Hill, London, 1971.

Flow chart for stress and flow analysis of fractured porous media.



VIII. USER'S GUIDE

The program "ROCMAS" is written in FORTRAN IV and uses both large core and small core memory of the CDC 7600. The large core is used for storage of

- (i) nodal points, their coordinates in two directions, their proper code used to describe boundary conditions, initial loads or displacements,
- and (ii) elements, their material type properties, the correspondence between structural nodes and flow nodes, and between structural elements and flow elements, flow boundary codes, and any other properties that are unique for each node or each element.

The large core is also used to store large matrices and vectors needed for the solution of the final system of equations and the equation identifiers for the three degrees of freedom at each nodal point.

The small core memory furnishes storage of the COMMON blocks as well as DIMENSION statements.

Since "ROCMAS" is not written to use a dynamic storage option, it is necessary to keep in mind the maximum size of the arrays for which large core storage is provided. For the time being, the following limits should be kept in mind:

Maximum number of nodal points = 300

Maximum number of structural elements (joints and solids) = 300

Maximum number of joint elements = 50

Maximum number of different materials = 12

The input data* should be prepared in the groups of cards described below:

<u>Group</u>	<u>Column</u>	<u>Format</u>	<u>Word</u>	<u>Explanation</u>
I-1	1-5	A5	"TITLE"	Title card to start with computation
I-2	1-72	8A9	HED	Any desired titling, or blank cards
I-3	1-72	8A9	HED	two cards.
I-4	1-5	I5	NUMNP	Total no. of nodal points in the mesh
	6-10	I5	NUMEL	Total no. of elements in the mesh
	11-15	I5	NUMMAT	Total no. of different materials
	16-20	I5	NSHELL	Highest no. of solid material
	21-25	I5	NPC	No. of boundary pressure cards
	26-30	I5	NJMP	No. of joints with modified aperture
	31-35	I5	IRAND	Random aperture generator if = 1, otherwise equal to zero
	36-40	I5	NIT	Total no. of time step iterations
	41-45	I5	IPLOT	Plot output requested, if equal to 1; otherwise equal to zero
	46-50	I5	IPUNCH	Punch requested for final joint element properties if = 1, otherwise = 0
	51-55	F5.0	TTOTAL	Total estimated on time (decimal seconds)
	56-65	F10.0	CONLIM	Joint stiffness convergence constant
	66-70	I5	NAXI	Axisymmetric problem if 1, two-dimensional problem if 0

* An example of input data preparation is given at the end.

<u>Group</u>	<u>Column</u>	<u>Format</u>	<u>Word</u>	<u>Explanation</u>
I-5	1-10	F10.3	AAM	Mean aperture lognormal distribution
	11-20	F10.3	THETA	Time integration factor
	21-30	F10.3	AAS	Standard deviation lognormal distribution
	31-40	F10.3	ACELX	x-direction acceleration
	41-50	F10.3	ACELY	y-direction acceleration
I-6	1-10	F10.3	XNHP	Maximum net head pressure (optional)
	11-20	F10.3	SPWT	Fluid specific gravity
	21-35	E15.5	VISC	Fluid viscosity
	36-40	I5	IPRINT	No. of time step printouts required
	41-45	I5	NDTN	Variable time step counter if > 1
	46-55	E10.5	DT	Initial time increment
	56-65	E10.5	SYSDIM	System dimension, if P_D , t_D calculated*
66-75	E10.5	TOTALQ	Total flow, if P_D , t_D calculated*	
II-1	1-8	A10	"MATERIAL"	Title card for material specifications
II-2	1-5	A10	"INCOMPRESS"	For incompressible fluid **
			"COMPRESS"	for compressible fluid

*Note that P_D , t_D calculation uses properties of first solid, therefore, it is meaningful only for a special class of problems.

**Only used for uncoupled steady state fluid flow problems. Minor modification of the solution algorithm is required for steady state coupled problems, i.e. when $\alpha \neq 0$ and incompressible fluid assumption is used.

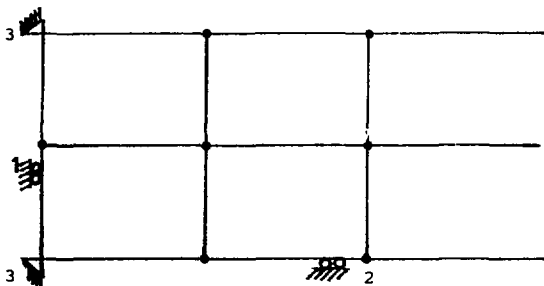
<u>Group</u>	<u>Column</u>	<u>Format</u>	<u>Word</u>	<u>Explanation</u>
II-3	<u>Properties of solid materials</u>			
	1-5	I5	MTYPE	Material type, NSHELL > MTYPE > 1
	6-14	E9.4	RO	Mass density
	15-23	E9.4	E(1,MTYPE)	Permeability
	24-32	E9.4	E(2,MTYPE)	Compression modulus
	33-41	E9.4	E(3,MTYPE)	Poisson's ratio
	42-50	E9.4	E(4,MTYPE)	Biot's constant α (pressure displacement coupling coefficient)
	51-59	E9.4	E(5,MTYPE)	Biot's constant M (reciprocal of specific storage in case of flow analysis alone)
	One card per material type should be punched. Maximum number of solid material cards is equal to NSHELL.			
II-4	<u>Fracture material properties</u>			
	1-5	I5	MTYPE	Material type
	6-14	E9.4	BLANK	
	15-23	E9.4	E(1,MTYPE)	Normal stiffness
	24-32	E9.4	E(2,MTYPE)	Tangential stiffness
	33-41	E9.4	E(3,MTYPE)	Cohesion
	42-50	E9.4	E(4,MTYPE)	Friction angle
	51-59	E9.4	E(5,MTYPE)	Maximum closure
	60-68	E9.4	E(6,MTYPE)	Biot's constant, α
	69-77	E9.4	E(7,MTYPE)	Biot's constant, M

<u>Group</u>	<u>Column</u>	<u>Format</u>	<u>Word</u>	<u>Explanation</u>
III	<u>Output Information</u>			
	1-6	A10	"OUTPUT"	Title card for output specifications
	1-80	40I2	NPP(I)	Number of perturbations in time step I
	1-80	40I2	IPAT(J)	Output scheme for each time step
	Output schemes:			
	(1)	IPAT=0		No prints, no plots requested
	(2)	IPAT=1		Print requested
	(3)	IPAT=2		Print and plot requested
IV	<u>Plot Information</u>			
	If IPLOT=0 skip this group.			
	1-10	E10.4	XLENGTH	x-dimension of plot (inches)
	11-20	E10.4	YLENGTH	y-dimension of plot (inches)
	21-30	E10.4	PSCL	Factor for plotting stresses in the solids
	31-40	E10.4	CONJT	Multiple for PSCL to plot stresses in joints

<u>Group</u>	<u>Column</u>	<u>Format</u>	<u>Word</u>	<u>Explanation</u>
V	<u>Nodes</u>			
V-1	1-5	A5	"NODES"	Title card for nodal points
V-2	1-5	I5	N	Nodal point number
	6-10	I5	NXP	Increment to reach next nodal point
	11-20	E10.3	R(N)	x-coordinate (R-if axisymmetric) of N
	21-30	E10.3	Z(N)	y-coordinate (z-if axisymmetric) of N
	31-40	E10.3	CD	Displacement code of N
	41-50	E10.3	CDI	Displacement code to be used for preceding node
	51-60	E10.3	DU	Load or displacement at N in x-direction
	61-70	E10.3	DV	Load or displacement at N in y-direction

Note: If CD or CDI are equal to:

- 0 DU and DV are specified loads
- 1 DU is specified displacement, DV is specified load
- 2 DU is specified load, DV is specified displacement
- 3 DU and DV are specified displacements (Fig. 7)

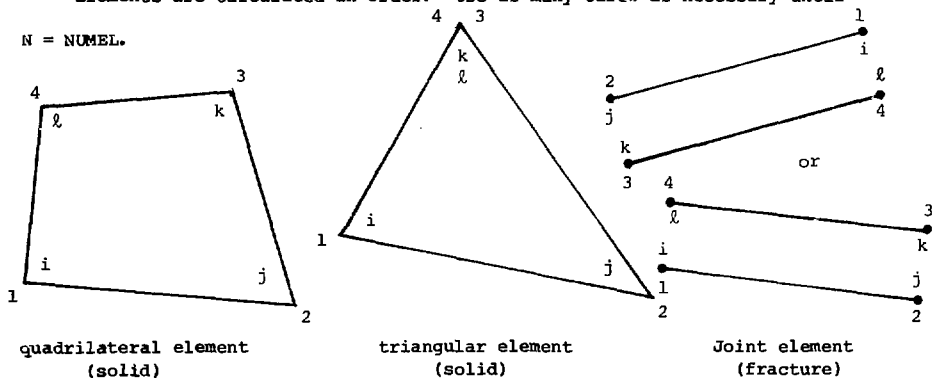


Sketch: Application of load or displacement boundary codes. Nodal point cards need not be in order, except when generating a set where the last node in the row should come after the first. The last nodal point of the system should appear on the last card.

<u>Group</u>	<u>Column</u>	<u>Format</u>	<u>Word</u>	<u>Explanation</u>
VI	<u>Elements</u>			
VI-1	1-7	A7	"ELEMENT"	Title card for elements
VI-2	1-5	I5	M	Element number
	6-10	I5	IX(M,1)	Nodal points 1 to 4 defining the element must be counterclockwise for solids and lengthwise for joints (Fig. 8)
	11-15	I5	IX(M,2)	
	16-20	I5	IX(M,3)	
	21-25	I5	IX(M,4)	
	26-30	I5	IX(M,5)	Material type
	31-35	I5	IXD(1)	Increments used to change IX(M,1) to reach next generated element
	36-40	I5	IXD(2)	
	41-45	I5	IXD(3)	
	46-50	I5	IXD(4)	
	51-55	I5	JXD	Increment used to alternate material type

Elements are calculated in order. Use as many cards as necessary until

$N = \text{NUMEL.}$



Sketch: Element nodal point numbering.

<u>Group</u>	<u>Column</u>	<u>Format</u>	<u>Word</u>	<u>Explanation</u>
--------------	---------------	---------------	-------------	--------------------

VII Boundary distribution load

If NPC = 0, skip this group.

VII-1	1-8	A8	"PRESSURE"	Title card for boundary pressures
VII-2	1-5	I5	I1	Nodal point number
	6-10	I5	I2	Nodal point number
	11-20	F10.3	PS1	Pressure at I1
	21-30	F10.3	PS2	Pressure at I2

VIII Flow conditions

This group must not appear before Group VII.

VIII-1	1-4	A4	"FLOW"	Title card for flow at the boundary
VIII-2	1-5	I5	N	Nodal point number. If joint use smaller nodal point across the joint.
	6-10	I5	NL	IB(N) = nonzero, if constant PHIO(N)
	11-20	F10.3	PH	PHIO(N) = pressure or head if SPWT = 0
	21-30	F10.3	QQ	Q(N) = flowrate at N

If IB(N) = 0 and Q(N) = 0.0, omit this card.

Cards are needed only if IB(N) ≠ 0 or if Q(N) ≠ 0.0.

<u>Group</u>	<u>Column</u>	<u>Format</u>	<u>Word</u>	<u>Explanation</u>
--------------	---------------	---------------	-------------	--------------------

IX Residual stresses

Skip this group if no initial stress is given.

IX-1	1-8	A8	"RESIDUAL"	Title card for initial stresses
IX-2	1-10	I10	N	Element number
	11-20	E10.3	RESID(N,1)	Stress in x-direction
	21-30	E10.3	RESID(N,2)	Stress in y-direction
	31-40	E10.3	RESID(N,3)	Stress in z-direction
	41-50	E10.3	RESID(N,4)	Shear stress in xy plane

Note that compressive stresses are negative. Repeat as many cards as needed to define NUMEL. The program will calculate stresses for intermediate elements by assigning the preceding values.

X	1-4	A4	"DONE"	Title card
---	-----	----	--------	------------

This card marks the end of the data for generating the mesh physical information for this particular problem.

<u>Group</u>	<u>Column</u>	<u>Format</u>	<u>Word</u>	<u>Explanation</u>
XI	<u>Joint properties modification</u>			
	Use only if NJMP > 0.			
XI	1-5	I5	I	Joint element to be modified
	6-15	F10.3	COEG	Coefficient to modify the aperture
	16-30	F15.5	COEM1	Coefficient to modify normal stiffness
	31-45	F15.5	COEM2	Coefficient to modify tangential stiffness
	46-60	F15.5	COEM3	Coefficient to modify cohesion
	61-75	F15.5	COEM4	Coefficient to modify friction angle
XII	1-5		"BLANK"	If the flow or pressure source is a step function (kept constant in time). Use another title card if the source is an initial pulse.
xIII	1-10	I10	NSTEP	Number of time steps with a constant time increment DT
	11-30	E20.5	DT	Constant time increment for NSTEP
XIV	Use as many cards as needed to reach NDTN in Group I. For steady state problems* use one card, NSTEP = 1 and DT > zero.			
XIV	1-3	E13	"END"	Final card in the data deck.

* Reminder: For steady state fluid flow problems, put E(6.MTYPE) equal to zero and use "INCOMPRESS" card.

APPENDIX I
SAMPLE PROBLEM
WITH SAMPLE INPUT OUTPUT

SAMPLE PROBLEM

As an example for data preparation, the problem of fluid flow to a well intersecting a vertical fracture is solved. Although the data is originally set up for coupled stress-flow analysis, the problem is first solved in uncoupled state for the purpose of comparison with the existing solution [Raghavan et al., (17)]. To achieve a conventional fluid flow analysis, one has to assign a zero value to the coupling coefficient α and a value equivalent to $1/S_g$ (inverse specific storage) to M . Later, allowing for the deformability of the medium, a coupled analysis is performed. As it is shown in Table 1, in this case $\alpha \neq 0$ (a value equal to 1.0 is assumed) and $M = 1/\rho C_f$. Figures 1 through 4 present the results of the modeling and following plates exhibit the setup of the data. PSF system equivalent units are used in the tabulation of the data set.

TABLE 1. Material properties used for the analysis of fluid flow in fractured rock mass.

Material type	Properties	Value
fluid	γ_f , specific weight	$9.8 \times 10^3 \text{ N/m}^3$
	C_f^{-1} , incompressibility	1.95 GPa
	η , viscosity	$2.8 \times 10^{-4} \text{ N-sec/m}^2$
porous rock	E , Young's modulus	2.45 GPa
	ν , Poisson's ratio	0.25
	γ_r , specific weight	$2.45 \times 10^4 \text{ N/m}^3$
	n , porosity	2.15
	k , permeability	10^{-5} m/s
	M , Biot's storage constant	coupled 1.47 GPa uncoupled* 14.0 GPa
	α , Biot's coupling constant	coupled 1.0 uncoupled 0.0
	fractures	K_N , initial normal stiffness
	K_S , initial tangential stiffness	0.50 GPa/m
	C_0 , cohesion	0.0
	ϕ , friction angle	$30^\circ.0$
	$2b$, initial aperture	$1 \times 10^{-3} - 1 \times 10^{-14} \text{ m}$
	n , porosity	0.15
	M , Biot's storage constant	coupled 1.47 GPa uncoupled* 14.0 GPa
	α , Biot's storage constant	coupled 1.0 uncoupled 0.0

* In this case M is the reciprocal of the specific coefficient of storage of the porous medium.

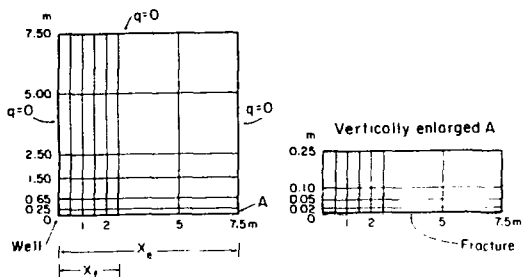


FIG. 1.--TWO-DIMENSIONAL FINITE ELEMENT MESH. (XBL 806-7222)

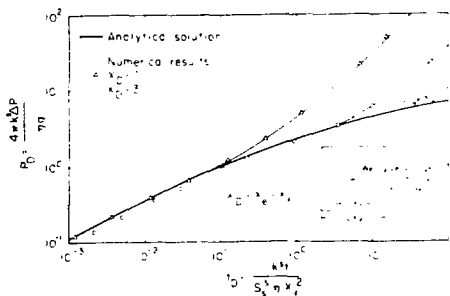


FIG. 2.-- P_D VERSUS t_d FOR A SINGLE FRACTURE INTERSECTING A WELL AT THE CENTER OF A RECTANGULAR POROUS MEDIUM. ANALYTICAL SOLUTION AFTER RAGHAVAN ET AL. (1976). (XBL 806-2703)

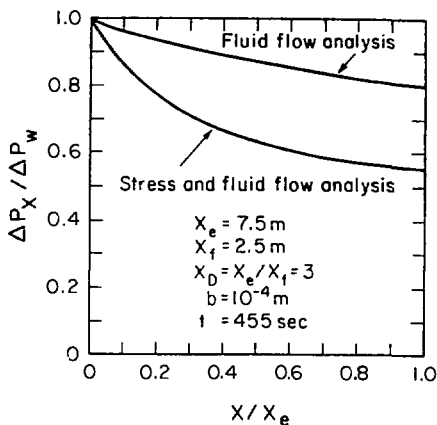


FIG. 3.--PRESSURE DROP ALONG SOFT FRACTURE OF 0.1 mm APERTURE IN FLUID FLOW ANALYSIS AND STRESS-FLUID FLOW ANALYSIS. (XBL 806-2705)

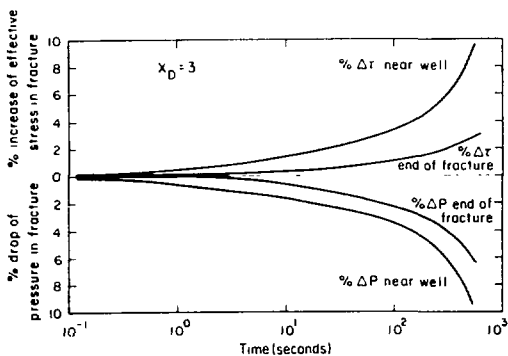


FIG. 4.--THE VARIATION OF PRESSURE AND EFFECTIVE STRESS ALONG THE NEAR AND FAR ENDS OF THE FRACTURE. (XBL 806-2706)

I. General parameters and material properties

PLANF STRAIN-FLOW ANALYSIS OF JUNCTION STRUCTURE

SIMULATION PUMPING OF CONFINED AQUIFER WITH SINGLE VERTICAL FRACTURE

INTERSECTING THE WELL---PLAIN STRAIN PROBLEM

NUMNP-NUMBER OF NODAL POINTS-----	88
NUMEL-NUMBER OF ELEMENTS-----	70
NUMMAT-NUMBER OF DIFFERENT MATERIALS-----	3
NSHELL-NUMBER OF SOLID MATERIALS-----	1
NPC-NUMBER OF BOUNDARY PRESSURE CARDS-----	16
NJNP-NUMBER OF JOINTS WITH MODIFIED APERTURES-----	-0
IRAND-RANDON APERTURE GENERATOR IF 1-----	-0
NIT-NUMBER OF TIME STEPS-----	35
IPLOT-PLOT INFORMATION REQUIRED IF 1-----	-0
IPUNCH-PUNCH IF 1-----	1
TTOTAL-ESTIMATED TOTAL CP TIME(DECIMAL SECONDS)-----	50
AAK-MEAN-APERTURE LOGNORMAL DISTRIBUTION-----	0.
AAS-STANDARD DEVIATION-LOGNORMAL DISTRIBUTION-----	0.
ACELX-X ACCELERATION (FEET/SECOND)-----	0.
ACELY-Y ACCELERATION (FEET/SECOND)-----	0.
XNHP-MAXIMUM NET HEAD PRESSURE (PSF)-----	0.
SPWT-FLUID SPECIFIC WEIGHT-----	-0.
NDTN-VARIABLE TIME-STEP COUNTER, IF G.T. 1-----	10
IPRT, NO. OF CYCLES FOR DISPL. PRINT-----	0
DT-INITIAL TIME INCREMENT-----	1.00000E-03
CONLM JCINT STIFF. CONVERG. CONSTANT-----	6250
MAXI-AXISYM. PROBLEM IF 1-----	-0
THEIA- TIME INTEGRATION CONSTANT-----	2.000
VISC-FLUID VISCOSITY (PSF)-----	5.85000E-06
SYSDIM-SYSTEM DIMENSION REQUIRED IF PD,TD WANTED	3.14160E+00
TOTALQ-TOTAL FLOW REQUIRED IF PD,TD WANTED-----	4.30000E-05

SIMULATION PUMPING OF CONFINED AQUIFER WITH SINGLE VERTICAL FRACTURE
INTERSECTING THE WELL---PLAIN STRAIN PROBLEM

MATERIAL NO. = 1

MASS DENSITY-----	4.85
PERMEABILITY-----	3.1000E-13
ELASTIC MODULUS-----	5.1400E+07
POISSONS RATIO-----	2.5000E-01
BIGTS CONSTANT(ALPHA)-----	0.
BIGTS CONSTANT(M)-----	2.0700E+07

MATERIAL NO. = 2

KN-----	1.0000E+08
KI-----	1.0000E+08
C-----	0.
PHI-----	2.0000E+01
MAX. CLOSURE-----	-3.2800E-04
BIGTS CONSTANT (ALPHA)-----	0.
BIGTS CONSTANT (M)-----	4.1100E+07

MATERIAL NO. = 3

KN-----	7.5000E+11
KI-----	7.5000E+11
C-----	0.
PHI-----	3.0000E+01
MAX. CLOSURE-----	-3.2800E-09
BIGTS CONSTANT(ALPHA)-----	-0.
BIGTS CONSTANT (M)-----	4.1100E+07

APPENDIX II

LISTING OF FORTRAN IV SOURCE PROGRAM

```

PROGRAM ROCMAS(INPUT=201,OUTPUT,PUNCH=201,PLOT,TAPE8,TAPE9, STRFLC
1 TAPE99=PLCT,TAPE90,TAPE1) STRFLC
C STRFLC
C ***** STRFLC
C PROGRAM ROCMAS STRFLC
C ***** STRFLC
C PLANE-STRAIN AND AXISYMMETRIC QUASI-STATIC STRESS-FLUID FLOW STRFLC
C ANALYSIS OF FRACTURED ROCK MASS. A DIRECT EQUATION SOLVER IS USED STRFLC
C TO SOLVE THE COUPLED EQUATIONS.A STIFFNESS PERTUREATION SCHEME STRFLC
C FORCES STRESSES AND DEFORMATIONS TO FOLLOW THE PROPER NON-LINEAR STRFLC
C CONSTITUTIVE LAW OF THE FRACTURE MATERIALS. STRFLC
C THIS CODE WAS BASICALLY DEVELOPED BY M.S. AYATOLLAHI IN 1978. STRFLC
C LATER,IN 1979,IT WAS CORRECTED,REVISED AND EXTENDED,FOR GENERAL STRFLC
C APPLICATION. BY J.NOORISHAD. STRFLC
C ***** STRFLC
C IN SPITE OF THE POUNDING WEIGHT),FOOT,SECOND HEACINGS,ANY CONSISTENT STRFLC
C SYSTEM OF UNITS COULD BE USED. STRFLC
C ***** STRFLC
C CODE(I)- STRUCTURAL NODAL POINT CODE THAT INDICATES WHAT BOUNDARY STRFLC
C CONDITION( LOAD OR DISPLACEMENT) IS ASSIGNED AT POINT I STRFLC
C (I,J,MTYPE)- MATERIAL MODULI (ROCK OR JOINT ) STRFLC
C EPSK- AVERAGE DEFORMATION OF A JOINT STRFLC
C IBIN(I)- FLOW MESH NODAL POINT CODE,IF #0 ASSIGNED VALUE OF HEAD STRFLC
C OR PRESSURE REMAINS CONSTANT AT POINT N STRFLC
C INDEX- PRINT PLCT CODE STRFLC
C IPAT- PRINT AND PLOT CODE-NO PRINT,NO PLOT IF 0,PRINT IF 1,PRINT, STRFLC
C PLOT IF 2 STRFLC
C IPER- TOTAL PERTURBATION INDEX STRFLC
C IX(I,M), I=1,5- THE FIRST FOUR REPRESENT NODAL POINTS AROUND ELEM STRFLC
C N IN STRUCTURAL MESH AND THE LAST INDICATES MTYPE STRFLC
C KN(I)- NORMAL STIFFNESS OF JOINT I CALCULATED INITIALLY FROM E(I,2) STRFLC
C KS(I)- TANGENTIAL STIFFNESS OF JOINT I CALCULATED FROM E(I,3) STRFLC
C NP-TIME STEP INDEX STRFLC
C MTYPE- NUMBER ASSIGNED TO EACH MATERIAL (STARTING WITH 1 ) STRFLC
C NIT-NUMBER OF TIME STEPS STRFLC
C MNN- PERTURBATION INDEX STRFLC
C NP- DUMMY FOR NPP STRFLC
C MPP(J)- NUMBER OF PERTURBATIONS IN TIME STEP NUMBER J STRFLC
C QIN)- FLOW RATE AT FLOW NODAL POINT N STRFLC
C PHID(N)-PRESCRIBED HEAD OR PRESSURE AT FLOW POINT N WHERE I9(N)#0 STRFLC
C R(I)- X COORDINATE OF STRUCTURAL NODAL POINT I STRFLC
C RESID(N,I), I=1,4 X, Y, Z, AND XY COMPONENTS OF RESIDUAL STRESS STRFLC
C RO(MTYPE)- SPECIFIC MASS OF ROCK MATERIAL STRFLC
C XLNGTH - X LENGTH OF MESH PLOT STRFLC
C YLNGTH - Y LENGTH OF MESH PLOT STRFLC
C DISPL - SCALE FACTOR FOR DISPLACEMENT PLOTS STRFLC
C PSF - SCALE FOR STRESS PLCT STRFLC
C SPWT-FLUID SPECIFIC WEIGHT STRFLC
C TFL- TIME NEEDED FOR FLOW CALCULATION STRFLC
C TIT- TIME SPENT FOR ONE PERTURBATION STRFLC
C TL- TIME LEFT STRFLC
C TST- TIME REQUIRED FOR REAC AND PRINT OF INPUT DATA STRFLC
C UR(I),UZ(I)-R AND Z COMPONENTS OF DISPLACEMENT OR LOAD AT POINT I STRFLC
C V- RELATIVE DISPLACEMENT OF OPPOSING NODAL POINTS IN A JOINT STRFLC
C VISC-FLUID VISCOSITY STRFLC
C MNI)- APERTURE OF FLOW ELEMENT N CALCULATED IN EACH ITERATION STRFLC
C MI(I)- INITIAL APERTURE OF JOINT I IN STRUTURAL MESH STRFLC
C Z(I)- Z OR Y COORDINATE OF STRUCTURAL NODAL POINT I STRFLC
C ***** STRFLC
C NOTE----- VECTORS DISP(150),DRG(2N)-IMP(50,4),IEL(50,2),SIGN(50), STRFLC
C AND SIG(150) ARE NOT USED IN THIS VERSION . STRFLC
C STRFLC

```

```

LARGE A(125000),IO(900)
LARGE IX(301,5),RESID(301,4),R(300),Z(300),WR(300),UZ(300) STRFLF
* ,CODE(300),IDEST(300),R,RN(50),R,KS(50),MT(50),IOUT(301),Q(300), LARGE.
*QP(50),M(50),VEL(50),FR(50),RE(50),GN(900),DISPZ(300,2),TEMP(300),LARGE.
*PHI0(300),IB(300),IDEQ(3,300),KCODE(3,300),TEL(50,2),IMP(50,4) LARGE.
* ,TL0A0(900),SIGN(50),SIGT(50),00@900) STRFLF
COMMON/BLANK/S(0,0),P(10),RSTRS(4),VOL,RRR(5),ZZZ(5),LEAD,RADN, BLANK.
1 RR(4),ZZ(4),IFAT(50),ACELX,ACELY,MRES,RC(12), BLANK.
2 MTYPE,XI,XCEI,YCEN,XTR(10),FAC,H(6),PD(4,12),00(2,4), BLANK.
3 PRS,PZS,PRT,PT,EG BLANK.
COMMON/GE/MSHELL,IPUNCH,E(7,12),INDEX,NP,MNH,NCORE,MUMNP,ICORR, GEN.2
1 MUEL,M02,MED(16),DISPL,NJELT,IPER,MUMMAT,PSF,PSFJ,XSCL,SPMT,GEN.3
3VISC,YSCCL,DSCCL,FSCCL,PJCL,NP(4),CONLIN,MAXI,NB,MEANG,LNGTH,NEQ,NJMPGEN.4
* ,MFL0N,MUMNP2,MUMNP,LN(12),NF2 GEN.5
COMMON/APTR,IRAND,NJUMP,AAS,AAN
COMMON/CCPOOL/XMIN,XMAX,YMIN,YMAX,CCXMIN,CCKMAX,CCYMIN,CCYMAX
COMMON/CCFACT/FACTOR
C
DIMENSION NPP(50),MUF(50) STRFLF
DIMENSION IXD(4),IXP(4),LST(0) STRFLF
LOGICAL FLAG STRFLF
DATA TITLE/5HTITLE/,ZMAT/0HMATERIAL/,ZOUT/6MOUTPUT/,FLOW/4HFLOW/, STRFLF
1 ZMODE/5HMODES/,ELEMEN/7HELEMENT/,PRESS/8HPRESSURE/, STRFLF
2 INCON/10HINCPRESS/,RESIX/8HRESIDUAL/,RESTAR/7HRESTART/, STRFLF
3 DONE/4HDONE/,BLANK/5HBLANK/,IXD/4*1/,END/3HEND/ STRFLF
C
FACTOR = 100. STRFLF
LOAD = 0 STRFLF
1 FORMAT (1H10A9/1H 0A9) STRFLF
STRFLF
5 READ 6, WORD STRFLF
6 FORMAT (ZA10) STRFLF
IF (WORD .EQ. TITLE) GO TO 1000 STRFLF
IF (WORD .EQ. ZMAT) GO TO 2000 STRFLF
IF (WORD .EQ. ZOUT) GO TO 3000 STRFLF
IF (WORD .EQ. ZMODE) GO TO 4000 STRFLF
IF (WORD .EQ. ELEMEN) GO TO 5000 STRFLF
IF (WORD .EQ. PRESS) GO TO 6000 STRFLF
IF (WORD .EQ. FLOW) GO TO 6500 STRFLF
IF (WORD .EQ. RESIX) GO TO 8000 STRFLF
IF (WORD .EQ. RESTAR) GO TO 9000 STRFLF
IF (WORD .EQ. DONE) GO TO 9999 STRFLF
IF (WORD .EQ. END) GO TO 300 STRFLF
STRFLF
C
UNIDENTIFIED CARD STRFLF
PRINT 10, WORD STRFLF
10 FORMAT (10HUNIDENTIFIED CARD A10/4H PROGRAM WILL SEARCH FOR NEXT STRFLF
1 TITLE CARD) STRFLF
STRFLF
C
SCAN DECK FOR NEXT CASE IF ANY STRFLF
15 READ 6, WORD STRFLF
IF (WORD .EQ. TITLE) GO TO 1000 STRFLF
IF (WORD .EQ. END) GO TO 300 STRFLF
GO TO 15 STRFLF
STRFLF
1000 READ 20, MED, MUMNP, MUEL, MSHELL, MPC, NJMP, IRAND, STRFLF
1 NIT, IPLCT, IPUNCH, ITOTAL, CONLIN, MAXI, AAN, THETA, STRFLF
2 AAS,ACELX,ACELY,XNHP,SPMT,VISC,IPRT,NOTN,DT,SYSZIN,TOTAL STRFLF
20 FORMAT (0A9/0A9/10I5,F5.0,F10.0,I5/5F10.3/2F10.3,E15.5, STRFLF
12I5,3E10.5) STRFLF
REWIND 0 STRFLF

```



```

GO TO 5
C
C MATERIAL PROPERTIES
2000 PRINT 1, MHD
      READ 2, ICOMP
      2 FORMAT (A10)
      IF (ICOMP.EQ. INCOMP) PRINT 3
      3 FORMAT (' FLUID IS INCOMPRESSIBLE *')
      DO 2035 N=1, NUMMAT
      READ 2010, MTYPE, RG(MTYPE), (E(J, MTYPE), J=1, 7)
2010 FORMAT (I5, 8E9.4)
      PRINT 2015, MTYPE
2015 FORMAT (/15H MATERIAL NO. =I3)
      IF (MTYPE.LE. NSHELL) GO TO 2019
      PRINT 2030, (E(J, MTYPE), J=1, 7)
      GO TO 2035
2019 PRINT 2020, RO(MTYPE), (E(J, MTYPE), J=1, 5)
2035 CONTINUE
2020 FORMAT (22H MASS DENSITY-----F8.2/22H PERMEABILITY-----
*E14.4/23H ELASTIC MODULUS -----E14.4/22H POISSONS RATIO-----E
*E14.4/23H BIOTS CONSTANT (ALPHA) E14.4/23H BIOTS CONSTANT(N)-----E
*I4.4)
2030 FORMAT (10H KN-----E25.4/10H KT-----E25.4/10H C-----E25.4/
110H PHI-----E25.4/20H MAX. CLOSURE-----E15.4/
* 23H BIOTS CONSTANT (ALPHA) E14.4/22H BIOTS CONSTANT ( N ) E14.4)
      GO TO 5
C
C INFORMATION FOR OUTPUT
3000 READ 3010, (NPP(I), I=1, NIT)
3010 FORMAT (40I2)
      ITOT = 0
      DO 3012 I=1, NIT
3012 ITOT = ITOT + APP(I)
      READ 3015, (IPAT(J), J=1, ITOT)
3015 FORMAT (40I2)
      PRINT 1, MHD
      K1 = 1
      DO 3025 I=1, NIT
      K2 = K1 + NPP(I) - 1
      PRINT 3020, NPP(I), I, (IPAT(J), J=K1, K2)
3020 FORMAT (/7I6, * PERTURBATIONS IN TIME STEP NUMBER *I3, 10X, *OUTPUT
*SCHEME *O2I3)
3025 K1 = K2 + 1
      IF (XPLOT.EQ. 0) GO TO 3035
      READ 3030, XLNGTH, YLNGTH, PSCL, CONJT
3030 FORMAT (4E10.4)
3035 GO TO 5
C
C ESTABLISH NOJAL POINT PROPERTIES
4000 DO 4010 N=1, NUMNP
4010 R(N) = BLANK
      N = 0
      NXP = 0
4015 NP = N
      IF (N.GE. NUMNP) GO TO 4035
      NX = NXP
      READ 4020, N, NXP, DR, DZ, CD, CDI, DU, DV
4020 FORMAT (2I9, 6E10.3)
      IF (N.LE. 0.DR.N.GT. NUMNP) GO TO 4035
      CODE(N) = CD
      R(N) = DR

```

```

      Z(N) = DZ                                STRFLC
      UR(N) = DU                                STRFLC
      UZ(N) = DV                                STRFLC
      IF(MX.EQ.0) GO TO 4015                    STRFLC
      IF((N-NP)*MX.GE.0) GO TO 4025            STRFLC
      MX = - MX                                  STRFLC
      PRINT 4021, NP,N                          STRFLC
4021 FORMAT(* INCREMENT FOR GENERATION BETWEEN NODES* I5* AND*I5* IS  STRFLC
      1F INCORRECT SIGN ** SIGN CHANGED*)    STRFLC
                                             STRFLC
4025 LX = (IABS(N-NP) + IABS(NX) - 1)/IABS(NX) STRFLC
      DR = (R(N)-R(NP))/LX                      STRFLC
      DZ = (Z(N)-Z(NP))/LX                      STRFLC
4030 NP = NP + NX                               STRFLC
      IF(MX.GT.0.AND.NP.GE.N) GO TO 4015       STRFLC
      IF(MX.LT.0.AND.NP.LE.N) GO TO 4015       STRFLC
      R(NP) = R(NP-MX) + DR                     STRFLC
      Z(NP) = Z(NP-MX) + DZ                     STRFLC
      CODE(NP) = CDI                             STRFLC
      UR(NP) = 0.                               STRFLC
      UZ(NP) = 0.                               STRFLC
      GO TO 4030                                STRFLC
C
C PRINT NODAL POINTS
4035 PRINT 1, HED                               STRFLC
      PRINT 4040                                STRFLC
4040 FORMAT(110#NODAL POINT TYPE X-ORDINATE Y-ORDINATE X-10 STRFLC
      1AD OR DISPLACEMENT Y LOAD OR DISPLACEMENT X-CODE T-CODE ) STRFLC
      DO 4055 N=1,MJHNP                          STRFLC
      IF(R(N).EQ.BLANK) PRINT 4045              STRFLC
4045 FCRMAT(* NO INPUT FOR THIS NODE * )        STRFLC
      IF(CODE(N).EQ.0.0) GO TO 4022             STRFLC
      IF(CODE(N).NE.3.0) GO TO 4023            STRFLC
      ID(2*N)=1                                  STRFLC
      ID(2*N-1)=1                                STRFLC
      GO TO 4022                                  STRFLC
4023 IF(CODE(N).NE.2.0) GO TO 4024             STRFLC
      ID(2*N)=1                                  STRFLC
      GO TO 4022                                  STRFLC
4024 IF(CODE(N).EQ.1) ID(2*N-1)=1             STRFLC
4022 CONTINUE                                   STRFLC
      IF(R(N).NE.BLANK) PRINT 4050,N,CODE(N),R(N),Z(N),UR(N),UZ(N), STRFLC
      , ID(2*N-1),ID(2*N)                       STRFLC
4050 FORMAT(I12,F12.3,2E12.3,2E24.7,2I10)      STRFLC
      IF(CODE(N).LT.1.0) CODE(N) = CODE(N) / 57.29577951 STRFLC
4055 CONTINUE                                   STRFLC
      GO TO 5                                     STRFLC
C
C NODAL POINTS, BAND WIDTH, CHECK CORE CAPACITY, JOINTS AND FLOW
5000 PRINT 1, HED                               STRFLC
      PRINT 5010                                STRFLC
5010 FORMAT (69#ELEMENT NO. I J K L MATERIAL JO STRFLC
      1INT NO WIDTH)                          STRFLC
      M = 1                                       STRFLC
      MBAND = 0                                    STRFLC
      JX = 0                                       STRFLC
5015 GO 5020 I=1,4                               STRFLC
5020 IXP(I) = IXD(I)                             STRFLC
      JX = JXD                                     STRFLC
      READ 5025, M, (IXM,I), I=1,5), IXD, JXD   STRFLC
5025 FORMAT (11I5)                             STRFLC

```



```

5102 IF (IDEST(J) .EQ. 0) IDEST(J)=K
      IF (IDEST(J) .LT. K) IDEST(J)=IDEST(J)
      IF (IDEST(J) .LE. K) GO TO 5106
      KK=IDEST(J)
      DO 5104 II=1, NUMNP
      IF (IDEST(II) .EQ. KK) IDEST(II)=K
5104 CONTINUE
5106 IF (L .EQ. 2) GO TO 5100
      I=IX (N, 2)
      J=IX (N, 3)
      K = MIND(I, J)
      L=2
      GO TO 5095
5108 CONTINUE
      DO 5110 N=1, NUMEL
      MTYPE=IX (N, 5)
      IF (MTYPE .EQ. NSHELL) GO TO 5110
      PERM=E (1, MTYPE)
      IF (ABS (PERM) .LT. E-12) GO TO 5110
      DO 5111 K=1, 4
      I=IX (N, K)
5111 IF (IDEST(I) .EQ. 0) IDEST(I)=I
5110 CONTINUE
      DO 5105 N=1, NUMNP
      I=IDEST (N)
      IF (I .EQ. 0) GO TO 5105
      IDEST(I)=IDEST (I)
5103 IF (I .NE. N) GO TO 5105
      NUHFNPN=NUHFNPN+1
      IDEST(N)=NUHFNPN
5105 CONTINUE
5113 PRINT 5112, MBAND, NJELT, NUFNPN
5112 FORMAT (35H0ST. STIFFNESS MATRIX BAND WIDTH =I5/20H NUMBER OF JIONSTRFLC.
      ST ELEMENTS =I5/2EH NUMBER OF FLOW NODES =I5) STRFLC.
      GO TO 5 STRFLC.
C PRESSURE CARDS IF ANY STRFLC.
6000 PRINT 1, MED STRFLC.
      PRINT 6010 STRFLC.
6010 FORMAT (/29H0PRESSURE BOUNDARY CONDITIONS/ 42H I J PRESSSTRFLC.
      1URE-I PRESSURE=J ) STRFLC.
      DO 6040 L=1, NPC STRFLC.
      READ 6015, I1, I2, PS1, PS2 STRFLC.
6015 FORMAT (2I5, 2F10.3) STRFLC.
      PRINT 6020, I1, I2, PS1, PS2 STRFLC.
6020 FORMAT (2I5, 2F10.3) STRFLC.
      DR = R(I2) - R(I1) STRFLC.
      DZ = Z(I1) - Z(I2) STRFLC.
      CC = CODE (I1) STRFLC.
      IF (CC .EQ. 3) GO TO 6030 STRFLC.
      PI = (Z.*PS1 + PS2)/6. STRFLC.
      IF (NAXI .NE. 0) STRFLC.
      1 PI = (R(I1)* (3.0*PS1+PS2) + R(I2)*(PS1+PS2)) / 12.0 STRFLC.
      SINA = 0. STRFLC.
      COSA = 1. STRFLC.
      IF (CC .GE. 0.8) GO TO 6025 STRFLC.
      SINA = SIN(CCA) STRFLC.

```

```

        COSA = COS(CC)
6825 IF (CC .EQ. 9.0 .OR. CC .EQ. 1.0) UZ(I1) = UZ(I1) + DR*PI
        IF (CC .NE. 1.0) UR(I1) = UR(I1) + DZ*PI*COSA + DR*PI*SINA
        STRFLC
6830 CC = CODE(I2)
        IF (CC .EQ. 3.0) GO TO 6840
        PI = (2.*PS2 + PS1)/6.
        IF (MAXI .NE. 0)
            1 PI = (R(I2)*(3.0*PS2+PS1) + R(I1)*(PS1+PS2)) / 12.0
        SINA = 8.
        COSA = 1.0
        IF (CC .GE. 9.0) GO TO 6035
        SINA = SIN(CC)
        COSA = COS(CC)
6835 IF (CC .NE. 1.0) UR(I2) = UR(I2) + DZ*PI*COSA + DR*PI*SINA
        IF (CC .EQ. 1.0 .OR. CC .EQ. 0.0) UZ(I2) = UZ(I2) + DR*PI
        STRFLC
6840 CONTINUE
        GO TO 5
        STRFLC
C
C***** FLOW NODE PROPERTIES ***
6500 CONTINUE
        DO 6501 I=1,NUMFN
            IO(I)=0
            PHIO(I)=0.0
6501 O(I)=0.0
        STRFLC
        IF (NUMFN .GT. 0) GO TO 7110
        PRINT 7105
        STRFLC
7105 FORMAT (37H FLOW CARDS MUST FOLLOW ELEMENT CARDS)
        LBA0 = 1
        STRFLC
7110 MBFLCW = 0
        STRFLC
        DO 7120 M=1,NUMEL
            MTYPE=IX(M,5)
            IF(MTYPE.LE.NSHELL) GO TO 7121
            I=IX(M,1)
            J=IX(M,2)
            K=IABS(IDEST(I)-IDEST(J))
            IF(K.GT.MBFLOW) MBFLOW=K
            GO TO 7120
        STRFLC
7121 DO 7122 I=1,3
            II=IX(M,I)
            I1=I+1
            DO 7122 L=I1,4
                LL=IX(M,L)
                K=IABS(IDEST(LL)-IDEST(II))
                IF(K.GT.MBFLOW) MBFLOW=K
            STRFLC
7122 CONTINUE
7120 CONTINUE
        MBFLOW=MBFLOW+1
        STRFLC
C
        PRINT 7125
7125 FORMAT(118H0FLOW NODAL PCINTS CODE X-ORDINATE Y-ORDINATE NST
        LET HEAD(PSF) FLOW RATE(CFS) CORRESPONDING NODAL POINTS)
        STRFLC
        NX = 1
        STRFLC
7130 READ 7135, N, NL, PH, QF
7135 FORMAT (2I5,2F10,3)
        STRFLC
        IF (N .GT. NUMNP .OR. N .LE. 0) GO TO 7170
        IF (N .GT. NK) GO TO 7145
        STRFLC

```

```

7140 L = IDEST(N)                                STRFLC
      IB(L) = NL                                STRFLC
      PHIO(L) = PH                              STPFLC
      Q(L)=QF                                  STRFLC
      GO TO 7150                                STRFLC
7145 L1 = IDEST(NK)                              STRFLC
      IF (L1 .LE. L) GO TO 7165                STRFLC
      L = L1                                    STRFLC
7150 DO 7151 J=1,0                               STRFLC
7151 LST(J) = 0                                  STRFLC
      J1 = 0                                    STRFLC
      DO 7155 J=NX,NUMNP                       STRFLC
      IF (IDEST(J) .NE. L) GO TO 7155         STRFLC
      J1 = J1 + 1                               STRFLC
      LST(J1) = J                              STRFLC
7155 CONTINUE                                   STRFLC
      PRINT 7160, L, IB(L),R(NX),Z(NX),PHIO(L),Q(L), (LST(J),J=1,J1) STRFLC
7160 FORMAT (2I12,2F12.2,2E19.6,4X,8I4)       STRFLC
      IF (J1.LE.1) GO TO 7162                 STRFLC
      JMIN=LST(1)                              STRFLC
      DO 7161 J=2,J1                           STRFLC
7161 JMIN=MIN0(JMIN,LST(J))                  STRFLC
      KEQ=KEQ-J1+1                              STRFLC
      JNUM=IDEQ(3,JMIN)                        STRFLC
      DO 100 J=1,J1                             STRFLC
      K=LST(J)                                  STRFLC
100 IDEQ(3,K)=JNUM                             STPFLC
      JMIN=JMIN+1                              STRFLC
      J1=0                                      STRFLC
      DO 101 K=JMIN,NUMNP                      STRFLC
      DO 101 J=1,3                              STRFLC
      IF (IDEQ(J,K).EQ.JNUM) J1=J1+1          STRFLC
101 IF (IDEQ(J,K).GT.JNUM) IDEQ(J,K)=IDEQ(J,K)-J1 STRFLC
7162 IF (L.EQ.NUMFNP) GO TO 7170             STRFLC
7165 NX = NX + 1                               STRFLC
      IF (NX - N) 7145, 7140, 7130           STRFLC
7170 PRINT 7175, NBFLEW                       STRFLC
7175 FORMAT(/ * F. CONDUCTIVITY MATRIX BAND WIDTH = * I5) STRFLC
                                             STRFLC
      DO 41 I=1,NUMNP                          STRFLC
      K=IDEST(I)                               STRFLC
      KODE(1,I)=I0(2*I-1)                     STRFLC
      KODE(2,I)=I0(2*I)                      STRFLC
41 KODE(3,I)=IB(K)                            STRFLC
                                             STRFLC
C ***** COMPUTE BANDWIDTH OF THE STRUCTURE **** STRFLC
                                             STRFLC
      MBAND=1                                  STRFLC
      DO 111 N=1,NUMEL                         STRFLC
      DO 111 I=1,4                             STRFLC
      IN=IX(N,I)                               STRFLC
      DO 111 II=1,3                            STRFLC
      IA=IDEQ(II,IN)                          STRFLC
      DO 111 J=1,4                             STRFLC
      JN=IX(N,J)                               STRFLC
      DO 111 JJ=1,3                            STRFLC
111 MBAND=MAX0(MBAND,IABS(IA-IDEQ(JJ,JN)))    STRFLC
      MBAND=MBAND+1                            STRFLC
      PRINT 102,MBAND,KEQ                      STRFLC

```

```

102 FORMAT(25H GLOBAL SYSTEM BANDWIDTH, I5/24H TOTAL SYSTEM EQUATIONS)STRFLC
1, I5) STRFLC
PRINT 51 STRFLC
51 FORMAT(10H NODE ,10H IDEQ(1,N),10H IDEQ(2,N),10H IDEQ(3,N) ,10H)STRFLC
* ID(1,N) ,10H ID(2,N) ,10H ID(3,N) ) STRFLC
DO 53 N=1,MUMNP STRFLC
53 PRINT 52 ,N,(IDEQ(I,N),I=1,3),(KODE(J,N),J=1,3) STRFLC
52 FORMAT(I5,8I10) STRFLC
GO TO 5 STRFLC
C STRFLC
C INITIAL STRESSES IF ANY STRFLC
0000 PRINT 1, MEO STRFLC
PRINT 0010 STRFLC
0010 FORMAT (37H0 I N I ' I A L S T R E S S E S /56H#ELEMENT X-STRFLC
1STRESS Y-STRESS Z-STRESS XY-STRESS) STRFLC
NRES = 1 STRFLC
L = 1 STRFLC
0015 READ 0020, N, (RESID(N,I), I=1,4) STRFLC
0020 FORMAT (I10,4E10.3) STRFLC
IF (N - L) 0040, 0035, 0025 STRFLC
0025 DO 0030 I=1,4 STRFLC
0030 RESID(L,I)=RESID(L-1,I) STRFLC
0035 PRINT 0037, L, (RESID(L,I), I=1,4) STRFLC
0037 FORMAT ( I5,3X,4F12.3) STRFLC
IF (L .EQ. MUMEL) GO TO 0050 STRFLC
L = L + 1 STRFLC
IF (N - L) 0015, 0035, 0025 STRFLC
0040 PRINT 0045, N STRFLC
0045 FCNAT(* RESIDUAL STRESS INPUT ERROR, N=*I4) STRFLC
LBAD = 1 STRFLC
GO TO 0015 STRFLC
0050 GO TO 5 STRFLC
C STRFLC
C RESTART PARAMETERS IF NEEDED STRFLC
9000 IF (NJELT .GT. 0) GO TO 9015 STRFLC
PRINT 9010 STRFLC
9010 FORMAT (40H RESTART CARDS MUST FOLLOW ELEMENT CARDS) STRFLC
GO TO 15 STRFLC
9015 READ 9005, (KN(I),KS(I),MT(I),N(I), I=1,NJELT) STRFLC
9005 FORMAT( 4E20.6 ) STRFLC
GO TO 5 STRFLC
C STRFLC
C ALL INPUT NOW IN --IF CORRECT PROCEED WITH SOLUTION STRFLC
9999 IF (LBAD .NE. 0) GO TO 15 STRFLC
C STRFLC
C PLOT MESH STRFLC
IF (IPLOT .EQ. 0) GO TO 124 STRFLC
C STRFLC
C PREPARE CONSTANTS FOR PLOTTING STRFLC
CCYMIN = (10.5 - YLNTH) / 2.0 STRFLC
CCYMAX = CCYMIN + YLNTH STRFLC
CCXMIN = 0.0 STRFLC
CCXMAX = XLNTH STRFLC
XMIN=R(1) STRFLC
YMIN=Z(1) STRFLC
KMAX=XMIN STRFLC
YMAX=YMIN STRFLC
DO 112 I=2,MUMNP STRFLC
IF (R(I) .GT. XMAX) XMAX = R(I) STRFLC
IF (R(I) .LT. XMIN) XMIN = R(I) STRFLC

```

```

IF (Z(I) .GT. YMAX) YMAX = Z(I)
IF (Z(I) .LT. YMIN) YMIN = Z(I)
112 CONTINUE
XCOM = XLNGTH / (YMAX-XMIN)
YCOM = YLNGTH / (YMAX-YMIN)
DISPL = 0.02 * (XMAX - XMIN)

XSCL = (XPAX - XMIN) / XLNGTH
YSCL = (YMAX - YMIN) / YLNGTH
DSCL = DISPL / XLNGTH
PSF=XSCL/PSCL*0.5
PSFJ = PSF / CONJT
PJCL=PSCL*CONJT

CALL CCBGA
WRITE (98, 115) MED
115 FORMAT (BA9/BA9)
CALL CCLTF (-1.2,0.5, 1, 2)
CALL CCLBL (1,1)
DO 119 N=1,NUMEL
NI=IX(N,1)
NJ=IX(N,2)
NK=IX(N,3)
NL=IX(N,4)
XTR(1) = R(NI)
XTR(2) = R(NJ)
XTR(3) = R(NK)
XTR(4) = R(NL)
XTR(5) = XTR(1)
XTR(6) = Z(NI)
XTR(7) = Z(NJ)
XTR(8) = Z(NK)
XTR(9) = Z(NL)
IF (IX(N,5) .GT. NSHELL) GO TO 117
XTR(10) = XTR(6)
CALL CCPLT (XTR 1), XTR(6), 5, 4HJOIN)
117 CONTINUE
COR = 3.
XCEN = XTR(1) + XTR(2) + XTR(3)
YCEN = XTR(6) + XTR(7) + XTR(8)
IF (NK .EQ. NL) GO TO 118
COR = 4.
XCEN = XCEN + XTR(4)
YCEN = YCEN + XTR(9)
118 XCEN=XCEN/COR*XCEN+.05
YCEN=YCEN/COR*YCEN+.1
119 CONTINUE
WRITE (98,121) XSCL, YSCL
121 FORNAT (15H 1 IN CN X AXIS/4H =E12.4,3H FT/15H 1 IN OM Y AXIS/
14H =E12.4,3H FT)
DO 123 I=1,NUMMAT
WRITE (99, 2815) I
IF (I .LE. NSHELL) GO TO 122
WRITE (99,2830) (E(J,I),J=1,7)
GO TO 123
122 WRITE(98,2828) RO(I),(E1J,I),J=1,6)
123 CONTINUE
XP = CCXMAX + 0.5
CALL CCLTF (XP, 18.5, 0, 2)
CALL CCNEXT
C***** INITIALIZE*****
DO 4 I=1,NJELT

```



```

C
170 MP = MP + 1
NCC=0
IP=NFP(P)
READ 1005,NSTEP,DT
STRFLC
STRFLC
STRFLC
STRFLC
STRFLC
C
174 CONTINUE
TIME=TIME+DT
STRFLC
STRFLC
175 DO 195 MNN=1,IP
FLAG = ,FALSE.
STRFLC
STRFLC
IPER=IPER+1
STRFLC
INDEX = IPAT(IPER)
STRFLC
C
185 CONTINUE
STRFLC
STRFLC
C PD,TD CALCULATED, IF SYSDIM AND TOTALQ IS SUPPLIED
STRFLC
STRFLC
QQ=TOTALQ
IF(QQ.NE.0.) GO TO 185
STRFLC
RD=1.0
STRFLC
TOT=1.0
STRFLC
GO TO 187
STRFLC
186 CONTINUE
RD= SYSDIM*E(1,1)/(VISC*QQ)
STRFLC
TOT=E(1,1)*TIME*E(5,1)/VISC
STRFLC
187 CONTINUE
STRFLC
C
IF(FLAG) GO TO 190
STRFLC
CALL STIFF(THETA*CT/2.,A(N2),A(N2),A(N3),A(N4),A(N5),NEQ,MUFPNP,
STRFLC
,MN,MN9,MBAND,MBFLOW,TIME)
STRFLC
C
C SOLVE FOR DISPLACEMENTS
STRFLC
STRFLC
C
CALL SOLVES(THETA,DT,TIME,A(N2),A(N2),A(N3),A(N4),A(N5),A(N6),
STRFLC
,*KODE,ID(1),ID(12),NUMMP,NEQ,NUMEL,NSHELL,MBAND,MBFLOW,
STRFLC
,*MURFNP,ICCMR,IDEST,INDEX,IPER,MNN,IDEQ,PHIO,Q,IP,QN,A(N7),MN9,
STRFLC
,S TLOAD)
STRFLC
321 CONTINUE
IF(THETA.EQ.1.0) GO TO 323
STRFLC
I=0
STRFLC
DO 325 K=1,NEQ
STRFLC
A(N3+I)=A(N3+I)/THETA+DRT*A(N5+I)
STRFLC
STRFLC
325 I=I+1
STRFLC
323 CONTINUE
STRFLC
IF(INDEX.NE.0) PRINT 324,MP
STRFLC
324 FORMAT('0ISPL AND PRESS. AT THE END OF TIME STEP NO. ',I5)
STRFLC
IF(INDEX.EQ.0) GO TO 192
STRFLC
PRINT 2008,TIME
STRFLC
2008 FORMAT(1H1, 30H DISPL. AND PRESSURES AT TIME , E15.4// 6X,
STRFLC
, 10H NODAL PT ,20H0ISPL IN X-DIREC ,20H0ISPL IN Y-DIREC
STRFLC
, 14H PRESSURE 22H DIMENSIONLESS TIME,TO,2EH DIMENSIONLESS PRSTRFLC
*ESSURE,PD//)
STRFLC
CALL PRINT(MUMNP,IDEQ,MNXI,R,RC,TOT,A(N3),TEMP)
STRFLC
326 FORMAT(I10,SE20.5)
STRFLC
192 CONTINUE
STRFLC
190 CALL STRFLD(A(N3),A(N4),A(N5),TIME,IP,FLAG,NCC,DT)
STRFLC
IF(FLAG) GO TO 191
STRFLC
IF(INDEX.NE.0) GO TO 193
STRFLC
C.....NOT NEEDED IF UNCOUPLED FLOW PROBLEM IS SOLVED.....
STRFLC
IF( E(4,1).EQ.0.0 ) GO TO 193
STRFLC
PRINT 324,MP
STRFLC
PRINT 2008,TIME
STRFLC

```

```

CALL PRINT (NUMNP,IDEQ,NA>I,R,RD,TOT,A(M3),TEMP)
193 CONTINUE
IPER=IPER+IP-MNN
GO TO 196
191 CALL SECOAD (T)
IF (IPER.EQ.1) TIT=T-TST
TL=TTOTAL-T
IF (TL.LE.TIT.AND.AM.NLT.IP) GO TO 205
195 CONTINUE
196 CONTINUE
I=0
DO 581 K=1,NEQ
A(M3+I)=A(M3+I)
A(M3+I)=0.0
TLOAD(K)=0.0
581 I=I+1
C
MCC=MCC+1
IF (MCC.GE.NSTEP) GO TO 600
1005 FCRMAT (110,E20.5)
MP=MP+1
IP=NPP(MP)
GO TO 174
600 CONTINUE
MDTN=MDTN+1
500 CALL SECOAD (T)
TL=TTOTAL-T
IF (TL.LE.TIT.AND.MD.NLT.MIT) PRINT 210
IF (MP.LT.MIT.AND.MD.NGT.0) GO TO 170
210 FORMAT ('NCT ENOUGH TIME FOR ANOTHER PERTURBATION')
IF (IPUNCH.EQ.1.OR.IPUNCH.EQ.3) GO TO 225
GO TO 235
205 PRINT 210
225 PUNCH 230, (KN(I),KS(I),WT(I),M(I), I=1,NJELT)
230 FCRMAT (4E20.6)
235 PRINT 240, TIT
240 FCRMAT (18H PERTURBATION TIMEE10.3,8H SECONDS)
GO TO 5
300 IF (IPLOT .EQ. 1) CALL CCEND
CALL EXIT
C
END
SUBROUTINE APERTUR
C
LARGE A (125000),ID(900)
LARGE IX(301,5),RESID(301,4),R(300),Z(300),UR(300),UZ(300)
* ,CODE(300),IDEST(300),R,KN(50),R,KS(50),WT(50),ICUT(301),Q(300),
LARGE *
*QP(50),M(50),VEL(50),FR(50),RE(50),QH(900),DISPI(300,2),TEMP(300),
LARGE *
*PHIO(300),IB(300),IDEQ(3,300),KODE(3,300),IEL(50,2),IMP(50,4)
LARGE *
* ,TLOAD(900),SIGN(50),SIGT(50),D90(600)
STRFPL *
COMMON/GEN/NSMELL,IPUNCH,E(7,12),INDEX,MP,MNN,NCORE,MUMP,ICCMFR,
GEN.2
1 IUMEL,NO2,NEO(16),DISPL,NJELT,IPER,NUMMAT,PSF,PSFJ,KSEL,SPHT,
GEN.3
JVISQ,YSCL,DSCLE,PSCLE,PJCL,AP(4),COM,IN,MAXI,M5,MBAND,LNCTM,NEQ,NJMP
GEN.4
* ,NDFLOW,NUMNF2,NUMNFP,LN(12),NF2
GEN.5
COMMON/APTR/IRAND,NJUMP,AAS,AAM
APT.2
IF (IRAND.NE.0) GO TO 18
STRFCL *
DO 15 J=1,NJELT
STPFCL *
I = IOUT(J)
STRFCL *

```



```

MAT=IABS(IX(I,5))
WT(J)=E(5,MAT)
15 CONTINUE
GO TO 35
C
10 PRINT 16
16 FORMAT (* APERATURES ARE RANDOMLY GENERATED*)
DO 20 K=1,NJELT
J = ICUTIK)
MAT=IABS( IX(J,5) )
APR=0.0
DO 25 I=1,12
YFL=RNRF(0)
25 APR=APR+YFL
VTH=(APR-E.0)*AAS+AAM
WT(K) = -EXP(VTH)
20 CONTINUE
35 IF( NJMP.EQ.0 ) GO TO 40
C
DO 50 JI=1,NJMP
READ 100,I,COEG,COEM1,COEM2,COEM3,COEM4
100 FORMAT (I5,F10.3,4F15.5)
PRINT 200 ,I,COEG,COEM1,COEM2,COEM3,COEM4
200 FORMAT (I14,7X,6HCOEG= ,F10.3,10X,7HCOEM1= ,F10.3,10X,7HCOEM2= ,F10.3,10X,7HCOEM3= ,F10.3,10X,7HCOEM4= ,F10.3)
DO 220 J = 1,NJELT
IF (IOUT(J) .EQ. I) GO TO 230
220 CONTINUE
230 WT(J) = COEG * WT(J)
MAT=IABS( IX(I,5) )
E(1,MAT)=COEM1*E(1,MAT)
E(2,MAT)=COEM2*E(2,MAT)
E(3,MAT)=COEM3*E(3,MAT)
E(4,MAT)=COEM4*E(4,MAT)
50 CONTINUE
C
40 CONTINUE
RETURN
END
SUBROUTINE STIFF(OT,A1,A2,2,BO,PO,NQ,NAP,MN,MN9,MT,MF,TIME)
C
LARGE A(125000),IO(900)
LARGE IX(301,5),RESID(301,4),R(300),Z(300),JR(300),UZ(300)
* ,COE(300),IDEST(300),R,KN(50),R,KS(50),WT(50),ICUT(301),Q(300),
*QP(50),W(50),VEL(50),FR(50),RE(50),QN(900),DISPI(300,2),TEMP(300),
* PHIQ(300),IB(300),IOEQ(3,300),KODE(3,300),IEL(50,2),IMP(50,4)
* ,TLOAD(900),SIGN(50),SIGT(90),DBO(600)
COMMON/BLANK/S(6,8),P(10),RSTRS(4),VCL,RRR(5),ZZZ(5),LBA0,RADN,
1 RR(4),ZZ(4),IPAT(50),ACELK,ACELY,NRES,RO(12),
2 MTYPE,XI,XCFN,CEN,XTR(10),FAC,H(6),PD(6,12),QQ(2,4),
3 PRS,FZS,PRT,FZT,EG
COMMON/GEN/MSHELL,IPUNCH,E(7,12),INDEX,MP,N4N,NCORE,NJMP,ICOMPR,GEN.2
1 NUPEL,N02,MED(16),DISFL,NJELT,IPER,NUMMAT,FSF,PSFJ,KSCAL,SFMT,GEN.3
3VISC,YSCAL,DSCL,FSCL,PJCL,NP(4),COMLIP,MAXI,NB,MEAND,LENGTH,MEQ,NJMPGEN.4
* ,NBFLOW,NUPFN2,NUMFNP,LM(12),MF2
COMMON/EP/ST(4,8),SO(2,4),AJ(8,2),DD(2,2),QJ(4),HR(6),MZ(5)
* ,EJ(2,2)
LARGE A1(NQ,1),A2(NMP,1),B(1),BO(1),PO(1)
DIMENSION PP(2),RP(2),TL(8)
COMMON/STF/SF(8,0),SC(8,4),SH(4,4),SE(4,4)

```

```

C                                          STRFLC
C                                          STRFLC
C          REMIND 8                       STRFLC
C          REMIND 9                       STRFLC
C          ISH=4                           STRFLC
C          JSH=2                            STRFLC
C          LBA0= 0                         STPFLE
C                                          STRFLC
C          DC 702 K=1,NEQ                 STRFLC
C          DD 702 L=1,MBAND                STRFLC
C          702 A1(K,L)=0.0                 STRFLC
C          DD 701 KK=1,MNP                STRFLC
C          DD 701 LL=1,MBFLCW             STRFLC
C          IF(INF2.GT.NUMFNPI) A2(KK,MBFLOW*LL)=0.0 STRFLC
C          701 A2(KK,LL)=0.0              STRFLC
C                                          STRFLC
C          MJ = 0                          STRFLC
C                                          STRFLC
C          DO 300 N=1,MJNEL                STRFLC
C          DD 200 I=1,4                    STRFLC
C          NP(I)=IX(N,I)                   STRFLC
C          200 CONTINUE                     STRFLC
C          MTYPE=IX(N,5)                   STRFLC
C          IF(MTYPE.LE.MSHCELL) GO TO 92   STRFLC
C          MJ=MJ+1                           STRFLC
C                                          STRFLC
C          C *****                        STRFLC
C          C JOINT MATERIAL PROPERTY ASSIGNMENT STRFLC
C          C                               STRFLC
C          KN AND KS ARE MODIFIED AFTER EACH PERTURBATION, THEREFORE, STRFLC
C          AFTER FIRST PERTURBATION OF FIRST TIME STEP CALCULATED STIFFNESSES STRFLC
C          ARE USED                          STRFLC
C          C                               STRFLC
C          WHEN RESTARTED STIFFNESS VALUES THAT ARE RESULTS OF PRECEEDING STRFLC
C          RUNS ARE READ IN DIRECTLY         STRFLC
C          C                               STRFLC
C          IF(INP.GT.1) GO TO 61             STRFLC
C          IF(NNH.GT.1) GO TO 61            STRFLC
C          IF (IPUNCH .GE. 2) GO TO 61     STRFLC
C          KN(INJ) = E(1,MTYPE)             STRFLC
C          KS(INJ) = E(2,MTYPE)             STRFLC
C          61 CONTINUE                       STRFLC
C                                          STRFLC
C          C *****                        STRFLC
C          C JOINT ELEMENTS *****         STRFLC
C          CALL JTSTIF (B,BO,PO,MJ,N)       STRFLC
C          IF (VOL.LI.0.0) IX(N,5)=-IX(N,5) STRFLC
C          CALL ASHMBLE (DT,A1,A2,N,S,AJ,DD,EJ,IOEQ,NEQ,NF2,IOEST,JSH) STRFLC
C          GO TO 300                         STRFLC
C          C *****                        STRFLC
C          C SOLID ELEMENTS *****         STRFLC
C          C                               STRFLC
C          92 CONTINUE                       STRFLC
C          IF ( IPER.GT.1.AND.SPMT.EQ.0.0) GO TO 94 STRFLC
C          IF(NMN.GT.1) GO TO 94            STRFLC
C          CALL ELSTIF (B,BO,PO,N)          STRFLC
C          CALL ASHMBLE (DT,A1,A2,N,SF,SC,SH,SE,IOEQ,NQ,NF2,IOEST,ISH) STRFLC
C          GO TO 300                         STRFLC
C          94 READ (8) SF,SC,SP,SE,NP        STRFLC
C          93 CALL ASHMBLE (DT,A1,A2,N,SF,SC,SH,SE,IOEQ,NQ,NF2,IOEST,ISH) STRFLC
C          300 CONTINUE                       STRFLC
C          IF(NAN.GT.1) GO TO 500           STRFLC

```

```

DO 301 I=1, NUMNP                                STRFLC
J=IDEST(I)                                       STRFLC
K=IDEO(3,I)                                     STRFLC
IF( KODE(3,I).LE.0 ) GO TO 350                  STRFLC
TLOADIK=PO(K)*1.0E+20                           STRFLC
QN(J)=TLOAD(K)                                  STRFLC
GO TO 301                                        STRFLC
350 QN(NUMNP+J)=TLOAD(K)+Q(J)                   STRFLC
301 CONTINUE                                     STRFLC
500 RETURN                                       STRFLC
END                                              STRFLC
SUBROUTINE JTSTIF(B,B0,PD,H,N)                  STRFLC
C
  LARGE A(125000),ID(900)                       STRFLC
  LARGE IX(301,5),RESID(3(1,4),R(300),Z(300),UR(300),UZ(300)) LARGE.
  * ,CDE(300),IDEST(300),R,KN(50),R,KS(50),WT(50),ICUT(301),O(300), LARGE.
  *QP(50),M(50),VEL(50),FR(50),RE(50),QN(900),DISPI(300,2),TEMP(300),LARGE.
  *PHIO(300),IB(300),IDEQ(3,300),KODE(3,300),IEL(50,2),IMP(50,4) LARGE.
  * ,TLOAD(900),SIGM(50),SIGT(50),DBO(600)      STRFLC
  COMMON/BLANK/S(8,8),P(10),RSTRS(4),VOL,RRR(5),ZZZ(5),LBD,RADN, BLANK.
1  RR(4),ZZ(4),IPAT(50),ACELX,ACELY,NRES,RO(12), BLANK.
2  NTYPE,XI,XCE,XCYCEN,XTR(10),FAC,M(8),PD(4,12),QQ(2,4), BLANK.
3  PRS,PZS,PRT,PZT,EG BLANK.
  COMMON/GEN/NSHELL,IPUNCH,E(7,12),INDEX,MP,NYN,NCORE,MUMNP,ICOMPR, GEN.2
1  NUNEL,NJ2,MED(16),DISPL,NJELT,IMR,NUMMAT,FSF,PSFJ,KSC,L,SPMT,GEN.3
3  VISL,YSC,L,DSCL,FSCL,PJCL,NP(4),CONLIM,MAXI,NB,MEAND,LANGTH,MEQ,NJPP,GEN.4
* ,MBFLOW,MUMNF2,MUMFNP,L(12),NF2 GEN.5
  COMMON/EN/ST(4,8),SQ(2,4),AJ(8,2),DD(2,2),QU(4),HR(6),HZ(6) EM.2
* ,EJ(2,2) EM.3
C
  LARGE B(1),B0(1),PD(1)                        STRFLC
  DIMENSION AS(4,4),TR(2,2),PPP(8),SS(4,4),TTF(6),SSS(6),V(4) STRFLC
  DIMENSION AT(8,2),CJ(8,2),DUM(24),PP(8)      STRFLC
  DIMENSION EPRO(8),CPRO(8)                     STRFLC
  DATA AT/1.,-1.,1.,-1.,-1.,1.,-1.,1./ STRFLC
  DATA AS/2.,1.,-1.,-2.,1.,2.,-2.,-1.,-1.,-2.,2.,1.,-2.,-1.,1.,2./ STRFLC
  DATA SS/-0.5,0.5,0.,0.,0.5,0.,0.5,0.,-0.5,0.,0.,-0.5,0.5,0.5,0., STRFLC
1  0.5,0.,0.,-0.5/ STRFLC
C
  DATA INCON/10HINC(PRESS)                     STRFLC
  II=IX(IN,1)                                    STRFLC
  JJ=IX(N,2)                                     STRFLC
  RM = -1.0                                      STRFLC
  IF (NAXI.NE.0) RM = -(R(JJ) + R(II)) / 2.0    STRFLC
  DR=R(JJ)-R(II)                                 STRFLC
  DZ=Z(JJ)-Z(II)                                 STRFLC
  VOL = SQRT(DR*DR + DZ*DZ)                       STRFLC
  IF (VOL.EQ.0.0) GO TO 470                       STRFLC
  STRFLC
  STRFLC
C** MATERIAL PROPERTIES                          STRFLC
50 COMS=KS(M)*VOL/6.0                            STRFLC
  COMN=KN(M)*VOL/6.0                              STRFLC
  STRFLC
C
  INITIALIZE                                     STRFLC
  DG 10G II=1.8                                  STRFLC
  P(II)=0.0                                       STRFLC
  EPRO(II)=0.0                                    STRFLC
  CPRO(II)=0.0                                    STRFLC
  DG 10G JJ=1.8                                  STRFLC
100 S(II,JJ) = 0.0                                STRFLC
  DG 99 I=1,4                                     STRFLC
  EJ(II)=0.0                                      STRFLC

```

```

99 DD(II)=0.0                                STRFLC
DD 98 I=1,16                                  STRFLC
99 AJ(I)=0.0                                  STRFLC
C        DEVELOP RESIDUAL STRESS CONTRIBUTIONS TO THE LOAD VECTOR STRFLC
C        C ***** STRFLC
C THE FOLLOWING SIGN CONVENTION IS ADOPTED, THE NORMAL STRESS IS POSITIVE STRFLC
C WHEN DIRECTED OUTWARD THE ELEMENT ON THE FACE (II, JJ). THE SHEAR STRESS STRFLC
C IS POSITIVE WHEN DIRECTED FROM II TO JJ AND KK TO LL INSIDE THE ELEMENT STRFLC
C
      TR(1,1)=DR/VOL                            STRFLC
      TR(1,2)=DZ/VOL                            STRFLC
      IF(IPER.GT.1) GO TO 171                   STRFLC
      SC = TR(1,1) * TR(1,2)                   STRFLC
      S2 = TR(1,2) ** 2                         STRFLC
      C2 = TR(1,1) ** 2                         STRFLC
111 RSTRS(1)=RESID(N,1)*S2+RESID(N,2)*C2+2.*RESID(N,4)*SC STRFLC
RSTRS(2)=(RESID(N,2)-RESID(N,1))*SC+RESID(N,4)*(S2-C2) STRFLC
      TFORMY=RSTRS(1)*VOL*RM                   STRFLC
      TFORMX=RSTRS(2)*VOL*RM                   STRFLC
      RATLO=0.0                                STRFLC
      IF(MAXI.EQ.0) GO TO 112                   STRFLC
      II=IX(N,1)                                STRFLC
      RATLO=(-1./RM)*[R(II)/2.+VOL/3.0]-0.5    STRFLC
112 PPP(1)=TFCRY*(0.5-RATLO)                   STRFLC
      PPP(2)=TFCRX*(0.5-RATLO)                 STRFLC
      PPP(3)=TFCRY*(0.5+RATLO)                 STRFLC
      PPP(4)=TFORX*(0.5+RATLO)                 STRFLC
      PPP(5)=-PPP(3)                           STRFLC
      PPP(6)=-PPP(4)                           STRFLC
      PPP(7)=-PPP(1)                           STRFLC
      PPP(8)=-PPP(2)                           STRFLC
171 CONTINUE                                  STRFLC
      DO 200 II=1,4                             STRFLC
      IN = II + II                             STRFLC
      IS = IN - 1                              STRFLC
      DO 200 JJ=1,4                             STRFLC
      JN = JJ + JJ                             STRFLC
      JS = JN - 1                              STRFLC
      TDUM=AS(II, JJ)                          STRFLC
      IF(MAXI.NE.0) TDUM=-TDUM*RM+SS(II, JJ)*DR STRFLC
      S(IS, JS)=COMS*TDUM                      STRFLC
200 S(IN, JN)=COMM*TDUM                      STRFLC
C        ROTATE TO GLOBAL COORDINATES          STRFLC
      TR(2,1) = -TR(1,2)                       STRFLC
      TR(2,2) = TR(1,1)                       STRFLC
      IF( (TR(1,1).EQ.1.) GO TO 450            STRFLC
      DO 400 NM=1,4                             STRFLC
      JJ = NM + NM                             STRFLC
      DO 410 II=1,8                             STRFLC
      TDUM=S(II, JJ-1)*TR(1,1)+S(II, JJ)*TR(2,1) STRFLC
      S(II, JJ) = S(II, JJ-1)*TR(1,2) + S(II, JJ) *TR(2,2) STRFLC
410 S(II, JJ-1)=TDUM                          STRFLC
      DO 420 II=1,8                             STRFLC
      TDUM=S(JJ-1, II)*TR(1,1)+S(JJ, II)*TR(2,1) STRFLC
      S(JJ, II) = S(JJ-1, II)*TR(1,2) + S(JJ, II)*TR(2,2) STRFLC
420 S(JJ-1, II)=TDUM                          STRFLC
400 CONTINUE                                  STRFLC

```

		STRFLC
C	450 CONTINUE	STRFLC
	IF(IPER.EQ.1) GO TO 465	STRFLC
	DO 460 I=1,4	STRFLC
	K=IX(M,I)	STRFLC
	II = I + I	STRFLC
	J = II - 1	STRFLC
	461 K1=IDEQ(1,K)	STRFLC
	K2=IDEQ(2,K)	STRFLC
	BO(K1)=BO(K1)+PPP(J)*TR(1,2)+PPP(II)*TR(2,2)	STRFLC
	BO(K2)=BO(K2)-PPP(J)*TR(2,2)+PPP(II)*TR(1,2)	STRFLC
	460 CONTINUE	STRFLC
	465 CONTINUE	STRFLC
C		STRFLC
	COM=1.0/(12.0*VISC)	STRFLC
	DO 60 L=1,4	STRFLC
	K=IX(M,L)	STRFLC
	K1=IDEQ(1,K)	STRFLC
	K2=IDEQ(2,K)	STRFLC
	60 V(L)=PO(K2)*TR(1,1)-PO(K1)*TR(1,2)	STRFLC
	EPSN=.5*(V(4)-V(1)+V(3)-V(2))	STRFLC
	MO=MT(M)	STRFLC
	IF(EPN.GE.MO) GO TO 61	STRFLC
	PRINT 62,N	STRFLC
	62 FORMAT('DISPLACEMENT GREATER THAN ALLOWED IN ELEMENT NO. ',I5)	STRFLC
	61 M(N)=ABS(ABS(MO)+EPSN)	STRFLC
	IF(M(N).LT.1.0E-8) M(N)=0.0	STRFLC
	EN=M(N)**3	STRFLC
	QP(N)=EN*COM*RM	STRFLC
		STRFLC
	DO 71 I=1,4	STRFLC
	71 DD(I)=QP(I)/VOL	STRFLC
	DD(1,2)=-DD(1,2)	STRFLC
	DD(2,1)=DD(1,2)	STRFLC
	K=IX(M,5)	STRFLC
	IF(ICOMP.EQ.INCCM) GO TO 73	STRFLC
	EE=VOL/16.0*E(7,K)	STRFLC
	EE=-EE*M(I)*RM	STRFLC
	DO 72 I=1,2	STRFLC
	DO 72 J=1,2	STRFLC
	72 EJ(I,J)=EE	STRFLC
	EJ(1,1)=2.0*EJ(1,1)	STRFLC
	EJ(2,2)=EJ(1,1)	STRFLC
	73 CONTINUE	STRFLC
		STRFLC
	OL=-E(6,K)*VOL*RM/4.0	STRFLC
	TSIN=OL*TR(1,2)	STRFLC
	TCOS=OL*TR(1,1)	STRFLC
	DO 300 I=1,4	STRFLC
	II=I+I	STRFLC
	AJ(II,1)=AT(II)*TCOS	STRFLC
	AJ(II-1,1)=AT(II-1)*TSIN	STRFLC
	AJ(II,2)=AJ(II,1)	STRFLC
	AJ(II-1,2)=AJ(II-1,1)	STRFLC
	300 CONTINUE	STRFLC
C		STRFLC
	IF(INN.GT.1) GO TO 80	STRFLC
	IF(SPMT.EQ.0.) GO TO 80	STRFLC
	DY=-TR(1,2)	STRFLC
	DG=QP(M)*SPNT	STRFLC
	GY=DG*DY/2.0	STRFLC

```

I1=IX(N,1) STRFLC
I2=IX(N,2) STRFLC
K1=IDEQ(3,I1) STRFLC
K2=IDEQ(3,I2) STRFLC
TLOAD(K1)=TLOAD(K1)+GY STRFLC
TLOAD(K2)=TLOAD(K2)-GY STRFLC
60 CONTINUE STRFLC
C STRFLC
IF(IPER.GT.1) GO TO 640 STRFLC
DO 600 I=1,2 STRFLC
DO 600 J=1,2 STRFLC
K=IX(N,J) STRFLC
L=IDEST(K) STRFLC
EPRO(I)=EPRO(I)+EJ(I,J)*PHZO(L) STRFLC
600 CONTINUE STRFLC
DO 610 I=1,8 STRFLC
DO 610 J=1,2 STRFLC
K=IX(N,J) STRFLC
L=IDEST(K) STRFLC
CPRO(I)=CPRO(I)+AJ(I,J)*PHIO(L) STRFLC
610 CONTINUE STRFLC
DO 620 J=1,2 STRFLC
K=IX(N,J) STRFLC
K3=IDEQ(3,K) STRFLC
BO(K3)=BO(K3)-EPRO(J) STRFLC
620 CONTINUE STRFLC
DO 630 J=1,4 STRFLC
K=IX(N,J) STRFLC
K1=IDEQ(1,K) STRFLC
K2=IDEQ(2,K) STRFLC
BO(K1)=BO(K1)+CPRC(IJ+J-1) STRFLC
BO(K2)=BO(K2)+CPRC(IJ+J) STRFLC
630 CONTINUE STRFLC
640 CONTINUE STRFLC
RETURN STRFLC
470 PRINT 471,N STRFLC
471 FORMAT(17H BAD JOINT ,N=I3/) STRFLC
LBAD=LBAD+1 STRFLC
RETURN STRFLC
END STRFLC
SUBROUTINE FORMB(S1,T1,IP) STRFLC
COMMON/BLANK/S(8,8),P(18),RSTRS(4),VOL,RRR(5),ZZZ(5),LBAD,RADN, BLANK,
1 MR(4),ZZ(4),IPAT(58),ACELX,ACELY,MRES,RO(12), BLANK,
2 MTYPE,XI,XCE,YCEN,XTR(18),FAC,M(6),PD(4,12),QQ(2,4), BLANK,
3 PRS,FZS,PRT,PZT,EG BLANK,
COMMON/EM/ST(4,8),SQ(2,4),AJ(8,2),DD(2,2),QU(4),HR(6),HZ(6) EM,2
* EJ(2,2) EM,3
DIMENSION HS(6),HT(6),II(6),JJ(6) STRFLC
DATA II/1,3,5,7,9,10/,JJ/2,4,6,8,11,12/ STRFLC
C STRFLC
DO 50 I=1,48 STRFLC
50 PD(I)=0.0 STRFLC
SM=1.0-S1 STRFLC
SP=1.0+S1 STRFLC
TM=1.0-T1 STRFLC
TP=1.0+T1 STRFLC
C STRFLC
H(1)=SM*TP/4. STRFLC
H(2)=SP*TP/4. STRFLC
H(3)=SM*TP/4. STRFLC
H(4)=SM*TP/4. STRFLC
H(5)=(1.0-S1)*S1 STRFLC

```

```

C      H(6)=(1.0-T1*T1)
C      HS(1)=-TH/4.
C      HS(2)=-HS(1)
C      HS(3)=TP/4.
C      HS(4)=-HS(3)
C      HS(5)=-2.*S1
C      HS(6)=0.0
C      HT(1)=-SH/4.
C      HT(2)=-SP/4.
C      HT(3)=-HT(2)
C      HT(4)=-HT(1)
C      HT(5)=0.0
C      HT(6)=-2.*T1
C      PZT=HT(1)*ZZ(1)+HT(2)*ZZ(2)+HT(3)*ZZ(3)+HT(4)*ZZ(4)
C      PZS=HS(1)*ZZ(1)+HS(2)*ZZ(2)+HS(3)*ZZ(3)+HS(4)*ZZ(4)
C      PRS=HS(1)*RR(1)+HS(2)*RR(2)+HS(3)*RR(3)+HS(4)*RR(4)
C      PRT=HT(1)*RR(1)+HT(2)*RR(2)+HT(3)*RR(3)+HT(4)*RR(4)
C      XJ=PRS*PZT-PRT*PZS
C      PSR=PZT/XJ
C      PTR=-PZS/XJ
C      PSZ=-PRT/XJ
C      PTZ=PRS/XJ
C      DO 100 I=1,6
C      HR(I)=PSR*HS(I)+PTR*HT(I)
100  HZ(I)=PSZ*HS(I)+PTZ*HT(I)
C      IF (IP.NE.0) GO TO 150
C      R=1
C      GO TO 170
150  R=H(1)*RR(1)+H(2)*RR(2)+H(3)*RR(3)+H(4)*RR(4)
C      FCRM STRAIN DISPLACEMENT MATRIX
C
170  DO 200 K=1,6
C      I=II(K)
C      J=JJ(K)
C      PD(1,I)=HR(K)
C      PD(2,J)=HZ(K)
C      IF (IP) 180,190,100
180  PD(3,I)=H(K)/R
190  PD(4,I)=HZ(K)
200  PD(4,J)=HR(K)
C      DO 300 K=1,4
C      QQ(1,K)=HR(K)
300  QQ(2,K)=HZ(K)
C
C      FAC=XJ*R
C      RETURN
C      END
C      SUBROUTINE ELSTIF(B,B0,PO,N)
C
C      LARGE A(1,25000),IO(900)
C      LARGE IX(301,5),RESIO(301,4),R(300),Z(300),UR(300),UZ(300)
C      * ,CODE(300),IDEST(300),R,KM(50),R,KS(50),HT(50),ICUT(301),Q(300),LARGE,
C      *QP(50),M(50),VEL(50),FR(50),RE(50),QH(900),JISPI(300,2),TEMP(300),LARGE,
C      *PHIQ(300),IB(300),IDEQ(3,300),CODE(3,300),IEL(50,2),IMP(50,4)
C      * ,TLOAD(900),SIGN(50),SIGT(50),DBO(600)
C      COMMON/BLANK/S(8,0),P(10),RSTRS(4),VGL,RRR(5),ZZ(5),LBD,RADN,
C      BLANK,2

```

```

1          RR(4),ZZ(4),IPAT(50),ACELX,ACELY,MRES,RC(12),   BLANK.
2      MTYPE,XI,XCE1,YCEN,XTR(10),FAC,H(6),PD(4,12),QQ(2,4),   BLANK.
3      PRS,PZS,PRT,PZT,EG                                       BLANK.
COMMON/GEN/MSHELL,IPUNCH,E(7,12),INDEX,MP,MN,NCRE,MUMMP,ICMFR, GEN.2
1      MUMEL,NO2,HED(16),DISPL,NJELT,IPER,MUMMAT,PSF,PSFJ,XSCL,SPWT,GEN.3
3      VISC,YACL,DACL,FSCL,PJCL,MP(4),COML,IN,MAXI,NB,MBAND,LNPTH,NEQ,RJMP,GEN.4
*      ,MDFLOW,MUMFZ,MUMFAP,LN(12),NFZ                               GEN.5
COMMON/EM/ST(4,8),SQ(2,4),AJ(8,2),DD(2,2),QU(4),HR(6),HZ(6)
*      ,EJ(2,2)                                                    EM.2
C
LARGE B(1),BO(1),PO(1)                                          STRFLC
DIMENSION DX(4),EE(1),EMU(1),EN(1),EM(1),OUM(2,4),           STRFLC
*      PR(10),TTT(6),SSS(6),QB(4),D(4,4)                          STRFLC
COMMON/STF/SF(8,8),SC(8,4),SH(4,4),SE(4,4)                   STRFLC
DIMENSION EPRO(10),CPRO(10)                                    STRFLC
DATA INCP/10HINCOMPRESS/,SSS/-.57735027,.,57735027,.,0,.,-.7745967,
.0,.,.7745967/,TTT/1.0,1.0,0.0,0.0,55555556,.,00000009,.,55555556/
C
DO 6 I=1,10
EPRO(I)=0.0
CPRO(I)=0.0
PR(I)=0.0
6 P(I)=0.0
DO 2 J=1,16
SE(J)=0.0
STRFLC
2 SH(J)=0.0
DO 3 JJ=1,32
ST(JJ)=0.0
STRFLC
3 SC(JJ)=0.0
DO 1 I=1,4
DX(I)=0.0
STRFLC
1 OX(I)=0.0
STRFLC
5 CONTINUE
DO 70 I=1,4
M=IX(N,I)
RR(I)=R(N)
ZZ(I)=Z(N)
STRFLC
70 CONTINUE
K=IX(N,5)
FACT=E(2,K)/((1.-2.*E(3,K))^(1.+E(3,K)))
STRFLC
C1=(1.-E(3,K))*FACT
STRFLC
C2=E(3,K)*FACT
STRFLC
C3=(.5-E(3,K))*FACT
STRFLC
EEN=E(4,K)
STRFLC
PERM=E(1,K)/VISC
STRFLC
IF (MAXI.EC.8) D7=0.0
STRFLC
IF (ICOMP.EQ.INC(N)) EEN=1.0
STRFLC
DO 85 I=1,64
SF(I)=0.0
STRFLC
85
C
FORM STRAIN AND FLOW MATRICES AT THE CENTER OF THE ELEMENT
C
DO 520 I=1,3
D(I,4)=0.0
STRFLC
D(4,I)=0.0
STRFLC
DO 510 J=1,3
D(I,J)=C2
STRFLC
510 D(I,I)=C1
STRFLC
520 D(4,4)=C3
STRFLC
CALL FORMB(0.0,0.0,0.0,MAXI)
STRFLC
DO 540 I=1,8
SQ(I)=PERM*QQ(I)
STRFLC
540 DO 533 I=1,4
STRFLC

```



```

      DO 533 J=1,8                                STRFLC
      DO 533 K=1,4                                STRFLC
533 ST(I,J)=ST(I,J)+D(I,K)*PD(K,J)              STRFLC

      K=IX(N,5)                                   STRFLC

      NTS=2                                        STRFLC
      IF(NAXI.NE.0) NTS=3                         STRFLC
      NN=(NTS-2)*3                                STRFLC

      DO 500 LR=1,NTS                              STRFLC
      S1=SSS(LR+NN)                               STRFLC
      DO 500 LZ=1,NTS                              STRFLC
      T1=SSS(LZ+NN)                               STRFLC
      CALL FORMB(S1,T1,NAXI)                      STRFLC
      FAC=FAC*TTT(LR+NN)*TTT(LZ+NN)             STRFLC
C
C ***** FORM NODAL LOAD VECTOR *****        STRFLC
C
      IF(ACELY.EQ.0.) GO TO 453                   STRFLC
      FACF=FAC*FO(K)*ACELY                       STRFLC
      DO 451 I=1,4                                STRFLC
      J=I+1                                       STRFLC
451 P(J)=P(J)-H(I)*FACF                         STRFLC
453 CONTINUE                                     STRFLC
      IF(IIPER.NE.1) GO TO 58                    STRFLC
      DO 57 I=1,8                                 STRFLC
      DO 57 J=1,4                                 STRFLC
57 PR(I)=PR(I)+RESID(N,J)*PD(J,I)*FAC         STRFLC
58 CONTINUE                                     STRFLC
C
C K MATRIX                                       STRFLC
C
      DO 98 I=1,8                                  STRFLC
      D1=(C1*PD(1,I)+C2*PD(2,I)+C2*PD(3,I))*FAC STRFLC
      D2=(C2*PD(1,I)+C1*PD(2,I)+C2*PD(3,I))*FAC STRFLC
      D3=(C2*PD(1,I)+C2*PD(2,I)+C1*PD(3,I))*FAC STRFLC
      D4=(C3*PD(4,I))*FAC                        STRFLC
      DO 90 J=I,8                                  STRFLC
90 SF(J,I)=SF(J,I)+D1*PD(1,J)+D2*PD(2,J)+D3*PD(3,J)+D4*PD(4,J) STRFLC
C
C C AND E MATRICES                              STRFLC
C
      FACN=FAC*EEN                               STRFLC
      DO 100 I=1,8                                STRFLC
      DB=PD(1,I)+PD(2,I)+PD(3,I)                STRFLC
      DO 100 J=1,4                                STRFLC
100 SC(I,J)=H(J)*DB*FACN+SC(I,J)              STRFLC
      IF(ICONPR.EQ.INCM) GO TO 150              STRFLC
      FACM=FAC.*F(5,K)                           STRFLC
      DO 130 I=1,4                                STRFLC
      DO 130 J=1,4                                STRFLC
130 SE(I,J)=H(I)*H(J)*FACM+SE(I,J)           STRFLC
150 CONTINUE                                     STRFLC
C
C H MATRIX                                       STRFLC
C
      FACK=FAC*FERM                               STRFLC
      DO 170 I=1,4                                STRFLC
      DX(I)=DX(I)+FACK*(QQ(1,I)*ACELX+QQ(2,I)*(-1.0)))*SPWT STRFLC
      DO 170 J=1,4                                STRFLC
      MN=QQ(1,I)*QQ(1,J)+QQ(2,I)*QQ(2,J)       STRFLC

```

```

170 SH(I,J)=H1*FACK+SH(I,J)
500 CONTINUE
C
C ***** FORM GLOBAL MODAL LOAD VECTOR *****
C
      IF(MAN.GT.1) GO TO 503
      DO 501 J=1,4
      K=IX(N,J)
      K1=IDEQ(1,K)
      K2=IDEQ(2,K)
      TLOAD(K1)=TLOAD(K1)-P(J+J-1)
      TLOAD(K2)=TLOAD(K2)-P(J+J)
      IF(IPER.GT.1) GO TO 501
      BO(K1)=BO(K1)-PR(J+J-1)
      BO(K2)=BO(K2)-PR(J+J)
501 CONTINUE
      IF(SPWT.EC.0) GO TO 503
      DO 502 I=1,4
      J=IX(N,I)
      K=IDEQ(3,J)
      TLOAD(K)=TLOAD(K)-DX(I)
502 CONTINUE
503 CONTINUE
      DO 505 I=1,8
      DO 505 J=1,4
505 SF(J,I)=SF(I,J)
C
      IF(IPER.GT.1) GO TO 830
      DO 800 I=1,4
      DO 800 J=1,4
      K=IX(N,J)
      L=IDEST(K)
      EPRO(I)=EPRO(I)+SE(I,J)*PHI(L)
800 CONTINUE
      DO 810 I=1,8
      DO 810 J=1,4
      K=IX(N,J)
      L=IDEST(K)
      CPRO(I)=CPRO(I)+SC(I,J)*PHI(L)
810 CONTINUE
      DO 820 J=1,4
      K=IX(N,J)
      K1=IDEQ(1,K)
      K2=IDEQ(2,K)
      K3=IDEQ(3,K)
      BO(K1)=BO(K1)+CPRC(J+J-1)
      BO(K2)=BO(K2)+CPRC(J+J)
      BO(K3)=BO(K3)-EPRC(J)
820 CONTINUE
830 CONTINUE
615 CONTINUE
      WRITE (9) ST,SQ,NP
      WRITE (8) SF,SC,SH,SE,NP
C
700 RETURN
C
C
      END
SUBROUTINE ASMBLE (DT,A1,A2,N,SF,SC,SH,SE,IDEQ,NQ,NMP,IDEST,NH)
C
COMMON/BLANK/S(8,8),P(18),RSTRS(4),VCL,RRR(5),ZZZ(5),LBAO,RADN,
1      RR(4),ZZ(4),IPAT(58),ACEIX,ACELY,NRES,RO(12),
      BLANK,2

```

```

2      MTYPE,XI,XCE,X,YCEN,XTR(10),FAC,H(6),PD(4,12),QQ(2,4),      BLANK.
3      PRS,FZS,PRT,PZT,EG      BLANK.
COMMON/GEN/NSHELL,IPUNCH,E(7,12),INDEX,MP,NMN,MCDFE,NUMMP,ICCMFR,  GEN,2
1      NUMEL,ND2,MED(16),DISPL,NJELT,IPER,NUMHAT,PSF,PSFJ,XSCL,SPHT,  GEN,3
3VISC,YISCL,DISCL,PSCL,PJCL,NP(4),CON,IM,NAXI,NB,MBAND,LENGTH,MEO,NJMPGEN,4
*      ,MBFLOW,NUMMF2,NUMFNP,LM(12),MF2      GEN,5
*      COMMON/EH/ST(4,8),SQ(2,4),AJ(3,2),DD(2,2),QJ(4),HR(6),HZ(6)  GEN,2
*      ,EJ(2,2)      EM,3
C      LARGE A1(AQ,1),A2(MNP,1),IDEST(1),IDEQ(3,1)      STRFLC
C      DIMENSION SF(8,1),SC(8,1),SH(INH,1),SE(NM,1)      STRFLC
      L=1      STRFLC
      DD 703 I=1,4      STRFLC
      J=NP(I)      STRFLC
      DD 704 K=1,2      STRFLC
      LH(L)=IDEG(K,J)      STRFLC
704 L=L+1      STRFLC
703 LH(I+8)=IDEQ(3,J)      STRFLC
      IJ=12      STRFLC
      IF(MTYPE.GT.NSHELL) IJ=10      STRFLC
      DD 701 I=1,8      STRFLC
      II=LH(I)      STRFLC
      DD 702 J=1,8      STRFLC
      JJ=LH(J)-II+1      STRFLC
702 IF(JJ.GT.0) A1(II,JJ)=A1(II,JJ)+SF(I,J)      STRFLC
      DD 701 J=9,IJ      STRFLC
      JJ=LH(J)-II+1      STRFLC
701 IF(JJ.GT.0) A1(II,JJ)=A1(II,JJ)+SC(I,J-8)      STRFLC
      DD 705 I=9,IJ      STRFLC
      II=LH(I)      STRFLC
      L=1      STRFLC
      DD 706 K=1,4      STRFLC
      K2=L+L      STRFLC
      K1=K2-1      STRFLC
      KK=LH(K1)-II+1      STRFLC
      LL=LH(K2)-II+1      STRFLC
      IF(KK.GT.0) A1(II,KK)=A1(II,KK)+SC(K1,I-8)      STRFLC
      IF(LL.GT.0) A1(II,LL)=A1(II,LL)+SC(K2,I-8)      STRFLC
706 L=L+1      STRFLC
      DD 705 J=9,IJ      STRFLC
      JJ=LH(J)-II+1      STRFLC
705 IF(JJ.GT.0) A1(II,JJ)=A1(II,JJ)-SH(I-8,J-8)*DT-SE(I-8,J-8)      STRFLC
      IJ=4      STRFLC
      IF(MTYPE.EY.NSHELL) IJ=2      STRFLC
      DD 720 I=1,IJ      STRFLC
      II=NP(I)      STRFLC
      LL=IDEST(II)      STRFLC
      DD 708 J=I,IJ      STRFLC
      J1=NP(J)      STRFLC
      KK=IDEST(J1)      STRFLC
      LLF=FINB(LL,KK)      STRFLC
      MBF=IABS(LL-KK)+1      STRFLC
      A2(LLF,MBF)=A2(LLF,MBF)+SH(I,J)      STRFLC
      IF(MNP.GT.NUMFNP) A2(LLF,MBFLOW+MBF)=A2(LLF,MBFLOW+MBF)-SE(II,J)  STRFLC
708 CONTINUE      STRFLC
1000 RETURN      STRFLC
      ENC      STRFLC
SUBROUTINE SOLVES(THETA,DT,TIME,A1,A2,B,BO,PO,H1,IO,MOH,MB,NUMMP,  STRFLC
*NEQ,MEL,NSH,MBAND,MBFLOW,NUMFNP,ICONPR,IOEST,INDEX,IPER,NMN,IDEO,  STRFLC
*PHIC,Q,IP,QA,QAF,TL)      STRFLC

```



```

        L=IDEST(I)                                STRFLC
        K=IDEQ(3,I)                                STRFLC
        TL(K)=0.0                                  STRFLC
241  B(K)=QA(L)                                    STRFLC
        DO 255 I=1,NEQ                               STRFLC
255  B(I)=B(I)+BQ(I)+TL(I)                         STRFLC
        CALL BACKS(NEQ,MBAND,A1,Q,MB)              STRFLC
276  IF(MNN.NE.IPI) RETURN                         STRFLC
        DO 270 I=1,MJMFNP                          STRFLC
        K3=IDEQ(3,I)                               STRFLC
        L=IDEST(I)                                 STRFLC
        Q2(NUMFNP+L)=B(K3)                        STRFLC
270  CONTINUE                                       STRFLC
        DO 280 J=1,MJMFNP                          STRFLC
        IF( I0(J).LE.0 ) QQ(J)=QQ(J)+HTDT2*QQ(NUMFNP+J) STRFLC
280  HI(J)=HI(J)+HTDT*PHIO(J)+OTH*Q2(NUMFNP+J)   STRFLC
275  RETURN                                         STRFLC
2009 FORMAT(I10,5E20,5)                          STRFLC
        END                                         STRFLC
        SUBROUTINE MODIFY(N,A1,NEQ)                STRFLC
        LARGE A1(NEQ,1)                           STRFLC
        A1(N,1)=1.0E+20                            STRFLC
        RETURN                                     STRFLC
        END                                         STRFLC
        SUBROUTINE PRCFIL(A2,MB,NEQ,MBAND)        STRFLC
        LARGE A2(NEQ,1),MB(1)                     STRFLC
C
        MN=NEQ*MBAND                               STRFLC
        DO 300 N=1,NEQ                              STRFLC
        NI=0                                         STRFLC
        NJ=0                                         STRFLC
        L=0                                          STRFLC
        IL=M+NEQ                                     STRFLC
        DO 100 I=IL,MN,NEQ                          STRFLC
        L=L+1                                        STRFLC
        IF(A2(I).NE.0.0) NI=I                       STRFLC
        IF(N-L)100,100,00                           STRFLC
80  IF(A2(I-L).NE.0.0) NJ=I-L                     STRFLC
100  CONTINUE                                       STRFLC
        MB(N)=NI                                     STRFLC
        MB(N+NEQ)=NJ                                STRFLC
300  CONTINUE                                       STRFLC
        RETURN                                     STRFLC
        END                                         STRFLC
        SUBROUTINE TRIA(NEQ,M,A1,MB)              STRFLC
C
        LARGE A1(1),MB(1)                          STRFLC
C
        ME=NEQ-1                                    STRFLC
        MN=M-1                                       STRFLC
        MM=MM*NEQ                                    STRFLC
        MK=NEQ-MM                                    STRFLC
        DO 300 N = 1, NEQ                            STRFLC
        MT=N-MK                                       STRFLC
        IF(MT.GT.0) MM=MM-NEQ                       STRFLC
        MB(N)=0                                       STRFLC
        IF(A1(N).EQ.0.0) GO TO 300                   STRFLC
        L=N                                          STRFLC
        IL=M+NEQ                                     STRFLC
        IH=N+MM                                       STRFLC
        JB = 0                                       STRFLC
        IB = 0                                       STRFLC

```

```

DO 200 I=IL,IM,MEQ                                STRFLC
L=L+1                                              STRFLC
J=L                                               STRFLC
IB=IB+1                                           STRFLC
C=A1(I)/A1(N)                                     STRFLC
IF (C.EQ.0.0) GO TO 200                          STRFLC
DO 180 K=I,IM,NEQ                                 STRFLC
A1(J)=A1(J)-C*A1(K)                              STRFLC
100 J=J+NEQ                                        STRFLC
A1(I)=C                                           STRFLC
JB=IB                                             STRFLC
200 CONTINUE                                       STRFLC
MB(N)=JB                                          STRFLC
300 CONTINUE                                       STRFLC
MB(MEQ)=8                                         STRFLC
RETURN                                             STRFLC
END                                                STRFLC
SUBROUTINE MULTPLY(A2,B,M1,QQ,MB,NEQ,MUMFNP)      STRFLC.
C                                                  STRFLC.
LARGE A2(MUMFNP,1),MB(1),M1(1),QQ(1)           STRFLC.
C DIMENSION B(1)                                STRFLC.
MM=MUMFNP-1                                       STRFLC.
DO 300 N1=1,MUMFNP                                STRFLC.
BB=A2(N1)*M1(N1)                                  STRFLC.
L=N1                                               STRFLC.
IL=N1+MUMFNP                                       STRFLC.
IH=MB(N1)                                          STRFLC.
IF (IH)120,120,50                                  STRFLC.
50 DO 180 I=IL,IH,MUMFNP                          STRFLC.
L=L+1                                              STRFLC.
BB=BB+A2(I)*M1(L)                                 STRFLC.
100 CONTINUE                                       STRFLC.
120 L=N1                                           STRFLC.
IL=N1+MM                                           STRFLC.
IH=MB(N1+MUMFNP)                                  STRFLC.
IF (IH)250,250,150                                STRFLC.
150 DO 200 I=IL,IH,MM                             STRFLC.
L=L-1                                              STRFLC.
BB=BB+A2(I)*M1(L)                                 STRFLC.
200 CONTINUE                                       STRFLC.
250 B(N1)=BB+B(N1)                                 STRFLC.
QQ(N1)=B(N1)                                       STRFLC.
300 CONTINUE                                       STRFLC.
RETURN                                             STRFLC.
END                                                STRFLC.
SUBROUTINE BACKS(IN,MM,A1,B,MB)                   STRFLC.
C                                                  STRFLC.
LARGE A1(1),B(1),MB(1)                            STRFLC.
C MMP=MM-1                                        STRFLC.
M=0                                               STRFLC.
270 N=N+1                                          STRFLC.
C=B(N)                                            STRFLC.
IF (A1(N).NE.0.0) B(N)=B(N)/A1(N)                STRFLC.
IF (N.EQ.MM) GO TO 300                           STRFLC.
IL=N+1                                           STRFLC.
IH=N+MB(N)                                        STRFLC.
M=M+1                                             STRFLC.
DO 285 I=IL,IH                                   STRFLC.
M=M+MM                                           STRFLC.
285 B(I)=B(I)-A1(N)*C                             STRFLC.

```

```

      GO TO 270                                STPFLC
C
300 IL=N                                      STPFLC
    N=N-1                                      STPFLC
    IF(N.EQ.0) RETURN                         STPFLC
    IH = N+MB(N)                              STPFLC
    N=N                                        STPFLC
    C=B(N)                                     STPFLC
    DO 400 I=IL,IH                            STPFLC
    M=M+NH                                     STPFLC
400 C=C-A1(N)*B(I)                           STPFLC
    B(N)=C                                     STPFLC
    GO TO 300                                 STPFLC
C
    ENB                                        STPFLC
SUBROUTINE STRFLC(B,BO,PO,TIME,IP,FLAG,NCC,JT) STPFLC
C
    LARGE A(125000),ID(900)                  STPFLC
    LARGE IX(301,5),RESID(301,4),R(300),Z(300),UR(300),UZ(300)
    * ,CODE(300),IDEST(300),R,KM(50),R,KS(50),MT(50),IGUT(301),Q(300)
    *QP(50),N(50),VEL(50),FR(50),RE(50),QN(900),JISPI(300,2),TEMP(300),
    * PHID(300),IB(300),IDEQ(3,300),KODE(3,300),IEL(50,2),IMP(50,4)
    * ,TLOAD(900),SIGN(50),SIGT(50),DBO(600)
    COMMON/BLANK/S(8,8),P(10),RSTRS(4),VOL,RRR(5),ZZZ(5),LBA0,RADN,
1    RRR(4),ZZ(4),IFAT(50),ACELX,ACELY,MRSE,RO(12),
2    MTYPE,XI,XCEN,YCEN,XTR(10),FAC,H(6),PO(4,12),QQ(2,4),
3    PRS,PZS,PRT,PZT,EG
    COMMON/GEN/NSHELL,IPUNCH,E(7,12),INDEX,MP,NNM,NODEE,MUMMP,ICOMPR,
1    NUMEL,ND2,HED(16),DISPL,NJELT,IPER,MUMHAT,PSF,PSFJ,KSCL,SPW,GEN,3
3    VISC,YSCL,DSCL,FSCL,PJCL,AP(4),COM,IM,MAXI,NB,MEAN0,LNGTH,MEQ,KJMP
    * ,MFL0W,NUMAP2,MUMFNP,LN(12),NFZ
    * ,EJ(2,2)
    COMMON/CCFOOL/XMIN,XMAX,YMIN,YMAX,CCXMIN,CCXMAX,CCYMIN,CCYMAX
    COMMON/EN/ST(4,8),SO(2,4),AJ(8,2),DD(2,2),QU(4),MR(6),HZ(6)
    * ,EJ(2,2)
    LARGE B(1),B0(1),P0(1)
    DIMENSION SIG(7),TP(6),QR(4)
    LOGICAL FLAG
C
C      COMPUTE ELEMENT STRESSES
1
MPRINT=0
REWIND 9
QPODR=0.0
MJ= 0
PI=4.0*ATAN(1.0)
RADN=180.0/PI
RAD2=0.5*RADN
P12=2.0*ATAN(1.0)
IF(INDEX.NE.0) PRINT 2001,TIME,MP,IPER
IF (IPER .EQ. 1) XMI =-1.0E15
C
IF (INDEX .LT. 2) GO TO 10
IF (XMIN .LT. XMI) GO TO 7
XCON = (XMAX-XMIN) * 0.125 / (CCXMAX-CCXMIN)
YCON = (YMAX-YMIN) * 0.125 / (CCYMAX-CCYMIN)
XPC = 0.05
YPC = 8.85
XMI = XMA
YMI = YMA
YMA = YMAX
OEL = XPC * (XMA - XMIN)

```

```

XMIN = XMIN - DEL                                STRFLC
XMAX = XMAX + DEL                                STRFLC
DEL = YPC * (YMA) - YMIN                         STRFLC
YMIN = YMIN - DEL                                STRFLC
YMAX = YMAX + DEL                                STRFLC
DEL = XPC * (CCXMAX - CCXMIN)                    STRFLC
CCXMIN = CCXMIN - DEL                             STRFLC
CCXMAX = CCXMAX + DEL                             STRFLC
DEL = YPC * (CCYMAX - CCYMIN)                    STRFLC
CCYMIN = CCYMIN - DEL                             STRFLC
CCYMAX = CCYMAX + DEL                             STRFLC
7 WRITE (98, 5) HED, MP, IPER                     STRFLC
5 FORMAT (8A9/8A9/17H ITERATION NUMBERI4,20H PERTUREATION NUMBERI4) STRFLC
CALL CCLTF (-1.8, 0.5, 1, 2)                       STRFLC
CALL CCL3L (1,1)                                   STRFLC
CALL CCPLCT (XMI, YMI, 1, 6HNOJOIN, 8, 1)         STRFLC
CALL CCPLCT (XMIN, YMIN, 1, 6HNOJOIN, 1, 1)       STRFLC
CALL CCPLCT (XMA, YMA, 1, 6HNOJOIN, 8, 1)         STRFLC
CALL CCPLCT (XMAX, YMAX, 1, 6HNOJOIN, 1, 1)       STRFLC
CALL CCPLCT (XMI, YMA, 1, 6HNOJOIN, 9, 1)         STRFLC
CALL CCPLCT (XMIN, YMA, 1, 6HNOJOIN, 1, 1)       STRFLC
CALL CCPLCT (XMA, YMA, 1, 6HNOJOIN, 9, 1)         STRFLC
CALL CCPLCT (XMAX, YMA, 1, 6HNOJOIN, 1, 1)       STRFLC
C
10 DO 300 N=1, NUMEL                               STRFLC
IF (INDEX ,EO, 0) GO TO 15                          STRFLC
MPRINT = MPRINT - 1                                 STRFLC
IF (MPRINT .GT. 0) GO TO 15                          STRFLC
MPRINT = 50                                         STRFLC
C
15 IX(N,5)=IABS(IX(N,5))                             STRFLC
MTYPE = IX(N,5)                                    STRFLC
C
IF (INDEX, NE, 2) GO TO 110                          STRFLC
DO 16 I=1,4                                         STRFLC
J=IX(N,I)                                           STRFLC
K1=IDEQ(1,J)                                       STRFLC
K2=IDEQ(2,J)                                       STRFLC
XTR(1)=R(J)+8*(K1)*DISPL                           STRFLC
II=I+5                                             STRFLC
16 XTR(II)=Z(J)+8*(K2)*DISPL                         STRFLC
XTR(5)=XTR(1)                                       STRFLC
XTR(10)=XTR(6)                                       STRFLC
COR = 3                                             STRFLC
XCEN = XTR(1) + XTR(2) + XTR(3)                     STRFLC
YCEN = XTR(8) + XTR(6) + XTR(7)                     STRFLC
IF (N3 .EQ. N4) GO TO 20                             STRFLC
COR = 4                                             STRFLC
XCEN = XCEN + XTR(4)                                 STRFLC
YCEN = YCEN + XTR(9)                                 STRFLC
20 XCEN = XCEN / COR                                 STRFLC
YCEN = YCEN / COR                                 STRFLC
IF (MTYPE .GT. MSHELL) GO TO 290                     STRFLC
C
PLOT GRID INCLUDING DISPLACEMENTS                   STRFLC
CALL CCPLCT (XTR(1), XTR(6), 5, 4HJOIN)             STRFLC
KOR = COR                                           STRFLC
DO 50 NC = 1, KOR                                   STRFLC

```



```

      N1=IX(IN,NC)                                STRFLC
      NI=IDEO(1,N1)                                STRFLC
      IF (B(N1) .EQ. 0.0) GO TO 30                  STRFLC
      XC = XCON                                     STRFLC
      IF (XTR(NC) .GT. XCEN) XC = -XCON            STRFLC
      YC = YCON                                     STRFLC
      IF (XTR(NC+5) .GT. YCEN) YC = -YCON         STRFLC
      XC = XTR(NC) + XC                             STRFLC
      YC = XTR(NC+5) + YC                           STRFLC
      NS=0                                          STRFLC
      IF(B(N1).GT.0.0) NS=0                          STRFLC
      CALL CCPL0T(XC, YC, 1, 6HNOJCIN, NS, 1)      STRFLC
30 CONTINUE                                       STRFLC

C
118 IF(MTYPE.GT.NSHELL) GO TO 290                STRFLC
      READ (9) ST,SO,MP                             STRFLC
      DO 31 I=1,4                                    STRFLC
      SIG(I)=RESID(N,I)                              STRFLC
31 QU(I)=0.0                                        STRFLC
      POAVE=0.0                                      STRFLC
      PAVE=0.0                                       STRFLC
      DO 50 I=1,4                                    STRFLC
      MI=MP(I)                                        STRFLC
      L=IDEO(1,MI)-1                                STRFLC
      M=2*I-1                                        STRFLC
      MM=M+1                                         STRFLC
      DO 40 K=M,MM                                   STRFLC
      L=L+1                                          STRFLC
      DO 40 J=1,4                                    STRFLC
40 SIG(J)=SIG(J)+ST(J,K)*B(L)                     STRFLC
      L=IDEO(3,MI)                                  STRFLC
      POAVE=POAVE+TEMP(NI)/4.0                      STRFLC
      PAVE=PAVE+B(L)/4.0                            STRFLC
      DO 45 K=1,2                                    STRFLC
45 QU(K)=QU(K)+SQ(K,I)*B(L)                       STRFLC
50 CONTINUE                                       STRFLC
      PDIFF=E(4,MTYPE)*(PAVE-POAVE)                STRFLC
      DO 55 I=1,3                                    STRFLC
55 SIG(I)=SIG(I)+PDIFF                             STRFLC
      GEFF=SPWT*(1,MTYPE)/VISC                     STRFLC
      QU(1)=-QU(1)                                  STRFLC
      QU(2)=-QU(2)+GEFF                             STRFLC
      CC=(SIG(1)+SIG(2))/2.0                         STRFLC
      BB=(SIG(1)-SIG(2))/2.0                         STRFLC
      CR=SQRT(BB**2+SIG(4)**2)                       STRFLC
      SIG(5)=CC+CR                                   STRFLC
      SIG(6)=CC-CR                                   STRFLC
      IF (SIG(4).GT.10E-15.OR.BB.GT.10E-15) GO TO 80 STRFLC
      EPS=8.78539816                                 STRFLC
      SIG(7)=100.0                                   STRFLC
      GO TO 90                                       STRFLC
80 SIG(7)=RAD2*ATAN2(SIG(4),BB)                    STRFLC
      EPS=ATAN2(SIG(4),BB)/2.0                      STRFLC
90 AA=ABS(QU(1))                                    STRFLC
      IF (AA.GT.10E-30) GO TO 100                   STRFLC
      ANG=P12                                        STRFLC
      GO TO 200                                       STRFLC
100 BB=ABS(QU(2)/QU(1))                             STRFLC
      ANG=SQRT(BB)                                   STRFLC
      ANG=ATAN(ANG)                                  STRFLC
200 QU(3)=QU(1)*COS(ANG)**2+QU(2)*SIN(ANG)**2     STRFLC

```

```

QU(4)=ANG*PADN STRFLC
IF(INDEX.EQ.8) GO TO 271 STRFLC
PRINT 270,N,(SIG(I),I=1,7),(QU(J),J=1,4) STRFLC
270 FORMAT (I8,12E10.2) STRFLC
2001 FCRMAT(1H1/* STRESSES AND FLOWS AT TIME *F10.3//* STRFLC
1 ITERATION NUMBER *I4,* PERTURBATION NUMBER *I4,/* STRFLC
2* ELEMENT*,4X,*SIGR*,6X,*SIGZ*,5X,*SIGT*,6X,*SIGRZ*,5X,*SIGMAX*, STRFLC
35X,*SIGMIN*,4X,*ANGLE*,5X,*FLWR*,6X,*FLWZ*,5X,*FLWMAX*,4X,*ANGLE STRFLC
4*/IF JOINT*,4X,*SIGN*,6X,*SIGS*,5X,*NDISP*,6X,*TDISP*,5X,*NSTIF*, STRFLC
55X,*TSTIF*,4X,*STRNGTH*,5X,*MIOTH*,5X,*FRFLO*,3X,* RE*) STRFLC
C STRFLC
271 CONTINUE STRFLC
C PLOT STRESSES STRFLC
IF (INDEX .LT. 2) GO TO 220 STRFLC
CC = COS(EPS) STRFLC
SS = SIN(EPS) STRFLC
XL = SIG(5) * CC * PSF STRFLC
XTR(1) = XCEM - XL STRFLC
XTR(2) = XCEM + XL STRFLC
XL = SIG(5) * SS * PSF STRFLC
XTR(5) = YCEM - XL STRFLC
XTR(6) = YCEM + XL STRFLC
CALL CCPLCT (XTR(1), XTR(5), 2, 4HJOIN) STRFLC
IF(SIG(5).GE.0.0) GO TO 210 STRFLC
XTR(1) = XTR(1) - 0.02 * SS STRFLC
XTR(2) = XTR(2) - 0.02 * SS STRFLC
XTR(5) = XTR(5) + 0.02 * CC STRFLC
XTR(6) = XTR(6) + 0.02 * CC STRFLC
CALL CCPLCT (XTR(1), XTR(5), 2, 4HJOIN) STRFLC
210 XL = SIG(6) * SS * PSF STRFLC
XTR(1) = XCEM + XL STRFLC
XTR(2) = XCEM - XL STRFLC
XL = SIG(6) * CC * PSF STRFLC
XTR(5) = YCEM - XL STRFLC
XTR(6) = YCEM + XL STRFLC
CALL CCPLCT (XTR(1), XTR(5), 2, 4HJOIN) STRFLC
IF(SIG(6).GE.0.0) GO TO 220 STRFLC
XTR(1) = XTR(1) - 0.02 * SS STRFLC
XTR(2) = XTR(2) - 0.02 * SS STRFLC
XTR(5) = XTR(5) - 0.02 * CC STRFLC
XTR(6) = XTR(6) - 0.02 * CC STRFLC
CALL CCPLCT (XTR(1), XTR(5), 2, 4HJOIN) STRFLC
C STRFLC
220 GO TO 300 STRFLC
290 CALL JTSTR(B,80,PO,M.,N,FLAG,IP) STRFLC
300 CONTINUE STRFLC
C STRFLC
IF(FLAG.OR.MN.EQ.IP) GO TO 302 STRFLC
PRINT 304, IPER STRFLC
304 FORMAT (52H0PPROBLEM CONVERGED IN THIS ITERATION AT PERTURBATION(I4) STRFLC
302 IF (INDEX .NE. 2) GO TO 330 STRFLC
WRITE (98,305) XSCI, YSCI, OSCL, PSCI, #JCL STRFLC
305 FORMAT (15H 1 IN CN X-AXIS/4H =E12.4,3H FT/15H 1 IN ON Y-AXIS/ STRFLC
14H =E12.4,3H FT/18H 1 IN DISPLACEMENT/4H =E12.4,3H FT/5H 1 IN/ STRFLC
24H =E12.4,11H PSF STRESS/5H 1 IN/4H =E12.4,14H PSF JT STRESS) STRFLC
DO 320 I=1,NUMHAT STRFLC
IF(I.GT.NSHELL) WRITE(98,315) I,(E(I,J),J=1,5) STRFLC

```

```

IF(I.LE.NSHELL) WRITE(90,308) I,RO(I), (E(K,I),K=1,6) STRFLC
308 FORMAT(/9M MATERIALI3/20H MASS DENSITY =F0.3/16H PERMEABILITY STRFLC
.Y =E14.3/21H ELASTIC MODULUS =E14.3/21H PCISSGN RATIO =F9,STRFLC
.3/23HBIOTS CONSTANT ALPHA =F10.3/19HBIOTS CONSTANT M =E14.3/22H STRFLC
.THERMAL EXPAN.COEF. =E14.3) STRFLC
STRFLC
315 FORMAT(/9M MATERIALI3/20H KN =E12.3/20H KS STRFLC
1 =E12.3/20H C =E12.3/20H PHI =STRFLC
2E12.3/20H MAX CLOSURE =E12.3) STRFLC
320 CONTINUE STRFLC
STRFLC
XP = CCXMAX + 0.5 STRFLC
CALL CCLTR (XP, 10.5, 0, 2) STRFLC
CALL CCNEXT STRFLC
330 RETURN STRFLC
C STRFLC
END STRFLC
SUBROUTINE JTSTR(B,BO,PO,H,N,FLAG,IP) STRFLC
C STRFLC
LARGE A(125000),ID(900) STRFLC
LARGE IX(301,5),RESID(301,4),R(300),Z(300),UR(300),UZ(300) STRFLC
* ,CODE(300),IDEST(300),R,KN(50),R,KS(50),MT(50),IGUT(301),Q(300), LARGE
* QP(50),M(50),VEL(50),FR(50),RE(50),QN(900),DISPI(300,2),FEMP(300),LARGE
* PHIO(300),IB(300),IDEG(13,300),KODE(3,300),IEL(50,2),IMP(50,4) STRFLC
* ,TLOAD(900),SIGN(50),SIGT(50),D90(600) STRFLC
COMMON/BLANK/S(8,8),P(10),RSTRS(4),VGL,RRR(5),ZZZ(5),LBD,PADN, BLANK
1 RR(4),ZZ(4),IPAT(50),ACELX,ACELY,NRES,RC(12), BLANK
2 MTYPE,XI,XCE,YCEN,XTR(10),FAC,M(6),PD(4,12),QQ(2,4), BLANK
3 PRS,FZS,PRT,FZT,EG BLANK
COMMON/GEN/NSHELL,IPURC,E(7,12),INDEX,MP,MNH,NCORE,NUMNP,ICCMFR, GEN.2
1 NUMEL,ND2,ME0(16),DISPL,NJELT,IPER,NUMMA1,FSF,PSFJ,XSCL,SPWT,GEN.3
3VISC,YSCL,DSCL,FSCL,PJCL,NF(4),CDMLN,NAXI,NB,MBAND,LENGTH,ME0,NJMP,GEN.4
* ,MBFLOW,NUMNF2,NMFAP,LM(12),NF2 GEN.5
COMMON/CCFOCL/XPIN,XMAX,YMIN,YMAX,CCXMIN,CCXMAX,CCYMIN,CCYMAX CCP00L
COMMON/EN/ST(4,8),SQ(2,4),AJ(8,2),DD(2,2),QU(4),HR(16),HZ(6) EH.2
* ,EJ(2,2) EH.3
COMMON/CCFACT/FACTOR STRFLC
C STRFLC
LARGE B(1),BD(1),PO(1) STRFLC
DIMENSION PPP(8),V(4),U(4) STRFLC
LOGICAL FLAG STRFLC
REAL L STRFLC
C *****ESTABLISH DISPLACEMENTS ALONG AND NORMAL TO JOINT STRFLC
C STRFLC
M = M + 1 STRFLC
CAYN = KN(M) STRFLC
CAYS = KS(M) STRFLC
EM1 = E(1,MTYPE) STRFLC
EM2 = E(2,MTYPE) STRFLC
EM3 = E(3,MTYPE) STRFLC
EM4 = E(4,MTYPE) STRFLC
FT=0.0 STRFLC
STREN=0.0 STRFLC
POAVE=0.0 STRFLC
STRFLC
I=IX(N,1) STRFLC
J= IX(N,2) STRFLC
DR=R(J)-R(I) STRFLC
DZ=Z(J)-Z(I) STRFLC
RR1 = 0.5 * (R(J) + R(I)) STRFLC
ZZ1 = 0.5 * (Z(J) + Z(I)) STRFLC
STRFLC

```



```

      IF (CAYN .GT. EM1) CAYN = EM1
      GO TO 230
STRFLC
STRFLC
STRFLC
C      FMRES .LE. 0 AND WT .NE. 0 AND EPSM .LE. 0
205 CAYN = (FN - FMRES) / ETHICK
      IF (CAYN .LT. EM1) CAYN = EM1
      GO TO 230
STRFLC
STRFLC
STRFLC
C      ETHICK = 0, FMRES .LE. 0 .OR. FMRES .GT. 0 AND EPSM .LT. 0
215 CAYN = CAYN * 1.0E10
      CAYS = CAYS * 1.0E10
      GO TO 260
STRFLC
STRFLC
STRFLC
C      FMRES .GT. 0
220 IF (EPSM .LT. 0.0 .AND. ETHICK .EQ. 0.0) GO TO 215
      IF (EPSM .EQ. 0.0) GO TO 230
      CAYN = -FMRES / EPSM
      IF (EPSM .LT. 0.0) CAYN = CAYN + EM1
STRFLC
STRFLC
STRFLC
C      CALCULATION OF KS
230 FT = CAYS * EPST + FTRES
      AFN = ABS(FN)
      EPSNLM = ABS(FMRES) / EM1
      IF (EPSM .GT. EPSALM .OR. FN .GT. 0.0) AFN = 0.0
      STREM = EM3 + AFN * TAN (EM4/57.29577951)
STRFLC
STRFLC
STRFLC
      IF (EPST .EQ. 0.0 ) GO TO 260
      IF (EM3 .EQ. 0.0 .AND. EM4 .EQ. 0.0) GO TO 260
      IF (EPST .LT. 0.0) STREM = - STREM
      CAYS = (-FTRES + STREM) / EPST
      IF (CAYS .EQ. 0.0) CAYS = 9.0E-9
STRFLC
STRFLC
STRFLC
      IF (CAYS .GT. EM2) CAYS = EM2
      ABS(FTRES) .LE. ABS(STREM)
      IF (ABS(FTRES) .GT. ABS(STREM)) GO TO 235
      GO TO 260
STRFLC
STRFLC
STRFLC
C      ABS(FTRES) .GT. ABS(STREM)
235 IF (FTRES * EPST .GE. 0.0) GO TO 260
STRFLC
STRFLC
STRFLC
C      FTRES AND EPST HAVE OPPOSITE SIGNS
      EPSLIM = 2.0 * STREM / EM2
      IF (ABS(EPST) .GT. EPSLIM) GO TO 260
STRFLC
STRFLC
STRFLC
C      ABS(EPST) .LE. EPSLIM
      CAYS = 1-FTRES - STREM / EPST + EM2
STRFLC
STRFLC
STRFLC
260 IF (ABS(CAYN-KN(M)) .GT. CONLIM .OR. ABS(CAYS-KS(M)) .GT. CONLIM)
1 FLAG = .TRUE.
      KN(M)=CAYN
      KS(M) = CAYS
STRFLC
STRFLC
STRFLC
C      ***** CALCULATE FLOW IN FRACTURES *****
C
C      IF (INDEXT.EQ.0) GO TO 500
115 NB=NT(M)
      IF (EPSM.GE.NB) GO TO 150
      PRINT 140,M
140 FORMAT('DISPLACEMENT GREATER THAN ALLOWED IN JOINT ELEMENT NO.*I5)
STRFLC
STRFLC
STRFLC
150 W(HI)=ABS(ABS(NB)+EPSM)
      CON=1.0/(12.0*VISC)
STRFLC
STRFLC
STRFLC

```

