

"TMRBAR" POWER BALANCE CODE FOR TANDEM MIRROR REACTORS

CONF-841010--12

General

DE85 003333

- Coupled, multi-region, zero dimensional power balance code.
- Configured for (a) MARS (quadrupole) mode and (b) TARA/MINIMARS (octupole-Axisymmetric) mode.
- Outputs include plasma parameters (densities temperatures, potentials, absorbed powers, etc.) and system engineering power balance parameters (recirculating powers, thermal powers, etc.)

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Central Cell Physics

- Fuel ion particle/energy balance.
- Electron energy balance.
- Alpha particle balance.
- Global charge balance.
- Hot alpha prompt losses:
 - (a) Non-adiabaticity
 - (b) FLR losses to halo.
- Pressure balance.

*Research sponsored by the Office of Fusion Energy, U.S. Department of Energy, under contract DE-AC05-84OR21400 with Martin Marietta Energy Systems, Incorporated.

MASTER

MINIMARS SUMMARY DATA FOR FIXED NET ELECTRIC POWER

FUSION POWER, Q, WALL LOADING

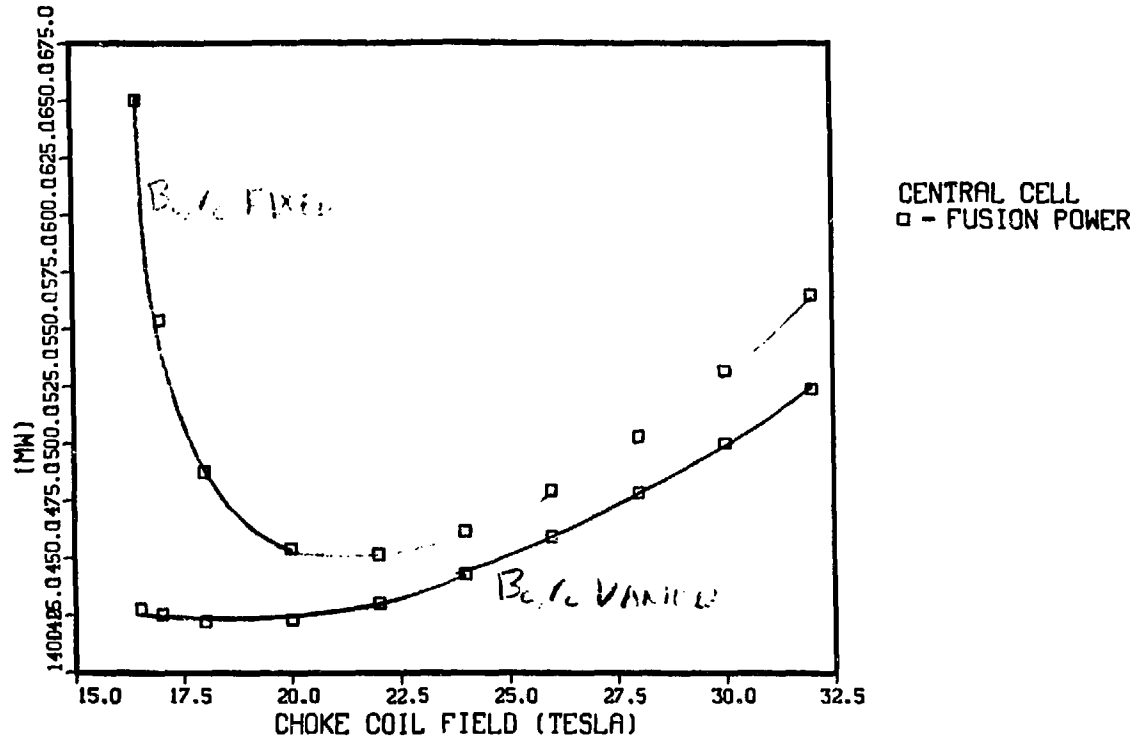
| CASE | PNETEL (MW) | PFUS (MW) | PFUS/VCC (MW/M3) | QPHYS | Q | QENGR | GAMMA (MW/M2) |
|-------|----------------|--------------|---------------------|---------|--------|-------|------------------|
| OOP1 | 688.888 | 1929.417 | 13.631 | 29.263 | 8.239 | 2.281 | 2.388 |
| OOP2 | 688.888 | 1658.268 | 14.538 | 37.634 | 12.351 | 3.838 | 2.461 |
| OOP3 | 688.888 | 1554.844 | 15.629 | 42.146 | 15.446 | 3.545 | 2.647 |
| OOP4 | 688.888 | 1487.471 | 17.611 | 45.954 | 18.778 | 4.851 | 2.982 |
| OOP5 | 688.888 | 1454.812 | 20.141 | 58.586 | 21.698 | 4.378 | 3.411 |
| OOP6 | 688.888 | 1451.588 | 21.584 | 55.659 | 23.537 | 4.416 | 3.655 |
| OOP7 | 688.888 | 1461.296 | 22.597 | 68.978 | 25.864 | 4.327 | 3.827 |
| OOP8 | 688.888 | 1479.825 | 23.388 | 66.364 | 26.425 | 4.159 | 3.961 |
| OOP9 | 688.888 | 1582.879 | 24.831 | 71.764 | 27.688 | 3.976 | 4.878 |
| OOP10 | 688.888 | 1531.856 | 24.557 | 77.173 | 28.862 | 3.778 | 4.159 |
| OOP11 | 688.888 | 1565.318 | 24.982 | 82.611 | 29.993 | 3.564 | 4.231 |
| OOP12 | 688.888 | 1438.765 | 11.855 | 54.371 | 23.884 | 4.832 | 2.218 |
| OOP13 | 688.888 | 1427.685 | 12.442 | 55.937 | 23.491 | 4.678 | 2.288 |
| OOP14 | 688.888 | 1425.383 | 13.848 | 57.544 | 23.983 | 4.717 | 2.357 |
| OOP15 | 688.888 | 1422.426 | 14.274 | 68.987 | 24.747 | 4.774 | 2.494 |
| OOP16 | 688.888 | 1423.825 | 16.893 | 68.266 | 26.512 | 4.889 | 2.759 |
| OOP17 | 688.888 | 1438.385 | 19.698 | 76.579 | 28.386 | 4.761 | 3.818 |
| OOP18 | 688.888 | 1442.671 | 22.688 | 85.946 | 38.368 | 4.654 | 3.245 |
| OOP19 | 688.888 | 1458.961 | 25.821 | 96.481 | 32.457 | 4.512 | 3.462 |
| OOP20 | 688.888 | 1478.317 | 29.866 | 188.267 | 34.648 | 4.352 | 3.659 |
| OOP21 | 688.888 | 1588.116 | 32.368 | 121.369 | 36.929 | 4.185 | 3.835 |
| OOP22 | 688.888 | 1523.894 | 35.682 | 135.861 | 39.296 | 4.818 | 3.998 |

B₀ r_c VARIED

| CASE | CLENGTH (M) | ELACELL (M) | CRADIUS (CM) | RCHOKE (CM) | BBAR (TESLA) | BVACB/C (TESLA) | FNC E14CM-3 |
|-------|----------------|----------------|-----------------|----------------|-----------------|--------------------|----------------|
| OOP1 | 148.947 | 18.824 | 55.888 | 23.239 | 16.888 | 3.388 | 2.855 |
| OOP2 | 119.516 | 18.828 | 55.888 | 22.834 | 16.588 | 3.388 | 2.126 |
| OOP3 | 184.632 | 18.841 | 55.888 | 22.448 | 17.888 | 3.388 | 2.212 |
| OOP4 | 88.877 | 18.845 | 55.888 | 21.728 | 18.888 | 3.388 | 2.364 |
| OOP5 | 75.963 | 9.962 | 55.888 | 28.467 | 28.888 | 3.388 | 2.555 |
| OOP6 | 78.765 | 9.895 | 55.888 | 19.395 | 22.888 | 3.388 | 2.663 |
| OOP7 | 68.849 | 9.718 | 55.888 | 18.469 | 24.888 | 3.388 | 2.738 |
| OOP8 | 66.545 | 9.597 | 55.888 | 17.668 | 26.888 | 3.388 | 2.797 |
| OOP9 | 65.889 | 9.495 | 55.888 | 16.945 | 28.888 | 3.388 | 2.845 |
| OOP10 | 65.648 | 9.495 | 55.888 | 16.387 | 38.888 | 3.388 | 2.884 |
| OOP11 | 65.933 | 9.323 | 55.888 | 15.734 | 32.888 | 3.388 | 2.916 |
| OOP12 | 97.681 | 9.873 | 62.737 | 23.237 | 16.888 | 2.536 | 2.156 |
| OOP13 | 95.858 | 9.893 | 61.728 | 22.634 | 16.588 | 2.567 | 2.288 |
| OOP14 | 94.281 | 9.795 | 68.748 | 22.868 | 17.588 | 2.597 | 2.268 |
| OOP15 | 91.598 | 9.721 | 58.858 | 28.982 | 18.888 | 2.657 | 2.363 |
| OOP16 | 87.714 | 9.588 | 55.298 | 19.872 | 28.888 | 2.773 | 2.567 |
| OOP17 | 85.487 | 9.447 | 52.821 | 17.432 | 22.888 | 2.884 | 2.767 |
| OOP18 | 84.288 | 9.322 | 49.886 | 16.886 | 24.888 | 2.998 | 2.964 |
| OOP19 | 84.897 | 9.282 | 46.246 | 14.759 | 26.888 | 3.892 | 3.155 |
| OOP20 | 84.672 | 9.888 | 43.727 | 13.664 | 28.888 | 3.189 | 3.348 |
| OOP21 | 85.873 | 8.978 | 41.448 | 12.781 | 38.888 | 3.291 | 3.515 |
| OOP22 | 87.688 | 8.872 | 39.392 | 11.851 | 32.888 | 3.58 | 3.688 |

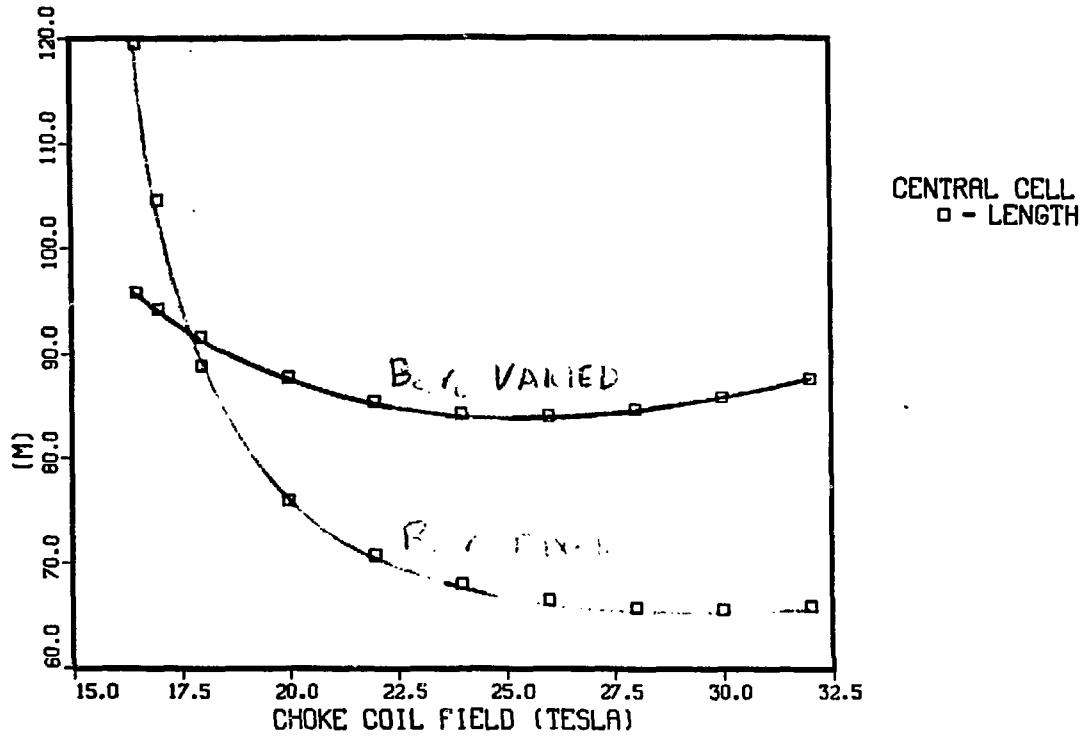
B₀ r_c VARIED

MINIMARS



YMIN- 1422. YMAX- 1650. NET ELECTRIC POWER - 600.0 MW

MINIMARS

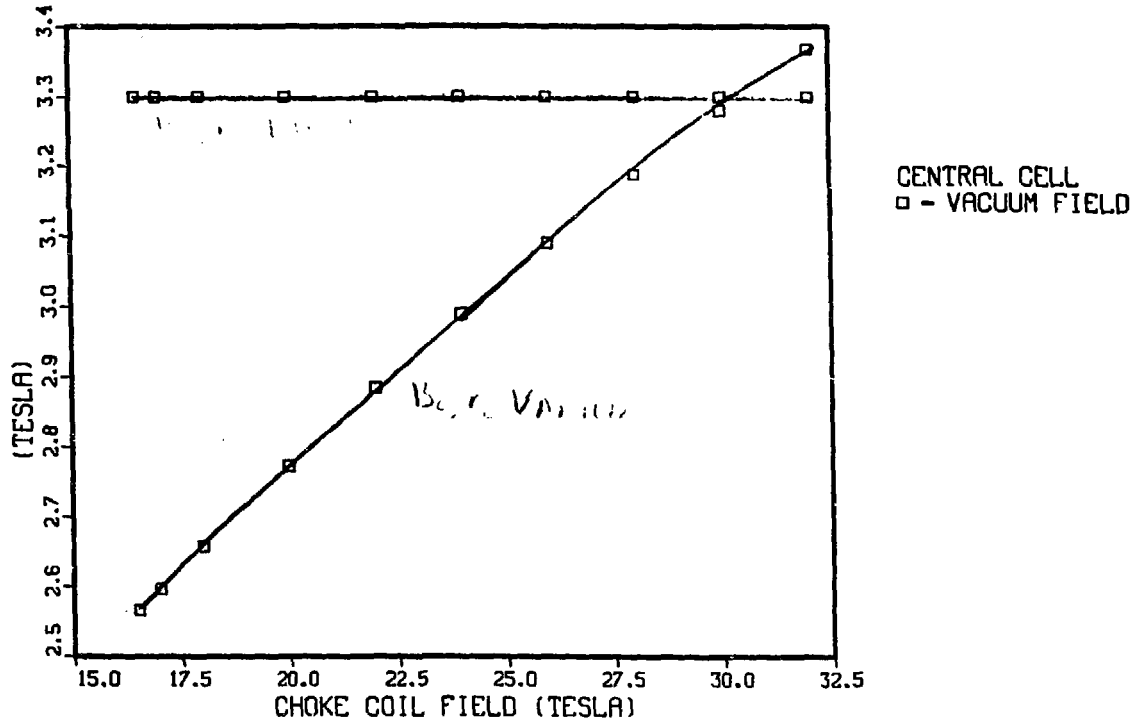


YMIN- 65.64

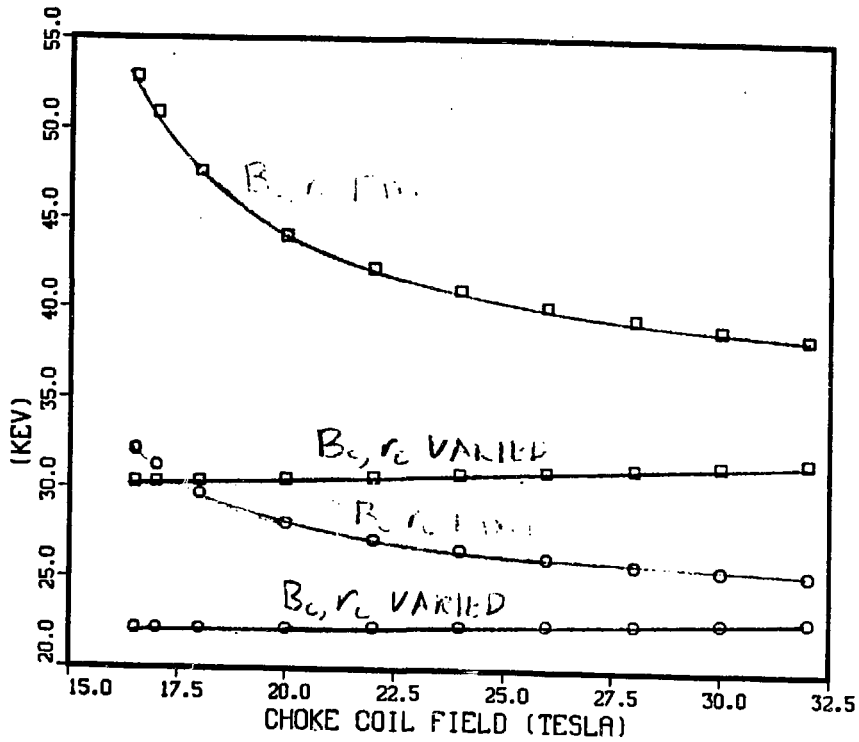
YMAX- 119.5

NET ELECTRIC POWER - 600.0 MW

MINIMARS



MINIMARS

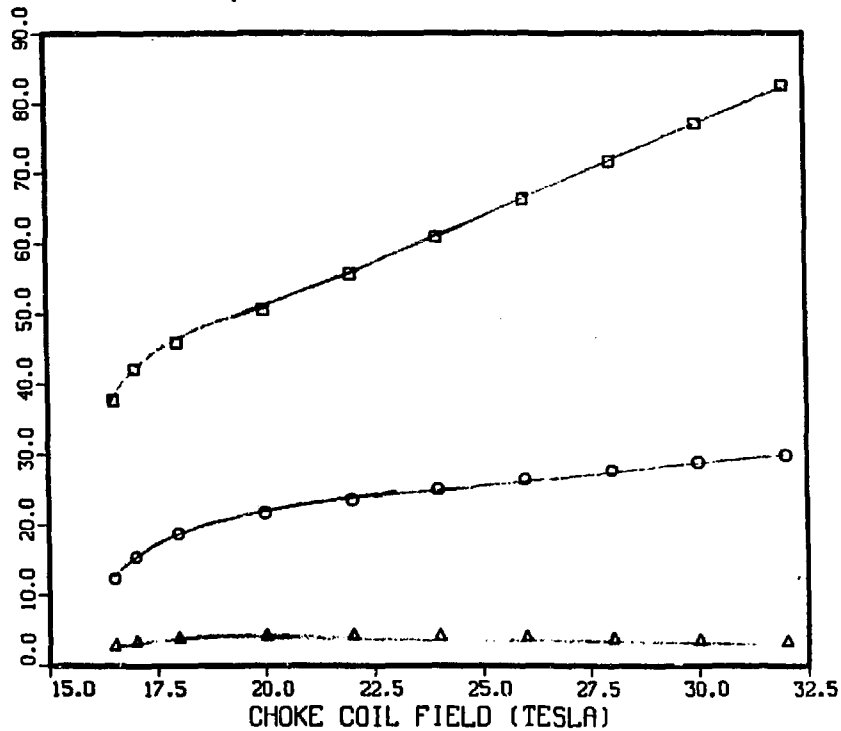


YMIN- 22.19

YMAX- 52.87

NET ELECTRIC POWER - 600.0 MW

MINIMARS



- - PHYSICS
- - FUSION
- △ - ENGINEERING

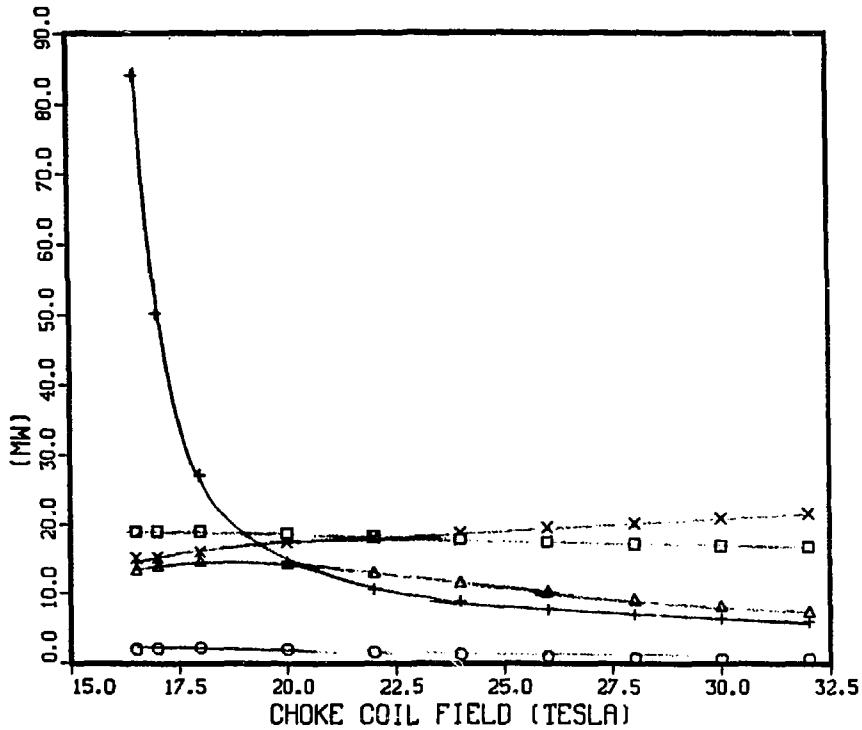
YMIN- 3.038

YMAX- 82.61

NET ELECTRIC POWER - 600.0 MW

MINIMARS

1.0 FIELD

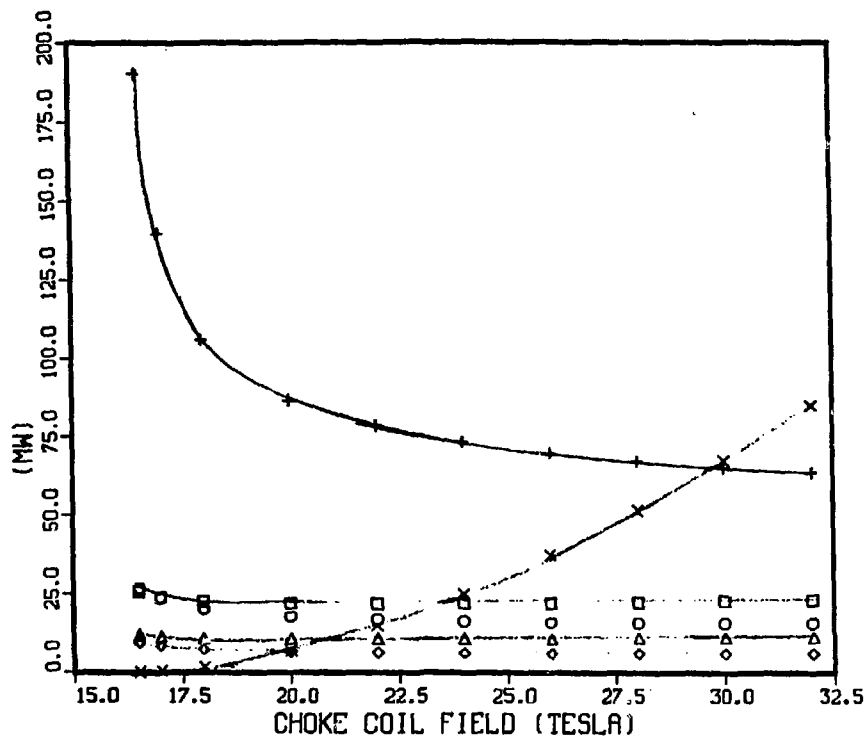


YMIN- 0.617

YMAX- 84.06

NET ELECTRIC POWER - 600.0 MW

MINIMARS



- POWER
- ⊕ - AUXILIARY PUMPS
 - - CRYOGEN SYSTEM
 - ✕ - FUELING SYSTEM
 - † - HEATING SYSTEMS
 - * - MAGNET SUPPLIES
 - ◇ - PLANT FACILITY

$$P_{AUX} = 1.04 + 0.12 \times P_{NET} \text{ (MW)}$$

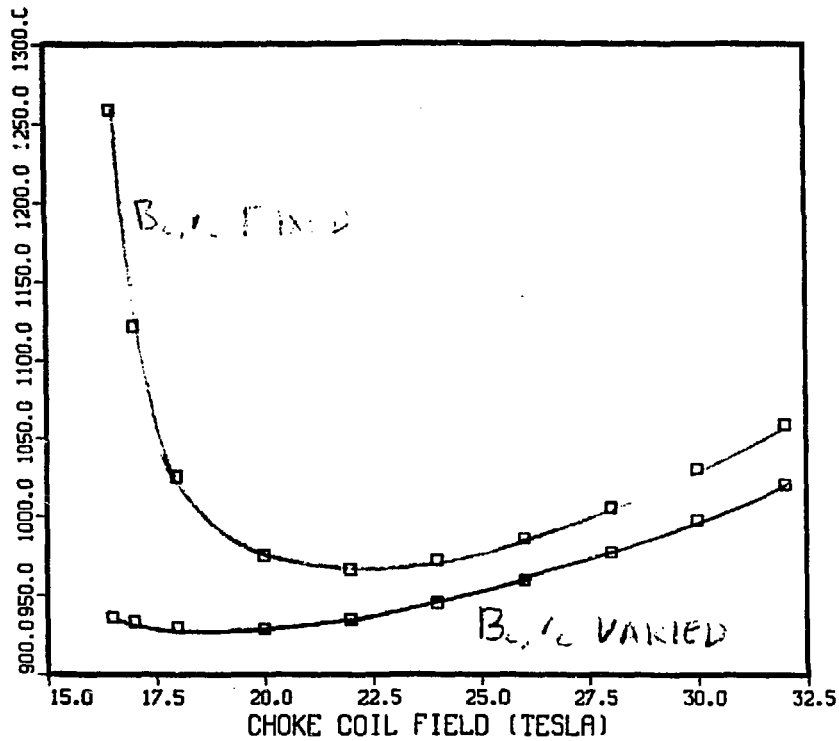
$$P_{THERM} = 2.0 + 0.000 \times P_{NET} \text{ (MW)}$$

$$P_{HEATL} [P_{ELEC}^A + P_{ELEC}^H + P_{ELEC}^{HE} + P_{NE} + P_{OP}]_{ELEC}$$

[Handwritten notes and calculations, including a boxed section with 'K' and other symbols]

YMIN= 0.121 YMAX= 190.4 NET ELECTRIC POWER = 600.0 MW

MINIMARS



YMIN- 929.1

YMAX- 1259.

NET ELECTRIC POWER - 600.0 MW

MINIMARS

1- FIXED

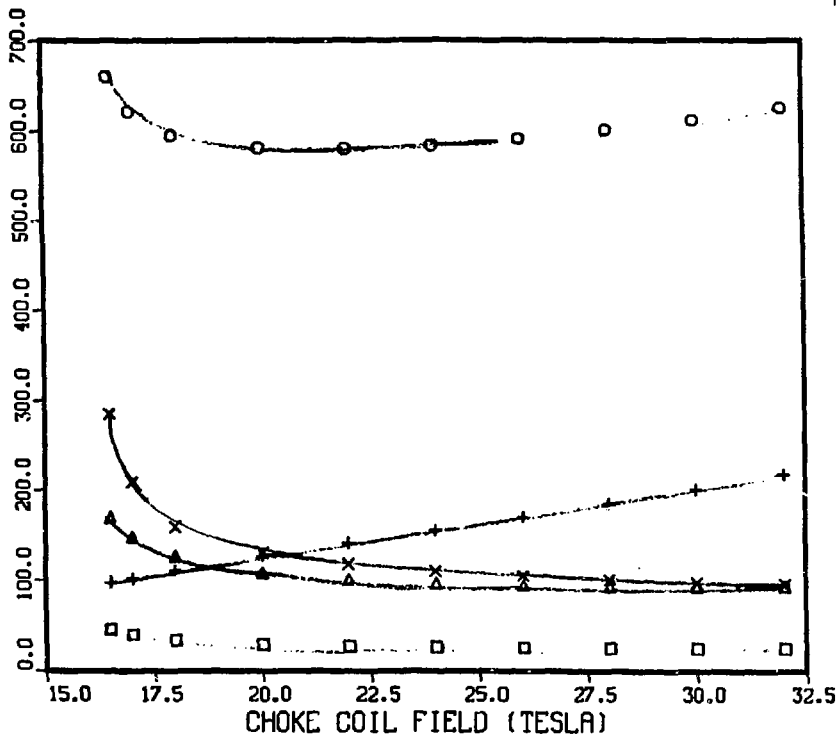
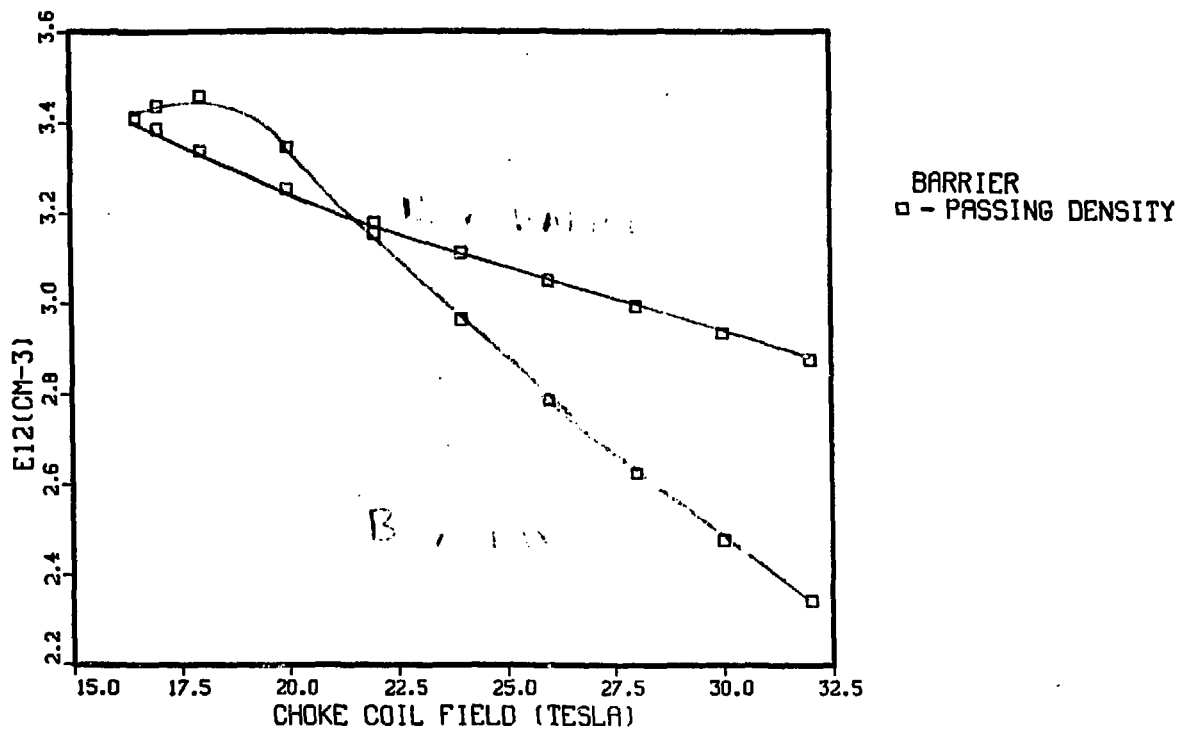


FIGURE OF MERIT
 □ - C.C. MAGNETS
 ○ - C.C. FACILITIES
 ▲ - BLANKET & SHIELD
 + - END CELL
 * - HEATING SYSTEMS

YMIN- 25.18 YMAX- 660.1 NET ELECTRIC POWER - 600.0 MW

MINIMARS



YMIN- 2.343 YMAX- 3.457 NET ELECTRIC POWER - 600.0 MW

MINIMARS SUMMARY DATA FOR FIXED NET ELECTRIC POWER AND WALL LOADING

FUSION POWER, Q, WALL LOADING

| CASE | PNETEL (MW) | PFUS (MW) | PFUS/VCC (MW/M3) | OPHYS | Q | QENGR | GAMMA (MW/M2) |
|-------|----------------|--------------|---------------------|---------|--------|-------|------------------|
| 0113A | 600.000 | 1531.841 | 3.395 | 85.930 | 33.422 | 4.276 | 0.761 |
| 0113 | 600.000 | 1472.281 | 7.169 | 95.688 | 32.474 | 4.641 | 1.249 |
| 0112 | 600.000 | 1591.836 | 11.831 | 249.150 | 70.932 | 4.213 | 1.000 |
| 0110 | 600.000 | 1436.049 | 15.362 | 102.408 | 34.702 | 4.999 | 2.000 |
| 0110 | 600.000 | 1424.346 | 18.999 | 64.665 | 25.815 | 4.779 | 3.000 |
| 0118 | 600.000 | 1454.348 | 21.078 | 44.393 | 20.327 | 4.243 | 4.000 |
| 0117 | 600.000 | 1525.761 | 25.438 | 38.075 | 18.596 | 3.656 | 5.000 |
| 0123G | 2000.000 | 4814.462 | 6.452 | 423.165 | 58.326 | 5.215 | 1.000 |
| 0123E | 2000.000 | 4542.017 | 11.513 | 253.056 | 46.439 | 6.200 | 2.000 |
| 0123D | 2000.000 | 4467.152 | 11.374 | 119.542 | 34.191 | 6.231 | 3.000 |
| 0123B | 2000.000 | 4458.329 | 19.153 | 136.110 | 36.626 | 6.374 | 4.000 |
| 0122B | 2000.000 | 4464.076 | 24.701 | 123.794 | 35.367 | 6.289 | 5.000 |
| 0122F | 2000.000 | 4515.333 | 49.505 | 122.904 | 35.328 | 5.941 | 8.000 |
| 0122H | 2000.000 | 4723.556 | 41.396 | 55.587 | 23.607 | 4.754 | 10.000 |

Power = 2000 MW
 Power = 2000 MW
 Power = 2000 MW

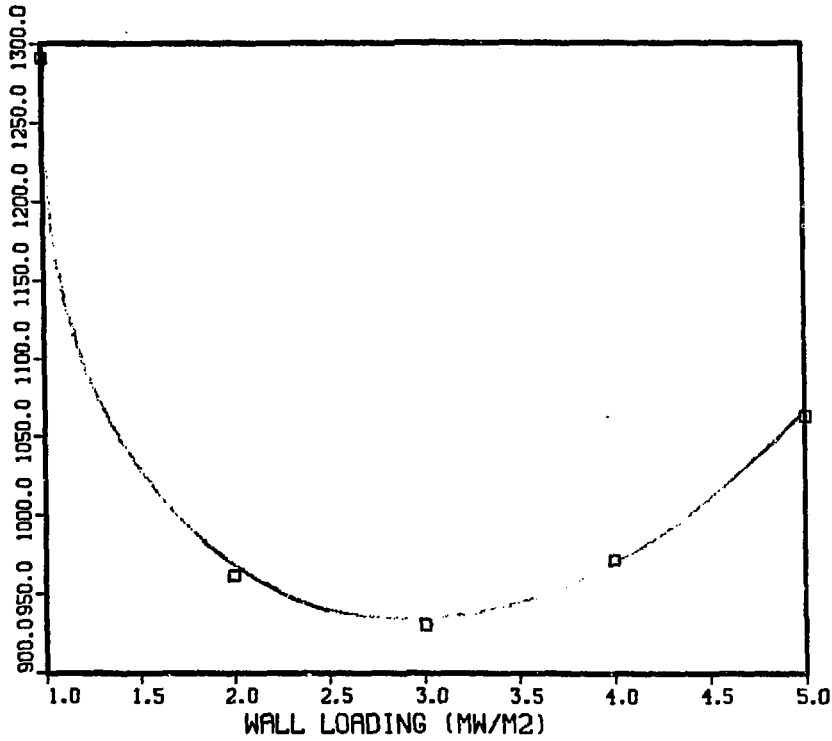
| CASE | CLENGTH (M) | ELACELL (M) | CRADIUS (CM) | RCHOKE (CM) | BBAR (TESLA) | BVAC/0 (TESLA) | ENC E14CM-3 |
|-------|----------------|----------------|-----------------|----------------|-----------------|-------------------|----------------|
| 0113A | 229.844 | 9.273 | 79.051 | 24.698 | 14.861 | 1.668 | 1.467 |
| 0113 | 176.797 | 9.190 | 60.000 | 20.015 | 16.754 | 2.020 | 2.000 |
| 0112 | 348.364 | 8.497 | 35.063 | 13.684 | 16.706 | 2.347 | 2.495 |
| 0110 | 135.998 | 9.205 | 46.776 | 17.169 | 2.654 | 2.654 | 2.518 |
| 0110 | 83.613 | 9.659 | 53.423 | 18.779 | 20.057 | 2.876 | 2.698 |
| 0118 | 58.516 | 10.065 | 61.265 | 20.523 | 22.091 | 3.750 | 2.698 |
| 0117 | 49.755 | 10.217 | 61.945 | 19.826 | 25.924 | 3.042 | 2.985 |
| 0123G | 734.471 | 8.894 | 56.867 | 19.860 | 15.545 | 2.041 | 1.795 |
| 0123E | 354.304 | 9.433 | 59.534 | 20.781 | 17.574 | 2.458 | 2.209 |
| 0123D | 180.823 | 10.298 | 83.149 | 27.167 | 18.587 | 2.502 | 2.130 |
| 0123B | 165.504 | 10.153 | 66.910 | 22.650 | 20.397 | 2.882 | 2.724 |
| 0122B | 138.679 | 10.273 | 64.407 | 21.729 | 21.864 | 3.091 | 3.068 |
| 0122F | 108.027 | 10.266 | 51.842 | 17.158 | 27.280 | 3.698 | 4.301 |
| 0122H | 68.997 | 11.170 | 72.554 | 22.854 | 28.221 | 3.717 | 3.754 |

Power = 600 MW
 Power = 2000 MW

| CASE | TC (KEV) | TEC (KEV) | BETAB | PINJMW (MW) | PABSMW (MW) | CALPH | SLOSH |
|-------|-------------|--------------|-------|----------------|----------------|-------|-------|
| 0113A | 19.362 | 17.213 | 0.330 | 45.834 | 17.827 | 0.032 | 1.184 |
| 0113 | 20.001 | 17.334 | 0.330 | 45.338 | 15.386 | 0.030 | 1.255 |
| 0112 | 22.001 | 19.807 | 0.330 | 22.442 | 6.389 | 0.040 | 1.381 |
| 0110 | 20.429 | 21.730 | 0.330 | 41.002 | 14.012 | 0.037 | 1.384 |
| 0110 | 31.326 | 21.593 | 0.330 | 55.175 | 22.026 | 0.034 | 1.465 |
| 0118 | 34.789 | 23.795 | 0.330 | 71.548 | 32.761 | 0.029 | 1.527 |

Power = 600 MW

MINIMARS



YMIN- 930.3

YMAX- 1291.

NET ELECTRIC POWER - 600.0 MW

MINIMARS

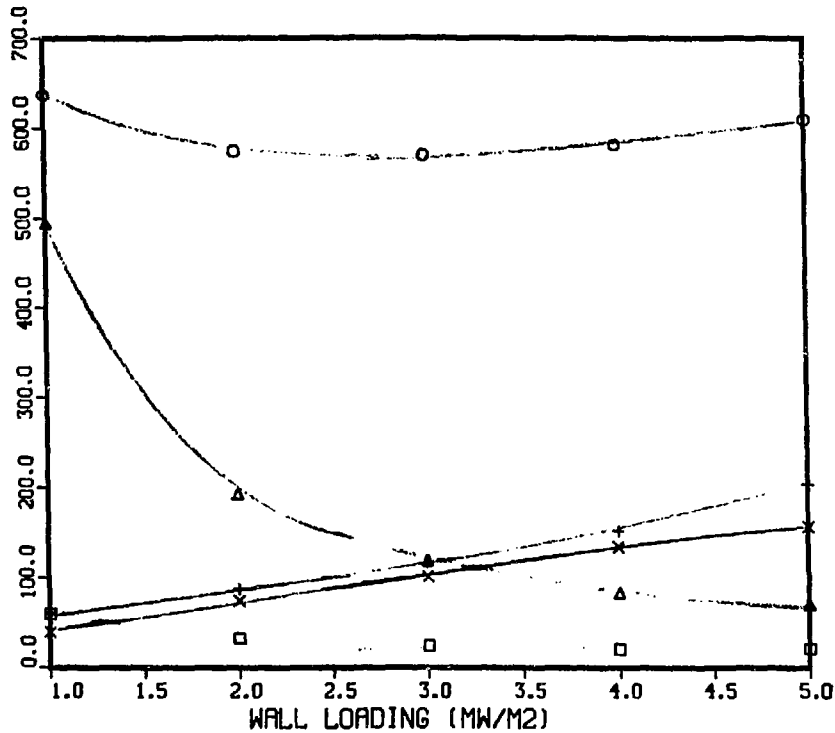


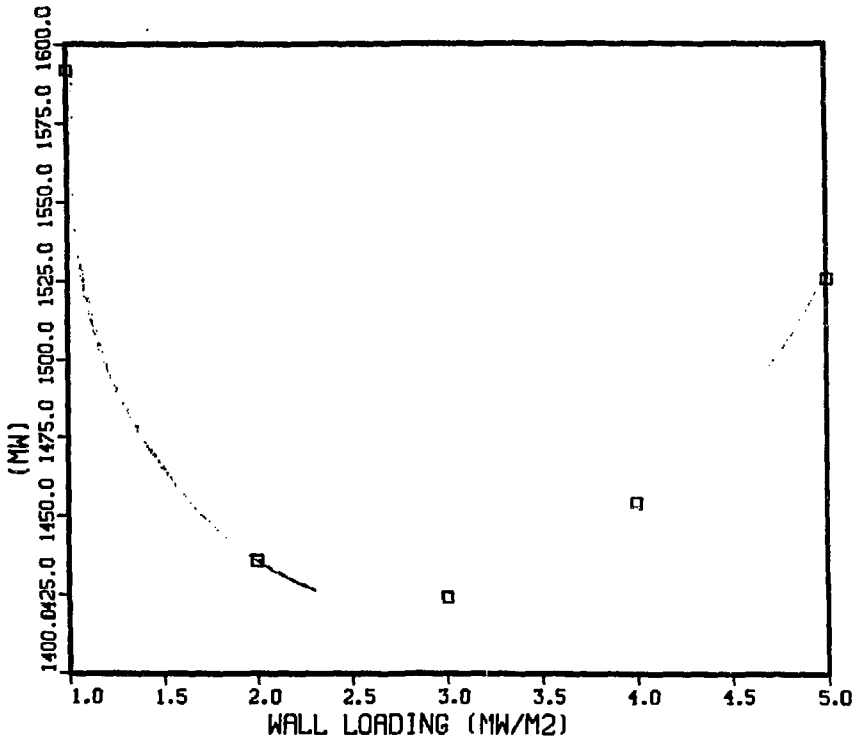
FIGURE OF MERIT
 □ - C.C. MAGNETS
 ○ - C.C. FACILITIES
 △ - BLANKET & SHIELD
 + - END CELL
 * - HEATING SYSTEMS

YMIN= 20.42

YMAX= 636.7

NET ELECTRIC POWER = 600.0 MW

MINIMARS

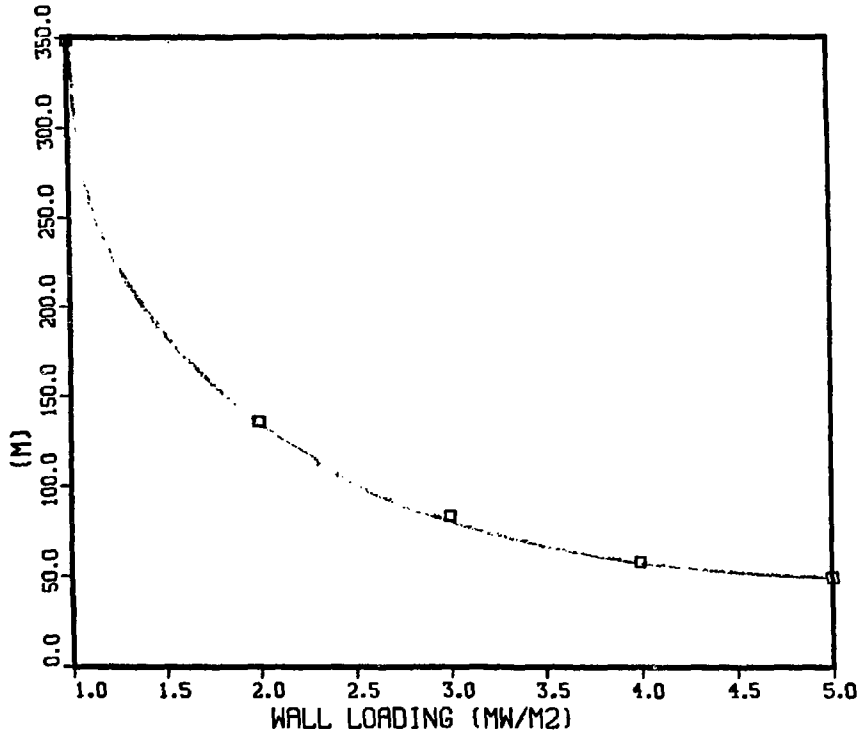


YMIN- 1424.

YMAX- 1592.

NET ELECTRIC POWER - 600.0 MW

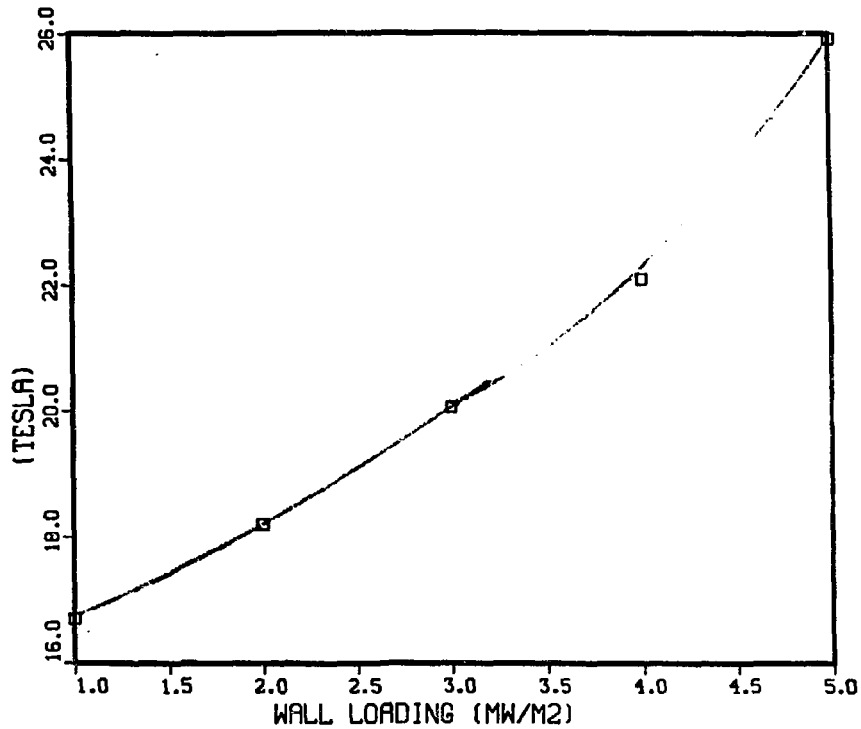
MINIMARS



CENTRAL CELL
⊕ - LENGTH

YMIN- 49.75 YMAX- 348.4 NET ELECTRIC POWER - 600.0 MW

MINIMARS

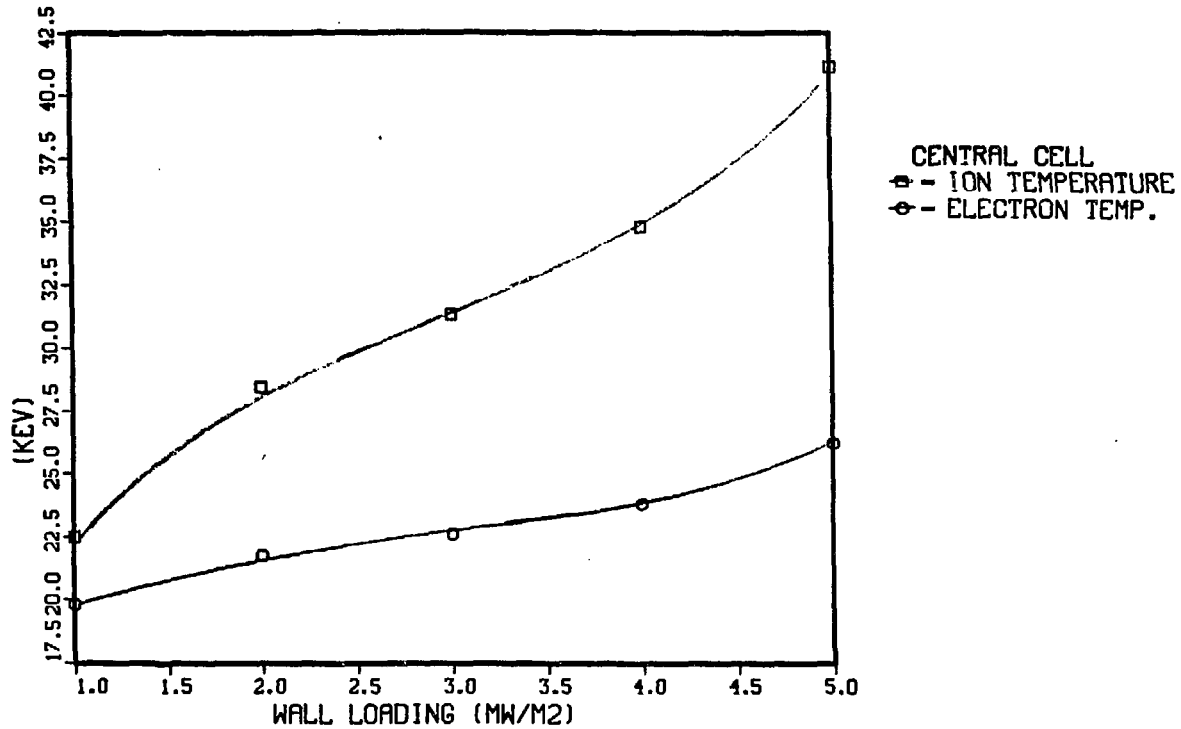


YMIN- 16.71

YMAX- 25.92

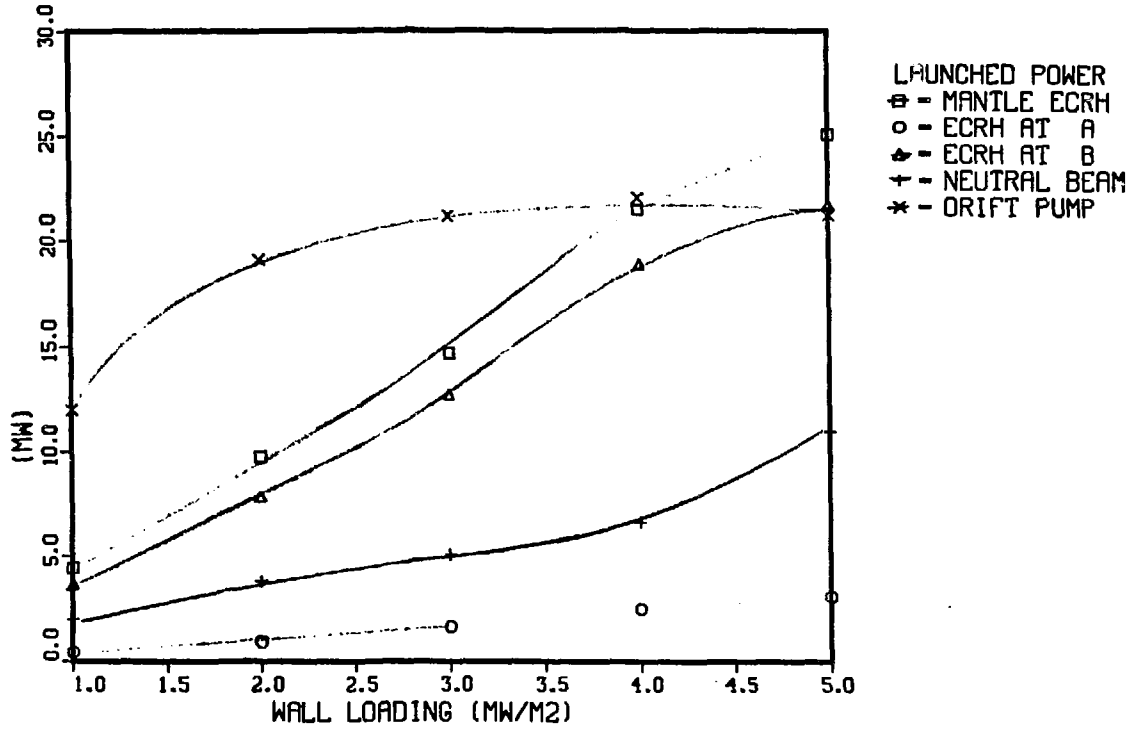
NET ELECTRIC POWER - 600.0 MW

MINIMARS



YMIN- 19.81 YMAX- 41.16 NET ELECTRIC POWER - 600.0 MW

MINIMARS

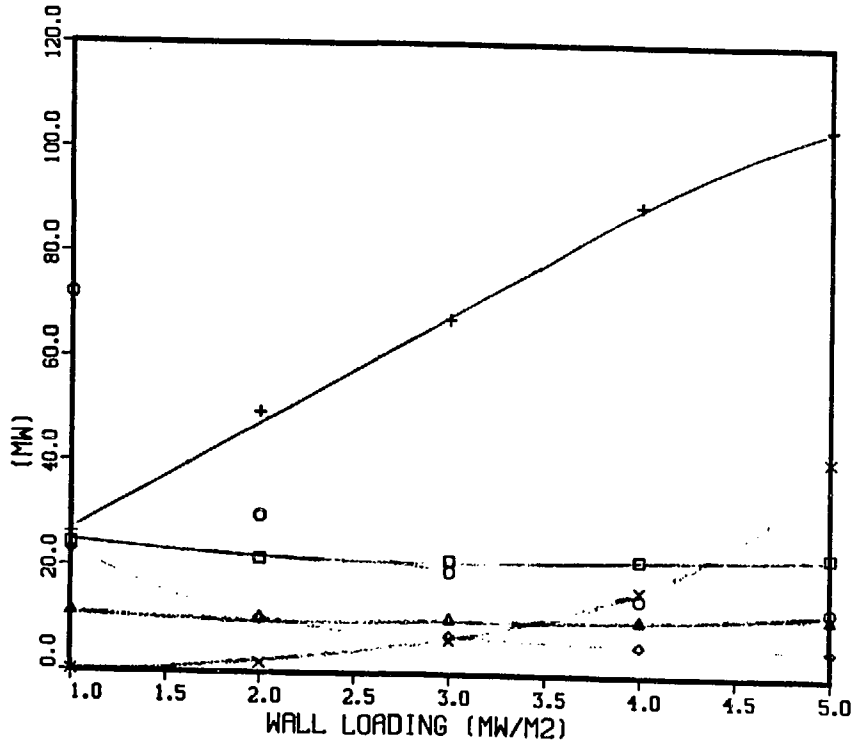


YMIN- 0.423

YMAX- 25.08

NET ELECTRIC POWER - 600.0 MW

MINIMARS



- POWER
- - AUXILIARY PUMPS
 - - CRYOGEN SYSTEM
 - ▲ - FUELING SYSTEM
 - + - HEATING SYSTEMS
 - * - MAGNET SUPPLIES
 - ◇ - PLANT FACILITY

$$P_{HEAT} = 2.0 + .017 \times P_{TOT} \text{ (MW)}$$

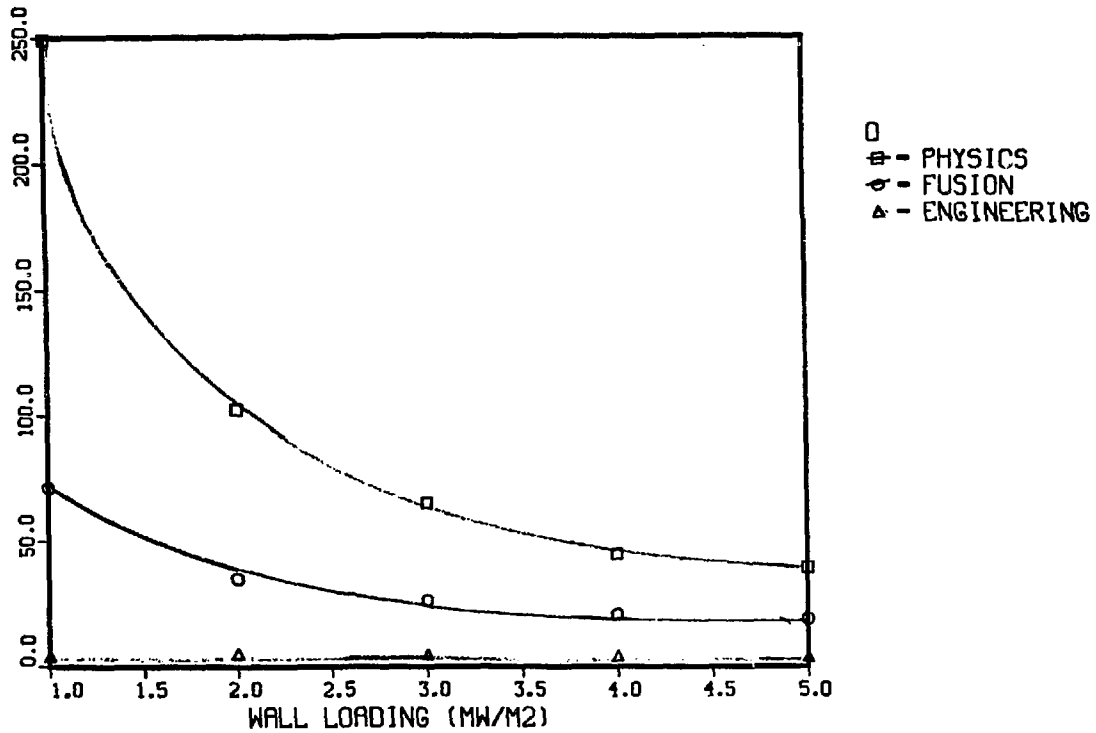
$$P_{ELEC} = 2.0 + .006 \times P_{TOT} \text{ (MW)}$$

$$P_{HEAT} = [P_{HEAT}^A + P_{HEAT}^B + P_{HEAT}^C + P_{HEAT}^D + P_{HEAT}^E]_{ELEC}$$

YMIN- 0.144 YMAX- 104.6 NET ELECTRIC POWER - 600.0 MW

1.0 () ()

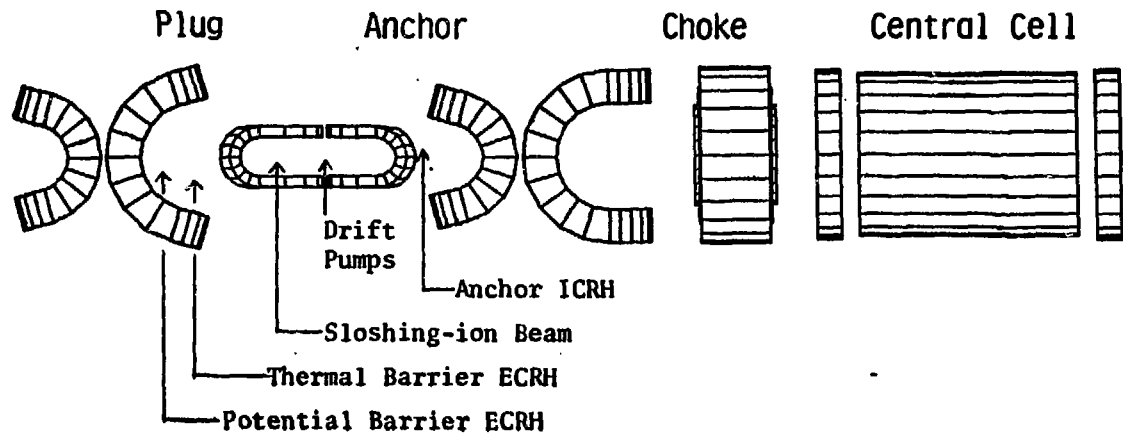
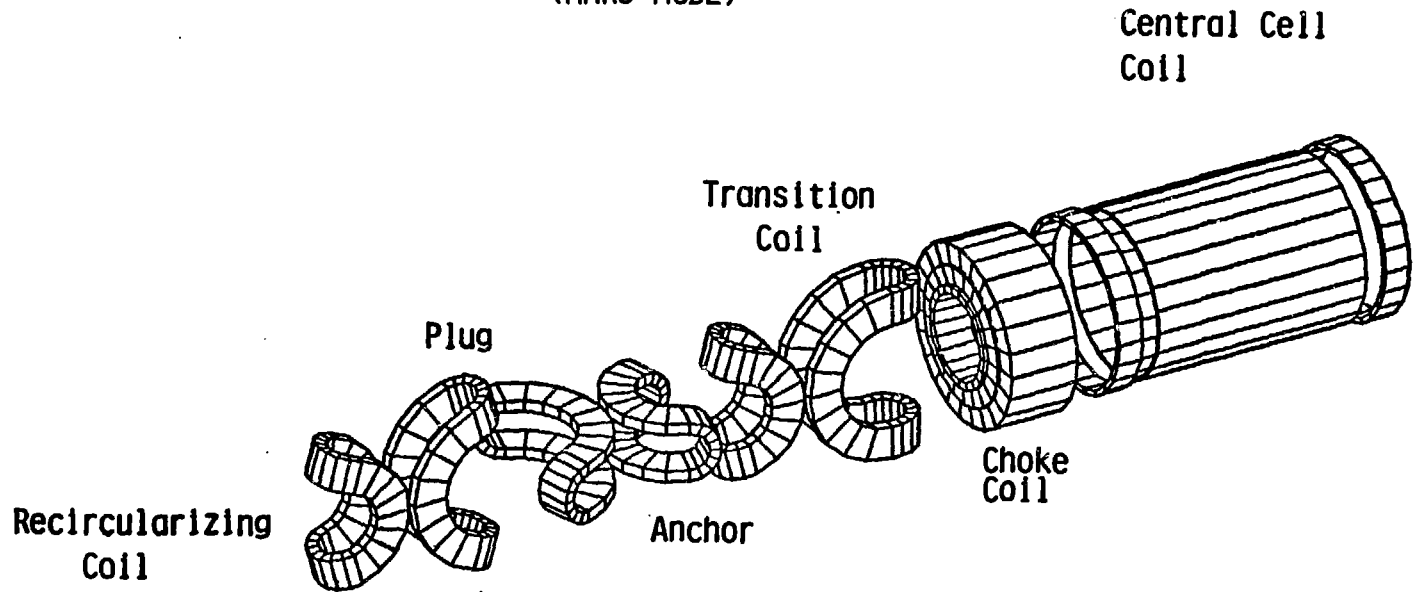
MINIMARS



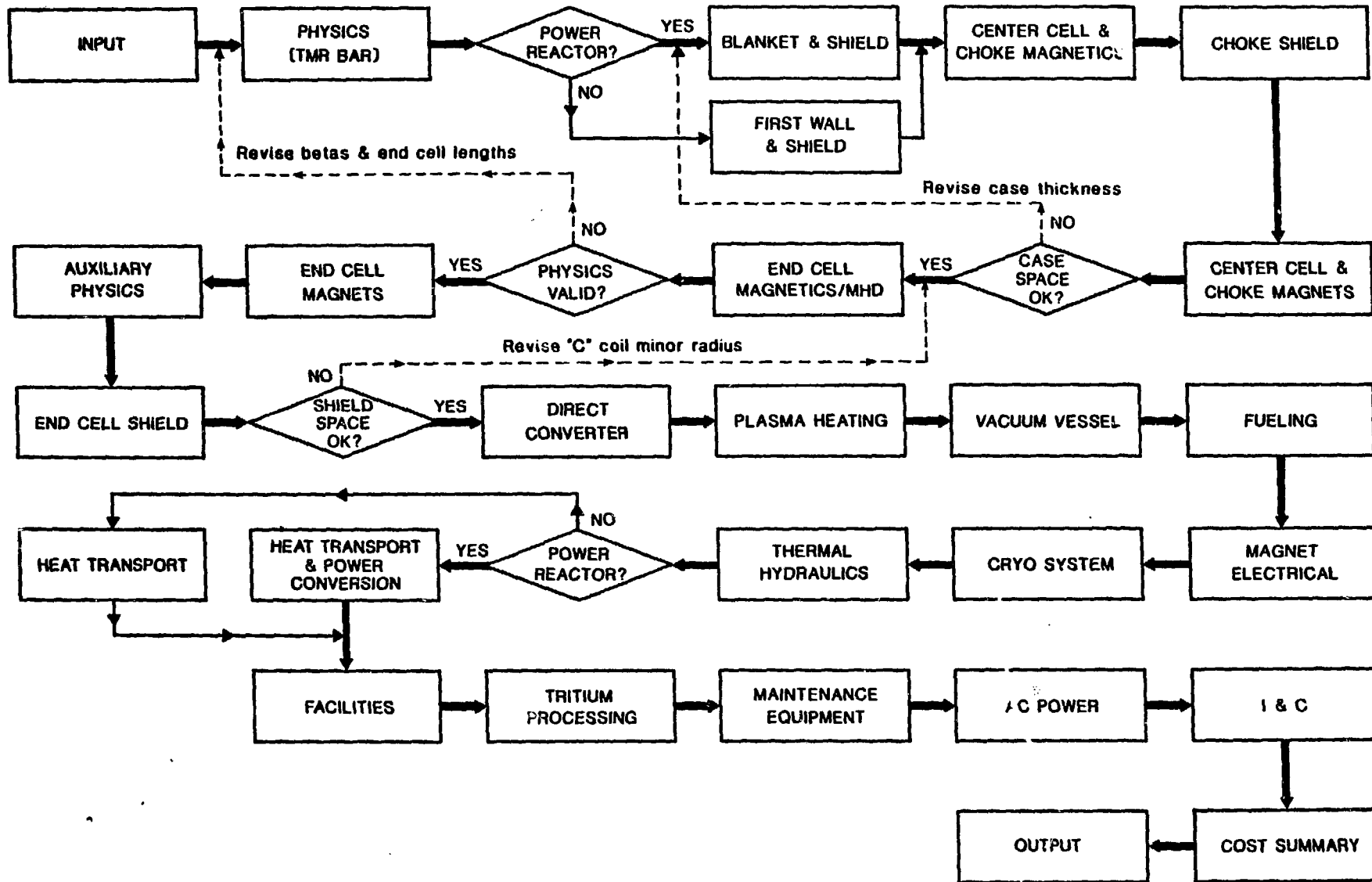
YMIN- 3.656 YMAX- 249.2 NET ELECTRIC POWER - 600.0 MW



FPD-II TYPE QUADRUPOLE MAGNET SET
(MARS-MODE)



TANDEM MIRROR REACTOR SYSTEMS CODE FLOW DIAGRAM





EXAMPLE CODE EXECUTION

Costs

Case 1

Case 2

| | | |
|--------------------------|------------|------------|
| Blanket | 30.3 | 29.4 |
| Shield | 65.5 | 61.9 |
| Choke Shield | 4.0 | 4.2 |
| Magnets | 175.4 | 167.0 |
| End Cell Shield | 2.5 | 3.8 |
| Direct Convertor | 5.2 | 3.9 |
| Plasma Heating | 65.8 | 75.0 |
| Fueling | 6.3 | 7.6 |
| Magnet Electrical | 12.8 | 12.5 |
| Cryoplant | 81.8 | 90.5 |
| Main Heat Transport | 96.1 | 97.2 |
| Auxiliary Heat Transport | 17.8 | 20.0 |
| Power Conversion | 99.6 | 99.7 |
| Facilities/equipment | 287.3 | 283.7 |
| Fuel Processing | 218.4 | 218.6 |
| Maintenance Equipment | 66.2 | 66.0 |
| AC Power | 26.9 | 28 |
| I&C | 64.3 | 64.2 |
| Vacuum Vessel | 98.7 | 80.2 |
| | <hr/> | <hr/> |
| | 1424.9 M\$ | 1413.4 M\$ |



EXAMPLE CODE EXECUTION

Parameters

| | <u>Case 1</u> | <u>Case 2</u> |
|------------------------------|---------------|---------------|
| Fusion Power (mw) | 1000 | 1000 |
| R_{CHOKE} (m) | 0.14 | 0.16 |
| R_{PLASMA} (m) | 0.46 | 0.53 |
| L_{CC} (m) | 124.1 | 111.9 |
| β_{CC} | 0.60 | .583 |
| Ti (keV) | 29.0 | 32.0 |
| Plasma Heating (mw) | 25.9 | 32.7 |
| W_L (mw/m ²) | 1.52 | 1.53 |
| Δ_B (m) | 0.7 | 0.7 |
| Δ_S (m) | 0.74 | 0.75 |
| $\Delta_{S \text{ Bio}}$ (m) | 1.52 | 1.53 |
| $P_e \text{ net}$ | 388 | 366 |
| Q | 3.44 | 2.91 |

BASIC 14 PHYSICS VARIABLES:

| | |
|--|----------------------------|
| (1) Transition Plasma B field | BPLAOT |
| (2) B_{ro} Plasma B field | BPI |
| (3) B_a Peak Plasma B Field | BPLAOA |
| (4) $g = (n_{pass} + n_{trap})/n_{pass}$ | XLILG |
| (5) $g_{\alpha} = (n_{pass,\alpha} + n_{trap,\alpha})/n_{pass,\alpha}$ | XLILGA |
| (6) Transition Potential | ETAT = ϕ_t/T_{ec} |
| (7) Geodesic Curvature Potential Maximum | ETAPI = ϕ_{ro}/T_{ec} |
| (8) Sloshing Ion Point Potential | ETAAP = ϕ_a'/T_{ec} |
| (9) Barrier Potential | ETAB = ϕ_b/T_{ec} |
| (10) Inboard Mirror Peak Potential | ETAMP = ϕ_{mp}/T_{ec} |
| (11) Central Cell Ion Confining Potential | ETAC = ϕ_c/T_c |
| (12) Central Cell Electron Temperature | TEC |
| (13) Central Cell Alpha Fraction | CALPH C_{α} |
| (14) Central Cell Floating Potential | ETAe = ϕ_e/T_{ec} |

OPTIONAL/OPTIMIZATION VARIABLES

| | |
|---|-------------------|
| (15) Central Cell Length | CLENGTH |
| (16) Central Cell Ion Temperature | TC |
| (17) Central Cell Radius | CRADIUS |
| (18) Barrier Beta | BETAB |
| (19) Warm electron heating point mirror ratio | SLOSH = B_a/B_b |
| (20) Central Cell Vacuum B field | BVACOC |
| (21) Choke Coil Vacuum B field | BBAR |
| (22) $\bar{E}_{hot} - T_{e,warm}$ | DELTEW |

NOTE: variables may have upper/lower bounds

any physics input constant may be changed into a variable



BASIC 14 PHYSICS CONSTRAINTS

- (1) $B_{\text{plasma},t} = B_{\text{vac.},t} (1 - \beta_t)^{1/2}$ (transition)
- (2) $B_{\text{plasma},c} = B_{\text{vac.},c} (1 - \beta_c)^{1/2}$ (geodesic curvature maximum)
- (3) $B_{\text{plasma},a} = B_{\text{vac.},a} (1 - \beta_a)^{1/2}$ (potential peak)
- (4) Global Charge Balance
- (5) Alpha Particle Balance
- (6) Quasi-neutrality in Transition (t)
- (7) Quasi-neutrality at Geodesic Curvature Maximum (c)
- (8) Quasi-neutrality at Sloshing Ion Injection Point (a')
- (9) Quasi-neutrality at Thermal Barrier (b)
- (10) Quasi-neutrality at Inboard Plug Mirror Peak (mp)
- (11) Quasi-neutrality in the Central Cell (c)
- (12) Electron Energy Balance
- (13) Ion Trapping Rate in (b), (t) = Removal Rate
- (14) Ion Energy Balance

OPTIONAL EXTERNAL CONSTRAINTS

- (15) Fixed Net Electric Power
- (16) Fixed Wall Loading
- (17) $\Delta T \geq \bar{E}_{\text{hot}} - T_{e,\text{warm}}$

MINISYSTEMS CODE

0 OBJECTIVE

MINIMIZE A USER-SPECIFIED SYSTEM FIGURE OF MERIT BY VARIATION OF UP TO 22 PLASMA ENGINEERING PARAMETERS SUBJECT TO A USER-SPECIFIED SET OF CONSTRAINTS.

0 RELATIONSHIP TO THE FULL TMRSC:

RUNS IN OPTIMIZATION MODE TO EXPLORE PLASMA ENGINEERING PARAMETER SPACE IN A SINGLE RUN. REQUIREMENTS ARE TO (A) OBTAIN REASONABLE OBJECTIVE PARAMETER BASELINES IN THE FIRST FEW MONTHS OF THE STUDY AND (B) PROVIDE A BASIS FOR SINGLE POINT RUNS OF THE FULL CODE WHEN AVAILABLE.

0 FIGURES OF MERIT FOR MINIMIZATION:

1. TOTAL SYSTEM CAPITAL COST
2. CENTRAL CELL IGNITION LENGTHS (USEFUL FOR IGNITION ETR'S)
3. TOTAL PLUG ECRH POWER
4. OTHERS-----?



"TMRBAR" POWER BALANCE CODE FOR TANDEM MIRROR REACTORS

General

- Coupled, multi-region, zero dimensional power balance code.
- Configured for (a) MARS (quadrupole) mode and (b) TARA/MINIMARS (octupole-Axisymmetric) mode.
- Outputs include plasma parameters (densities temperatures, potentials, absorbed powers, etc.) and system engineering power balance parameters (recirculating powers, thermal powers, etc.)

Central Cell Physics

- Fuel ion particle/energy balance.
- Electron energy balance.
- Alpha particle balance.
- Global charge balance.
- Hot alpha prompt losses:
 - (a) Non-adiabaticity
 - (b) FLR losses to halo.
- Pressure balance.

OPTIMIZATION PROCEDURE

(1) Find Feasible Starting Point

- Solve 14 nonlinear physics constraint equations.
May fix T_c , central cell length or fusion power if no external constraints are used.
- Solve using a modified Newton's method:
Plug warm electron temperature equation.
Minimization of mantle ECRH vs. mantle hot electron energy.
- Solve optional external constraints.
Fixed net electric power.
Fixed wall loading.
Fixed $\Delta T = (\bar{E}_{\text{hot}} - T_{e,\text{warm}})$

(2) Select Optimization Function

- May minimize or maximize any combination of physics variables.
For example:
Minimize cost figure of merit.
Minimize neutral beam power.
Minimize total rf power.
Minimize central cell length.
Maximize fusion power.
Maximize wall loading.

OPTIMIZATION PROCEDURE (con't)

(3) If Optimization Finds an Infeasible Point

- Attempts to find a feasible point using all physics and external constraints.
If unsuccessful, reduces the number of constraints by 1 until a solution is found or the number of constraints < 14

(4) Output From Both Starting and Final Points is Stored

- Formatted output file is created.
- Namelist file created.
Can be used as the input file for the next run.
- Namelist file created for plotting.
Can combine this file with previous run files and plot the cumulative results using a separate plotting code and make a summary output file.
- Output file created.
Contains physics variables and constraint equations values for each iteration to be plotted if iteration diagnostic information is required.



COST FIG. OF MERIT IN CURRENT USE

$$\text{F.O.M} = \underbrace{C_1 B_C^2 L_C r_{C,\text{mag}}^2}_{\substack{\text{C. Cell} \\ \text{Magnets}}} + \underbrace{C_2 L_C}_{\substack{\text{C. Cell} \\ \text{blnkt. \& Build-} \\ \text{shield} \quad \text{ing}}} + \underbrace{C_3 L_C}_{\text{B.O.P.}} + \underbrace{C_4 P_{\text{fusion}}}_{\text{B.O.P.}}$$

$$+ \underbrace{C_5 B^2_{\text{end cell}} V_{\text{end cell}}}_{\substack{\text{choke coil and end cell} \\ \text{magnets}}} + \underbrace{C_6 P_{\text{heat., wall plug}}}_{\substack{\text{Plasma Heating} \\ \text{Systems}}}$$

$$r_{C,\text{mag}} = r_C + r_{\text{halo}} + r_{\text{blnkt}} + r_{\text{shield}}$$

$$B_{\text{end cell}} = (B_{\text{choke}} + B_{\text{outer mirror}})/2$$

$$V_{\text{end cell}} = r_{\text{outer mirror}}^2 L_{\text{end cell}}$$

$$C_1 = 7.19 \times 10^{-3} \text{ M\$ T}^{-2} \text{ m}^{-3}$$

$$C_2 = 0.93 \text{ M\$ m}^{-1}$$

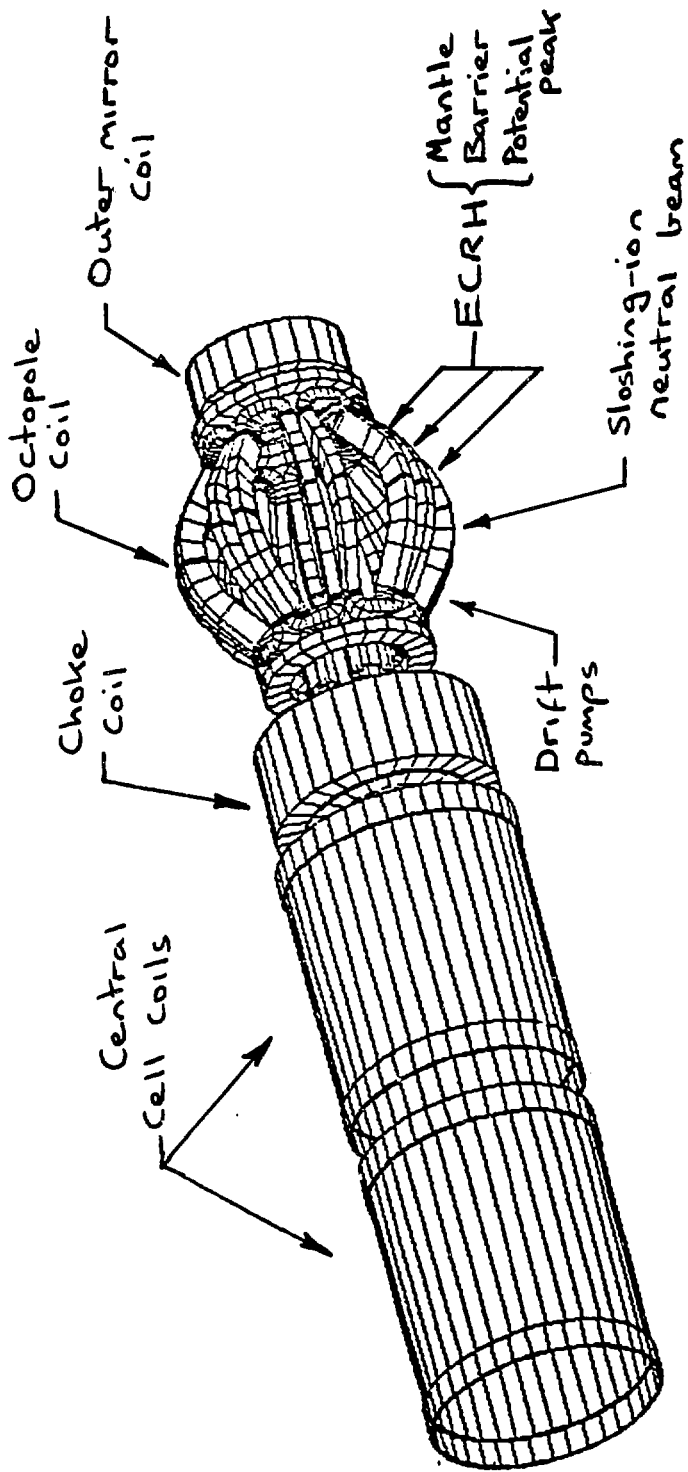
$$C_3 = 0.5 \text{ M\$ m}^{-1}$$

$$C_4 = 0.4 \text{ M\$/MW}_{\text{fusion}}$$

$$C_5 = 2.67 \times 10^{-2} \text{ M\$ T}^{-2} \text{ m}^{-3}$$

$$C_6 = 1.5 \text{ M\$ 1MW}_{\text{wall plug}}$$

OCTOPOLE (MINIARS-MODE) MAGNET SET



OCTOPOLE VERSUS QUADRUPOLE END PLUGS
- A COMPARISON OF MARS AND MINIMARS

ADVANTAGES

- 0 SHORTER END CELL MAGNET LENGTHS:
 - SHORTER CENTRAL CELL LENGTHS FOR IGNITION; SMALLER REACTOR SIZES.
 - CHEAPER, MORE COMPACT, END CELL MAGNET CONFIGURATION.

- 0 SIMPLE MIRROR CONFIGURATION WITH (NEARLY) AXISYMMETRIC* MAGNETIC FLUX BUNDLE IN END CELL:
 - REDUCED RADIAL DRIFTS.
 - SIMPLIFIED CORE PLASMA POWER BALANCE COMPUTATION - ONLY ONE END-CELL MIRROR REGION.

*CORE PLASMA ONLY; MANTLE IS NON-AXISYMMETRIC.

DISADVANTAGES

- 0 ACCESS PROBLEMS IN COMPACT END PLUG (INTEGRATION OF SEVEN MAJOR SUBSYSTEMS)

- 0 HOT ELECTRON MANTLE WITH ADDITIONAL ECRH SYSTEM REQUIRED IN END CELL.

- 0 OCTOPOLE MAGNET HAS COMPLEX WINDING GEOMETRY AND CONSTRUCTION.

- 0 AXISYMMETRY MAKES DRIFT PUMPING OF TRAPPED IONS MORE DIFFICULT.

MACHINE BASELINES BASED ON PRELIMINARY
TRADE STUDIES WITH MINI-SYSTEMS CODE

BASIS: MINIMIZATION OF COST FIGURE OF MERIT SUBJECT TO 600
MW_E FIXED NET ELECTRIC POWER.

| | <u>20 T</u> | <u>BCHOKE</u> <u>22 T</u> | <u>24 T</u> |
|------------------------------------|-------------|------------------------------|-------------|
| <u>GENERAL</u> | | | |
| NET ELECTRIC POWER, MW | 600 | 600 | 600 |
| FUSION POWER, MW | 1423 | 1430 | 1443 |
| Q | 68 | 77 | 86 |
| COLD DT FUELING CURRENT, KA | 1.12 | 1.12 | 1.11 |
| <u>CENTRAL CELL</u> | | | |
| L _C ·M | 87.7 | 85.4 | 84.3 |
| B _C ·T | 2.77 | 2.88 | 2.99 |
| <B _C > | 0.6 | 0.6 | 0.6 |
| R _C ·M | 0.553 | 0.520 | 0.490 |
| R _{WALL} ·M | 0.748 | 0.707 | 0.671 |
| B, MW/M ² | 2.76 | 3.00 | 3.25 |
| <u>CHOKE COIL</u> | | | |
| B _{CHOKE} | 20 | 22 | 24 |
| B _{S/C} ·T | 16 | 16 | 16 |
| B _{INSERT} ·T | 4 | 6 | 8 |
| P _{INSERT} *·MW | ~6.44 | ~13.2 | ~21.6 |
| <u>END PLUG</u> | | | |
| B _{PLUG} | 0.33 | 0.33 | 0.33 |
| B _{MANTLE} | 0.9 | 0.9 | 0.9 |
| END PLUG* MIRROR LENGTH·M | 9.58 | 9.45 | 9.32 |
| PLUG MINIMUM FIELD* T | 1.5 | 1.5 | 1.5 |
| MANTLE MINIMUM FIELD*·T | 1.4 | 1.4 | 1.4 |
| <u>ABSORBED POWERS - BOTH ENDS</u> | | | |
| P _{NB} ·MW | 0.672 | 0.597 | 0.533 |
| F _{TRAP} | 0.140 | 0.133 | 0.127 |
| P _{ECRH-A} ' MW | 1.10 | 0.955 | 0.835 |
| P _{ECRH-B} ' MW | 7.97 | 7.08 | 6.28 |
| P _{ECRH-M} ' MW | 11.1 | 10.1 | 9.15 |
| TOTAL INJECTED POWER | 20.8 | 18.7 | 16.8 |